

# EE101: Circuit Analysis

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*References: L. Bobrow*

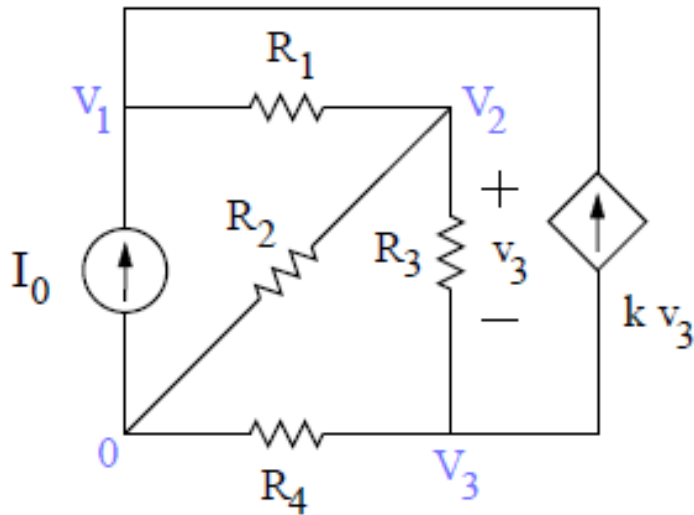
# Outline

- Nodal analysis
- Mesh analysis
- Thevenin and Norton theorems
- Maximum power transfer
- Linearity and superposition

# Nodal analysis

- Application of Kirchhoff's current law (KCL)
- Variables are voltages
- Solve a set of simultaneous equations
- Can be used for any circuit
  - Non-planar also  $\rightarrow$  element crossing over another

# Nodal analysis: Example



- Define a reference node: “0”
- Define node voltages  $V_1$ ,  $V_2$  for other nodes
- Write KCL for the non-reference nodes in terms of node voltages

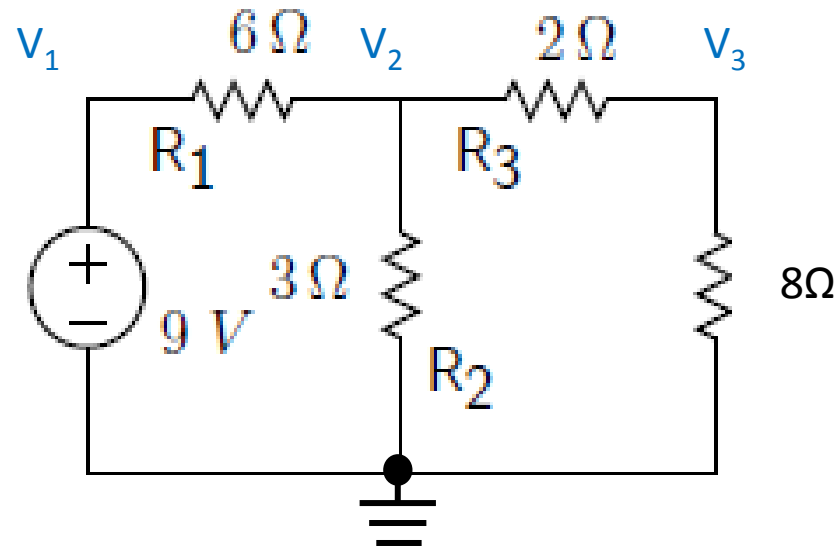
$$\frac{1}{R_1}(V_1 - V_2) - I_0 - k(V_2 - V_3) = 0,$$

$$\frac{1}{R_1}(V_2 - V_1) + \frac{1}{R_3}(V_2 - V_3) + \frac{1}{R_2}(V_2) = 0,$$

$$k(V_2 - V_3) + \frac{1}{R_3}(V_3 - V_2) + \frac{1}{R_4}(V_3) = 0.$$

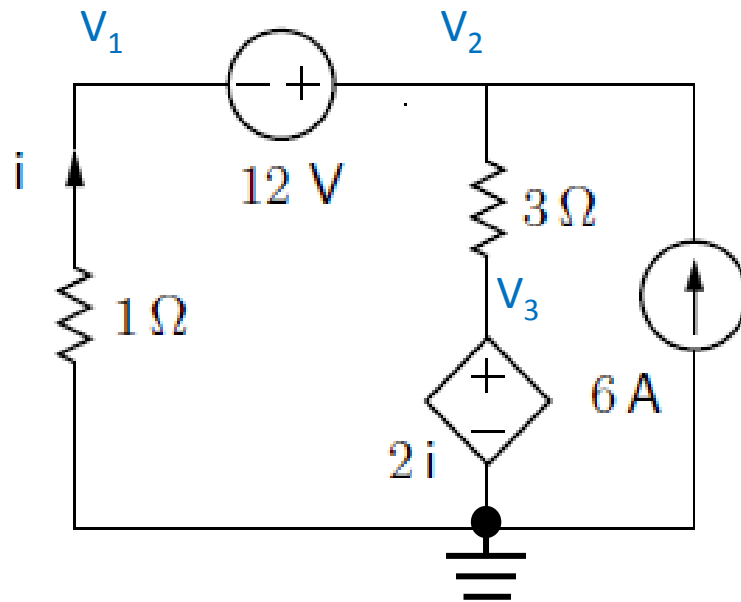
- Solve (n-1) simultaneous eqns for the node voltages  $\rightarrow$  currents

# Nodal analysis with voltage sources



- Voltage source where one terminal is connected to reference node
- By inspection,  $V_1 = 9\text{ V}$
- Only two unknown variables remain
  - $V_2$  and  $V_3$

# Nodal analysis with voltage sources



$$V_2 - V_1 = 12$$

$$-V_1 + 6 = (V_2 - V_3)/3 \text{ at node } V_2$$

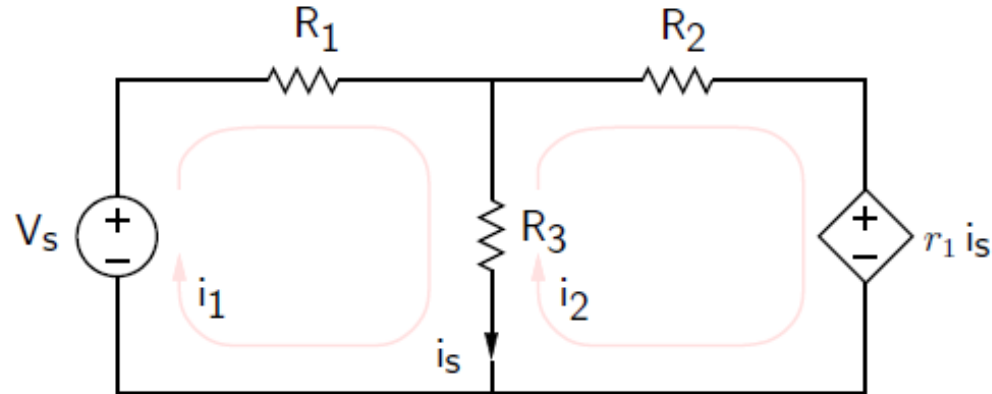
$$V_3 = 2i = -2V_1 \text{ at node } V_3$$

- Voltage source between two non-reference nodes
- By inspection,  $V_2 - V_1 = 12 \text{ V}$

# Mesh analysis

- Application of Kirchhoff's voltage law (KVL)
- Variables are currents
- Solve a set of simultaneous equations
- Can***not*** be used for any circuit
  - Planar circuits → element not crossing over another

# Mesh analysis: An example

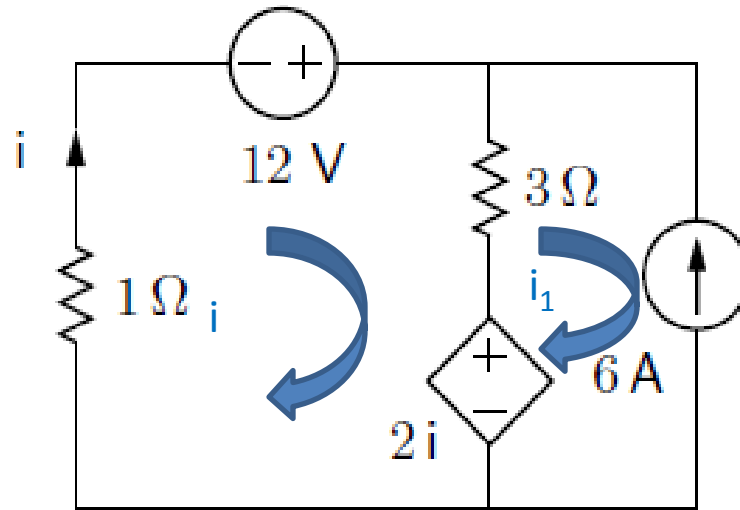


- 2D space divided into finite and infinite windows (surrounding the ckt)  $\rightarrow$  meshes
- $i_1$  and  $i_2$  are mesh currents (clock or anti-clockwise)
  - Current through  $R_3$  is  $i_s = i_1 - i_2$
- Write KVL for the meshes and solve for  $i_1$  and  $i_2$  (m equations for m meshes)

$$\begin{aligned} -V_s + i_1 R_1 + (i_1 - i_2) R_3 &= 0, \\ R_2 i_2 + r_1 (i_1 - i_2) + (i_2 - i_1) R_3 &= 0. \end{aligned}$$

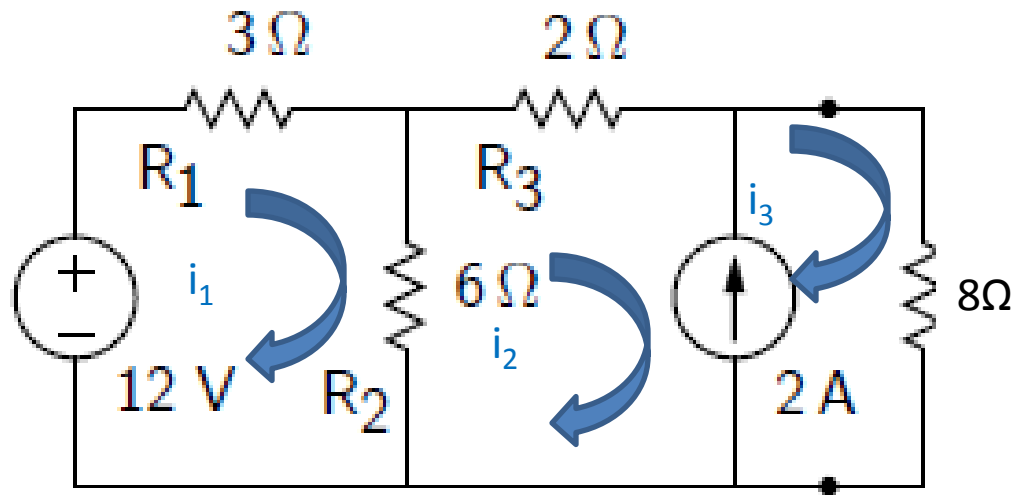


# Mesh analysis with current sources



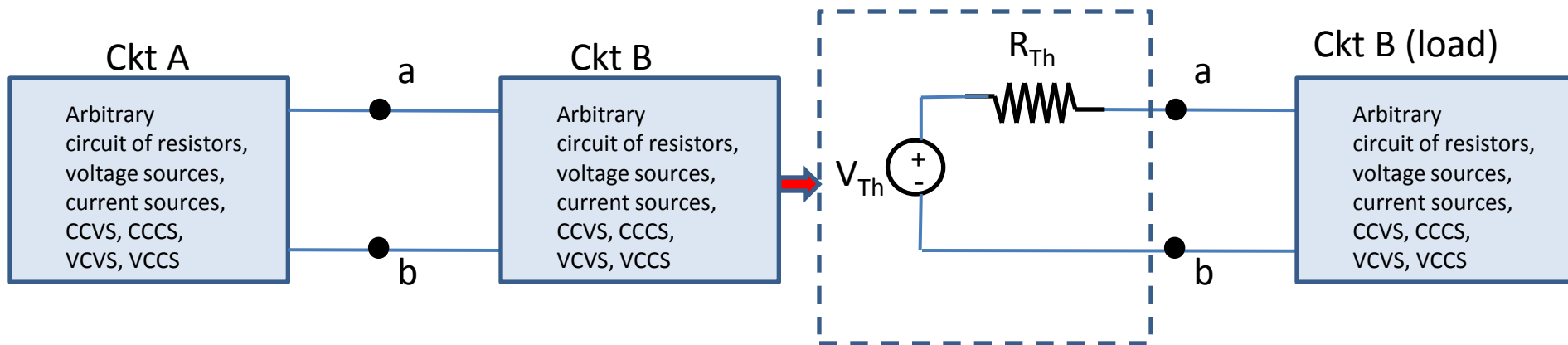
- Current source part of a single mesh
- By inspection,  $i_1 = -6\text{ A}$
- Only one unknown quantity  $\rightarrow i$ , one mesh

# Mesh analysis with current sources



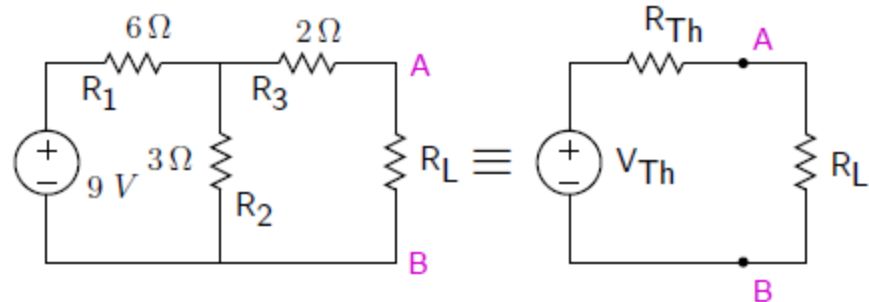
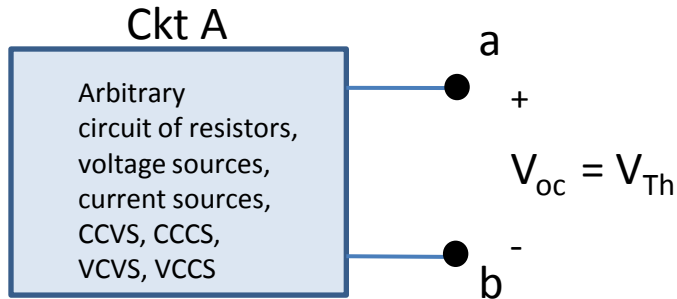
- Current source is part of two meshes
- By inspection,  
$$-i_3 - i_2 = 2$$
- Remaining two equations can be obtained from meshes for  $i_1$  and  $i_2$

# Thevenin's theorem

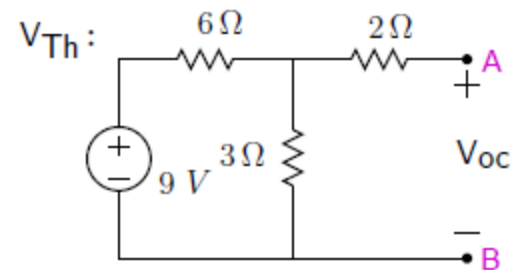


- Circuit A contains no dependent source that depends on a variable in Circuit B and vice versa
- Series combination of voltage source  $V_{Th}$  and  $R_{Th}$  is called the Thevenin equivalent of circuit A
  - $V_{Th} \rightarrow$  Open circuit voltage, also called  $V_{oc}$
  - $R_{Th} \rightarrow$  Output resistance or Thevenin Resistance, also called  $R_o$

# How to find $V_{Th}$ ?

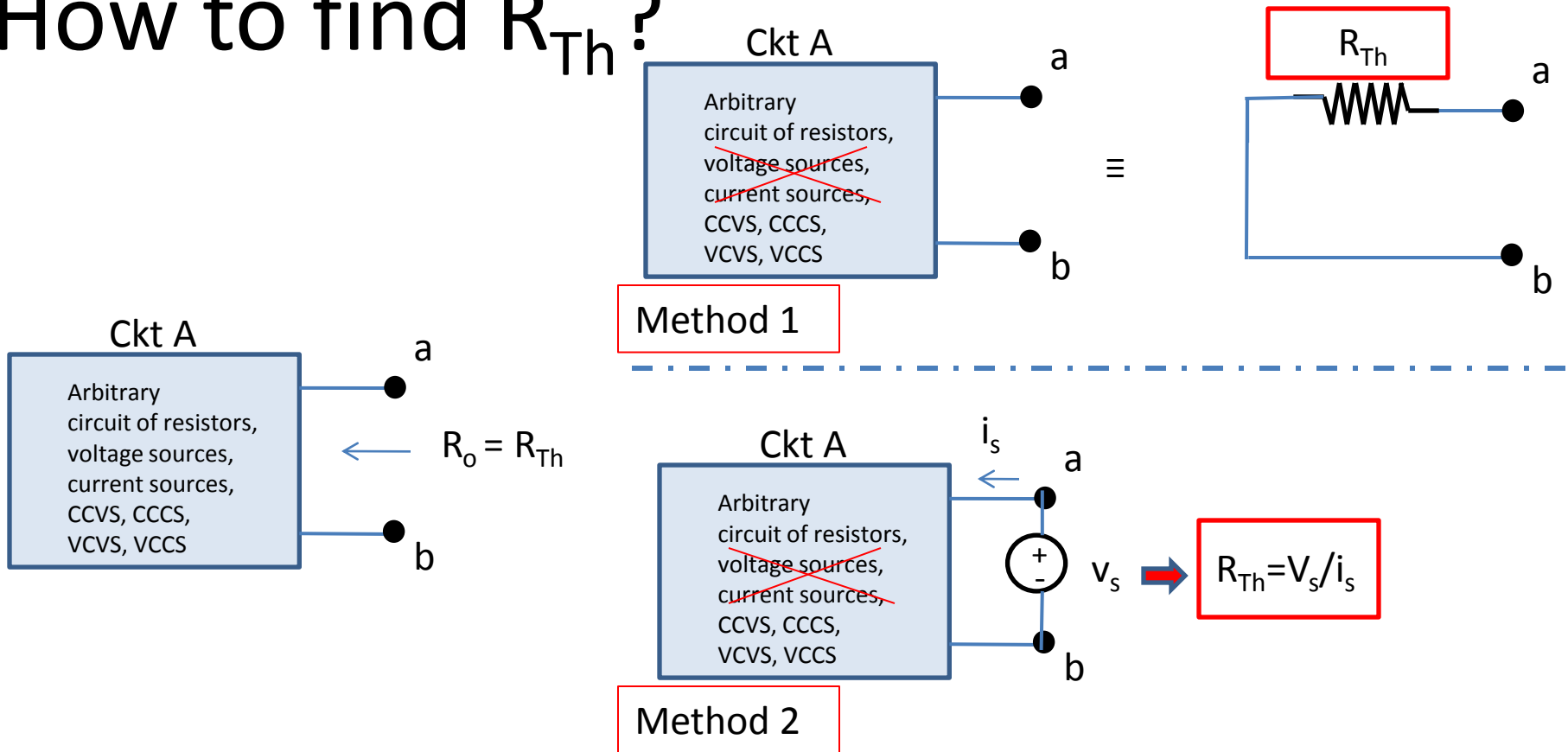


- Simply find the open circuit voltage between a and b.



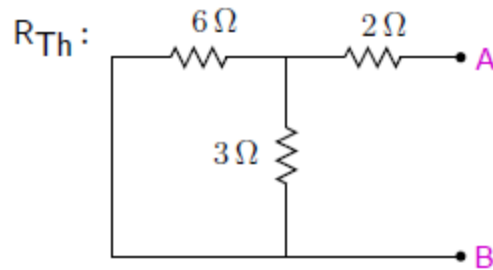
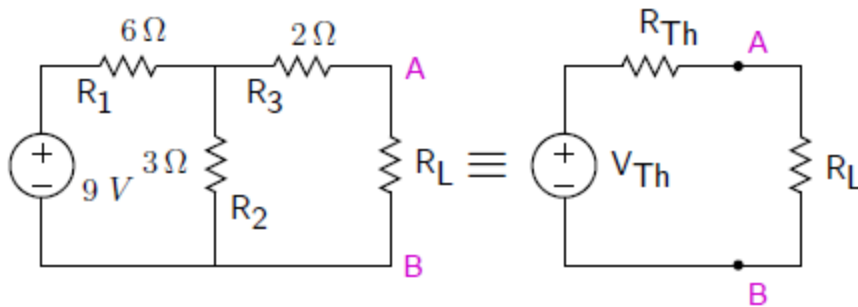
$$V_{oc} = 9V \times \frac{3\Omega}{6\Omega + 3\Omega}$$
$$= 9V \times \frac{1}{3} = 3V$$

# How to find $R_{Th}$ ?



- $R_o$  is the effective resistance of Ckt A as "seen" from a-b
- Method 1:
  - Deactivate all independent sources – short ckt for voltage sources and open ckt for current sources
  - $R_{Th}$  can be found by inspection
- Method 2:
  - Apply an independent voltage test source and taking ratio of voltage to current

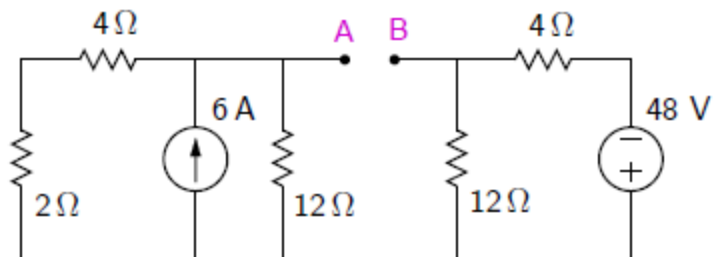
# $R_{Th}$ ( $R_o$ ) Example



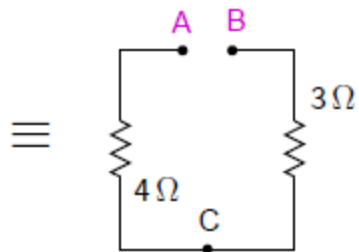
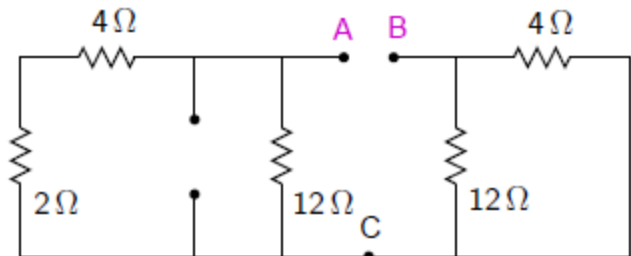
$$\begin{aligned} R_{Th} &= (R_1 \parallel R_2) + R_3 = (3 \parallel 6) + 2 \\ &= 3 \times \left( \frac{1 \times 2}{1 + 2} \right) + 2 = 4 \Omega \end{aligned}$$

- Series and parallel combination of resistors

# Example

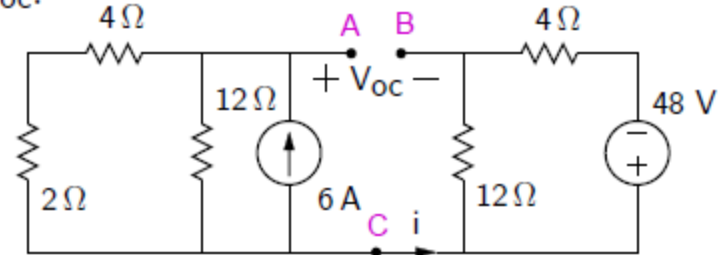


$R_{Th}$ :



$$\Rightarrow R_{Th} = 7\Omega$$

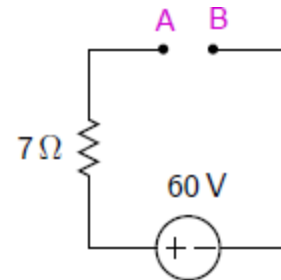
$V_{oc}$ :



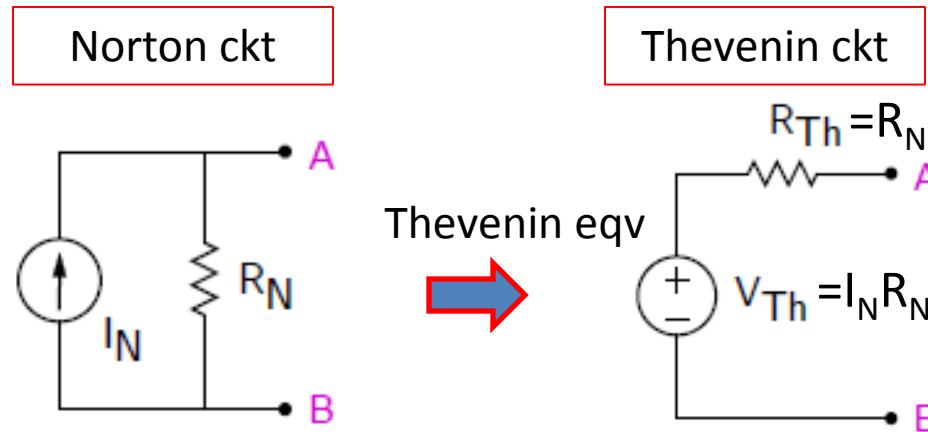
Note:  $i = 0$  (since there is no return path).

$$\begin{aligned} V_{AB} &= V_A - V_B \\ &= (V_A - V_C) + (V_C - V_B) \\ &= V_{AC} + V_{CB} \\ &= 24\text{ V} + 36\text{ V} = 60\text{ V} \end{aligned}$$

$$\begin{aligned} V_{Th} &= 60\text{ V} \\ R_{Th} &= 7\Omega \end{aligned}$$



# Norton's Theorem

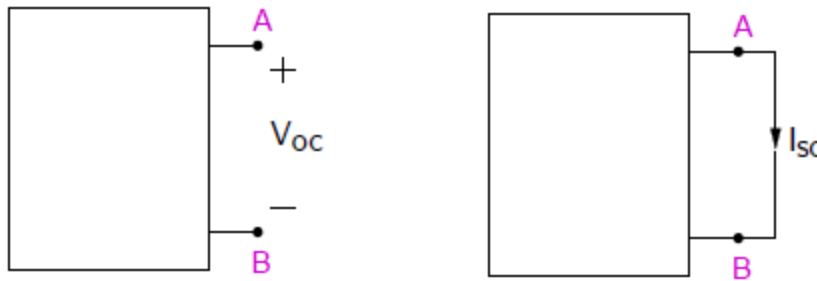


- The two circuits above are equivalent
- $I_N$  is also called “short circuit” current  $I_{sc}$
- Note that  $R_{Th} = V_{Th} / I_N \rightarrow R_{Th} = V_{oc} / I_{sc}$



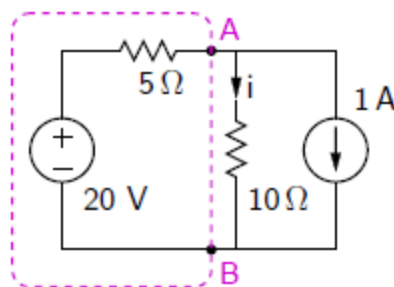
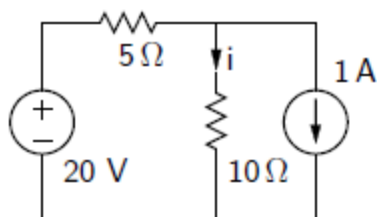
# Method 3 for finding $R_{TH}$

$$R_{TH} = V_{TH} / I_N \rightarrow R_{TH} = V_{OC} / I_{SC}$$



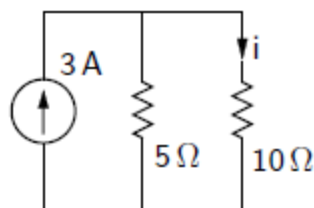
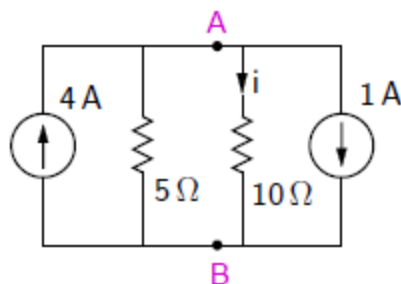
- Find  $V_{OC}$
- Find  $I_{SC}$
- $R_{TH} = V_{OC} / I_{SC}$
- Note that no sources are deactivated in this method

# Example for Norton Equivalent Ckt



$$R_N = 5\ \Omega$$

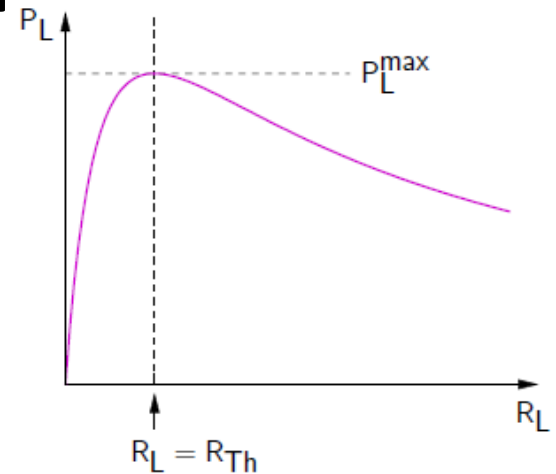
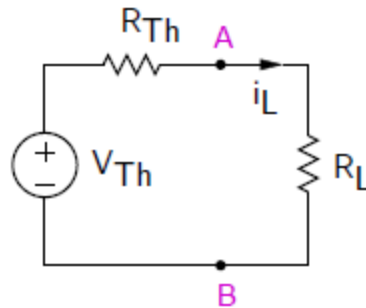
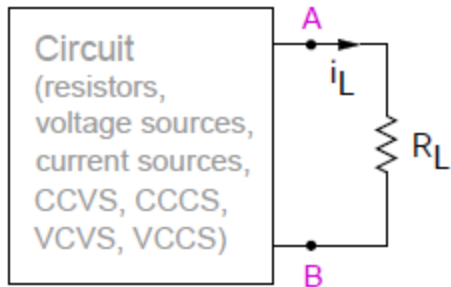
$$I_N = \frac{20\text{ V}}{5\ \Omega} = 4\text{ A}$$



$$i = 3\text{ A} \times \frac{5}{5 + 10}$$

$$= 1\text{ A}$$

# Maximum Power Transfer



$$i_L = \frac{V_{Th}}{R_{Th} + R_L},$$

$$P_L = V_{Th}^2 \times \frac{R_L}{(R_{Th} + R_L)^2}$$

For  $\frac{dP_L}{dR_L} = 0$ , we need

$$\frac{(R_{Th} + R_L)^2 - R_L \times 2(R_{Th} + R_L)}{(R_{Th} + R_L)^4} = 0,$$

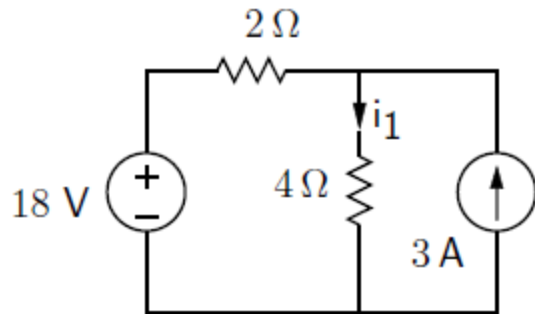
$$R_{Th} + R_L = 2 R_L \Rightarrow R_L = R_{Th}.$$

- Power transferred to the load is  $P_L = i_L^2 R_L$
- For what value of  $R_L$  will the power transferred be maximum?
- Replace with Thevenin equivalent
- What is the maximum power transferred  $\rightarrow P_L^{\max}$ ?

# Linearity and Superposition

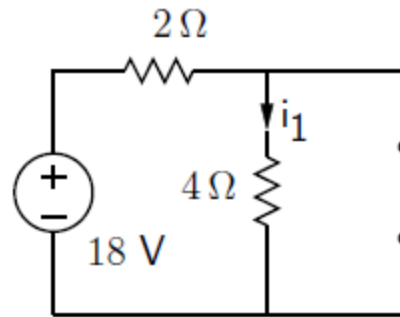
- Circuit containing independent sources, dependent sources, resistors is linear, i.e. system of equations describing the circuit is linear
- The dependent sources are assumed to be linear, i.e.  $v=ai_c^2+b$  will make it non-linear
- For a linear system we can apply the principle of superposition
- For ckts this implies, computing the response for each independent source separately and add the individual contributions to get the final true response.
  - Cannot be applied to dependent sources
  - Superposition corresponds to superposition of response due to independent sources
  - One independent source at a time  $\rightarrow$  deactivate all other independent sources
  - For a current source deactivation  $\rightarrow i_s=0 \rightarrow$  replace with an open circuit
  - For a voltage source deactivation  $\rightarrow v_s=0 \rightarrow$  replace with a short circuit

# Example



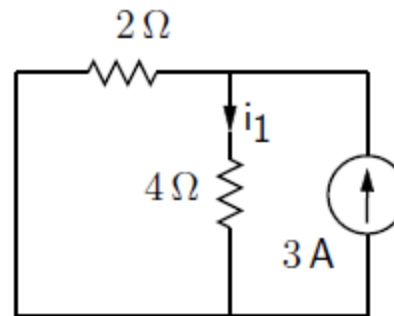
$$i_1^{\text{net}} = i_1^{(1)} + i_1^{(2)} = 3 + 1 = 4 \text{ A}$$

Case 1: Keep  $V_S$ , deactivate  $I_S$ .



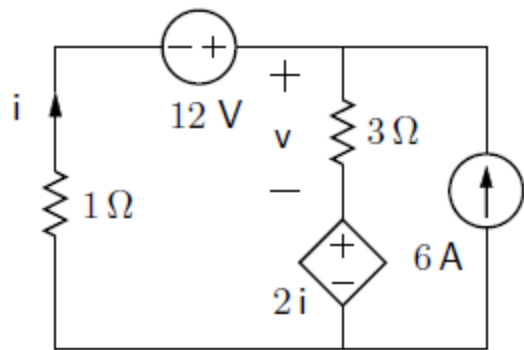
$$i_1^{(1)} = 3 \text{ A}$$

Case 2: Keep  $I_S$ , deactivate  $V_S$ .



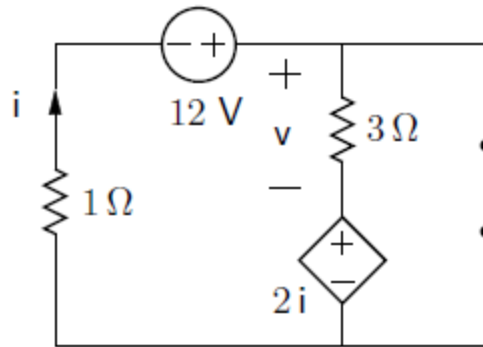
$$i_1^{(2)} = 3 \text{ A} \times \frac{2 \Omega}{2 \Omega + 4 \Omega} = 1 \text{ A}$$

# Example



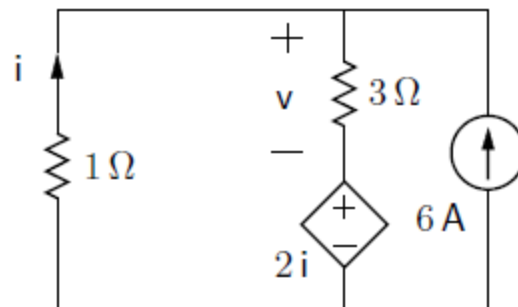
$$v^{\text{net}} = v^{(1)} + v^{(2)} = 6 + 9 = 15 \text{ V}$$

Case 1: Keep  $V_S$ , deactivate  $I_S$ .



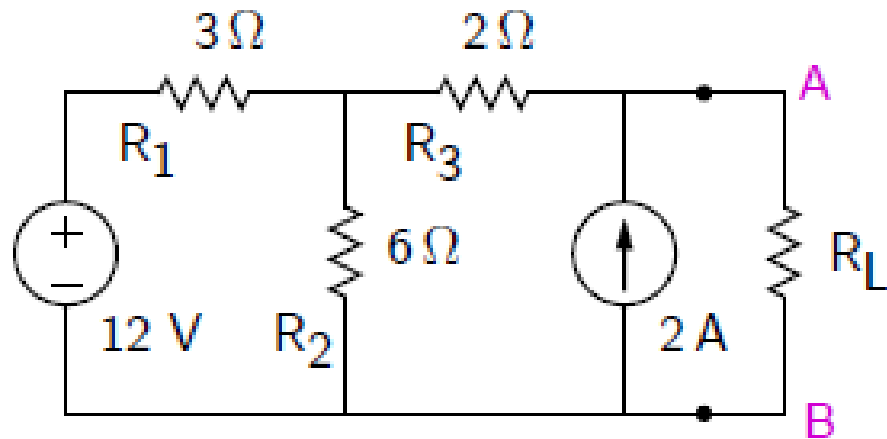
$$\begin{aligned} \text{KVL: } -12 + 3i + 2i + i &= 0 \\ \Rightarrow i &= 2 \text{ A}, v^{(1)} = 6 \text{ V.} \end{aligned}$$

Case 2: Keep  $I_S$ , deactivate  $V_S$ .



$$\begin{aligned} \text{KVL: } i + (6 + i)3 + 2i &= 0 \\ \Rightarrow i &= -3 \text{ A}, v^{(2)} = (-3 + 6) \times 3 = 9 \text{ V.} \end{aligned}$$

Try the following as HW

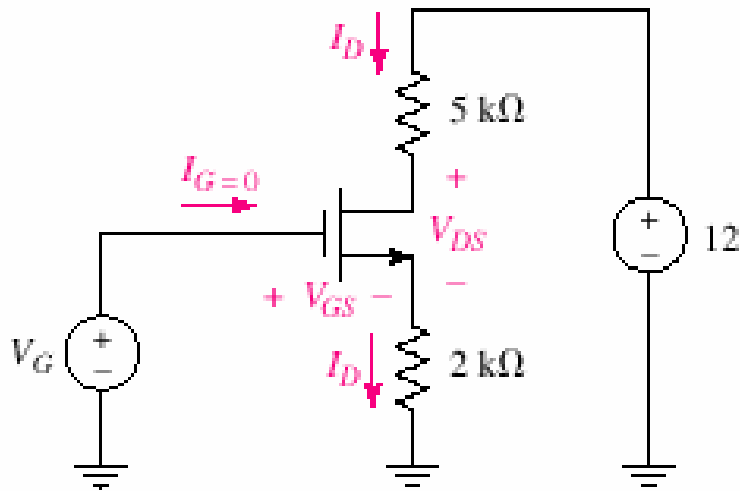


- Find  $R_L$  for which  $P_L$  is maximum

# Backup



# Problem 1



## Solution

(a) By KVL,  $-12 + 5000I_D + V_{DS} + 2000I_D = 0$

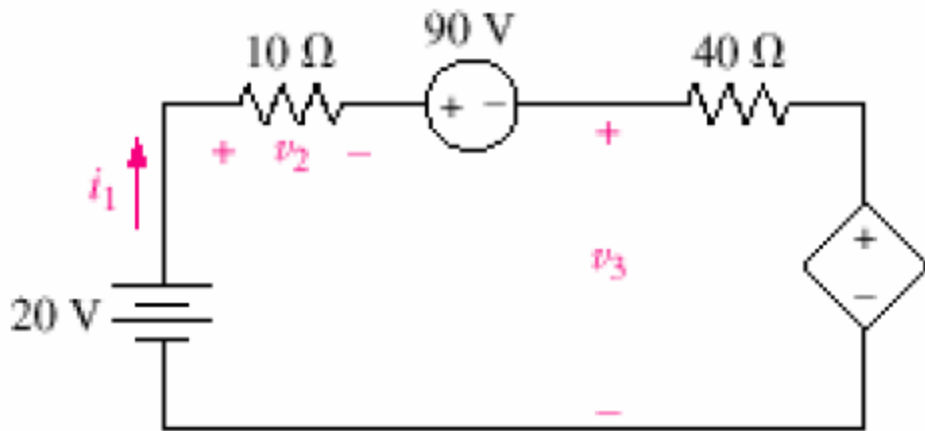
Therefore,  $V_{DS} = 12 - 7(1.5) = 1.5\text{ V}.$

(b) By KVL,  $-V_G + V_{GS} + 2000I_D = 0$

Therefore,  $V_{GS} = V_G - 2(2) = -1\text{ V}.$

(a) If  $I_D = 1.5\text{ mA}$ , compute  $V_{DS}$ . (b) If  $I_D = 2\text{ mA}$  and  $V_G = 3\text{ V}$ , compute  $V_{GS}$ .

# Problem 2



Label the dependent source  $1.8v_3$ . Find  $v_3$  if (a) the 90-V source generates 180 W; (b) the 90-V source absorbs 180 W; (c) the dependent source generates 100 W; (d) the dependent source absorbs 100 W of power.

Applying KVL, we find that

$$-20 + 10i_1 + 90 + 40i_1 + 1.8v_3 = 0 \quad [1]$$

Also, KVL allows us to write

$$v_3 = 40i_1 + 1.8v_3$$

$$v_3 = -50i_1$$

So that we may write Eq. [1] as

$$50i_1 - 1.8(50)i_1 = -70$$

$$\text{or } i_1 = -70/-40 = 1.75 \text{ A.}$$

Since  $v_3 = -50i_1 = -87.5 \text{ V}$ , *no further information is required to determine its value.*

The 90-V source is absorbing  $(90)(i_1) = 157.5 \text{ W}$  of power and the dependent source is absorbing  $(1.8v_3)(i_1) = -275.6 \text{ W}$  of power.

*Therefore, none of the conditions specified in (a) to (d) can be met by this circuit.*