

# BICEP Array cryostat and mount design

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## ABSTRACT

BICEP Array is a Cosmic Microwave Background (CMB) polarization experiment that will begin observing at the South Pole in early 2019. This experiment replaces the five BICEP2 style receivers that compose the Keck Array with four larger BICEP3 style receivers observing at six frequencies from 30 to 270GHz. The 95GHz and 150GHz receivers will continue to push the already deep BICEP/Keck CMB maps while the 30/40GHz and 220/270GHz receivers will constrain the synchrotron and galactic dust foregrounds respectively. Here we report on the design and performance of the BICEP Array instruments focusing on the mount and cryostat systems.

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## 1. INTRODUCTION

### 2. THE BICEP/Keck EXPERIMENTS

The BICEP/Keck experiments are a staged series of microwave telescopes that observe the CMB from the geographic South Pole. Each successive generation of telescope builds upon the experience gained with the previous while providing increasingly sensitive data. The experiments target degree-scale B-mode polarization in the CMB which could have been generated by primordial gravitational waves during the epoch of inflation. Detection of this signal requires separating the Inflationary Gravitational Wave (IGW) component from foreground sources such as polarized galactic dust emission and galactic synchrotron radiation, as well as the gravitational lensing component. Foreground signal exhibits strong frequency dependence (see Figure ??) which allows these components to be isolated from the IGW signal by observing the microwave sky across a range of frequencies. *Keck Array* consists of five BICEP2 style receivers with observations spread across four frequency bands (95, 150, 220, and 270 GHz). In combination with the BICEP2 data the *Keck Array* has published the strictest constraint on this signal to date of  $r < 0.07$ .<sup>7</sup> BICEP Array builds on the success of the *Keck Array* by deploying four BICEP3 style receivers and expanding observations into two additional frequency bands at 30, and 40 GHz. Extrapolating from achieved performance, BICEP Array is projected to reach  $\sigma(r) < 0.004$ , either detecting the IGW signal or improving the constraint to  $r < 0.008$ .

### 3. CRYOSTAT DESIGN

BICEP array continues the successful design philosophy of the previous Bicep / Keck receivers. An 80" tall vacuum shell contains two nested stages with nominal operating temperatures of 50K and 4K which accommodate optical elements and shield the sub-Kelvin receiver. A cross section of the cryostat is shown in Figure ?. The top section of the vacuum jacket houses the vacuum window and a stack of Zotefoam filters which reduce infrared loading onto the colder stages. The use of low-conductivity structural supports keeps the interior stages sufficiently supported while conducting only a small amount of heat from the room temperature vacuum vessel. These supports are described in more detail in section ?. The intermediate 50K stage serves as a radiation shield for the interior 4K stage. The lower  $\sim 70\%$  of this stage is wrapped with a 0.04" thick magnetic shield composed of Amuneal A4K. The top of this stage additionally accommodates an Alumina filter to further reduce infrared loading onto the sub-Kelvin receiver. The 4K stage serves as a second radiation shield while also providing mounting interfaces for two Alumina lenses and optical baffling.

The cryostat design enables ease of access to the focal plane assembly without disturbing the majority of thermal joints or the back-end cabling. The cryostat disassembles by lifting off shells successively from the outside in, leaving a stand-alone base behind which contains the sub-Kelvin focal plane assembly, readout electronics, and the cooling system as shown in Figure ?. In this state, the focal plane and detector modules may be freely accessed for maintenance and other technical activities. Access to the underside of the focal plane and the readout electronics is provided by hatches on the bottom side of the Vacuum shell and 50K bases. This scheme significantly reduces the time required for disassembly when accessing the focal plane and re-assembly afterwards by allowing critical thermal junctions and difficult part matings to remain undisrupted.

### 3.1 Thermal Architecture

The 50K and 4K radiation shields are cooled by the first and second stages respectively of a Cryomech PT415-RM Pulse Tube cooler. This cryocooler is capable of maintaining a first stage temperature of  $< 45\text{K}$  under a 40W load and a second stage temperature of  $< 4\text{K}$  under a 1.5W load. The cooler of these two stages is required to maintain a sufficiently cold temperature to allow the operation of a three stage Helium sorption fridge which cools the sub-Kelvin receiver. The interior stages must therefore be well insulated in order to stay within the thermal budget. Table ?? breaks down the thermal loading onto the 4K and 50K stages. Individual components are described below.

The radiation absorbed by the interior stages is reduced by the use of Multi Layer Insulation (MLI) wrapped around the outside of the 50K and 4K stages. Where there is insufficient room for uncompressed insulation, high emissivity Aluminum tape is used on parallel faces to decrease the radiation absorbed by the lower temperature surface. The radiation shields are additionally attached to higher temperature stages via a low thermal conductivity support system. The front end of each shell is constrained by thin Ti-Al-4V straps which are allowed to flex along the axial direction of the cryostat to absorb differential thermal contraction. At the back end the 50K and 4K stages are supported by six trusses. Each truss has two high tensile strength / thermal conductivity rods bonded to Aluminum blocks with Stycast epoxy. We use G10-FR4 for the backend supports between the Vacuum shell and the 50K radiation shield but switch to Carbon Fiber between the 50K and 4K shells due to the former's lower thermal conductivity at low temperatures. Figure ?? shows fabricated examples of the front and back-end supports.

In addition to providing radiation shielding and mount points for low temperature optics, the 50K and 4K stages provide natural heat sinks for the cryocables that connect the sub-Kelvin electronics to the exterior - room temperature - data acquisition system. By sinking the cryocables to the 50K stage the conductive loading onto the 50K stage is significantly reduced. Likewise, the heatsinks on the 4K stage significantly reduce the conductive loading onto the sub-Kelvin receiver.

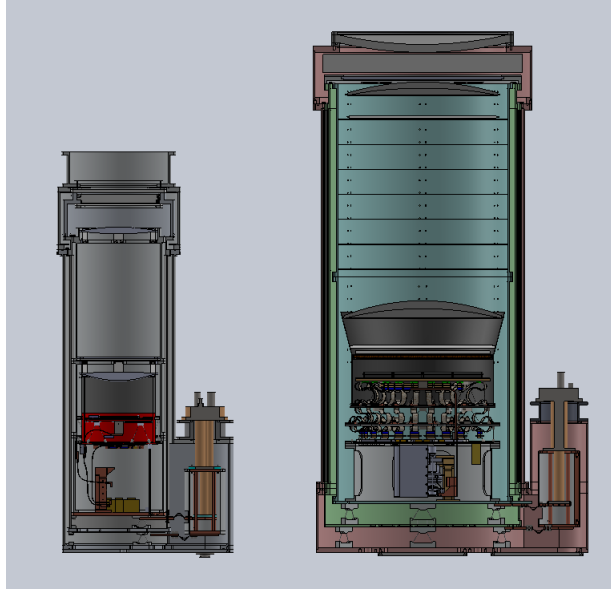


Figure 1. A CAD cross section of a single Keck Array receiver (left) and a Bicep Array receiver (right). The Bicep Array cryostats more than double the volume of their Keck Array counterparts with mapping speed equal to  $\sim 5$  times that of a Keck receiver at the same frequency.

### 3.2 Copper Braid Heat Straps

The heat straps connecting the pulse tube cooler to the 50K and 4K stages of the cryostat needs to have large thermal conductance but also be fairly flexible to suppress vibrations transmitted to the focal plane. BICEP

Array uses custom made Oxygen Free High thermal Conductivity (OFHC) Copper assemblies each composed of multiple straps. As shown in Figure ?? each heat strap consists of two end blocks connected by a series of multi-layered braided wire straps. The braided straps comprise seven layers of OFHC braid pressure fused into a small diameter OFHC pipe section on either end. The pressure fusing is performed by a hydraulic press under a load of 20 Tons while external constraint is provided by a Steel die. We have been able to achieve thermal conductance of  $G = 600 \frac{\text{mW}}{\text{K}}$  @4K per strap in laboratory tests.

The heat straps in the Bicep Array cryostat combine a number of these straps to achieve high thermal conductance. Two layers of braided straps are sandwiched around an OFHC plate on both ends. These plates provide mounting interfaces to the rest of the cryostat and the pulse tube cooler. Stainless steel plates on the top and bottom sides of this interface allow the use of 1/4" stainless steel bolts to create a high pressure joint and reduce thermal contact resistance. Figure ?? shows a fully assembled heat strap assembly that interfaces between the 4K radiation shield and the 2nd stage of the pulse tube.

#### 4. MOUNT

The larger size of the BICEP Array as compared to the *Keck Array* it replaces requires a larger motorized platform for operation. Designed by Eric Chauvin, the new BICEP Array mount uses the same three axis design as the previous BICEP/*Keck* experiments which augments the azimuth and elevation axes with rotation about the boresight of the array. A cross section of the new mount assembly is shown below in Figure 2. As with previous BICEP/*Keck* experiments, the cryostats are enclosed within an accordion-like environmental shield which co-rotates in azimuth and flexes as the mount tips down in elevation. A separate central plate provides a mounting interface for four optical baffles - one per receiver - and co-rotates with the receivers about the array boresight.

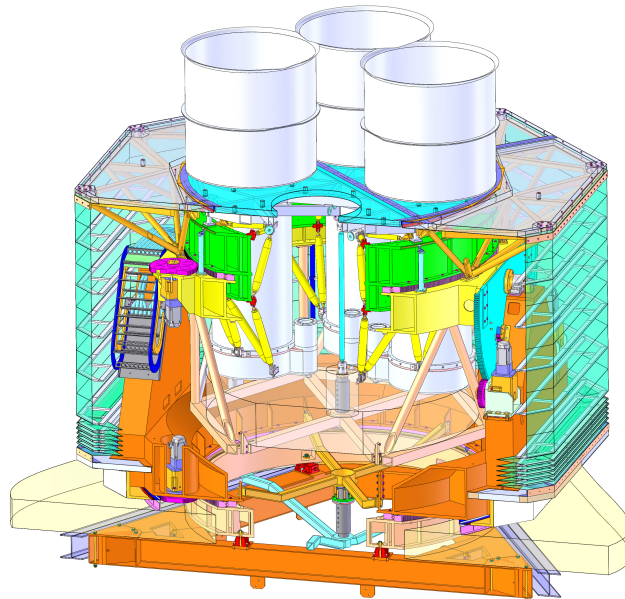


Figure 2. A CAD rendering of the new Bicep Array. The surrounding accordion-like environmental shield is shown in teal while the two rotary unions are depicted in gray and can be seen along the central axis of the mount.

The BICEP Arraymount includes two separate rotary unions which allow continuous rotation about the azimuth and deck axes without the need for a cable wrap. These rotary unions were designed at DSTI and each contain 10 Helium channels. Eight of these connect the pulse tubes and their compressors while two channels serve as pressure guards. An additional Nitrogen channel provides a pressurized environment on the backside of thin membrane structures which shield the receivers' vacuum windows from the Antarctic winter. Inclusion of

slip rings at both ends of the union additionally provide data and power connections to electronics fixed to the same structure as the cryostats. These rotary unions allow the Helium compressors - required to operate the pulse tube coolers - to sit well below the mount structure in the stationary tower. Helium lines route upwards into the lower fixed half of the first rotary union and then out through the upper half which rotates in Azimuth along with the receivers. The hoses from the upper half are then routed through a short cable chain that provides flexure when rotating in elevation. The second rotary union is then similarly connected with the free section rotating about the array boresight.

## 5. OPERATIONS

BICEP Array will consist of four receivers observing in 6 frequency bands. Two receivers will continue to observe in the 95 and 150 GHz bands where the BICEP/*Keck* maps are deepest and where combined foreground signal is at a minimum. These will be augmented by two dual-band receivers at 30/40 GHz and 220/270 GHz with the two frequencies interleaved in a checkerboard pattern. With the increased sensitivity at 95 and 150 GHz these two additional receivers will be required to push constraints on polarized emission from galactic synchrotron and dust further than the currently available data. The 30/40 GHz receiver will extend the observations into two new bands at which the synchrotron foreground is expected to dominate. The *Keck Array* is already observing in the 220 and 270 GHz bands. However with significantly increased throughput and a detector count of over 9 times the entire *Keck Array*, the dual band 220/270 GHz Bicep Array receiver will rapidly eclipse current sensitivity. In only a few days of observation, this receiver will surpass the dust sensitivity of the *Planck* 353 GHz data in the BICEP/*Keck* field.

The observing power of BICEP Array will be concentrated on the same  $\sim 400 \text{ deg}^2$  patch of sky as the existing BICEP/*Keck* data. By directly observing cosmological foregrounds with the new dual band receivers in the patch at which the BICEP/*Keck* data is already the deepest we will be able to directly constrain these foregrounds in our own patch of sky, significantly reducing the effect of any spatial variation in the foregrounds' spectral energy distribution. Increasing foreground constraints will be complemented by simultaneously increasing sensitivity to  $r$  with the single band receivers.