

## Design of Non-recursive or FIR Filters

Described by

$$y(n) = \sum_{k=0}^N h(k) x(n-k)$$

$h(k)$ : impulse response sequence or coefficient of the filter.

### Advantages

- (1) Inherently stable
- (2) They can provide linear phase characteristics, speech processing and data processing
- (3) Quantization effects can be made small
- (4) They can be implemented in parallel/pipeline fashions using array processors.

### Disadvantages

- (1) For a sharp cut-off performance a large order filter is required.
- (2) They need "fractional delays" in some cases. (cannot be realized by physical devices)

### Frequency Response of FIR Filter

$h(n)$ : impulse response  $n \in [0, N-1]$

$$h(n) = 0 \quad \forall n \notin [0, N-1], n < 0$$

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

Transfer Function.

$N-1$  zeros,  
and  $(N-1)$  poles at  $z=0$

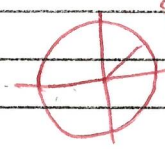
Let  $z = e^{j\Omega}$   $H(e^{j\Omega}) = H(e^{j(\Omega+2\pi)}) \quad \forall \Omega \in \mathbb{Z}$

$$H(e^{j\Omega}) = \sum_{n=0}^{N-1} h(n) e^{-j\Omega n} = \text{DFT} \{h(n)\}$$

$$\Omega = \frac{2\pi k}{N}$$

$$\text{DFT} \{h(n)\} = H(k) = \sum_{n=0}^{N-1} h(n) e^{-j \frac{2\pi k n}{N}}$$

$z = e^{j\Omega} = e^{j \frac{2\pi k}{N}}$



We can use IDFT to get the result. (FIR filter).

Following cases are considered

Case 1: Symmetric

$$h(n) = h(N-1-n)$$

(a) N: odd

$$H(e^{j\Omega}) = \underbrace{e^{-j\Omega \left(\frac{N-1}{2}\right)}}_{\text{phase}} \underbrace{\sum_{n=0}^{\left(\frac{N-1}{2}\right)} \alpha(n) \cos \Omega n}_{\text{magnitude}}$$

where  $\alpha(n) = 2h\left[\left(\frac{N-1}{2}\right) - n\right] \quad n=1, 2, \dots, \frac{N-1}{2}$

$$\alpha(0) = h\left(\frac{N-1}{2}\right)$$

This has linear phase characteristics.

$$\phi(\Omega) = -\Omega \left(\frac{N-1}{2}\right)$$

group delay  $\tau_g = -\frac{d\phi(\Omega)}{d\Omega} = \left(\frac{N-1}{2}\right)$   
= integer.



(b) N: Even

$$H(e^{j\Omega}) = e^{-j\Omega \left(\frac{N-1}{2}\right)} \sum_{n=1}^{\frac{N}{2}} \beta(n) \cos[\Omega(n-\frac{1}{2})]$$

$\beta(n) = h\left(\frac{N}{2}-n\right)$ ,  $n=1, 2, \dots, \frac{N}{2}$   
 At  $\Omega=\pi$ ,  $H(e^{j\Omega}) = 0$  i.e. HPF cannot be approximated

Case 2: Antisymmetric

$$h(n) = -h(N-1-n)$$

$$h\left(\frac{N-1}{2}\right) = 0$$

(a) N: odd

$$H(e^{j\Omega}) = e^{-j\Omega \left(\frac{N-1}{2}\right)} e^{j\frac{\Omega}{2}} \sum_{n=1}^{\frac{N-1}{2}} \gamma(n) \sin \Omega n$$

$$\gamma(n) = h\left[\left(\frac{N-1}{2}\right)-n\right], \quad n=1, 2, \dots, \frac{N-1}{2}$$

At  $\Omega=0$   
 and  $\Omega=\pi$   
 $|H(e^{j\Omega})| \neq 0$   
 Hilbert transform  
 + differentiator

(b) N: Even

$$H(e^{j\Omega}) = e^{-j\Omega \left(\frac{N-1}{2}\right)} e^{j\frac{\Omega}{2}} \sum_{n=1}^{\frac{N}{2}} \gamma(n) \sin[\Omega(n-\frac{1}{2})]$$

$$\gamma(n) = h\left(\frac{N}{2}-n\right) \quad n=1, 2, \dots, \frac{N}{2}$$

At  $\Omega=0 \Rightarrow H(e^{j\Omega}) = 0$   
 $\Omega=\pi \quad H \neq 0$

## (b) Design of FIR Filters

There are two groups of design methods:

### Indirect method

- (a) Windowing method
- (b) Frequency Sampling method

### Direct method

- (a) Computer Aided Optimization Method  
(Remez Exchange Algorithm)

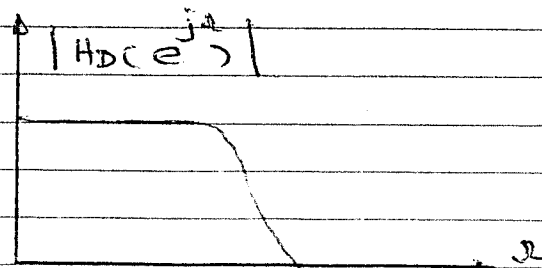
Desired frequency response is  $H_D(e^{j\omega})$

$$h_D(n) = \frac{1}{2\pi} \int_{-\frac{\Omega_s}{2}}^{\frac{\Omega_s}{2}} H_D(e^{j\omega}) e^{j\omega n} d\omega$$

$$= \text{IDTFT} \{ H_D(e^{j\omega}) \}$$

IDTFT  $\{ H_D e^{j\omega} \}$  is normally of infinite extent !!!

$$\begin{aligned} H_D(e^{j\omega}) &= \text{DTFT} \{ h_D(n) \} \\ &= \sum_{n=-\infty}^{\infty} h_D(n) e^{-j\omega n} \end{aligned}$$

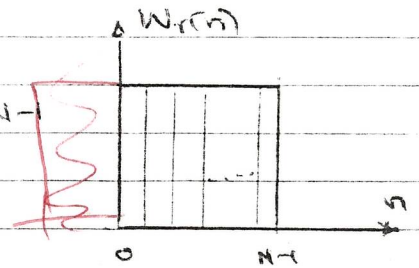


# (a) Windowing Methods (i) Rectangular Windowing

Assume  $h_0(n)$  is the impulse response of the desired filter which is of infinite extent, then

$$h(n) = h_0(n) w_r(n)$$

where  $w_r(n) = \begin{cases} 1 & 0 \leq n \leq N-1 \\ 0 & \text{otherwise} \end{cases}$



width of main lobe =  $4\pi/N$

$w_r(n)$  : rectangular window.

$$W_r(e^{j\omega}) = \text{DFT} \{w_r(n)\} = \sum_{n=0}^{N-1} e^{-j\omega n} = \frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}}$$

$$= \frac{\sin(\omega N/2)}{\sin(\omega/2)}$$

repetitive Sinc function

(see pp 60)

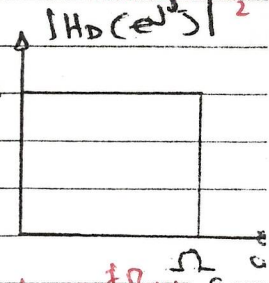
$N \rightarrow$  increase ~~main lobe~~ narrows

$$|W_r(e^{j\omega})| = \frac{|\sin \omega N/2|}{|\sin \omega/2|}, \quad \phi(\omega) = \begin{cases} -\omega(N-1)/2 & \text{when } \sin \omega/2 > 0 \\ \omega(N-1)/2 & \text{when } \sin \omega/2 < 0 \end{cases}$$

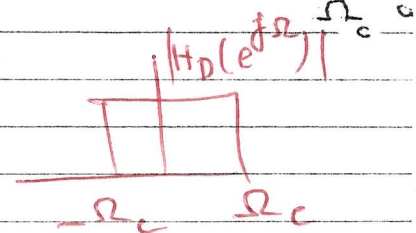
## Example

Design a LPF

$$H_D(e^{j\omega}) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$



$$h_D(n) = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega n} d\omega$$



$$= \frac{1}{jn} \sin \omega_c n$$

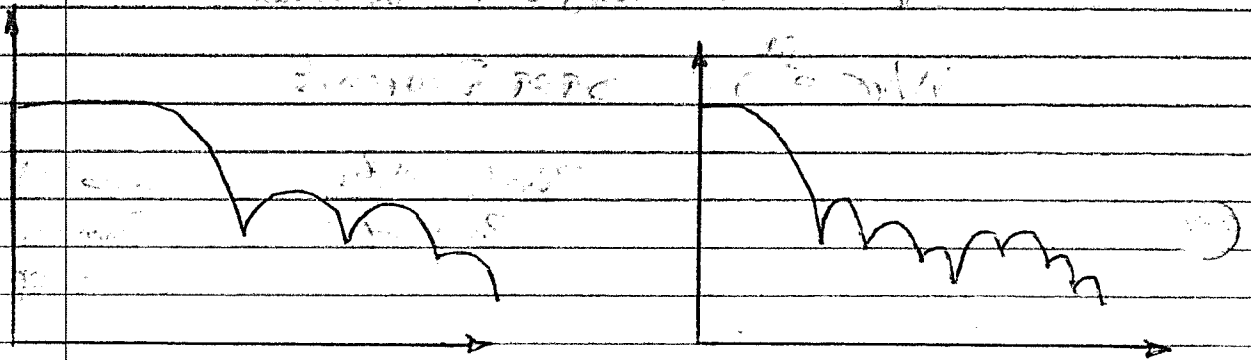
$$= \frac{\omega_c}{jn \omega_c} \sin \omega_c n$$

$$= \frac{2e}{\pi} \sin \pi n$$

$$h(n) = h_D(n) \cdot w(n)$$

$$H(e^{j\omega}) = H_D(e^{j\omega}) * W_R(e^{j\omega})$$

Because of the sharp window this will lead to the Gibbs phenomenon (ie output contains ripples). # of ripples increase with number of points, but amplitude will remain same.



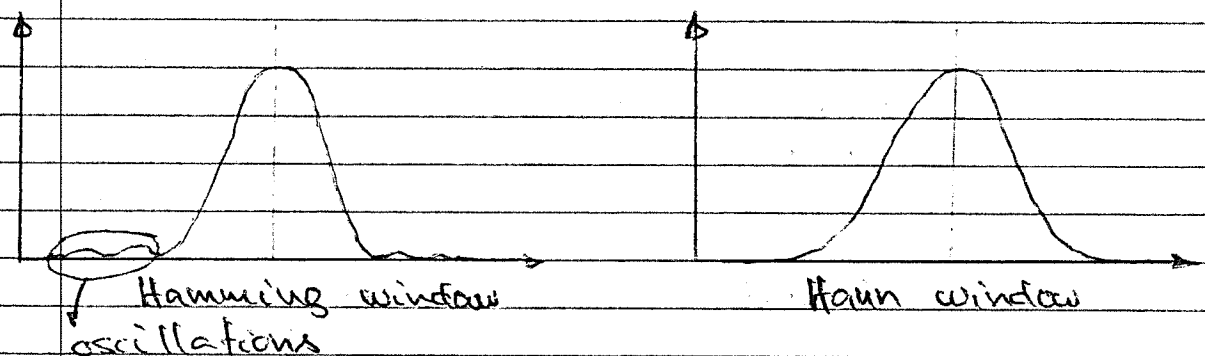
By adding more points we cannot get rid of Gibbs phenomenon.

## (2) Hann and Hamming Windows

$$w_H(n) = \begin{cases} \alpha + (1-\alpha) \cos \frac{2\pi n}{N-1} & \text{for } |n| \leq \frac{N-1}{2} \\ 0 & \text{otherwise} \end{cases}$$

$\alpha = 0.5$  Hann window

$\alpha = 0.54$  Hamming window



$$W_H(e^{j\Omega}) = \alpha \frac{\sin(\Omega N/2)}{\sin(\Omega/2)}$$

$$+ \frac{\{1 - \alpha \sin[\Omega N/2 - N\pi/(N-1)]\}}{2 \sin[\Omega/2 - \pi/(N-1)]}$$

$$+ \frac{\{1 - \alpha \sin[\Omega N/2 + N\pi/(N-1)]\}}{2 \sin[\Omega/2 + \pi/(N-1)]}$$

These windows will greatly reduce the amplitude of the ripples introduced in output by Gibbs phenomena.

### (3) Blackman Window

$$W_B(n) = \begin{cases} 0.42 + 0.5 \cos \frac{2\pi n}{N-1} + 0.8 \cos \frac{4\pi n}{N-1} & \text{for } |n| \leq \frac{N-1}{2} \\ 0 & \text{otherwise} \end{cases}$$

### (4) Kaiser Window

Optimum in the sense that the energy is concentrated in the main lobe.

$$W_K(n) = \begin{cases} \frac{I_0(\beta) [1 - (2n/N-1)^2]^\beta}{I_0(\beta)} & |n| \leq \frac{N-1}{2} \\ 0 & \text{otherwise} \end{cases}$$

$I_0()$ : modified zeroth order Bessel function of 1st kind

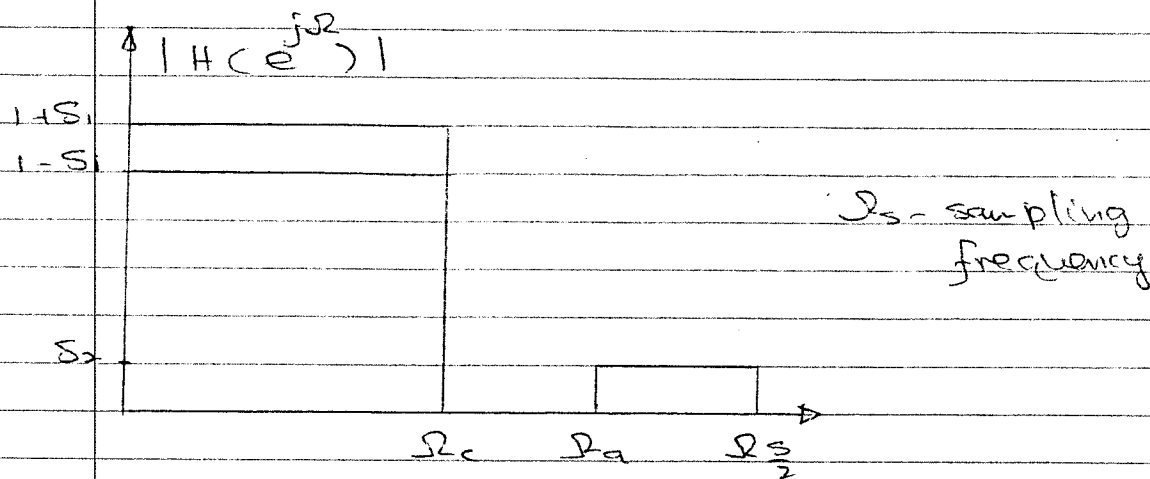
$\beta$ : parameter which determines trade-offs between the main lobe and the peak of the side lobe

$$I_0(x) = 1 + \sum_{m=1}^{\infty} \left[ \frac{(x/2)^m}{m!} \right]^2$$

1st fifteen is sufficient for most of applications.



## Design Procedure for Kaiser Window



Find

(1) The normalized transition BW

$$\Delta\Omega = \frac{\Omega_a - \Omega_c}{\Omega_s}$$

(2) Stopband attenuation

$$A = -20 \log_{10} \delta$$

$$\delta = \min(\delta_1, \delta_2)$$

Assume that  $\delta_1 \approx \delta_2$

(3) The order is given by

$$N \approx \frac{A - 7.85}{14.36 \Delta\Omega}$$

(4) Shape parameter  $\beta$  is

$$\beta = \begin{cases} 0.1102 (A - 8.7) & A \geq 50 \\ 0.5842 (A - 21)^{0.4} + 0.07886 (A - 21) & 21 < A < 50 \\ 0 & \text{for } A < 21 \end{cases}$$

example:

Design a LPF using Kaiser window to satisfy

$$\Omega_c = 2000 \text{ rad/sec}$$

$$\Omega_a = 3000 \text{ rad/sec}$$

$$\Omega_s = 20000 \text{ rad/sec}$$

$$A = 50 \text{ dB}$$

$$\Delta\Omega = \frac{\Omega_a - \Omega_c}{\Omega_s} = 0.05$$

$$N \approx \frac{A - 7.95}{14.36 \Delta\Omega} = \frac{50 - 7.95}{14.36 (0.05)} \approx 59$$

$$\beta = 0.102 (50 - 8.7) \approx 4.55$$

$$H(z) = z^{-\frac{(N-1)}{2}} \sum_{n=0}^{\frac{(N-1)}{2}} \frac{a_n}{2} [z^n + z^{-n}]$$

Transfer function for all window methods

Transfer function of the designed filter where

$$a_0 = W_k(\omega) h_d(\omega)$$

$$a_n = 2 W_k(n) h_d(n)$$

Disadvantages of Window methods:

(1) It is very difficult to find coefficients  $h_d(n)$  accurately

(2) It cannot get rid of Gibbs phenomenon.

\* Kaiser window gives the best result of all other windows.

(b)  $N$  : Even

$$H(e^{j\Omega}) = e^{-j\Omega \frac{(N-1)}{2}} e^{j\pi/2} \sum_{n=1}^{N/2} \theta(n) \sin[\Omega(n-\frac{1}{2})]$$

Where

$$\theta(n) \triangleq 2h(\frac{N}{2}-n), \quad n \in [1, \frac{N}{2}]$$

In this case at  $\Omega = 0$ ,  $H(e^{j\Omega}) = 0$ .

### Design methods

- 1- Windowing
- 2- Frequency Sampling method
- 3- Computer Aided Design methods.

### Frequency Sampling method

*In ECE 412 notes*

Idea: Given the frequency response of the desired filter,  $H_{des}(e^{j\Omega})$ , sample it to obtain  $H(k)$  and then take IDFT of  $\{H(k)\}$  to get  $\{h(n)\}$

Note that  $\{h(n)\}$  and  $\{H(k)\}$  are assumed to be finite extent sequences.

Let the transfer function of the FIR filter be

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

We know that

$$H(k) = H(z) \Big|_{z = e^{j\frac{2\pi k}{N}}}$$

## Direct Method

## Computer Aided Optimization

McClellan - prices

- (a) Bubble Exchange Algorithm - McCeller and Parks  
(b) Linear Programming

## Chebyshev Approximation

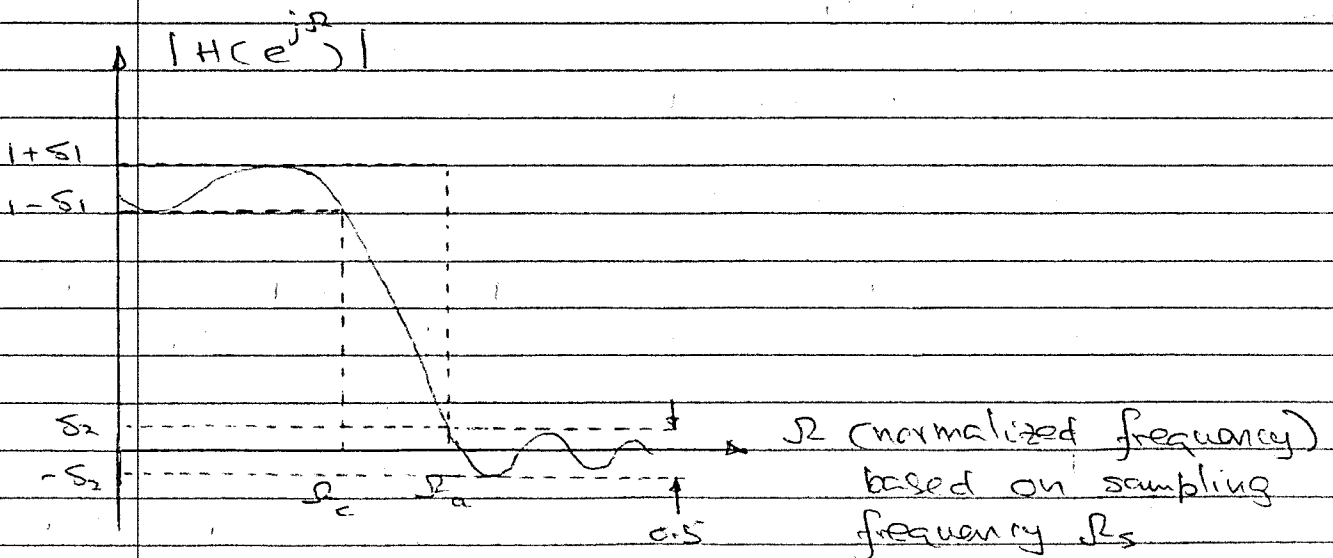
Consider a linear phase FIR filter with  $N = \text{odd}$  and half symmetric.

$$H(e^{j\Omega}) = e^{-j\Omega \frac{(N-1)}{2}} \sum_{n=0}^{N-1} \alpha(n) \cos \Omega n$$

$$d(n) = 2h\left(\frac{N-1}{2} - n\right) \quad n \in \left[1, \frac{N-1}{2}\right]$$

$$x(0) = h \left( \frac{N-1}{2} \right)$$

objective: Find  $\{h_{nm}\}$  or  $\{x_{nm}\}$  so that  $H(e^{j\omega})$  has certain desired characteristics.





$S_r$ : allowed passband ripple  
 $S_s$ : allowed stopband ripple  
 $\Omega_p$ : desired passband edge  
 $\Omega_s$ : desired stopband edge

Define

$$B_p = \{ \Omega : 0 \leq \Omega \leq \Omega_p \}$$

$$B_s = \{ \Omega : \Omega_s \leq \Omega \leq 0.5 \} \quad F = B_p \cup B_s$$

Given  $H_D(e^{j\Omega})$  as the desired frequency response  
 and a positive weight function  $W(e^{j\Omega})$ , then  
 design  $\tilde{H}(e^{j\Omega})$  Find  $\alpha(n)$

$$|\tilde{H}(e^{j\Omega})| = \left| \sum_{n=0}^{(N-1)/2} \alpha(n) \cos \Omega n \right|$$

so that

$$E(e^{j\Omega}) = \frac{W(e^{j\Omega})}{E(e^{j\Omega})} [\tilde{H}(e^{j\Omega}) - H_D(e^{j\Omega})]$$

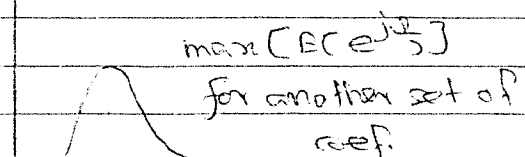
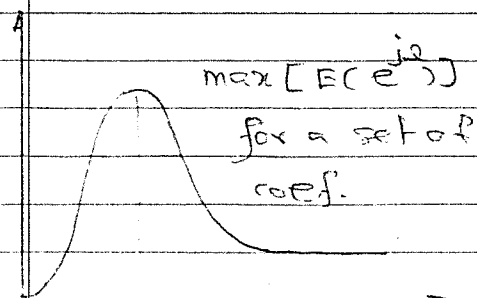
$$\|E(e^{j\Omega})\|_{\infty} = \max_{\Omega \in F} \left[ W(e^{j\Omega}) |\tilde{H}(e^{j\Omega}) - H_D(e^{j\Omega})| \right]$$

$\|E\|$  is minimized.

$$F = B_p \cup B_s \quad \text{and}$$

$L_{\infty}$  norm is defined

$$\|E(e^{j\Omega})\|_{\infty} = \min_{\{\text{coeff. } \alpha(k)\}} \left[ \max_{\Omega \in F} |E(e^{j\Omega})| \right]$$



Examples for  $H_D(e^{j\Omega})$  and  $w(e^{j\Omega})$

$$H_D(e^{j\Omega}) = \begin{cases} 1 & \Omega \in B_P \\ 0 & \Omega \in B_S \end{cases}$$

$$w(e^{j\Omega}) = \begin{cases} \frac{S_2/S_1}{\sqrt{K}} & \Omega \in B_P \\ 1 & \Omega \in B_S \end{cases}$$

$$K = \frac{S_1}{S_2} \quad S_1 < S_2$$

### Number of Extrema

For an optimal linear phase FIR filter, the error function has at least  $(M+1)$  extrema, where

$$M = \left( \frac{N-1}{2} \right)$$

$$|H(e^{j\Omega})| = \sum_{n=0}^M \alpha'_n (\cos \Omega)^n$$

$$\frac{d|H(e^{j\Omega})|}{d\Omega} = -\sin \Omega \sum_{n=1}^M n \alpha'_n (\cos \Omega)^{n-1}$$

can show that above  $f'$  has  $n$  extrema.

# \* Alternation Theorem

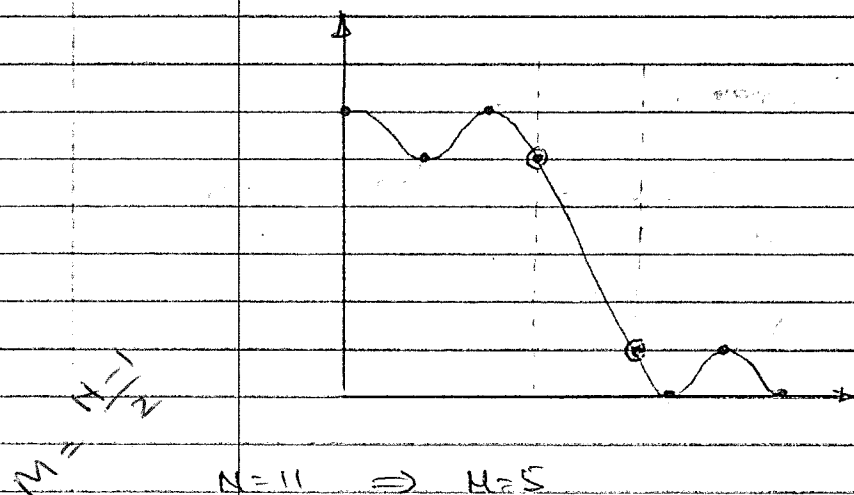
Let  $F \in [0, 1/2]$ . For  $H(e^{j\omega})$  to be the unique best approximation (weighted chebyshev) on  $F$  to  $H_d(e^{j\omega})$  it is necessary and sufficient that the error function  $E(e^{j\omega})$  exhibit on  $F$  at least  $(M+2)$  "alternations".

$$i \quad E(e^{j\omega_i}) = -E(e^{j\omega_{i-1}}) = \pm \|E\|$$

with  $\omega_0 \leq \omega_1 \leq \omega_2 \dots \leq \omega_{M+1}$ ,  $\omega_i \in F$

where  $\|E\| = \max_{\omega \in F} |E(e^{j\omega})|$

example:



$$NP=3$$

$$NS=3$$

two extra points  
where alternation  
change sign.

This kind of filters are known as extra ripple filter  
 $(M+3)$  alternations

$$|H(e^{j\omega})| = \left| \sum_{n=0}^5 a_n \cos n\omega \right|$$

## Remez Exchange Algorithm for optimal FIR filter Design

Assume  $(M+2)$  points  $(M+3)$  for extra ripple case) of alternations are approximately known. i.e.

$\{\Omega_i, i=0, 1, \dots, M+1\}$  and the error at these points has a magnitude of  $S$ . Then at the  $i$ th step of the algorithm,

$$W(e^{j\Omega_i}) | H(e^{j\Omega_i}) - H_d(e^{j\Omega_i}) | = (-1)^i S$$

$$i=0, 1, \dots, M+1$$

Arranging these equations in matrix and using

$$H(e^{j\Omega}) = \sum_{n=0}^M x(n) \cos \Omega n$$

1	$\cos \Omega_0 \quad \cos 2\Omega_0 \quad \dots \quad \cos M\Omega_0$	$\frac{1}{W(e^{j\Omega_0})}$	$x(0)$	$H_d(e^{j\Omega_0})$
1	$\cos \Omega_1 \quad \cos 2\Omega_1 \quad \dots \quad \cos M\Omega_1$	$\frac{-1}{W(e^{j\Omega_1})}$	$x(1)$	$H_d(e^{j\Omega_1})$
$\vdots$			$\vdots$	$\vdots$
1	$\cos \Omega_{M+1} \quad \cos 2\Omega_{M+1} \quad \dots \quad \cos M\Omega_{M+1}$	$\frac{(-1)^{M+1}}{W(e^{j\Omega_{M+1}})}$	$x(M+1)$	$H_d(e^{j\Omega_{M+1}})$
		$S$		

paper: Chebyshev approximation for non-recessive digital filters