# One dimensional Burgers' equation

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# 1 Non-linear Burgers' equation

We consider the non-linear viscous Burgers' equation

$$w_t - \nu w_{xx} + w w_x = f_s \qquad \text{in} \quad (0, 1) \times (0, \infty)$$
 (1)

with boundary conditions

$$w(0,t) = u_s, w_x(1,t) = g_s (2)$$

and initial condition

$$w(x,0) = w_0(x) \tag{3}$$

### 1.1 Stationary Burgers' equation

The stationary Burgers' equation is given by

$$-\nu w_{xx} + ww_x = f_s \qquad \text{in} \quad (0,1) \tag{4}$$

with boundary conditions

$$w(0) = u_s, \qquad w_x(1) = g_s \tag{5}$$

An unstable stationary solution can be obtained as

$$w_s = -\frac{\nu\pi}{2}(1+\epsilon)\tan\left(\frac{\pi}{4}(1+\epsilon) + C_0\right) \tag{6}$$

with the conditions

$$0 < \epsilon < 1,$$
  $-\frac{\pi}{4} < C_0 < 0,$   $(1 + \epsilon) \tan \left(\frac{\pi}{4}(1 + \epsilon) + C_0\right) = 1$ 

We choose

$$\epsilon = 0.6$$
  $\Longrightarrow$   $C_0 = \arctan(1/(1+\epsilon)) - \frac{\pi}{4}(1+\epsilon) = -0.69803774609235$ 

# 2 Nonlinear system without control

We set  $z = w - w_s$ . The equation satisfied by z is

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} + z \frac{\mathrm{d}z}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} \quad \text{in} \quad (0, 1) \times (0, \infty)$$
 (7)

with boundary conditions

$$z(0,t) = 0,$$
  $z_x(1,t) = 0$  (8)

and initial conditions

$$z(x,0) = w_0(x) - w_s(x) (9)$$

We multiply by a test function  $\phi$  with  $\phi(0) = 0$  to obtain the weak formulation

$$\int_0^1 z_t \phi dx + \nu \int_0^1 \frac{\partial z}{\partial x} \frac{d\phi}{dx} dx + \int_0^1 w_s \frac{\partial z}{\partial x} \phi dx + \int_0^1 z \frac{\partial w_s}{\partial x} \phi dx + \int_0^1 z \frac{dz}{dx} \phi dx = 0$$

Divide domain into N elements with vertices

$$0 = x_0 < x_1 < \dots < x_N = 1, \qquad x_i = ih, \qquad h = \frac{1}{N}$$

The finite element solution can be written as

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x)$$

while the stationary solution expressed as

$$w_s(x) = \sum_{i=1}^{N} w_s^j \phi_j(x) + u_s \phi_0(x)$$

where  $w_s^j = w_s(x_j)$ . Here the  $\{\phi_j\}$  are the usual  $P_1$  basis functions. The approximate weak formulation is

$$\int_{0}^{1} z_{t} \phi_{i} dx = -\nu \int_{0}^{1} \frac{\partial z}{\partial x} \frac{d\phi_{i}}{dx} dx - \int_{0}^{1} w_{s} \frac{\partial z}{\partial x} \phi_{i} dx - \int_{0}^{1} z \frac{\partial w_{s}}{\partial x} \phi_{i} dx$$
$$- \int_{0}^{1} z \frac{dz}{dx} \phi_{i} dx, \qquad \forall i = 1, 2, ..., N$$

or

$$\sum_{j=1}^{N} z'_{j}(t) \int_{0}^{1} \phi_{i} \phi_{j} dx = -\sum_{j=1}^{N} \sum_{k=1}^{N} z_{j}(t) z_{k}(t) \int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx 
- \sum_{j=1}^{N} z_{j}(t) \left[ \nu \int_{0}^{1} \phi'_{i} \phi'_{j} dx + u_{s} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{j})' dx \right] 
- \sum_{j=1}^{N} z_{j}(t) \left[ \sum_{k=1}^{N} w_{s}^{k}(t) \left( \int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx + \int_{0}^{1} \phi_{k} \phi'_{j} \phi_{i} dx \right) \right]$$

We use the following notations:

- $\mathbf{z} = [z_1, z_2, ..., z_N]^{\top}$
- $\mathbf{w}_s = [w_s^1, w_s^2, ..., w_s^N]^{\top}$
- $\mathbf{M} \in \mathbb{R}^{N \times N}$  with  $\mathbf{M}(i, j) = \int_0^1 \phi_i \phi_j \mathrm{d}x$
- $\mathbf{A}1 \in \mathbb{R}^{N \times N}$  with  $\mathbf{A}1(i,j) = \int_0^1 \phi_i' \phi_j' dx$
- $\mathbf{A}2 \in \mathbb{R}^{N \times N}$  with  $\mathbf{A}2(i,j) = \int_0^1 \phi_i(\phi_0 \phi_j)' \mathrm{d}x$
- $\mathbf{D}1 \in \mathbb{R}^{N \times N \times N}$  with  $\mathbf{D}1(i, j, k) = \int_0^1 \phi_i \phi_j' \phi_k dx$

Thus we have a non-linear system of first order ODEs in z

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{R}\mathbf{H}\mathbf{S}$$

where

$$\mathbf{RHS}(i) = -\mathbf{z}^{\top}\mathbf{D}1(:,:,i)\mathbf{z} - \left[\nu\mathbf{A}1(i,:) + u_s\mathbf{A}2(i,:) + \mathbf{w}_s^{\top}(\mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top})\right]\mathbf{z}$$

This is implemented and solved in burger.m

Warning It is not good computational practice to compute the three dimensional matrices like **D**1 since it requires large storage. But we will use this approach here since we are only in 1-D case.

#### 2.1 Excercises

1. The initial condition is chosen as

$$z(x,0) = \delta \sin(\pi x/2)$$

Run program burger.m with delta = 0. The zero solution does not change with time. This corresponds to the stationary solution for the original Burgers's equation.

2. Take different initial conditions by varying delta, and convince yourself that the zero solution is unstable. Try delta = 0.1 and delta = -0.1 and see how the solution evolves.

# 3 Linearized Burgers' equation

### 3.1 Feedback control

Consider the linearized equation

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} \tag{10}$$

$$z(0,t) = u(t), \qquad \frac{\partial z}{\partial x}(1,t) = 0 \tag{11}$$

$$z(x,0) = w_0(x) - w_s(x)$$
(12)

The weak formulation is given by

$$\int_0^1 \left( \frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} \right) \phi \mathrm{d}x = -\nu \int_0^1 \frac{\partial z}{\partial x} \frac{\partial \phi}{\partial x} \mathrm{d}x$$

We look for a finite element solution of the form

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x) + u(t)\phi_0(x)$$

The approximate weak formulation is

$$\int_0^1 \left( \frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} \right) \phi_i \mathrm{d}x = -\nu \int_0^1 \frac{\partial z}{\partial x} \frac{\partial \phi_i}{\partial x} \mathrm{d}x, \qquad i = 1, 2, \dots, N$$

Ignoring the  $\frac{du}{dt}$  term gives us

$$\sum_{j=1}^{N} \frac{\mathrm{d}z_j}{\mathrm{d}t} \int_0^1 \phi_i \phi_j \mathrm{d}x = \sum_{j=1}^{N} z_j \left[ -\nu \int_0^1 \phi_i' \phi_j' \mathrm{d}x - \int_0^1 w_s \phi_i \phi_j' \mathrm{d}x - \int_0^1 \phi_i \phi_j \frac{\mathrm{d}w_s}{\mathrm{d}x} \right]$$
$$+ u \left[ -\int_0^1 w_s \phi_i \phi_0' \mathrm{d}x - \int_0^1 \phi_i \phi_0 \frac{\mathrm{d}w_s}{\mathrm{d}x} \mathrm{d}x - \nu \int_0^1 \phi_i' \phi_0' \mathrm{d}x \right]$$

Using the expression for  $w_s$  mentioned above, we get

$$\sum_{j=1}^{N} \frac{dz_{j}}{dt} \int_{0}^{1} \phi_{i} \phi_{j} dx = \sum_{j=1}^{N} z_{j} \left[ -\nu \int_{0}^{1} \phi'_{i} \phi'_{j} dx - u_{s} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{j})' dx \right] 
+ \sum_{j=1}^{N} z_{j} \left[ -\sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{j} \phi'_{k} \phi_{i} dx - \sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{k} \phi'_{j} \phi_{i} dx \right] 
+ u \left[ -2u_{s} \int_{0}^{1} \phi_{i} \phi_{0} \phi'_{0} dx - \sum_{k=1}^{N} w_{s}^{k} \int_{0}^{1} \phi_{i} (\phi_{0} \phi_{k})' dx - \nu \int_{0}^{1} \phi'_{i} \phi'_{0} dx \right]$$

We use the following notations:

• 
$$\mathbf{z} = [z_1, z_2, ..., z_N]^{\top}$$

• 
$$\mathbf{w}_s = [w_s^1, w_s^2, ..., w_s^N]^{\top}$$

• 
$$\mathbf{M} \in \mathbb{R}^{N \times N}$$
 with  $\mathbf{M}(i,j) = \int_0^1 \phi_i \phi_j \mathrm{d}x$ 

• 
$$\mathbf{A}1 \in \mathbb{R}^{N \times N}$$
 with  $\mathbf{A}1(i,j) = \int_0^1 \phi_i' \phi_j' dx$ 

• 
$$\mathbf{A}2 \in \mathbb{R}^{N \times N}$$
 with  $\mathbf{A}2(i,j) = \int_0^1 \phi_i(\phi_0 \phi_j)' \mathrm{d}x$ 

• 
$$\mathbf{D}1 \in \mathbb{R}^{N \times N \times N}$$
 with  $\mathbf{D}1(i, j, k) = \int_0^1 \phi_i \phi_j' \phi_k dx$ 

• 
$$\mathbf{A}(i,:) = -\nu \mathbf{A}1(i,:) - u_s \mathbf{A}2(i,:) - \mathbf{w}_s^{\top} \left[ \mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top} \right], \quad \forall i = 1, 2, ..., N$$

• 
$$\mathbf{d}1 \in \mathbb{R}^N$$
 with  $\mathbf{d}1(i) = \int_0^1 \phi_i \phi_0 \phi_0' dx$ 

• 
$$\mathbf{d}2 \in \mathbb{R}^N$$
 with  $\mathbf{d}2(i) = \int_0^1 \phi_i' \phi_0' \mathrm{d}x$ 

• 
$$\mathbf{B} = -2u_s\mathbf{d}1 - \mathbf{A}2 \cdot \mathbf{w}_s - \nu \mathbf{d}2$$

This can be written in matrix form as

$$\mathbf{M}\frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{A}\mathbf{z} + \mathbf{B}u$$

The control u(t) is obtained in terms of the feedback matrix  $\mathbf{K} = [K_1, K_2, ..., K_N]$ 

$$u(t) = -\sum_{j=1}^{N} K_j z_j(t)$$

The feedback gain  $\mathbf{K}$  is given by

$$\mathbf{K} = \mathbf{R}^{-1} \mathbf{B}^{\top} \mathbf{P} \mathbf{M}$$

where **P** is solution of algebraic Riccati equation (ARE)

$$\mathbf{A}^{\mathsf{T}}\mathbf{P}\mathbf{M} + \mathbf{M}^{\mathsf{T}}\mathbf{P}\mathbf{A} - \mathbf{M}^{\mathsf{T}}\mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^{\mathsf{T}}\mathbf{P}\mathbf{M} + \mathbf{Q} = 0$$

$$(\mathbf{M}, \mathbf{A} - \mathbf{B}\mathbf{K}) \text{ is stable}$$

#### 3.2 Partial information with noise

Consider the linearized model with noise in the model

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2} + \eta \tag{13}$$

$$z(0,t) = u(t), \qquad \frac{\partial z}{\partial r}(1,t) = 0 \tag{14}$$

$$z(x,0) = w_0(x) - w_s(x) (15)$$

Assume that we have access to partial information corrupted by noise

$$y = Hz + \mu$$

H being a suitable observation operator. We shall consider the case where H is given by

$$Hz(t) = z(1,t)$$

In the FEM setup, we get

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{A}\mathbf{z} + \mathbf{B}u + \boldsymbol{\eta}$$
$$\mathbf{v} = \mathbf{H}\mathbf{z} + \boldsymbol{\mu}$$

where the observation operator is approximated as

$$\mathbf{H} = (0, 0, ..., 0, 1)^{\top} \in \mathbb{R}^{N}$$

### 3.3 Estimation problem

Consider the

$$\frac{\partial z_e}{\partial t} + w_s \frac{\partial z_e}{\partial x} + z_e \frac{\mathrm{d}w_s}{\mathrm{d}x} = \nu \frac{\partial^2 z_e}{\partial x^2} + L(Hz - Hz_e)$$
 (16)

$$z_e(0,t) = u(t), \qquad \frac{\partial z_e}{\partial x}(1,t) = 0$$
 (17)

$$z_e(x,0) = 0 (18)$$

In the FEM setup, we have

$$\mathbf{M} \frac{\mathrm{d} \mathbf{z}_e}{\mathrm{d} t} = \mathbf{A} \mathbf{z}_e + \mathbf{B} u + \mathbf{L} (\mathbf{y} - \mathbf{H} \mathbf{z}_e)$$

The filtering gain L is given by

$$\mathbf{L} = \mathbf{M} \mathbf{P}_e \mathbf{H}^{\top} \mathbf{R}_{\boldsymbol{\mu}}^{-1}$$

where  $\mathbf{P}_e$  is solution of

$$\mathbf{A}\mathbf{P}_{e}\mathbf{M} + \mathbf{M}\mathbf{P}_{e}\mathbf{A}^{\top} - \mathbf{M}\mathbf{P}_{e}\mathbf{H}^{\top}\mathbf{R}_{\mu}^{-1}\mathbf{H}\mathbf{P}_{e}\mathbf{M} + \mathbf{R}_{\eta} = 0$$

$$(\mathbf{M}, \mathbf{A} - \mathbf{L}\mathbf{H}) \text{ is stable}$$

### 3.4 Coupled linear system

The feedback is based on estimated solution  $u = -\mathbf{K}\mathbf{z}_e$ 

$$egin{array}{ll} \mathbf{M}rac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} &=& \mathbf{A}\mathbf{z} - \mathbf{B}\mathbf{K}\mathbf{z}_e + oldsymbol{\eta} \ \mathbf{M}rac{\mathrm{d}\mathbf{z}_e}{\mathrm{d}t} &=& \mathbf{L}\mathbf{H}\mathbf{z} + (\mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H})\mathbf{z}_e + \mathbf{L}oldsymbol{\mu} \end{array}$$

or in matrix form

$$\begin{bmatrix} \mathbf{M} & \mathbf{0} \\ \mathbf{0} & \mathbf{M} \end{bmatrix} \frac{\mathrm{d}}{\mathrm{d}t} \begin{bmatrix} \mathbf{z} \\ \mathbf{z}_e \end{bmatrix} = \begin{bmatrix} \mathbf{A} & -\mathbf{B}\mathbf{K} \\ \mathbf{L}\mathbf{H} & \mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H} \end{bmatrix} \begin{bmatrix} \mathbf{z} \\ \mathbf{z}_e \end{bmatrix} + \begin{bmatrix} \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{L} \end{bmatrix} \begin{bmatrix} \boldsymbol{\eta} \\ \boldsymbol{\mu} \end{bmatrix}$$

The initial condition is given by

$$\mathbf{z}(0) = \mathbf{z}_0, \qquad \mathbf{z}_e(0) = 0$$

This is implemented in program lin\_lqg.m

#### 3.5 Excercises

- 1. Run program lin\_lqg.m
- 2. Check stabilizabilty of (A, B) using the Hautus criterion.
- 3. Set  $(\mathbf{Q} = 0)$  which corresponds to minimal norm control. Run the code and observe the solution and control.
- 4. Set  $(\mathbf{Q} = \mathbf{M})$  and run the code. How has the solution and control beaviour changed?
- 5. Vary  $\mathbf{R}$  in the range (0.01, 10) and observe how the feedback gain  $\mathbf{K}$  varies.
- 6. For  $\mathbf{Q} = 0$ , modify the code to solve the control and estimation problem for only the unstable components.

### 4 Non-linear system with control and estimation

We will solve the non-linear equation for the perturbation  $z = w - w_s$ .

$$\frac{\partial z}{\partial t} + w_s \frac{\partial z}{\partial x} + z \frac{\mathrm{d}w_s}{\mathrm{d}x} + z \frac{\mathrm{d}z}{\mathrm{d}x} = \nu \frac{\partial^2 z}{\partial x^2}$$
$$z(0,t) = u(t), \quad z_x(1,t) = 0, \quad z(x,0) = w^{\delta}(x)$$

We multiply by a test function  $\phi$  with  $\phi(0) = 0$  to obtain the weak formulation

$$\int_0^1 z_t \phi dx + \nu \int_0^1 \frac{\partial z}{\partial x} \frac{d\phi}{dx} dx + \int_0^1 w_s \frac{\partial z}{\partial x} \phi dx + \int_0^1 z \frac{\partial w_s}{\partial x} \phi dx + \int_0^1 w \frac{dw}{dx} \phi dx = 0$$

The finite element solution can be written as

$$z(x,t) = \sum_{j=1}^{N} z_j(t)\phi_j(x) + u(t)\phi_0(x)$$

while the stationary solution expressed as

$$w_s(x) = \sum_{i=1}^{N} w_s^j \phi_j(x) + u_s \phi_0(x)$$

The Galerkin approximation is

$$\int_{0}^{1} z_{t} \phi_{i} dx = -\nu \int_{0}^{1} \frac{\partial z}{\partial x} \frac{d\phi_{i}}{dx} dx - \int_{0}^{1} w_{s} \frac{\partial z}{\partial x} \phi_{i} dx - \int_{0}^{1} z \frac{\partial w_{s}}{\partial x} \phi_{i} dx$$
$$- \int_{0}^{1} z \frac{dz}{dx} \phi_{i} dx, \qquad \forall i = 1, 2, ..., N$$

Ignoring the  $\frac{du}{dt}$  term and using the expression for  $w_s$ , we get

$$\begin{split} \sum_{j=1}^{N} z_j'(t) \int_0^1 \phi_i \phi_j \mathrm{d}x &= -\sum_{j=1}^{N} \sum_{k=1}^{N} z_j(t) z_k(t) \int_0^1 \phi_j \phi_k' \phi_i \mathrm{d}x \\ &- \sum_{j=1}^{N} z_j(t) \left[ \nu \int_0^1 \phi_i' \phi_j' \mathrm{d}x + u_s \int_0^1 \phi_i (\phi_0 \phi_j)' \mathrm{d}x \right] \\ &- \sum_{j=1}^{N} z_j(t) \left[ \sum_{k=1}^{N} w_s^k(t) \left( \int_0^1 \phi_j \phi_k' \phi_i \mathrm{d}x + \int_0^1 \phi_k \phi_j' \phi_i \mathrm{d}x \right) \right] \\ &- u(t) \left[ \sum_{j=1}^{N} z_j \int_0^1 \phi_i (\phi_0 \phi_j)' \mathrm{d}x + \sum_{k=1}^{N} w_s^k \int_0^1 \phi_i (\phi_0 \phi_k)' \mathrm{d}x \right] \\ &- u(t) \left[ \nu \int_0^1 \phi_i' \phi_0' \mathrm{d}x + 2u_s \int_0^1 \phi_i \phi_0 \phi_0' \mathrm{d}x \right] - u(t)^2 \int_0^1 \phi_i \phi_0 \phi_0' \mathrm{d}x \end{split}$$

Thus we have the system

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{R}\mathbf{H}\mathbf{S}_1 + \mathbf{R}\mathbf{H}\mathbf{S}_2$$

where

$$\mathbf{RHS}_1(i) = -\mathbf{z}^{\top} \mathbf{D}1(:,:,i)\mathbf{z} - \left[\nu \mathbf{A}1(i,:) + u_s \mathbf{A}2(i,:) + \mathbf{w}_s^{\top} (\mathbf{D}1(:,:,i) + \mathbf{D}1(:,:,i)^{\top})\right] \mathbf{z}$$

$$\mathbf{RHS}_2(i) = -u(t) \left[\mathbf{A}2(\mathbf{z} + \mathbf{w}_s) + 2u_s \mathbf{d}1 + \nu \mathbf{d}2\right] - u(t)^2 \mathbf{d}1$$

The control u(t) is obtained from the linear estimation problem

$$u(t) = -\sum_{j=1}^{N} K_j z_e^j$$

We solve the non-linear system and the linear estimator in a coupled manner.

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}}{\mathrm{d}t} = \mathbf{R}\mathbf{H}\mathbf{S}_1 + \mathbf{R}\mathbf{H}\mathbf{S}_2$$

$$\mathbf{M} \frac{\mathrm{d}\mathbf{z}_e}{\mathrm{d}t} = \mathbf{L}\mathbf{H}\mathbf{z} + (\mathbf{A} - \mathbf{B}\mathbf{K} - \mathbf{L}\mathbf{H})\mathbf{z}_e$$

$$\mathbf{z}(0) = \mathbf{z}_0, \qquad \mathbf{z}_e(0) = 0$$

This is implemented in burger\_lqg.m

### 4.1 Excercises

- 1. Run program burger\_lqg.m
- 2. Vary  $\mathbf{R}$  in the range (0.01, 10) and observe how the feedback gain  $\mathbf{K}$  changes. How does the solution and control change with  $\mathbf{R}$ .

# 5 List of Programs

- 1. get\_system\_mat.m: Computes FEM matrices
- 2. feedback\_matrix.m: Computes feedback matrix
- 3. stationarysol.m: Computes exact unstable stationary solution
- 4. burger.m: Solves the non-linear model, without feedback
- 5. lin\_lqg.m: Solves the coupled estimation and control system for the linear problem
- 6. burger\_lqg.m: Solves the coupled estimation and control system for the non-linear problem
- 7. rhs\_burger.m: Computes the right hand side for the non-linear problem, without feedback

8.	<pre>rhs_burger_lqg.m: Computes the right hand side for coupled estimation and control system with the non-linear problem</pre>