



Review of Techniques for Bearings & Gearbox Diagnostics

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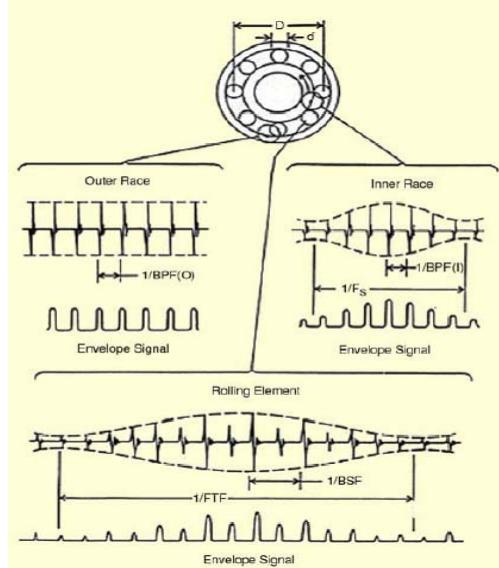
IMAC Conference - Feb. 3, 2010
Jacksonville FL

Rolling Element Bearing Faults



Rolling Element Bearing Faults

- Ball damage
- Inner race defect
- Outer race defect
- Cage damage



Rolling Element Bearing Faults

$$\text{ball passing frequency outer race } BPF_O = \frac{nf_r}{2} \left\{ 1 - \frac{d}{D} \cos \phi \right\}$$

$$\text{ball passing frequency inner race } BPF_I = \frac{nf_r}{2} \left\{ 1 + \frac{d}{D} \cos \phi \right\}$$

$$\text{fundamental train frequency } FTF = \frac{f_r}{2} \left\{ 1 - \frac{d}{D} \cos \phi \right\}$$

$$\text{Ball spin frequency } BSF = \frac{D}{2d} \left\{ 1 - \left(\frac{d}{D} \cos \phi \right)^2 \right\}$$

D = pitch dia; d = ball dia; ϕ = contact angle;
n = no. of balls



Assumptions Made in Bearing Fault Frequencies Equations

1. All balls/rollers are equal in diameter
2. There is pure rolling contact between balls, inner race and outer race.
3. There is no slipping between the shaft and the bearing
4. Outer race is stationary and inner race rotates

In practice there is always some sliding and slippage specially when a bearing is under load and after some wear

Approximate formulas:

$$\text{BPFI} = 0.55-0.6 \times \text{No. of balls} \times \text{RPM}$$

$$\text{BPFO} = 0.45 \times \text{No. of balls} \times \text{RPM}$$

$$\text{BSF} = 3.5 \times \text{RPM}$$

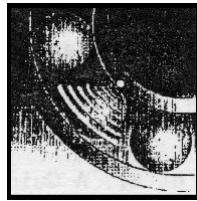


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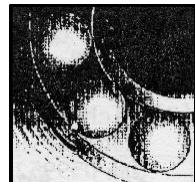
Bearing Defects



BPFO



BPFI

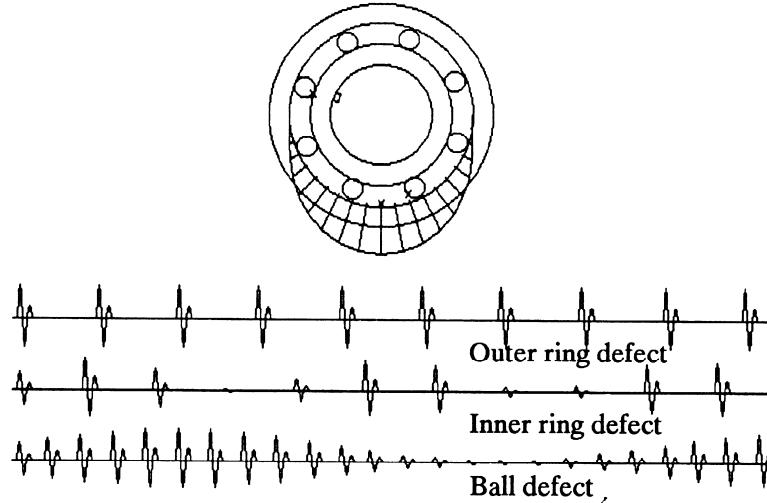


BSF



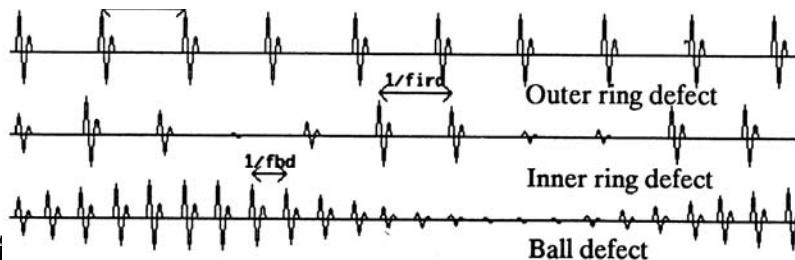
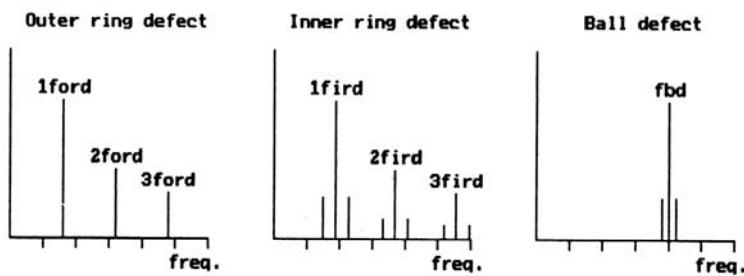
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Time Domain Impact Response



7

Illustration of Sidebands



8

How do we analyze vibration signature of bearing faults? & Issues

- Observe the time waveform and the spectrum to see differences between the good and bad bearing data
- Compare the observed frequencies with the calculated frequencies. Are the peaks present ?
- Signals are often masked by large amplitude periodic components
- Direct Spectral analysis may not give sufficient information
- Bearing faults create a series of impacts which are amplified by resonances: bearing, sensors, structure etc
- This creates envelopes of specific faults at high frequencies
- Fault signals are not periodic; appear more like random
- Some cases can be treated as cyclostationary
- New techniques are still being developed



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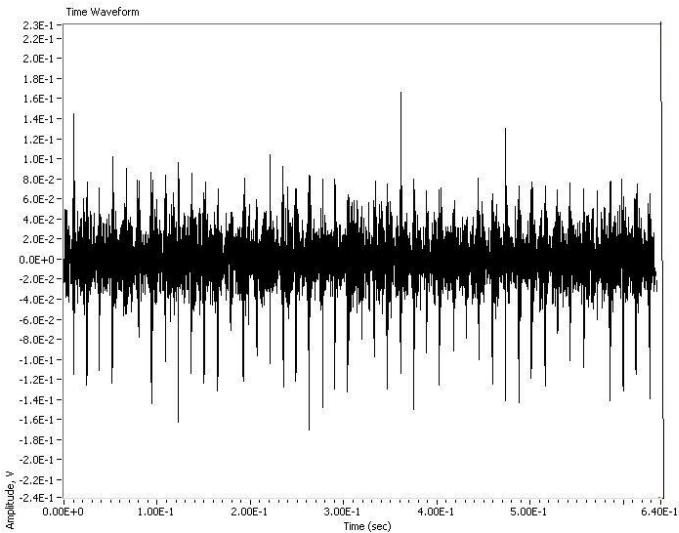
Techniques Currently used in Industrial Products

- Time Waveform Analysis
- Frequency Spectral Analysis
- High Frequency Detection (HFD)
- Stress Wave Analysis or Spike Energy
- PeakView ®
- Enveloping

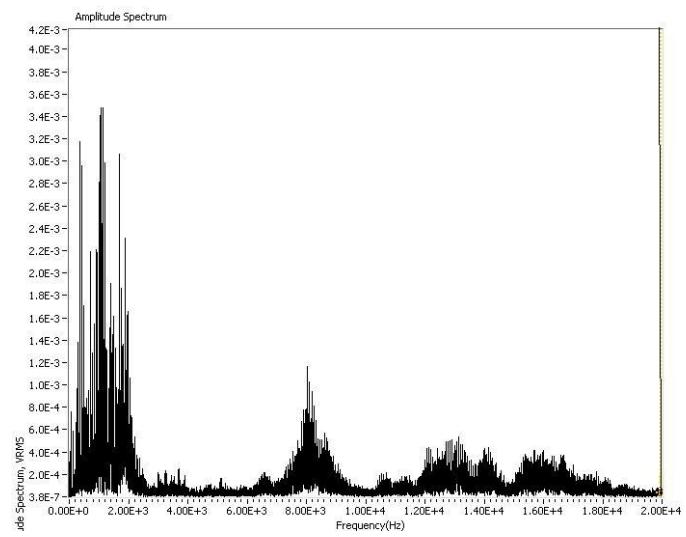


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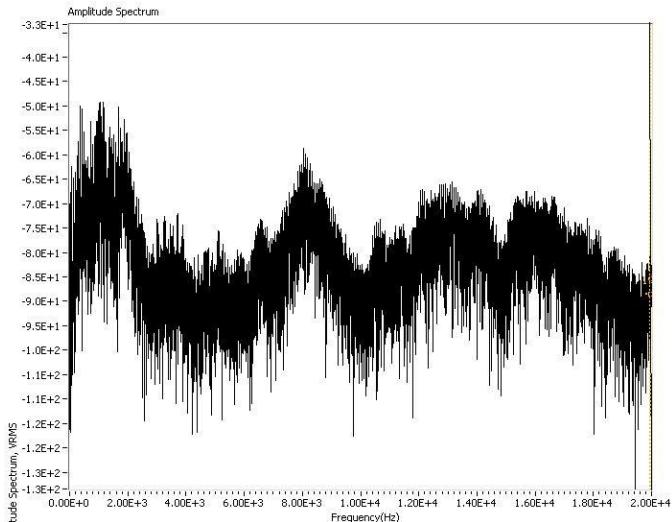
Typical Bearing Outer race Fault Waveform



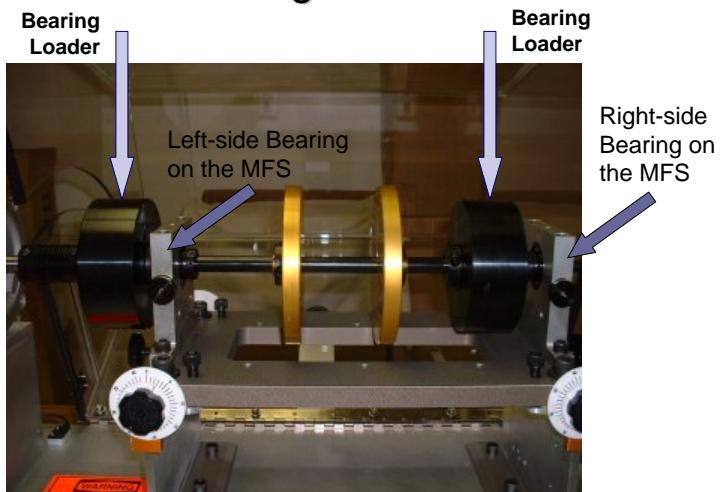
Typical Bearing Outer race Fault Spectra



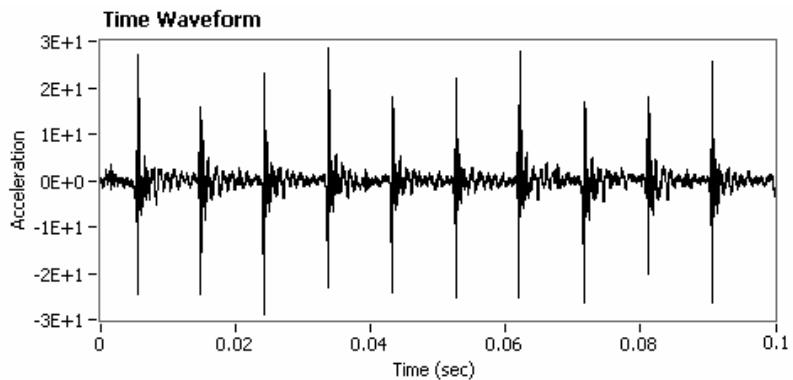
Typical Bearing Outer race Fault Spectra



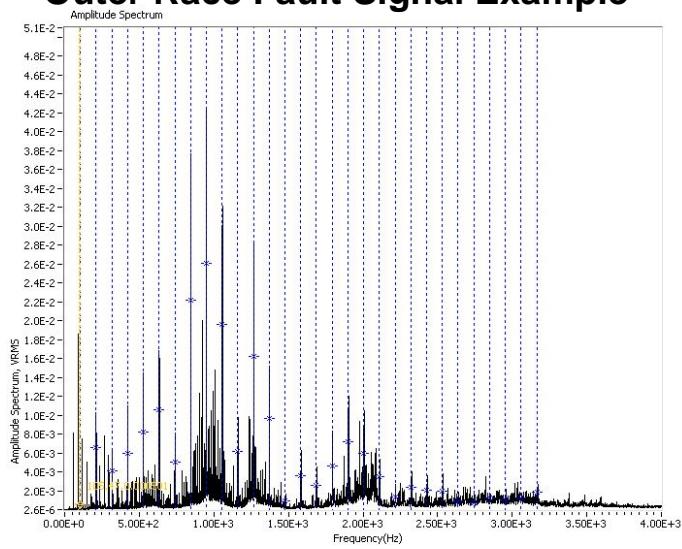
Bearing Fault



Bearing Outer Race Faults



Outer Race Fault Signal Example



The harmonics of BPFO show up clearly

MB ER-10K bearing parameters:
Number of rolling element: 8
Rolling element diameter: 0.3125 Inches
Pitch diameter: 1.319 inch
Contact angle: 0 degree

$$BPFO = \frac{Nb}{2} * \left(1 - \frac{Bd}{Pd} * \cos\theta\right)$$



Bearing Faults for MB ER-10K bearing at the Running Speed of 2,004 RPM

Notation	Fault Frequency Multiplier	Fault Frequency (Hz)	Harmonics of the Running Speed	Harmonic Frequencies (Hz)	Delta Frequencies (Hz)	Resolution to Detect the Fault Frequencies = Delta Frequencies/4 (Hz)
BPFI	4.9480	165.3176	5	167.0570	1.7394	0.4349
BFPO	3.0520	101.9704	3	100.2340	1.7364	0.4341
BSF	1.9920	66.5547	2	66.8230	0.2683	0.0671

RPM Harmonics

1	2	3	4	5	6	7	8
33.411	66.823	100.234	133.646	167.057	200.469	233.880	267.291
1.674E-5	1.966E-5	1.014E-5	4.219E-5	1.309E-4	7.179E-5	9.206E-5	7.807E-5

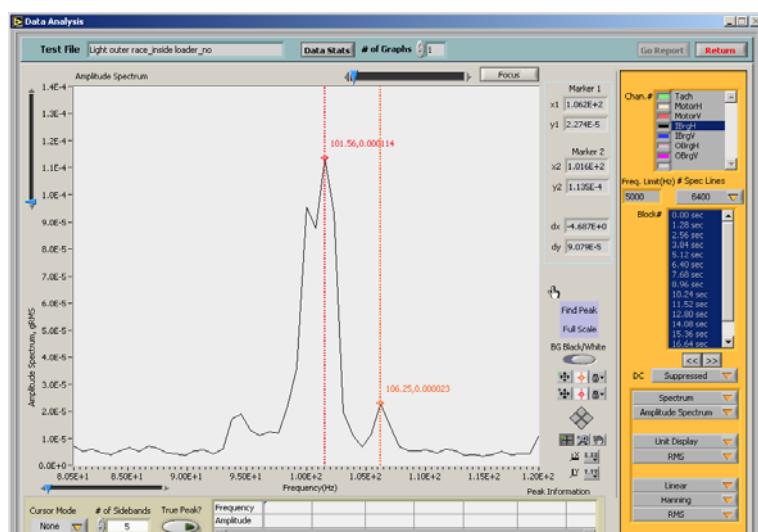


Spectral Resolution for 5,000 Hz Maximum Frequency Setting

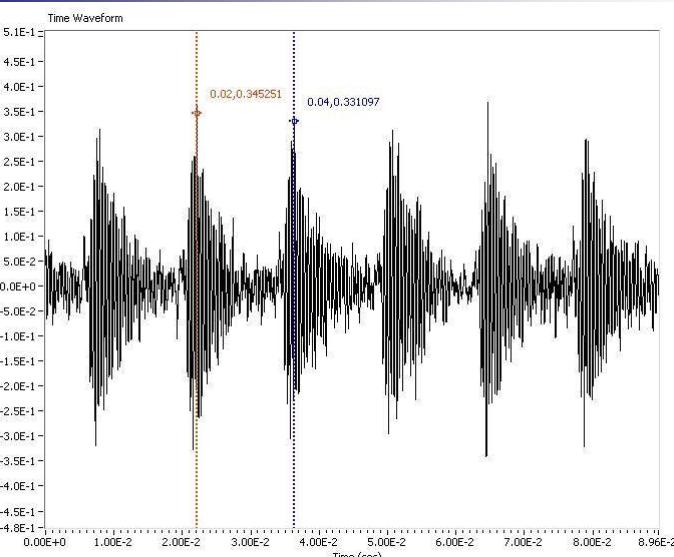
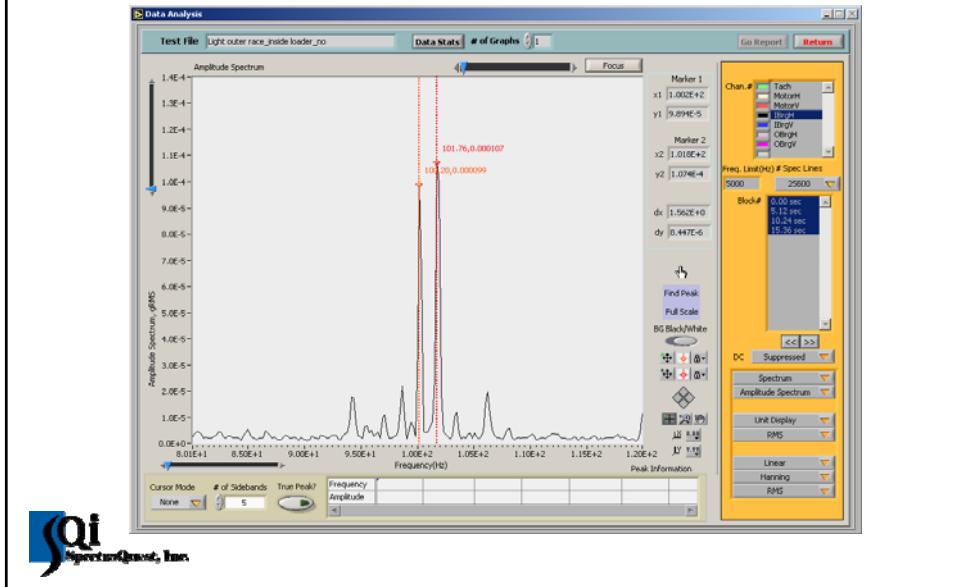
Spectral Lines	Resolution, Hz	Resolution, RPM
100	50.0000	3,000.0000
200	25.0000	1,500.0000
400	12.5000	750.0000
800	6.2500	375.0000
1,600	3.1250	187.5000
3,200	1.5625	93.7500
6,400	0.7813	46.8750
12,800	0.3906	23.4375
25,600	0.1953	11.7188
51,200	0.0977	5.8594
102,400	0.0488	2.9297



Resolution: 6400 FFT Lines using a Hanning Window

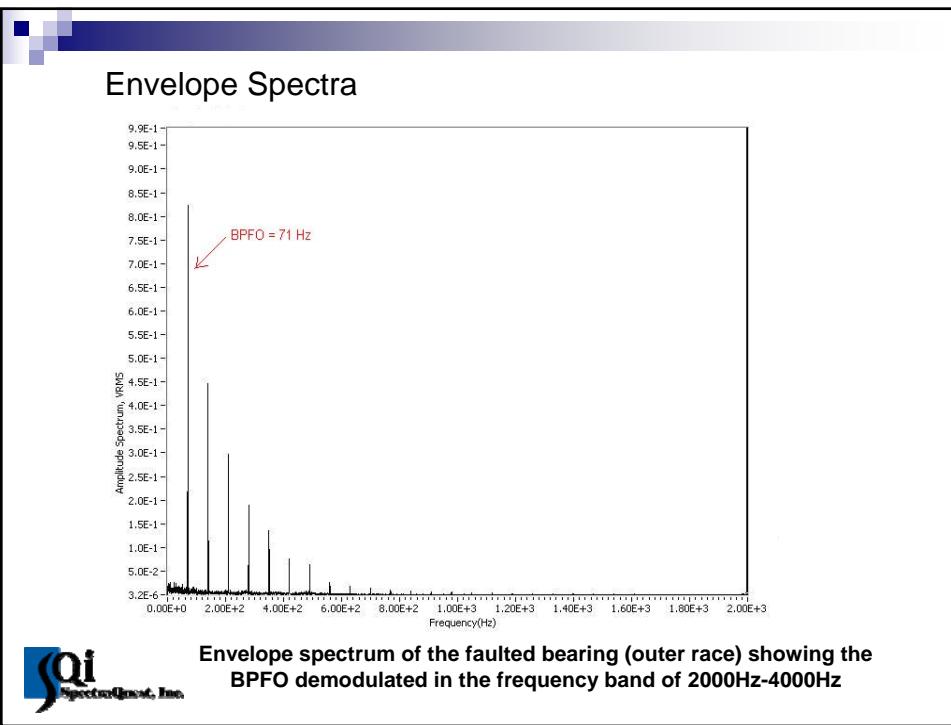
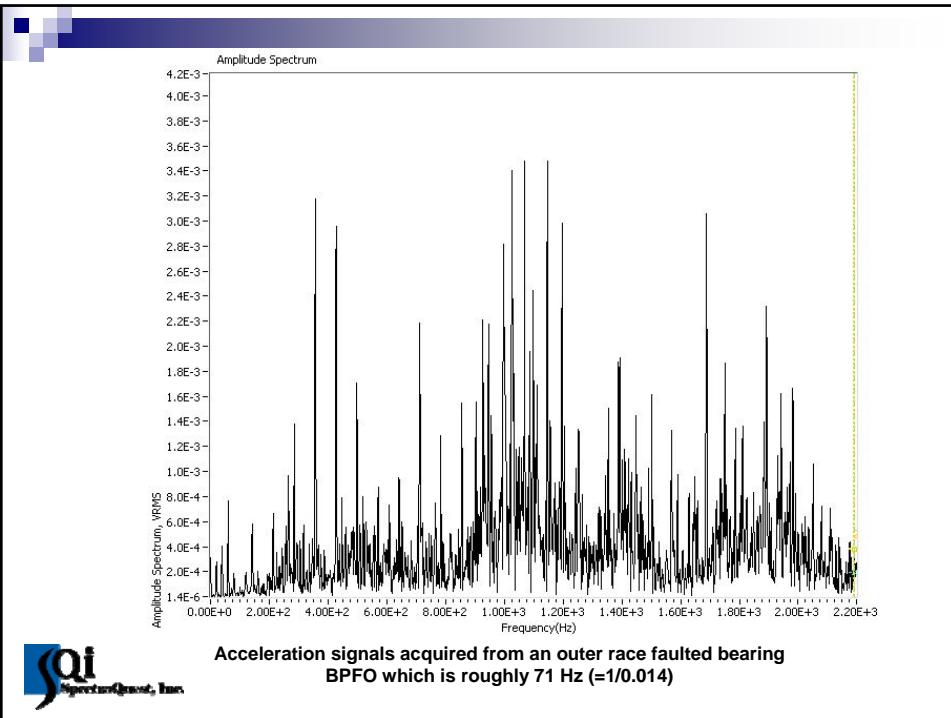


Resolution: 25600 FFT Lines using a Hanning Window

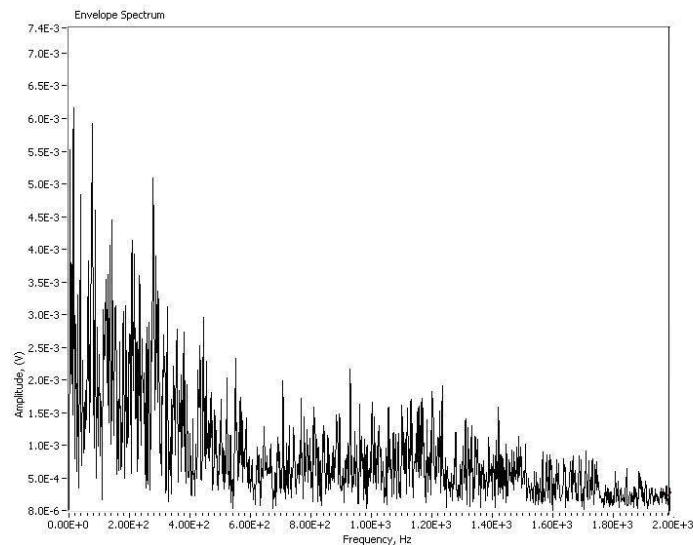


Acceleration signals acquired from an outer race faulted bearing
BPFO which is roughly 71 Hz (=1/0.014)



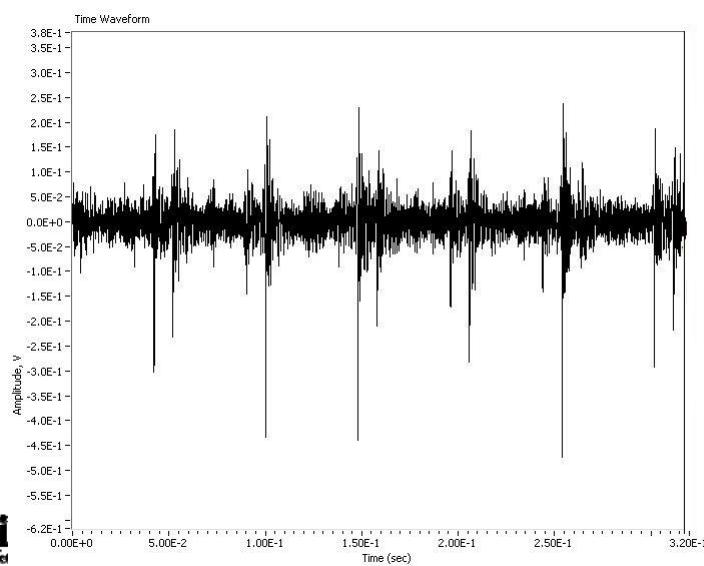


Effect of demodulation band

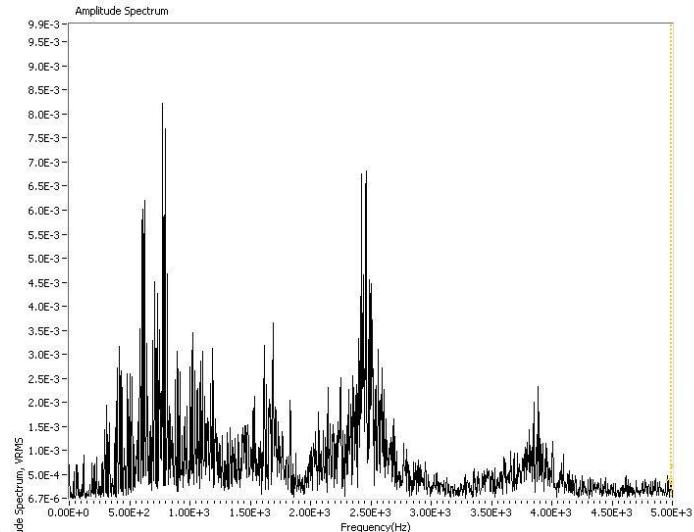


Envelope spectrum of the faulted bearing (outer race) not showing the
BPFO demodulated in 10k-12k Hz band

Inner race Fault Time Waveform

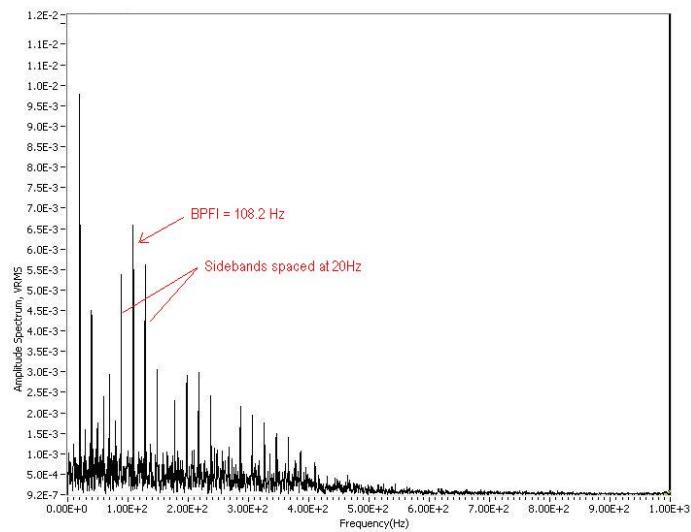


Inner Race Fault Spectra



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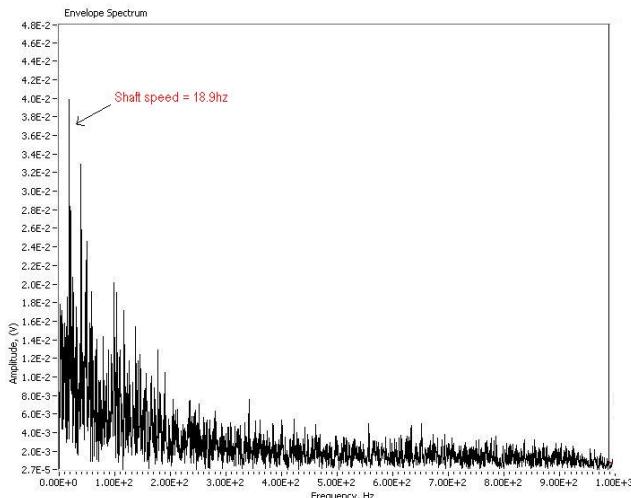
Envelope Spectrum



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Envelope spectrum of the inner race faulted bearing with a shaft speed of 20 Hz showing the BPFI and sidebands with a 750 psi load

Effect of load



Envelope spectrum of the inner race faulted bearing not showing the BPFI under no load

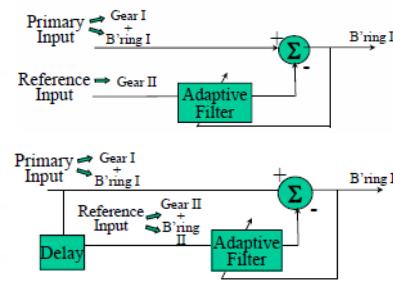
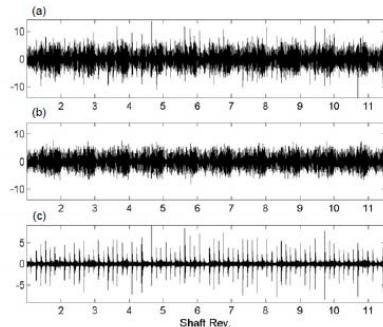
New Techniques under Research

- Adaptive Noise Cancellation (ANC)
- Self-adaptive Noise Cancellation (SANC)
- Spectral Kurtosis
- Discrete Random Separation
- Cyclostationary Signal Analysis
- Julian
- Hilbert-Huang Transform
- Entropy



■ Adaptive Noise Cancellation (ANC)

- Removes the random components from the periodic components
- Requires reference input along with primary input
- SANC uses the delayed primary signal as reference signal
- It uses the fact that bearing signals has a short correlation length



Ref: Prof. Bob Randall



Fault bearing signal with gear signal (b) Gear signal –discrete components
(c) Bearing components- random components

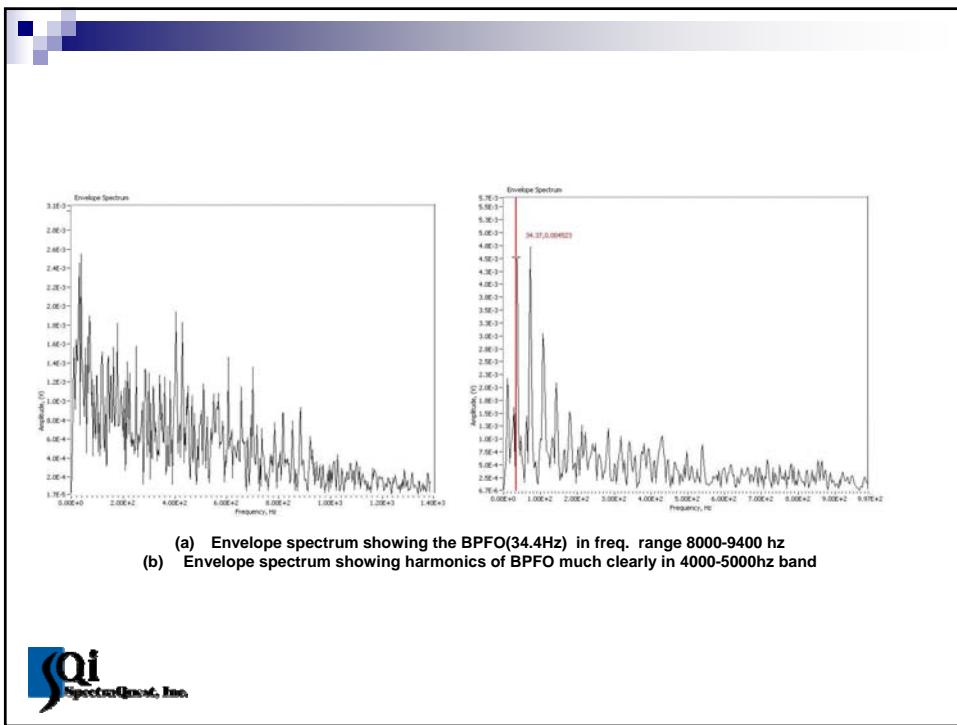
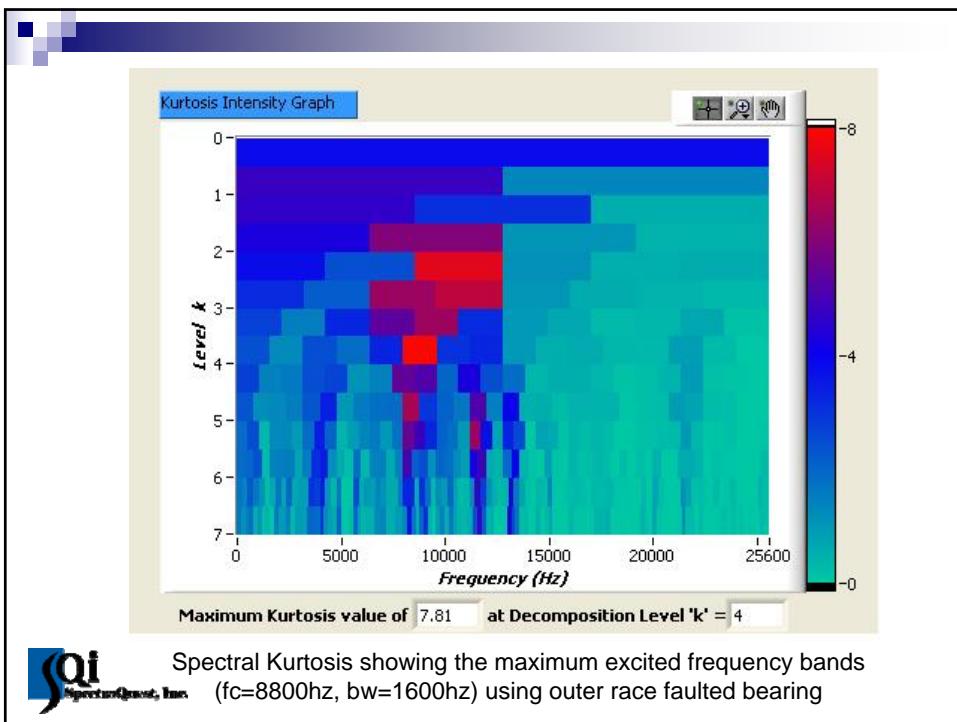
■ Spectral Kurtosis

- Calculates Kurtosis for each frequency line
- Identifies the impulsiveness in the data
- Uses short time Fourier transform
- Determines optimum band for demodulation

$$kurtosis(y) = \frac{\text{mean}(y^2)}{(\text{mean}(y))^2} - 3$$

y = autospectrum value
(ie amplitude squared)





Gearbox Diagnostics



Techniques for Gearbox Vibration Analysis

- Time Waveform Analysis
- Spectral Analysis
- Order Analysis
- Time synchronous averaging
- Cepstrum Analysis
- Amplitude and Phase Demodulation
- Transmission Error Analysis



Gear Diagnostic Parameters (Vibration Based) Page 1 of 2

MFPT

Gear Diagnostic Parameters (Vibration Based)

Parameter	Reference
RMS	Root Mean Square of the signal
Kurtosis	4th Statistical Moment of the signal normalized by the square of the variance of the signal.
Delta RMS	Change in the Root Mean Square of the signal
Crest Factor	Swanson, N.S. Application of Vibration Signal Analysis Techniques to Signal Monitoring. Conference on Friction and Wear in Engineering 1980. Institution of Engineers, Australia, Barton, Australia, 1980, pp 262-267.
Sideband Level Factor	Fitzgerald, A.P. and Stewart, R.M. Some Gear Diagnostics Using Vibration Analysis. ARL-AERO-RP07-74-027, Aerobus Research Laboratory, Department of Defence Melbourne Australia, 1985.
Energy Ratio	Swanson, N.S. Application of Vibration Signal Analysis Techniques to Signal Monitoring. Conference on Friction and Wear in Engineering 1980. Institution of Engineers, Australia, Barton, Australia, 1980, pp 262-267.
FMD	Stewart, R.M. Some Useful Data Analysis Techniques for Gearbox Diagnostics. Machine Health Monitoring Group, Institute of Sound and Vibration Research, University of Southampton, Report MSHMR/1977, July 1977.
FM2	Stewart, R.M. Some Useful Data Analysis Techniques for Gearbox Diagnostics. Machine Health Monitoring Group, Institute of Sound and Vibration Research, University of Southampton, Report MSHMR/1977, July 1977.
FM4	Stewart, R.M. Some Useful Data Analysis Techniques for Gearbox Diagnostics. Machine Health Monitoring Group, Institute of Sound and Vibration Research, University of Southampton, Report MSHMR/1977, July 1977.
MBA	Martin, H.R. Stochastic Moment Analysis As a Means of Surface Damage Detection. Proceedings of the 7th International Modal Analysis Conference, Society for Experimental Mechanics, Schenectady, NY, 1989, pp. 1016-1021.
MBA	Martin, H.R. Stochastic Moment Analysis As a Means of Surface Damage Detection. Proceedings of the 7th International Modal Analysis Conference, Society for Experimental Mechanics, Schenectady, NY, 1989, pp. 1016-1021.
NA4	Zakrzewski, J.J., Townsend, D.P., Decker, H.J. An Analysis of Gear Fault Detection Methods. NASA Lewis Research Center, NASA Lewis Research Center, NASA Lewis Research Center, 18th Annual Meeting of the Vibration Institute, NASA TM 105950, AVSCOM TR 92-C-035, April 1992.
NA4*	Decker, H.J., Hendrickson, R.F., Zellner, J.C. An Enhancement to the NA4 Gear Diagnostic Parameter. NASA Lewis Research Center, NASA Lewis Research Center, NASA TM 105953, April 1992.
NB4	Dengler, J.J., Haensel, R.F., Decker, H.J. Application of Fault Detection Techniques to Spiral Bevel Gear Fatigue Data. NASA Lewis Research Center/U.S. Army Research Laboratory, 4th Mechanical Failures Prevention Group, Wakefield, Mass., Report AFML-TR-97-ARG-0345.
NB4*	Application of difference between NA4 and NA4* to NB4. No paper published.
NP4	Polyanshuk, V.V., Choi, F.K., Braun, M.J. Gear Fault Detection with Time-Frequency based Parameter NP4. Proceedings from the 8th International Symposium on Transport Phenomena and Dynamics of Rotating Machinery (ISROMAC-8), Honolulu, Hawaii, 1998.

http://mfpt.org/Archive%2001\%20Pages\mfpt_geardiagnosticparam.html 1/28/2010

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Gearbox Vibration

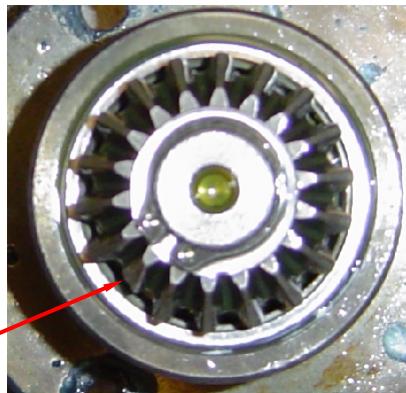
The diagram illustrates a gearbox assembly. On the left, a top-down view shows the housing with two shafts extending from it: the 'input shaft' on the bottom-left and the 'output shaft' on the top-left. On the right, a side view shows the internal components: a 'gear' mounted on a shaft and a 'pinion' meshing with it. Arrows point from the text labels to their respective parts in the diagram.

Transmission ratio: 1.5:1, (27 and 18 teeth)

SQI SpectraQuest, Inc.

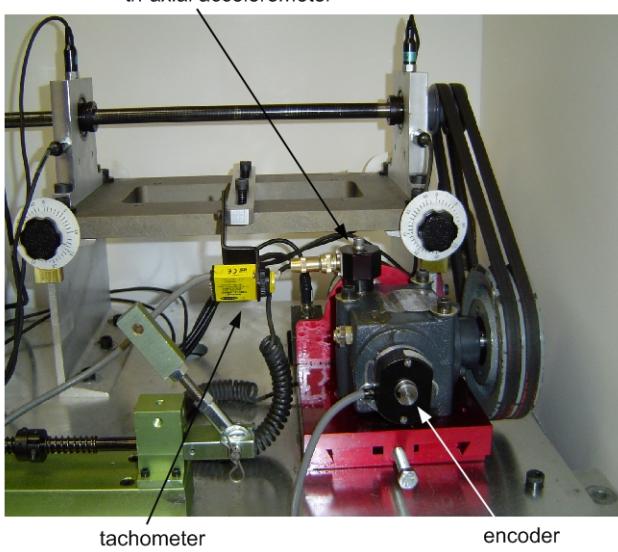
Gearbox Vibration

Missing of tooth



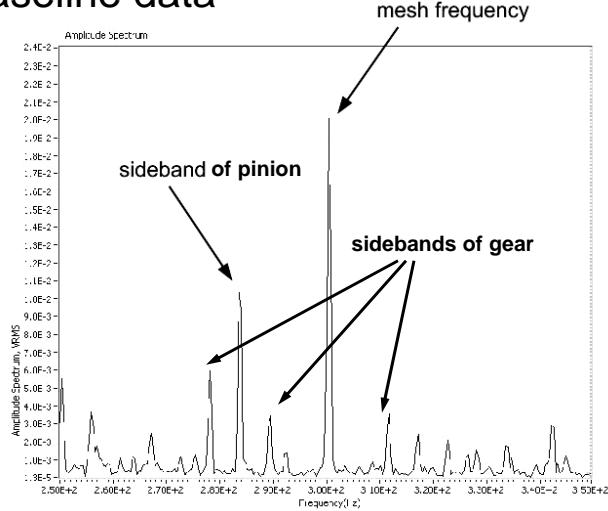
Gearbox Vibration

tri-axial accelerometer



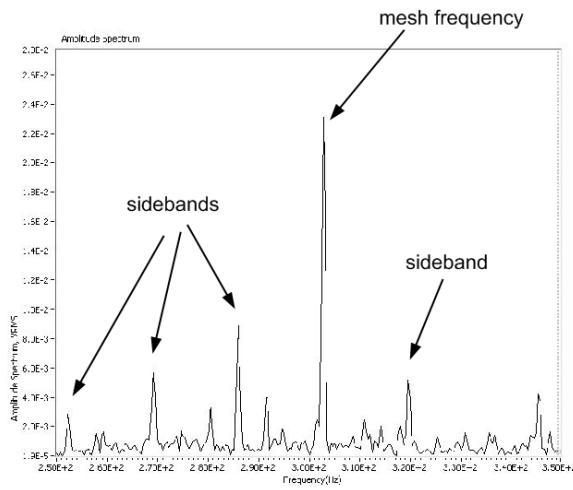
Gearbox Vibration

Baseline data



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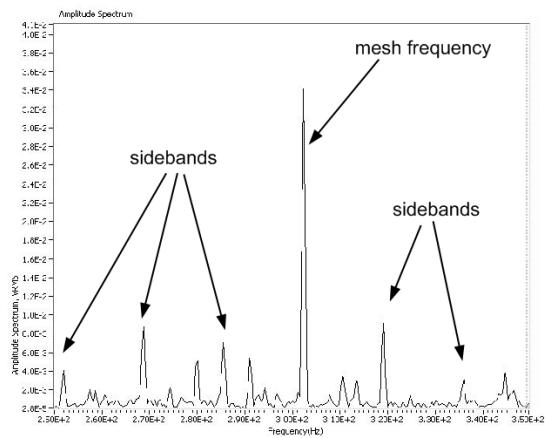
Spectrum of Fault Level 1 Data



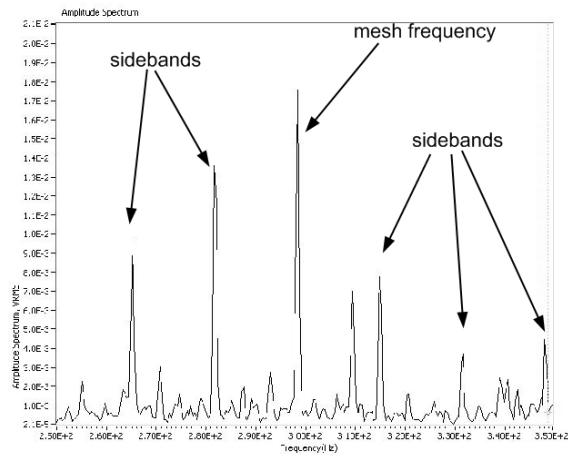
SQI
SpectraQuest, Inc.

Compared with baseline, more pinion sidebands emerge

Spectrum of Fault Level 2 Data



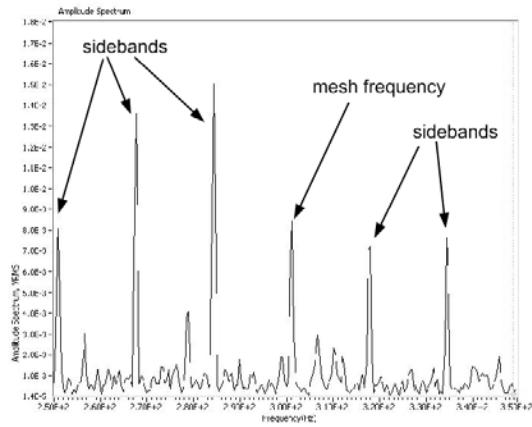
Spectrum of Fault Level 3 Data



Compared with baseline, the amplitudes of pinion sidebands Increase significantly.



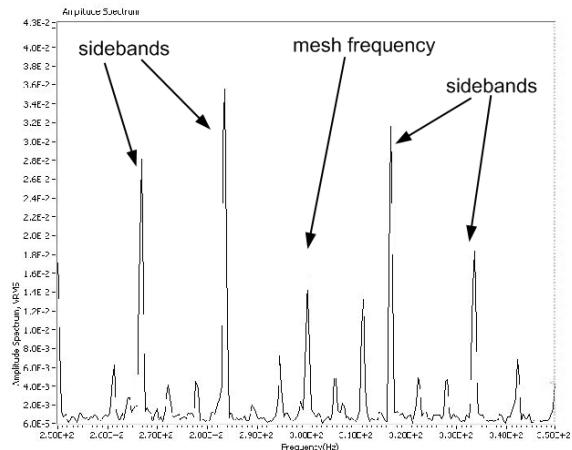
Spectrum of Fault Level 4 Data



The amplitudes of pinion sidebands continually Increase.



Spectrum of Fault Level 5 Data



The amplitudes of pinion sidebands exceed that of the mesh frequency

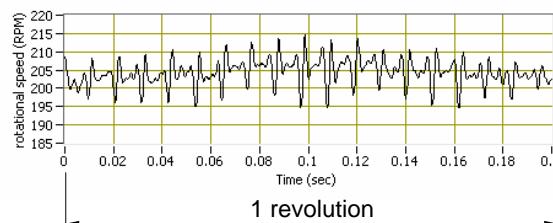


For the missing of a tooth.

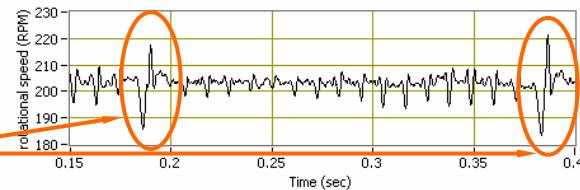
Gear vibration – order analysis

Speed variation captured using encoder

Intact gear
(small spikes are
caused by gear
meshing)

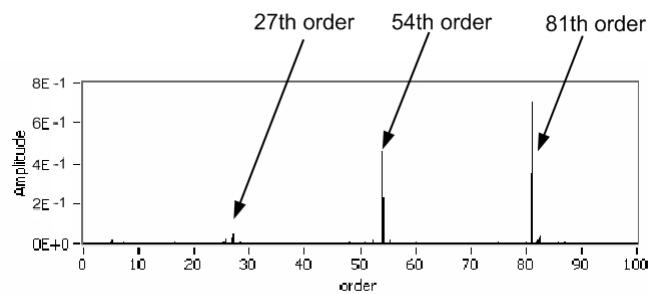


Fault level 5
(impacts caused
by missed tooth)



Gear vibration – order analysis

Speed Variation Order Spectrum - baseline

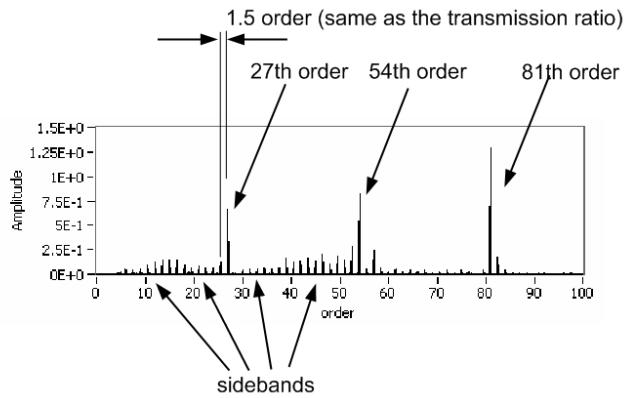


The number of teeth on gearbox output shaft is 27. The 27th, 54th and 81th orders have high amplitude. They correspond to the mesh frequency and its 2nd and 3rd harmonics.



Gear vibration – order analysis

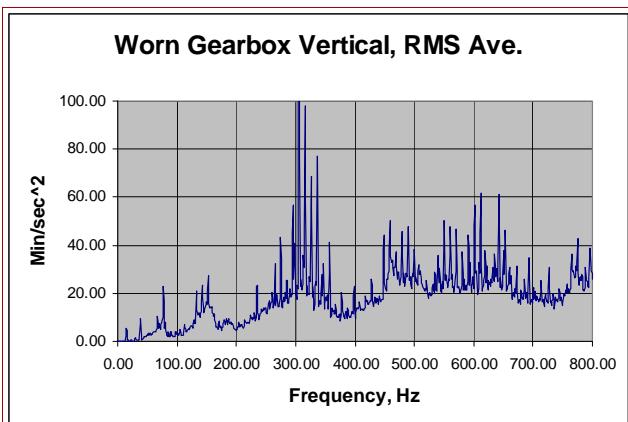
Speed Variation Order Spectrum – fault level 5



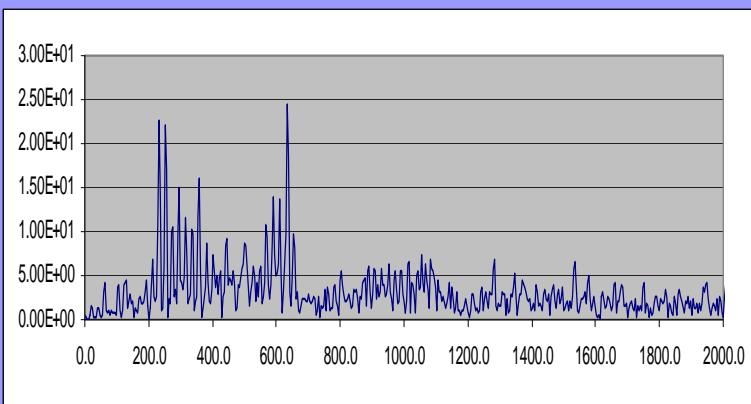
Pinion sidebands emerge clearly for the missing of a tooth



Time Synchronous Averaging

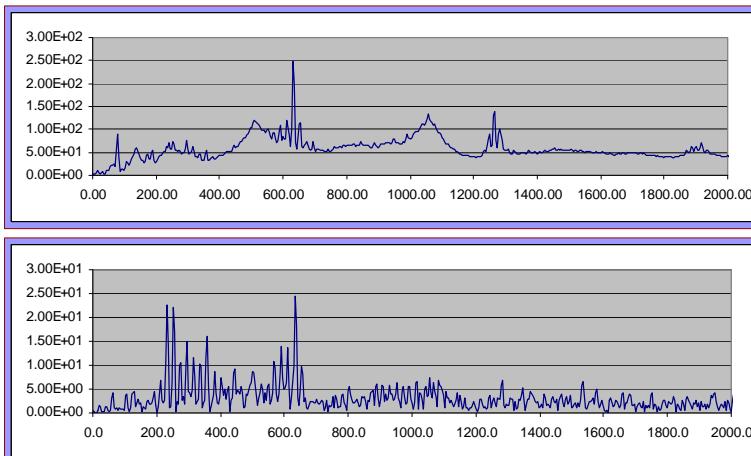


Time Synchronous Averaging



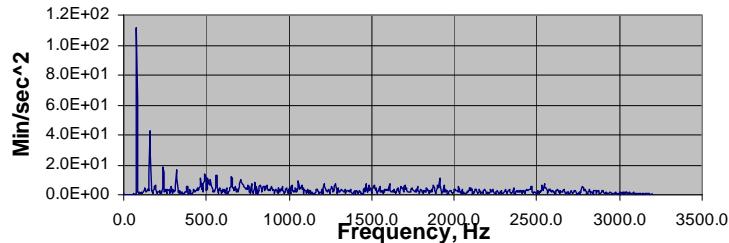
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Worn Gearbox data comparison, two Types of Averaging



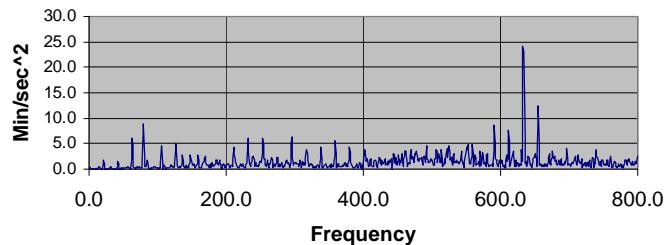
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Worn Gearbox Time Synchronous Averaging



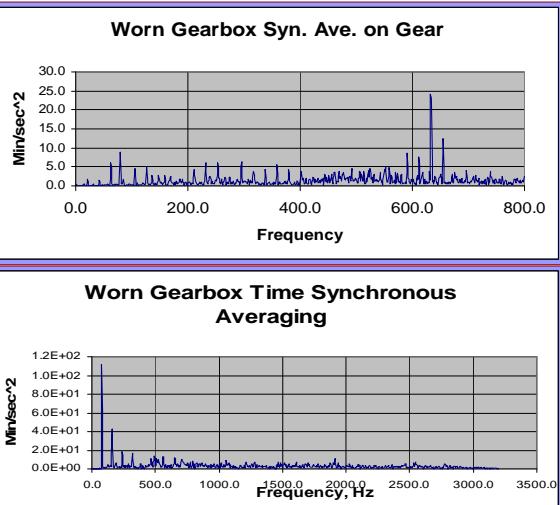
53

Worn Gearbox Syn. Ave. on Gear



54

Worn Gearbox data comparison, TSA at Two Shafts



55

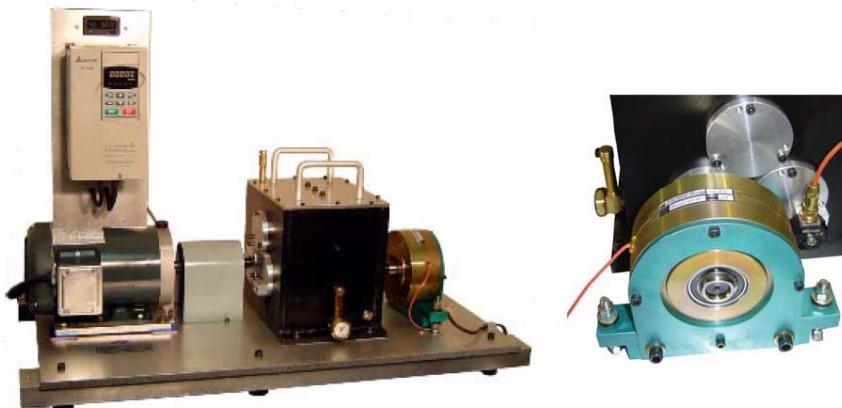
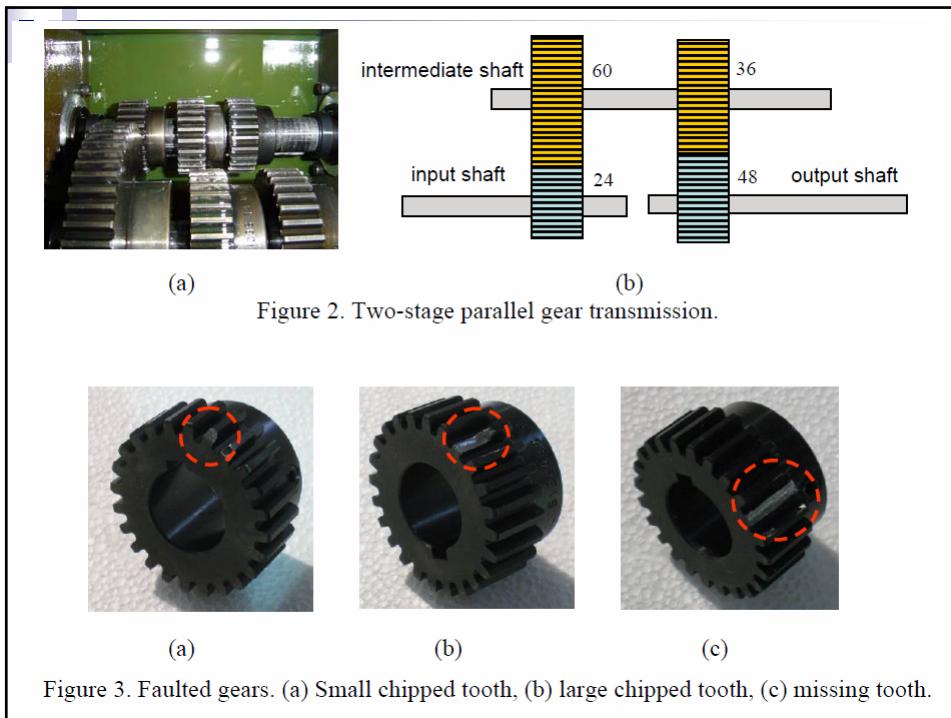


Figure 1. Gearbox dynamics simulator and the magnetic brake.





Speed = 59.37 Hz

$$f_{m1} = 24 \times f_i,$$

$$f_{m2} = f_i \times \frac{24}{60} \times 36,$$

f_{m1} and f_{m2} are roughly 1425 Hz and 854 Hz,

Side bands = 59.37, 23.7, 17.8 Hz

Baseline Data

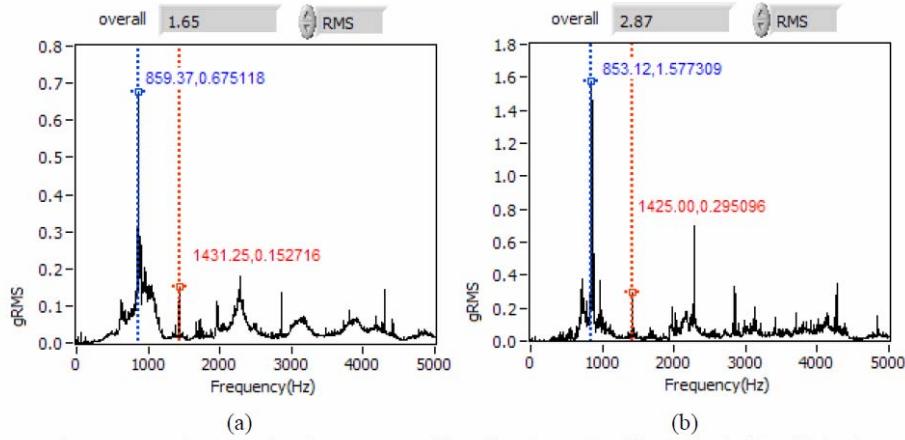


Figure 5. Gearbox acceleration spectra of baseline data. (a) without load, (b) with load.



Chipped Tooth Data

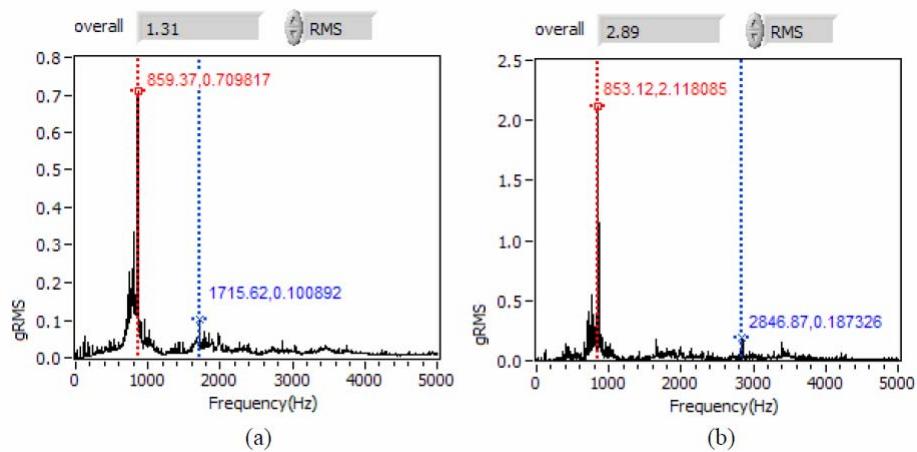


Figure 6. Gearbox acceleration spectra of Test 6. (a) without load, (b) with load.



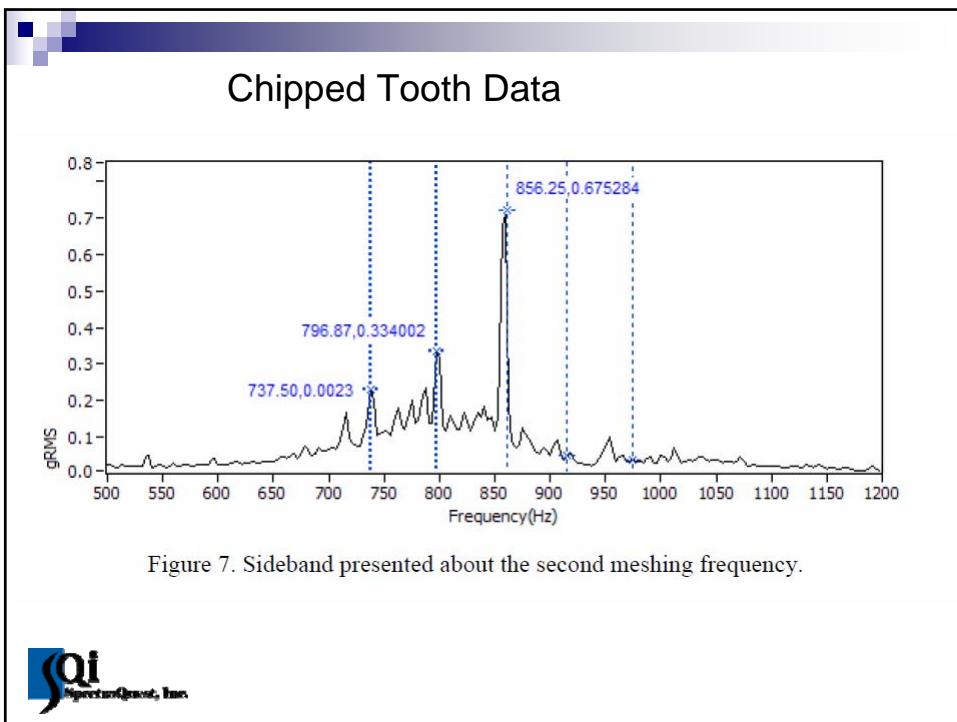


Figure 7. Sideband presented about the second meshing frequency.

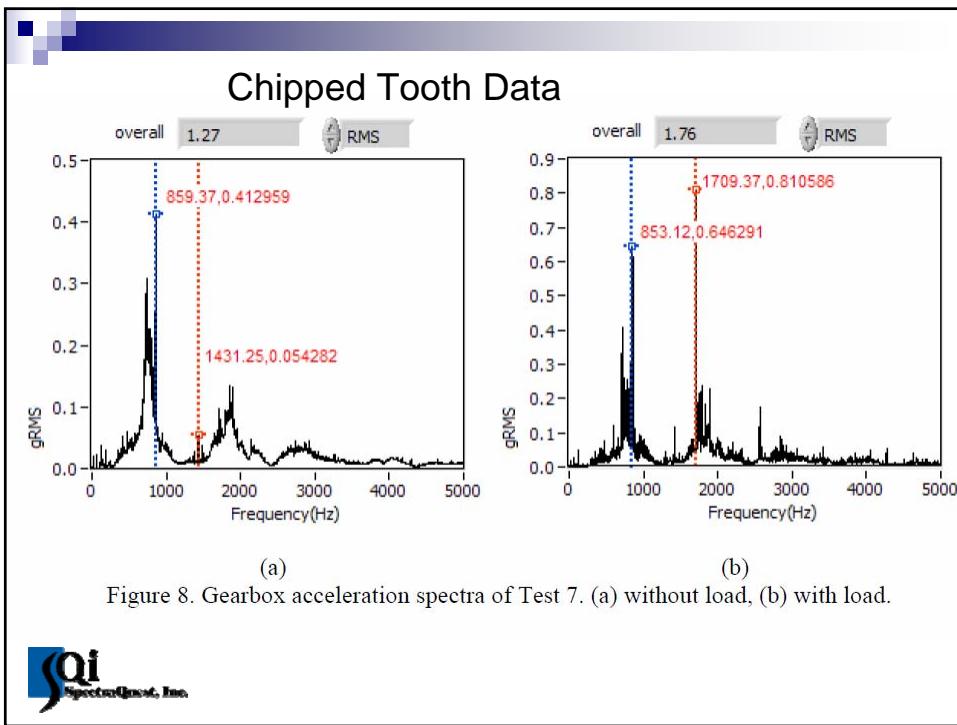


Figure 8. Gearbox acceleration spectra of Test 7. (a) without load, (b) with load.



Missing Tooth Data

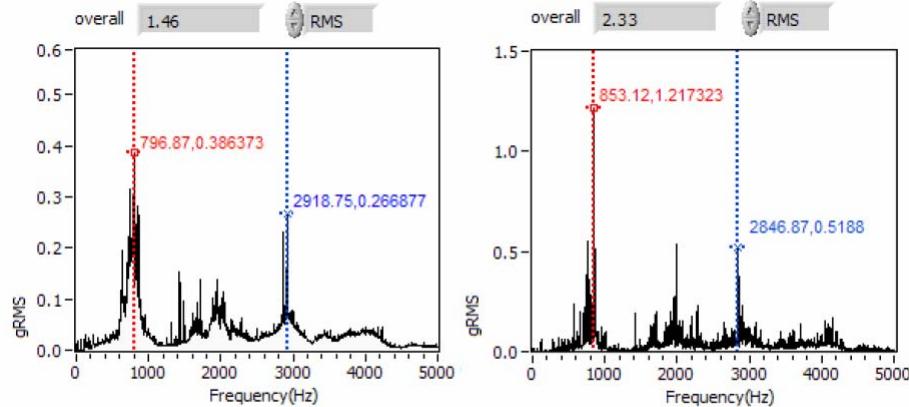


Figure 9. Gearbox acceleration spectra of Test 5. (a) without load, (b) with load.



Missing Tooth Data

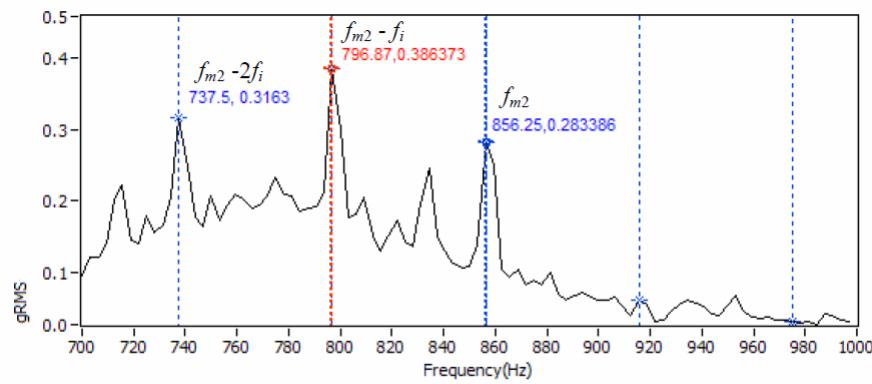


Figure 10. Sidebands about f_{m2} .



Missing Tooth Data

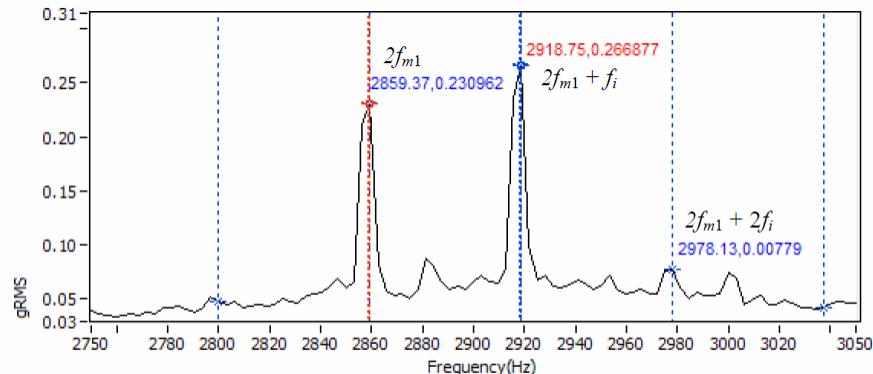


Figure 11. Sidebands about the $2f_{m1}$.



■ Cepstrum Analysis

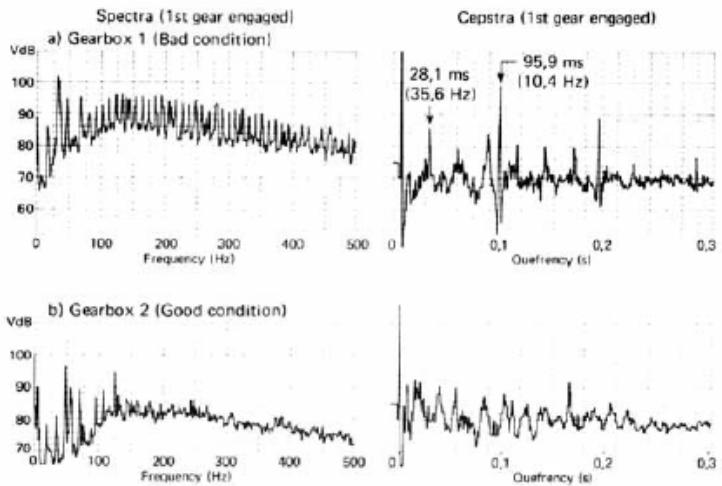
- Inverse Fourier transform of logarithmic spectrum
- Useful for detecting changes in sideband families
- Echo, Transmission path, etc
- Quefrency, Rahmonic, Gamplitude, Lifter, Saphe

$$C(\tau) = \mathfrak{I}^{-1}[\log(X(f))]$$

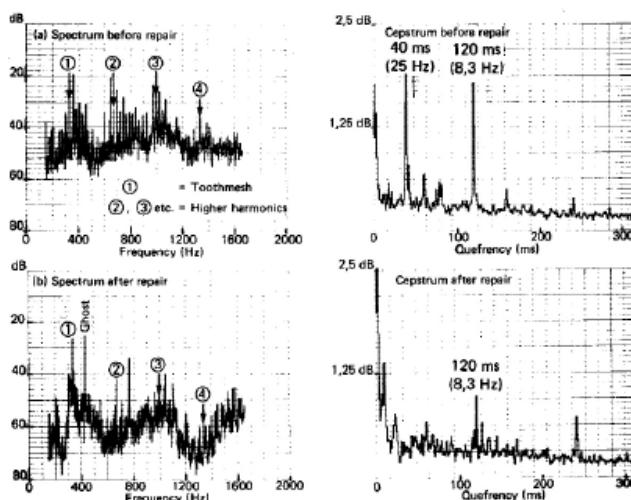
Where $X(f)$ is the Fourier transform of $x(t)$



Cepstrum Analysis



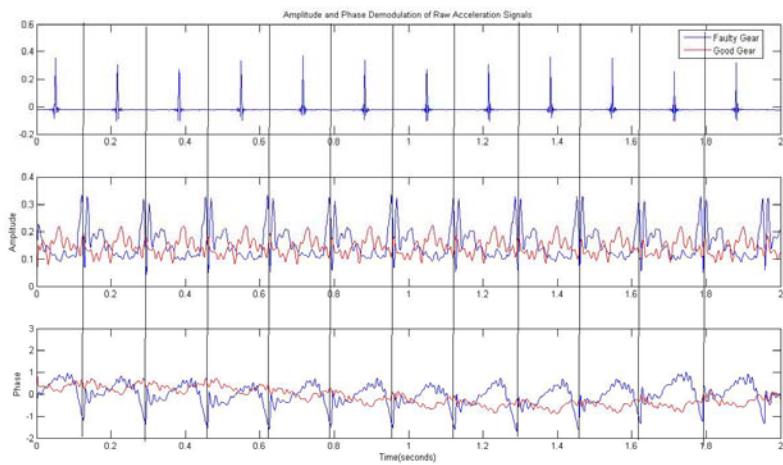
Signal Separation with Cepstrum



Use of cepstrum to remove sideband patterns

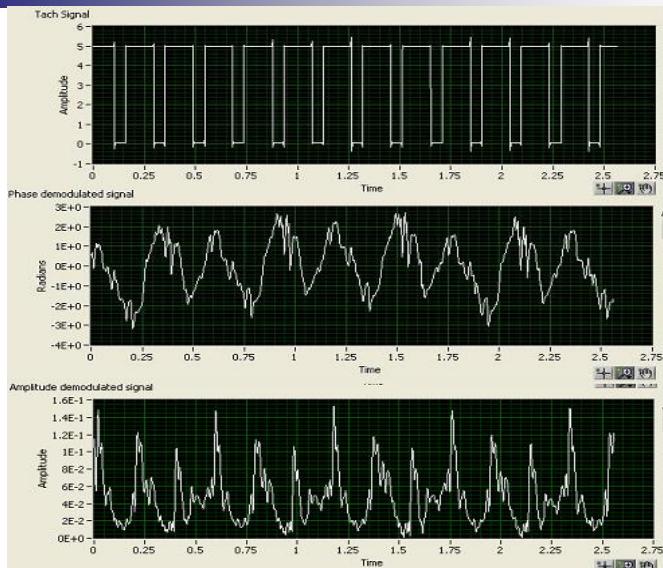
Ref: Prof. Bob Randall

Amplitude & Phase Demodulation



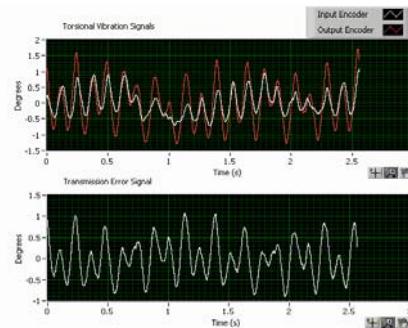
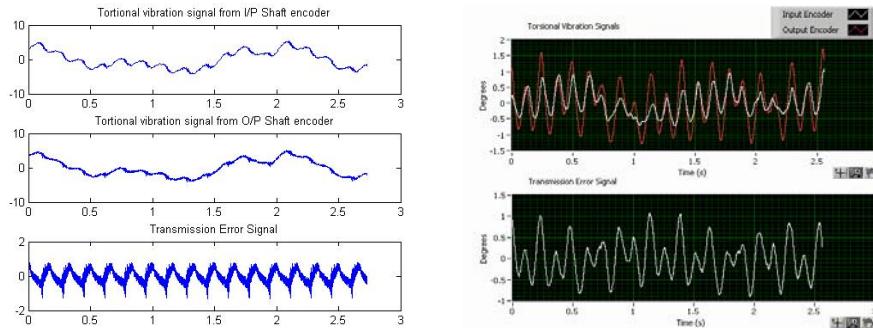
Amplitude and Phase Demodulation of raw acceleration signals from a gearbox with chipped tooth ; note both phase and amplitude demodulation work

Ref: Prof. Bob Randall

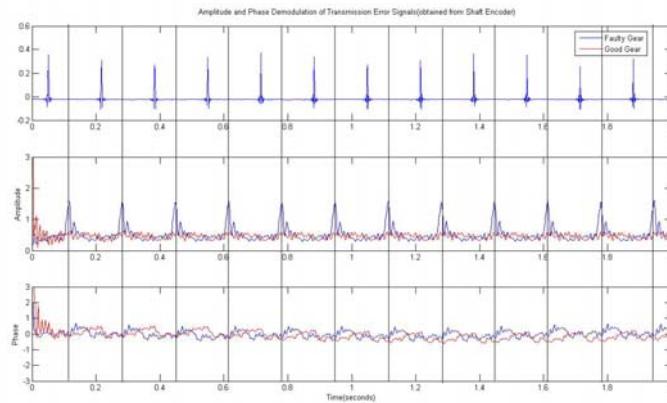


Amplitude and Phase Demodulation of raw acceleration signals from a parallel shaft gearbox with chipped tooth (where phase demodulation did not work)

Transmission Error



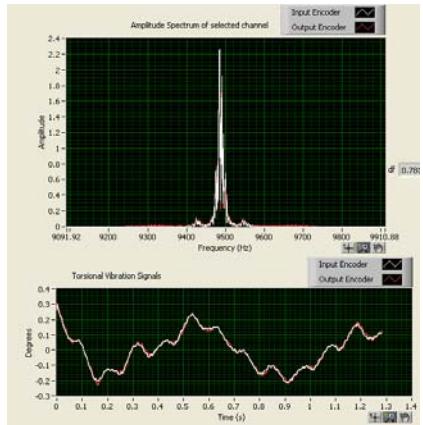
Amplitude & Phase Demodulation on Transmission Error Signal



Note that amplitude demodulation worked
but phase demodulation did not work



Torsional Vibration Signals obtained from TVC
with zero degree deflection



Torsional Vibration Signals obtained from TVC
with 12.5 degree deflection

