

# BJT Amplifiers (Analog Circuits)

EE 101

S. Lodha

Reference material: L. Bobrow's Book

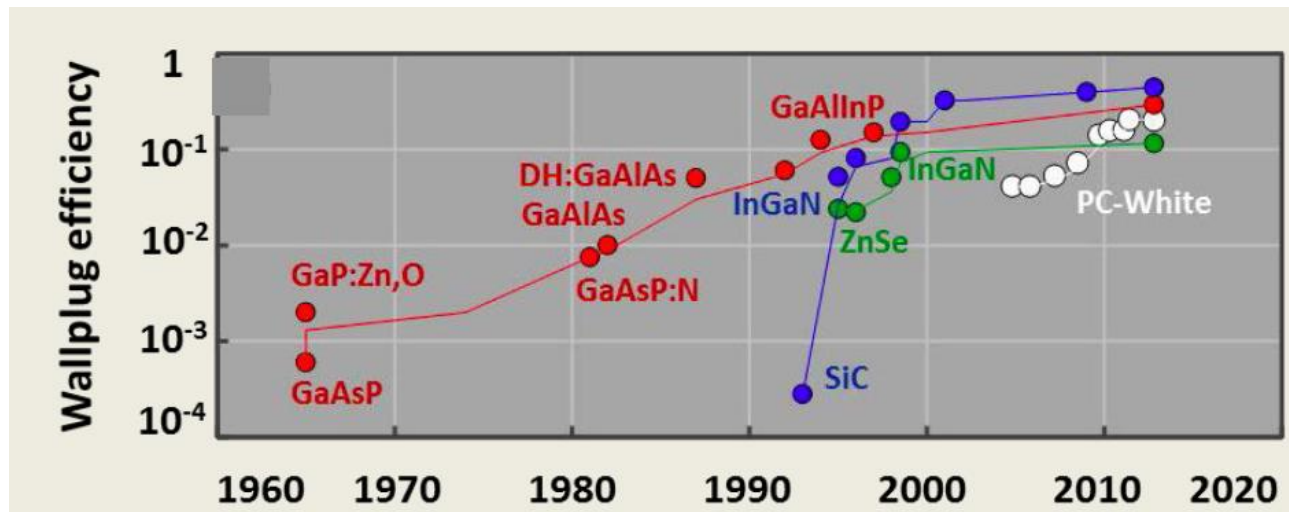
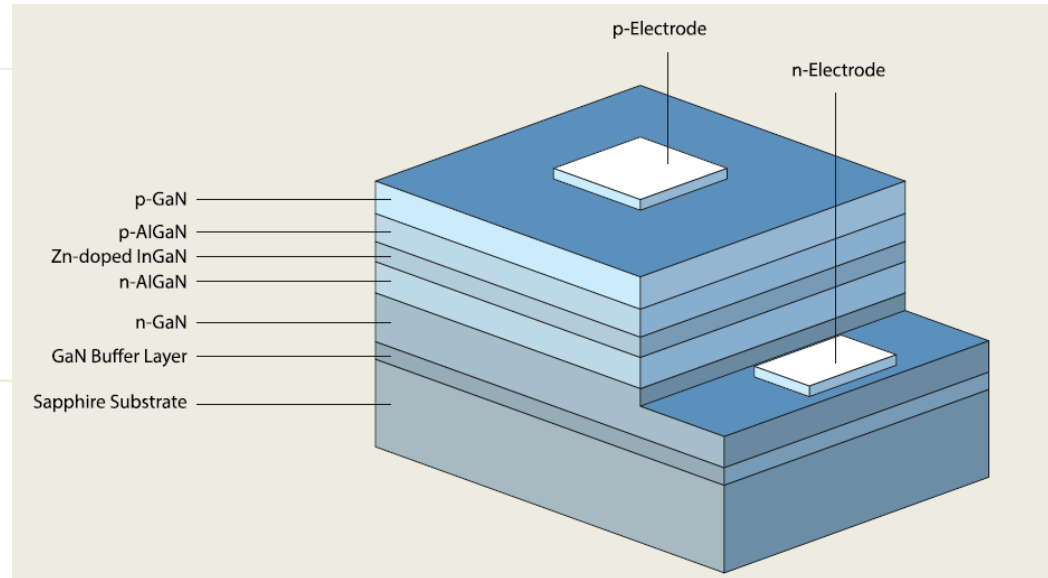
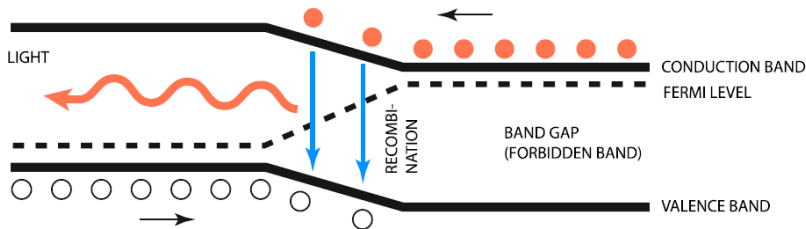
# Nobel Prize in Physics 2014



Isamu Akasaki, Hiroshi Amano and Shuji Nakamura

**EFFICIENT BLUE LIGHT-EMITTING DIODES LEADING  
TO BRIGHT AND ENERGY-SAVING WHITE LIGHT SOURCES**

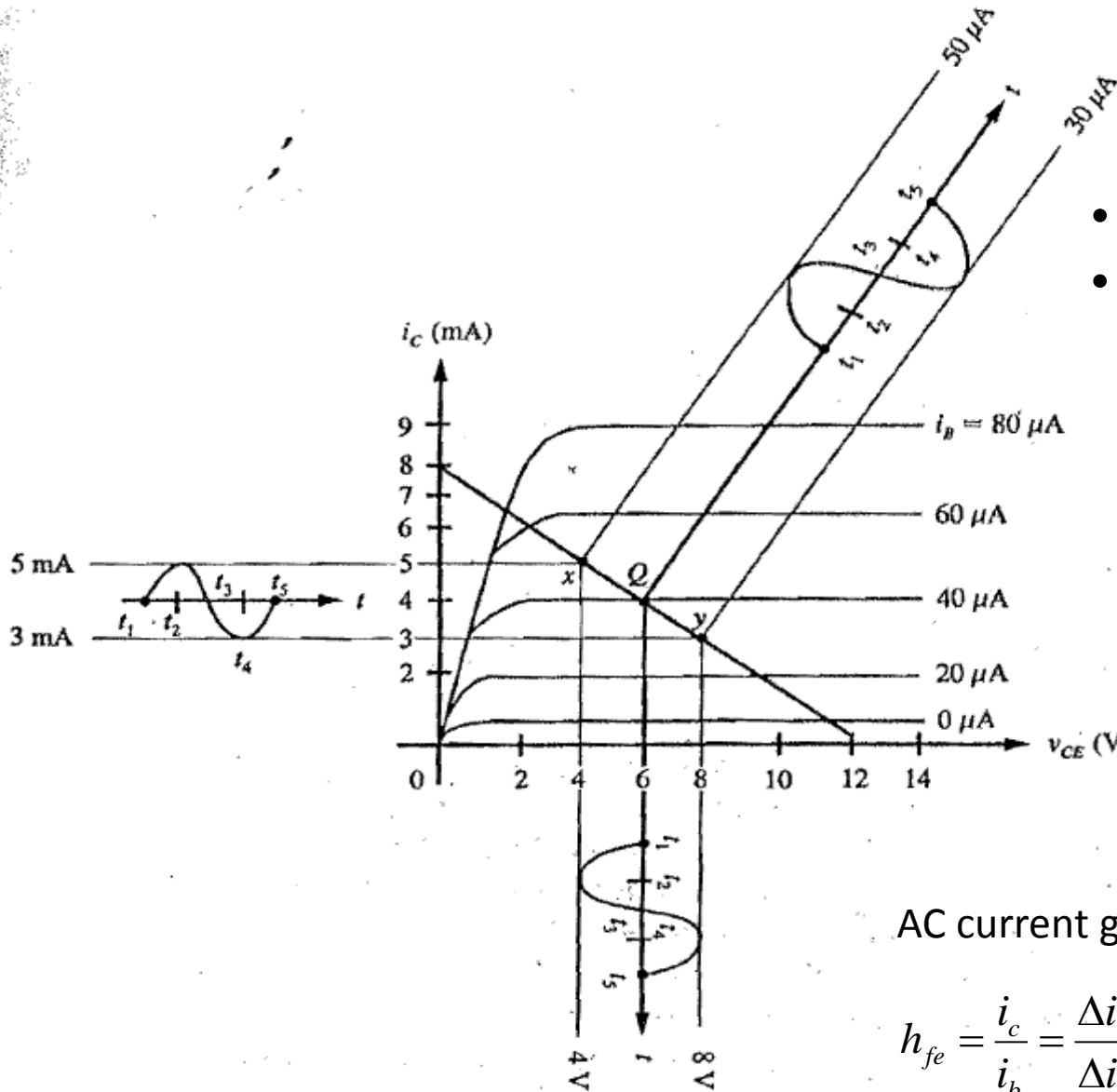
# Blue LED



# Impact

- Transformed entire lighting industry
  - 20-30% of electricity is used for lighting
  - Standard bulb → 16 lm/W (4% efficiency)
  - LED → 300 lm/W (50% efficiency)
    - 100,000 hour lifetime
- Other applications
  - Displays in electronics
  - Sensors etc.

# BJT Amplifier: Collector Characteristics



- Active region operation
- $Q \rightarrow$  quiescent operating point

$$i_C = I_{CQ} + i_c = 4 + \sin \omega t \text{ mA}$$

$$i_B = I_{BQ} + i_b = 40 + 10 \sin \omega t \text{ } \mu A$$

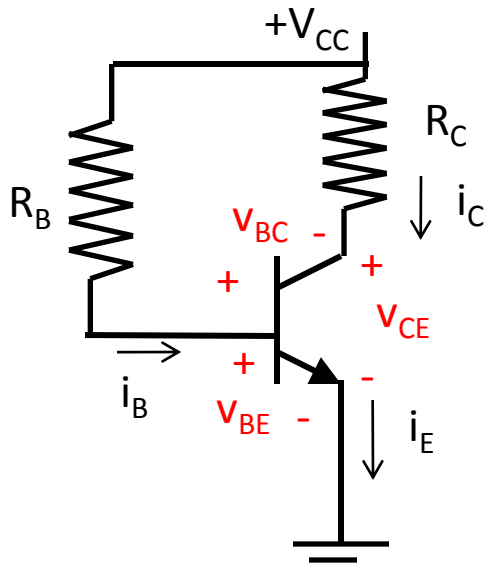
$$v_{CE} = V_{CE} + v_{ce} = 6 - 2 \sin \omega t \text{ V}$$

AC current gain  $h_{fe} = \beta_{ac}$

$$h_{fe} = \frac{i_c}{i_b} = \frac{\Delta i_C}{\Delta i_B} = \frac{i_{Cx} - i_{Cy}}{i_{Bx} - i_{By}} = \frac{(5 - 3) \times 10^{-3}}{(50 - 30) \times 10^{-6}} = 100$$

# DC biasing of BJT: Fixed Bias

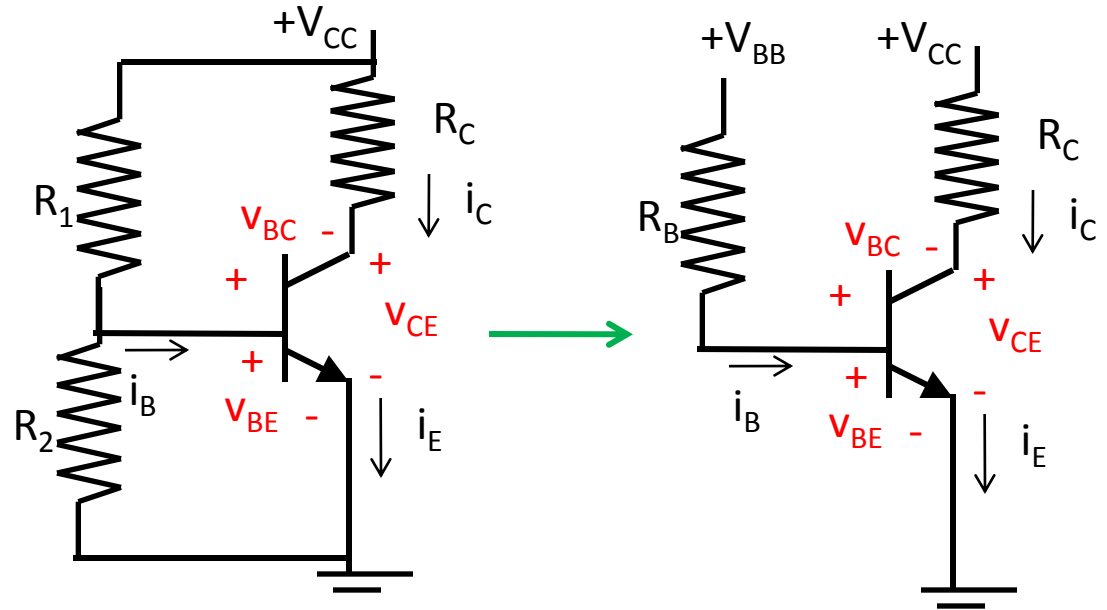
Example 1



$$i_B = \frac{V_{CC} - v_{BE}}{R_B} \quad i_C = h_{FE} i_B$$

$$v_{CE} = -R_C h_{FE} i_B + V_{CC}$$

Example 2 (Voltage divider bias)



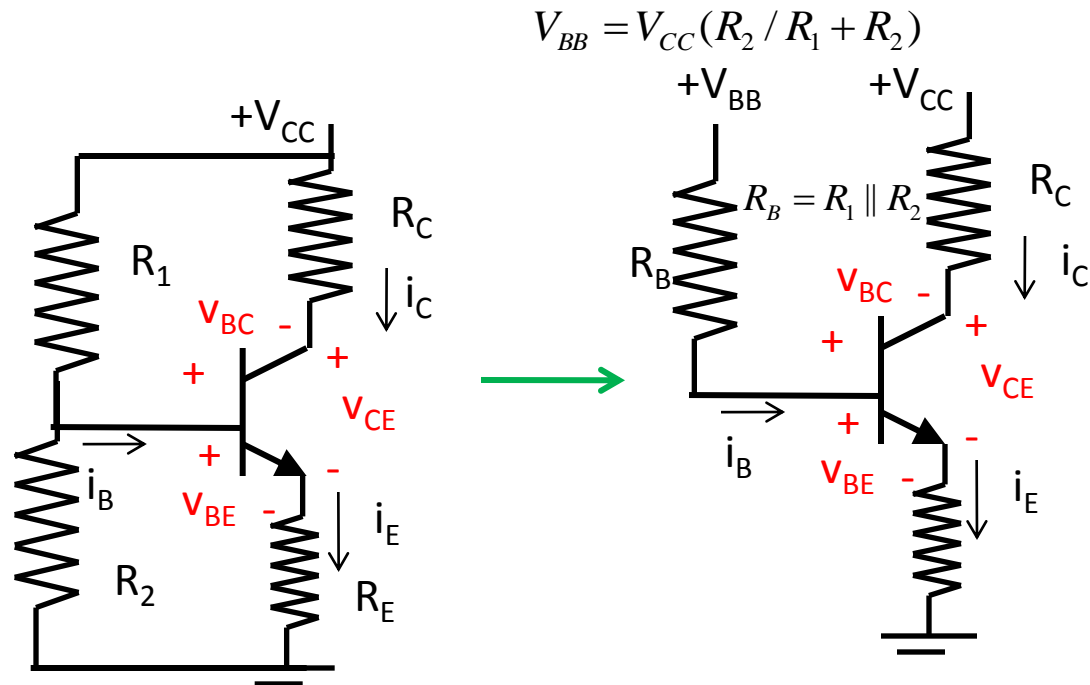
Thevenin  
Equivalent

$$R_B = R_1 \parallel R_2$$

$$V_{BB} = V_{CC} (R_2 / R_1 + R_2)$$

- In fixed bias, variations (temperature, transistor-to-transistor) in  $h_{FE}$  can affect Q point
  - $h_{FE}$  increases,  $i_C$  increases

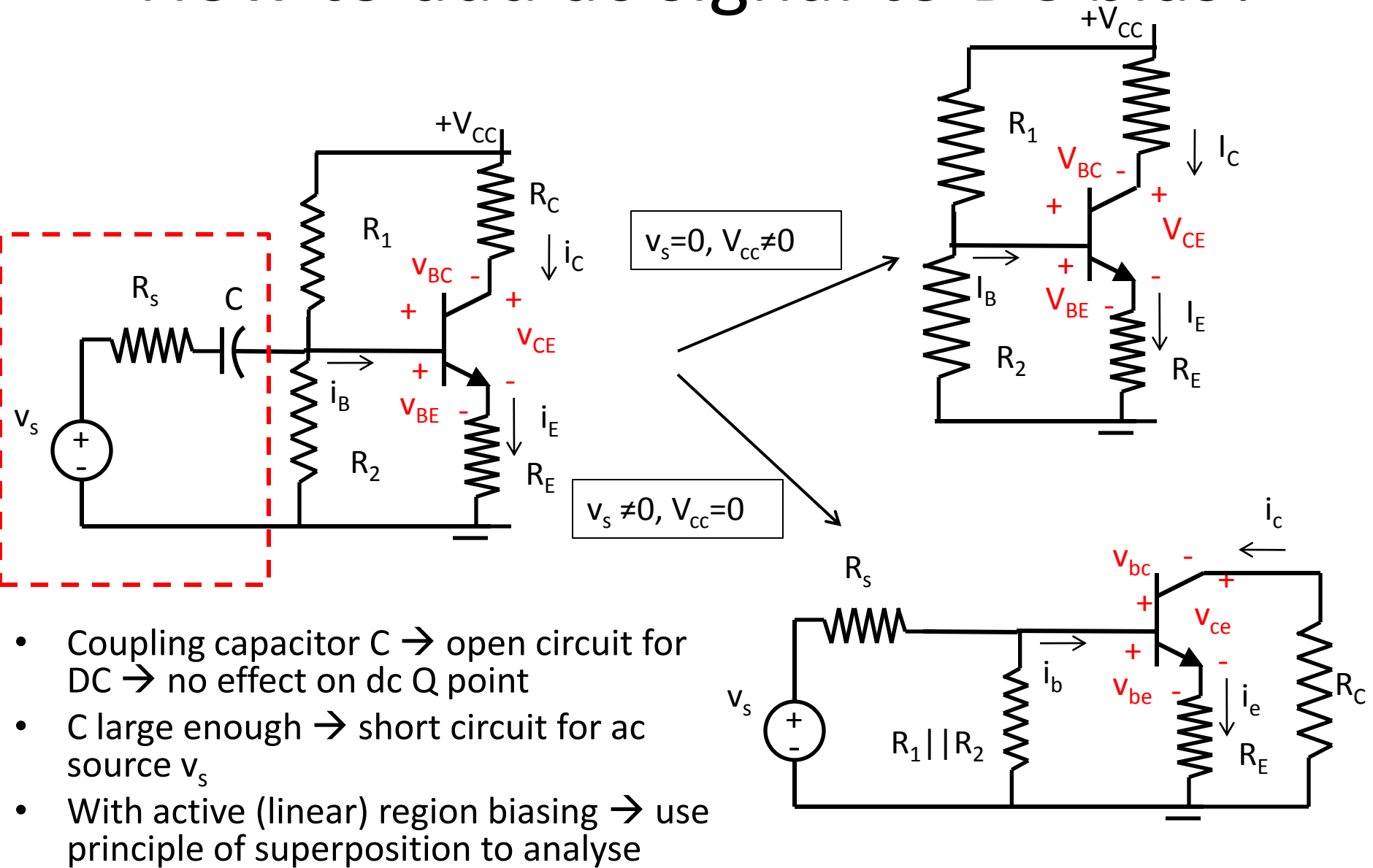
# DC biasing of BJT: Self-Bias



$$V_{BB} = R_B i_B + v_{BE} + R_E (i_B + i_C) \Rightarrow i_B = \frac{V_{BB} - v_{BE}}{R_B + (1 + h_{FE}) R_E}$$

- If  $h_{FE}$  increases  $\rightarrow i_C$  tends to increase but  $i_B$  decreases and tends to decrease  $i_C$
- **More stable** Q point, also called self-biasing circuit

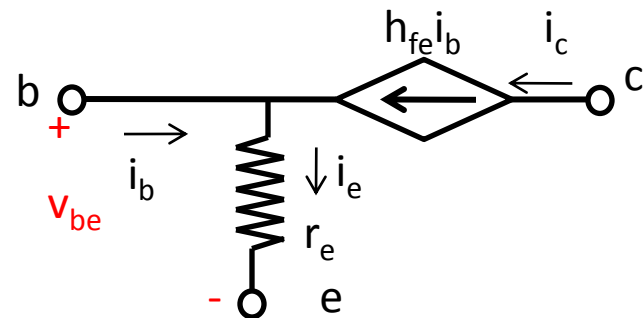
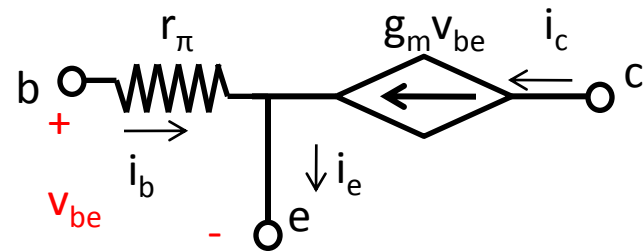
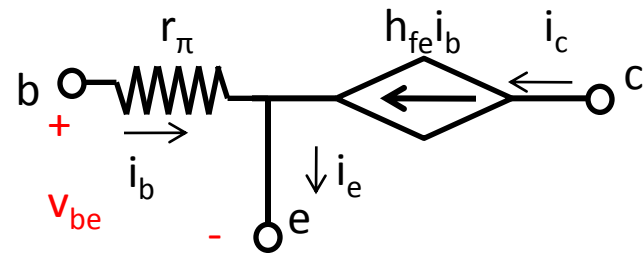
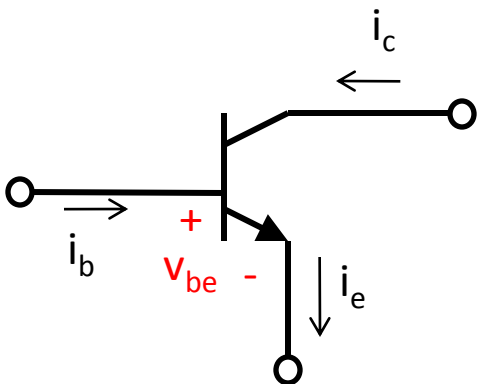
# How to add ac signal to DC bias?



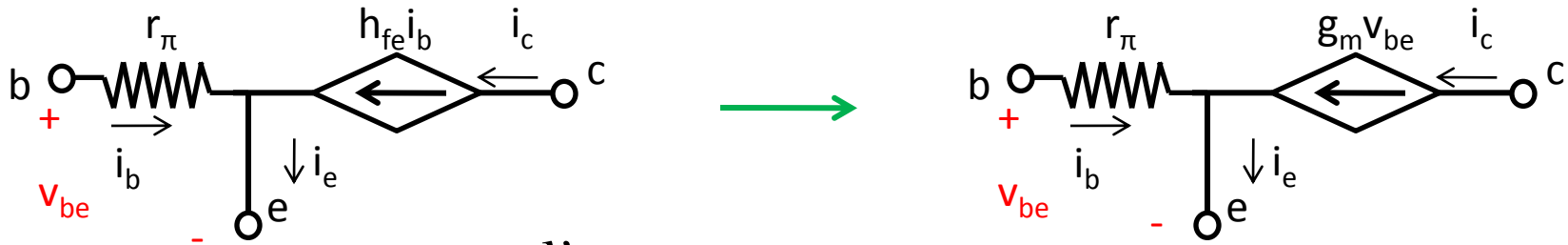


# Small signal ac models

- Ac signal is small such that
  - transistor operates in active mode
  - Non-linear effects/distortions can be ignored
    - o/p characteristics are linear and parallel



# Small signal model

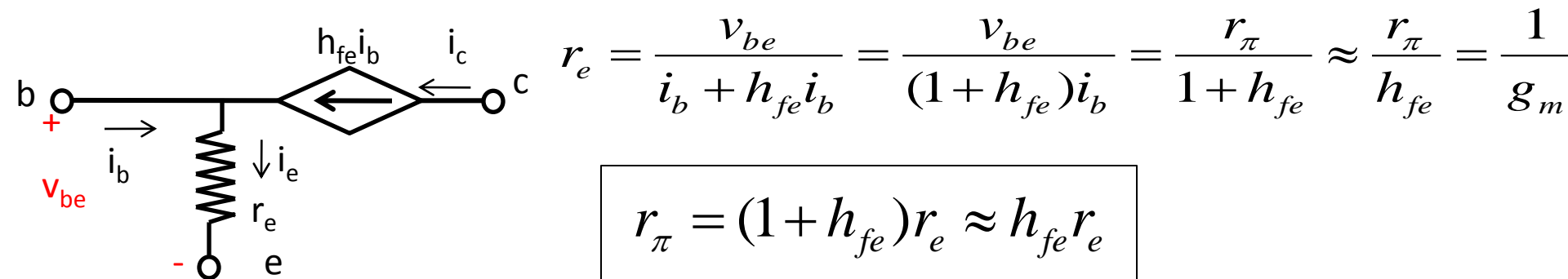


$$i_b = \frac{v_{be}}{r_\pi}$$

Ac base resistance =  $r_\pi$

$$h_{fe}i_b = h_{fe} \frac{v_{be}}{r_\pi} = g_m v_{be}$$

$$\text{Transconductance } g_m = h_{fe}/r_\pi$$



$$r_e = \frac{v_{be}}{i_b + h_{fe}i_b} = \frac{v_{be}}{(1 + h_{fe})i_b} = \frac{r_\pi}{1 + h_{fe}} \approx \frac{r_\pi}{h_{fe}} = \frac{1}{g_m}$$

$$r_\pi = (1 + h_{fe})r_e \approx h_{fe}r_e$$

# $g_m, r_\pi, r_e$

For npn transistor in active mode

$$i_C = I_S (e^{v_{BE}/V_T} - 1) \approx I_S e^{v_{BE}/V_T}$$

$$di_C = d[I_S (e^{v_{BE}/V_T} - 1)] = \frac{1}{V_T} (I_S e^{v_{BE}/V_T}) dv_{BE} \approx \frac{i_C}{V_T} dv_{BE}$$

$$g_m = \frac{i_c}{v_{be}} = \frac{di_C}{dv_{BE}} = \frac{i_C}{V_T}$$

Biased at  $i_C = I_{CQ}$ ,

$$g_m = \frac{I_{CQ}}{V_T}$$

$$r_e = \frac{1}{g_m} = \frac{V_T}{I_{CQ}}$$

$$r_\pi = h_{fe} r_e = \frac{h_{fe} V_T}{I_{CQ}}$$

At room temperature,  
 $V_T = kT/q = 0.026 \text{ V}$