

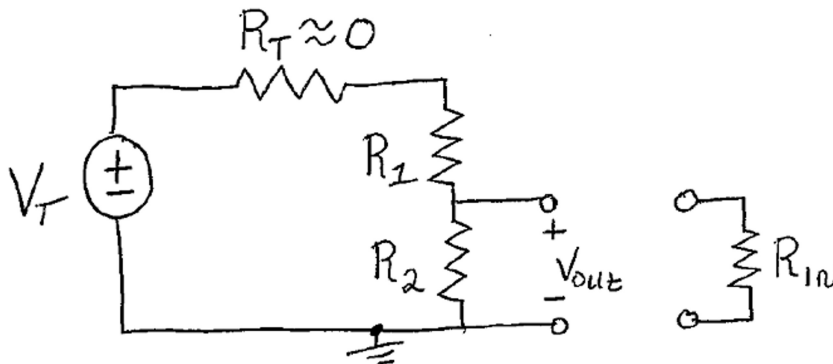
Homework 4

Friday, March 5, 2021 1:51 PM

"I pledge my honor I have abided by the Stevens Honor system."

- Alex J. Adams

1. A sensor has a Thevenin equivalent circuit with V_T and R_T . This sensor is connected to a two-resistor attenuator as shown below.



The output of this two-resistor attenuator (V_{out}) is to be connected to the input of a measuring instrument which has an input resistance given by R_{in} . This problem examines the design of the attenuator and the loading error in V_{out} due to the input resistance R_{in} . To simplify the analysis, we can assume that R_T is small and can be neglected in this problem. Thus, for this problem, we can assume R_T is zero. The value of V_T is equal to 3 Volts.

- Attenuator Design:** Determine the values of R_1 and R_2 which will satisfy the following two requirements.
 - i) The current flowing through both R_1 and R_2 before connecting to R_{in} should be 0.01 ma. (Hint; use Ohm's Law).
 - ii) V_{out} before connecting to R_{in} should equal $(0.4) \cdot V_T$.

$$V_T = 3 \text{ V. } R_T \approx 0 \Omega$$

$$.4(3) = (.01 \times 10^{-3}) R_2$$

$$R_2 = 120,000 \Omega$$

$$V_T = I (R_1 + R_2)$$

$$3 = (.01 \times 10^{-3}) (R_1 + 120,000)$$

$$R_1 = 180,000 \Omega$$

- Determining the input resistance R_{in} :** Using the correct values for R_1 and R_2 from part (a) of this problem, determine the minimum value of R_{in} for a loading error of $(0.02) \cdot V_T$. (Hint; to simplify the analysis, I suggest you solve for " R_{eq} " first. Once you have solved for R_{eq} , you can solve for R_{in}).

$$.4V_T - .02V_T$$

$$1.4 - .06 = 1.34$$

$$R_{eq} = \frac{R_2 R_{in}}{R_2 + R_{in}}$$

$$\text{Loading Error} = V_{\text{Before}} - V_{\text{After}}$$

$$1.34 = V_{\text{Before}} - \frac{R_2}{R_{eq} + R_1} (V_T) \quad (3)$$

$$1.34 = 1.4 - \frac{R_{eq}}{R_{eq} + 180,000}$$

$$-.06 = - \frac{R_{eq}}{R_{eq} + 180,000}$$

negTH

$$\frac{-0.06}{3} = - \frac{R_{eq}}{R_{eq} + 180,000}$$

$$-0.02 R_{eq} - 3,600 = -R_{eq}$$

$$3,673.47 = \frac{(120,000) R_{in}}{120,000 + R_{in}}$$

$$R_{eq} = 3,673.47 \Omega$$

$$440,816,327 + 3,673.47 R_{in} = 120,000 R_{in}$$

$$116,326.53 R_{in} = 440,816,327$$

$$R_{in} = 3,789.47 \Omega$$

2. Please refer to the two graphs on slide 61 in our Lecture Notes for Chapter Three. (The title of the slide is *Example 6.1*). The two graphs given on this slide are the graphs of the magnitude and phase of the transfer function for a filter.

- a. Is this filter an active or a passive filter? Why?

This is an active filter because it also amplifies input voltages.

- b. Is this filter a high-pass, bandpass, or low-pass filter? Why?

This is a low-pass filter, for the values to the left of f_c are not 0 but they are 0 to the right.

- c. What is the cut-off (or corner) frequency of this filter?

$f_c \approx 2500 \text{ Hz}$, Above this value $H(f) = 0$.

- d. You are given the following input voltage. Determine the output voltage of the filter.

$$V_{in}(t) = (7.87) \cdot \cos(4000\pi t - 15.8^\circ)$$

$$7.87 \angle 15.8^\circ$$

$$\omega < 2000 \text{ Hz} : H(f) = 2 \text{ and } \angle H(f) = 60^\circ$$

$$f = 2000 \text{ Hz} ; H(f) = 2 \text{ and } \angle H(f) = 60^\circ$$

$$V_{out} = V_{in}(H_f) = 7.87 \angle 15.8^\circ \cdot 2 \angle 60^\circ = 15.74 \angle 75.8^\circ$$

$$V_{out} = 15.74 \cos(4000\pi t - 75.8^\circ)$$