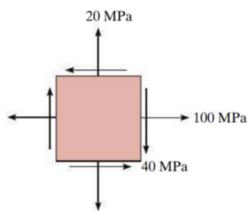


*- Alex Gaskins*

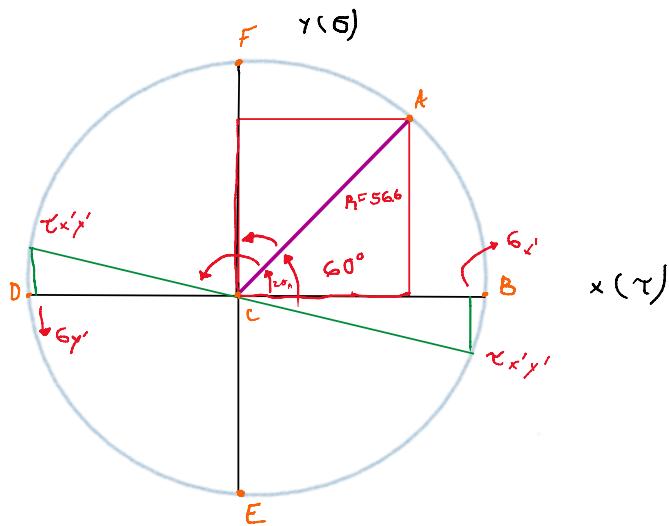
- 14-55.** Determine (a) the principal stresses and (b) the maximum in-plane shear stress and average normal stress. Sketch a properly oriented element for each case.



$$\sigma_x = 100 \text{ MPa}$$

$$\sigma_y = 20 \text{ MPa}$$

$$\tau_{xy} = -40 \text{ MPa}$$



$$\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2}$$

$$\sigma_{avg} = \frac{100 + 20}{2} = 60 \text{ MPa}$$

Center Point: (60, 0)

$$R = \sqrt{(\frac{\sigma_x - \sigma_y}{2})^2 + (\tau_{xy})^2}$$

$$R = \sqrt{(\frac{100 - 20}{2})^2 + (-40)^2}$$

$$R = 56.6 \text{ MPa}$$

A.)

Point B and D

$$\sigma_1 > \sigma_2$$

$$\sigma_1 = 60 + R = 60 + 56.6 = 116.6 \text{ MPa}$$

$$\sigma_2 = 60 - R = 60 - 56.6 = 3.4 \text{ MPa}$$

$\angle \theta_p = \text{Angle from } \overline{CA} \text{ to } \overline{CB} \text{ for } \sigma_p \text{ at } 1\sigma_1$

$$\angle \theta_p = \tan^{-1} \left( \frac{40}{100 - 60} \right)$$

$$\angle \theta_1 = \tan^{-1}(1)$$

$$\angle \theta_1 = 45^\circ$$

$$\theta_1 = 22.5^\circ$$

$\angle \theta_2 = \text{Angle from } CA \text{ to } CD$

$$\angle \theta_2 = 180 - \angle \theta_1$$

$$\theta_2 = 67.5^\circ$$

B.)

$$\sigma_{max}(\text{in-plane}) = \pm 56.6 \text{ MPa}$$

$\theta_3 = \text{Angle from } CA \text{ to } CF$

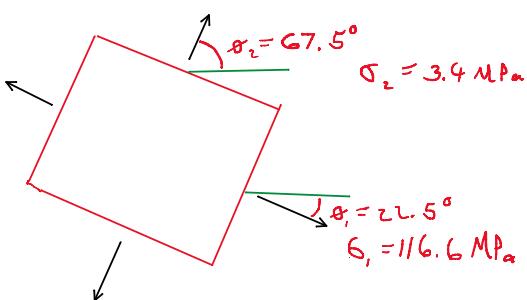
$$\angle \theta_3 = \tan^{-1}\left(\frac{100 - 60}{40}\right)$$

$$\angle \theta_3 = \tan^{-1}(1)$$

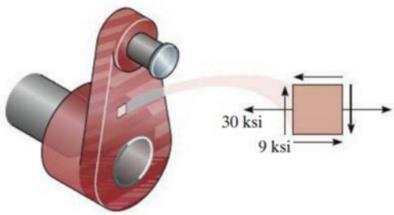
$$\angle \theta_3 = 45^\circ$$

$$\theta_3 = 22.5^\circ$$

$$\sigma_{avg} = 60 \text{ MPa} \text{ at center of circle}$$



- \*14-56. Determine (a) the principal stress and (b) the maximum in-plane shear stress and average normal stress. Sketch a properly oriented element for each case.



$$\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} = \frac{30 + 0}{2}$$

$$\sigma_{avg} = 15 \text{ ksi}$$

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$R = \sqrt{\left(\frac{30 - 0}{2}\right)^2 + (-9)^2}$$

$$R = \tau_{max} = \pm 17.5 \text{ ksi}$$

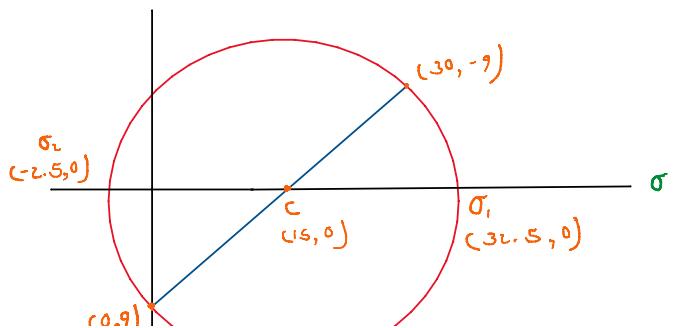
A.)  $\sigma_1 = \sigma_{avg} + R$        $\sigma_2 = \sigma_{avg} - R$   
 $\sigma_1 = 15 + 17.5$        $\sigma_2 = 15 - 17.5$   
 $\sigma_1 = 32.5 \text{ ksi}$        $\sigma_2 = -2.5 \text{ ksi}$

$$\tan(2\theta_1) = \frac{\tau_{xy}}{\left(\frac{\sigma_x - \sigma_y}{2}\right)}$$

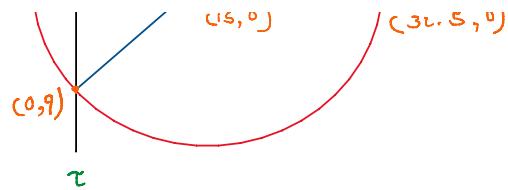
$$\tan(2\theta_1) = \frac{-9}{15}$$

$$\theta_1 = -15.5^\circ$$

B)  $\sigma_1 = 32.5 \text{ ksi}$        $\sigma_2 = -2.5 \text{ ksi}$



$$B.) \tan(2\theta_s) = \left( -\frac{\sigma_x - \sigma_y}{2\tau_{xy}} \right)$$



$$\tan(2\theta_s) = \left( -\frac{30 - 0}{2(-9)} \right)$$

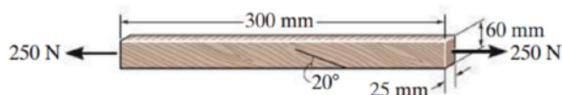
$$\theta_s = 29.5^\circ$$

$$\tau_{max(in-plane)} = \left( -\frac{\sigma_x - \sigma_y}{2} \right) \sin(2\theta_s) + \tau_{xy} \cos(2\theta_s)$$

$$\tau_{max(in-plane)} = \left( -\frac{30 - 0}{2} \right) \sin(2(29.5)) + (-9) \cos(2(29.5))$$

$$\tau_{max(in-plane)} = -17.5 \text{ ksi}$$

**14-61.** The grains of wood in the board make an angle of  $20^\circ$  with the horizontal as shown. Determine the normal and shear stresses that act perpendicular and parallel to the grains if the board is subjected to an axial load of 250 N.



$$\sigma = \frac{250}{(60)(25)}$$

$$\sigma = 166.67 \text{ kPa}$$

$$\theta = 90 - 20$$

$$\theta = 70^\circ$$

$$\sigma_x = \frac{\sigma_x + \sigma_y}{2} + \left( \frac{\sigma_x - \sigma_y}{2} \right) \cos(2\theta) + \tau_{xy} \sin(2\theta)$$

$$\sigma_x = \frac{166.67}{2} + \frac{166.67}{2} \cos(140) + 0$$

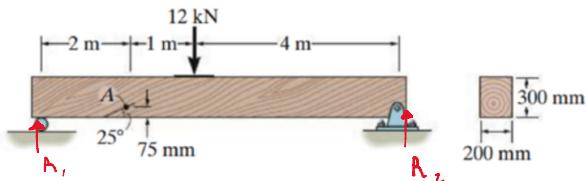
$\sigma_x = 19.50 \text{ kPa}$

$$\tau_x = \left( -\frac{\sigma_x - \sigma_y}{2} \right) \sin(2\theta) + \tau_{xy} \cos(2\theta)$$

$$\tau_x = -\frac{166.67}{2} \sin(140)$$

$\tau_x = -53.57 \text{ kPa}$

**14-23.** The wood beam is subjected to a load of 12 kN. If grains of wood in the beam at point A make an angle of  $25^\circ$  with the horizontal as shown, determine the normal and shear stress that act perpendicular and parallel to the grains due to the loading.



$$I = \frac{1}{12} b h^3$$

$$I = \frac{(200)(300)^3}{12}$$

$$I = 450 \times 10^6 \text{ mm}^4$$

$$\sum M_A = 0$$

$$R_1(7) - 12(4) = 0$$

$$R_1 = 6.857 \text{ kN.}$$

At point A:

$$6.857 - V_A = 0$$

$$V_A = 6.857 \text{ kN.}$$

$$\sum F_y = 0$$

$$R_2 + 6.857 - 12 = 0$$

$$R_2 = 5.143 \text{ kN.}$$

$$\sum M_A = 0$$

$$6.857(2) - M_A = 0$$

$$M_A = 13.714 \text{ kN}\cdot\text{m}$$

$$\sigma_A = \frac{M_A y_A}{I} = \frac{(13.714 \times 10^6)(75)}{(450 \times 10^6)}$$

$$\sigma_A = 2.2857 \text{ MPa}$$

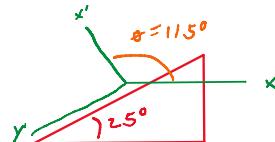
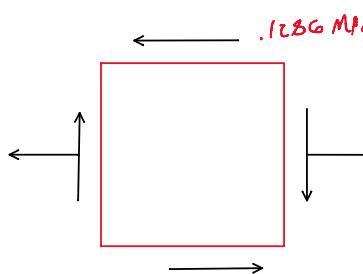
$$Q = A_y = 200(75)(112.5)$$

$$Q = 1.685 \times 10^6 \text{ mm}^3$$

$$\tau_A = \frac{V_A Q_A}{I t}$$

$$\tau_A = \frac{(6.857 \times 10^3)(1.6875 \times 10^6)}{(450 \times 10^6)(200)}$$

$$\tau_A = .1286 \text{ MPa}$$



$$\sigma_{x'} = \left( \frac{\sigma_x + \sigma_y}{2} \right) + \left( \frac{\sigma_x - \sigma_y}{2} \right) \cos(2\theta) + \tau_{xy} \sin(2\theta)$$

$$\sigma_{x'} = \left( \frac{2.2857 + 0}{2} \right) + \left( \frac{2.2857 - 0}{2} \right) \cos(230) - .1286 \sin(230)$$

$$\boxed{\sigma_{x'} = .5068 \text{ MPa}}$$

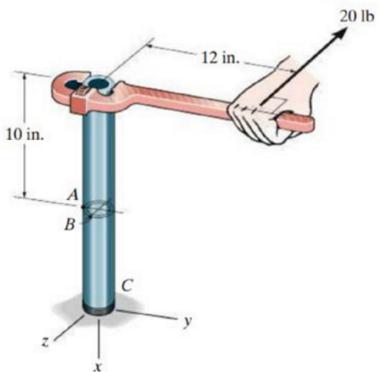
$$\sigma_{x'} = .5063 \text{ MPa}$$

$$\tau_{xy'} = -\left(\frac{\sigma_x - \sigma_y}{2}\right) \sin(2\theta) + \tau_{xy} \cos(2\theta)$$

$$\tau_{xy'} = -\left(\frac{2.2857 - 0}{2}\right) \sin(230) - .1286 \cos(230)$$

$$\tau_{xy'} = .9582 \text{ MPa}$$

**R14-1.** The steel pipe has an inner diameter of 2.75 in. and an outer diameter of 3 in. If it is fixed at C and subjected to the horizontal 20-lb force acting on the handle of the pipe wrench, determine the principal stresses in the pipe at point A, which is located on the surface of the pipe.



$$(Q_A)_z = \bar{\epsilon}_{y'} A'$$

$$(Q_k)_z = \frac{4(1.5)}{3\pi} \left[ \frac{1}{2} \pi (1.5)^2 \right] - \frac{4(1.375)}{3\pi} \left[ \frac{1}{2} \pi (1.375)^2 \right]$$

$$(Q_k)_z = .51693 \text{ in.}^3$$

$$I = \frac{\pi}{4} (1.5^4 - 1.375^4) = 1.1687 \text{ in.}^4$$

$$J = \frac{\pi}{2} (1.5^4 - 1.375^4) = 2.3374 \text{ in.}^4$$

$$\sigma_A = \frac{M_y z}{I_y}$$

$$\tau_k = \frac{20(.51693)}{1.1687(2)(1.25)} - \frac{240(1.5)}{2.3374}$$

$$\sigma_k = \frac{200(0)}{1.1687}$$

$$\tau_k = -118.6 \text{ psi}$$

$$\sigma_k = 0$$

$$\sigma_{\text{in-plane}} = \frac{\sigma_x + \sigma_z}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_z}{2}\right)^2 + \tau_k^2}$$

$$\sigma_{\text{in-plane}} = 0 \pm \sqrt{0 + (-118.6)^2}$$

$$\sigma_B = \frac{200(1.5)}{1.1687}$$

$$\sigma_1 = 118.6 \text{ psi} \quad \sigma_2 = -118.6 \text{ psi}$$

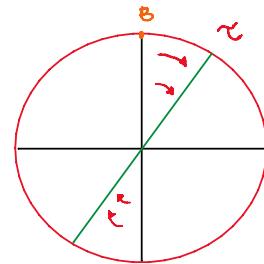
$$\sigma_B = \frac{200(1.5)}{1.1687}$$

$$\sigma_1 = 118.6 \text{ psi} \quad \sigma_2 = -118.6 \text{ psi}$$

$$\sigma_B = 256.7 \text{ psi}$$

$$\tau_B = \frac{240(1.5)}{2.3374}$$

$$\tau_B = 154 \text{ psi}$$



$$\sigma_p = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\sigma_p = \frac{256.7 + 0}{2} \pm \sqrt{\left(\frac{256.7 - 0}{2}\right)^2 + (-154)^2}$$

$$\sigma_{p1} = 329 \text{ psi} \quad \sigma_{p2} = -72.1 \text{ psi}$$