

EE101: RL, RC, RLC Circuit Analysis

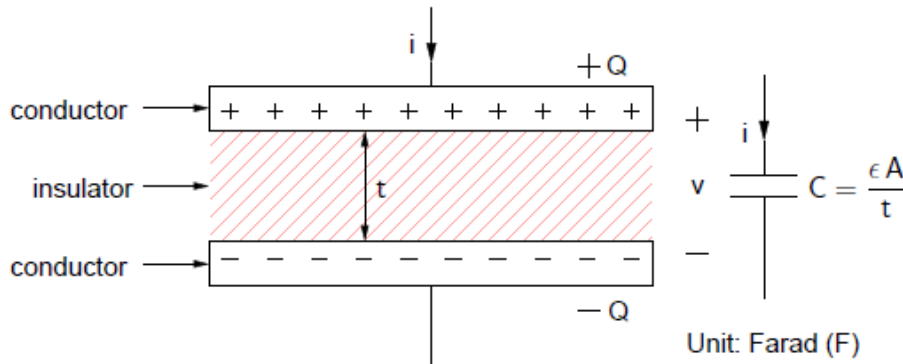
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References: L. Bobrow

Capacitors and Inductors

- Voltage-current has differential/integral (w.r.t time) relationship
 - Currents and voltages that vary with time
- Elements that store energy
- Resistor + L/C \rightarrow First-order circuit
 - First order linear diff eqn
 - Natural response (no source); Complete response (with independent source)
- Two energy storage elements \rightarrow Second order circuit
 - Second order, linear diff eqns
 - Natural and complete response

Capacitors



$$i(t) = C \frac{dv}{dt}$$

$$v(t) = \frac{1}{C} \int i(t) dt$$

$$p(t) = v(t) \times i(t)$$

$$W(t) = \int p(t) dt$$

$$W(t) = \int p(t) dt$$

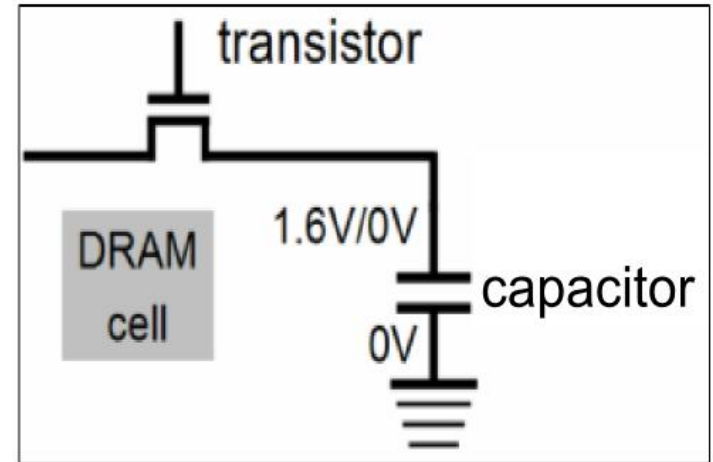
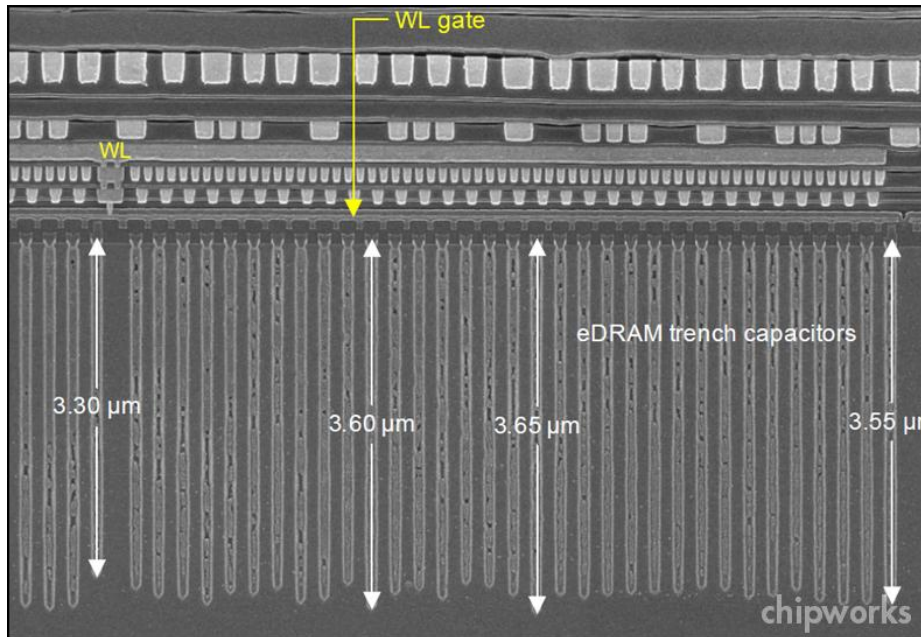
$$= C \int v \frac{dv}{dt} dt$$

$$= C \int v dv$$

$$= \frac{1}{2} C v^2$$

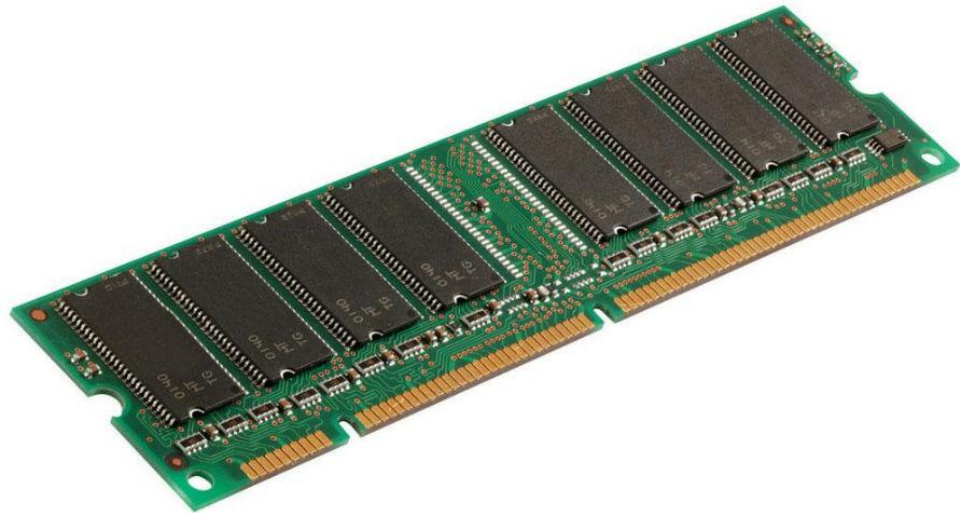
- Available as discrete components as well as in integrated circuits
- Various shapes and sizes, can vary from pF to 10's of uF
 - glass, ceramic, plastic film, air, paper, mica, etc. as dielectrics
- For constant V (dc condition), $i=0 \rightarrow$ open circuit
- Extensive use in
 - Memory applications, power stabilization, analog filters, resonant circuits for frequency tuning etc.

DRAM capacitors in Si



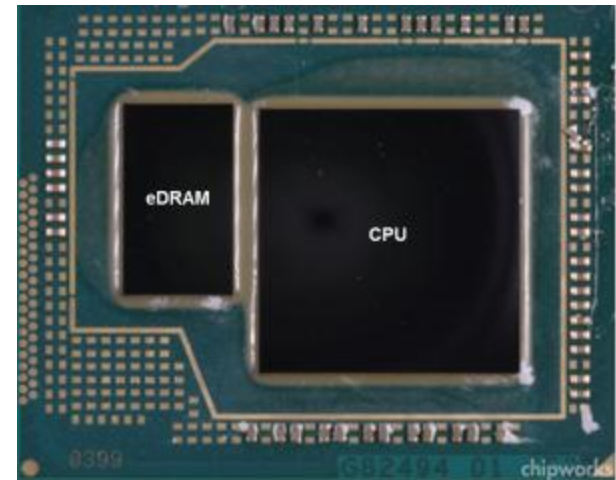
- Charged and Discharged Capacitor \rightarrow stores 1 or 0
- Charge can leak away \rightarrow Volatile memory

Embedded or non-embedded DRAM



Off-chip (non-embedded)

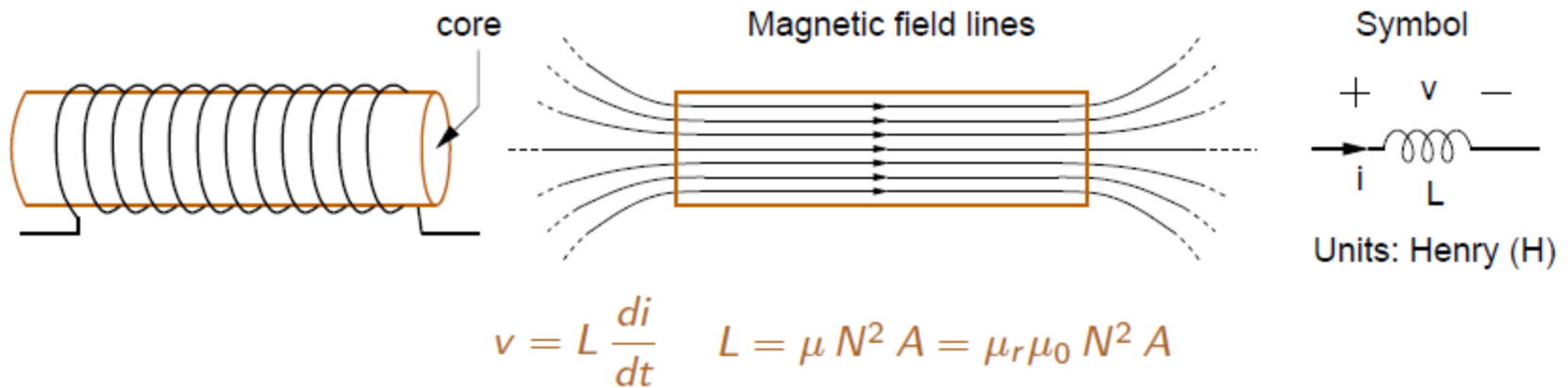
Intel Haswell 22nm CPU



On-chip (embedded)

- State-of-the-art DRAM capacitor technology is integrated with the CPU technology

Inductors



- μ_r can vary from 5000 (Fe) to 10^6 (supermalloy: Ni- 79%, Mo- 5%, Fe)
- For constant I (dc condition), $V=0 \rightarrow$ short circuit
- Extensive use in
 - Analog/RF electronics, power supplies and systems, analog filters, resonant circuits etc.

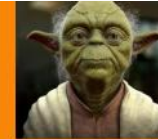
Applications



- Large inductor used in a power station

Applications

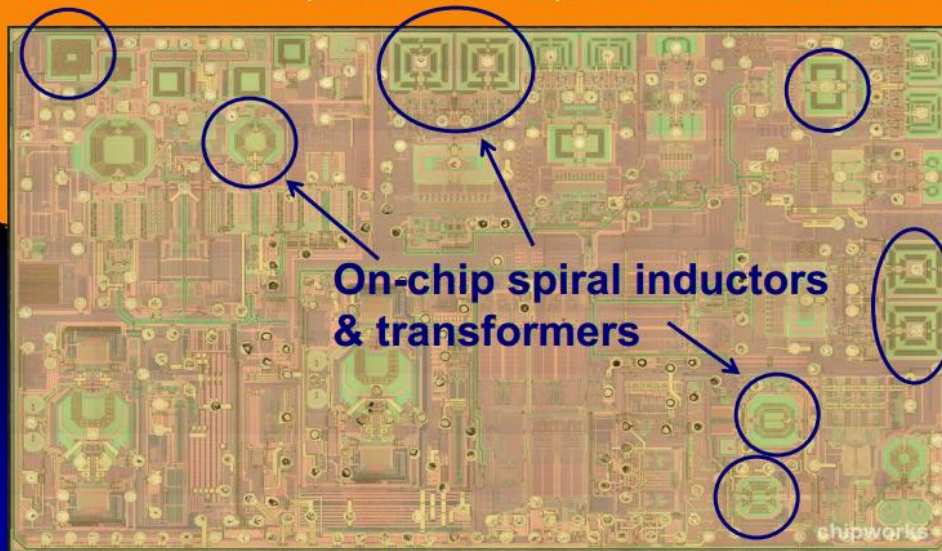
ANALOG / MIXED-SIGNAL / RF SOC SYSTEM-ON-CHIP ENABLING 4G LTE



Qualcomm RTR8600 multi-band/mode RF transceiver



Companion chip MDM9615 4G LTE Modem. This device is a 28-nm LTE (FDD and TDD), HSPA+, EV-DO Rev B, TD-SCMA modem.



**4G Speed in HK
55Mbps!!**



Source: <http://www.chipworks.com/blog/recentteardowns/2012/10/02/apple-iphone-5-the-rf/>

- RF communication chip in iphone 5

Basic relationships

Capacitors

$$i(t) = C \frac{dv(t)}{dt}$$

$$v(t) = v(t_0) + \frac{1}{C} \int_{t_0}^t i(t) dt$$

$$v(t) = \frac{1}{C} \int_{-\infty}^t i(t) dt$$

$$w_C(t) = \frac{1}{2} C v^2(t)$$

Inductors

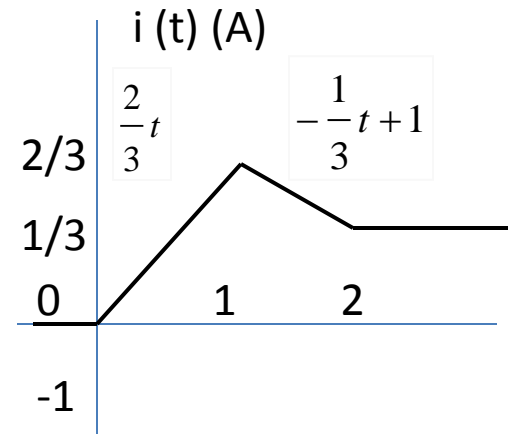
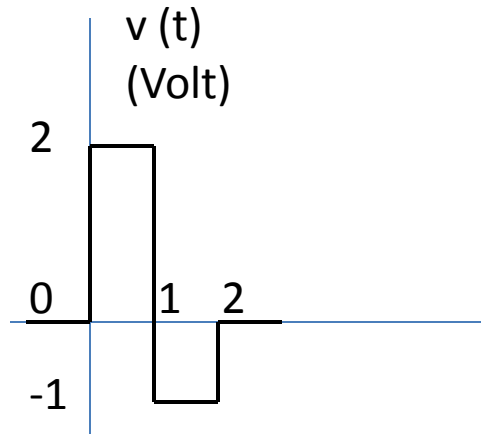
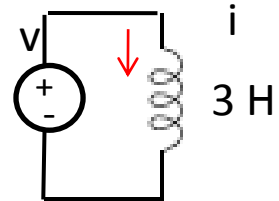
$$v(t) = L \frac{di(t)}{dt}$$

$$i(t) = i(t_0) + \frac{1}{L} \int_{t_0}^t v(t) dt$$

$$i(t) = \frac{1}{L} \int_{-\infty}^t v(t) dt$$

$$w_L(t) = \frac{1}{2} L i^2(t)$$

Simple RL circuit



- What is $i(t)$?

For $t \leq 0$ s, $v(t) = 0$ V

$$i(t) = \frac{1}{L} \int_{-\infty}^t v(t) dt = 0 \text{ A}$$

For $1 < t \leq 2$ s, $v(t) = -1$ V

$$i(t) = i(t_0) + \frac{1}{L} \int_{t_0}^t v(t) dt = i(1) + \frac{1}{L} \int_1^t v(t) dt = \frac{2}{3} (1) + \frac{1}{3} \int_1^t (-1) dt = -\frac{1}{3} t + 1$$

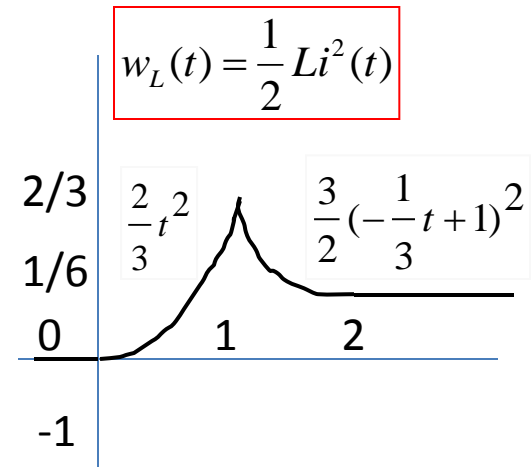
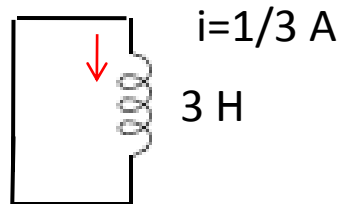
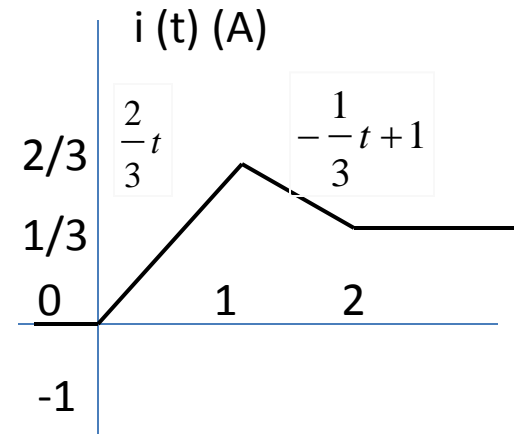
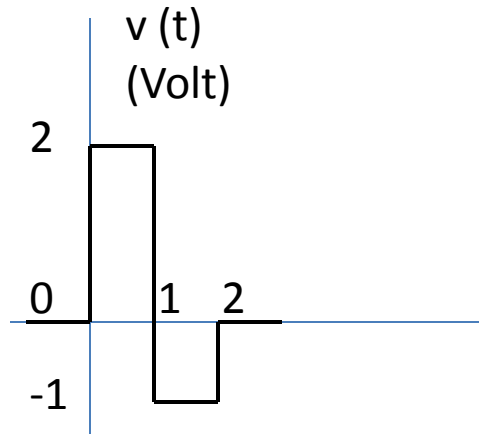
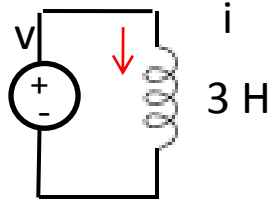
For $0 < t \leq 1$ s, $v(t) = 2$ V

$$i(t) = i(t_0) + \frac{1}{L} \int_{t_0}^t v(t) dt = i(0) + \frac{1}{L} \int_0^t v(t) dt = 0 + \frac{1}{3} \int_0^t 2 dt = \frac{2}{3} t$$

Similarly for $t > 2$ s

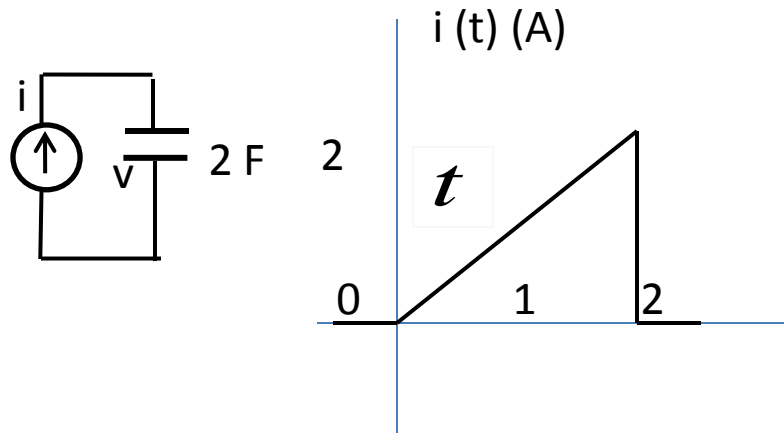
$$i(t) = 1/3 \text{ A}$$

Simple RL circuit



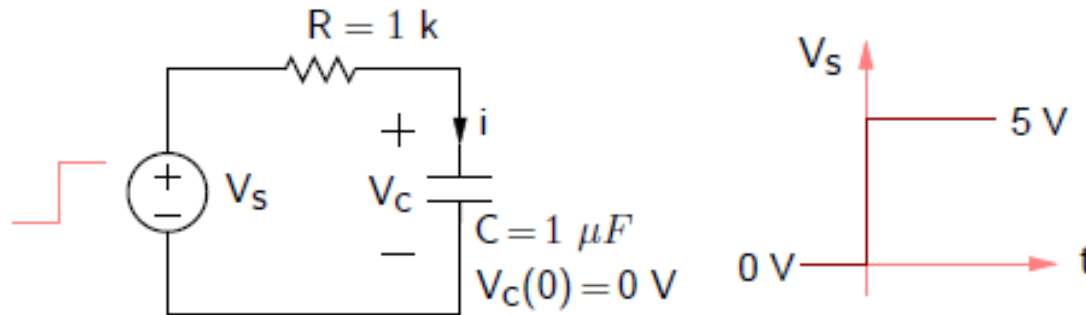
- For $t > 2$ s
- Inductor has 0 volts across it but finite current
- Voltage source and inductor are ideal and energy stays constant for $t > 2$ s

Simple RC circuit- HW



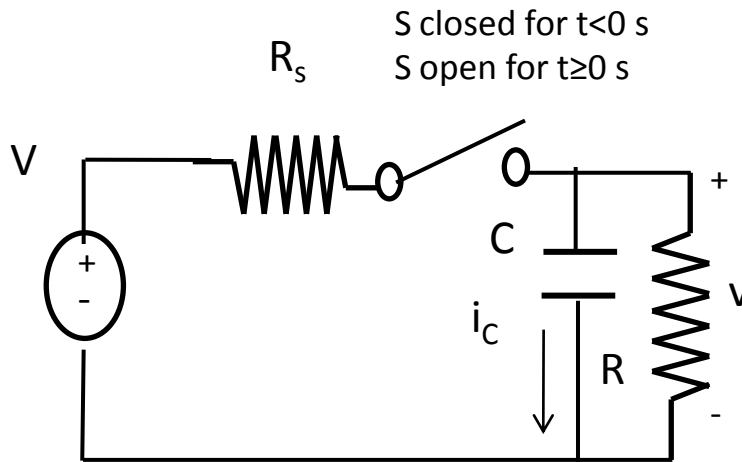
- What is $v(t)$ and $w_C(t)$?
- You will see that even when the current is zero there will be a non-zero voltage across the capacitor

Can capacitor V change suddenly?



- How fast can V_c change?
- Suppose V_c changes by 1 V in $1\text{ }\mu\text{s}$
 - $dV_c/dt = 10^6\text{ V/s}$
 - $i = C dV_c/dt = 1\text{ A}$
 - Voltage drop across $R = 1000\text{ V}$!
 - Violates KVL
 - Hence $V_c(0^+) = V_c(0^-) \rightarrow$ A capacitor does not allow abrupt changes in the ckt if there is a finite resistance in the ckt
 - Similarly an inductor does not allow abrupt changes in i_L

First order RC circuit- natural response



$$v(t) = \frac{RV}{R + R_s} \quad t < 0 \text{ s}$$

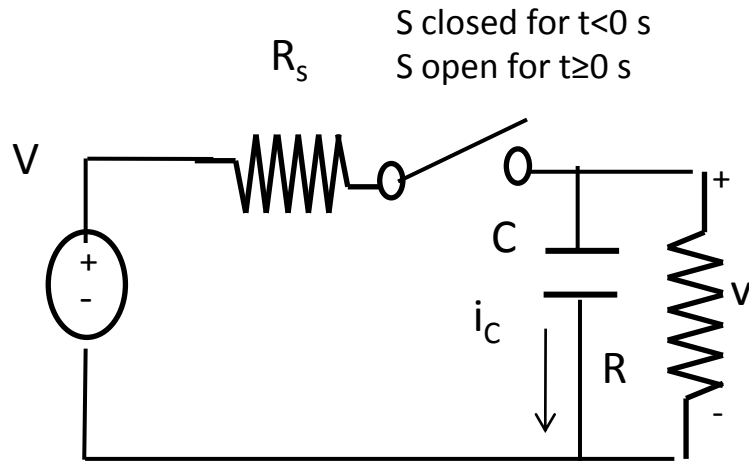
$$v(0) = \frac{RV}{R + R_s} \quad t = 0 \text{ s}$$

$$i_C + i_R = 0$$

$$C \frac{dv}{dt} + \frac{v}{R} = 0 \quad t > 0 \text{ s}$$

- For $t < 0$ s, this is a dc circuit
- Capacitor behaves as open circuit
- At $t = 0$, S opens, voltage cannot change instantaneously
- First order ($v(t)$, $dv(t)/dt$) differential eqn \rightarrow first order circuit
- Homogenous linear differential eqn (every non-zero term is of first degree)
 - Solve for $v(t)$ with the initial condition $v(0)$

First order RC ckt- natural response



$$C \frac{dv}{dt} + \frac{v}{R} = 0 \quad t \geq 0 \quad v(0) = \frac{RV}{R + R_s}$$

$$v(t) = v(0)e^{-\frac{t}{RC}} \quad t \geq 0 \text{ s}$$

$$i_C(t) = -i_R(t) = -\frac{v(0)}{R} e^{-\frac{t}{RC}}$$

$$w_C(0) = \frac{1}{2} C v^2(0)$$

$$w_R = \int_0^{\infty} i_R^2(t) R dt = \frac{1}{2} C v^2(0) = w_C(0)$$

Energy stored in capacitor is dissipated by the resistor

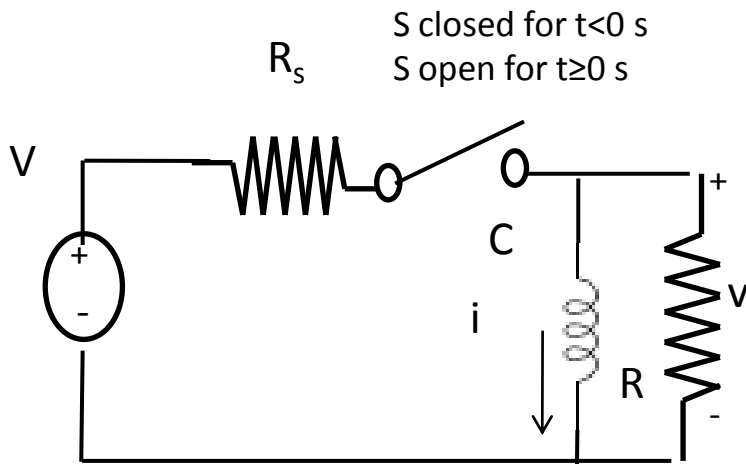
In general,

$$\frac{dx(t)}{dt} + ax = 0$$

$$x(t) = x(0)e^{-at} \quad t \geq 0 \text{ s}$$

Only the initial condition $v(0)$ has an effect on the circuit for $t \geq 0$ s \rightarrow
Natural response

First order RL circuit- natural response



$$L \frac{di}{dt} + Ri = 0 \quad t \geq 0 \text{ s} \quad i(0) = \frac{V}{R_s}$$

$$i(t) = i(0)e^{-\frac{Rt}{L}} \quad t \geq 0 \text{ s}$$

$$v(t) = -Ri(t) = -Ri(0)e^{-\frac{Rt}{L}}$$

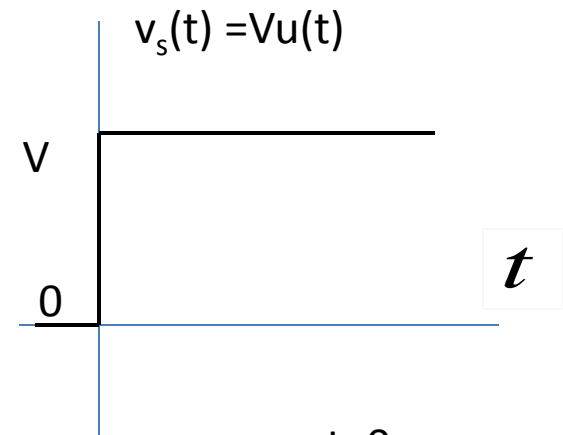
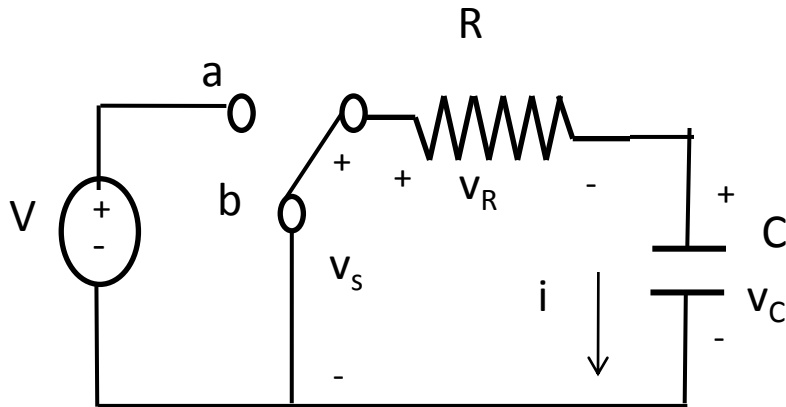
$$w_L(0) = \frac{1}{2} Li^2(0)$$

$$w_R = \int_0^{\infty} i^2(t) R dt = \frac{1}{2} Li^2(0) = w_L(0)$$

- Similar to the first-order RC ckt

First order RC circuit- complete response

S moved from b to a at $t=0$



$$u(t) = 0 \quad t < 0 \text{ s}$$

$$u(t) = 1 \quad t \geq 0 \text{ s}$$

By KCL

$$\frac{dv_C}{dt} + \frac{v_C}{RC} = \frac{Vu(t)}{RC}$$

$$v_C(t) = 0 \text{ for } t < 0$$

$$\frac{dv_C}{dt} + \frac{v_C}{RC} = \frac{V}{RC} \quad t > 0$$

Non-homogenous first order diff eqn.

$$\frac{dx(t)}{dt} + ax(t) = f(t)$$

$f(t) \rightarrow$ forcing function

$$x(t) = e^{-at} \int e^{at} f(t) dt + Ae^{-at} = x_f(t) + x_n(t)$$

Forced response
Steady-state response

Natural response
Transient response

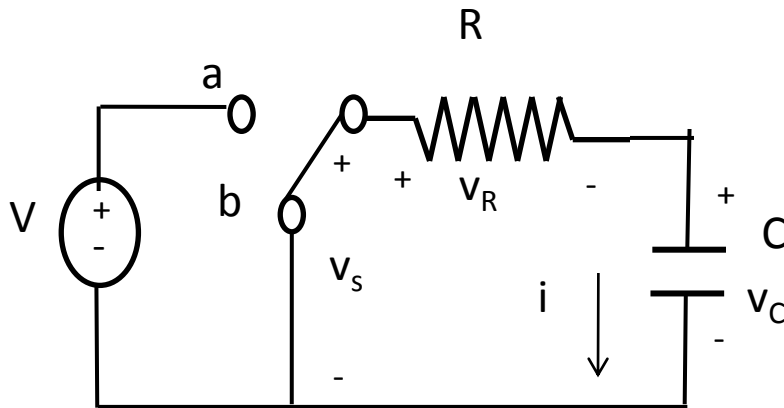
If $f(t)=b$ (constant)

$$x_f(t) = \frac{b}{a}$$

$$x(t) = \frac{b}{a} + Ae^{-at}$$

First order RC circuit- complete response

S moved from b to a at $t=0$

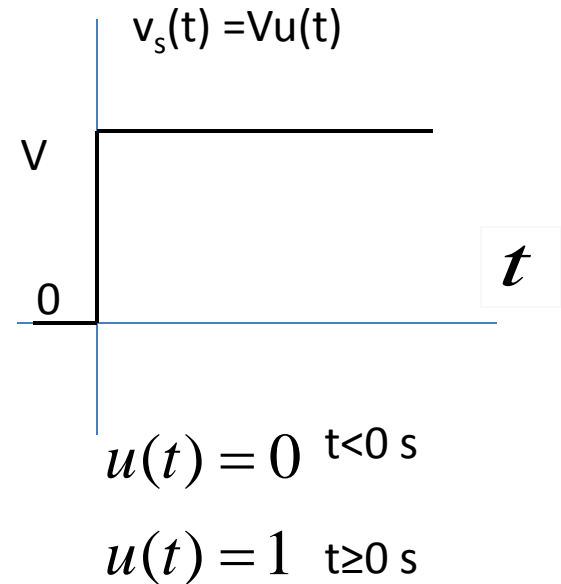


$$\frac{dv_C}{dt} + \frac{v_C}{RC} = \frac{V}{RC} \quad t > 0$$

$$v_C(t) = V + Ae^{-\frac{t}{RC}}$$

$$v_C(0) = 0 \text{ V} \rightarrow A = -V$$

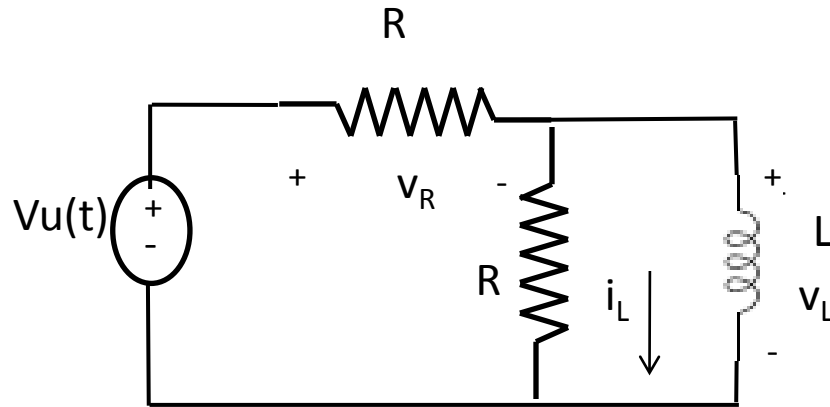
$$v_C(t) = V(1 - e^{-\frac{t}{RC}})$$



$$v_C(t) = V(1 - e^{-\frac{t}{RC}})u(t)$$

$$i_C(t) = \frac{V}{R}e^{-\frac{t}{RC}}u(t)$$

First order RL circuit with forcing function - HW

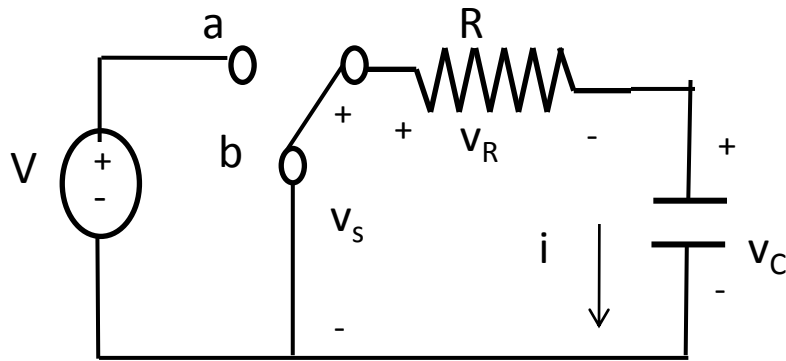


If a parallel R is connected then find out the new $v_L(t)$ and $i_L(t)$.

- Show that

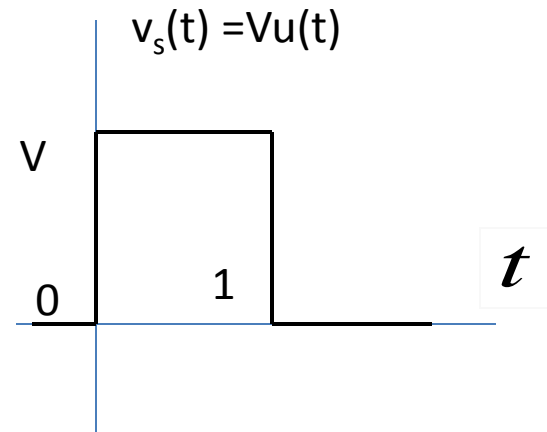
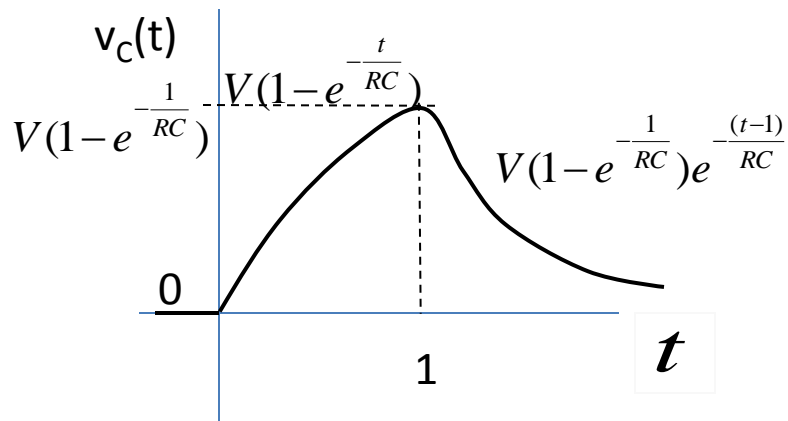
$$v_L(t) = Ve^{-\frac{Rt}{L}}u(t)$$
$$i_L(t) = \frac{V}{R}(1 - e^{-\frac{Rt}{L}})u(t)$$

Linearity and time-invariance



For $0 \leq t < 1$ s, complete response

$$v_C(t) = V(1 - e^{-\frac{t}{RC}})$$



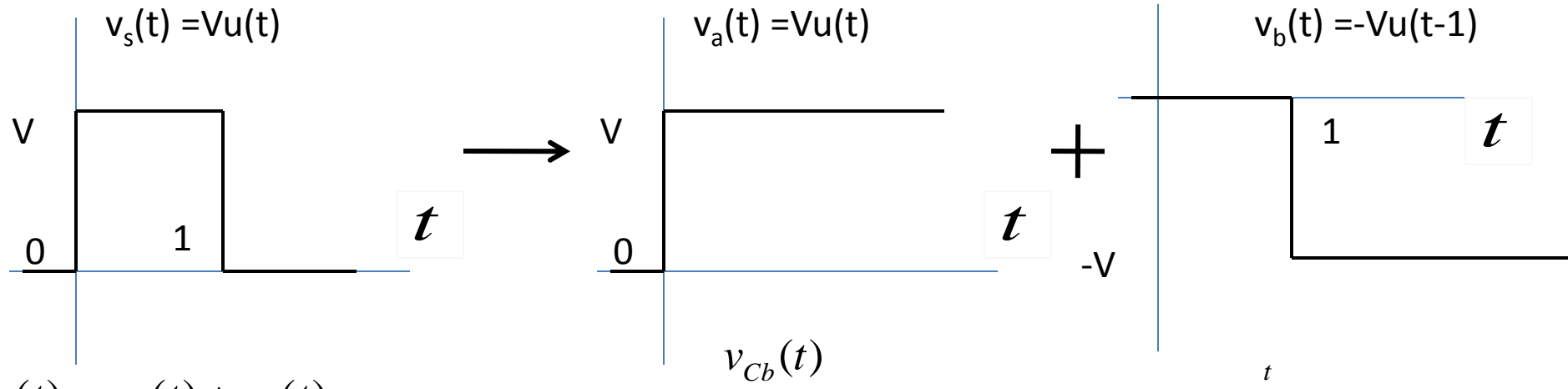
For $t > 1$ s, natural response

$$v_C(1) = V(1 - e^{-\frac{1}{RC}})$$

$$v_C(t) = v_C(1)e^{-\frac{(t-1)}{RC}}$$

$$v_C(t) = V(1 - e^{-\frac{1}{RC}})e^{-\frac{(t-1)}{RC}}$$

Linearity and time-invariance



$$v_s(t) = v_a(t) + v_b(t)$$

$$v_C(t) = v_{Ca}(t) + v_{Cb}(t)$$

$$v_C(t) = V(1 - e^{-\frac{t}{RC}})u(t) + v_{Cb}(t)$$

$v_{Cb}(t)$
 Response to $-Vu(t)$ is $-V(1 - e^{-\frac{t}{RC}})u(t)$

Response to $-Vu(t-1)$ is $-V(1 - e^{-\frac{t-1}{RC}})u(t-1)$

$$v_C(t) = V(1 - e^{-\frac{t}{RC}})u(t) - V(1 - e^{-\frac{t-1}{RC}})u(t-1)$$

- This is due to “time invariance” \rightarrow excitation delayed by time $t \rightarrow$ response delayed by the same time t
- Differential equation has constant coefficients

Solution Check

$$v_C(t) = 0 \quad t < 0 \text{ s}$$

$$v_C(t) = V(1 - e^{-\frac{t}{RC}}) \quad 0 \leq t < 1 \text{ s}$$

$$v_C(t) = V(1 - e^{-\frac{1}{RC}})e^{-\frac{(t-1)}{RC}} \quad t \geq 1 \text{ s}$$

Complete and natural response

$$v_C(t) = V(1 - e^{-\frac{t}{RC}})u(t) - V(1 - e^{-\frac{t-1}{RC}})u(t-1)$$

$$v_C(t) = 0 \quad t < 0 \text{ s}$$

$$v_C(t) = V(1 - e^{-\frac{t}{RC}}) \quad 0 \leq t < 1 \text{ s}$$

Linearity and time-invariance

$$v_C(t) = V(1 - e^{-\frac{t}{RC}}) - V(1 - e^{-\frac{t-1}{RC}}) = Ve^{-\frac{(t-1)}{RC}}(1 - e^{-\frac{1}{RC}}) \quad t \geq 1 \text{ s}$$

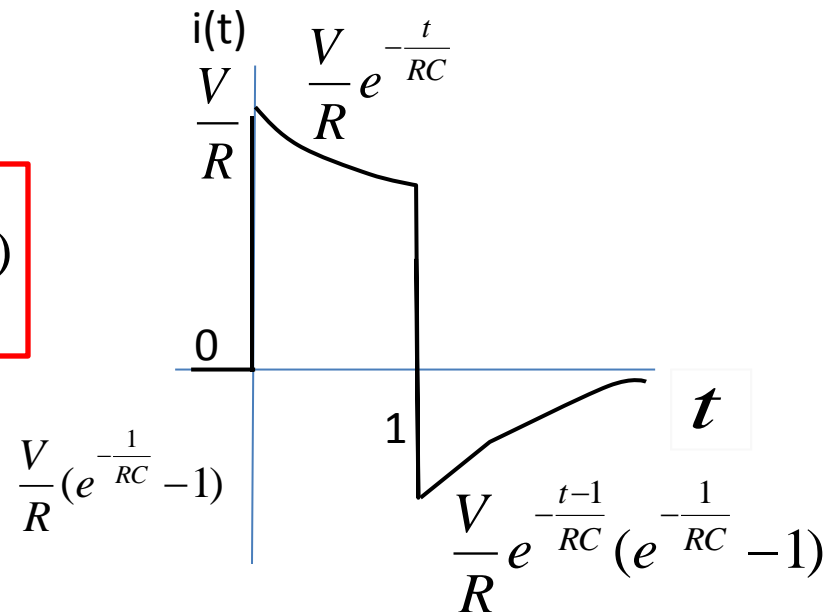
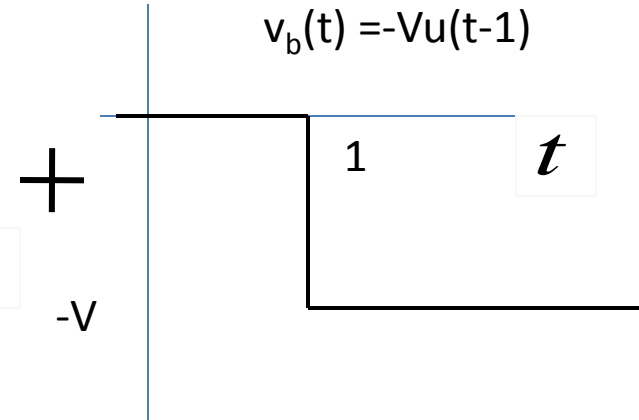
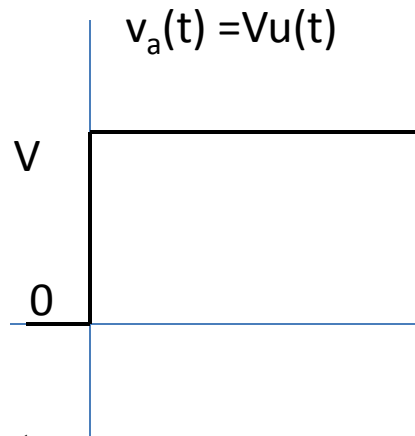
Current

$$v_s(t) = v_a(t) + v_b(t)$$

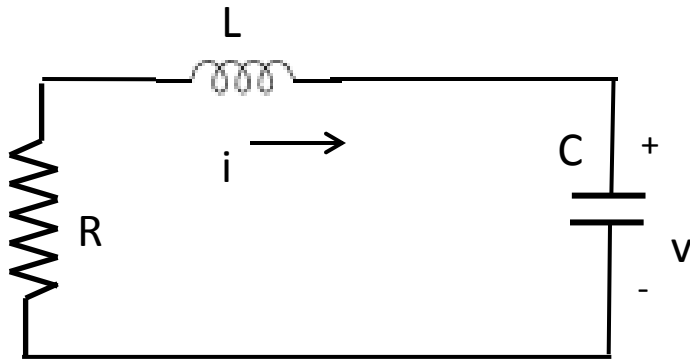
$$i_a(t) = \frac{V}{R} e^{-\frac{t}{RC}} u(t)$$

$$i_b(t) = -\frac{V}{R} e^{-\frac{t-1}{RC}} u(t-1)$$

$$i(t) = i_a(t) + i_b(t) = \frac{V}{R} e^{-\frac{t}{RC}} u(t) - \frac{V}{R} e^{-\frac{t-1}{RC}} u(t-1)$$



Series RLC circuit: Natural response



Three cases are possible:

1. $\alpha > \omega_n$ s_1 and s_2 are real \rightarrow
overdamped case
2. $\alpha < \omega_n$ s_1 and s_2 are complex \rightarrow
 $s_1 = -\alpha - \sqrt{-(\omega_n^2 - \alpha^2)} = -\alpha - j\omega_d$
 $s_2 = -\alpha + \sqrt{-(\omega_n^2 - \alpha^2)} = -\alpha + j\omega_d$
underdamped case
3. $\alpha = \omega_n$ $s_1 = s_2 = \alpha \rightarrow$ **critically damped case**

$$v + Ri + L \frac{di}{dt} = 0$$

$$v + RC \frac{dv}{dt} + LC \frac{d^2v}{dt^2} = 0$$

$$\frac{d^2v}{dt^2} + \frac{R}{L} \frac{dv}{dt} + \frac{1}{LC} v = 0$$

$$\frac{d^2v}{dt^2} + 2\alpha \frac{dv}{dt} + \omega_n^2 v = 0$$

Assume

$$v(t) = Ae^{st}$$

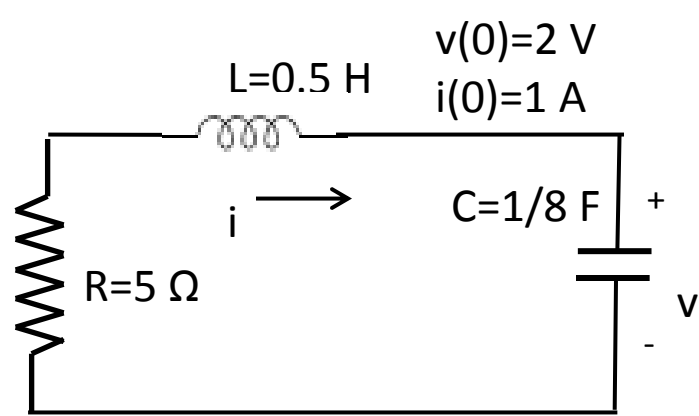
$$s^2 + 2\alpha s + \omega_n^2 = 0$$

$$s_1 = -\alpha - \sqrt{\alpha^2 - \omega_n^2}$$

$$s_2 = -\alpha + \sqrt{\alpha^2 - \omega_n^2}$$

$$v(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

A_1 and A_2 are obtained from initial conditions



Case 1: Overdamped case

$$\alpha = \frac{R}{2L} = 5 > \omega_n = \frac{1}{\sqrt{LC}} = 4$$

$$s_1 = -\alpha - \sqrt{\alpha^2 - \omega_n^2} = -8$$

$$s_2 = -\alpha + \sqrt{\alpha^2 - \omega_n^2} = -2$$

$$v(t) = A_1 e^{-8t} + A_2 e^{-2t}$$

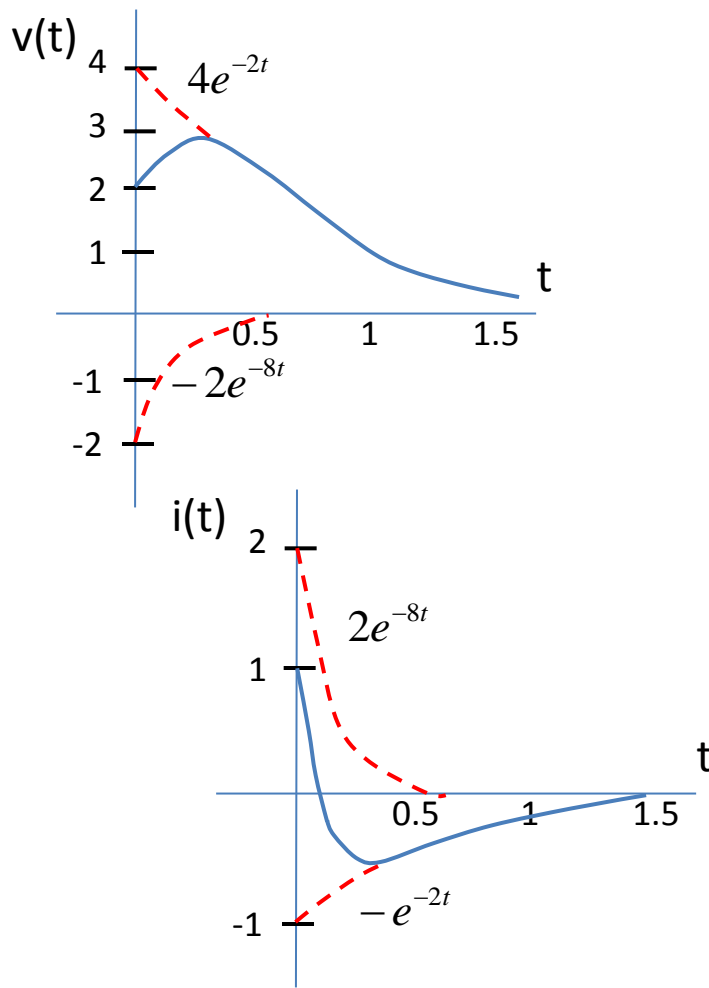
$$i(t) = C \frac{dv}{dt} = -A_1 e^{-8t} - \frac{A_2}{4} e^{-2t}$$

$$i(0) = 1 \text{ A}$$

$$v(0) = 2 \text{ V}$$

$$v(t) = -2e^{-8t} + 4e^{-2t}$$

$$i(t) = 2e^{-8t} - e^{-2t}$$



Case 2: Underdamped case

$$\omega_d = \sqrt{\omega_n^2 - \alpha^2} = 7$$

$$\alpha = \frac{R}{2L} = 1 < \omega_n = \frac{1}{\sqrt{LC}} = \sqrt{50}$$

$$s_1 = -\alpha - \sqrt{\alpha^2 - \omega_n^2} = -1 - j7$$

$$s_2 = -\alpha + \sqrt{\alpha^2 - \omega_n^2} = -1 + j7$$

$$v(t) = e^{-t} (A_1 e^{-j7t} + A_2 e^{j7t}) = e^{-t} (B_1 \cos 7t + B_2 \sin 7t)$$

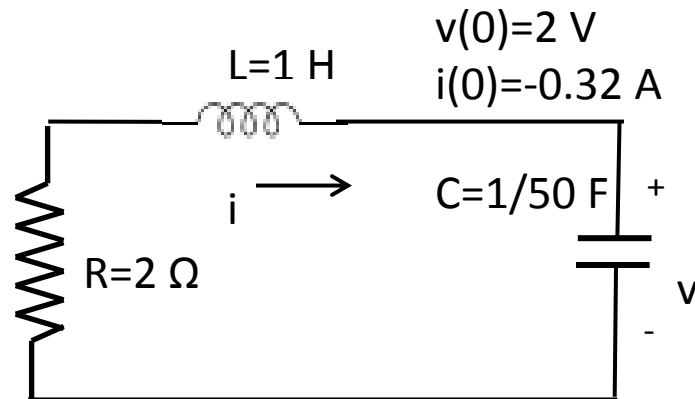
$$i(t) = C \frac{dV}{dt}$$

$$i(0) = -0.32 \text{ A}$$

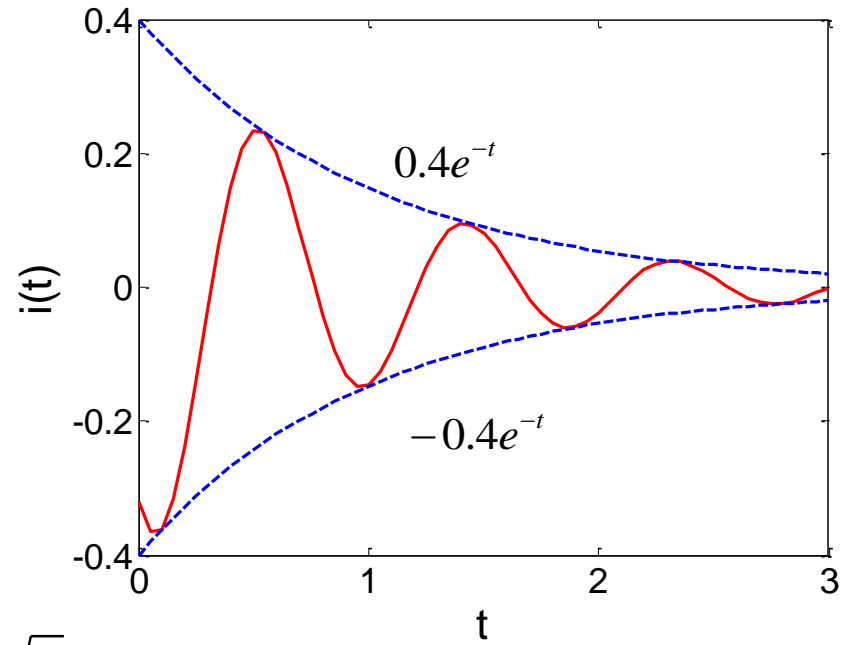
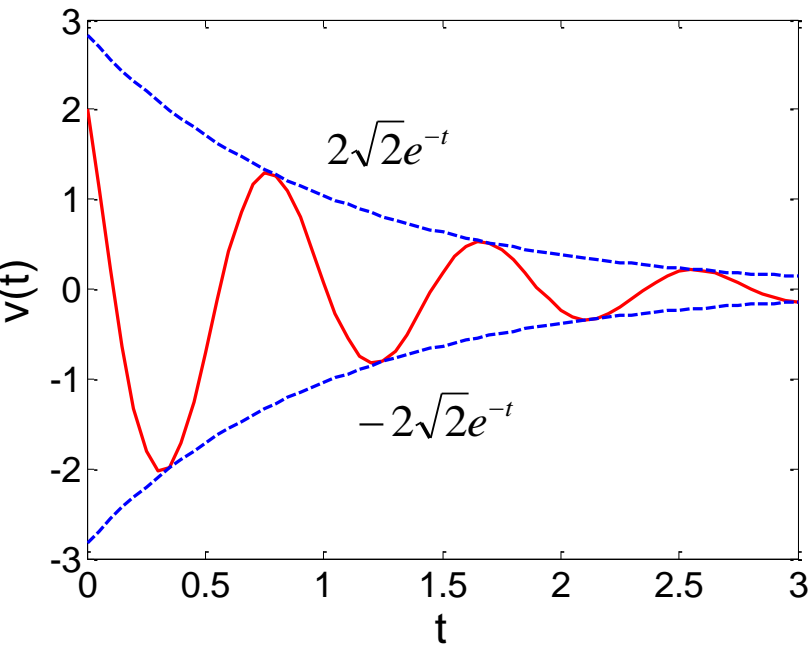
$$v(0) = 2 \text{ V}$$

$$v(t) = 2e^{-t} (\cos 7t - \sin 7t)$$

$$i(t) = e^{-t} (-0.32 \cos 7t - 0.24 \sin 7t)$$



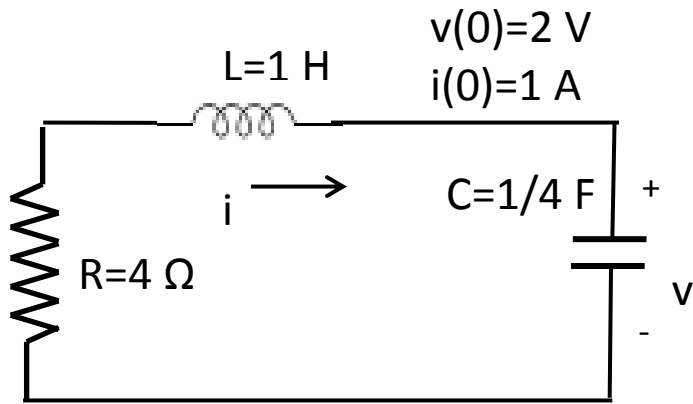
Underdamped case



$$v(t) = 2e^{-t}(\cos 7t - \sin 7t) = 2\sqrt{2}e^{-t} \cos(7t + \pi/4)$$

$$i(t) = e^{-t}(-0.32 \cos 7t - 0.24 \sin 7t) = 0.4e^{-t} \cos(7t + 2.5)$$

- Product of a real exponent and a sinusoid \rightarrow damped sinusoid
- Energy transferred back and forth between L and C and dissipated in R
- α is the damping factor, smaller the α more the oscillations \rightarrow more underdamped
- What if $\alpha=0$? \rightarrow perfect sinusoid \rightarrow oscillator
- ω_d is the damped natural frequency or damped frequency
- ω_n is the undamped natural frequency or undamped frequency



$$\alpha = \frac{R}{2L} = 2 = \omega_n = \frac{1}{\sqrt{LC}} = 2$$

$$v(t) = A_1 t e^{-2t} + A_2 e^{-2t}$$

$$i(t) = C \frac{dv}{dt}$$

$$i(0) = 1\text{ A}$$

$$v(0) = 2\text{ V}$$

$$v(t) = (8t + 2)e^{-2t}$$

$$i(t) = (-4t + 1)e^{-2t}$$

Case 3. Critically Damped Case

$$v + RC \frac{dv}{dt} + LC \frac{d^2v}{dt^2} = 0$$

$$\frac{d^2v}{dt^2} + \frac{R}{L} \frac{dv}{dt} + \frac{1}{LC} v = 0$$

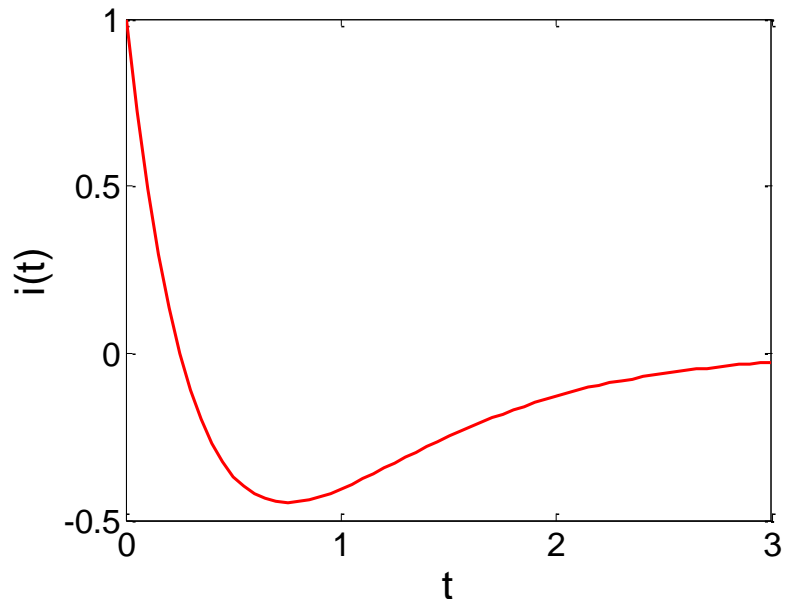
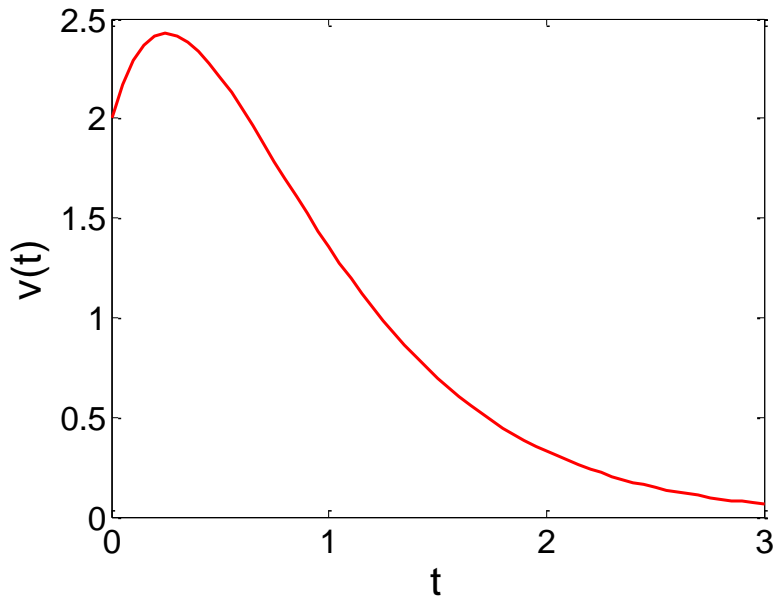
$$\frac{d^2v}{dt^2} + 2\alpha \frac{dv}{dt} + \omega_n^2 v = 0$$

$$\alpha = \omega_n$$

$$\frac{d^2v}{dt^2} + 2\alpha \frac{dv}{dt} + \alpha^2 v = 0$$

$$v(t) = (A_1 t + A_2) e^{-\alpha t}$$

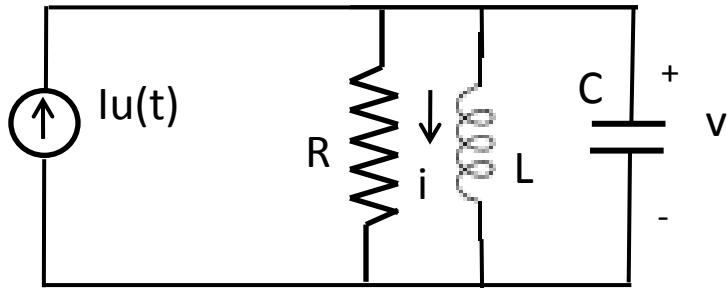
Case 3. Critically Damped Case



$$v(t) = (8t + 2)e^{-2t}$$

$$i(t) = (-4t + 1)e^{-2t}$$

RLC Circuits: Complete response



$$Iu(t) = \frac{v}{R} + i + C \frac{dv}{dt}$$

$$\frac{d^2 i}{dt^2} + \frac{1}{RC} \frac{di}{dt} + \frac{1}{LC} i = \frac{I}{LC} u(t)$$

$$\frac{d^2 i}{dt^2} + \frac{1}{RC} \frac{di}{dt} + \frac{1}{LC} i = \frac{I}{LC} \quad t > 0_s$$

$$i(t) = i_f(t) + i_n(t)$$

Forced response
Steady-state response

Natural response
Transient response

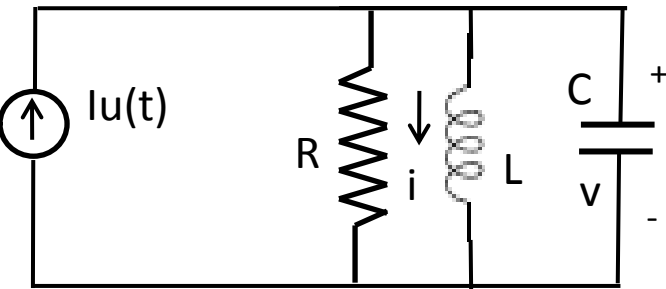
$$i_f(t) = K$$

$$K / LC = I / LC \Rightarrow K = I$$

$$\frac{d^2 i_n}{dt^2} + 2\alpha \frac{di_n}{dt} + \omega_n^2 i_n = 0$$

$$\alpha = \frac{1}{2RC}, \omega_n = \frac{1}{\sqrt{LC}}$$

RLC Circuits: Complete response



$$i(t) = i_f(t) + i_n(t)$$

$$i(t) = I + A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

Overdamped

$$i(t) = I + e^{-\alpha t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

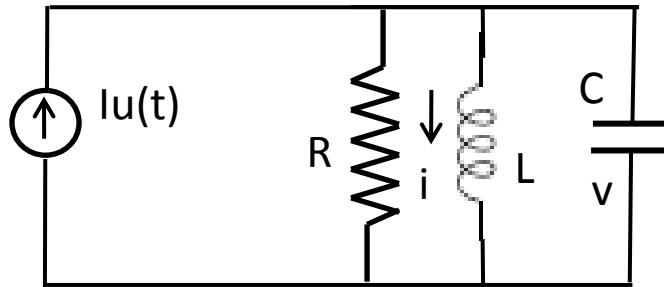
Underdamped

$$i(t) = I + A_1 t e^{-\alpha t} + A_2 e^{-\alpha t}$$

Critically damped

- A_1 and A_2 are determined from initial conditions
- When the current is switched on, $i(0)=0$ and $v(0)=0$ since these cannot change instantaneously
- After a long time, similar to dc \rightarrow inductor carries I amps, voltage across $C=0$ V.
- Shapes of i and v waveforms between initial and final values depends on the case

Case 1. Overdamped case



$$R=6\ \Omega, L=7\ \text{H}, C=1/42\ \text{F}, Iu(t)=6u(t)$$

For $t > 0$ s

$$\frac{d^2 i}{dt^2} + \frac{1}{RC} \frac{di}{dt} + \frac{1}{LC} i = \frac{I}{LC}$$

$$\frac{d^2 i}{dt^2} + 7 \frac{di}{dt} + 6i = 36$$

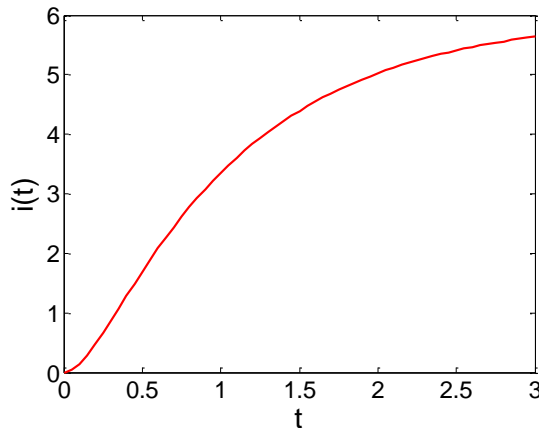
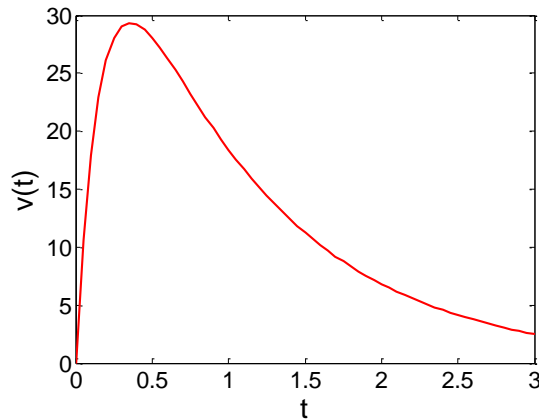
$$\alpha = 7/2 > \omega_n = \sqrt{6} \quad \text{Overdamped}$$

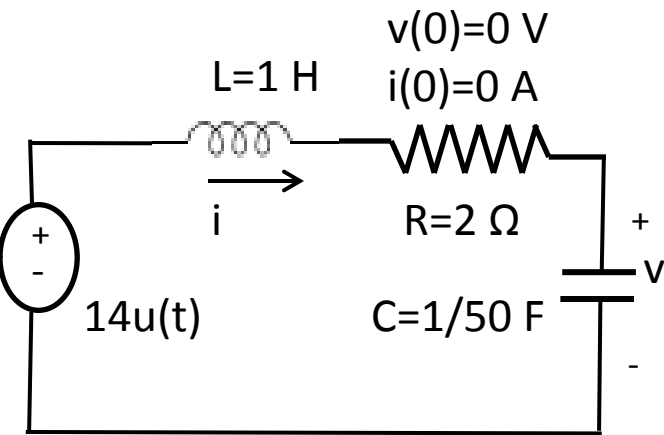
$$i(t) = 6 + A_1 e^{-6t} + A_2 e^{-t}$$

$$i(0) = v(0) = 0$$

$$i(t) = (6 + 1.2e^{-6t} - 7.2e^{-t})u(t)$$

$$v(t) = (-50.4e^{-6t} + 50.4e^{-t})u(t)$$





Case 2. Underdamped Case

$$\frac{d^2v}{dt^2} + \frac{R}{L} \frac{dv}{dt} + \frac{1}{LC} v = \frac{V}{LC}$$

$$\frac{d^2v}{dt^2} + 2 \frac{dv}{dt} + 50v = 50 \times 14$$

$$\alpha = 1 < \omega_n = \sqrt{50}$$

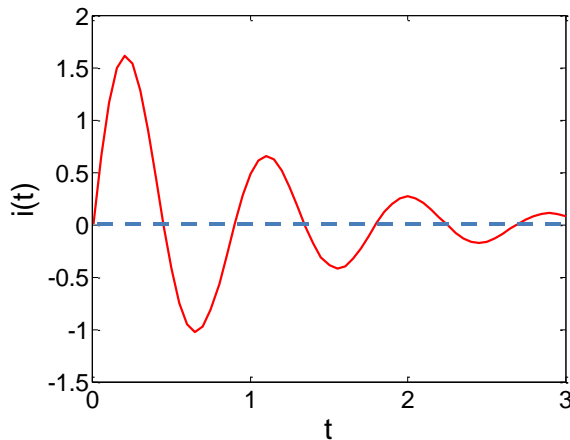
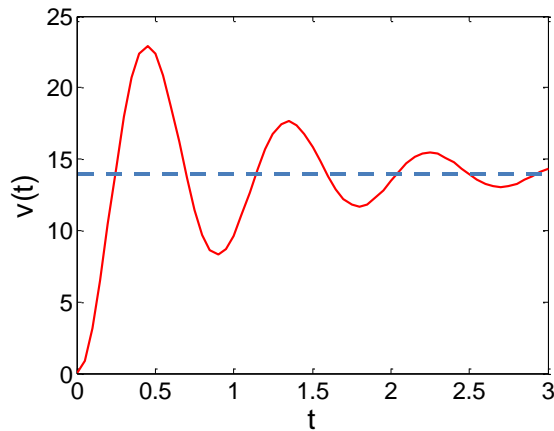
$$\omega_d = \sqrt{50 - 1} = 7$$

$$v(t) = 14 + e^{-t} (A_1 \cos 7t + A_2 \sin 7t)$$

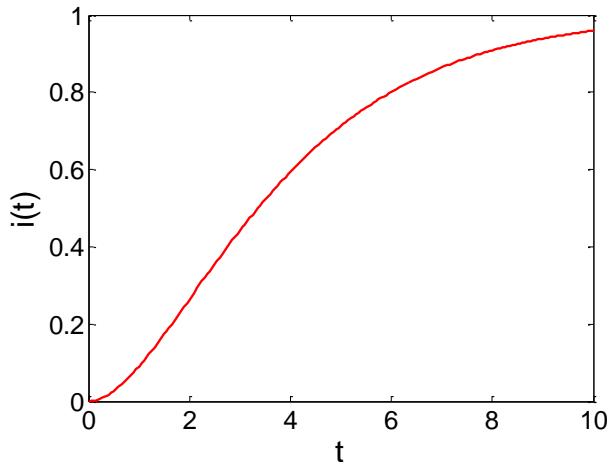
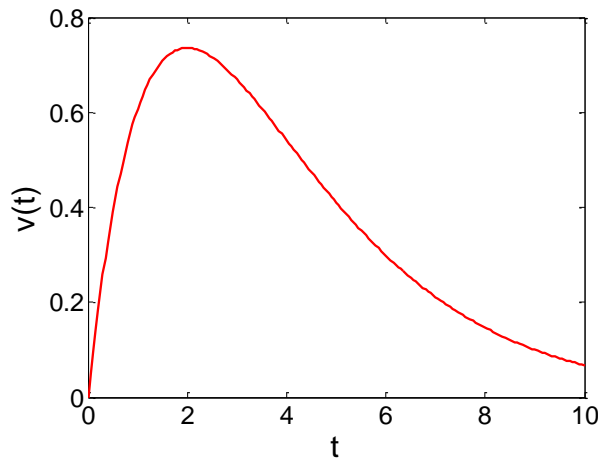
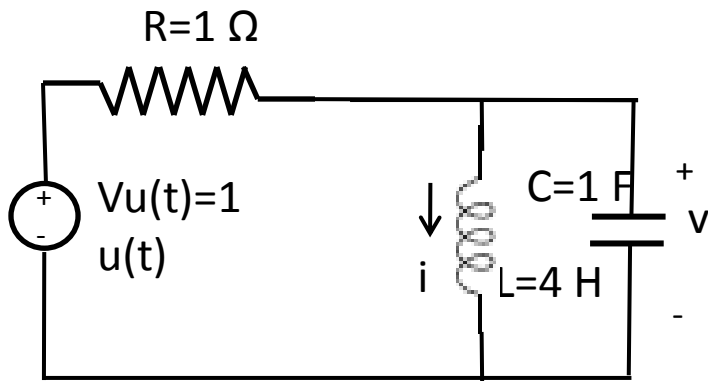
$$i(0) = v(0) = 0$$

$$v(t) = 14 + e^{-t} (-14 \cos 7t - 2 \sin 7t) = 14 - 10\sqrt{2}e^{-t} \cos(7t - 0.142)$$

$$i(t) = C dv(t) / dt = 2e^{-t} \sin 7t$$



Case 3. Critically Damped



$$\frac{d^2 i}{dt^2} + \frac{1}{RC} \frac{di}{dt} + \frac{1}{LC} i = \frac{V}{RLC}$$

$$\alpha = 1/2 = \omega_n = 1/2$$

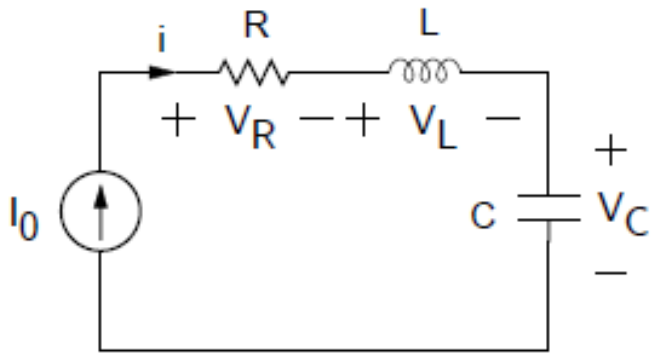
$$i(t) = 1 + A_1 t e^{-t/2} + A_2 e^{-t/2}$$

$$i(0) = v(0) = 0$$

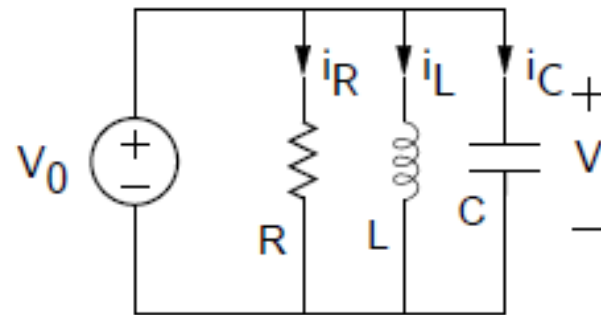
$$i(t) = \left(1 - \frac{1}{2} t e^{-t/2} - e^{-t/2}\right) u(t)$$

$$v(t) = L di(t) / dt = t e^{-t/2} u(t)$$

Trivial circuits



$$V_R = i R, \quad V_L = L \frac{di}{dt}, \quad V_C = \frac{1}{C} \int i dt.$$



$$i_R = V/R, \quad i_C = C \frac{dV}{dt}, \quad i_L = \frac{1}{L} \int V dt.$$