

Calvin Passmore

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ECE 5420

Lab Amplifiers

1 Prelab

$$i = 1/2 * K_n * V_{ov}^2$$

$$V_{gs} = V_{ds}$$

$$i = (V_{dd} - V_{ds}) / (R_{ref})$$

$$V_{ds} = V_{dd} - i * R_{ref} = V_{gs}$$

$$i = 1/2 * K_n * (V_{dd} - i * R - V_{th})^2$$

$$i = 1/2 * K_n * [(V_{dd}^2 - V_{dd} * R - V_{th} V_{dd}) + (-V_{dd} i * R + i^2 * R^2 + V_{th} * i * R) + (-V_{th} * V_{dd} + V_{th} * i * R + V_{th}^2)]$$

$$i = 1/2 * K_n [V_{dd}^2 + i^2 * R^2 + V_{th}^2 - 2 * V_{dd} * i * R + 2 * V_{th} * i * R - 2 * V_{th} * V_{dd}]$$

$$0 = i^2 (1/2 * K_n * R^2) + i (-2 * V_{dd} * R + 2 * V_{th} * R - 1) + (V_{dd}^2 + V_{th}^2 - 2 * V_{th} * V_{dd})$$

$$i = ((2 * V_{dd} * R - 2 * V_{th} * R + 1) \pm \sqrt{(-2 * V_{dd} * R + 2 * V_{th} * R - 1)^2 - 2 * K_n * R^2 * (V_{dd}^2 + V_{th}^2 - 2 * V_{th} * V_{dd})}) / (K_n * R)$$

```
In [ ]: from math import sqrt
Vdd = 5 # V
Vth = 0.75
Kn = 0.7e-3 # A
R = 10e3 # Ohm

i_refp = ((2 * Vdd * R - 2 * Vth * R + 1) + sqrt((-2 * Vdd * R + 2 * Vth * R - 1)**2 - 2 * Kn * R**2 * (Vdd
```

```
i_refn = ((2 * Vdd * R - 2 * Vth * R + 1) - sqrt((-2 * Vdd * R + 2 * Vth * R - 1)**2 - 2 * Kn * R**2 * (Vd
print(i_refp)
print(i_refn)
```

24283.874839036227

2.12516096377554

i_ref = 2.125 mA

gm = sqrt(2 * IB * Kn)

ro = 1 / (λ * IB)

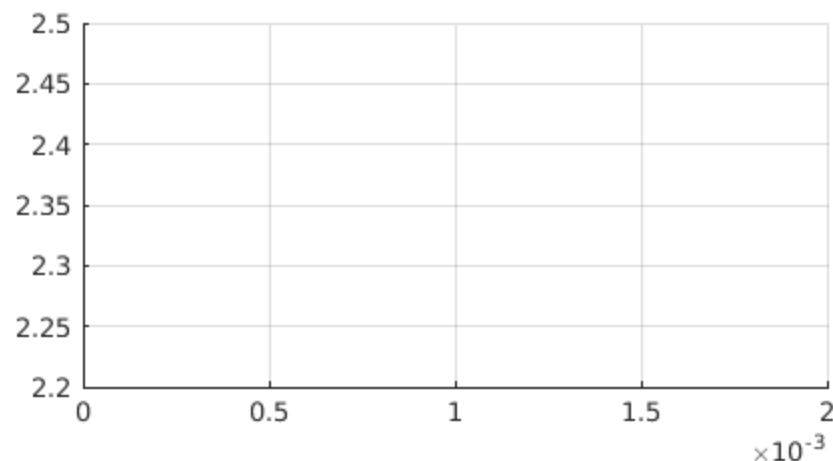
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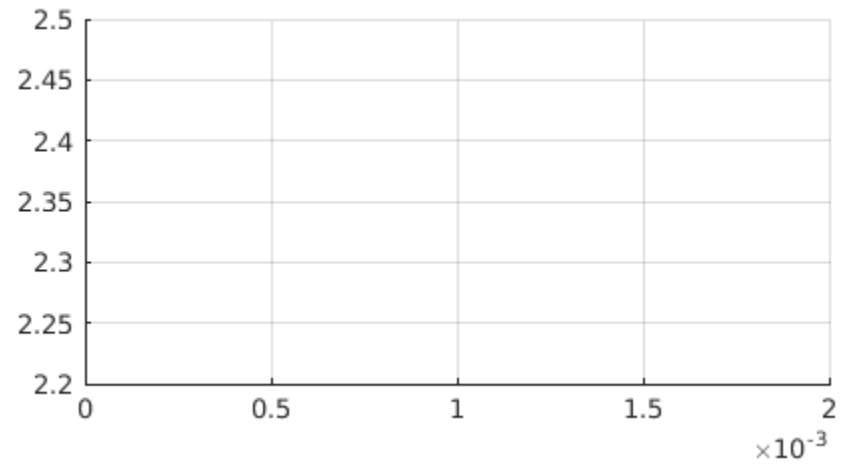
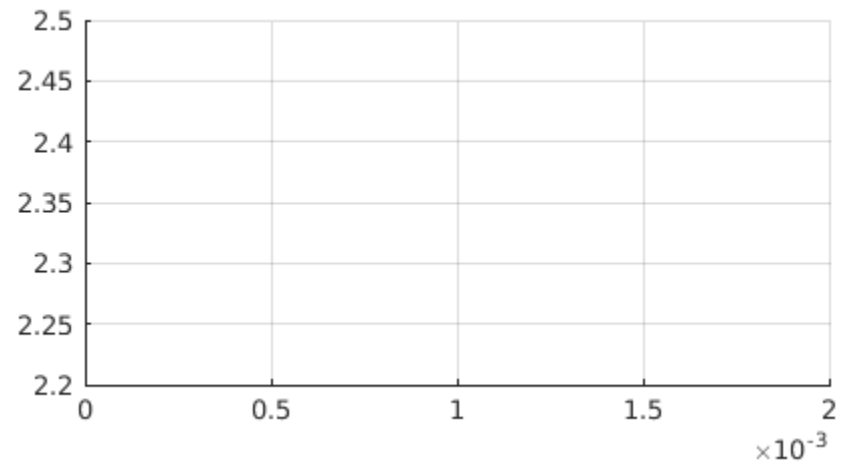
Here is the results table that I generated

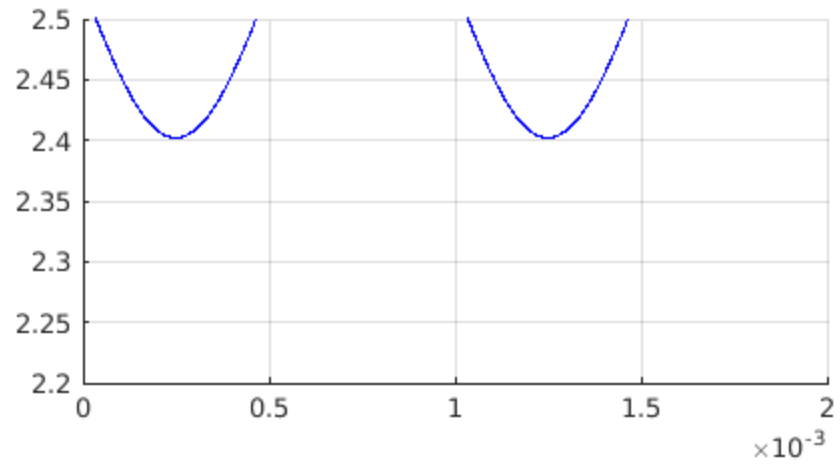
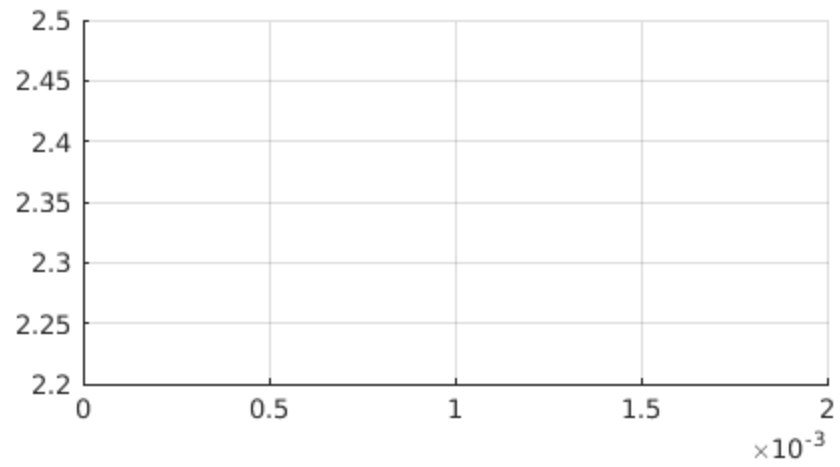
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1	1.359372e-11	2.440357e-10	5.888259e+12	2.172622e+11	
1	-4.50000e+00	4.562770e-08	7.934292e+01	3.799016e+01	3.868502e+03
2	4.802508e-07	5.566229e-07	1.735504e+08	1.161310e+08	
2	-4.00000e+00	6.795952e-05	1.064588e+02	4.054363e+01	6.098432e+05
3	2.204869e-04	1.200721e-04	8.519460e+05	1.011310e+06	
3	-3.50000e+00	2.491448e-04	8.294510e+01	3.837581e+01	1.492871e+06
4	4.165233e-04	2.200303e-04	3.530310e+05	4.271133e+05	
4	-3.00000e+00	4.547100e-04	7.023761e+01	3.693139e+01	2.396698e+06
5	5.626861e-04	2.916084e-04	2.170066e+05	2.773860e+05	
5	-2.50000e+00	6.353315e-04	6.246272e+01	3.591242e+01	3.212763e+06
6	6.676993e-04	3.411058e-04	1.583717e+05	2.163229e+05	
6	-2.00000e+00	7.405122e-04	5.791314e+01	3.525554e+01	3.784932e+06
7	7.257644e-04	3.665050e-04	1.309852e+05	1.926588e+05	
7	-1.50000e+00	7.572604e-04	5.541913e+01	3.487319e+01	4.048810e+06
8	7.405037e-04	3.703683e-04	1.190680e+05	1.894083e+05	
8	-1.00000e+00	7.669354e-04	5.323740e+01	3.452434e+01	4.277513e+06
9	7.506235e-04	3.725796e-04	1.098886e+05	1.875853e+05	
9	-5.00000e-01	7.752391e-04	5.124653e+01	3.419329e+01	4.497689e+06
	7.590347e-04	3.744656e-04	1.022302e+05	1.860515e+05	

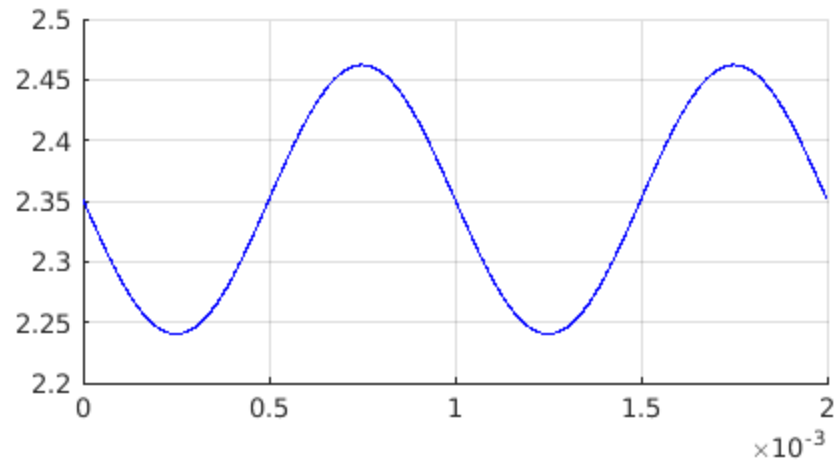
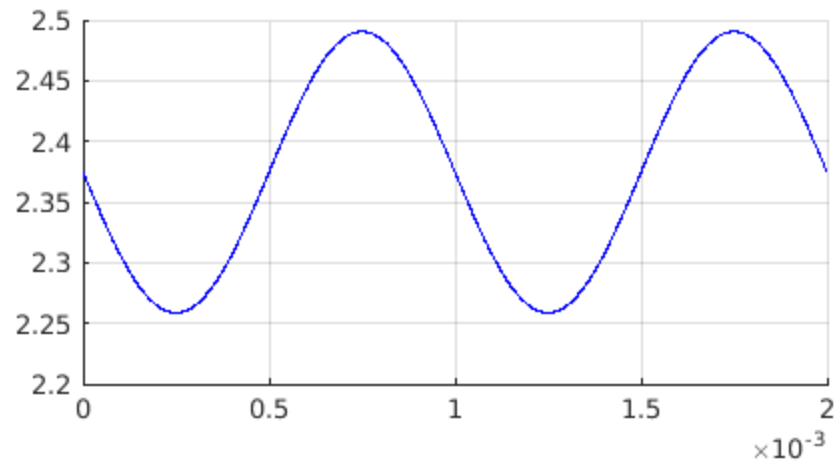
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	7.662185e-04	3.761616e-04	9.565915e+04	1.846886e+05	
11	5.000000e-01	7.896944e-04	4.766377e+01	3.356377e+01	4.930925e+06
	7.724354e-04	3.777235e-04	8.988962e+04	1.834469e+05	
12	1.000000e+00	7.962122e-04	4.600242e+01	3.325561e+01	5.149585e+06
	7.778460e-04	3.791819e-04	8.471235e+04	1.822989e+05	
13	1.500000e+00	8.023825e-04	4.438177e+01	3.294409e+01	5.374236e+06
	7.825525e-04	3.805568e-04	7.995818e+04	1.812266e+05	
14	2.000000e+00	8.082623e-04	4.275979e+01	3.262071e+01	5.610062e+06
	7.866128e-04	3.818618e-04	7.547212e+04	1.802178e+05	
15	2.500000e+00	8.138936e-04	4.107699e+01	3.227197e+01	5.868826e+06
	7.900404e-04	3.831069e-04	7.108454e+04	1.792632e+05	
16	3.000000e+00	8.193079e-04	3.923251e+01	3.187292e+01	6.172022e+06
	7.927870e-04	3.842998e-04	6.656053e+04	1.783559e+05	
17	3.500000e+00	8.245299e-04	3.701496e+01	3.136754e+01	6.564790e+06
	7.946772e-04	3.854463e-04	6.146744e+04	1.774904e+05	
18	4.000000e+00	8.295776e-04	3.381623e+01	3.058250e+01	7.193957e+06
	7.951190e-04	3.865509e-04	5.465628e+04	1.766626e+05	
19	4.500000e+00	8.344579e-04	2.586071e+01	2.825281e+01	9.342615e+06
	7.898892e-04	3.876154e-04	3.962895e+04	1.758704e+05	

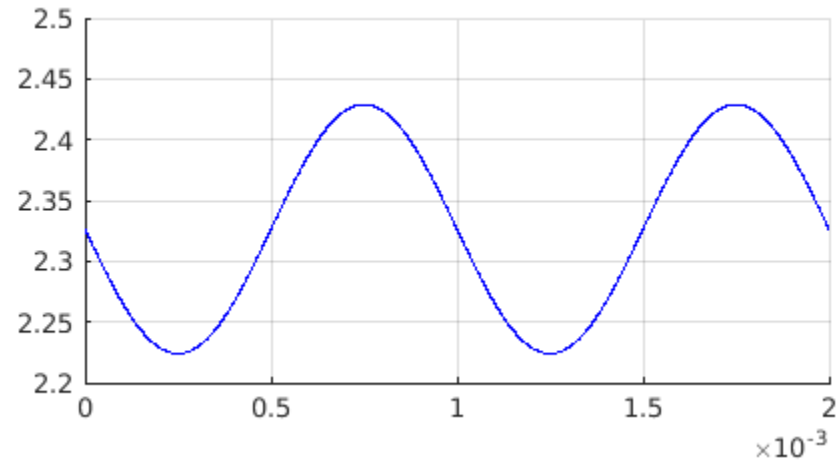
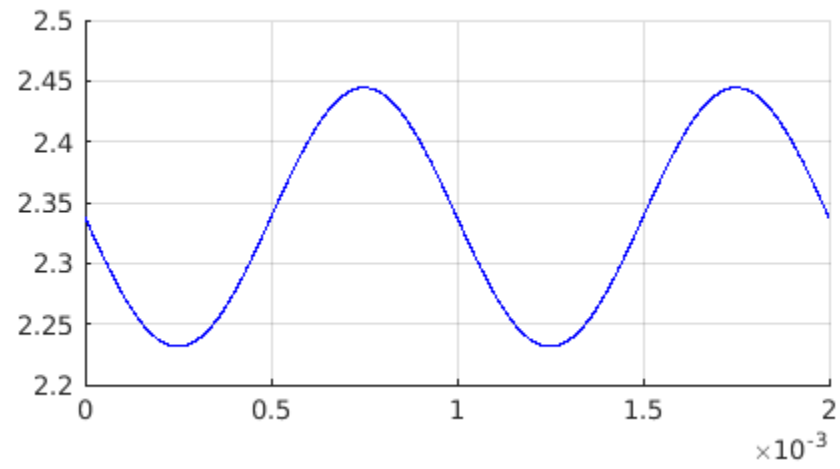
Here the plots I produced when running plot_tran.m in order (1 - 20)

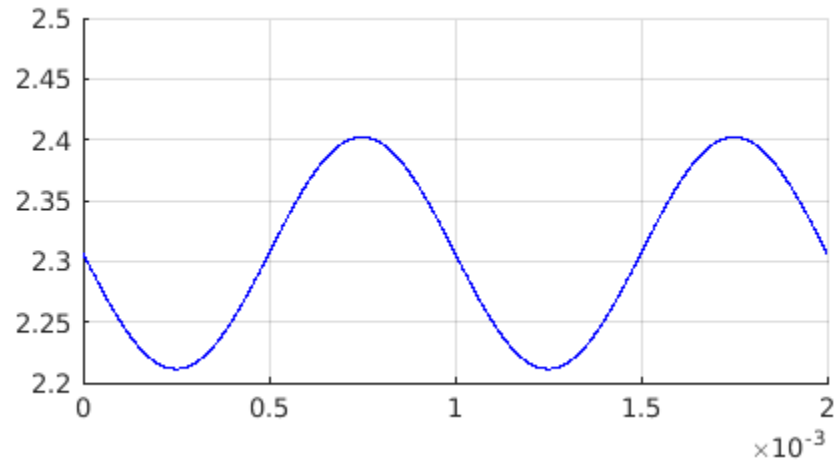
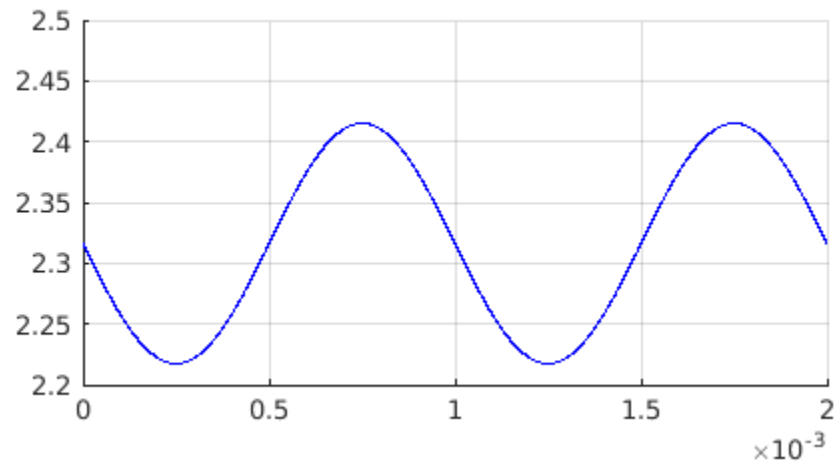


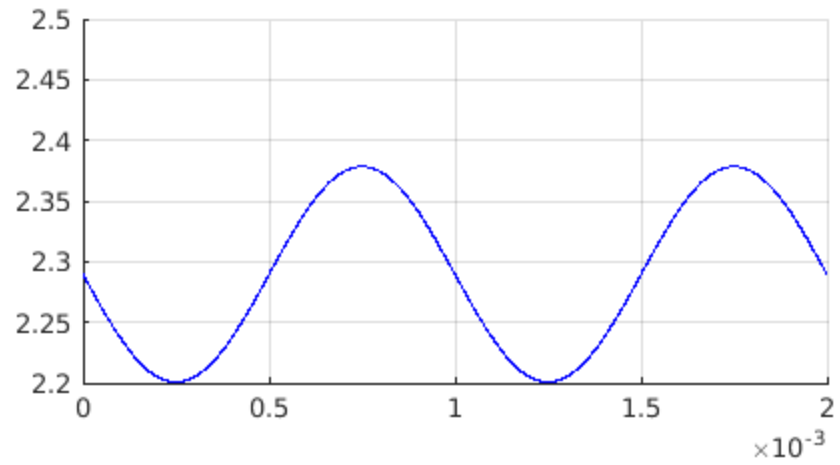
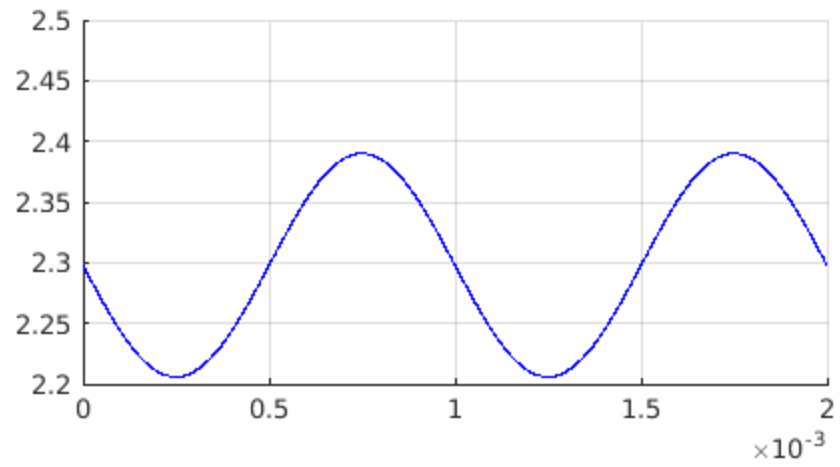


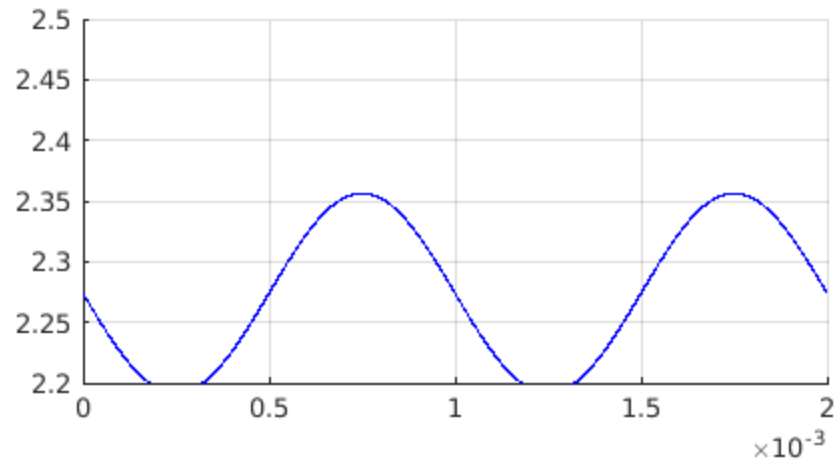
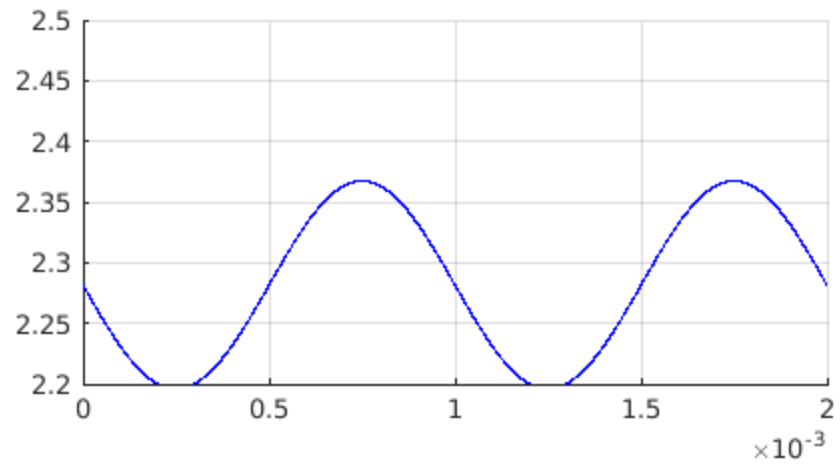


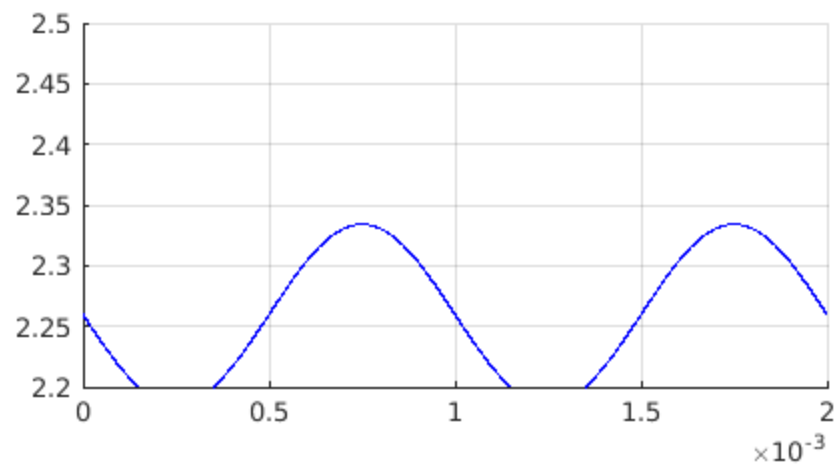
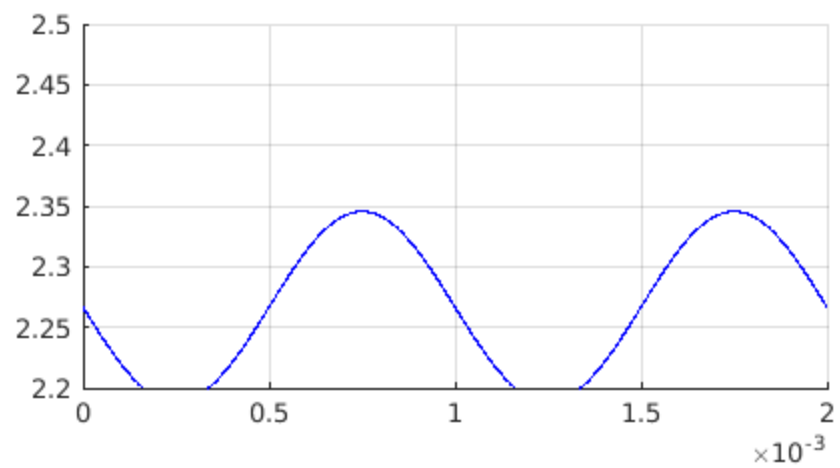


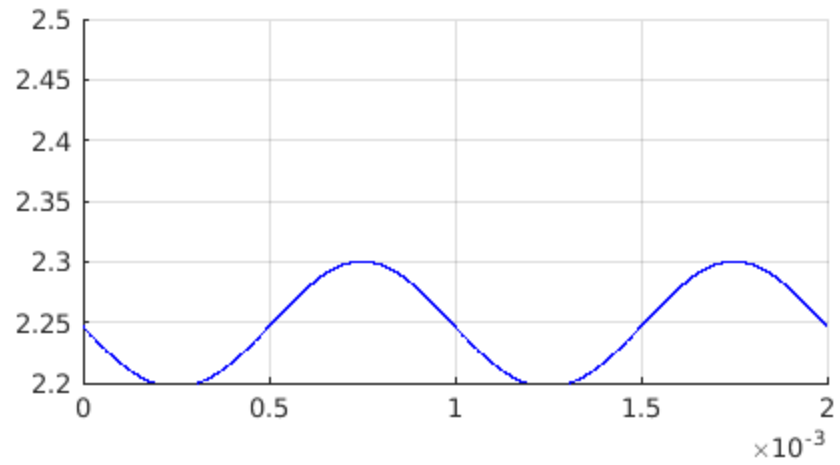
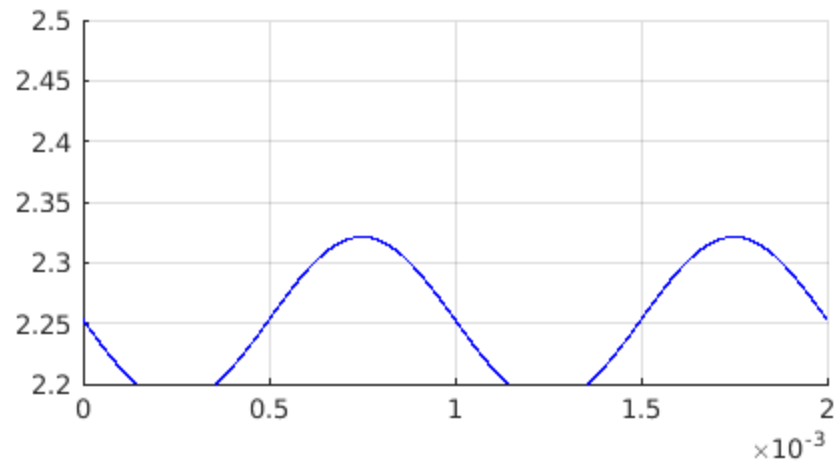


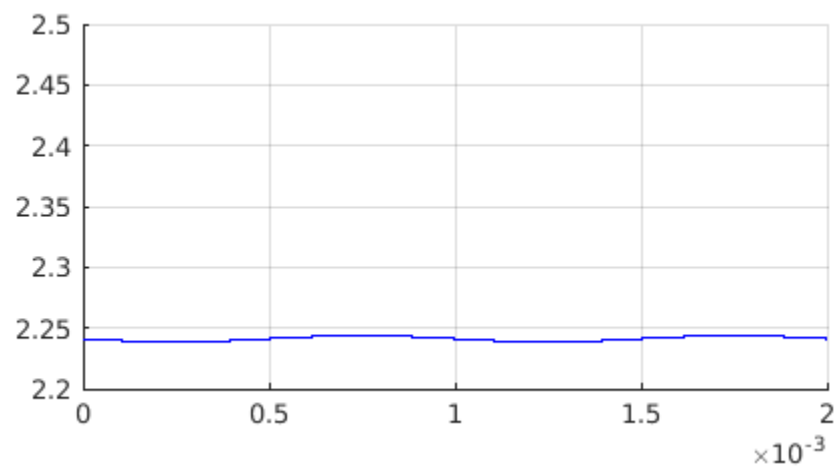




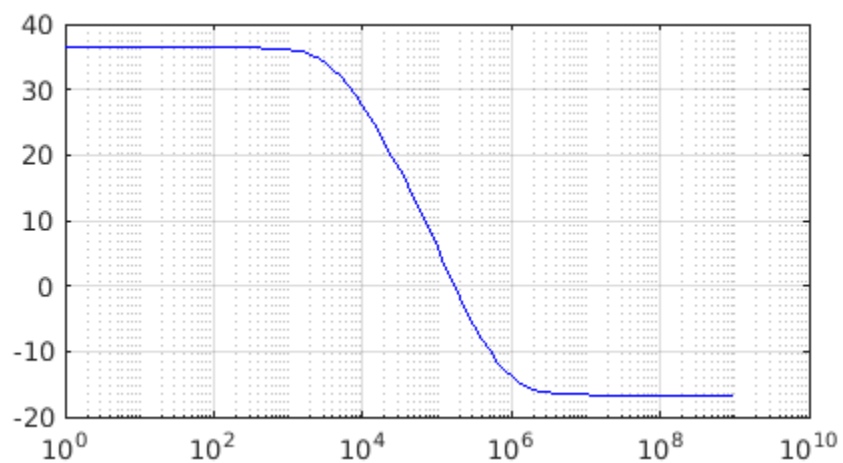


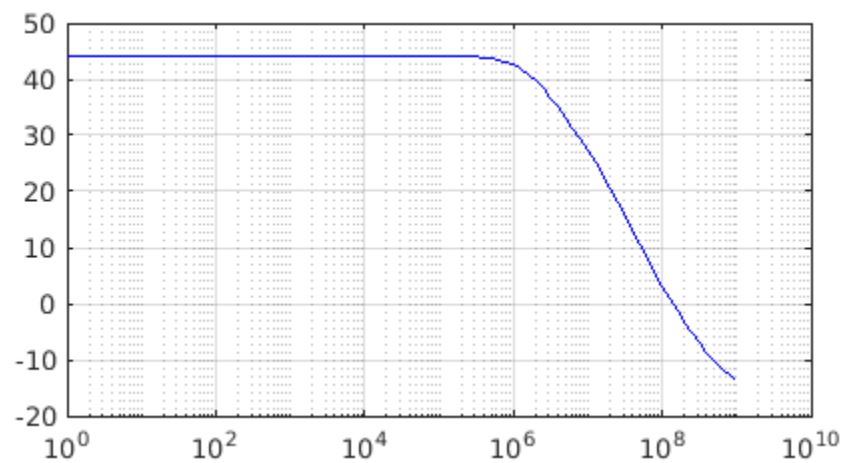
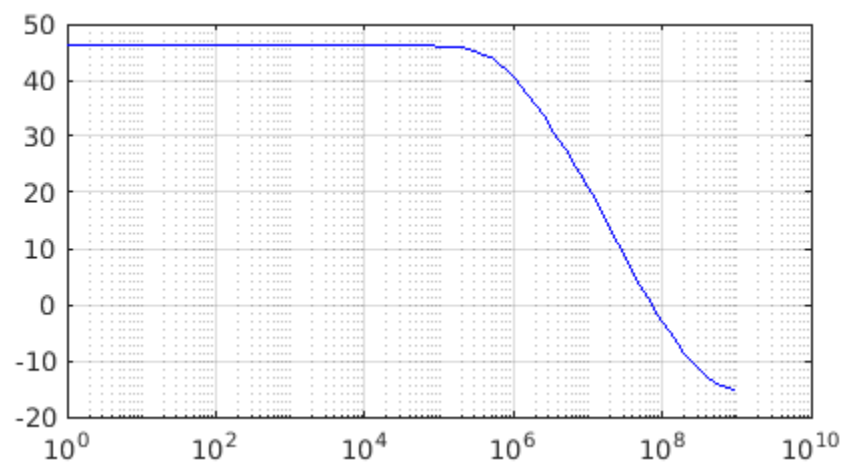


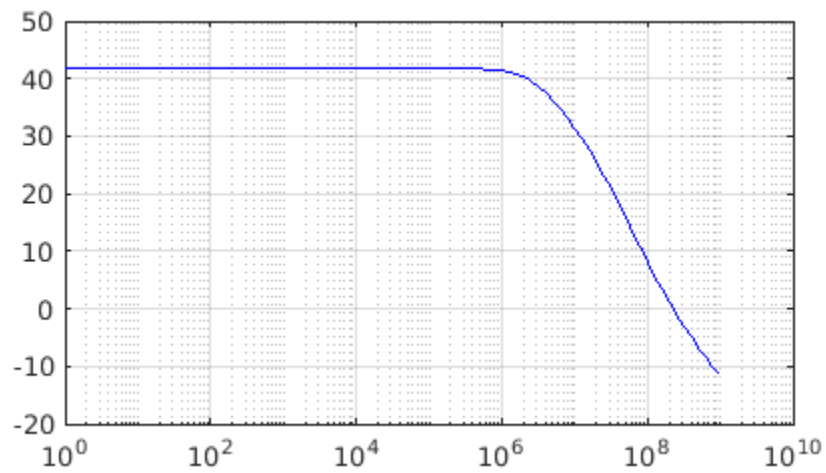
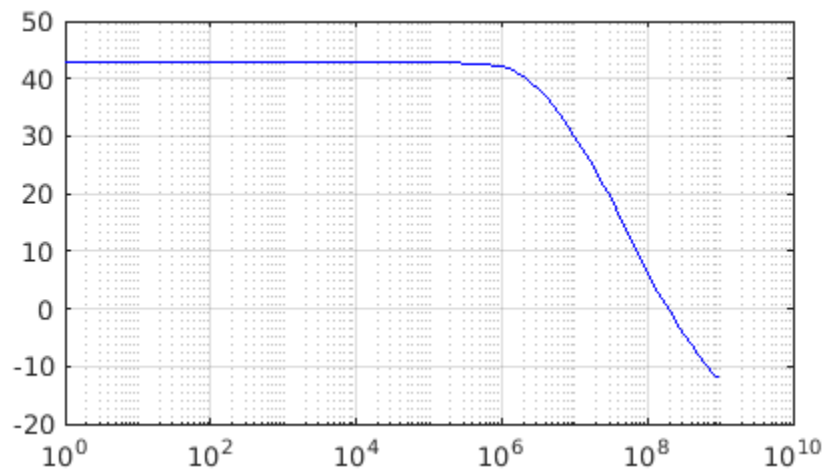


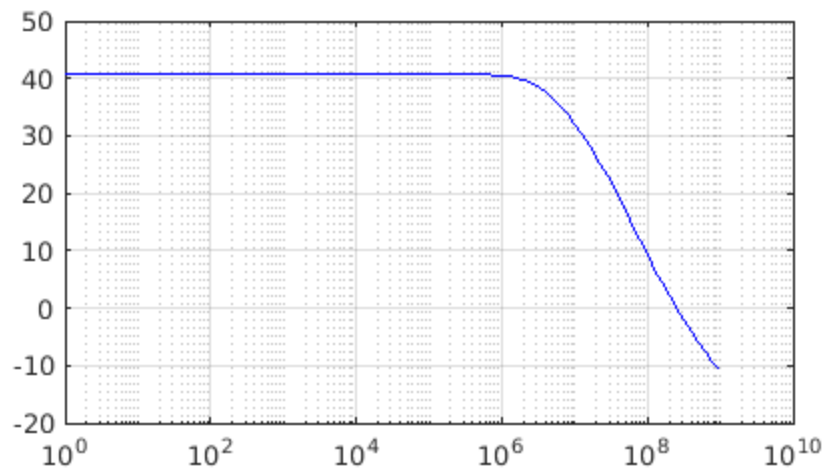
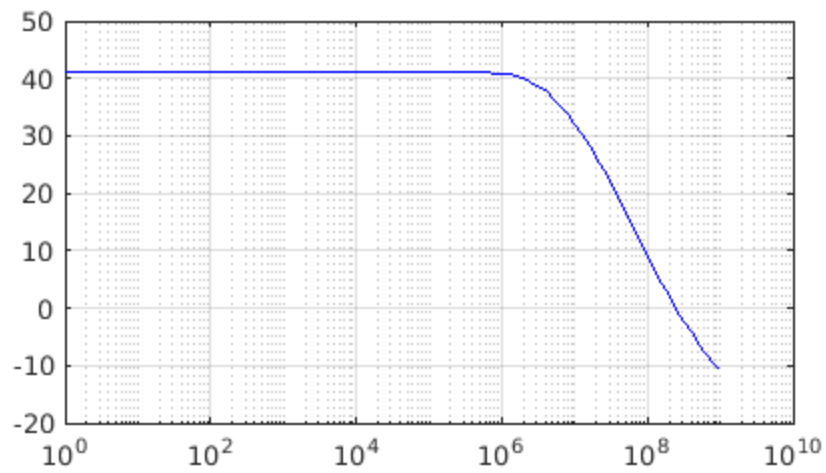


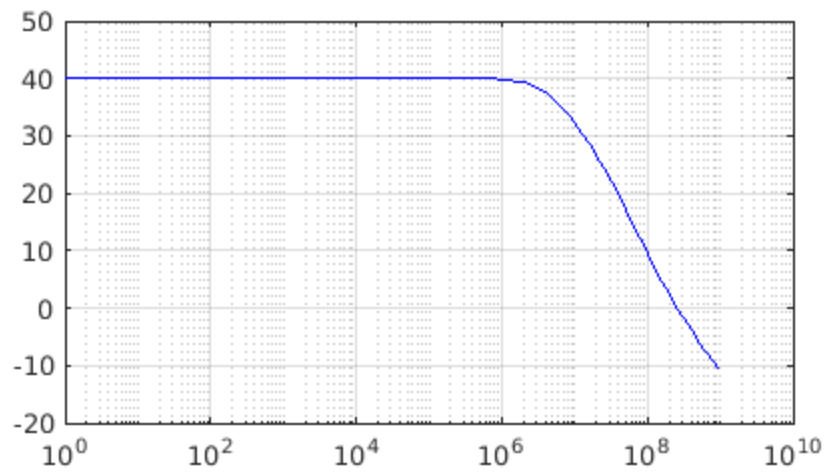
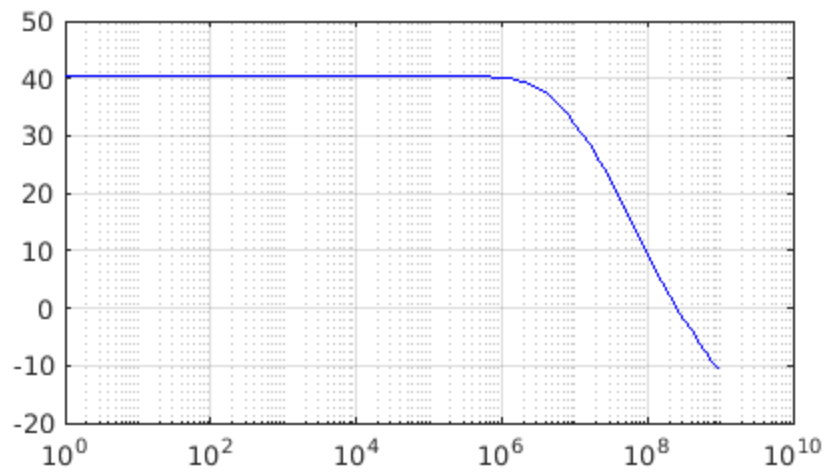
Here the plots I generated when running plot_ac.m in order (1 - 20)

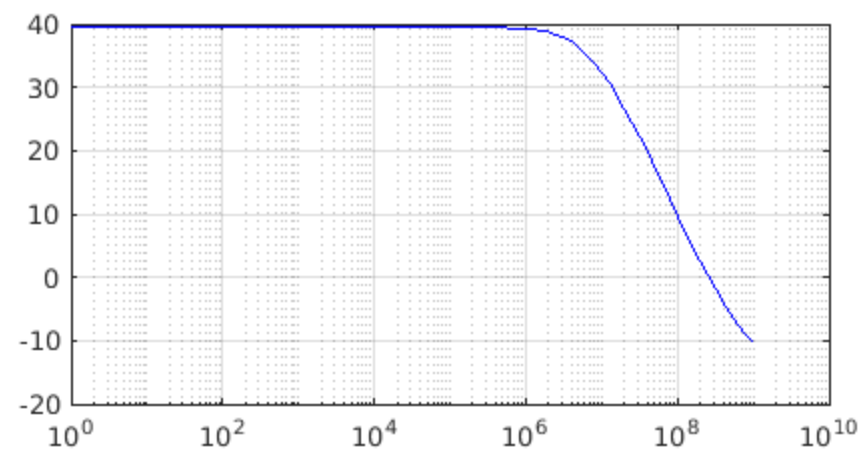
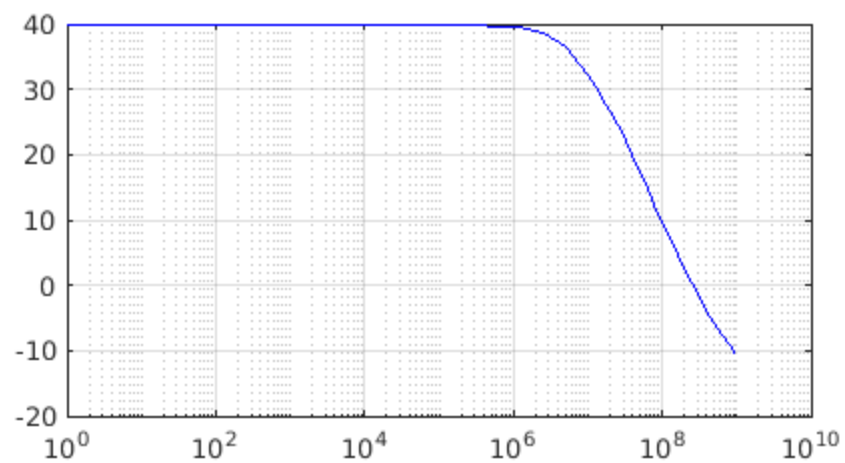


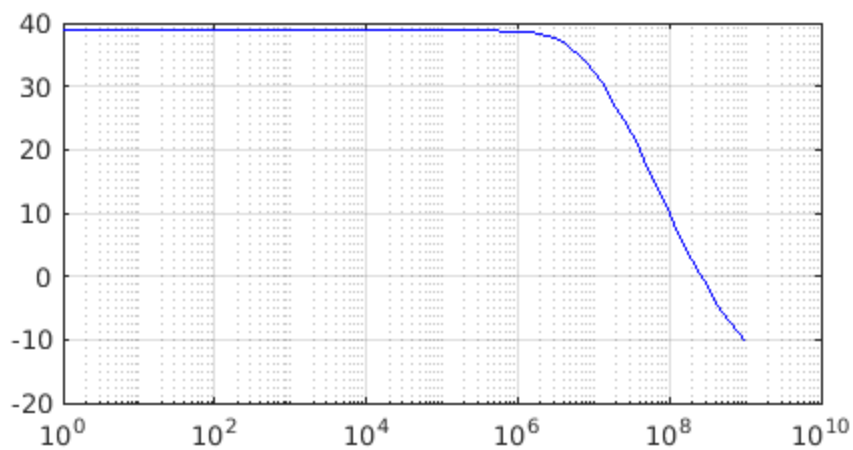
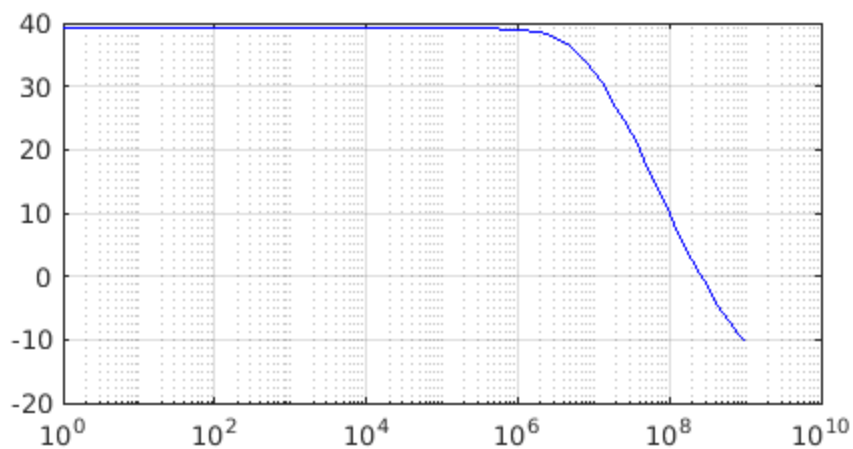


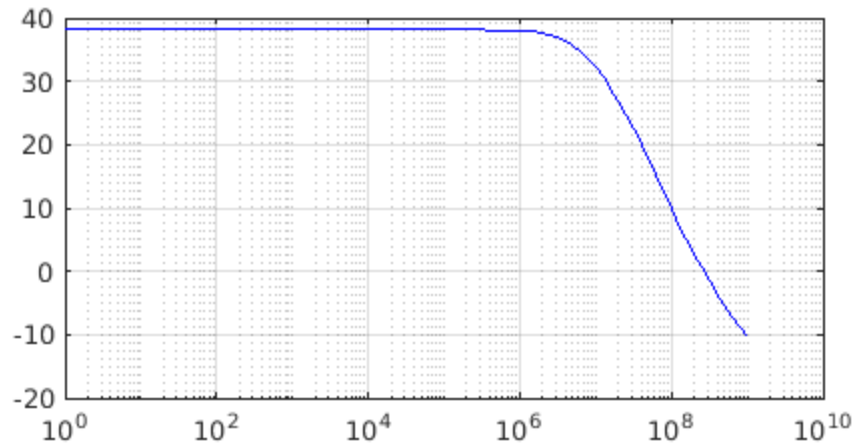
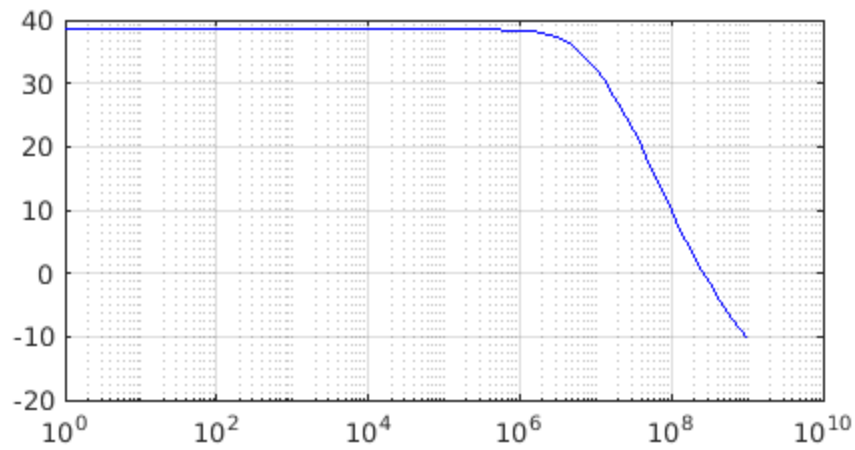


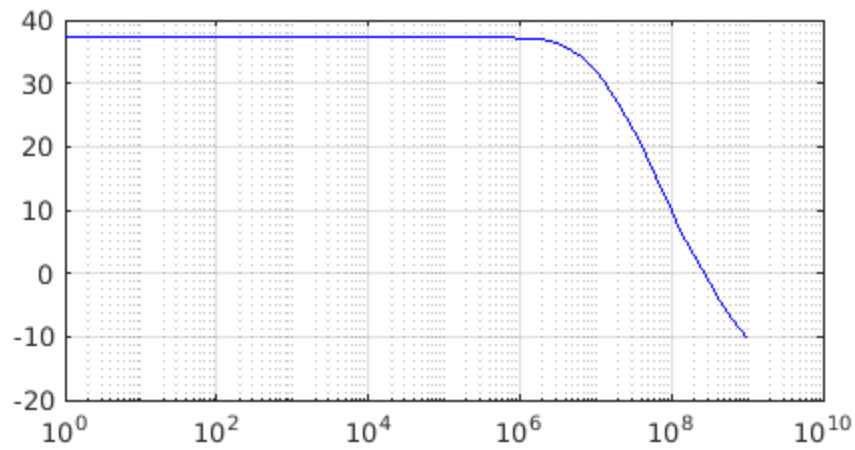
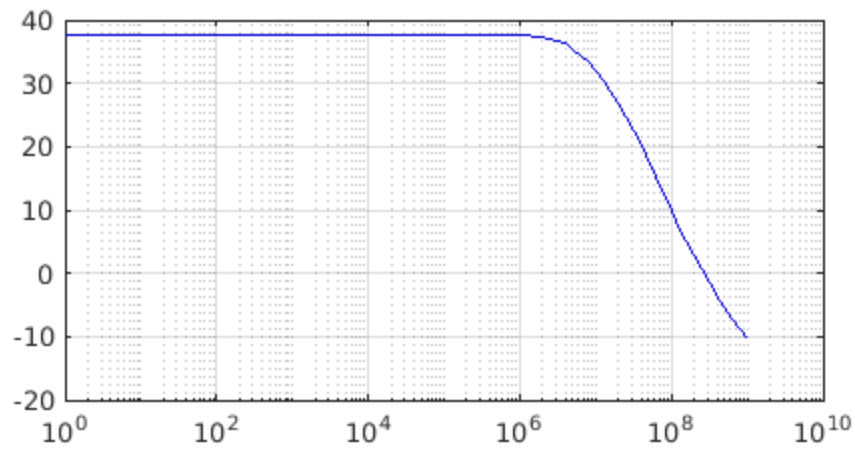


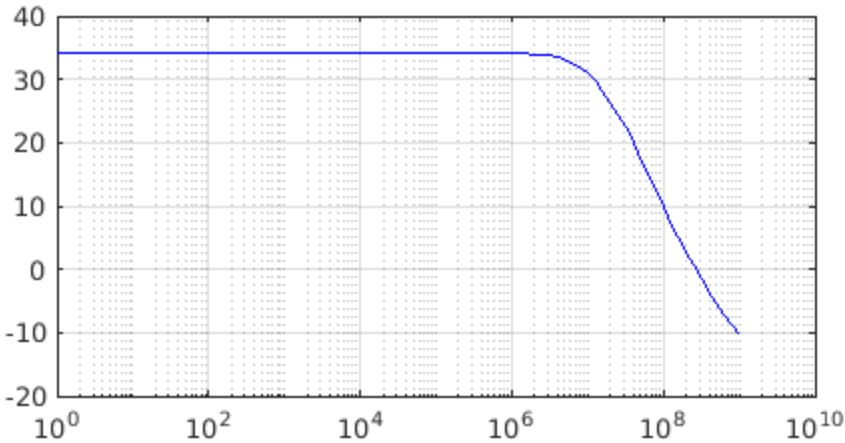
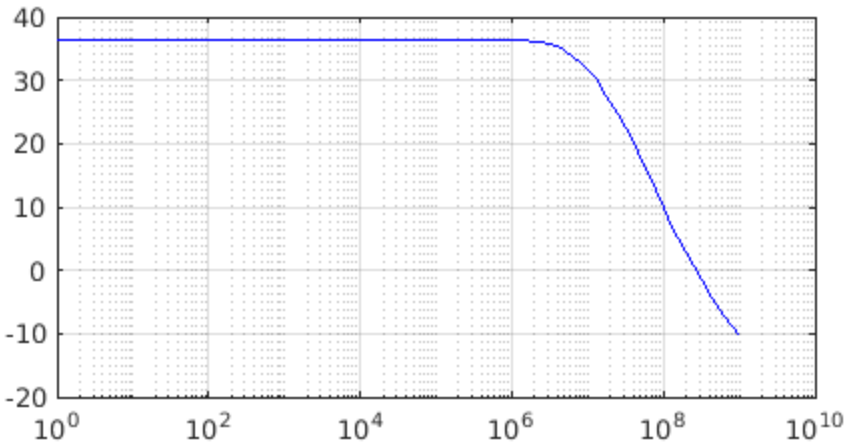


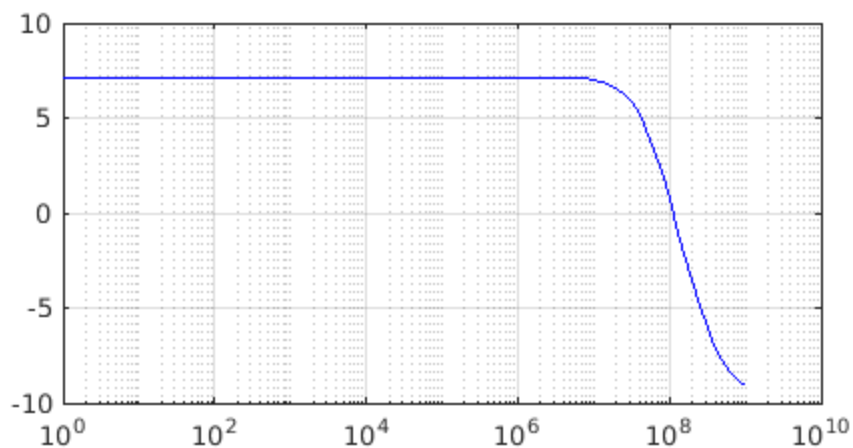




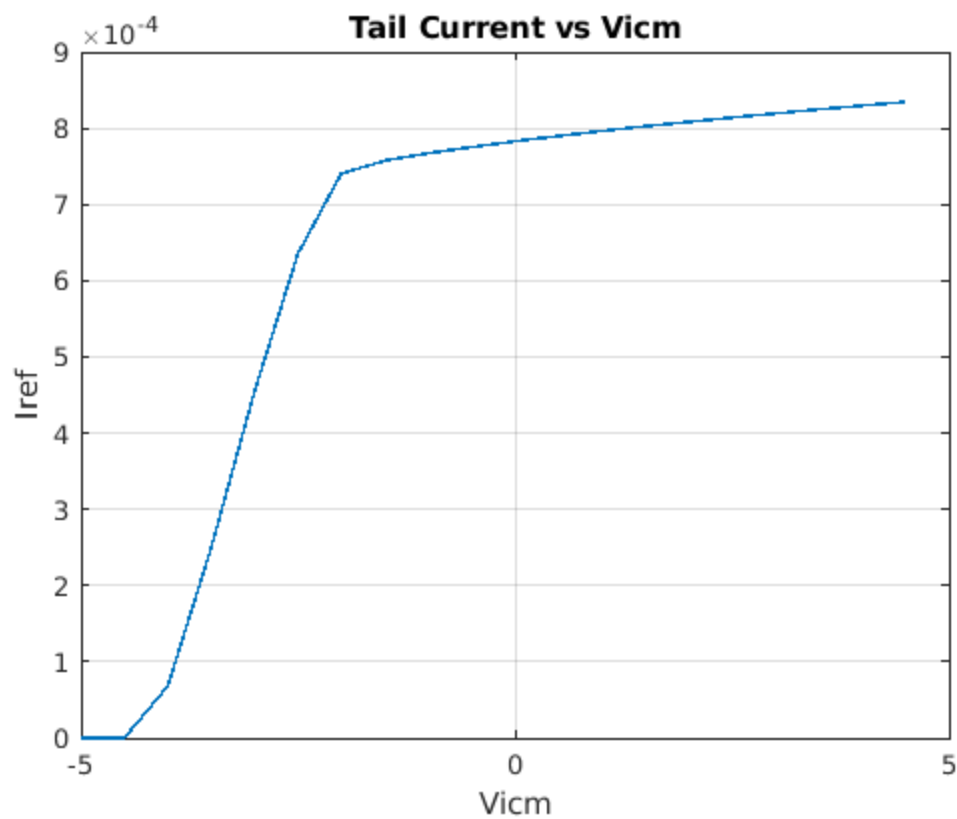


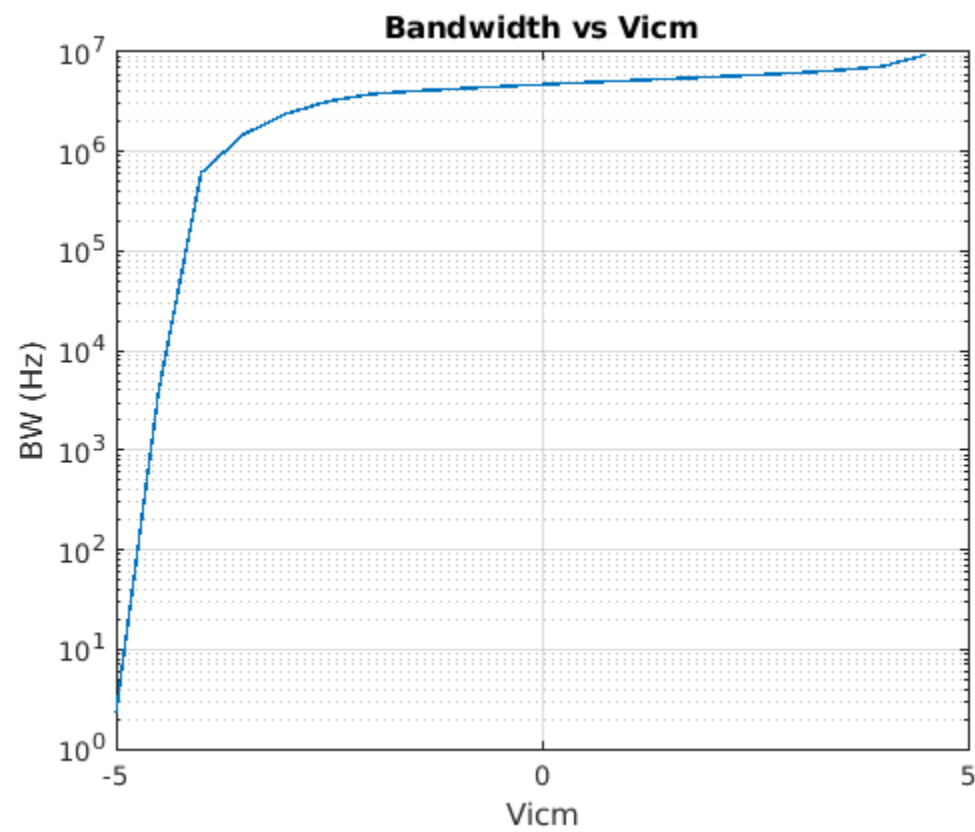


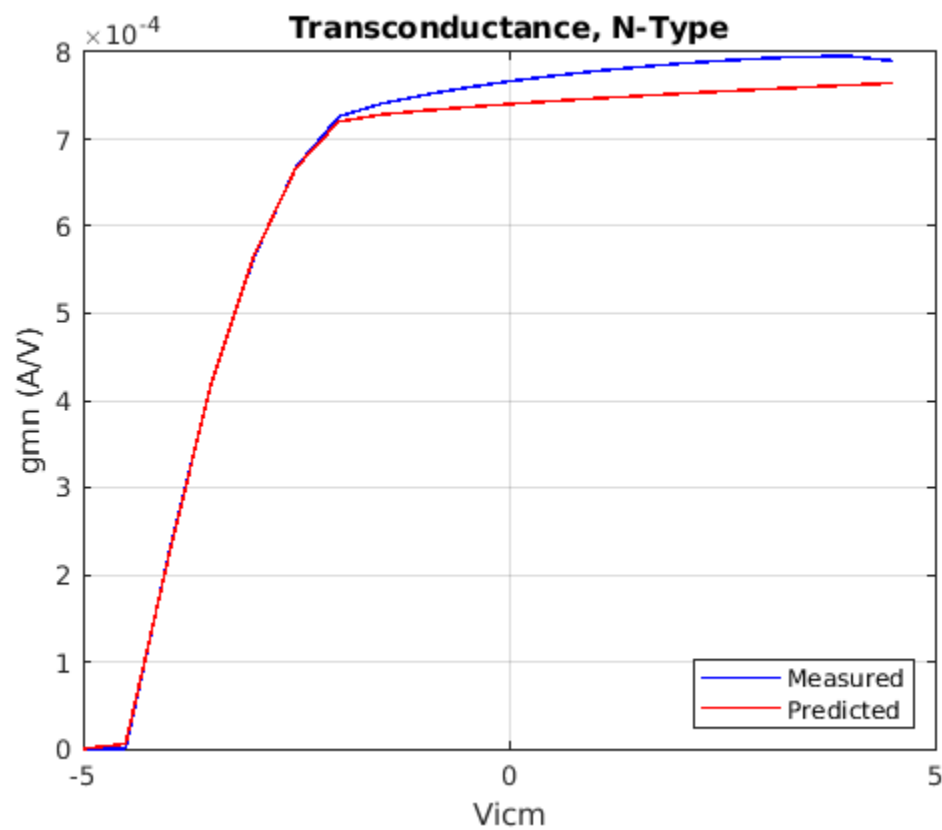


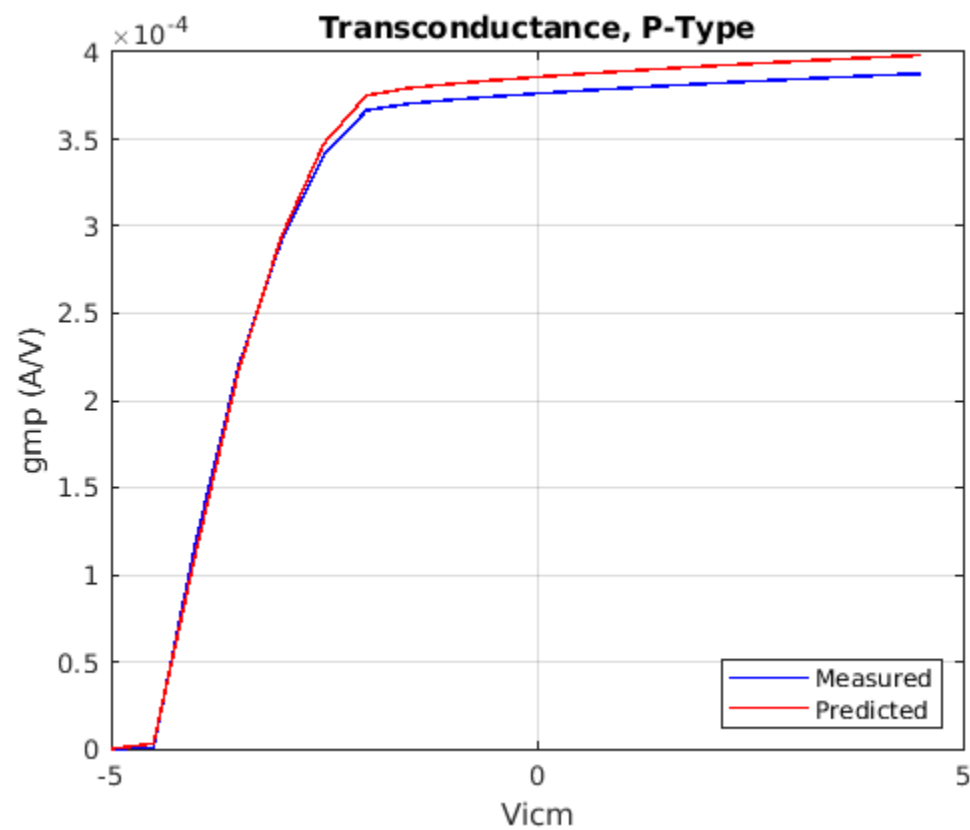


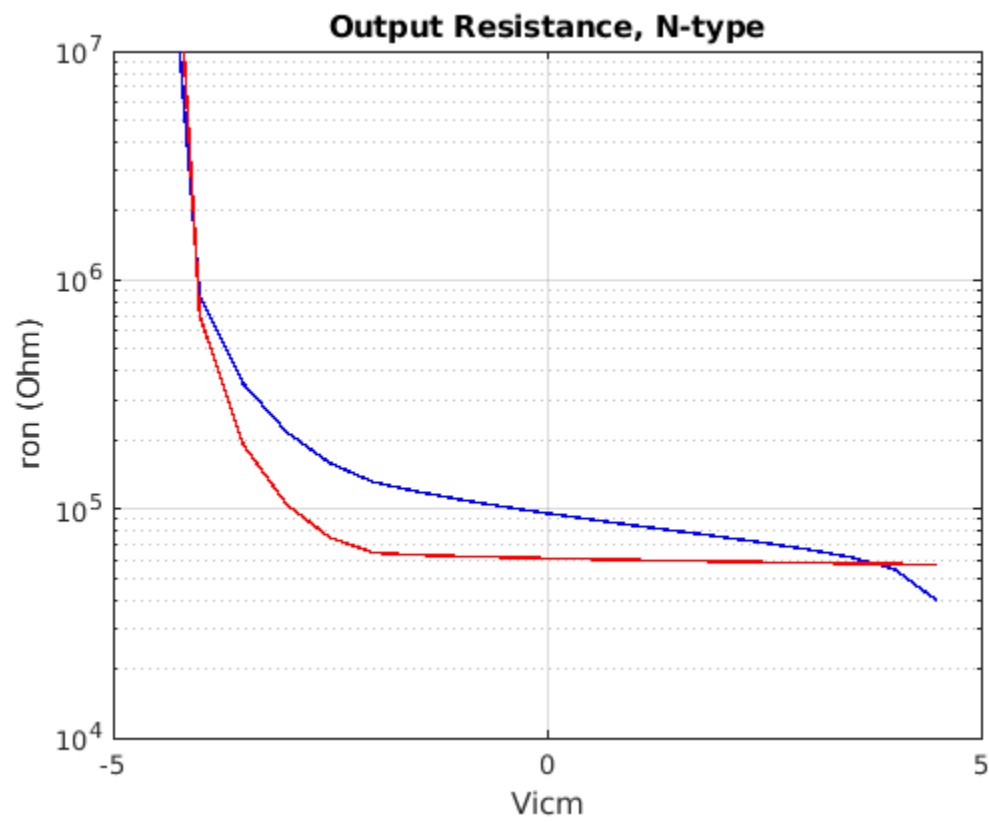
Here are the plots from plot_measurements.m in order of the figure numbers they popped up as

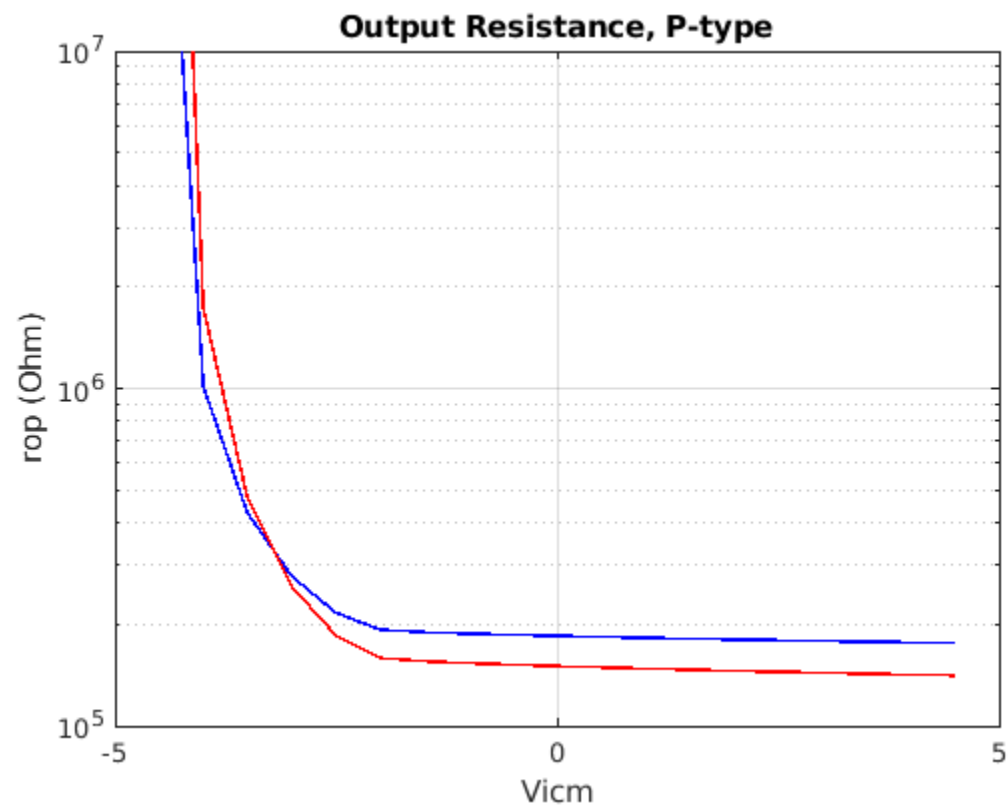


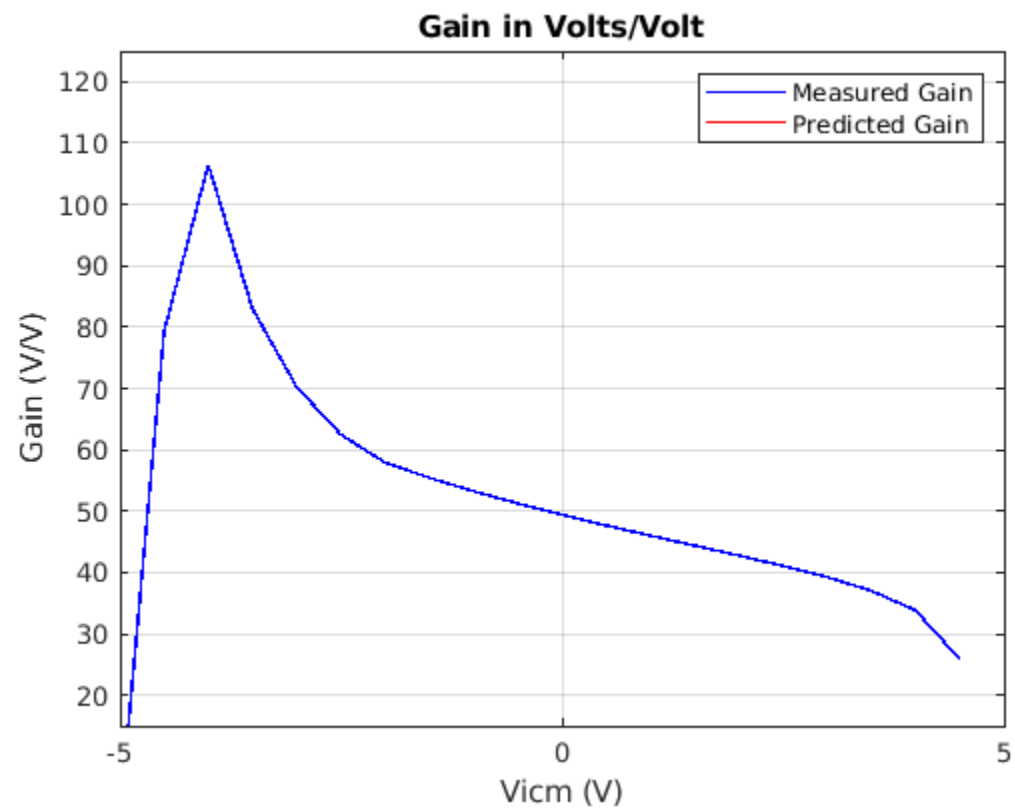


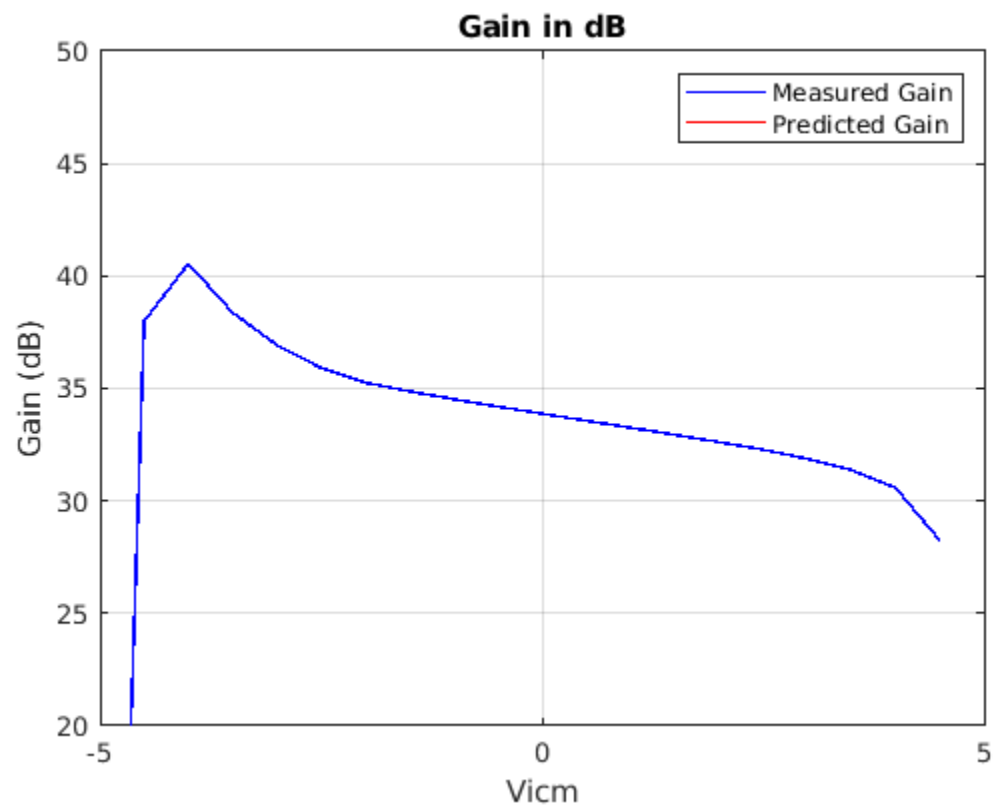


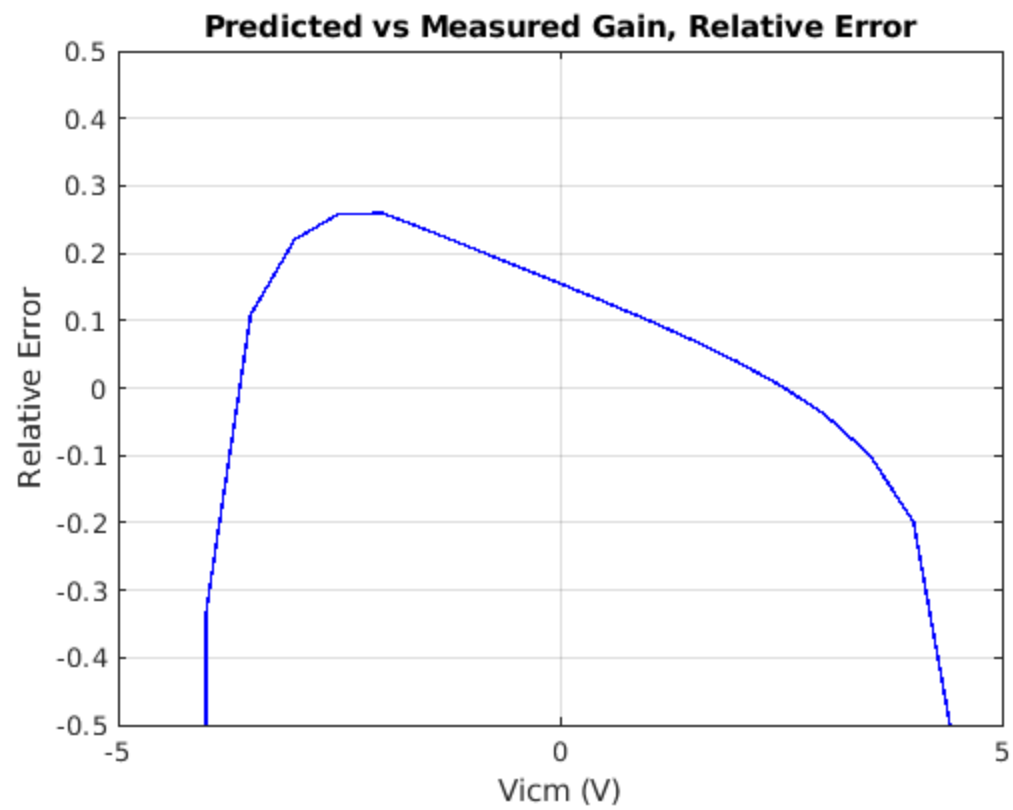


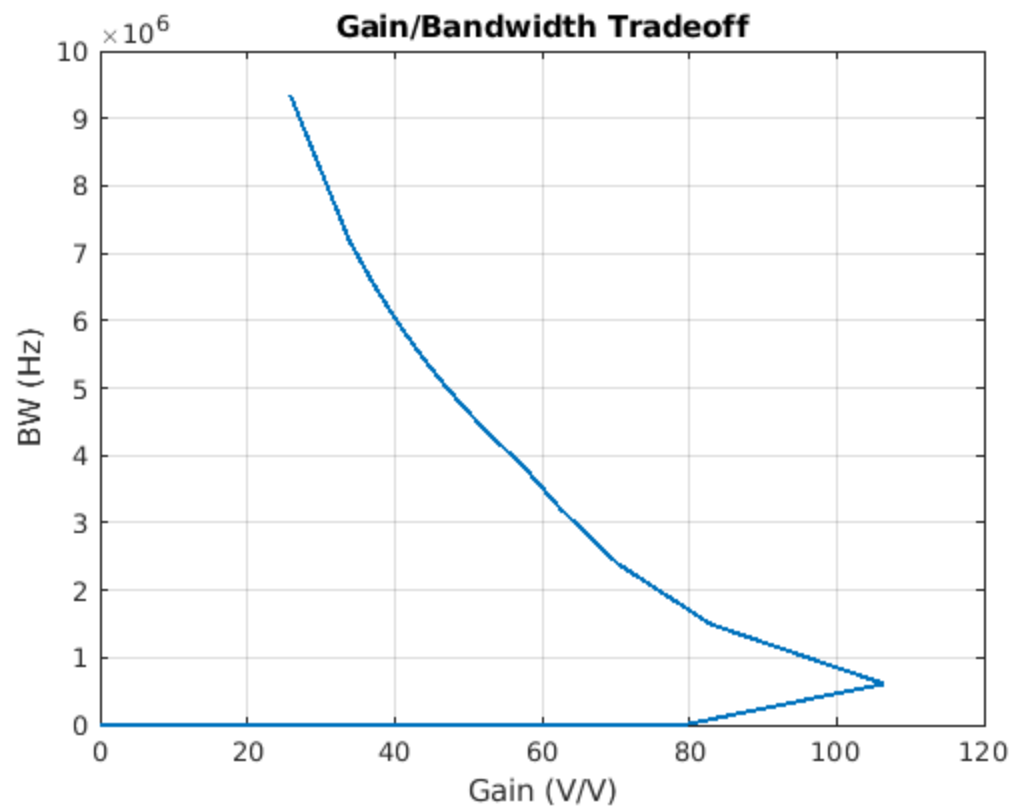


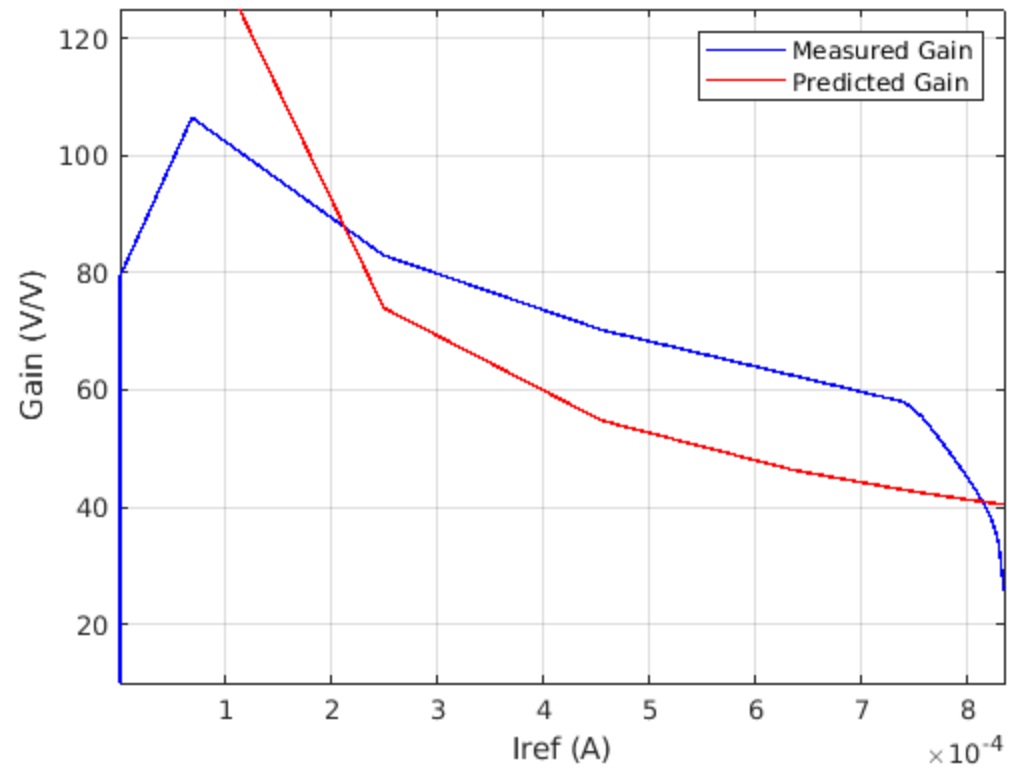


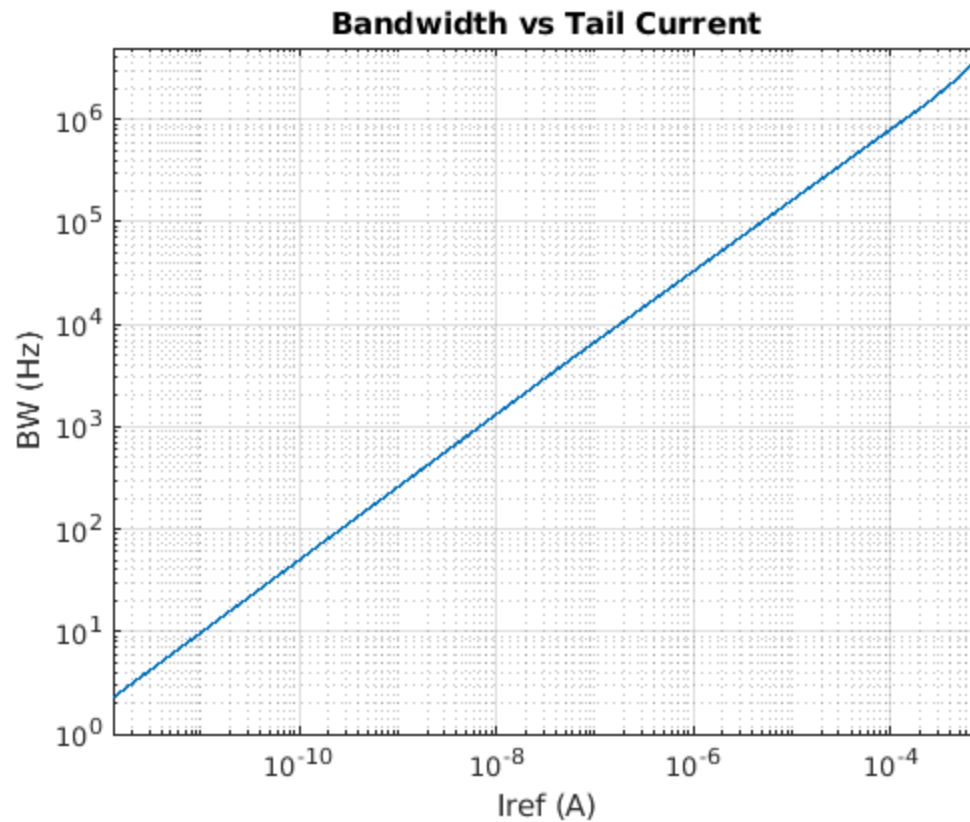












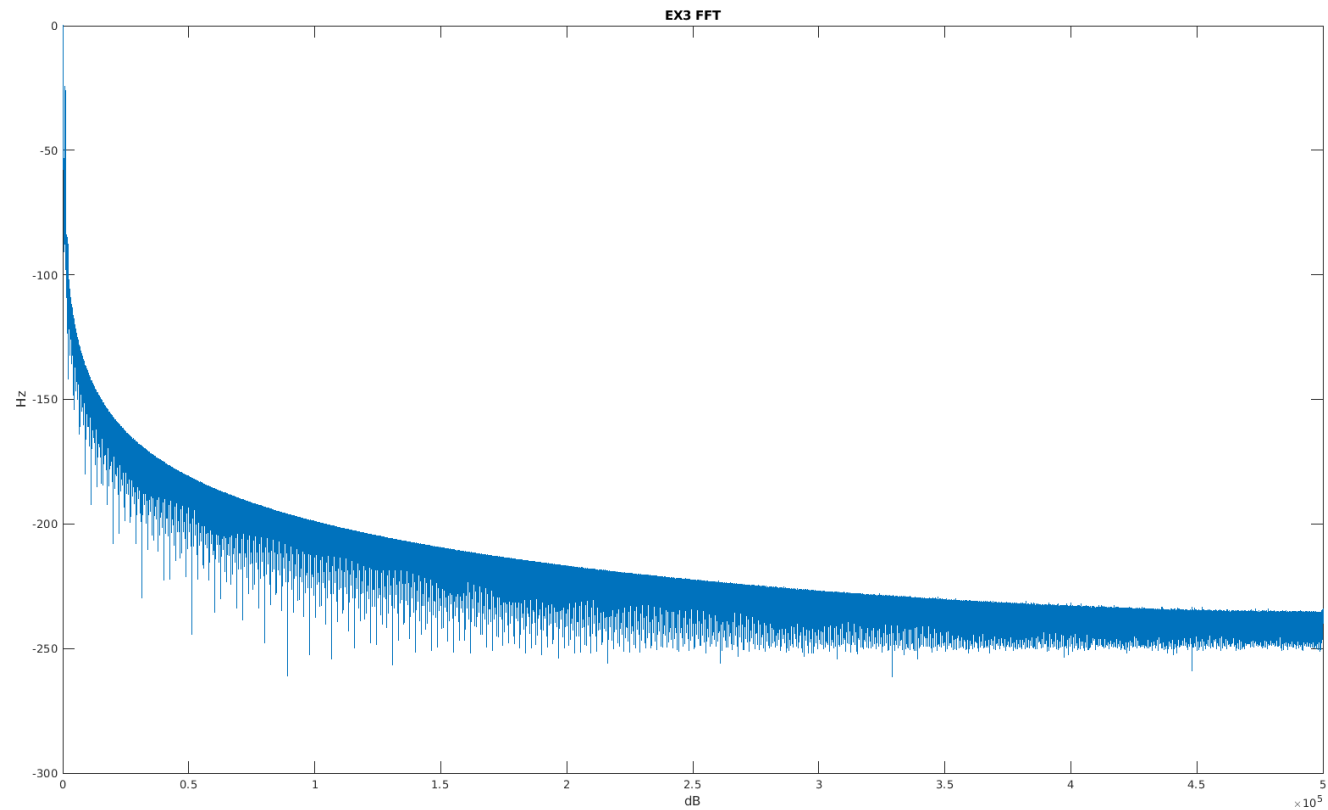
Conclusions

The accuracy of the predictions were fairly close to the simulated solutions, but there were obvious differences. For instance the transconductance and output resistances were fairly close; however the difference of the predictions vs the simulation gets quite exaggerated when using the resistance and transconductance in calculations like Gain/Current.

The trade of between Bandwidth and Gain is that after about .75 MHz the gain is slowing getting lower. So using this circuit for high frequency systems would be not as useful as using them for low frequency systems.

3

Here is the plot for the FFT

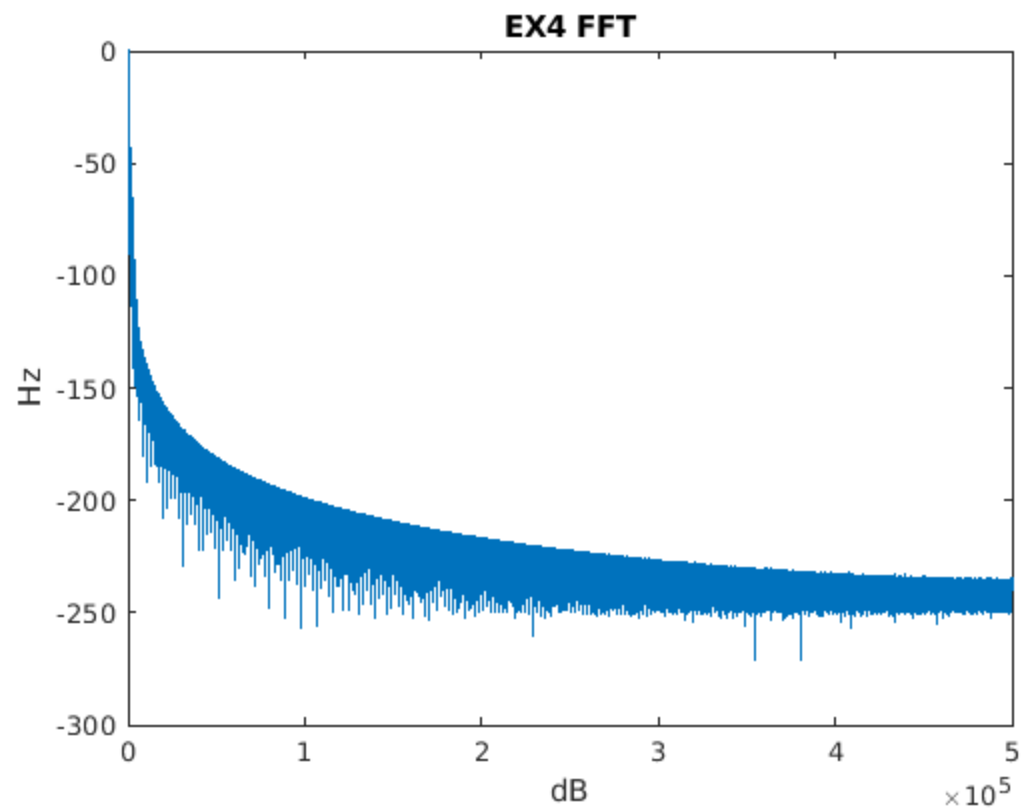


and the calculated SNR is -62.3347

```
data = importdata("fft.dat"); plot(data(:,1),data(:,2)); title("EX3 FFT") ylabel('Hz') xlabel('dB') axis([0, 500000, -300, 0]) fftsnr = snr(data(:,2),data(:,1))
```

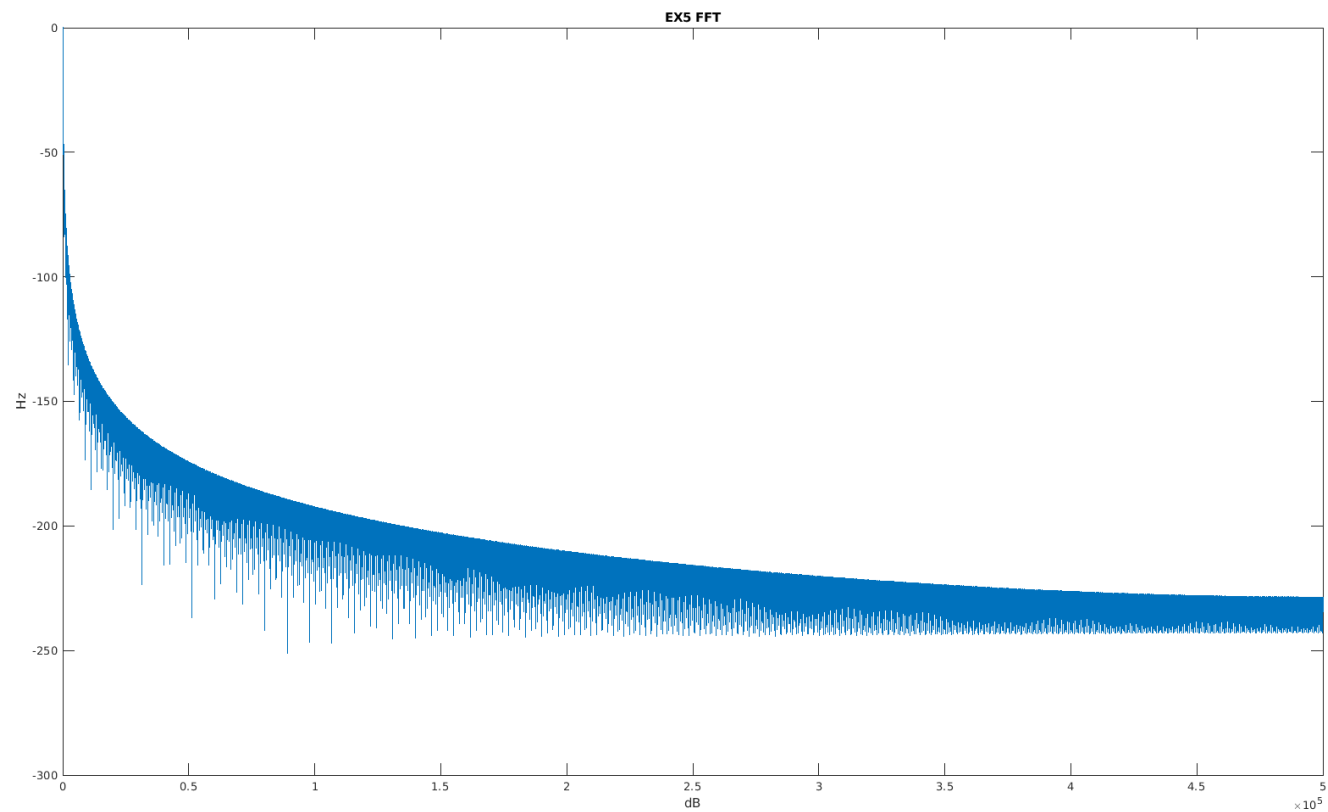
4

Changed Vin to 10mV in ex3.sp. Below is the float, and the SNR is -62.3353



5

Below is the fft analysis and the SNR is -62.5993



6

Calculating A_{v0} and g_m

```
In [ ]: from math import sqrt
```

```
Kp = 0.19  
Vthp = -0.74  
Vdd = 5 # v  
Vg = 4  
Vgs = Vg - Vdd
```

```

Vov = Vgs - Vthp
ID = 1/2 * Kp * Vov**2

gm = sqrt(2 * ID * Kp)
av = -gm * R

print(gm)
print(av)

```

```

0.049400000000000006
-494.00000000000006

```

```
gm = 0.0494 Av0 = -494
```

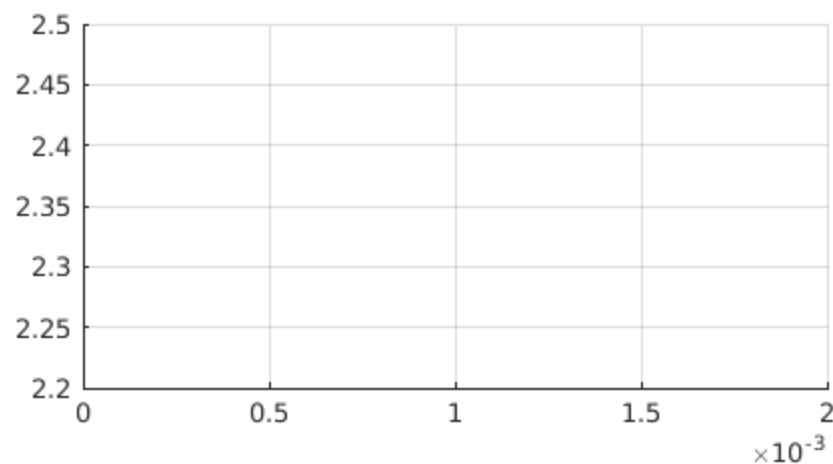
7

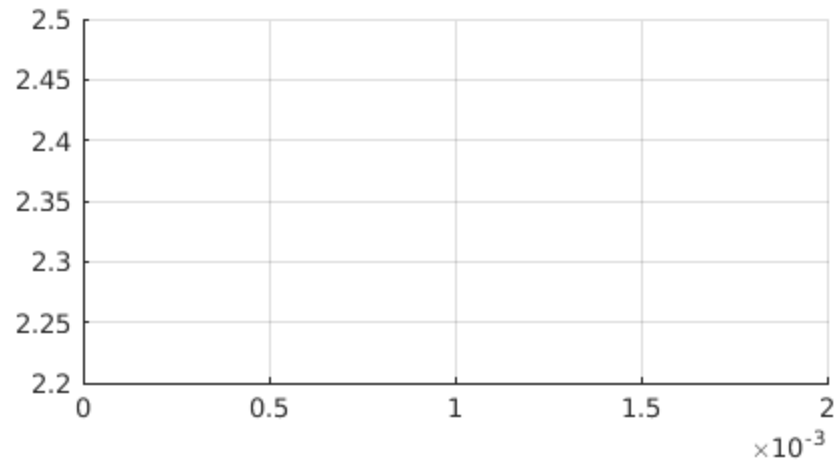
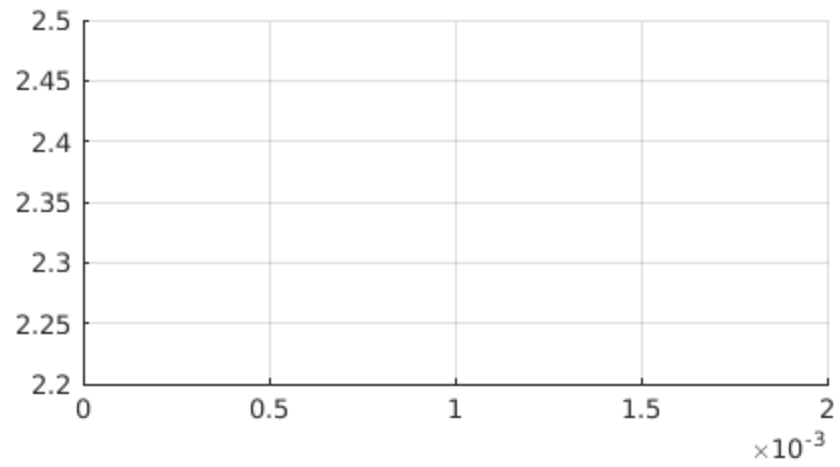
ex2.sp with opamp.sp:

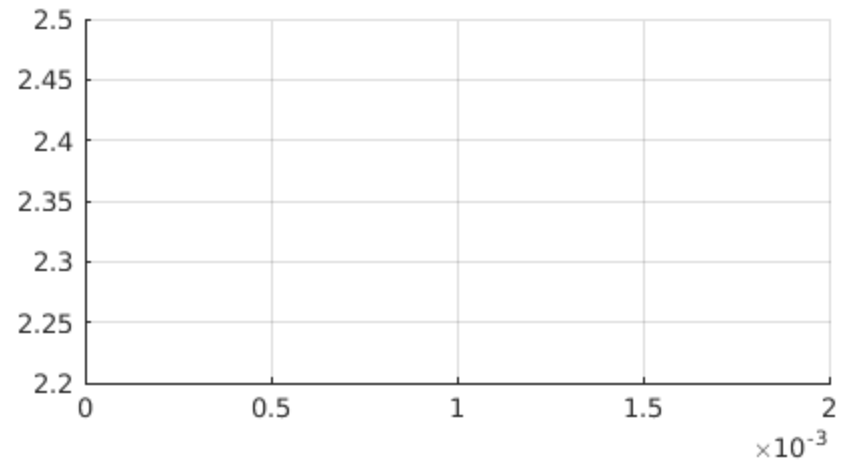
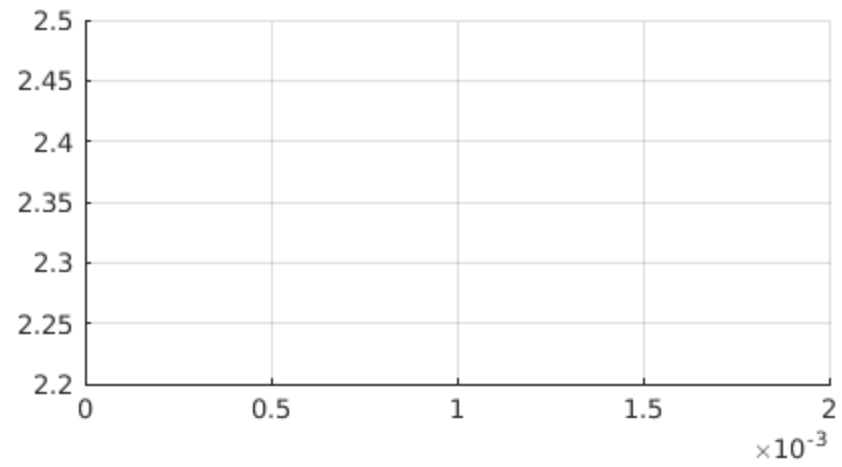
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1	1.359389e-11	2.427459e-10	5.888254e+12	2.183838e+11	0.000000e+00
1	-4.50000e+00	4.562162e-08	2.239358e-01	-1.29975e+01	0.000000e+00
2	4.802516e-07	5.563758e-07	1.735504e+08	1.161814e+08	0.000000e+00
2	-4.00000e+00	6.795952e-05	1.735734e-03	-5.52103e+01	0.000000e+00
3	2.204869e-04	1.200720e-04	8.519460e+05	1.011311e+06	0.000000e+00
3	-3.50000e+00	2.491448e-04	5.259033e-04	-6.55819e+01	0.000000e+00
4	4.165233e-04	2.200303e-04	3.530310e+05	4.271133e+05	0.000000e+00
4	-3.00000e+00	4.547100e-04	5.926116e-04	-6.45446e+01	0.000000e+00
5	5.626861e-04	2.916084e-04	2.170066e+05	2.773860e+05	0.000000e+00
5	-2.50000e+00	6.353315e-04	9.510242e-04	-6.04362e+01	0.000000e+00
6	6.676993e-04	3.411058e-04	1.583717e+05	2.163229e+05	0.000000e+00
6	-2.00000e+00	7.405122e-04	2.248149e-04	-7.29635e+01	0.000000e+00
7	7.257644e-04	3.665050e-04	1.309852e+05	1.926588e+05	0.000000e+00
7	-1.50000e+00	7.572604e-04	2.131827e-04	-7.34250e+01	0.000000e+00
8	7.405037e-04	3.703683e-04	1.190680e+05	1.894083e+05	0.000000e+00
8	-1.00000e+00	7.669354e-04	2.038254e-04	-7.38148e+01	0.000000e+00
9	7.506235e-04	3.725796e-04	1.098886e+05	1.875853e+05	0.000000e+00
9	-5.00000e-01	7.752391e-04	1.962282e-04	-7.41448e+01	0.000000e+00
10	7.590347e-04	3.744656e-04	1.022302e+05	1.860515e+05	0.000000e+00
10	0.000000e+00	7.827466e-04	1.871757e-04	-7.45550e+01	0.000000e+00

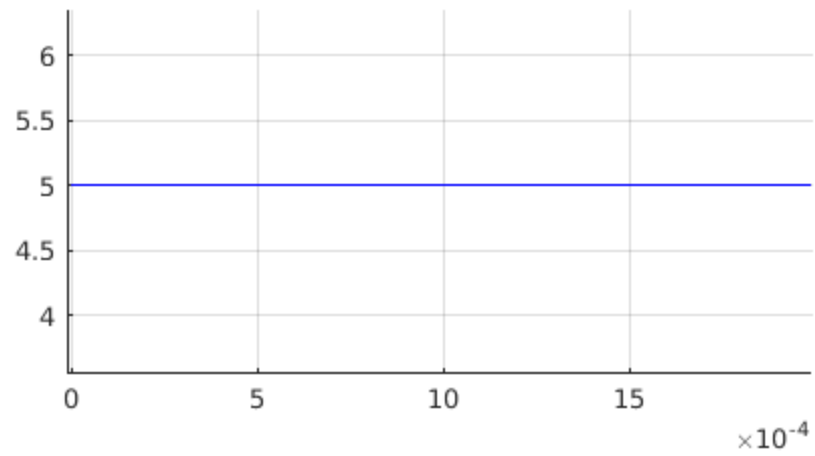
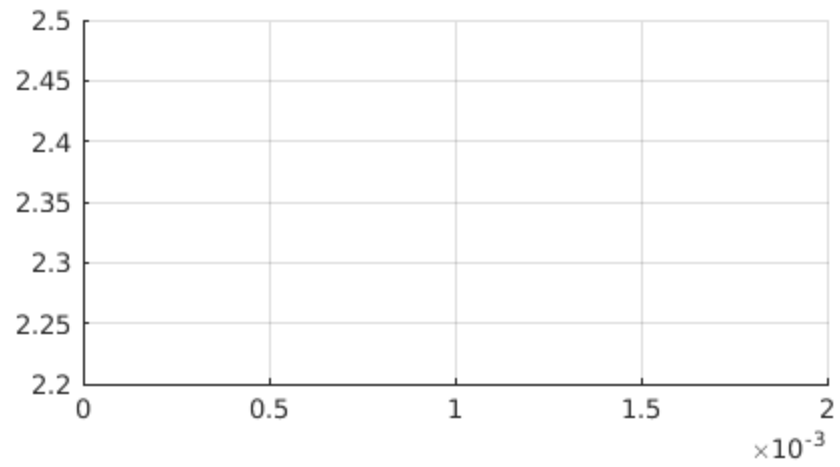
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11	5.000000e-01	7.896944e-04	1.799763e-04	-7.48957e+01
7.724354e-04	3.777235e-04	8.988962e+04	1.834469e+05	
12	1.000000e+00	7.962122e-04	1.732769e-04	-7.52252e+01
7.778460e-04	3.791819e-04	8.471235e+04	1.822989e+05	
13	1.500000e+00	8.023825e-04	1.666835e-04	-7.55622e+01
7.825525e-04	3.805568e-04	7.995818e+04	1.812266e+05	
14	2.000000e+00	8.082623e-04	1.601143e-04	-7.59114e+01
7.866128e-04	3.818618e-04	7.547212e+04	1.802178e+05	
15	2.500000e+00	8.138936e-04	1.533663e-04	-7.62854e+01
7.900404e-04	3.831069e-04	7.108454e+04	1.792632e+05	
16	3.000000e+00	8.193079e-04	1.460529e-04	-7.67098e+01
7.927870e-04	3.842998e-04	6.656053e+04	1.783559e+05	
17	3.500000e+00	8.245299e-04	1.379676e-04	-7.72045e+01
7.946772e-04	3.854463e-04	6.146744e+04	1.774904e+05	
18	4.000000e+00	8.295776e-04	1.259132e-04	-7.79986e+01
7.951190e-04	3.865509e-04	5.465628e+04	1.766626e+05	
19	4.500000e+00	8.344579e-04	9.580314e-05	-8.03724e+01
7.898892e-04	3.876154e-04	3.962895e+04	1.758704e+05	

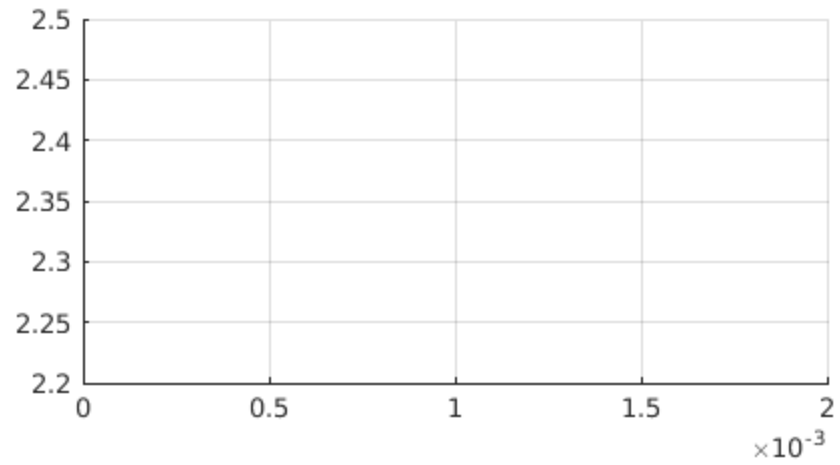
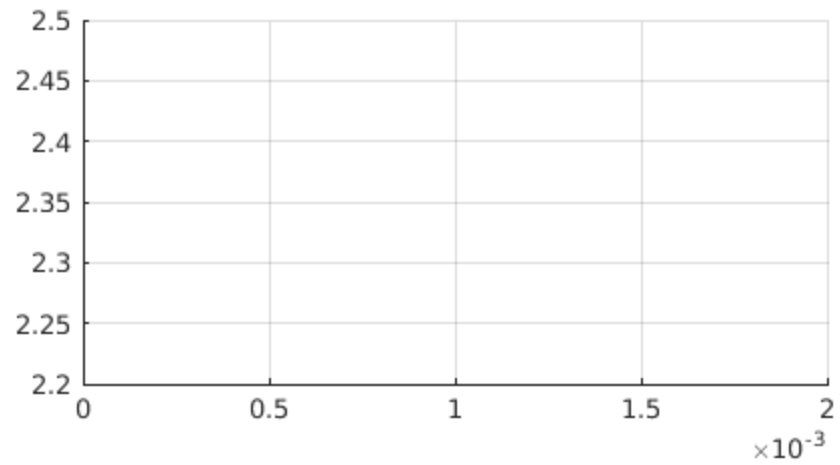
Transient plots in order of their figure numbers

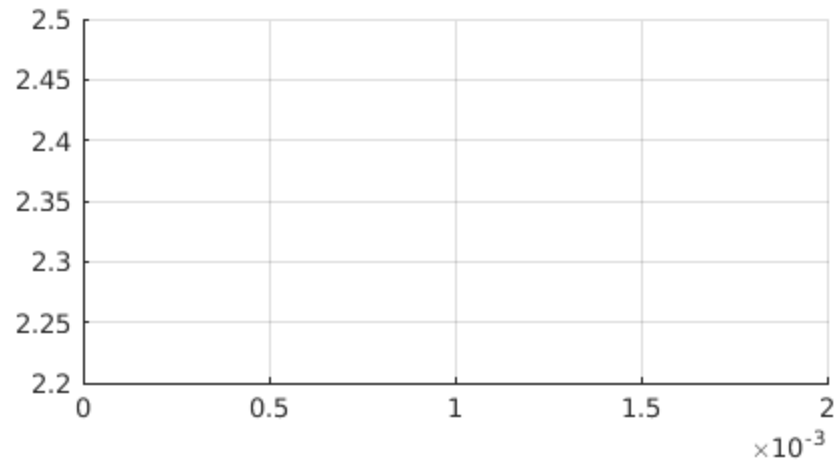
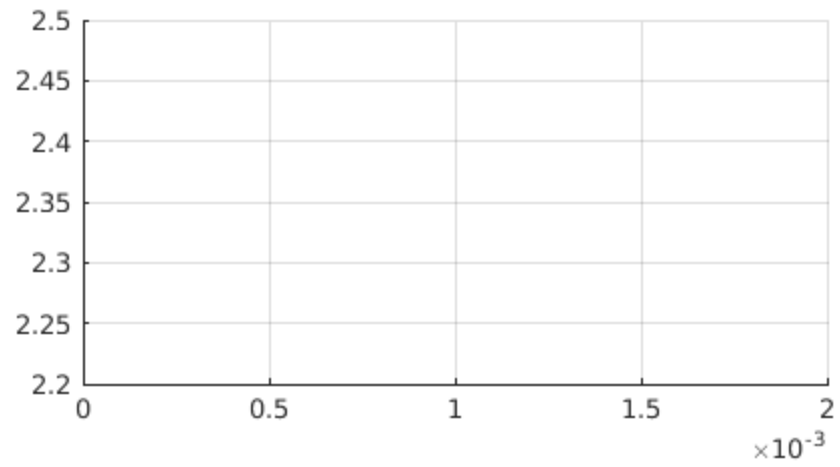


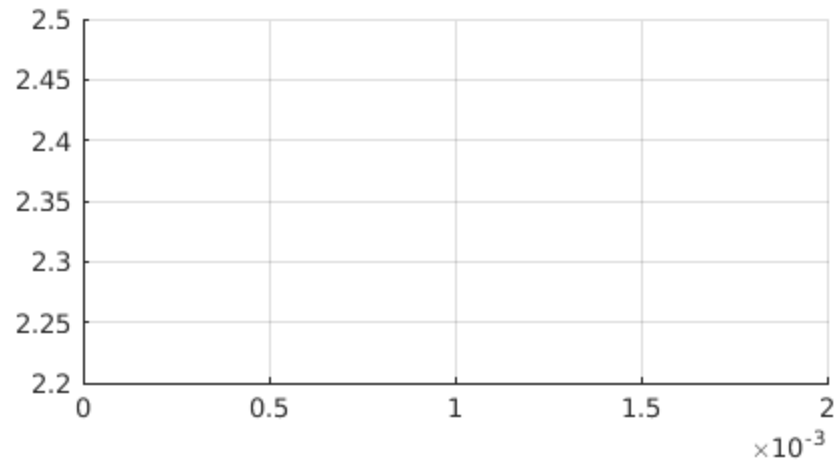
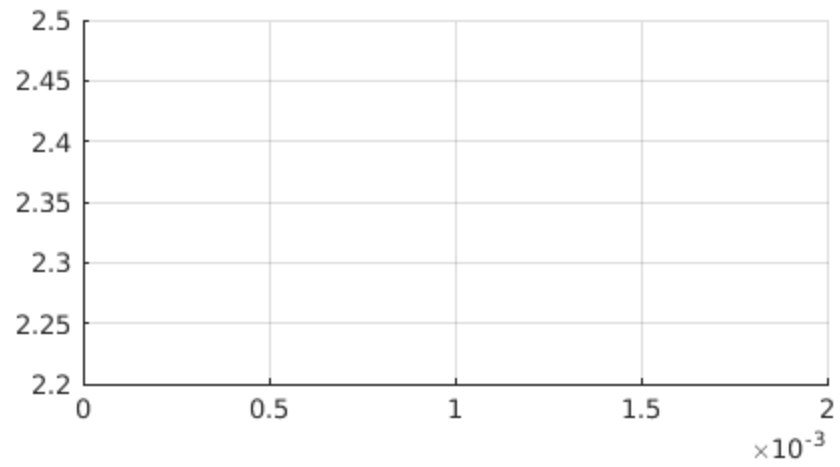


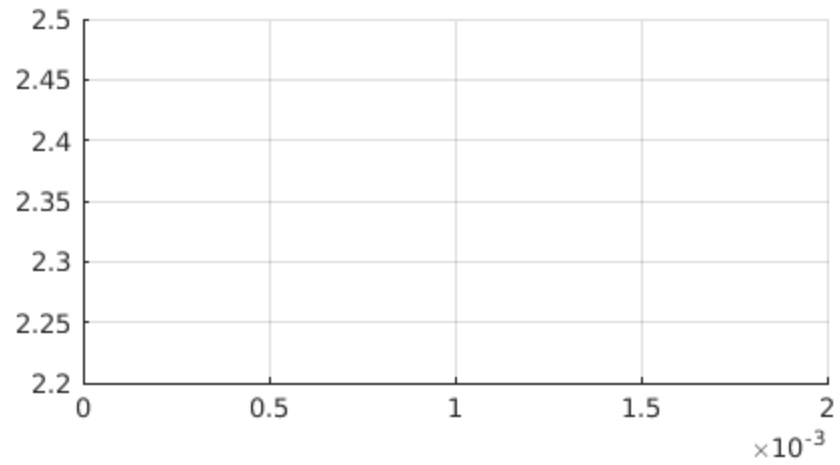
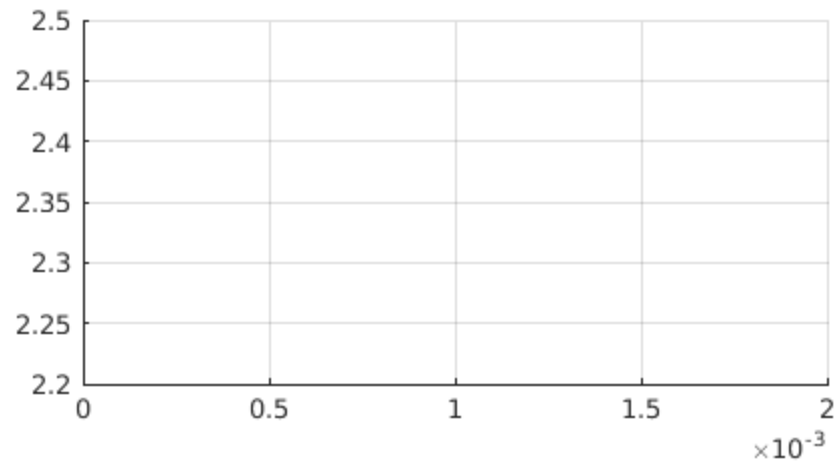


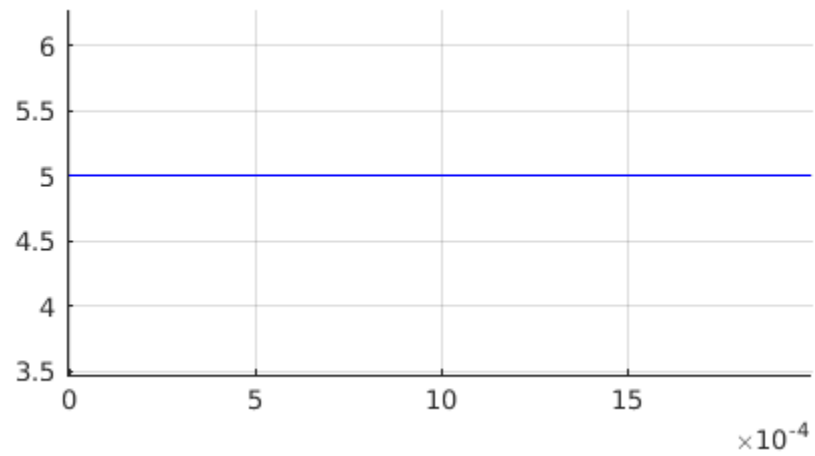
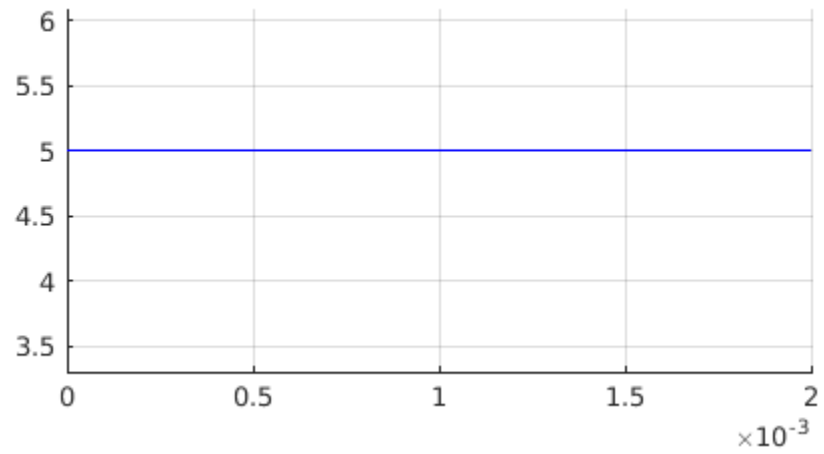


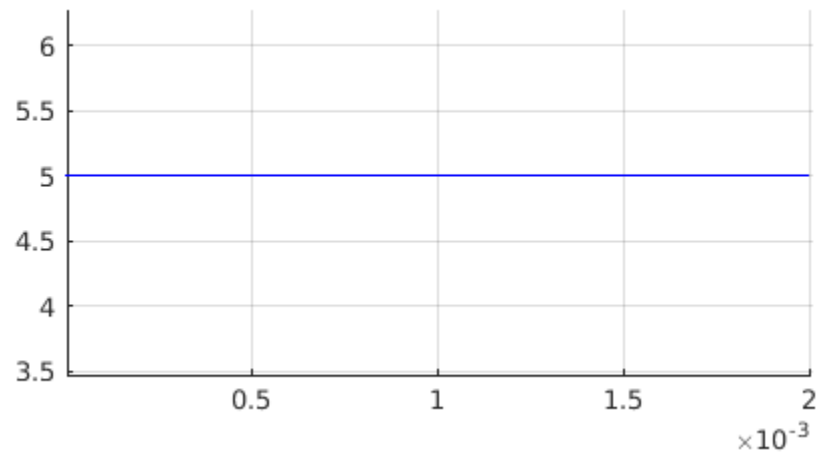
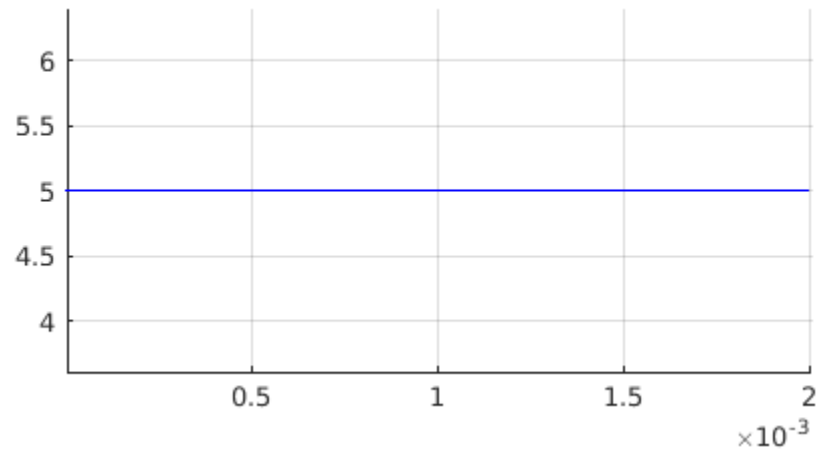


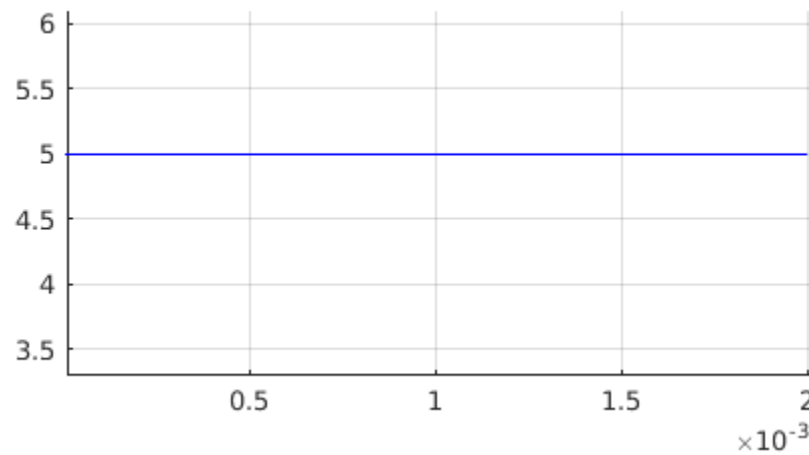




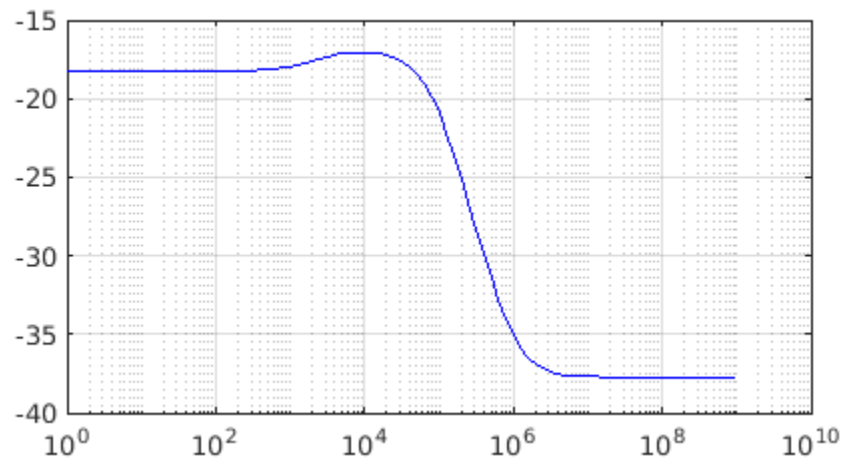


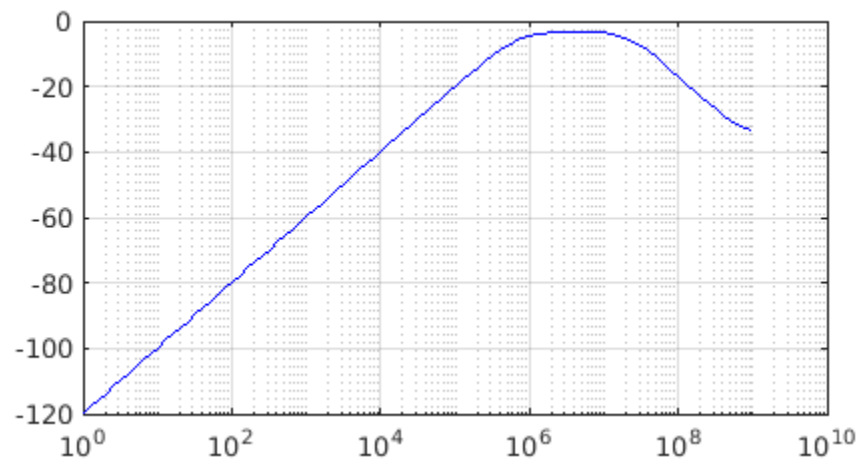
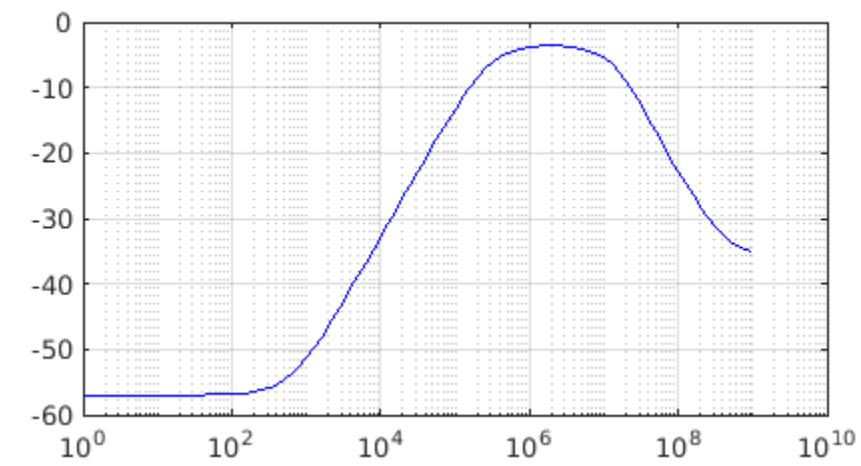


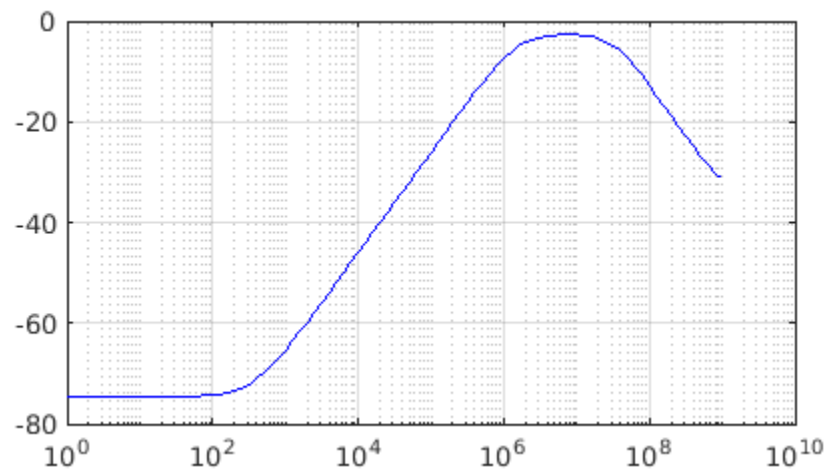
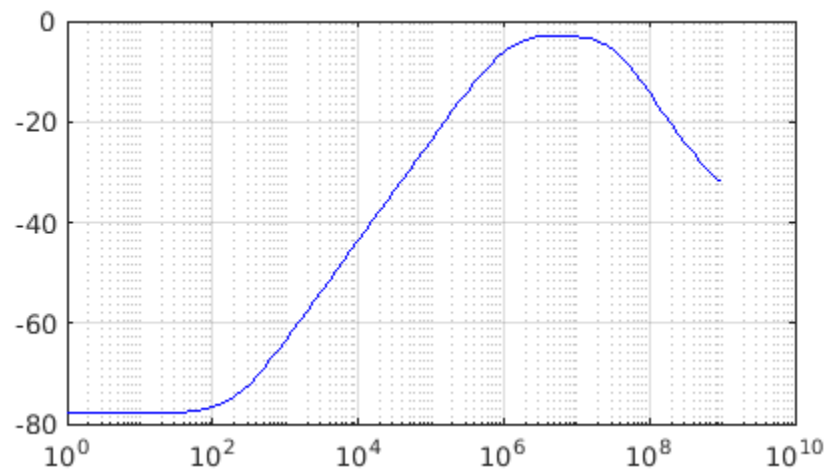


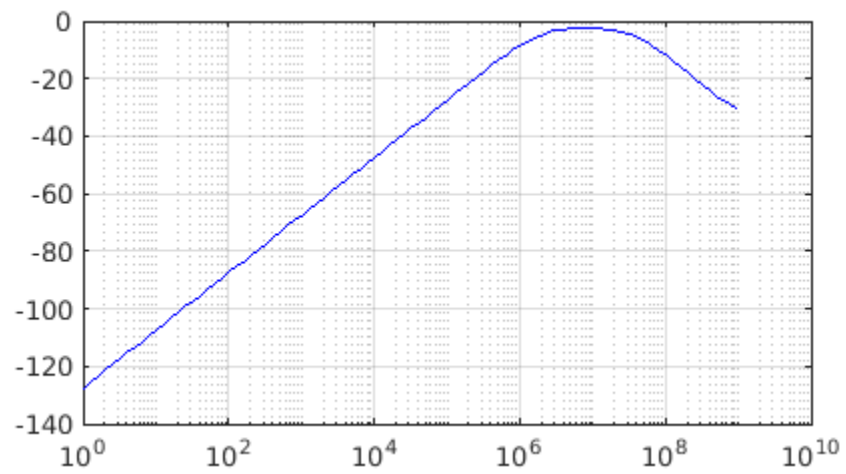
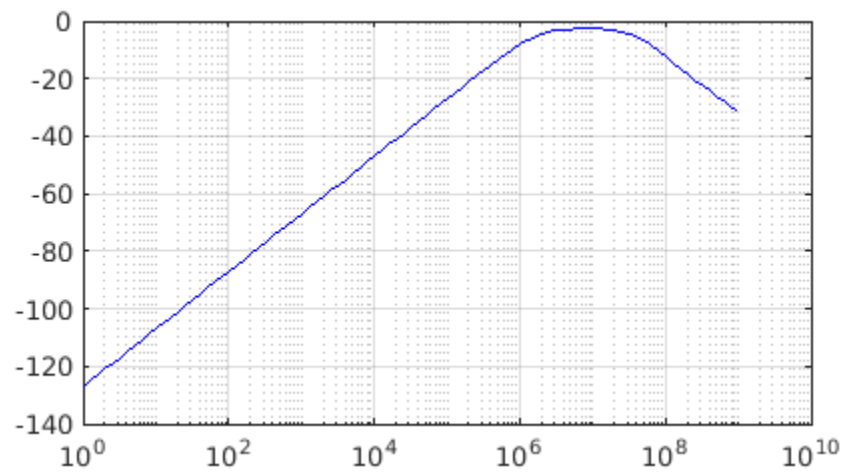


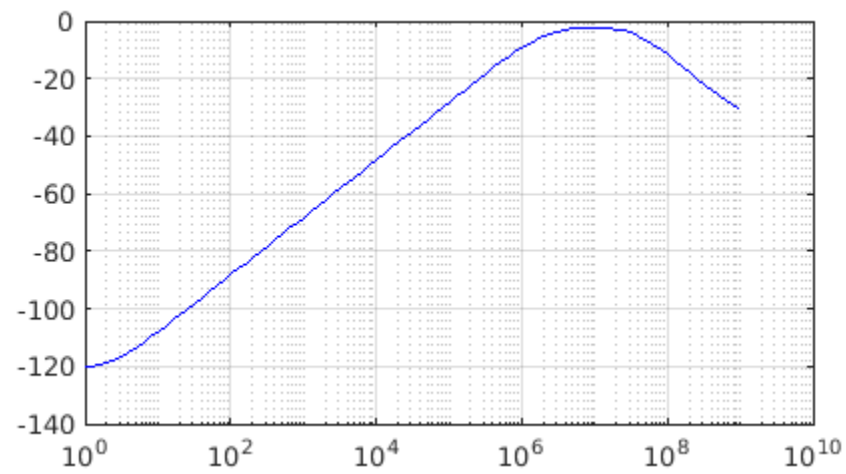
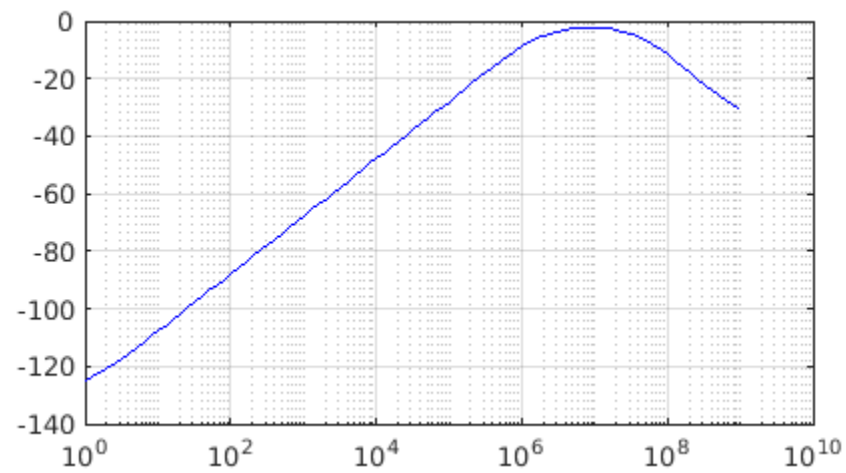
AC plots in order of their figure number

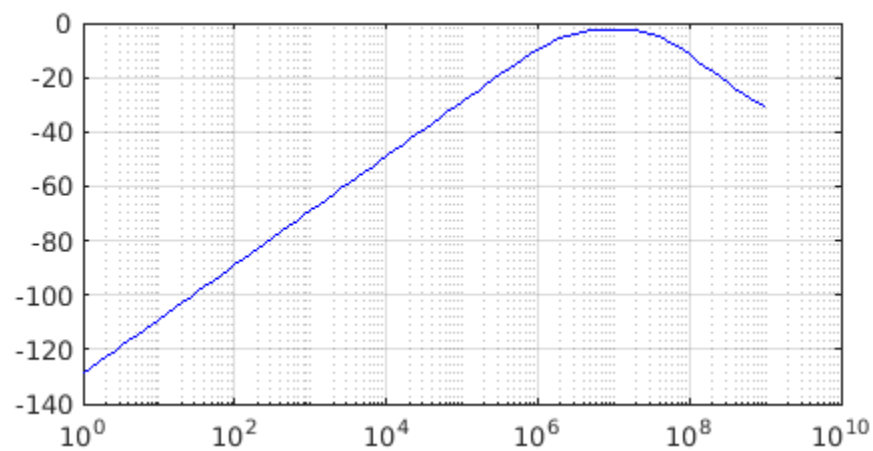
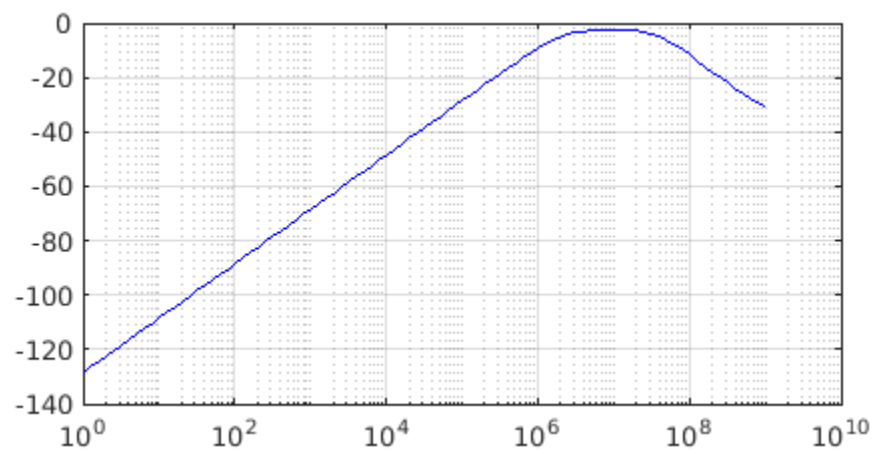


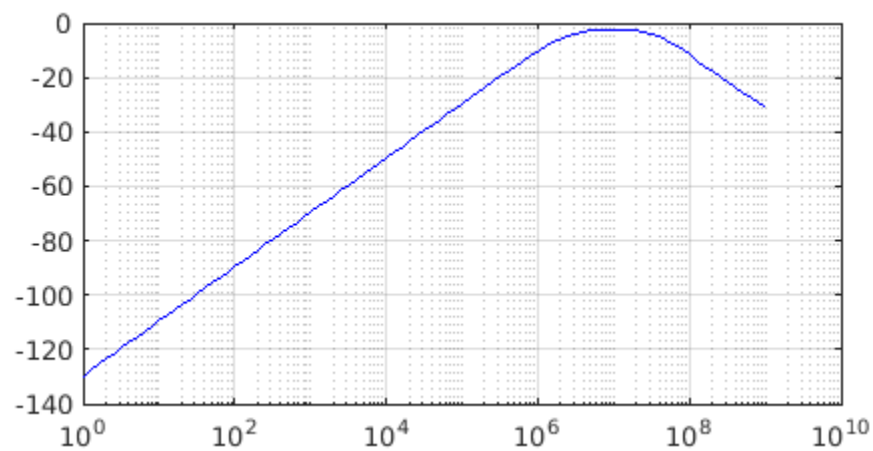
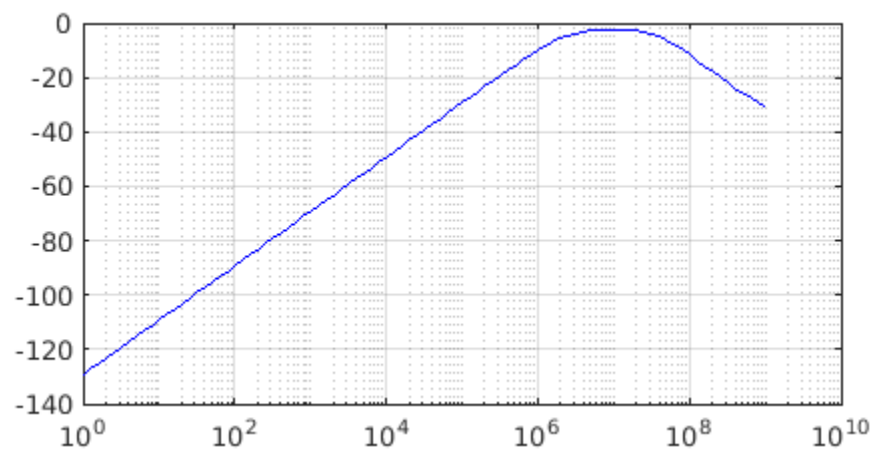


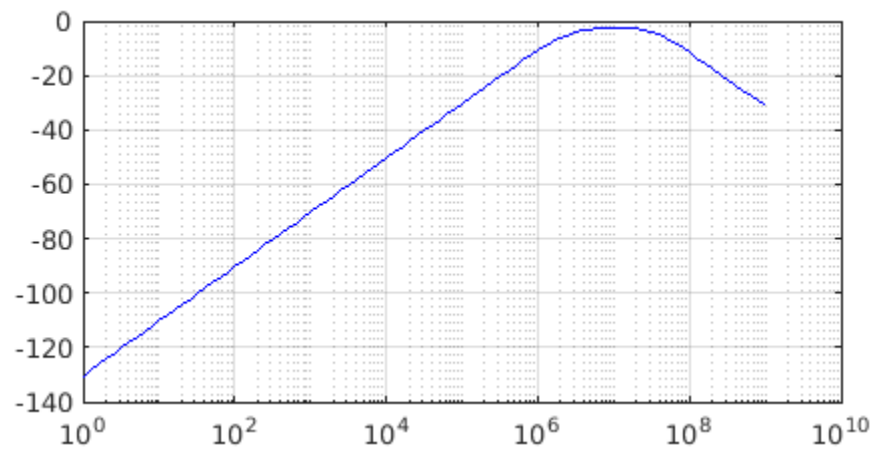
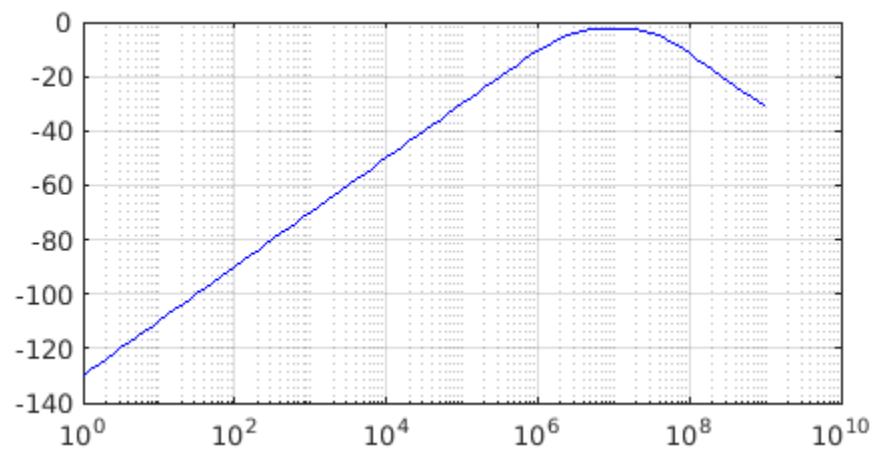


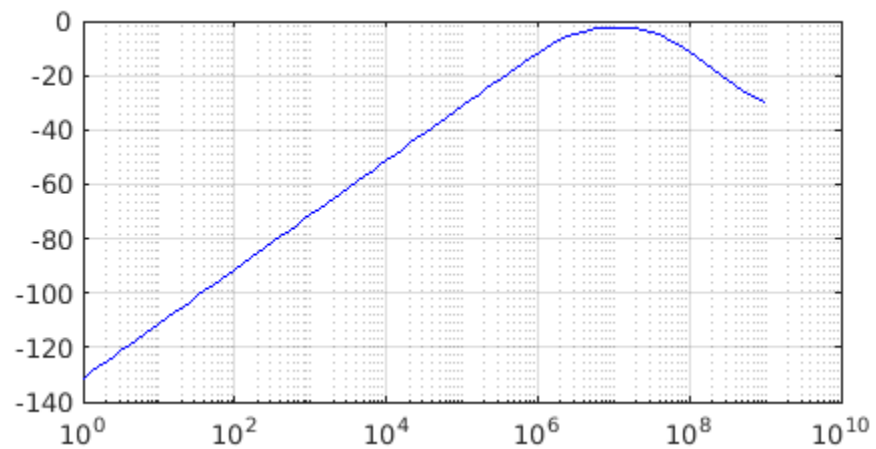
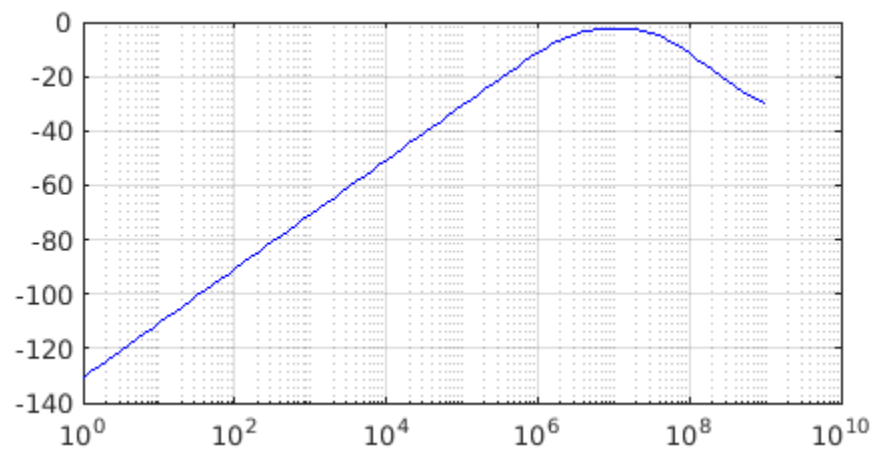


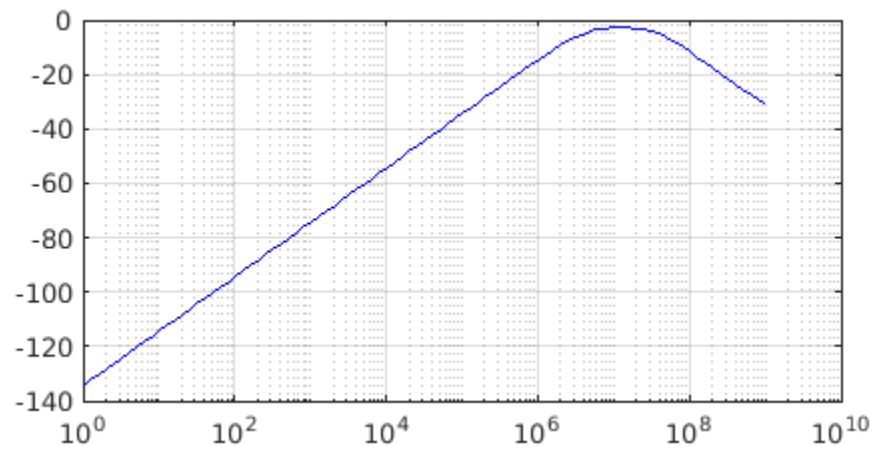
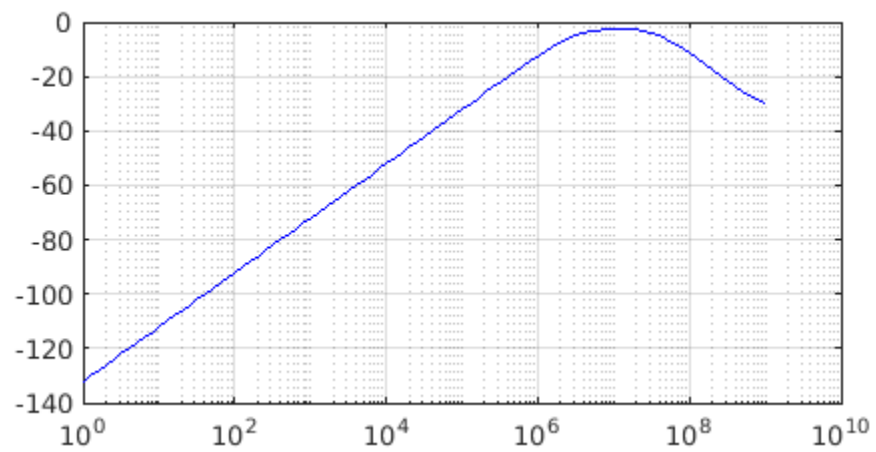


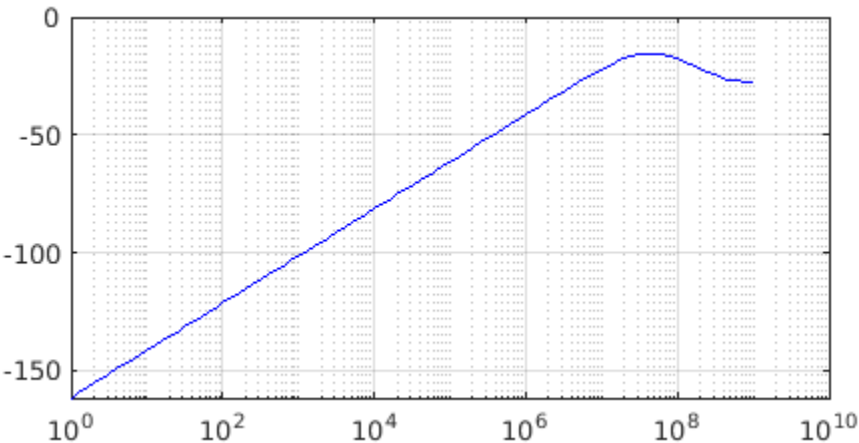




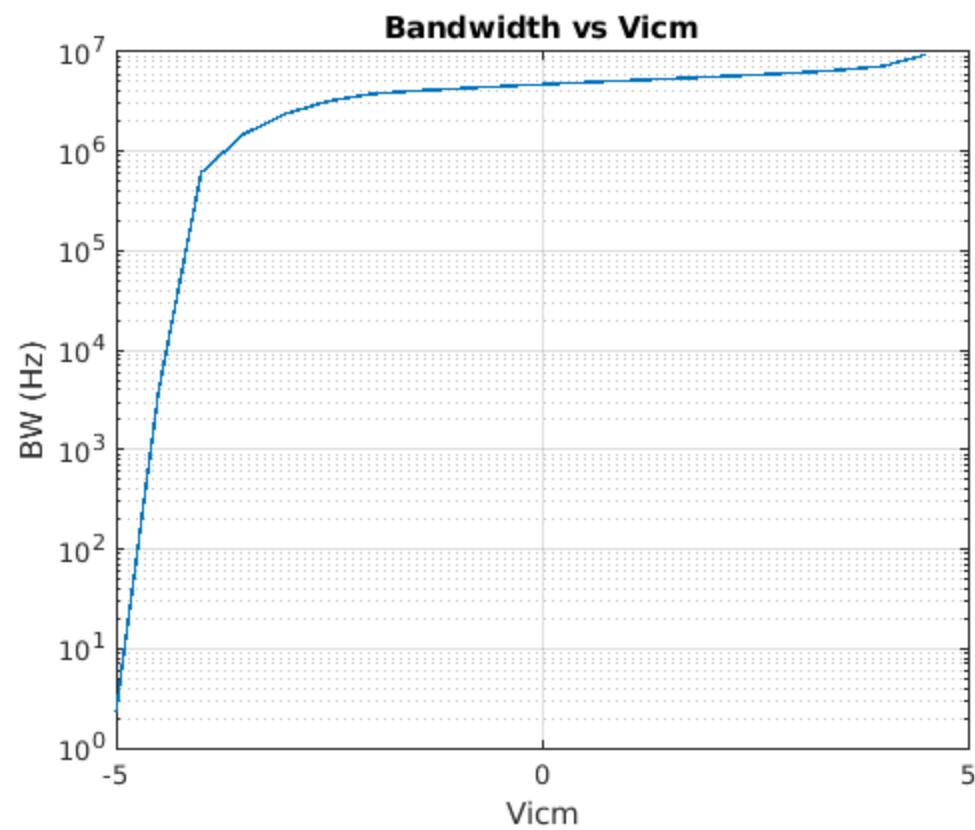


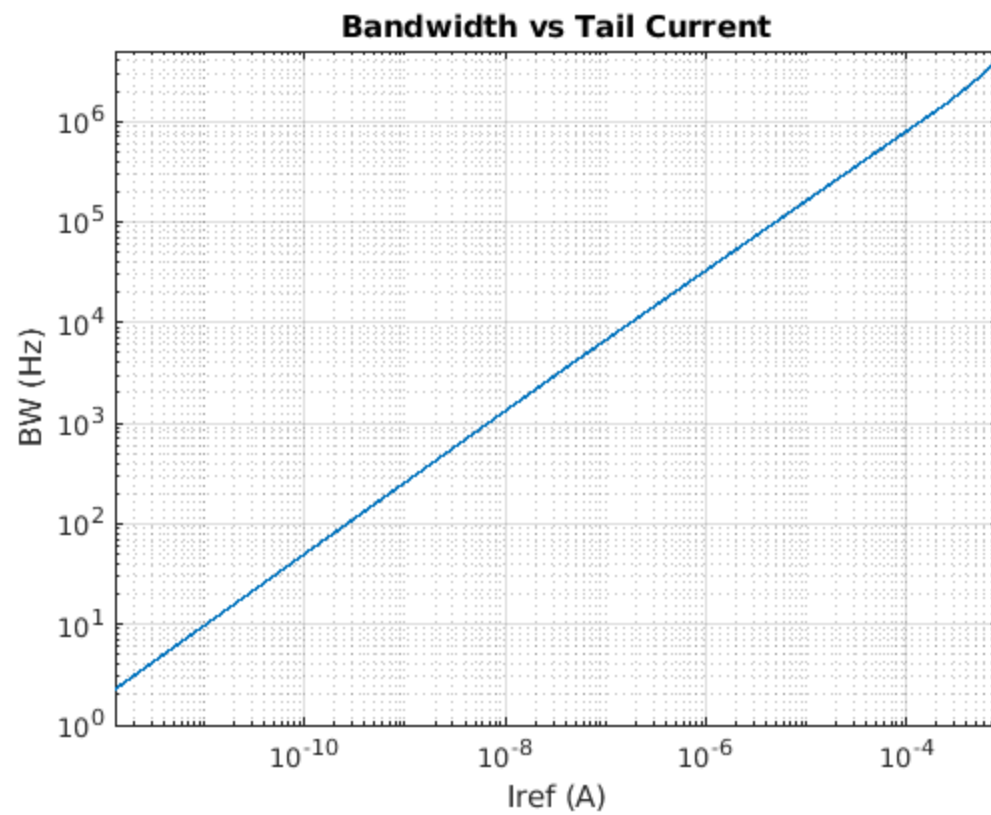


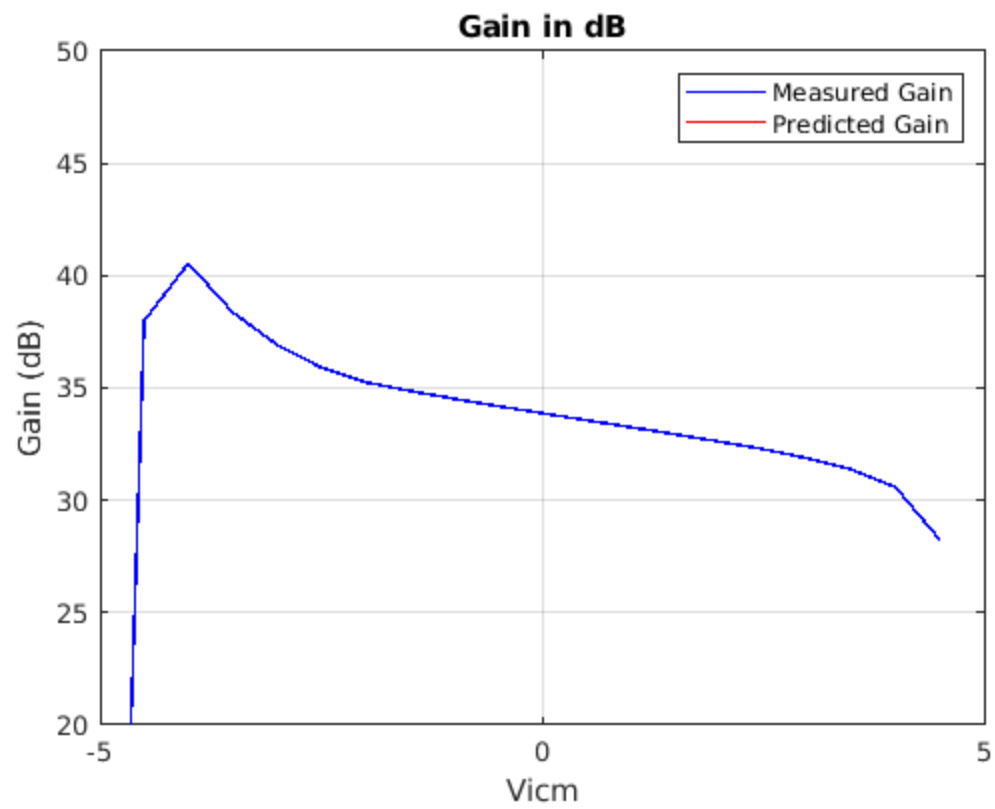


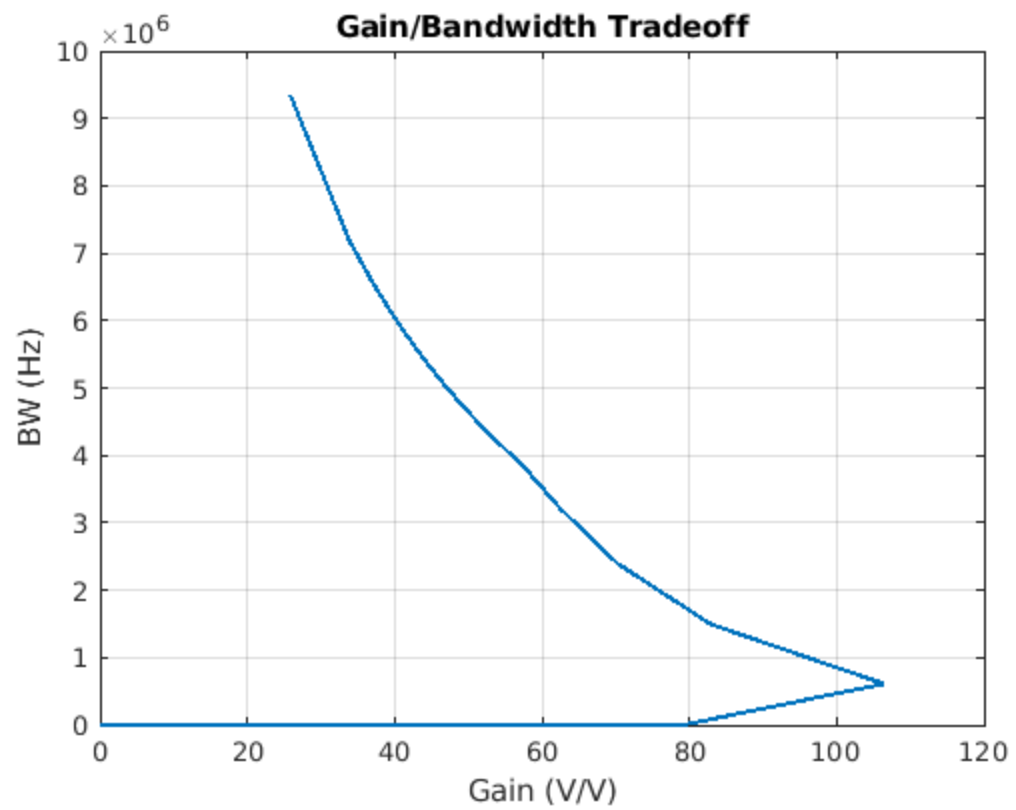


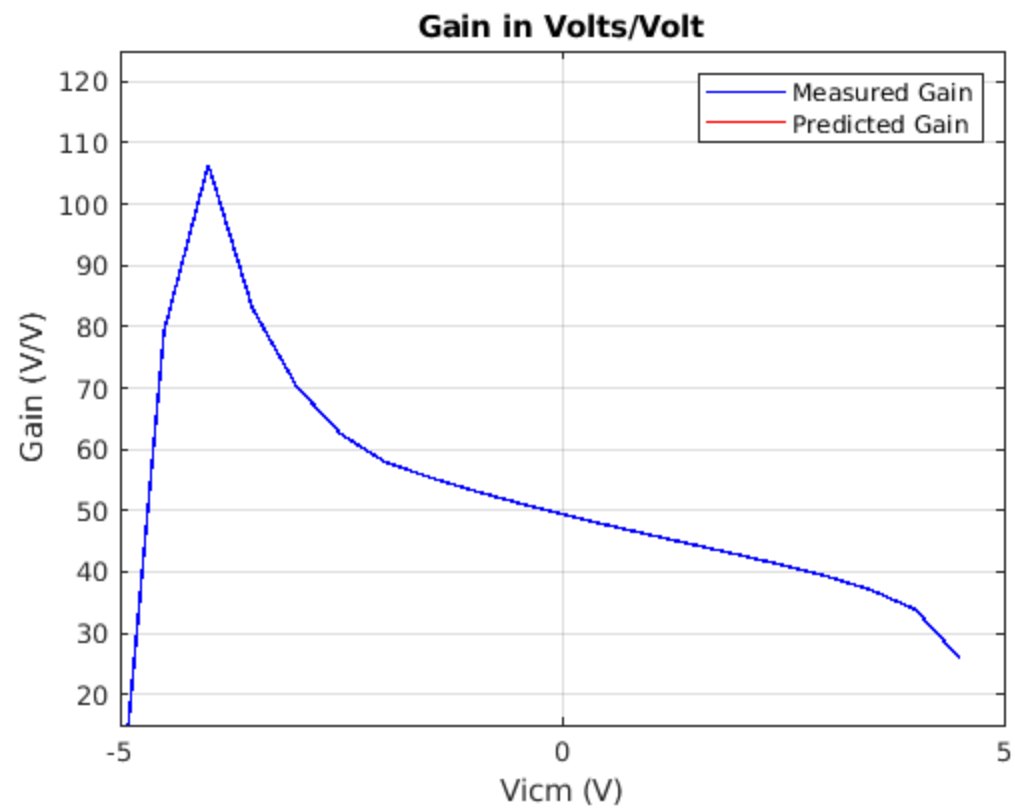
Plot Measurements:

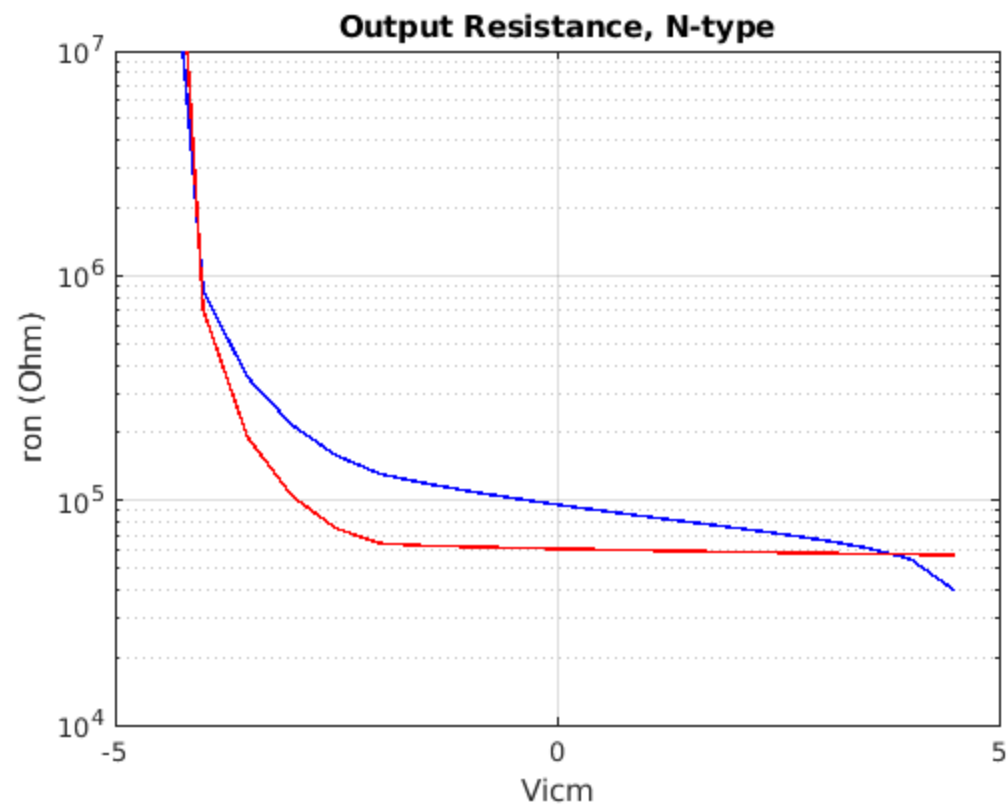


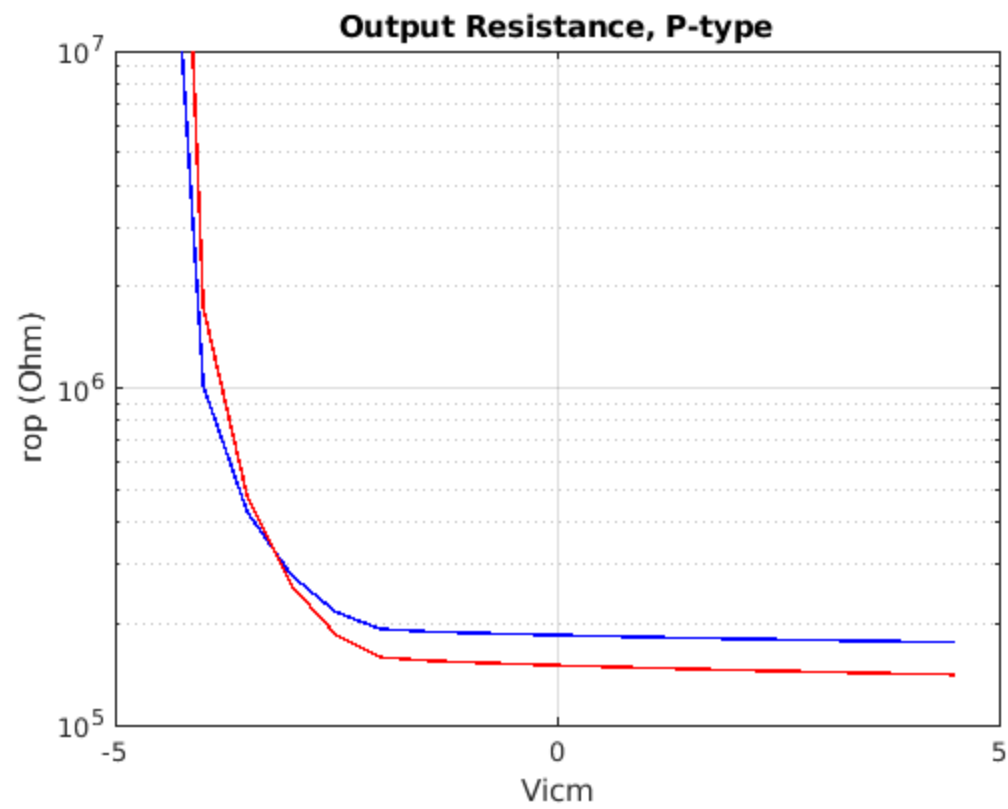


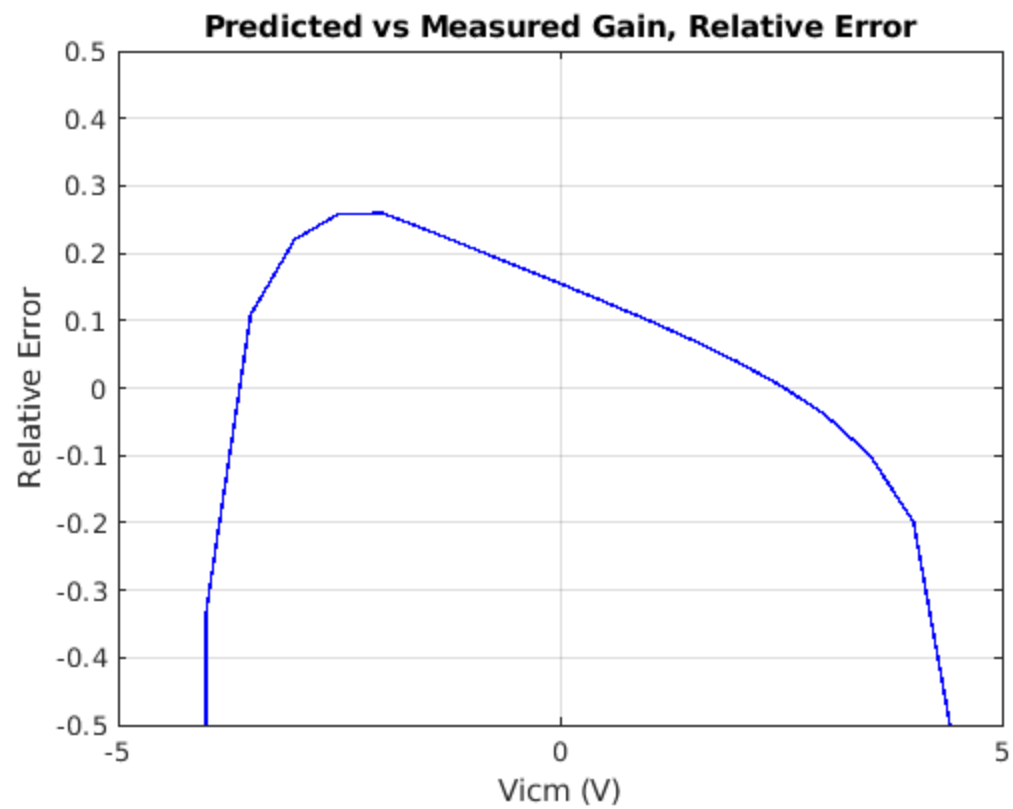


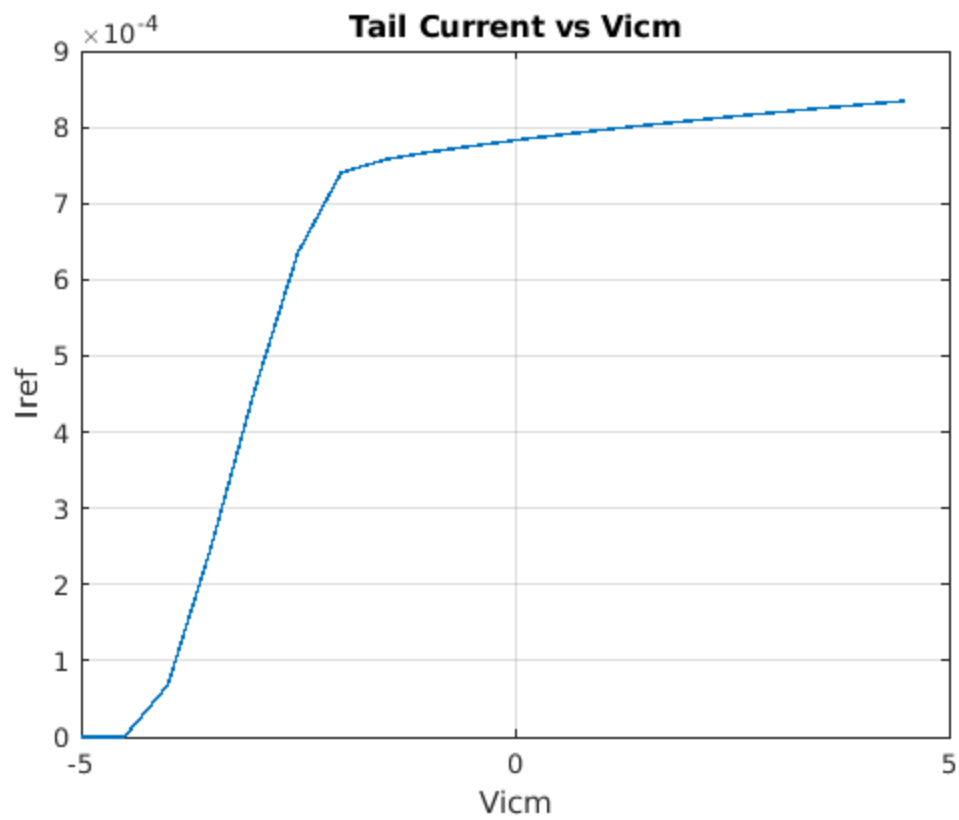


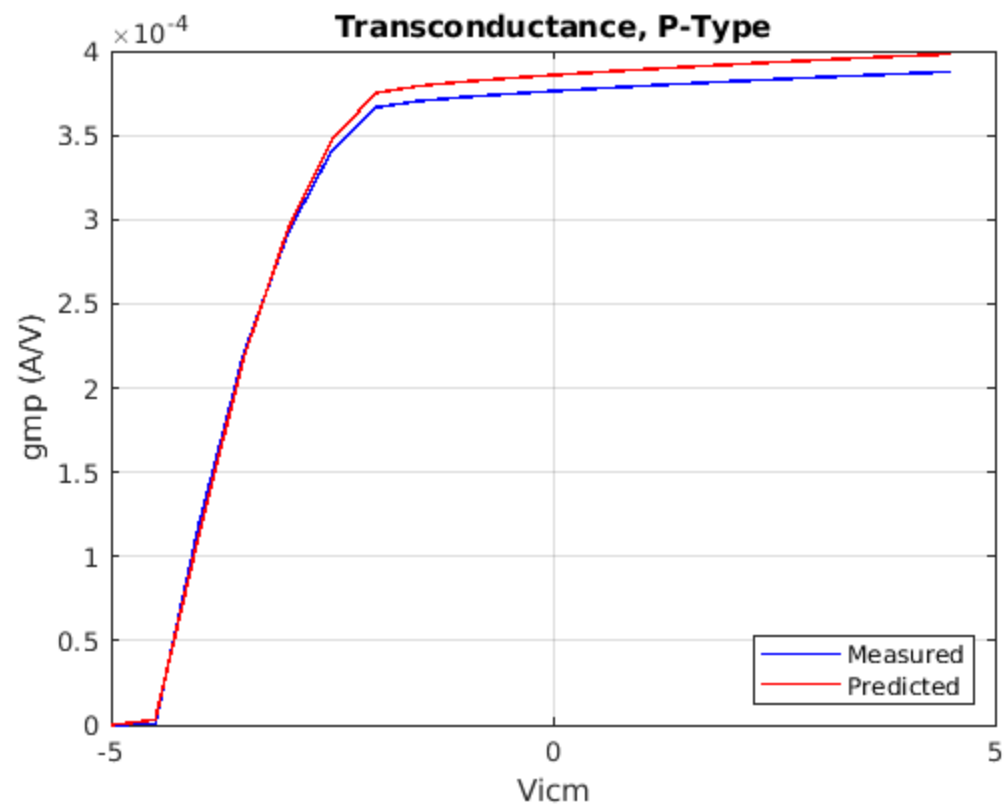


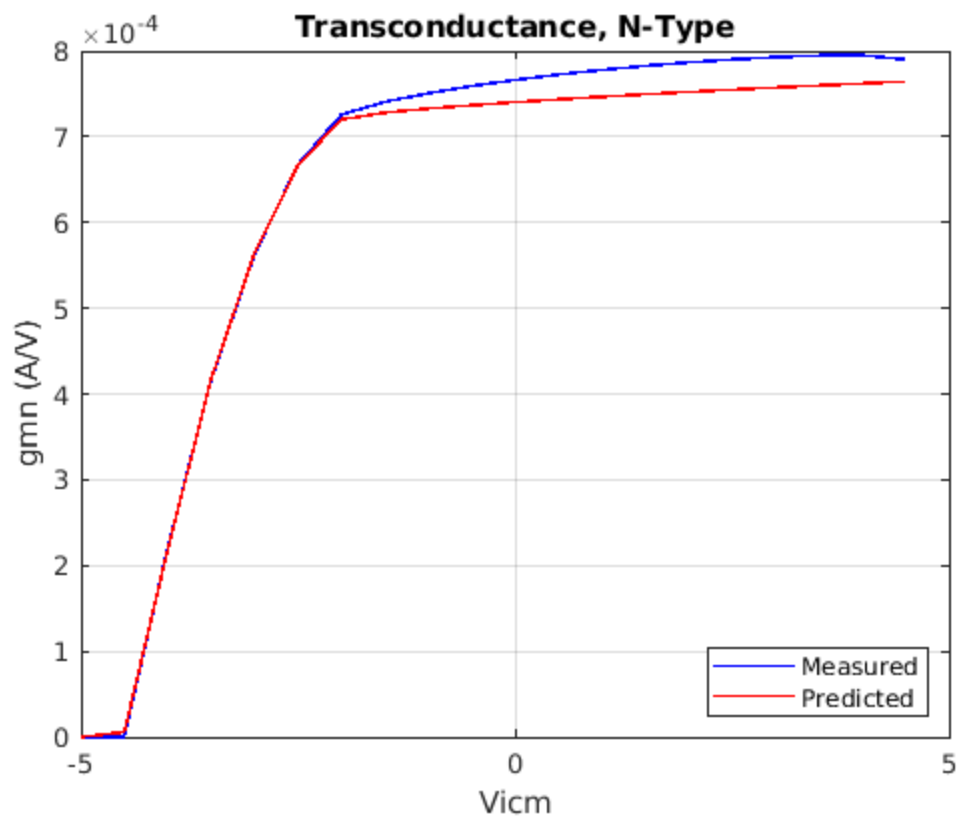






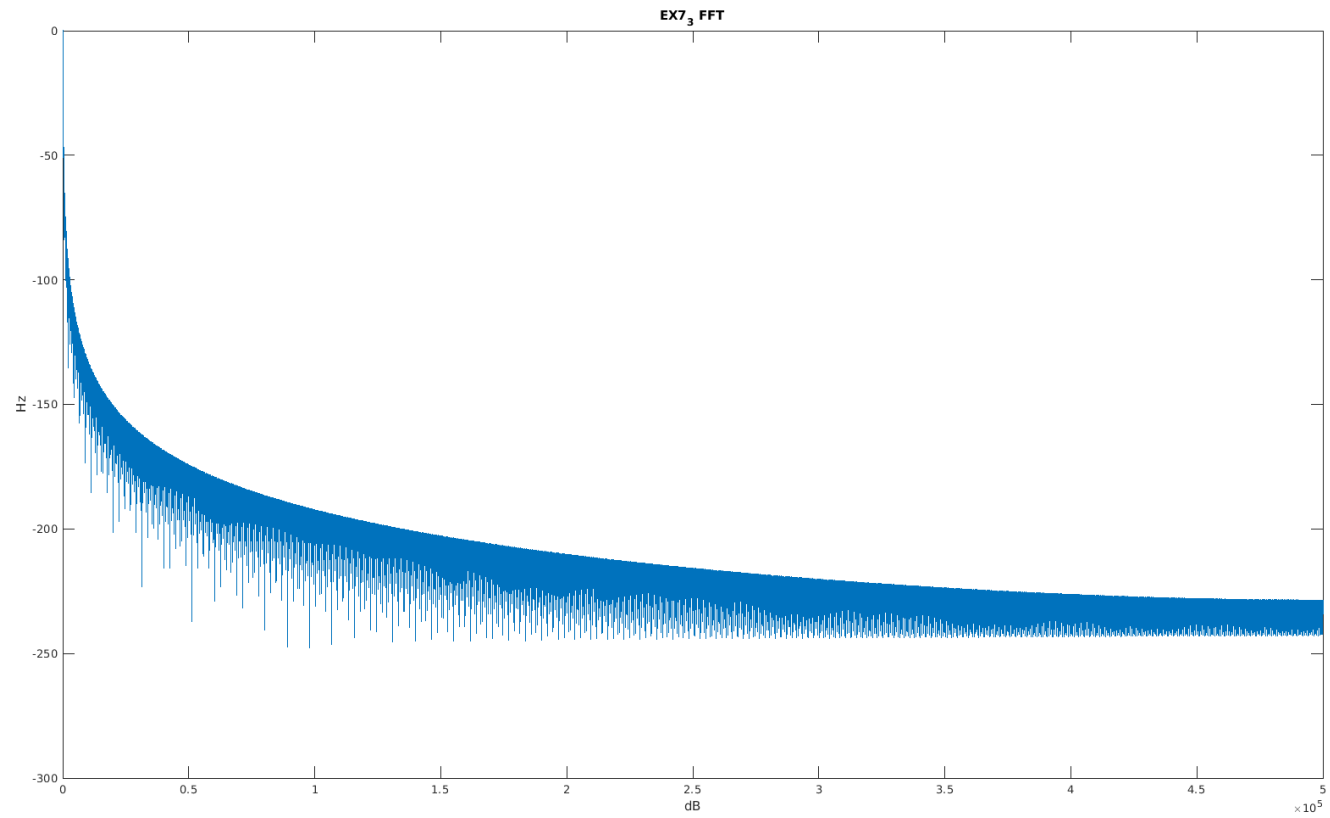






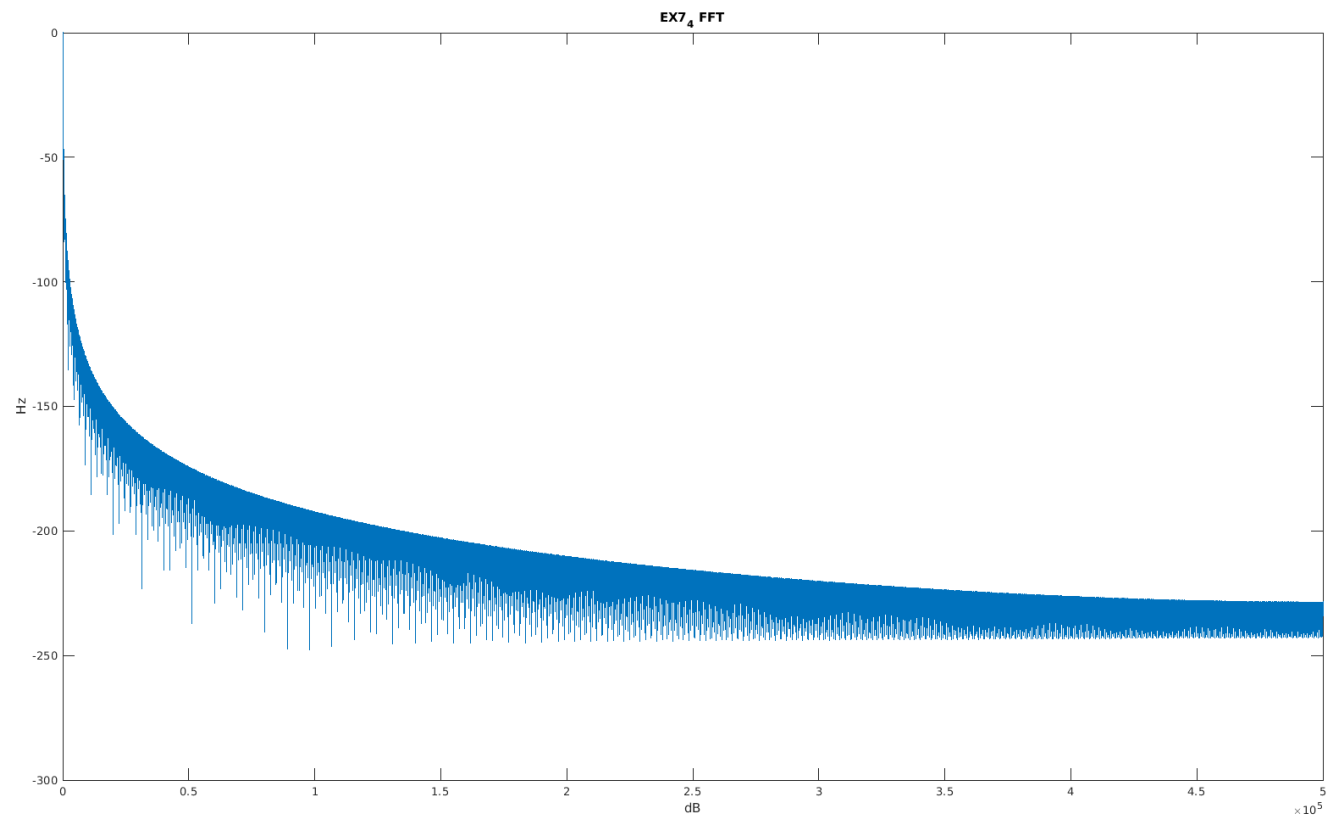
ex3:

SNR: -62.5993



ex4:

SNR: -62.5993



8

The open loop gain would be $V_{out}/(V_{in}+V_{icm}-V_{icm}) = V_{out}/V_{in}$

```
In [ ]: R1 = 1e3
        R2 = 10e3

        closed_gain = 1 + (R2/R1)
        print(closed_gain)
```

11.0

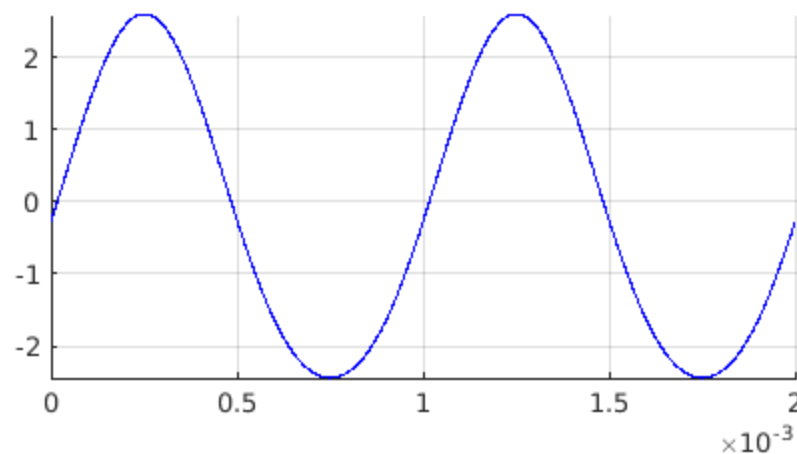
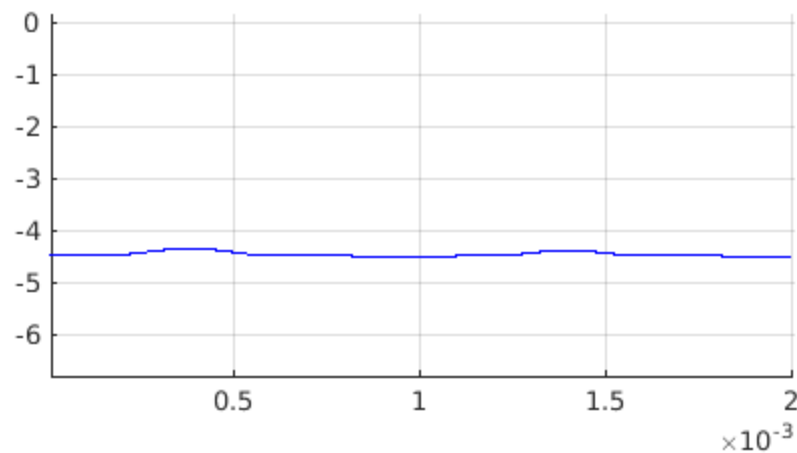
9

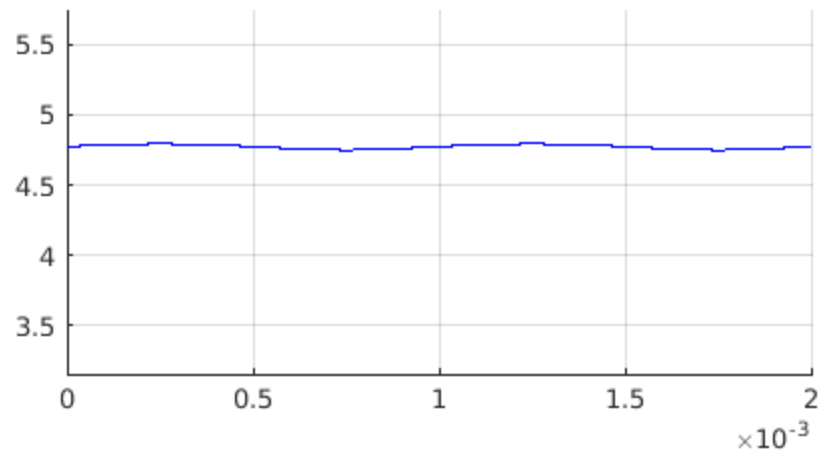
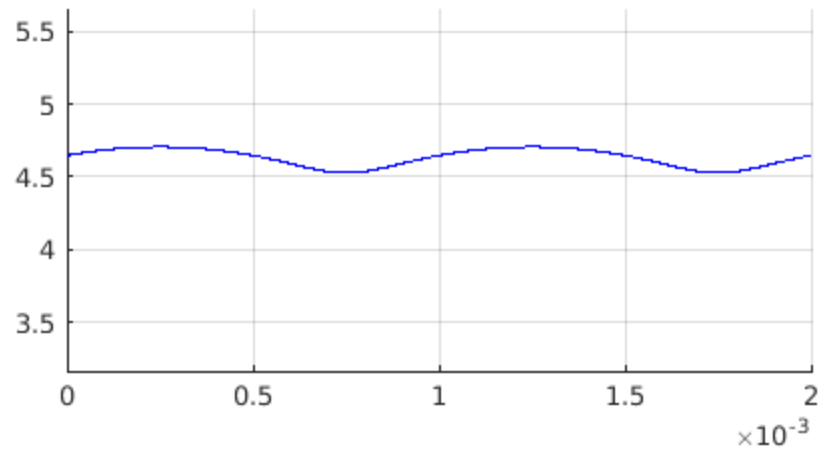
running ex2.sp with the added resistors:

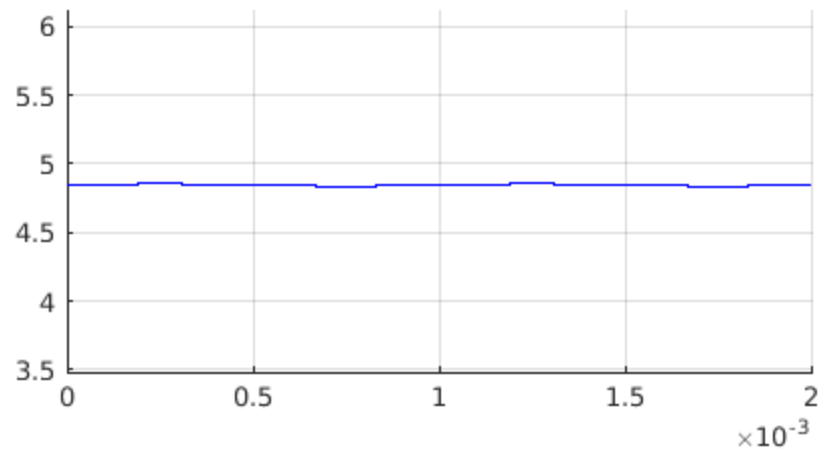
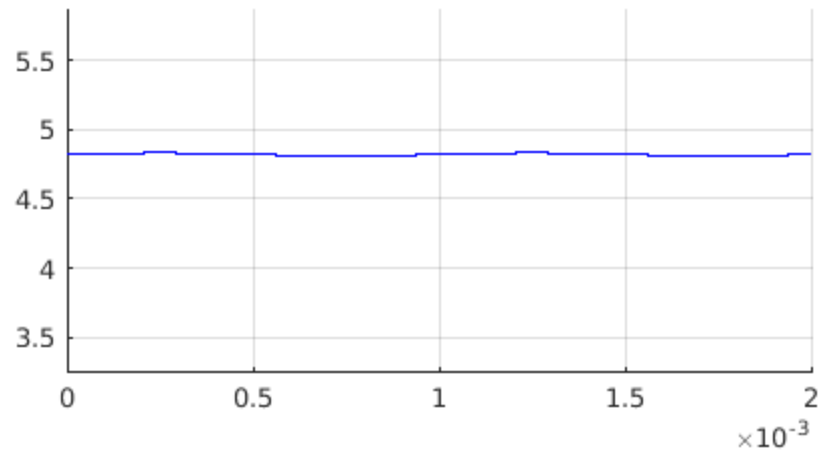
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1	1.359370e-11	2.440341e-10	5.888260e+12	2.172636e+11	
1	-4.50000e+00	4.562245e-08	3.599480e+01	3.112480e+01	2.352601e+03
2	4.802516e-07	5.563800e-07	1.735504e+08	1.161806e+08	
2	-4.00000e+00	6.795952e-05	1.258725e+03	6.199861e+01	2.213339e+05
3	2.204869e-04	1.200721e-04	8.519460e+05	1.011310e+06	
3	-3.50000e+00	2.491448e-04	4.463809e+01	3.299411e+01	6.453134e+05
4	4.165233e-04	2.200303e-04	3.530310e+05	4.271133e+05	
4	-3.00000e+00	4.547100e-04	1.081790e+01	2.068286e+01	1.082363e+06
5	5.626858e-04	2.916081e-04	2.170067e+05	2.773866e+05	
5	-2.50000e+00	6.353315e-04	5.716284e+00	1.514228e+01	1.466356e+06
6	6.676968e-04	3.411038e-04	1.583725e+05	2.163249e+05	
6	-2.00000e+00	7.405122e-04	4.059474e+00	1.216939e+01	1.738711e+06
7	7.257644e-04	3.665050e-04	1.309852e+05	1.926588e+05	
7	-1.50000e+00	7.572604e-04	3.468593e+00	1.080307e+01	1.866346e+06
8	7.405037e-04	3.703683e-04	1.190680e+05	1.894083e+05	
8	-1.00000e+00	7.669354e-04	2.992677e+00	9.521197e+00	1.983660e+06
9	7.506235e-04	3.725796e-04	1.098886e+05	1.875853e+05	
9	-5.00000e-01	7.752391e-04	2.576169e+00	8.219487e+00	2.104502e+06
10	7.590347e-04	3.744656e-04	1.022302e+05	1.860515e+05	
10	0.000000e+00	7.827466e-04	2.206006e+00	6.872132e+00	2.231213e+06
11	7.662185e-04	3.761616e-04	9.565915e+04	1.846886e+05	
11	5.000000e-01	7.896944e-04	1.873938e+00	5.455102e+00	2.372117e+06
12	7.724354e-04	3.777235e-04	8.988962e+04	1.834469e+05	
12	1.000000e+00	7.962122e-04	1.574001e+00	3.940101e+00	2.542911e+06
13	7.778460e-04	3.791819e-04	8.471235e+04	1.822989e+05	
13	1.500000e+00	8.023825e-04	1.301645e+00	2.289854e+00	2.772334e+06
14	7.825525e-04	3.805568e-04	7.995818e+04	1.812266e+05	
14	2.000000e+00	8.082623e-04	1.053305e+00	4.510856e-01	3.126418e+06
15	7.866128e-04	3.818618e-04	7.547212e+04	1.802178e+05	
15	2.500000e+00	8.138936e-04	8.261552e-01	-1.65877e+00	3.927282e+06
16	7.900404e-04	3.831069e-04	7.108454e+04	1.792632e+05	
16	3.000000e+00	8.193079e-04	6.179622e-01	-4.18076e+00	9.629904e+06

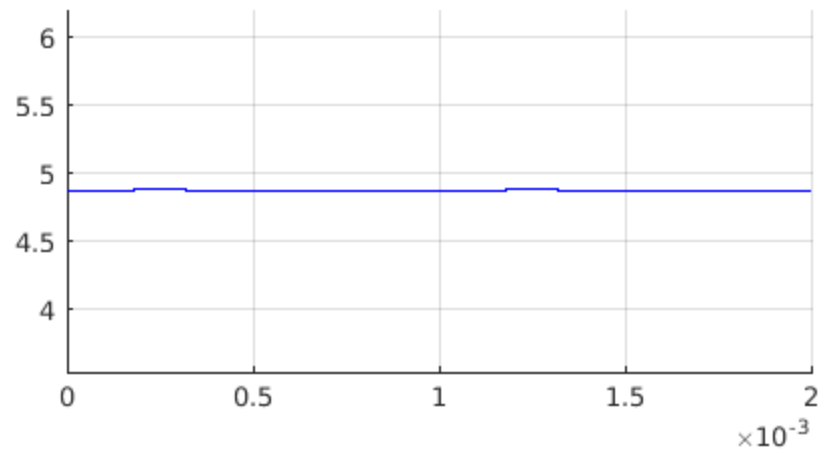
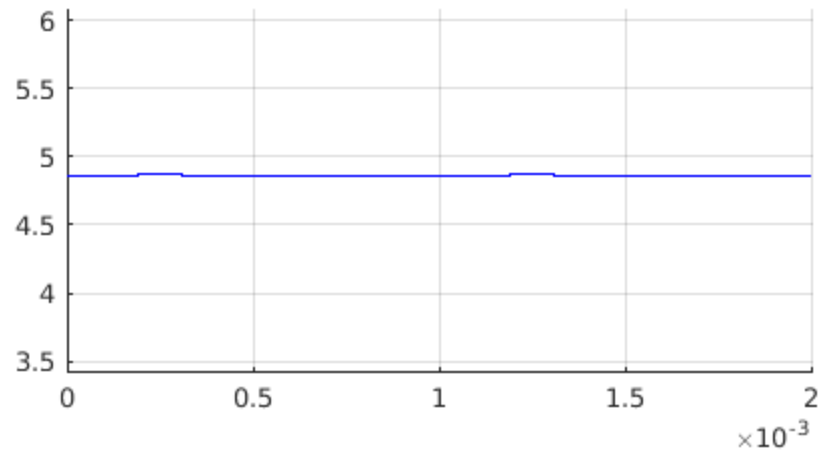
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17	3.500000e+00	8.245299e-04	4.270001e-01	-7.39144e+00
7.946772e-04	3.854463e-04	6.146744e+04	1.774904e+05	
18	4.000000e+00	8.295776e-04	2.519136e-01	-1.19750e+01
7.951190e-04	3.865509e-04	5.465628e+04	1.766626e+05	
19	4.500000e+00	8.344579e-04	8.870148e-02	-2.10414e+01
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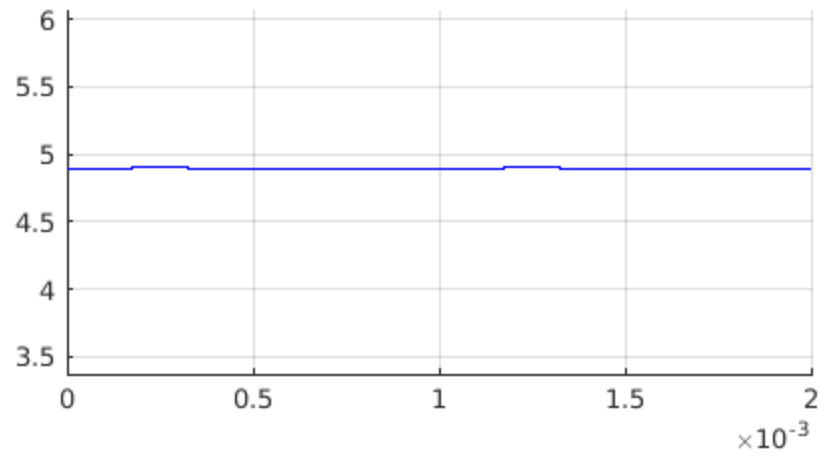
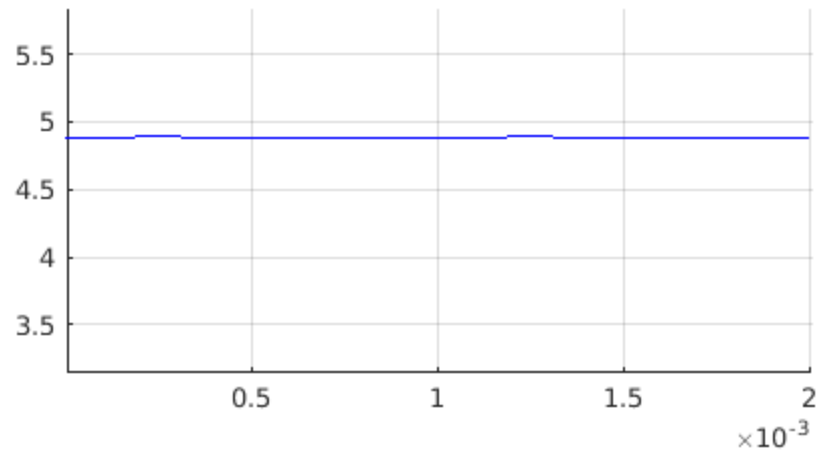
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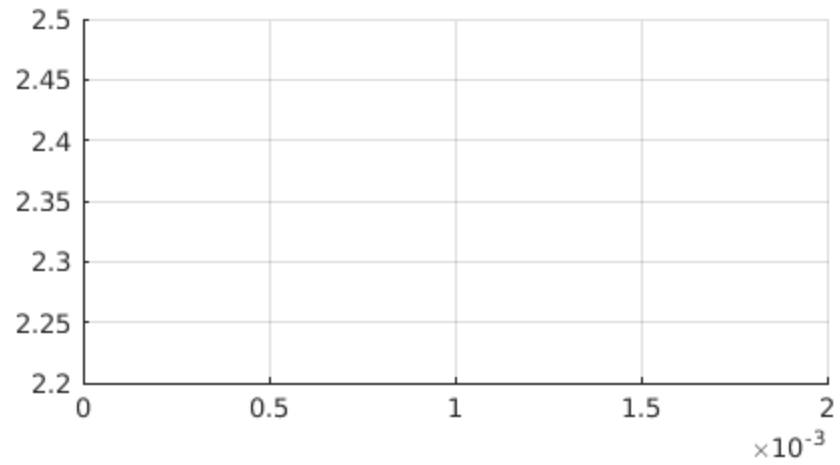
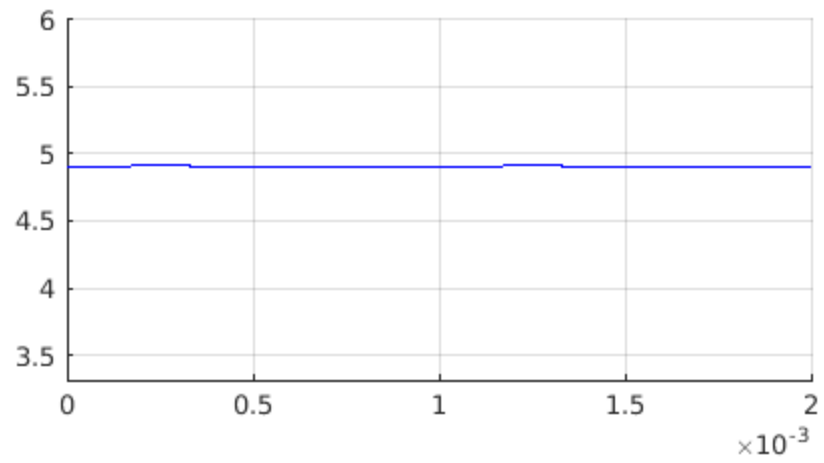


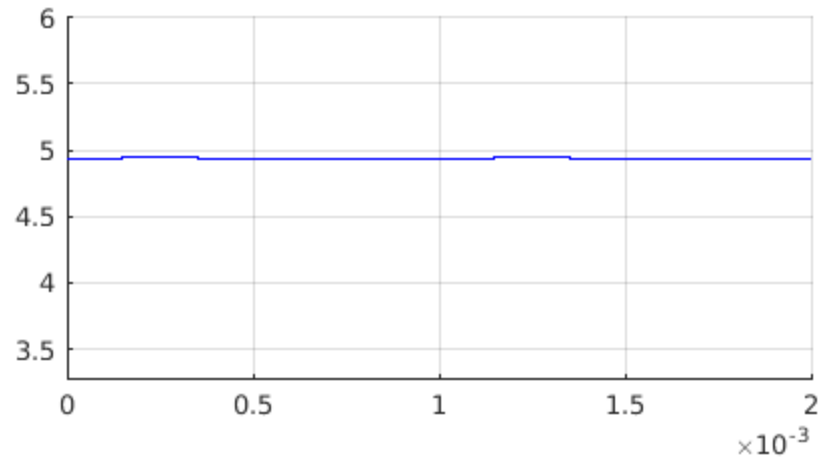
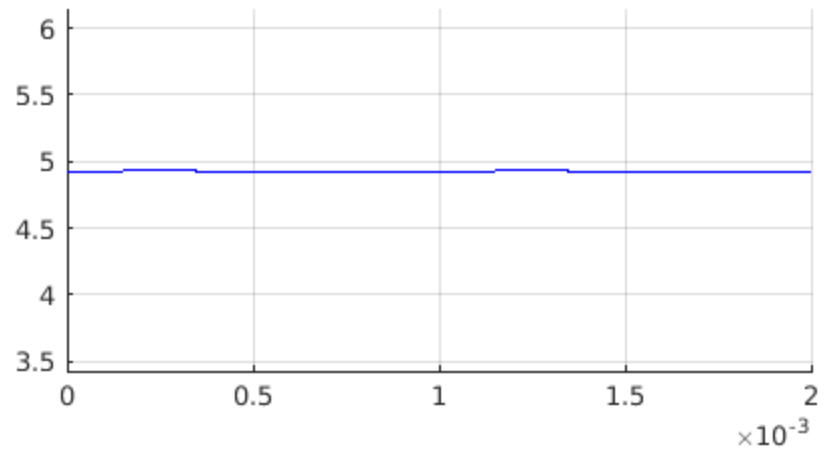


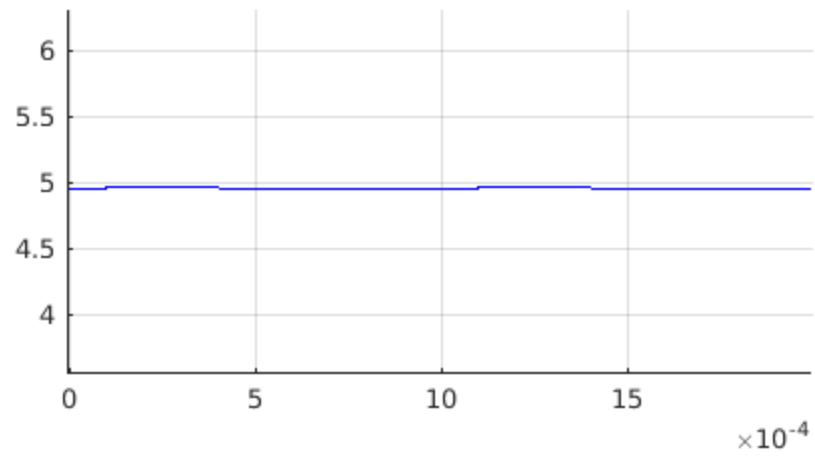
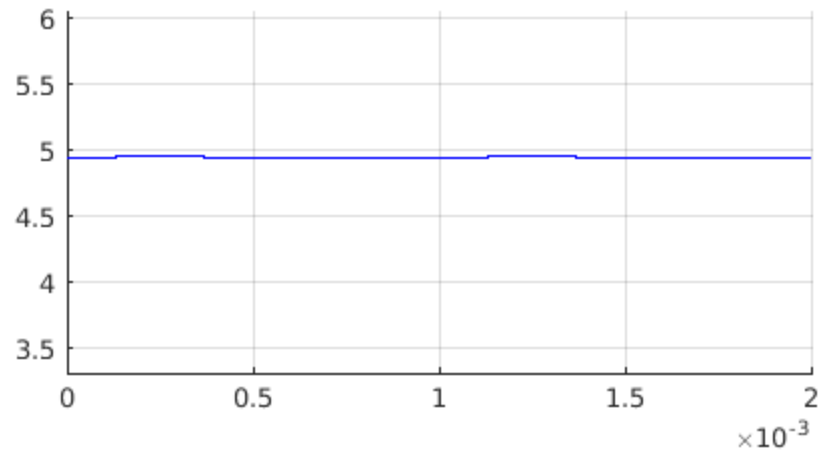


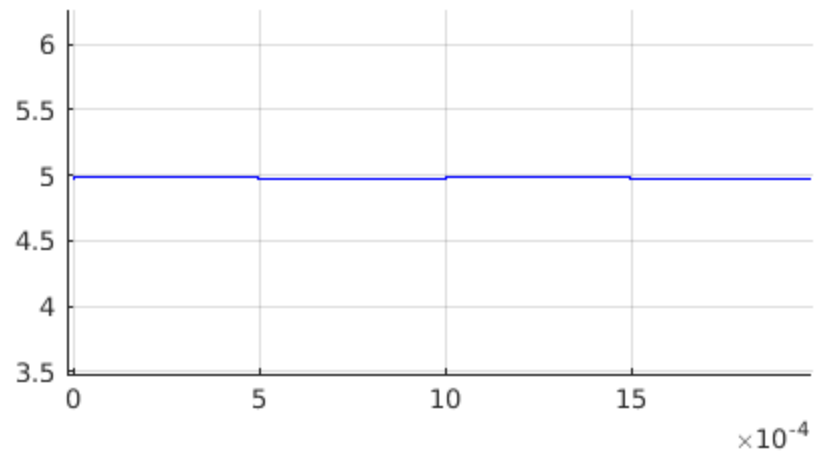


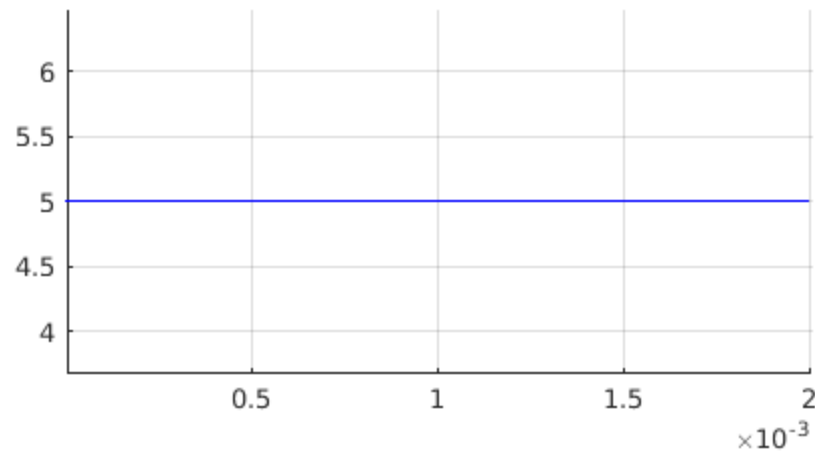
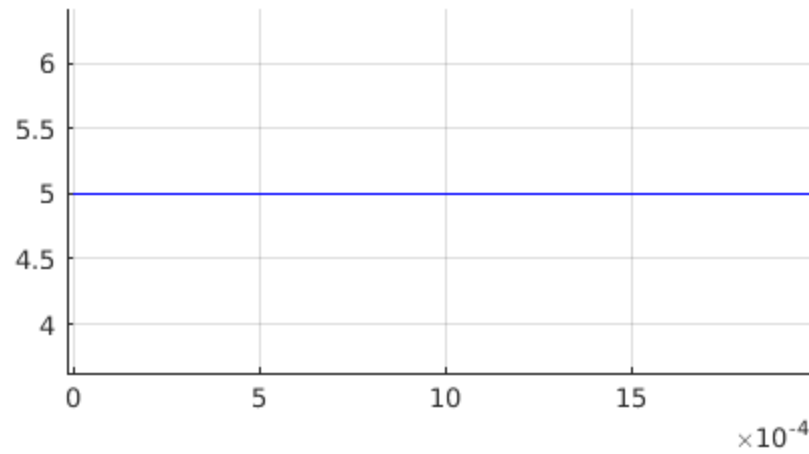




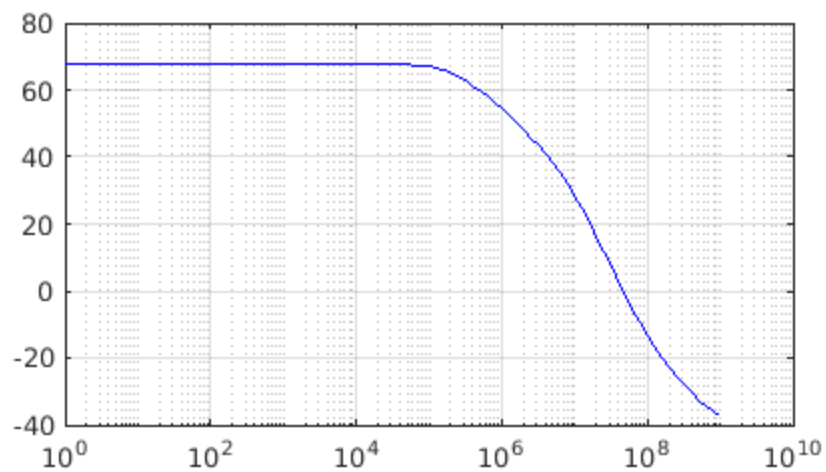
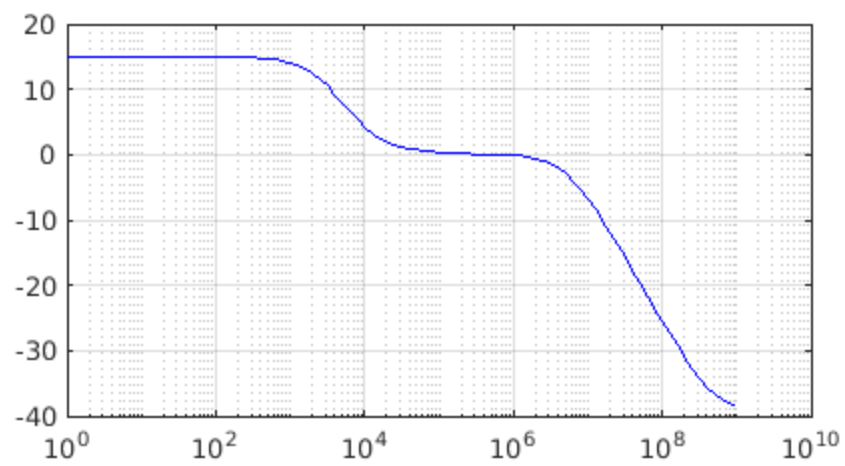


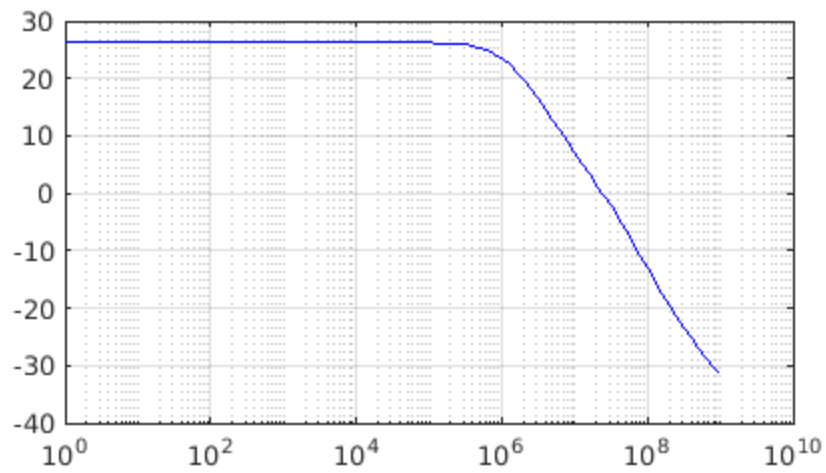
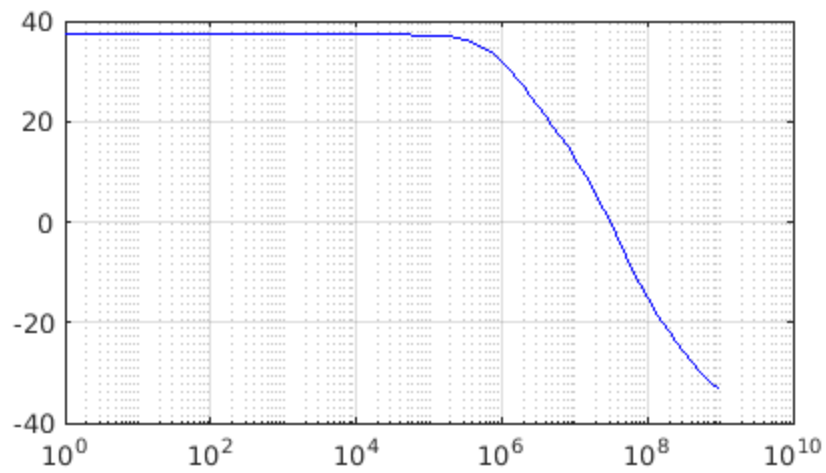


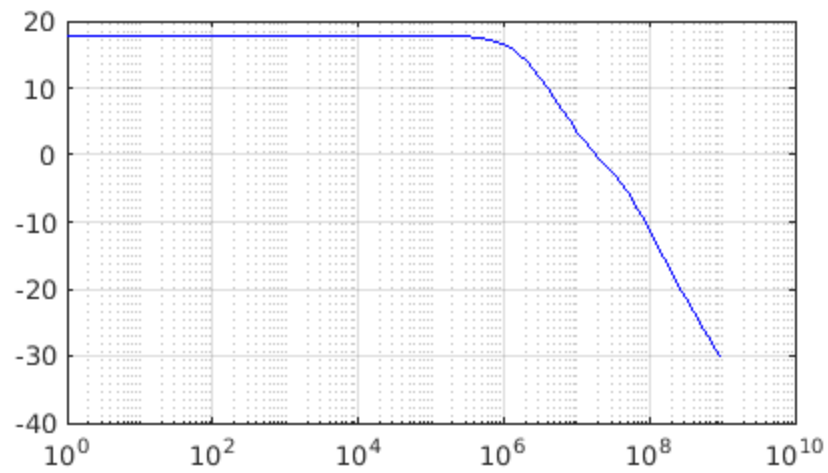
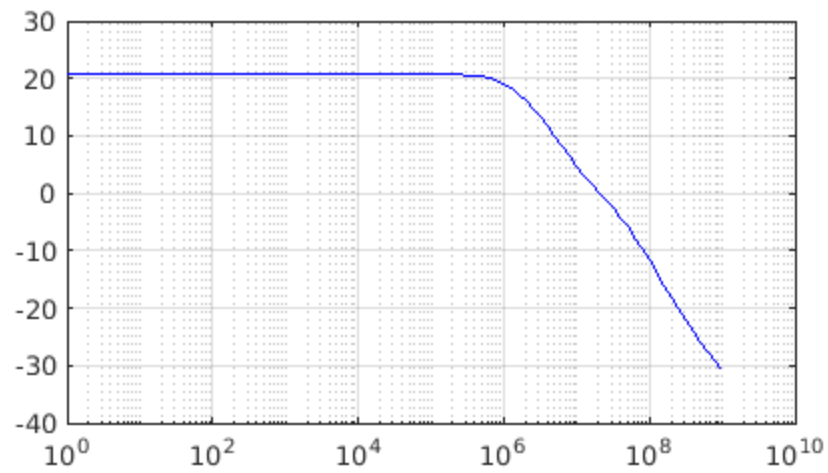


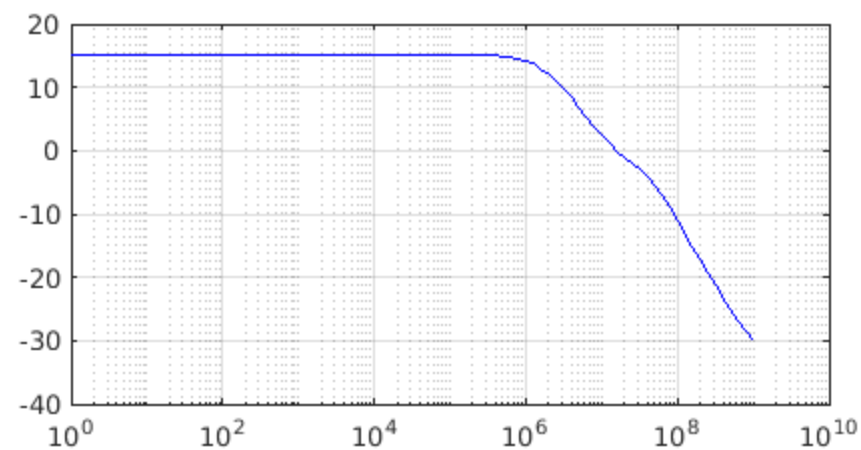
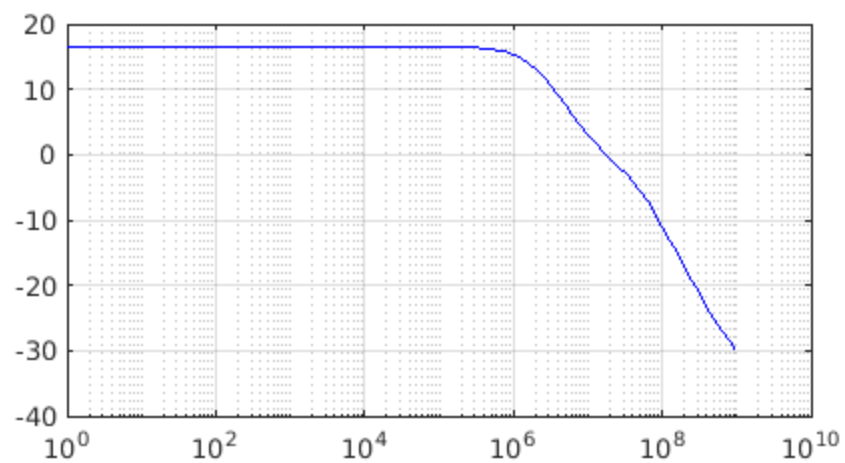


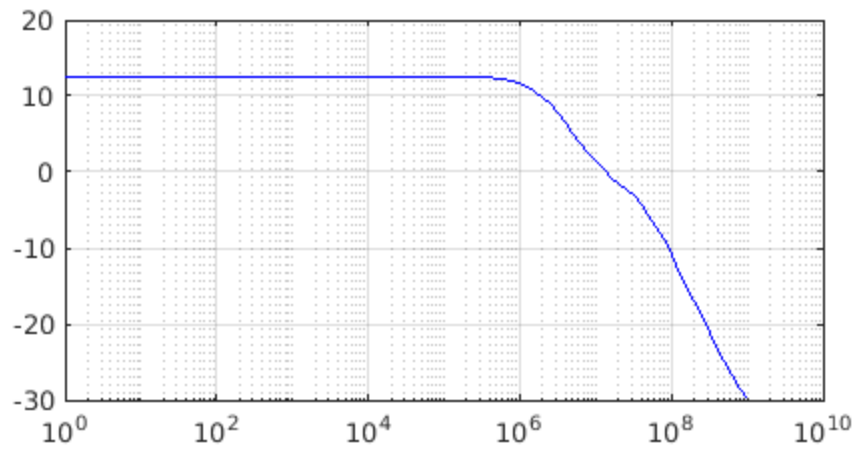
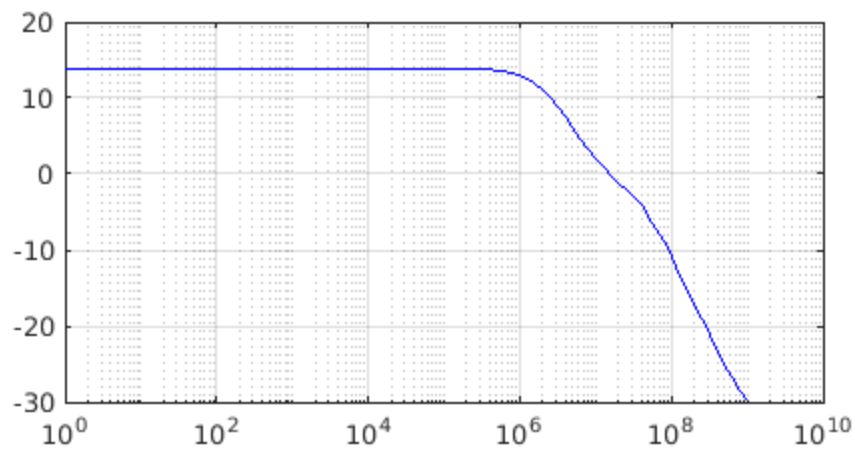
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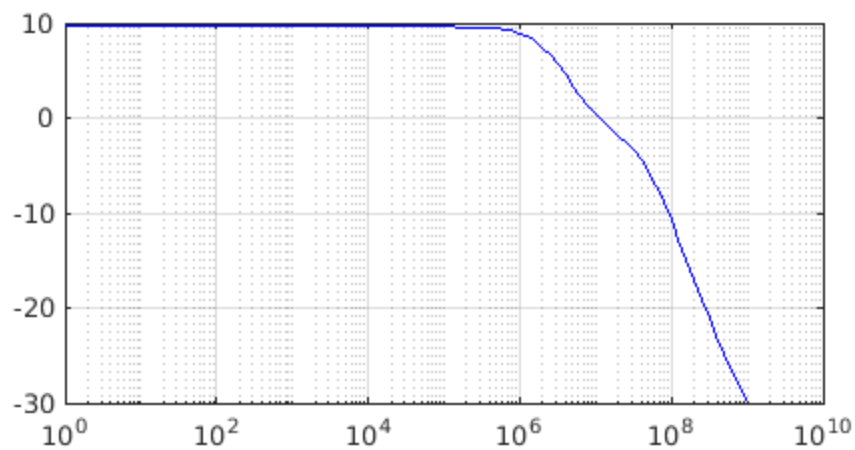
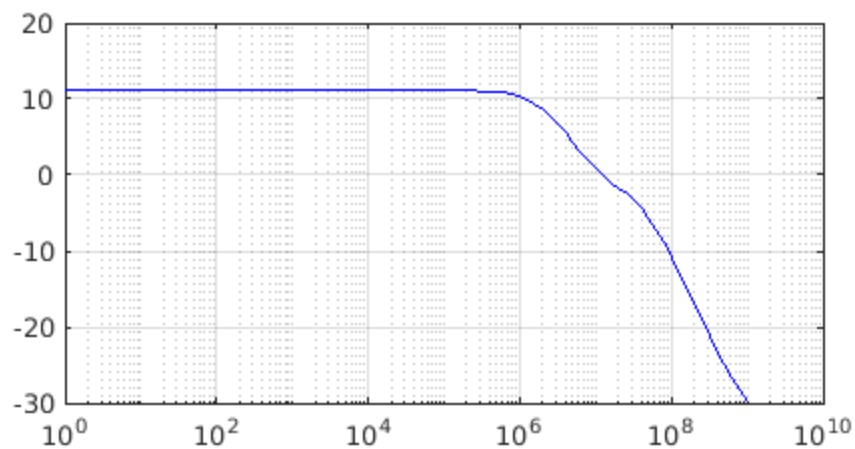


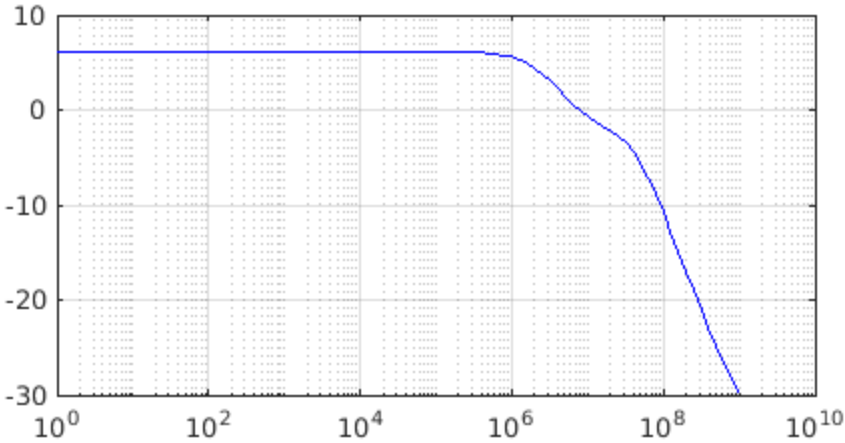
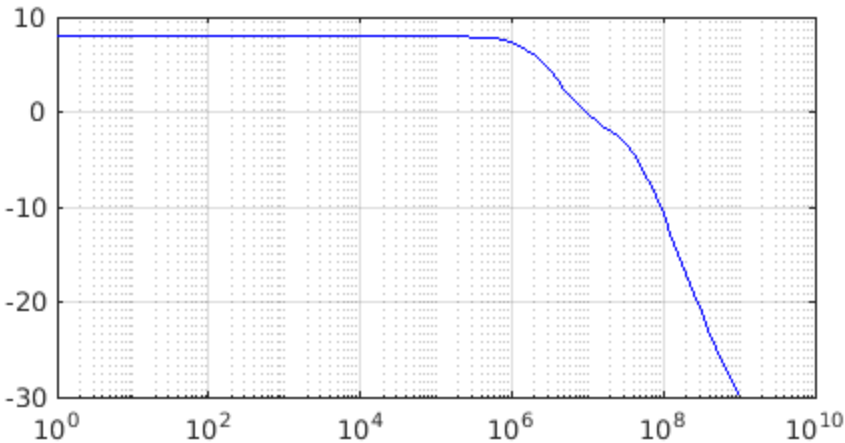


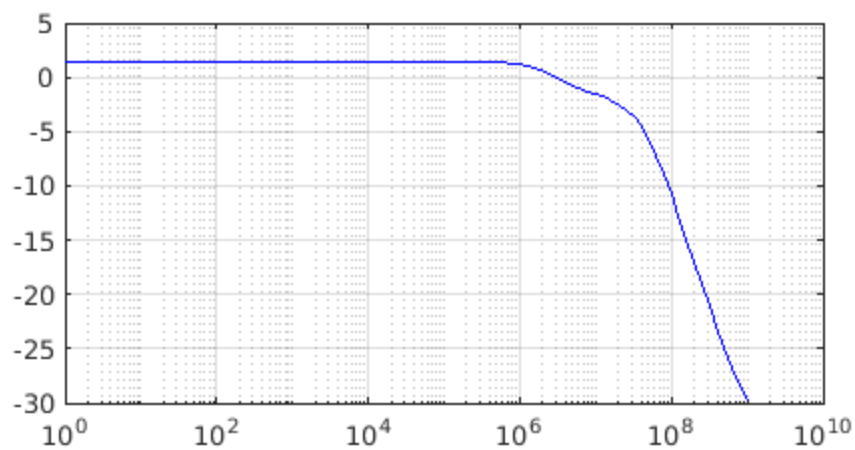
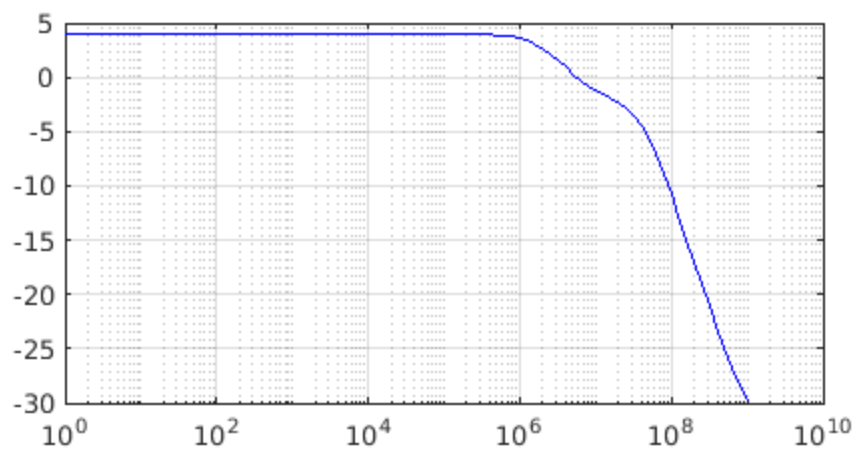


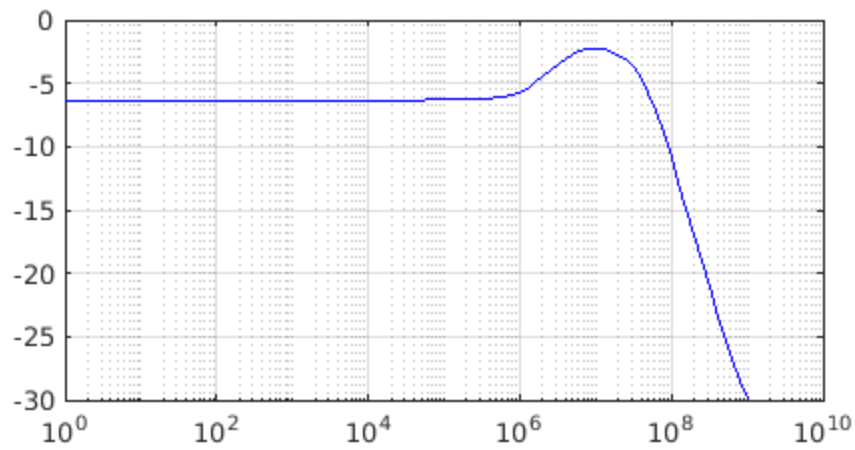
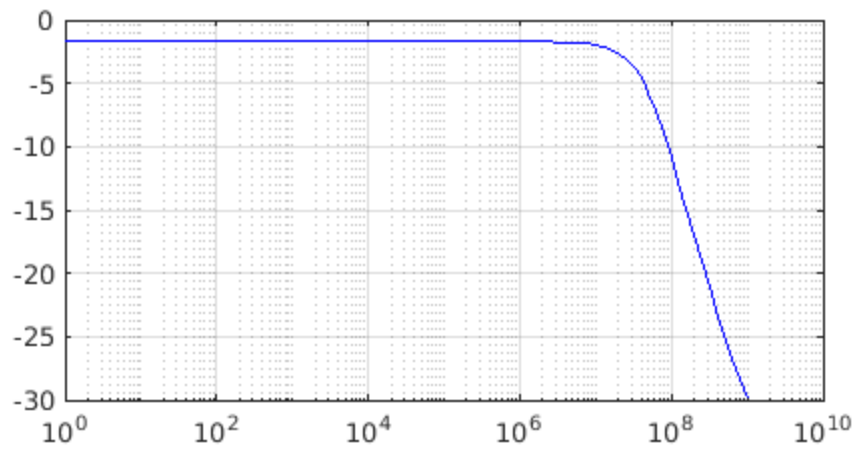


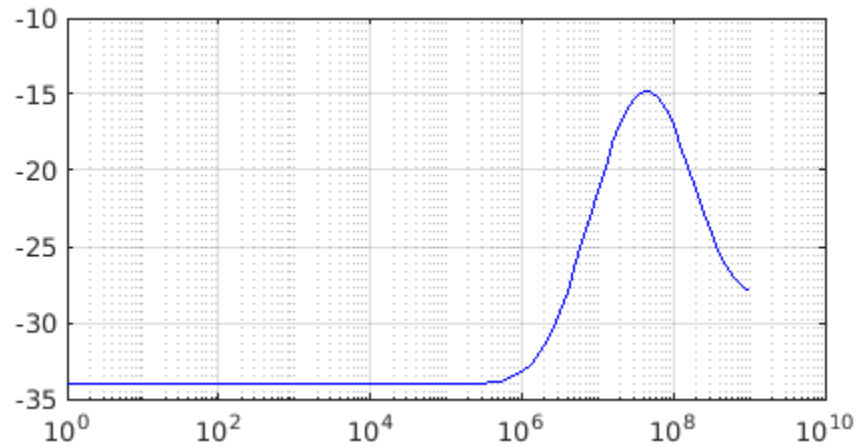
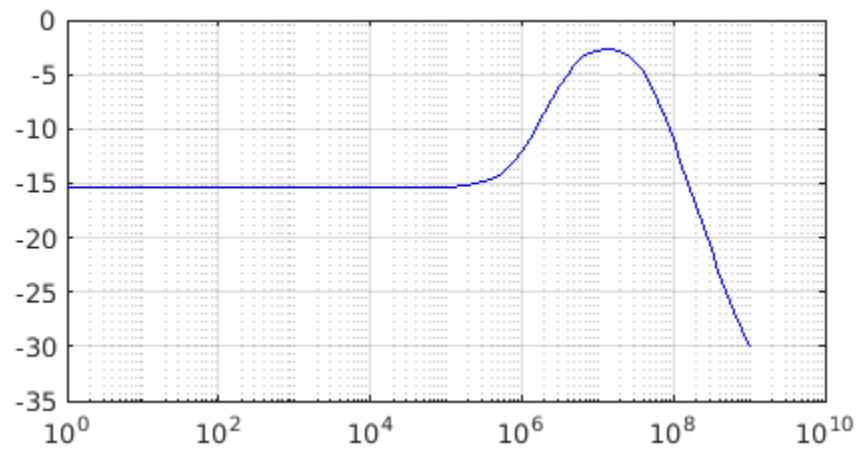




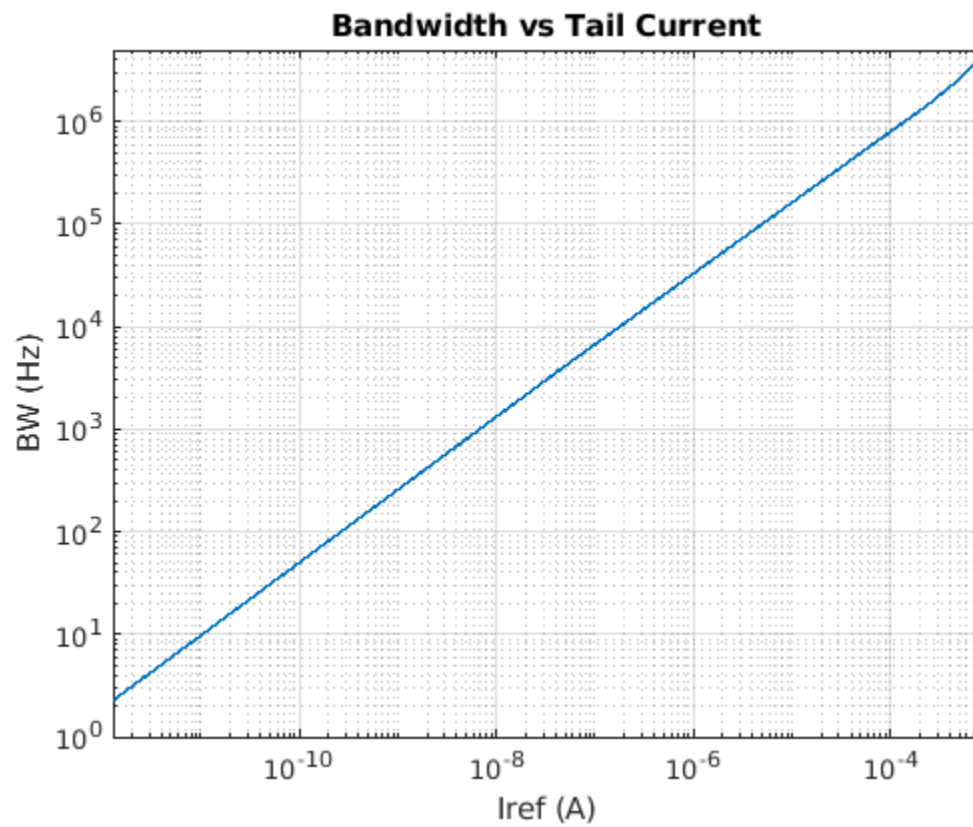


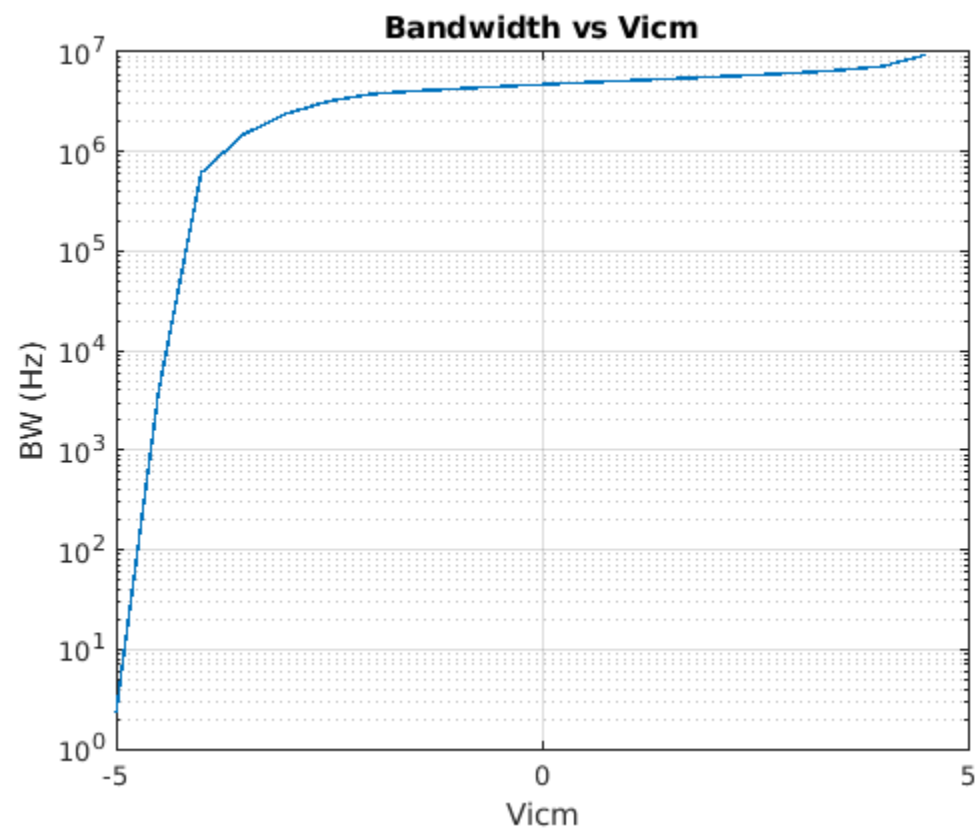


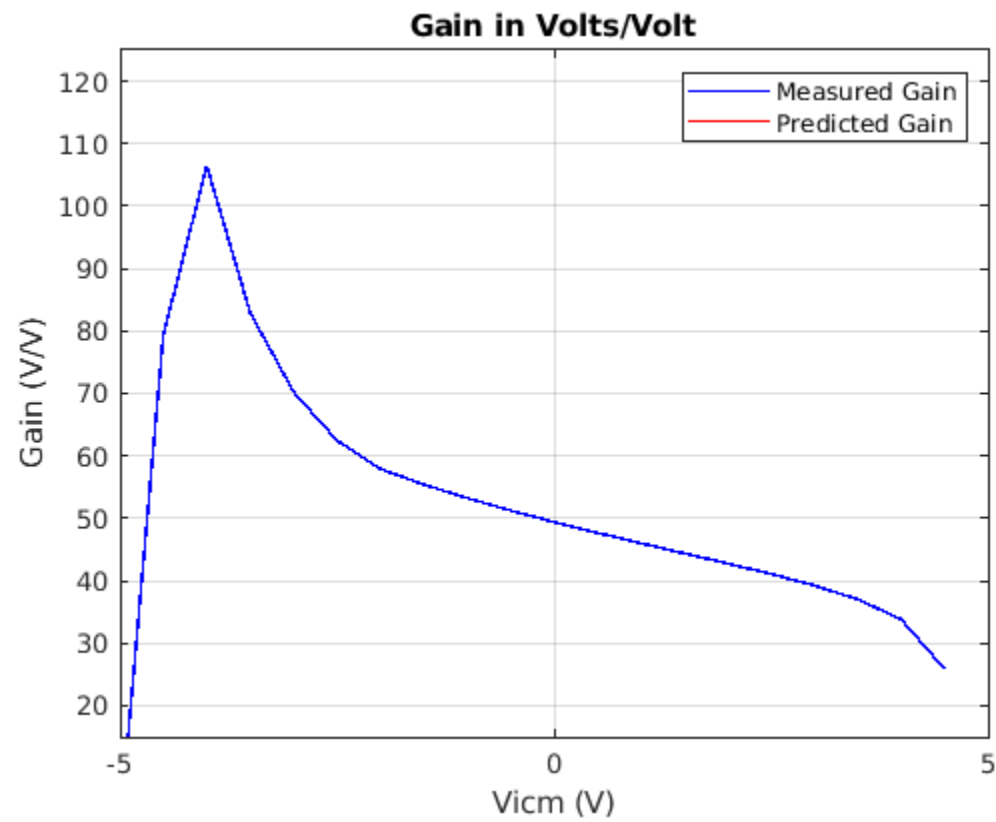


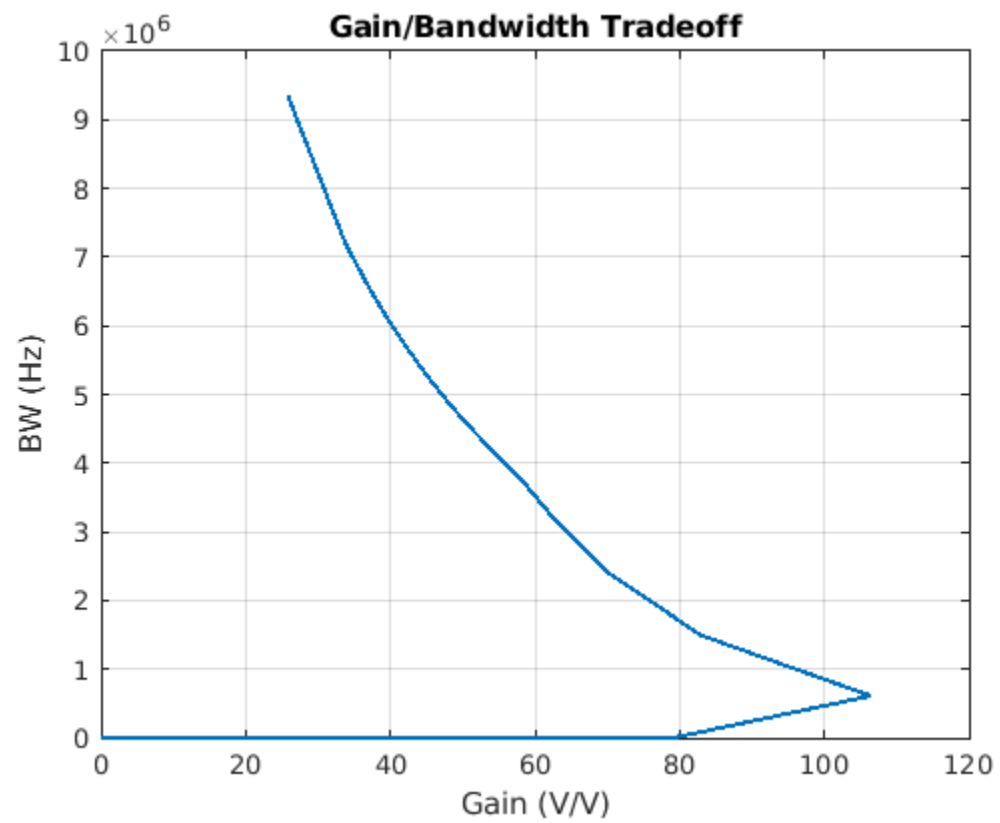


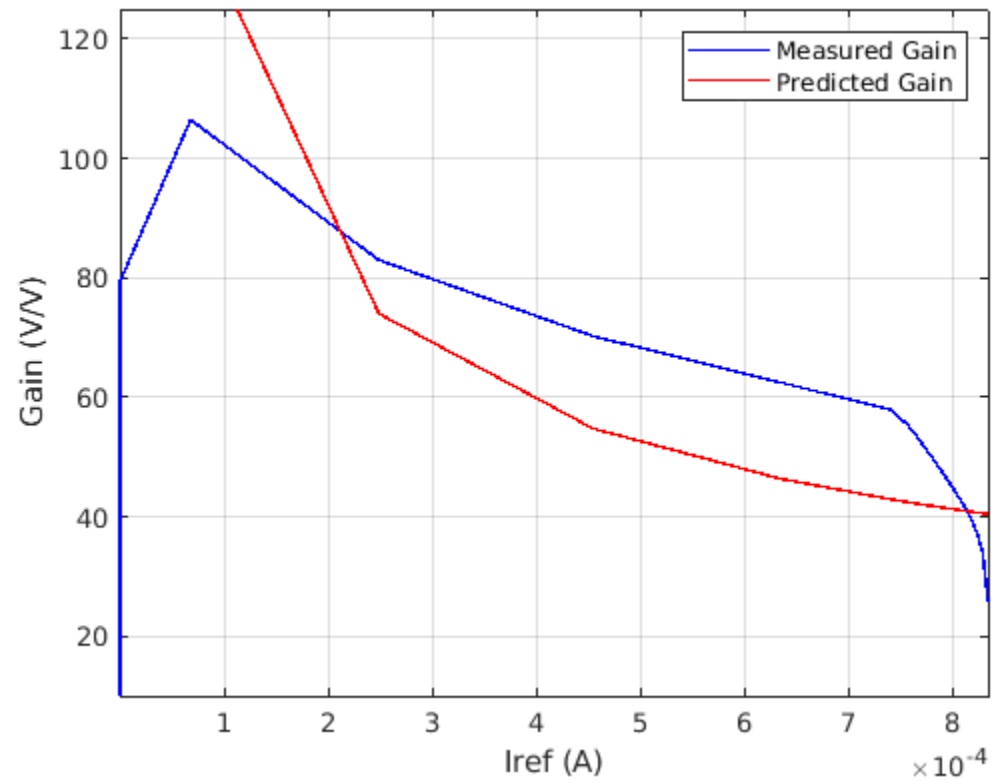
Plot Measurements:

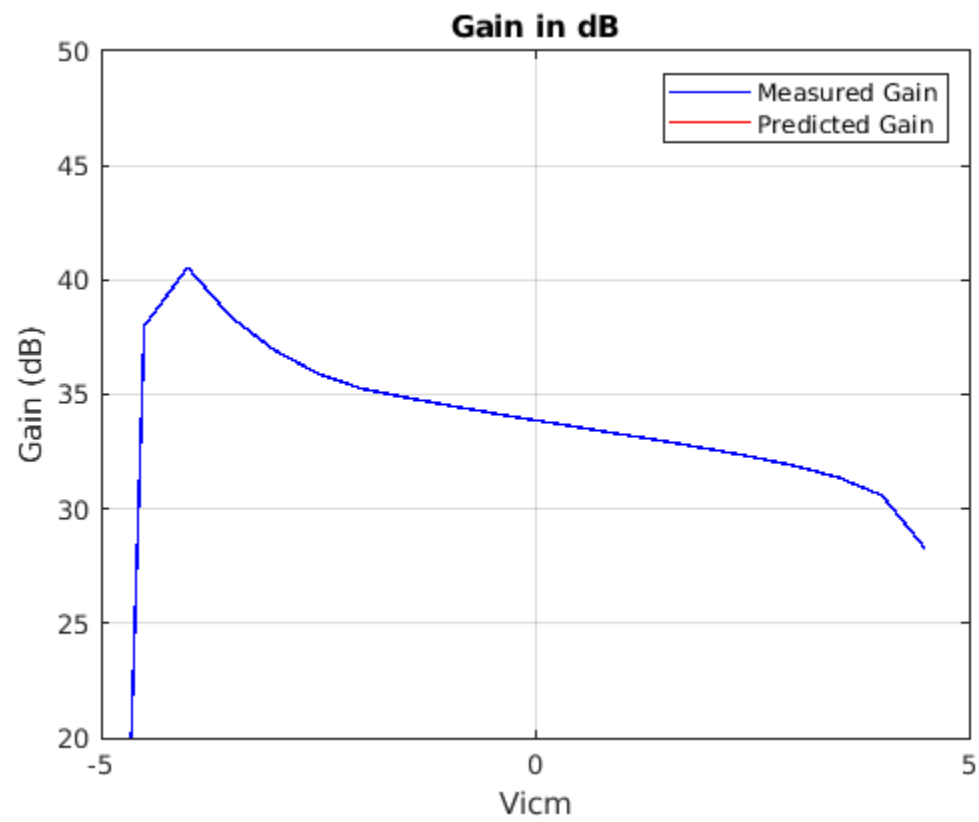


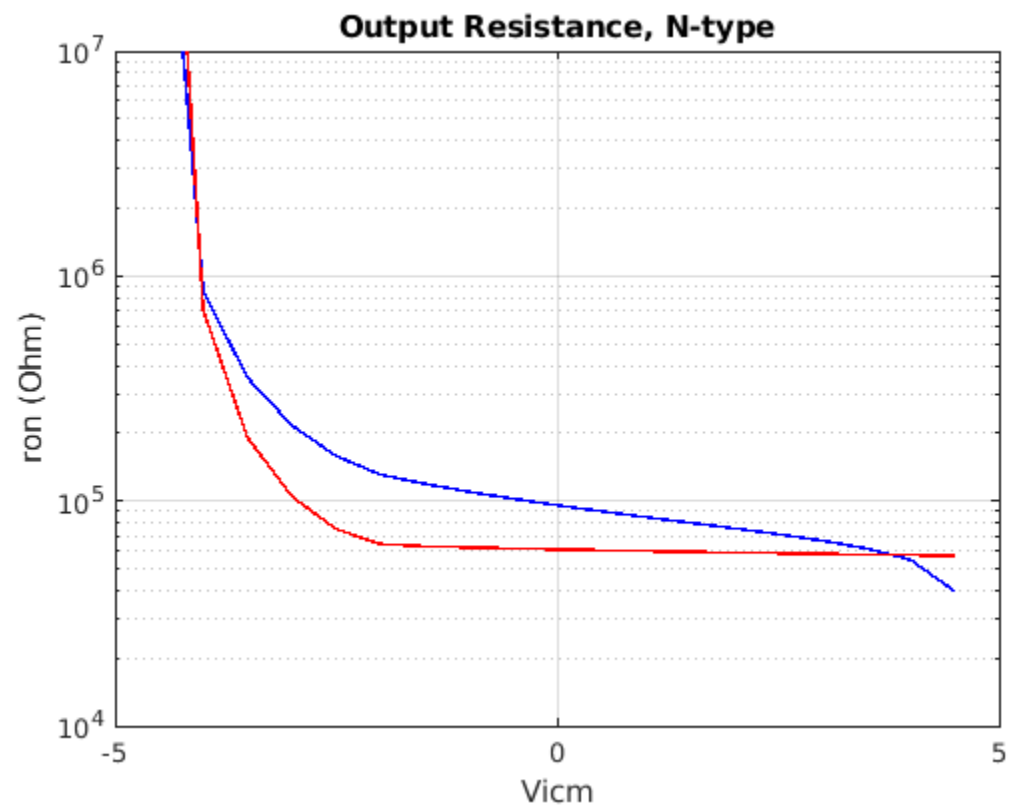


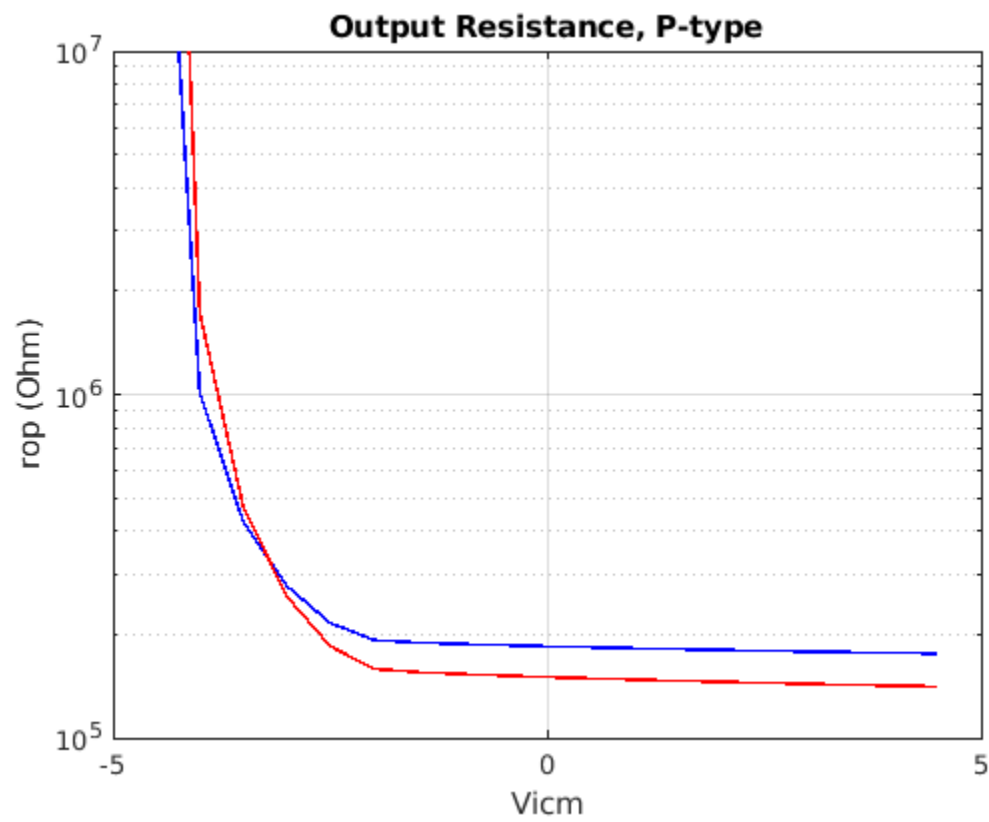


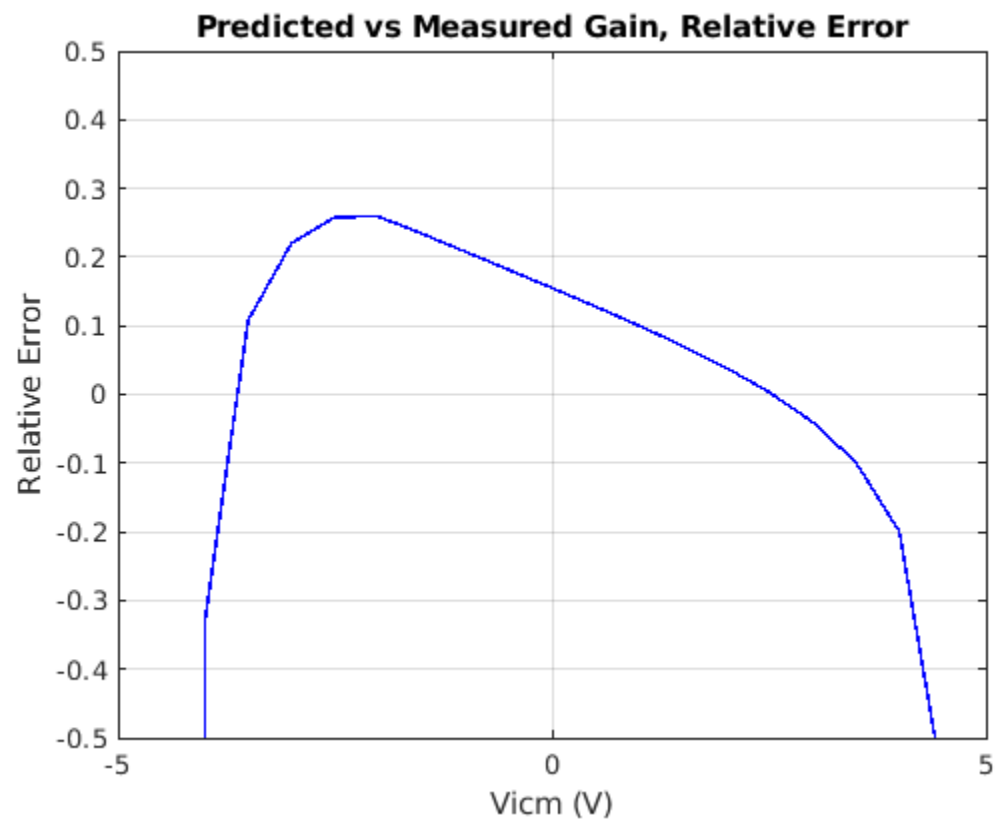


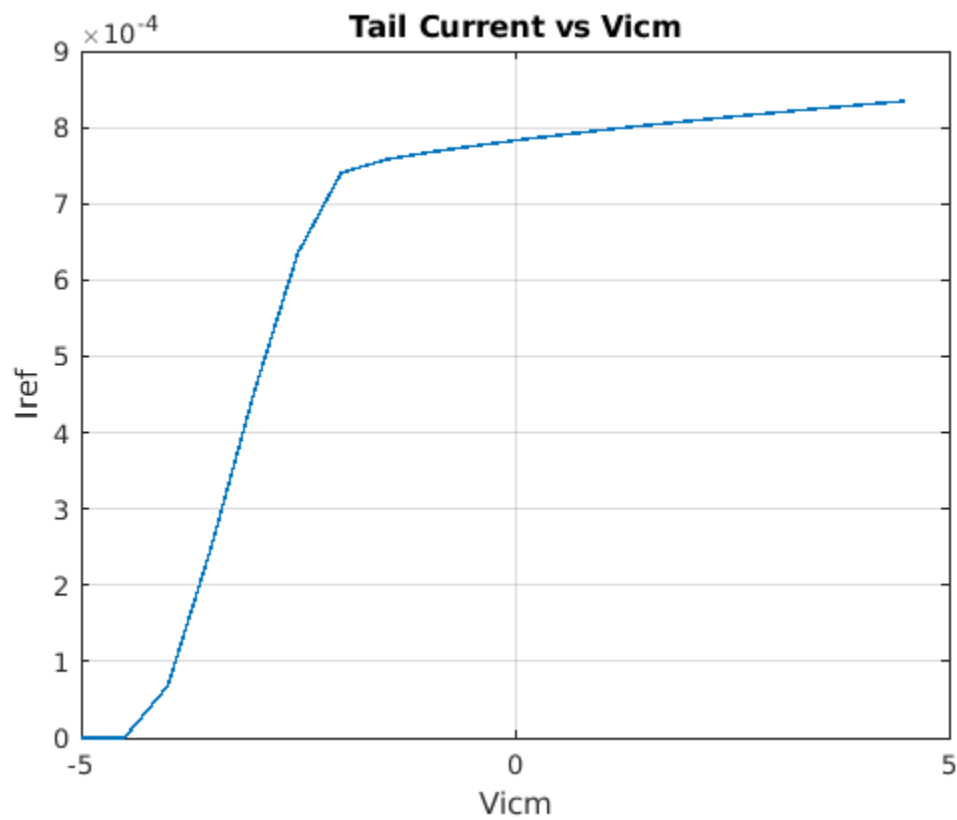


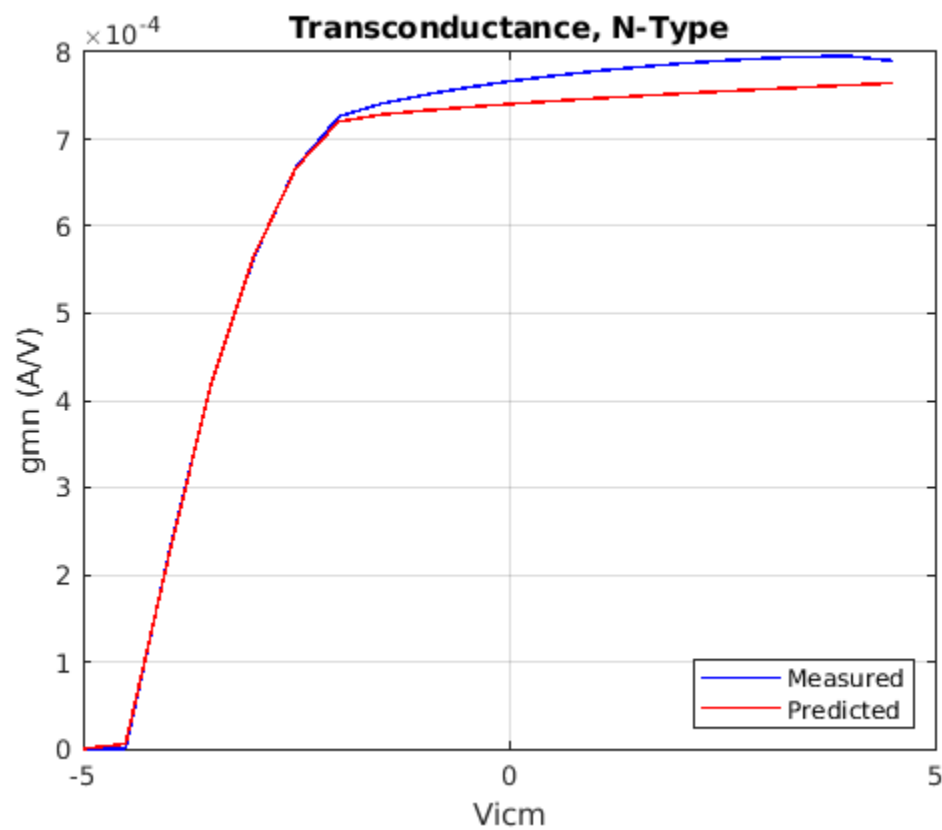


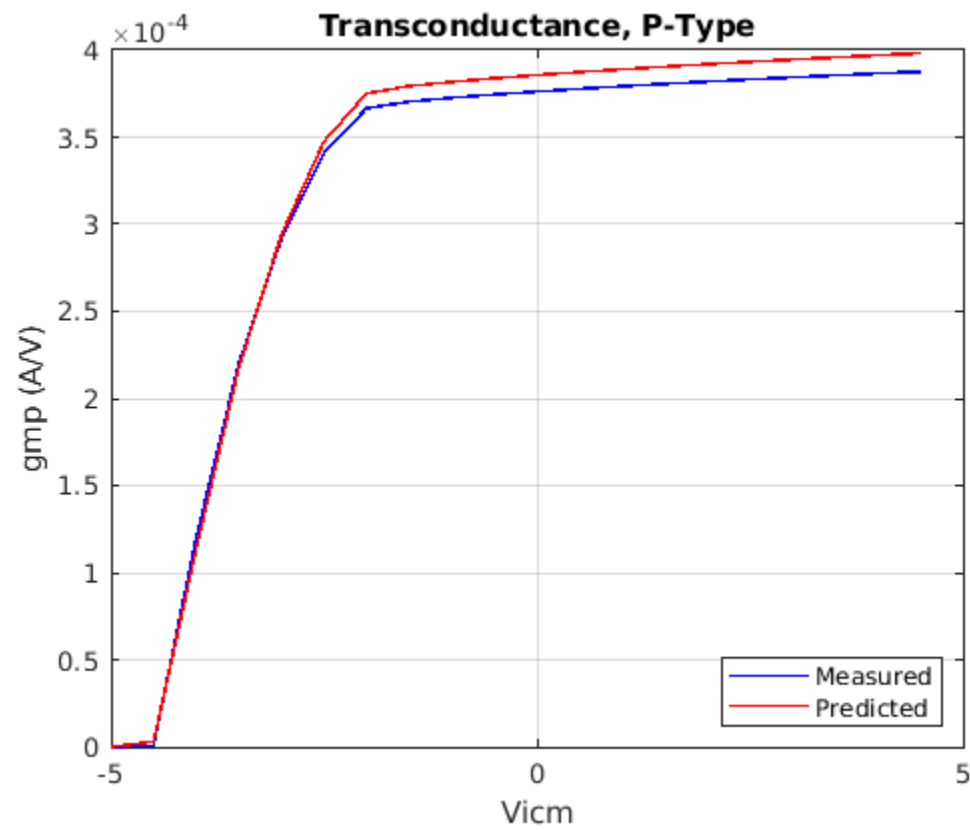




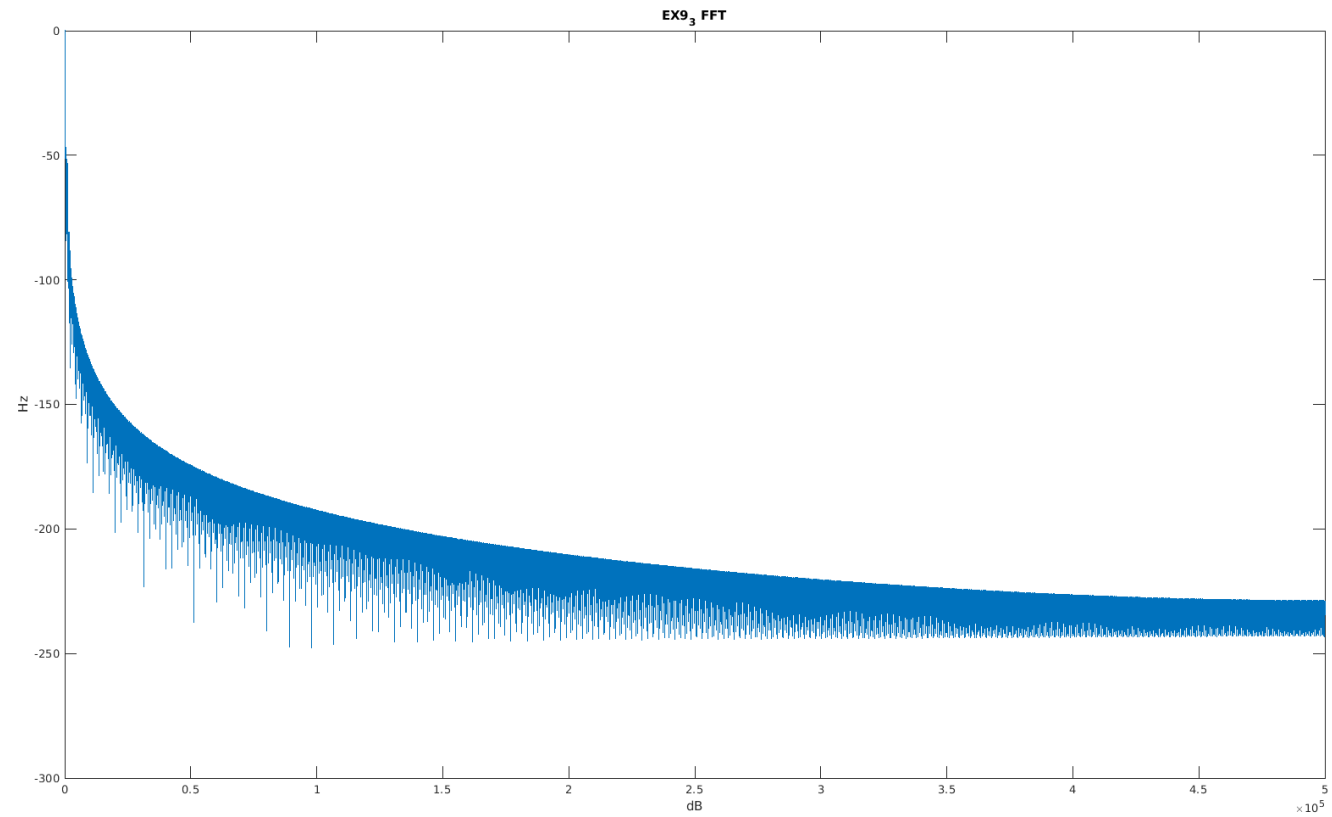




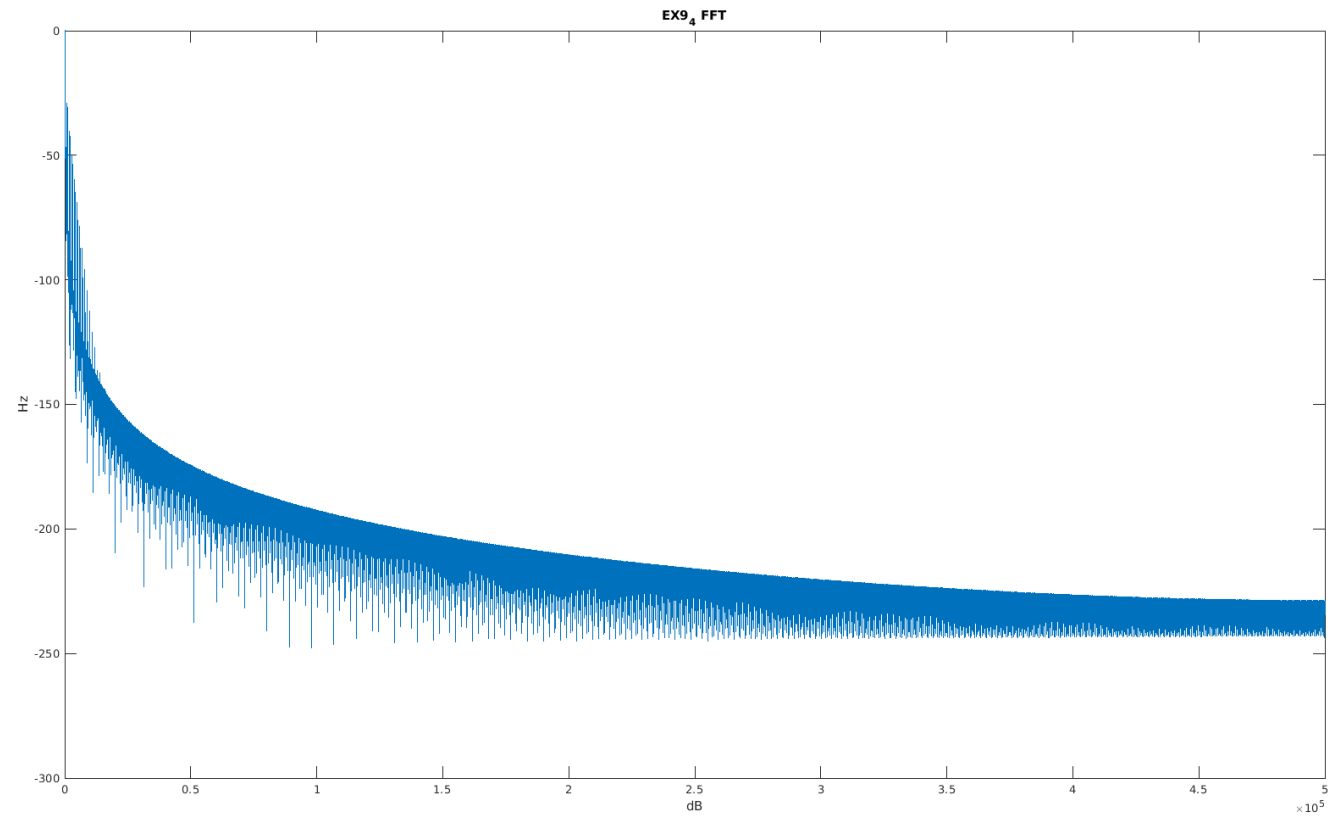




ex3.sp with the added resistors SNR: -62.5920



3x4.sp with the added resistors SNR: -62.5950



These results compare relatively well with what was predicted in problem 8, except for non-idealities of the OTA