

Assignment 1 - Transmission Lines

Monday, January 25, 2016 8:21 AM

- 10.1** The parameters of a certain transmission line operating at $\omega = 6 \times 10^8 \text{ rad/s}$ are $L = 0.35 \mu\text{H/m}$, $C = 40 \text{ pF/m}$, $G = 75 \mu\text{S/m}$, and $R = 17 \Omega/\text{m}$. Find γ , α , β , λ , and Z_0 .

$$\gamma = \sqrt{(R+j\omega L)(G+j\omega C)} \quad \rightarrow$$

$$Z = R + j\omega L = 17 \frac{\Omega}{\text{m}} + j(6 \times 10^8 \frac{\text{rad}}{\text{s}}) 0.35 \mu\text{H} = 17 + j210 \frac{\Omega}{\text{m}} \quad \text{net series impedance}$$

$$Y = G + j\omega C = 75 \frac{\text{mS}}{\text{m}} + j(6 \times 10^8 \frac{\text{rad}}{\text{s}}) 40 \text{ pF} = 75 \text{ mS} + 24 \text{ mS} \quad \text{net shunt admittance}$$

$$\gamma = \sqrt{ZY} = \sqrt{(44.305 \cdot 10^3, 2.2467) \frac{\text{rad}}{\text{m}}} \quad \text{propagation constant}$$

$$\alpha + j\beta = \sqrt{ZY} \quad \rightarrow$$

$$\alpha = 94.305 \text{ m} \frac{\text{Np}}{\text{m}}$$

$$\beta = 2.247 \frac{\text{rad}}{\text{m}} \quad \text{phase constant}$$

$$\beta = \frac{2\pi}{\lambda} \rightarrow \lambda = \frac{2\pi}{\beta} = 2.7966 \text{ m} \quad \text{wavelength}$$

$$Z_0 = \sqrt{\frac{Z}{Y}} \rightarrow Z_0 = \sqrt{\frac{(17, 210)}{(75 \mu, 24 \text{ m})}} = 93.62 - j3.637 \frac{\Omega}{\text{m}} \quad \text{characteristic impedance}$$

↖ can't assume lossless

- 10.5** Two characteristics of a certain lossless transmission line are $Z_0 = 50 \Omega$ and $\gamma = 0 + j0.2\pi \text{ m}^{-1}$ at $f = 60 \text{ MHz}$ (a) find L and C for the line. (b) A load $Z_L = 60 + j80 \Omega$ is located at $z = 0$. What is the shortest distance from the load to a point at which $Z_{in} = R_{in} + j0$?

$$\gamma = \alpha + j\beta \rightarrow \beta = 0.2\pi \frac{\text{rad}}{\text{m}}$$

$$\beta = \omega \sqrt{LC} \rightarrow C = \frac{\beta^2}{L\omega^2} \rightarrow \frac{\beta^2}{L\omega^2} = \frac{L}{Z_0^2} \rightarrow \frac{\beta^2 Z_0^2}{\omega^2} = L^2 \rightarrow \frac{\beta Z_0}{\omega} = L$$

$$Z_0 = \sqrt{\frac{L}{C}} \rightarrow C = \frac{L}{Z_0^2} \rightarrow L = \frac{0.2\pi (50)}{2\pi 60 \text{ M}} = 83.3 \text{ nH/m}$$

$$C = \frac{L}{Z_0^2} = \frac{83.3 \text{ nH}}{50^2} = 33.3 \text{ pF/m}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(60, 80) - 50}{(60, 80) + 50} = (0.40541, 0.43243) \rightarrow \text{in polar form} \rightarrow 0.59275 \angle 46.898^\circ$$

$$Z_{max} = \frac{-1}{2\beta} (\phi + 2n\pi) \xrightarrow{n=0} Z_{max} = \frac{-1}{2(0.2\pi)} (46.848 \frac{\pi}{180} + \phi) = -0.65067 \rightarrow 651 \text{ mm}$$

- 10.6** A $50\text{-}\Omega$ load is attached to a 50-m section of the transmission line of Problem 10.1, and a 100-W signal is fed to the input end of the line. (a)

- 10.6** A 50Ω load is attached to a 50-m section of the transmission line of Problem 10.1, and a 100-W signal is fed to the input end of the line. (a) Evaluate the distributed line loss in dB/m . (b) Evaluate the reflection coefficient at the load. (c) Evaluate the power that is dissipated by the load resistor. (d) What power drop in dB does the dissipated power in the load represent when compared to the original input power? (e) On partial reflection from the load, how much power returns to the input and what dB drop does this represent when compared to the original 100-W input power?



$$\text{Power loss (dB)} = 8.69 \text{ dB} \xrightarrow{\text{from 10.1}} 8.69 (44.305 \text{ m}) (50\text{m}) = 40.976 \text{ dB}$$

$$\text{Power loss (dB/m)} = 40.976 \text{ dB} / 50\text{m} = 0.8195 \text{ dB/m}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} \xrightarrow{\text{from 10.1}} \Gamma_L = \frac{50 - (93.62, -3.637)}{50 + (93.62, -3.637)} = (-0.304 + j17.62) 10^{-3}$$

$$\text{POWER AT LOAD } \langle P(z) \rangle = \langle P(0) \rangle e^{-2az} \rightarrow \langle P(50) \rangle = 100\text{W} e^{-2(44.305)(50)} = 8.0239 \text{ mW}$$

$$\text{POWER DISSIPATED BY LOAD } \frac{\langle P_t \rangle}{\langle P_i \rangle} = 1 - |\Gamma|^2 \rightarrow \langle P_L \rangle = (1 - |\Gamma|^2) \langle P_i \rangle = (1 - |\Gamma|^2) 8.0239 \text{ mW} = 7.28 \text{ mW}$$

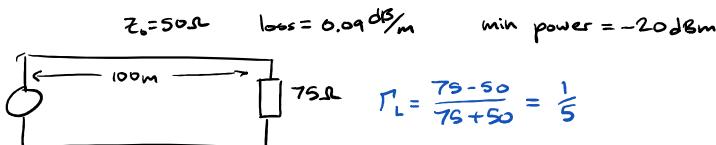
$$\text{Power loss (dB)} = 10 \log \frac{\langle P(0) \rangle}{\langle P(z) \rangle} \rightarrow P = 10 \log \frac{100}{7.28 \text{ mW}} = 41.38 \text{ dB} \quad \downarrow \text{1 round trip}$$

$$\text{POWER RETURNED AFTER ROUND TRIP } \langle P(z) \rangle = \langle P(0) \rangle e^{-2az} \rightarrow \langle P(100) \rangle = 100 e^{-2(44.305)(50+50)} = 643.83 \text{ nW}$$

$$\text{POWER REFLECTED BY LOAD } \frac{\langle P_r \rangle}{\langle P_i \rangle} = |\Gamma|^2 \rightarrow P = |\Gamma|^2 643.83 \text{ nW} = 59.70 \text{ nW}$$

$$\text{Decibel drop (dB)} = 10 \log \frac{\langle P(0) \rangle}{\langle P(z) \rangle} \rightarrow P = 10 \log \frac{100}{59.70 \text{ nW}} = 94.24 \text{ dB}$$

- 10.8** An absolute measure of power is the dBm scale, in which power is specified in decibels relative to one milliwatt. Specifically, $P(\text{dBm}) = 10 \log_{10}[P(\text{mW})/1\text{mW}]$. Suppose that a receiver is rated as having a *sensitivity* of -20 dBm , indicating the *minimum* power that it must receive in order to adequately interpret the transmitted electronic data. Suppose this receiver is at the load end of a 50Ω transmission line having 100-m length and loss rating of 0.09 dB/m . The receiver impedance is 75Ω , and so is not matched to the line. What is the minimum required input power to the line in (a) dBm , (b) mW ?



$$Z_0 = 50\Omega \quad \text{loss} = 0.09 \text{ dB/m} \quad \text{min power} = -20 \text{ dBm}$$

$$\Gamma_L = \frac{75 - 50}{75 + 50} = \frac{1}{5}$$

LOSS DUE TO TRANSMISSION

$$L(\text{dB}) = 0.09 \frac{\text{dB}}{\text{m}} (100\text{m}) = 9 \text{ dB}$$

LOSS DUE TO MISMATCHED LOAD

$$\frac{\langle P_t \rangle}{\langle P_{in} \rangle} = 1 - |\Gamma|^2 \nmid L(\text{dB}) = 10 \log \frac{\langle P_{in} \rangle}{\langle P_t \rangle}$$

$$\frac{P_{in}}{P_t} = 10 \log \frac{1}{1 - |\Gamma|^2} = 0.17779 \text{ JR}$$

$$\frac{P_{in}}{P_{out}} = 1 - |\Gamma|^2 \quad \nabla \quad L(\text{dB}) = 10 \log \frac{P_{in}}{P_{out}}$$

$$\hookrightarrow L_2(\text{dB}) = 10 \log \frac{P_m}{P_m(1 - |\Gamma|^2)} = 10 \log \frac{1}{1 - (\frac{1}{5})^2} = 0.17729 \text{ dB}$$

TOTAL LOSS

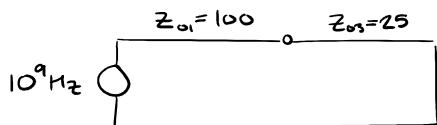
$$L(\text{dB}) = 9 \text{ dB} + 0.17729 \text{ dB} = 9.17729 \text{ dB}$$

MINIMUM INPUT

$$P_{in}(\text{dB}) = P_{min} + P_{loss} = -20 \text{ dB} + 9.17729 \text{ dB} = \boxed{-10.823 \text{ dB}}$$

$$P_{in}(\text{W}) = 10 \text{ W} \cdot 10^{-\frac{P(\text{dB})}{10}} = 10^{-\frac{10.823}{10}} = \boxed{82.74 \mu\text{W}}$$

- 10.10** Two lossless transmission lines having different characteristic impedances are to be joined end to end. The impedances are $Z_{01} = 100 \Omega$ and $Z_{03} = 25 \Omega$. The operating frequency is 1 GHz. (a) Find the required characteristic impedance, Z_{02} , of a quarter-wave section to be inserted between the two, which will impedance-match the joint, thus allowing total power transmission through the three lines. (b) The capacitance per unit length of the intermediate line is found to be 100 pF/m. Find the shortest length in meters of this line that is needed to satisfy the impedance-matching condition. (c) With the three-segment setup as found in parts (a) and (b), the frequency is now doubled to 2 GHz. Find the input impedance at the line-1-to-line-2 junction, seen by waves incident from line 1. (d) Under the conditions of part (c), and with power incident from line 1, evaluate the standing wave ratio that will be measured in line 1, and the fraction of the incident power from line 1 that is reflected and propagates back to the line 1 input.



FROM EQN 103

$$Z_{02} = \sqrt{Z_{01} \cdot Z_{03}} \rightarrow Z_{02} = \sqrt{100 \cdot 25} = \boxed{50 \Omega}$$

$$Z_0 = \sqrt{\frac{L}{C}} \rightarrow L = Z_0^2 C \rightarrow L_2 = Z_{02}^2 C_2 = 50^2 (10^{-12}) = 2.5 \mu\text{H}$$

$$\beta = \omega \sqrt{LC} = \frac{2\pi}{\lambda} \rightarrow \lambda = \frac{2\pi}{\omega \sqrt{LC}} = \frac{2\pi}{10^9 \cdot 2\pi \sqrt{2.5 \times 100 \times 100 \times 10^{-12}}} = 2 \text{ m}$$

↑ in Hz

$$\text{FROM EQN 100 CONDITIONS } l = \frac{1}{4}\lambda = \frac{1}{4} \cdot 2 \text{ m} = \boxed{0.05 \text{ m}}$$

Frequency x2 $\therefore \lambda/2$ instead of $\lambda/4 \therefore Z_{in} = Z_L$ EQN 77

$$s = \frac{1 + |\Gamma|}{1 - |\Gamma|} \oplus \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} \rightarrow \Gamma_{in} = \frac{25 - 100}{25 + 100} = \frac{-3}{5}$$

$\rightarrow s = \boxed{4}$

- 10.14** A lossless transmission line having characteristic impedance $Z_0 = 50 \Omega$ is driven by a source at the input end that consists of the series combination of a 10-V sinusoidal generator and a $50-\Omega$ resistor. The line is one-quarter wavelength long. At the other end of the line, a load impedance, $Z_L = 50 - j50 \Omega$ is attached. (a) Evaluate the input impedance to the line

seen by the voltage source-resistor combination; (b) evaluate the power that is dissipated by the load; (c) evaluate the voltage amplitude that appears across the load.

$$\text{For } \frac{1}{4} \quad Z_{in} = \frac{Z_{0s}}{Z_L} \rightarrow Z_{in} = \frac{50^2}{(50, -50)} = (25, 25)$$

$$I^* = \frac{V^*}{Z^*}$$

$$V_o = V_o \frac{R_L}{R_s + R_L}$$

$$I^* = \frac{(V_o)^*}{Z_{in}^*} = \frac{(V_o \frac{Z_{in}}{Z_{in} + Z_{in}})^*}{Z_{in}^*} = \left(\frac{10 \frac{(25, 25)}{50 + (25, 25)}}{(25, 25)} \right)^*$$

$$I^* = \frac{(4, 2)^*}{(25, 25)^*} = (0.12, 0.04)$$

$$\langle P \rangle = \frac{1}{2} \operatorname{Re} \{ V I^* \} \rightarrow \frac{1}{2} \operatorname{Re} \{ V_{in} I^* \} = \frac{1}{2} \operatorname{Re} \{ (4, 2)(0.12, 0.04) \} = 0.2 \text{ W}$$

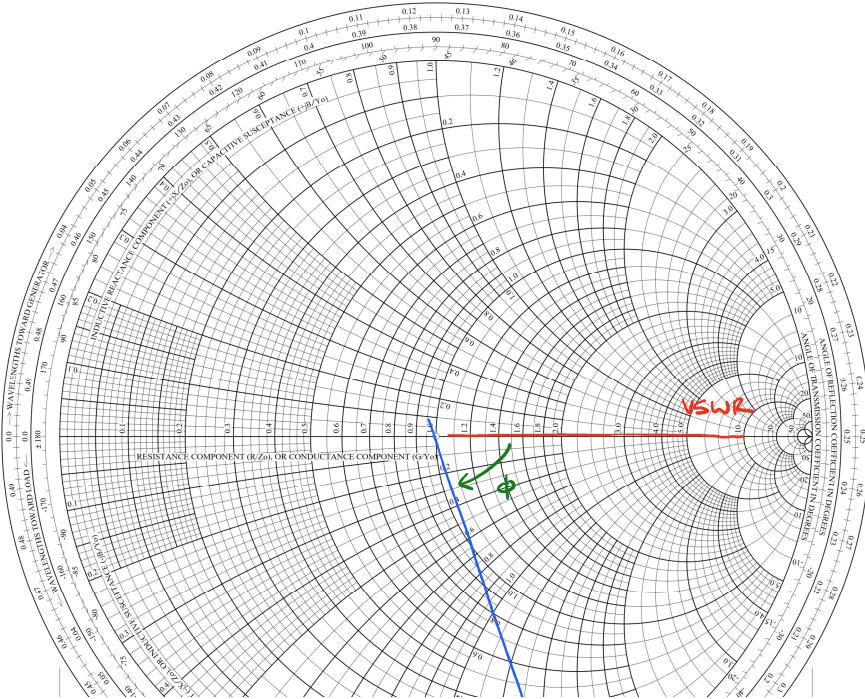
$$V_o^+ = \frac{V_{in}}{e^{j\beta s} + \Gamma_L e^{-j\beta L}}$$

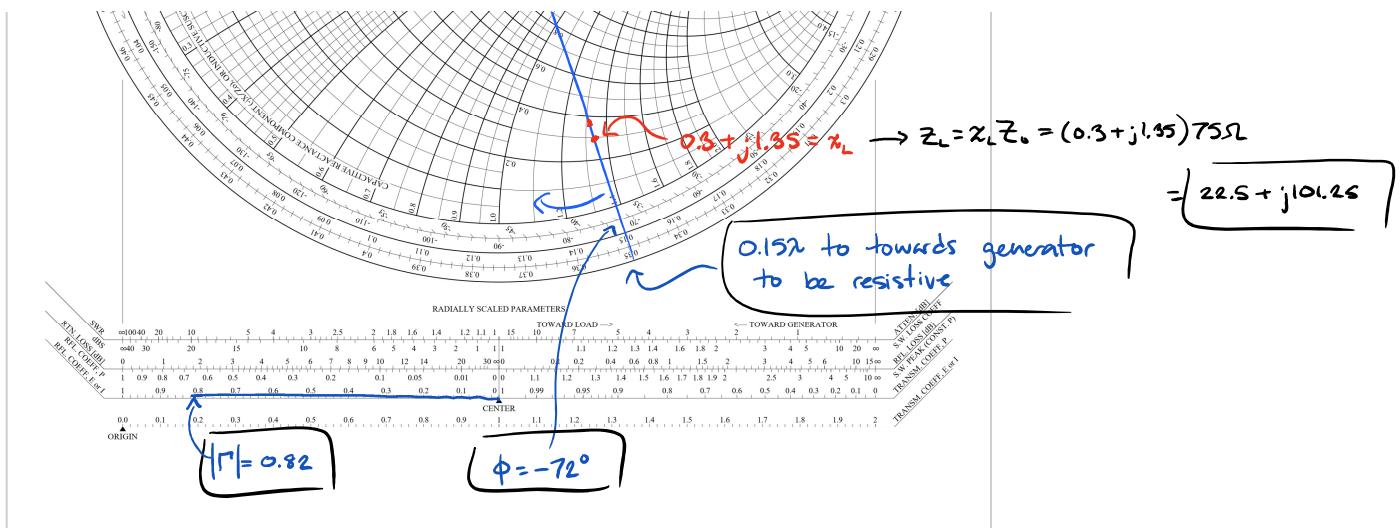
$$V_L = V_o^+ (1 + \Gamma_L)$$

- 10.22** A lossless 75- Ω line is terminated by an unknown load impedance. A VSWR of 10 is measured, and the first voltage minimum occurs at 0.15 wavelengths in front of the load. Using the Smith chart, find (a) the load impedance; (b) the magnitude and phase of the reflection coefficient; (c) the shortest length of line necessary to achieve an entirely resistive input impedance.

The Complete Smith Chart

Black Magic Design

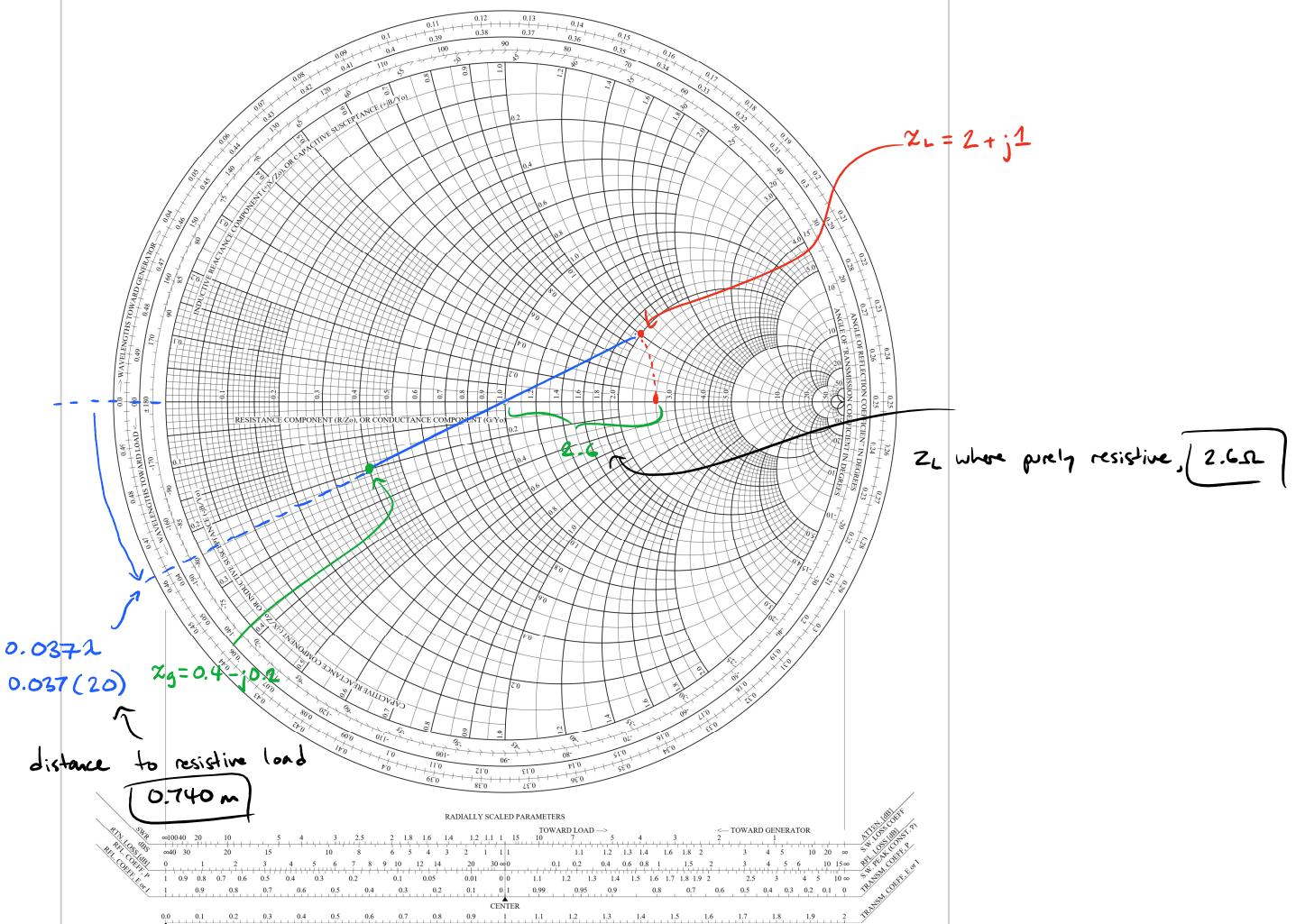




- 10.23** The normalized load on a lossless transmission line is $2 + j1$. Let $\lambda = 20$ m and make use of the Smith chart to find (a) the shortest distance from the load to a point at which $z_{in} = r_{in} + j0$, where $r_{in} > 0$; (b) z_{in} at this point. (c) The line is cut at this point and the portion containing z_L is thrown away. A resistor $r = r_{in}$ of part (a) is connected across the line. What is s on the remainder of the line? (d) What is the shortest distance from this resistor to a point at which $z_{in} = 2 + j1$?

The Complete Smith Chart

Black Magic Design



- 10.32** In Figure 10.17, let $Z_L = 250 \Omega$, $Z_0 = 50 \Omega$, find the shortest attachment distance d and the shortest length d_1 of a short-circuited stub line that will provide a perfect match on the main line to the left of the stub. Express all answers in wavelengths.

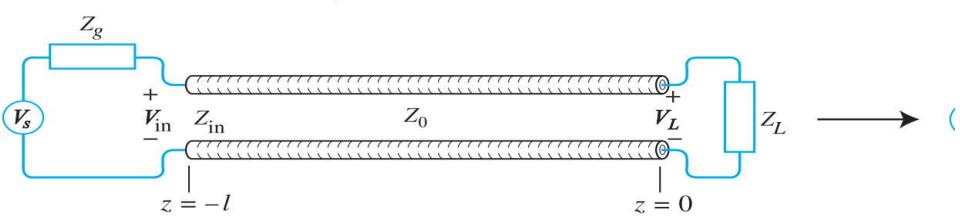


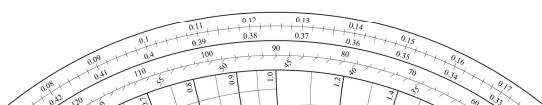
Figure 10.7 Finite-length transmission line configuration and its equivalent circuit $\frac{Z_L - Z_0}{Z_0} = 5 \Omega$

The Complete Smith Chart

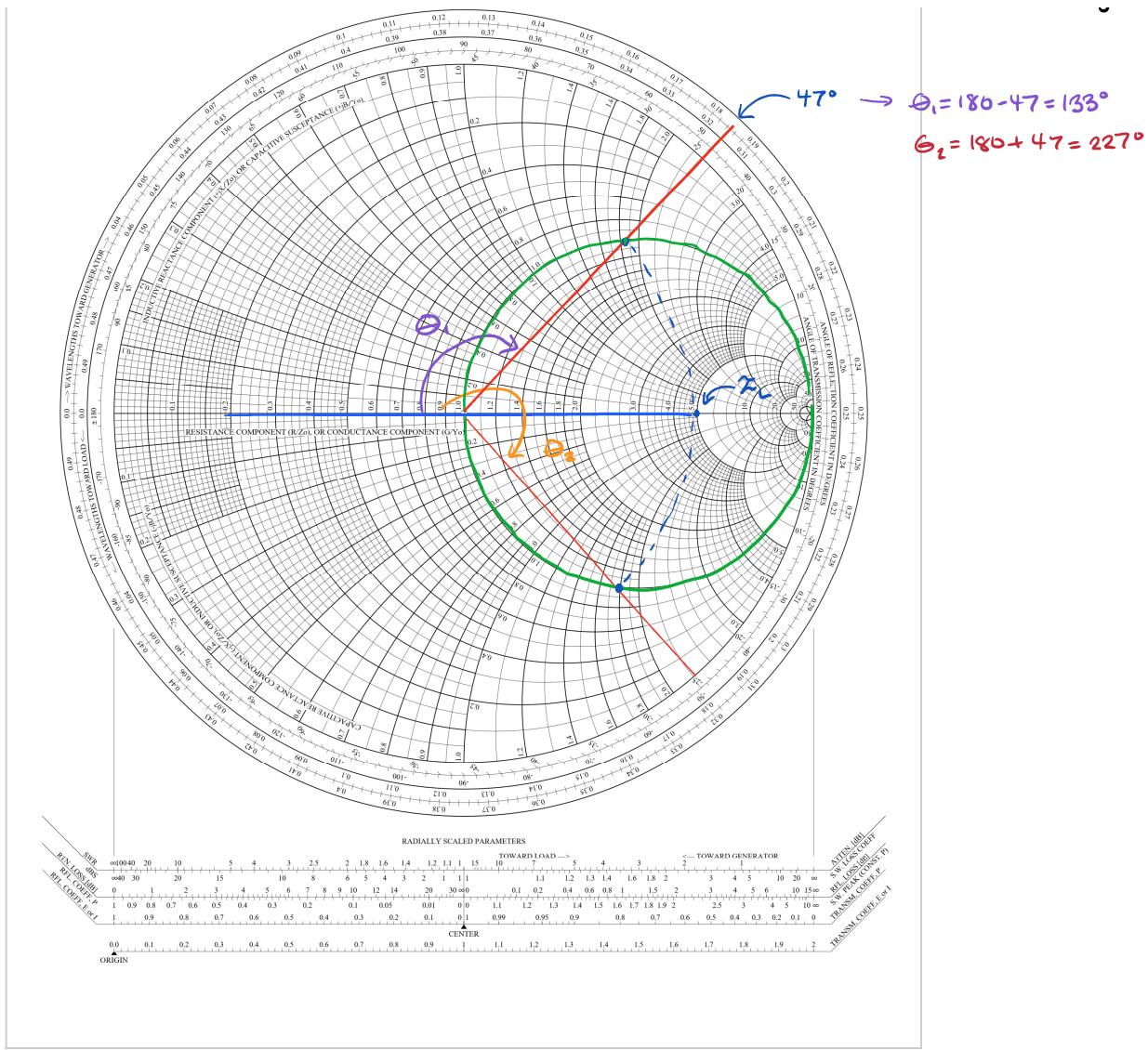
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$$\Theta = \frac{4\pi}{2} d_1 \rightarrow d_1 = 133^\circ \frac{1/4}{180} \lambda = 0.1847 \lambda$$

↑ stub length



— 4.70 — ... — 1.00 —



- 10.40** In the charged line of Figure 10.25, the characteristic impedance is $Z_0 = 100 \Omega$, and $R_g = 300 \Omega$. The line is charged to initial voltage, $V_0 = 160 \text{ V}$, and the switch is closed at $t = 0$. Determine and plot the voltage and current through the resistor for time $0 < t < 8l/v$ (four round-trips). This problem accompanies Example 10.12 as the other special case of the basic charged-line problem, in which now $R_g > Z_0$.

$$\Gamma = \frac{Z_L - Z_0}{Z_0 + Z_0} \rightarrow \Gamma_g = \frac{300 - 100}{300 + 100} = \frac{1}{2}$$

$$I^+ = \frac{V^+}{Z_0}, \quad I^- = -\frac{V^-}{Z_0}$$

$$V^+ = V_0 \frac{Z_0}{Z_0 + R_g} \rightarrow V_1^+ = 160 \text{ V} \frac{100 \Omega}{100 \Omega + 300 \Omega} = 40 \text{ V}$$

$$V^- (0, t) = \Gamma V^+ (0, t) \rightarrow V_1^- = \Gamma_L V_1^+ = 40 \text{ V}$$

$$V_2^+ = \Gamma_g V_1^- = 20 \text{ V}, \quad V_2^- = \Gamma_L V_2^+ = 20 \text{ V}$$

$$V_3^+ = \Gamma_g V_2^- = 10 \text{ V}, \quad V_3^- = \Gamma_L V_3^+ = 10 \text{ V}$$

$$V_4^+ = \Gamma_g V_3^- = 5 \text{ V}, \quad V_4^- = \Gamma_L V_4^+ = 5 \text{ V}$$

$$V_{R_1} = V_o^- + V_i^+ = 120 \text{ V}$$

$$I_{i1}^+ = \frac{V_i^+}{Z_0} = \frac{40}{100} = 0.4 \text{ A}$$

$$V_{R_2} = V_i^- + V_o^+ = 60 \text{ V}$$

$$I_{i2}^+ = \frac{V_o^+}{Z_0} = \frac{20}{100} = 0.2 \text{ A}$$

$$V_{R_3} = V_o^- + V_i^+ = 30 \text{ V}$$

$$I_{i3}^+ = \frac{V_i^+}{Z_0} = \frac{10}{100} = 0.1 \text{ A}$$

$$V_{R_4} = V_o^- + V_o^+ = 15 \text{ V}$$

$$I_{i4}^+ = \frac{V_o^+}{Z_0} = \frac{5}{100} = 0.05 \text{ A}$$

$$V_{R_5} = 7.5 \text{ V}$$

$$I_{i5}^+ = \frac{V_o^+}{Z_0} = \frac{2.5}{100} = 0.025 \text{ A}$$

