#### 4-1

$$T_{\infty} = T_m + A_m \sin \omega \tau$$

Energy balance: 
$$q = hA(T - T_{\infty}) = \rho cV \left(\frac{dT}{d\tau}\right)$$

Let  $K = \frac{hA}{\rho cV}$  along with initial condition  $T = T_0$  at  $\tau = 0$ ;

Solution is:

$$T - T_m = (T_0 - T_m)e^{-K\tau} + \left(\frac{KA_m}{\omega^2 + K^2}\right)[\omega(e^{-K\tau} - \cos\omega\tau) + K\sin\omega\tau]$$

#### 4-2

$$\alpha = 1.8 \times 10^{-6} \text{ m}^2/\text{sec}$$

$$2L = 2.5 \text{ cm}$$

$$T_i = 150^{\circ}\text{C}$$
  $T_1 = 30^{\circ}\text{C}$ 

$$\tau = 1 \text{ min} = 60 \text{ sec}$$

$$\tau = 1 \text{ min} = 60 \text{ sec}$$
 
$$\frac{\pi x}{2L} = \frac{\pi}{2}; \left(\frac{\pi}{2L}\right)^2 \alpha \tau = 1.705$$

$$\frac{T - T_1}{T_i - T_1} = \frac{4}{\pi} [0.1818 - 7.22 \times 10^{-8} + 6.15 \times 10^{28}] = 0.231$$

$$T = 30 + (0.231)(150 - 30) = 57.8$$
°C  $\frac{\alpha \tau}{L^2} = 0.69$   $\frac{\theta_0}{\theta_i} = 0.25$ 

$$\frac{\alpha \tau}{L^2} = 0.69 \qquad \frac{\theta_0}{\theta_i} = 0.25$$

### 4-3

at 
$$\tau = 0$$
 
$$\frac{x}{2L} = \frac{1}{2}$$
 
$$\frac{\pi x}{2L} = \frac{\pi}{2}$$
 
$$\frac{T - T_1}{T_i - T_1} = \frac{4}{\pi} \left( \sin \frac{\pi}{2} + \frac{1}{3} \sin \frac{3\pi}{2} + \frac{1}{5} \sin \frac{5\pi}{2} + \frac{1}{7} \sin \frac{7\pi}{2} \right) = 0.9216$$
 correct value is 1.0 Error = 7.84%

$$q = \sigma A(T^4 - T_{\infty}^4) + hA(T - T_{\infty}) = -c\rho V \frac{dT}{d\tau}$$

$$T_0 = 250^{\circ}\text{C} \qquad T = 90^{\circ}\text{C} \qquad T_{\infty} = 35^{\circ}\text{C}$$

$$R_{th} = \frac{1}{2} \left( \frac{\Delta x}{kA} \right) = \left( \frac{1}{2} \right) \left[ \frac{0.05}{(0.2)^2 (370)} \right] = 1.69 \times 10^{-3}$$

$$C_{th} = \rho c V = (8900)(380)(0.05)(0.2)^2 = 6764$$

$$\frac{1}{R_{th}C_{th}} = 0.0875$$

$$\frac{T - T_{\infty}}{T_0 - T_{\infty}} = \exp(-0.0875\tau) = \frac{90 - 35}{250 - 35} = 0.2558$$

$$\tau = 15.58 \text{ sec}$$

$$m = \rho V$$
  $\rho = 2707 \text{ kg/m}^3$   $c = 896 \frac{J}{\text{kg} \cdot ^{\circ}\text{C}}$   $h = 58$   
 $\frac{4}{3}\pi r^3(2700) = 6$   $r = 0.0807 \text{ m}$   
 $A = 4\pi r^2 = 0.0822 \text{ m}^2$   
 $\frac{hA}{\rho cV} = \frac{(58)(0.0822)}{(6)(896)} = 8.87 \times 10^{-4}$   
 $\frac{90 - 20}{300 - 20} = \exp(-8.87 \times 10^{-4}\tau) = 0.25$   
 $\tau = 1563 \text{ sec}$ 

#### 4-9

$$\frac{q}{A} = \sigma \varepsilon (T^4 - T_s^4) = -\rho c (2L) \frac{dT}{d\tau}$$

$$\frac{dT}{T_s^4 - T^4} = \frac{\sigma \varepsilon}{2\rho cL} d\tau$$

$$\int_{T_i}^T \frac{dT}{T_s^4 - T^4} = \left[ \frac{1}{4T_s^3} \log \left| \frac{T_s + T}{T_s - T} \right| + \frac{1}{2T_s^3} \tan^{-1} \left( \frac{T}{T_s} \right) \right]_{T_i}^T \tag{a}$$

$$\int_0^\tau \frac{\sigma \varepsilon d\tau}{2\rho cL} = \frac{\sigma \varepsilon \tau}{2\rho cL} \tag{b}$$

Setting (a) = (b) produces an equation for T as a function of  $\tau$ . For specific problems the answer is more easily obtained with numerical methods.

#### 4-10

$$T_0 = 25^{\circ}\text{C}$$
  $T_{\infty} = 150^{\circ}\text{C}$   $h = 120 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $T = 120^{\circ}\text{C}$ 

$$\rho = 7817 \quad c = 460 \quad d = 6.4 \text{ mm}$$

$$\frac{A}{V} = \frac{4}{d}$$

$$\frac{hA}{\rho cV} = \frac{(120)(4)}{(0.0064)(7817)(460)} = 0.02086$$

$$\frac{T - T_{\infty}}{T_0 - T_{\infty}} = \exp\left(-\frac{hA}{\rho cV}\tau\right)$$

$$\frac{120 - 25}{150 - 25} = 0.76 = e^{-0.02086\tau}$$

$$\tau = 13.16 \text{ sec}$$

### 4-11

$$T_{\infty} = 20^{\circ}\text{C}$$
  $T_{0} = 200^{\circ}\text{C}$   $h = 28$   $d = 5 \text{ cm}$   $T = 90^{\circ}\text{C}$   $\rho = 8954$   $c = 383$   $\frac{A}{V} = \frac{3}{r}$   $\frac{hA}{\rho cV} = \frac{(28)(3)}{(0.025)(8954)(383)} = 9.8 \times 10^{-4}$   $\frac{90 - 20}{200 - 20} = 0.3889 = e^{-9.8 \times 10^{-4}\tau}$   $\tau = 964 \text{ sec}$ 

### 4-13

Lumped Capacity 
$$\rho = 8954$$
  $c = 383$ 

$$\frac{hA}{\rho cV} = \frac{(15)(4\pi)(0.015)^2}{(8954)(383)\left[\frac{4}{3}\pi(0.015)^3\right]} = 8.75 \times 10^{-4}$$

$$\frac{25 - 10}{50 - 10} = e^{-8.75 \times 10^{-4}\tau}$$
  $\tau = 1121 \text{ sec}$ 

$$\rho = 2707 c = 896 \sigma A T^4 = -\rho c V \frac{dT}{d\tau} T \text{ in } ^\circ K$$

$$\frac{dT}{T^4} = \frac{-\sigma A}{\rho c V} d\tau \frac{1}{T^3} - \frac{1}{T_0^3} = \frac{\sigma A \tau}{\rho c V}$$

$$T = -240 + 273 = 33 \text{ K} T_0 = 40 + 273 = 313 \text{ K} \tau = 9.9 \times 10^6 \text{ sec}$$

$$\rho = 999.8 c = 4225 L = 2d A = 2.5\pi d^2 V = \frac{1}{2}\pi d^3$$

$$d = 6.06 \text{ cm} A = 288.5 \text{ cm}^2$$

$$\frac{hA}{\rho cV} = \frac{(15)(288.5)(10^{-4})}{(999.8)(4225)(350)(10^{-6})} = 2.927 \times 10^{-4}$$

$$\frac{15 - 20}{1 - 20} = e^{-2.927 \times 10^{-4}\tau} \tau = 456 \text{ sec}$$

#### 4-16

$$\frac{h(V/A)}{k} = \frac{(10)(0.006)}{(3)(204)} = 9.8 \times 10^{-5}$$
lumped capacity  $\rho = 2707$   $c = 896$ 

$$\frac{200 - 20}{400 - 20} = e^{-\left[\frac{(10)(3)\tau}{(0.006)(896)(2707)}\right]} = 0.4737$$
  $\tau = 362$  sec

#### 4-17

$$\frac{h(V/A)}{k} = \frac{hV}{3k} = \frac{(20)(0.02)}{(3)(380)} = 3.5 \times 10^{-4}$$
lumped capacity  $c = 383$   $\rho = 8954$ 

$$\frac{80 - 30}{220 - 30} = e^{-\left[\frac{(20)(3)\tau}{(0.02)(383)(8954)}\right]} = 0.263 \quad \tau = 1494 \text{ sec}$$

$$A = \frac{90 - 35}{2} = 27.5^{\circ}\text{C} \qquad x = 5 \text{ cm} = 0.05 \text{ m} \qquad k = 1.37 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$$

$$a = 7 \times 10^{-7} \text{ m}^{2}/\text{sec} \qquad n = \frac{1 \text{ cyc}}{15 \text{ min}} = 1.1111 \times 10^{-3} \text{ cyc/sec}$$

$$x = \sqrt{\frac{\pi n}{\alpha}} = 0.05 \left[ \frac{\pi (1.1111 \times 10^{-3})}{7 \times 10^{-7}} \right]^{1/2} = 3.531$$

$$2n\pi\tau = 2\pi (1.1111 \times 10^{-3})(2)(3600) = 50.26$$

$$2\pi n\tau - x\sqrt{\frac{\pi n}{\alpha}} = 46.734 \text{ radians} = 2677.66^{\circ}$$

$$\cos(2677.66) = -0.925 \qquad \sin(2677.66) = 0.3801$$

$$\frac{q}{A} = kAe^{-x\sqrt{\frac{\pi n}{\alpha}}} \left( \sqrt{\frac{\pi n}{\alpha}} \right) [\cos(2677.66) + \sin(2677.66)]$$

$$\frac{q}{A} = (1.37)(27.5)(e^{-3.531})(-0.925 + 0.3801) = -0.601 \text{ W/m}^{2}$$

#### 4-19

Maximum points when sine function is max, i.e.:

$$2\pi n\tau - x\sqrt{\frac{\pi n}{\alpha}} = \frac{\pi}{2} \quad \text{at } x = 0 \qquad \tau = \frac{\pi}{4\pi n} = \frac{1}{4n}$$

$$\text{at } x = x_1 \qquad \tau = \frac{\pi}{4\pi n} + \frac{x\sqrt{\frac{\pi n}{\alpha}}}{2\pi n} = \frac{1}{4n} + \frac{x}{2}\sqrt{\frac{1}{\pi \cos n}}$$

$$\Delta \tau = \frac{x}{2}\sqrt{\frac{1}{\pi \cos n}}$$

#### 4-20

$$T_{i} = 54^{\circ}\text{C} \qquad T_{\infty} = 10^{\circ}\text{C} \qquad h = 10 \frac{\text{W}}{\text{m}^{2} \cdot {}^{\circ}\text{C}} \qquad x = 7 \text{ cm} \qquad \tau = 30 \text{ min}$$

$$\alpha = 7 \times 10^{-7} \text{ m}^{2}/\text{sec} \qquad k = 1.37 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$$

$$\frac{x}{2\sqrt{\alpha \tau}} = \frac{0.07}{2[(7 \times 10^{-7})(30)(60)]^{1/2}} = 0.986 \qquad \frac{T - T_{i}}{T_{\infty} - T_{i}} = 0.021$$

$$\frac{h\sqrt{\alpha \tau}}{k} = \frac{(10)[(7.7 \times 10^{-7})(30)(60)]^{1/2}}{1.37} = 0.258 \qquad T = 53.08^{\circ}\text{C}$$

#### 4-21

$$T_i = 300^{\circ}\text{C}$$
  $T_0 = 35^{\circ}\text{C}$   $x = 7.5 \text{ cm}$   $\tau = 4 \text{ min} = 240 \text{ sec}$   
 $\alpha = 11.23 \times 10^{-5} \text{ m}^2/\text{s}$   
 $X = \frac{x}{2\sqrt{\alpha\tau}} = \frac{0.075}{2[(11.23 \times 10^{-5})(240)]^{1/2}} = 0.2284$   
erf  $X = 0.2533 = \frac{T - T_0}{T_1 - T_0}$   $T = 102.1^{\circ}\text{C}$ 

$$\alpha = 7 \times 10^{-7} \text{ m}^2/\text{s}$$
  $T_i = 55^{\circ}\text{C}$   $T_0 = 15^{\circ}\text{C}$   $T = 25^{\circ}\text{C}$   
 $x = 5 \text{ cm}$   $\frac{T - T_0}{T_i - T_0} = \frac{25 - 15}{55 - 15} = 0.25 = \text{erf } X$   $X = 0.2253 = \frac{x}{2\sqrt{\alpha\tau}}$   
 $\tau = 17,589 \text{ sec} = 4.89 \text{ hr}$ 

$$\frac{q_0}{A} = 0.5 \times 10^6 \text{ W/m}^2 \qquad \tau = 300 \text{ s} \qquad T_i = 20^{\circ}\text{C} \qquad k = 386$$

$$\alpha = 11.23 \times 10^{-5} \text{ m}^2/\text{s}$$

$$\frac{x = 0}{x} = 0$$

$$T = 20 + \frac{(2)(0.5 \times 10^6) \left[ \frac{(11.23 \times 10^{-5})(300)}{\pi} \right]^{1/2}}{386} e^0 = 288.3^{\circ}\text{C}$$

$$\frac{x = 15 \text{ cm}}{X = \frac{x}{2\sqrt{\alpha \tau}}} = \frac{0.15}{2[(11.23 \times 10^{-5})(300)]^{1/2}} = 0.4086$$

$$\frac{x^2}{4\alpha \tau} = 0.167 \qquad \text{erf } X = 0.4173$$

$$T - T_i = \frac{2(0.5 \times 10^6) \left[ \frac{(11.23 \times 10^{-5})(300)}{\pi} \right]^{1/2}}{10.23 \times 10^{-5} \times 10^{-5}} e^{-0.167} - \frac{(0.5 \times 10^6)(0.15)}{386} (1 - 0.4173)$$

$$= 113.8$$

$$T = 133.8^{\circ}\text{C}$$

**4-24** All cases remain at 20°C because  $x/2(\alpha\tau)^{1/2}$  is so large.

$$T_i = 90^{\circ}\text{C}$$
  $T_0 = 30^{\circ}\text{C}$   $x = 7.5 \text{ cm}$   $\tau = 10 \text{ sec}$   $k = 386 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$ 

$$\frac{q}{A} = \frac{-k(T_i - T_0)}{\sqrt{\pi \alpha \tau}} e^{\frac{-\chi^2}{4\alpha \tau}}$$

$$\frac{q}{A} = \frac{(-386)(90 - 30)}{[\pi(11.23 \times 10^{-5})(10)]^{1/2}} \exp\left[\frac{-(0.075)^2}{4(11.23 \times 10^{-5})(10)}\right] = -111.3 \text{ kW/m}^2$$

### 4-27

$$T_i = 30^{\circ}\text{C}$$
  $\frac{q_0}{A} = 15,000 \text{ W/m}^2$   $x = 2.5 \text{ cm}$   $\tau = 120 \text{ sec}$   
 $k = 204$   $\alpha = 8.42 \times 10^{-5}$   
 $T - T_i = \frac{15,000}{204} \left\{ 2 \left[ \frac{(8.42 \times 10^{-5})(120)}{\pi} \right]^{1/2} \exp \left[ \frac{-(0.025)^2}{4(8.42 \times 10^{-5})(120)} \right] - (0.025) \left[ 1 - \text{erf} \left( \frac{0.025}{2\sqrt{8.42 \times 10^{-5}(120)}} \right) \right] \right\}$   
 $= 6.59$   
 $T = 36.59^{\circ}\text{C}$ 

#### 4-30

$$\frac{h(V/A)}{k} = \frac{h(r/3)}{k} = \frac{(78)\left(\frac{0.028}{3}\right)}{204} = 0.00357$$
Therefore: Lumped capacity  $\rho = 2707$ ,  $c = 896$ 

$$\frac{hA}{\rho cV} = \frac{3h}{r\rho c} = \frac{(3)(78)}{(0.028)(2707)(896)} = 0.00345$$

$$\frac{73 - 23}{355 - 23} = e^{-0.00345\tau}$$

#### 4-31

 $\tau = 549 \text{ sec}$ 

$$\frac{T - T_0}{T_i - T_0} = \frac{-1 - (-1)}{-20 - (-1)} = 0.5263 = \text{erf } \frac{x}{2\sqrt{\alpha \tau}}$$

$$\frac{x}{2\sqrt{\alpha \tau}} = 0.5267$$

$$\tau = \frac{1}{0.048} \left[ \frac{(0.015)(3.2808)}{2(0.5267)} \right]^2 = 0.04547 \text{ hr} = 163.7 \text{ sec}$$

$$\frac{q}{A} = 900 \text{ W/m}^2 \qquad T_i = 20^{\circ}\text{C} \qquad x = 10 \text{ cm} \qquad \tau = 9 \text{ hr} = 32,400 \text{ sec}$$

$$k = 1.37 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \qquad \alpha = 7.5 \times 10^{-7} \text{ m}^2/\text{s}$$

$$T = 20 + \frac{(2)(900)\left[(7.5 \times 10^{-7})\frac{32,400}{\pi}\right]^{1/2}}{1.37} \exp\left[\frac{-(0.1)^2}{4(7.57 \times 10^{-7})(32,400)}\right]$$

$$-\frac{(900)(0.1)}{1.37}\left[1 - \text{erf}\left(\frac{0.1}{(2)(7.5 \times 10^{-7})(32,400)^{1/2}}\right)\right]$$

$$= 81.5^{\circ}\text{C}$$

$$T_i = 300^{\circ}\text{C}$$
  $T_0 = 100^{\circ}\text{C}$   $x = 0.03 \text{ m}$   $T = 200^{\circ}\text{C}$   $\frac{200 - 100}{300 - 100} = 0.5 = \text{erf}\left(\frac{x}{2\sqrt{\alpha\tau}}\right)$   $\alpha = 0.444 \times 10^{-5}$   $\frac{x}{2\sqrt{\alpha\tau}} = 0.48$   $\tau = \frac{\left[\frac{0.03}{(2)(0.48)}\right]^2}{0.444 \times 10^{-5}} = 2200 \text{ sec}$ 

$$T_i = 40^{\circ}\text{C}$$
  $h = 25 \frac{\text{W}}{\text{m}^2 \cdot ^{\circ}\text{C}}$   $T_{\infty} = 2^{\circ}\text{C}$   $x = 0.08 \text{ m}$   $T(x) = 20^{\circ}\text{C}$   
 $\alpha = 5.2 \times 10^{-7}$   $k = 0.69 \frac{\text{W}}{\text{m} \cdot ^{\circ}\text{C}}$   
 $\frac{T - T_i}{T_{\infty} - T_i} = \frac{20 - 40}{2 - 40} = 0.5263$   $\frac{x}{2\sqrt{\alpha \tau}} \approx 0.4$   
 $\tau = \frac{\left[\frac{0.08}{(2)(0.4)}\right]^2}{5.2 \times 10^{-7}} = 19,231 \text{ sec}$ 

#### 4-35

$$T_i = 30^{\circ}\text{C} \qquad \frac{q}{A} = 3 \times 10^4 \qquad \tau = 10 \text{ min} = 600 \text{ sec} \qquad x = 3 \text{ cm}$$

$$k = 2.32 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \qquad \alpha = 9.2 \times 10^{-7} \text{ m}^2/\text{s}$$

$$T = 30 + \frac{(2)(3 \times 10^4) \left[ (9.2 \times 10^{-7}) \frac{600}{\pi} \right]^{1/2}}{2.32} \exp \left[ \frac{-(0.03)^2}{(4)(9.2 \times 10^{-7})(600)} \right]$$

$$-\frac{(3 \times 10^4)(0.03)}{2.32} \left\{ 1 - \text{erf} \left[ \frac{0.03}{(2)(9.2 \times 10^{-7})(600)} \right] \right\}$$

$$= 30 + 228 = 258^{\circ}\text{C}$$

#### 4-36

From symmetry same as inf. plate 6 cm thick

$$\tau = 360 \text{ sec}$$
  $L = 30 \text{ cm}$   $\alpha = 11.23 \times 10^{-5}$   $k = 370$   $\frac{\alpha \tau}{L^2} = 44.92$   $\frac{\theta_{x=L}}{\theta_i} = \frac{150 - 100}{250 - 100} = 0.33$ 

1

Iterative Solution:

| $\frac{k}{hL}$ | $\frac{	heta_0}{	heta_i}$ | $\frac{	heta}{	heta_0}$ | $rac{	heta}{	heta_i}$ | $\frac{\theta}{\theta_i}$ - 0.33 |
|----------------|---------------------------|-------------------------|------------------------|----------------------------------|
| 100            | 0.65                      | 1.0                     | 0.65                   | 0.32                             |
| 50             | 0.42                      | 0.98                    | 0.41                   | 0.08                             |
| 45             | 0.38                      | 0.98                    | 0.37                   | 0.04                             |
| 40             | 0.34                      | 0.98                    | 0.33                   | 0                                |

$$h = \frac{370}{(40)(0.03)} = 308.3 \frac{\text{W}}{\text{m}^2 \cdot ^{\circ}\text{C}}$$

$$L = 5 \text{ cm}$$
  $h = 1400$   $k = 230$   $T_i = 400$   $\alpha = 8.42 \times 10^{-5}$ 
 $T_{\infty} = 90$   $T_0 = 180$   $\frac{k}{hL} = 3.29$   $\frac{\theta_0}{\theta_i} = 0.29$   $\frac{\alpha \tau}{L^2} = 5.0$ 

$$\tau = \frac{(0.05)^2(5)}{8.42 \times 10^{-5}} = 148 \text{ sec}$$

$$T_i = 350^{\circ}\text{C}$$
  $T_{\infty} = 80^{\circ}\text{C}$   $T_0 = 150^{\circ}\text{C}$   $\tau = 6 \text{ min} = 360 \text{ sec}$ 

$$k = 374 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$$
  $\alpha = 11.23 \times 10^{-5}$   $L = 0.1 \text{ m}$   $\frac{\alpha \tau}{L^2} = 4.04$ 

$$\frac{\theta_0}{\theta_i} = \frac{150 - 80}{250 - 80} = \frac{70}{170} = 0.412$$
  $\frac{x}{L} = 1.0$   $\frac{k}{hL} \approx 4.0$ 

$$h = \frac{374}{(4.0)(0.1)} = 935 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$$

#### 4-39

$$L = 5 \text{ cm} T_i = 400^{\circ}\text{C} T_{\infty} = 90^{\circ}\text{C} h = 1400 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$$

$$k = 204 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \alpha = 8.4 \times 10^{-5} \text{ m}^2/\text{s} \frac{\theta_0}{\theta_i} = \frac{180 - 90}{400 - 90} = 0.29$$

$$\frac{k}{hL} = \frac{204}{(1400)(0.05)} = 2.91 \frac{\alpha\tau}{L^2} = 4.2 \tau = \frac{(4.2)(0.05)^2}{8.4 \times 10^{-5}} = 125 \text{ sec}$$

$$L = 0.015 \text{ m} \qquad T_i = 500^{\circ}\text{C} \qquad T_{\infty} = 40^{\circ}\text{C} \qquad h = 150 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$$

$$k = 16.3 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \qquad \alpha = 0.44 \times 10^{-5} \text{ m}^2/\text{s} \qquad \frac{k}{hL} = \frac{6.3}{(150)(0.015)} = 7.24$$
at  $\frac{x}{L} = 1.0 \qquad \frac{\theta}{\theta_0} = 0.93$ 
For  $\frac{\theta_0}{\theta_i} = \frac{120 - 40}{500 - 40} = 0.174 \qquad \frac{\alpha \tau}{L^2} = 13.9$ 

$$\tau = \frac{(13.9)(0.015)^2}{0.44 \times 10^{-5}} = 711 \text{ sec}$$
For  $\frac{\theta}{\theta_i} = 0.174 \qquad \frac{\theta_0}{\theta_i} = \frac{0.174}{0.93} = 0.187 \qquad \frac{\alpha \tau}{L^2} = 13$ 

$$\tau = \frac{(13)(0.015)^2}{0.44 \times 10^{-5}} = 665 \text{ sec}$$

$$r_0 = 5 \text{ cm}$$
  $L = 5 \text{ cm}$   $T_i = 250^{\circ}\text{C}$   $T_{\infty} = 30^{\circ}\text{C}$   $h = 280 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $k = 43 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\alpha = 1.172 \times 10^{-5} \text{ m}^2/\text{sec}$   $\tau = 2 \text{ min} = 120 \text{ sec}$   $\frac{\alpha \tau}{L^2} = \frac{\alpha \tau}{r_0^2} = 0.563$   $\frac{k}{hL} = \frac{k}{hr_0} = 3.071$   $\frac{\text{cylinder:}}{\theta_i} = 0.86$   $\frac{\theta_0}{\theta_i} = 0.86$   $\frac{\theta_0}{\theta_i} = 0.93$   $\frac{\theta_2}{\theta_0} = 0.86$   $\frac{\theta_0}{\theta_i} = 0.86$ 

### 4-42

$$T - T_i = \left[\frac{Q_0}{A\rho c(\pi\alpha\tau)^{1/2}}\right] \exp\left(\frac{-x^2}{4\alpha\tau}\right)$$

$$\frac{q}{A} = -k\frac{\partial T}{\partial x}$$

$$= -k\left[\frac{Q_0}{A\rho c(\pi\alpha\tau)^{1/2}}\right] \exp\left(\frac{-x^2}{4\alpha\tau}\right)\left(\frac{-2x}{4\alpha\tau}\right)$$

$$= \frac{1}{2}\frac{x}{\tau}\left[\frac{Q_0}{A(\pi\alpha\tau)^{1/2}}\right] \exp\left(\frac{-x^2}{4\alpha\tau}\right)$$

#### 4-43

Assume behaves like center of 20 cm thick wall with  $T_i = 15^{\circ}C$ ,

$$c = 900$$
,  $\rho = 2200$ ,  $k = 2.32$ ,  $\alpha = 1.17 \times 10^{-6}$ 

$$h = 65$$
,  $\theta_0/\theta_i = (5-(-10))/(15-(-10)) = 0.6$ 

$$k/hL = 0.356$$

Fig. 4-7(b) 
$$\alpha \tau / L^2 = 0.48$$

$$\tau = (0.48)().1)^2/1.17 \times 10^{-6} = 4100 \text{ sec}$$

Q/A = 1.0 MJ/m<sup>2</sup>; 
$$T_i = 20^{\circ}\text{C}$$
;  $x = 0.023$ ;  $\tau = 1.8 \text{ s}$ 

$$\alpha = 8.4 \times 10^{-5}; \ \rho = 2700; \ c = 896$$
Eq. (4-13b)
$$T = 20 + \{10^{6/}/(2700)(896)[\pi(8.4 \times 10^{-5})(1.8)]^{1/2}\} \exp[-0.023^2/(4)(8.4 \times 10^{-5})(1.8)]$$
=27.91°C

#### 4-45

$$\rho = 7817 \qquad c = 460 \qquad \alpha = 0.44 \times 10^{-5} \qquad x = 0.01 \qquad \tau = 3$$

$$\frac{Q_0}{A} = 10^7 \text{ J/m}^2 \qquad T_i = 0^{\circ}\text{C}$$

$$T - 0 = \frac{10^7}{(7817)(460)[\pi(0.44 \times 10^{-5})(3)]^{1/2}} \exp\left[\frac{-(0.01)^2}{(4)(0.44 \times 10^{-5})(3)}\right]$$

$$T = 431.9e^{-1.894} = 64.99^{\circ}\text{C}$$

$$64.99 = \frac{431.9}{1 \times 10^7} \left( \frac{Q_0}{A} \right) \exp \left[ -\left( \frac{1.2}{1} \right)^2 (1.894) \right]$$
$$\frac{Q_0}{A} = 2.3 \times 10^7 \text{ J/m}^2$$

From Prob. 4-40

$$\frac{q}{A} = \frac{1}{2} \frac{x}{\tau} \left[ \frac{Q_0}{A(\pi \alpha \tau)^{1/2}} \right] \exp\left(\frac{-x^2}{4\alpha \tau}\right)$$

$$= \frac{0.01}{(2)(3)} \frac{(10^7)}{[\pi (0.44 \times 10^{-5})(3)]^{1/2}} e^{-1.894}$$

$$= (2.588 \times 10^6)(0.1505) = 3.89 \times 10^5 \text{ W/m}^2$$

#### 4-48

$$\rho = 2700$$
  $c = 896$   $\alpha = 8.42 \times 10^{-5}$   $x = 0.002$   $\tau = 0.2$ 

$$600 - 30 = \frac{Q_0/A}{(2700)(896)[\pi(8.42 \times 10^{-5})(0.2)]^{1/2}} \times \exp\left[\frac{-(0.002)^2}{(4)(8.42 \times 10^{-5})(0.2)}\right]$$

$$570 = \frac{\left(\frac{Q_0}{A}\right)e^{-0.0594}}{17,596}$$

$$\frac{Q_0}{A} = 10.64 \text{ MJ/m}^2$$

#### 4-49

$$ho = 4000$$
  $c = 760$   $\alpha = 120 \times 10^{-7}$   $x = 0.0002$   $\tau = 0.2$ 

$$900 - 40 = \frac{Q_0/A}{(2700)(760)[\pi(120 \times 10^{-7})(0.2)]^{1/2}} \exp \left[ \frac{-(0.0002)^2}{(4)(120 \times 10^{-7})(0.2)} \right]$$

$$860 = \frac{(Q_0/A)e^{-0.0042}}{8347}$$

$$\frac{Q_0}{A} = 7.2 \text{ MJ/m}^2$$

$$\rho = 2700 \qquad c = 840 \qquad \alpha = 3.4 \times 10^{-7} \qquad x = 0.0002 \qquad \tau = 0.2$$

$$900 - 40 = \frac{Q_0/A}{(2700)(840)[\pi (3.4 \times 10^{-7})(0.2)]^{1/2}} \exp \left[ \frac{-(0.0002)^2}{(4)(3.4 \times 10^{-7})(0.2)} \right]$$

$$860 = \frac{(Q_0/A)e^{-0.1471}}{1048}$$

$$\frac{Q_0}{A} = 1.04 \text{ MJ/m}^2$$

#### 4-51

$$r_0 = 5.5 \text{ cm}$$
  $T_i = 300^{\circ}\text{C}$   $T_{\infty} = 50^{\circ}\text{C}$   $h = 1200 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $T_0 = 80^{\circ}\text{C}$ 

$$\rho = 2707$$
  $c = 896 \frac{\text{J}}{\text{kg} \cdot {}^{\circ}\text{C}}$   $k = 204 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\alpha = 8.4 \times 10^{-5} \text{ m}^2/\text{s}$ 

$$\frac{k}{hr_0} = \frac{204}{(1200)(0.055)} = 3.09$$
  $\frac{\theta_0}{\theta_i} = \frac{80 - 50}{300 - 50} = 0.12$   $\frac{\alpha \tau}{r_0^2} = 3.7$ 

$$\tau = \frac{(3.7)(0.055)^2}{8.4 \times 10^{-5}} = 133 \text{ sec}$$
  $\frac{h^2 \alpha \tau}{k^2} = \frac{(1200)^2(8.4 \times 10^{-5})(133)}{(204)^2} = 0.386$ 

$$\frac{hr_0}{k} = 0.324$$
  $\frac{Q}{Q_0} = 0.85$ 

$$Q_0 = \rho cV\theta_i = (2707)(896)(300 - 50)\pi(0.055)^2 = 5.76 \text{ MJ}$$
 $Q = (0.85)(5.76) = 4.9 \text{ MJ}$ 

#### 4-52

$$\alpha = 9.5 \times 10^{-7} \text{ m}^2/\text{s} \qquad r_0 = 1.25 \text{ cm} \qquad k = 1.52 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$$

$$T_i = 25^{\circ}\text{C} \qquad T_{\infty} = 200^{\circ}\text{C} \qquad h = 110 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}} \qquad \tau = 3 \text{ min} = 180 \text{ sec}$$

$$\frac{k}{hr_0} = \frac{1.52}{(110)(0.0125)} = 1.105 \qquad \frac{r}{r_0} = \frac{0.64}{1.25} = 0.51$$

$$\frac{\alpha \tau}{r_0^2} = \frac{(9.5 \times 10^{-7})(180)}{(0.0125)^2} = 1.094 \qquad \frac{\theta_0}{\theta_i} = 0.12 \qquad \frac{\theta_r}{\theta_0} = 0.89$$

$$\text{center } T = (25 - 200)(0.12) + 200 = 179^{\circ}\text{C} \qquad r = 6.4 \text{ mm}$$

$$T = (25 - 200)(0.12)(0.89) + 200 = 181.3^{\circ}\text{C}$$

$$T_i = 300^{\circ}\text{C}$$
  $T_0 = 120^{\circ}\text{C}$   $d = 1.5 \text{ mm}$   $r_0 = 0.75 \text{ mm}$   $T_{\infty} = 100^{\circ}\text{C}$   
 $h = 5000 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $k = 35 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\alpha = 2.34 \times 10^{-5} \text{ m}^2/\text{s}$   
 $\frac{k}{hr_0} = \frac{35}{(5000)(0.00075)} = 9.33$   $\frac{\theta_0}{\theta_i} = \frac{120 - 100}{300 - 100} = 0.1$   
 $\frac{\alpha \tau}{r_0^2} = 7.3$   $\tau = \frac{(7.3)(0.00075)^2}{2.34 \times 10^{-5}} = 0.175 \text{ sec}$ 

$$r_0 = 5 \text{ cm}$$
  $T_{\infty} = 10^{\circ}\text{C}$   $T_i = 250^{\circ}\text{C}$   $h = 280$   $\alpha = 1.172 \times 10^{-5}$ 
 $T_0 = 150^{\circ}\text{C}$   $k = 43$   $\frac{\theta_0}{\theta_i} = \frac{150 - 10}{250 - 10} = 0.583$ 

$$\frac{k}{hr_0} = \frac{43}{(280)(0.05)} = 3.07$$
  $\frac{\alpha \tau}{r_0^2} = 0.75$ 

$$\tau = \frac{(0.75)(0.05)^2}{1.172 \times 10^{-5}} = 160 \text{ sec} = 2.67 \text{ min}$$

$$T_i = 200^{\circ}\text{C}$$
  $T_{\infty} = 20^{\circ}\text{C}$   $h = 14 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $r_0 = 0.0075 \text{ m}$ 

$$T_0 = 50^{\circ}\text{C}$$
  $k = 0.78 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\alpha = 3.4 \times 10^{-7}$ 

$$\frac{k}{hr_0} = \frac{0.78}{(14)(0.0075)} = 7.43$$
  $\frac{\theta_0}{\theta_i} = \frac{50 - 20}{200 - 20} = 0.167$ 

$$\frac{\alpha \tau}{r_0^2} = 4.5$$
  $\tau = \frac{(4.5)(0.0075)^2}{3.4 \times 10^{-7}} = 744 \text{ sec}$ 

#### 4-56

$$r_0 = 0.0075 \text{ m}$$
  $T_i = 200^{\circ}\text{C}$   $h = 5000 \frac{\text{W}}{\text{m}^2 \cdot ^{\circ}\text{C}}$   $T_{\infty} = 100^{\circ}\text{C}$   
 $T_0 = 120^{\circ}\text{C}$   $k = 35 \frac{\text{W}}{\text{m} \cdot ^{\circ}\text{C}}$   $\alpha = 2.34 \times 10^{-5}$   
 $\frac{k}{hr_0} = \frac{35}{(5000)(0.00075)} = 9.33$   $\frac{\theta_0}{\theta_i} = \frac{120 - 100}{200 - 100} = 0.2$   
 $\frac{\alpha \tau}{r_0^2} = 5.2$   $\tau = \frac{(5.2)(0.00075)^2}{2.34 \times 10^{-5}} = 0.125 \text{ sec}$ 

$$T_i = 250^{\circ}\text{C}$$
  $T_{\infty} = 30^{\circ}\text{C}$   $h = 570$   $\tau = 120 \text{ sec}$   $L_1 = L_2 = 1.25 \text{ cm}$   $L_3 = 3.75 \text{ cm}$   $k = 43 \frac{\text{W}}{\text{m} \cdot \text{°C}}$   $\alpha = 1.172 \times 10^{-5} \text{ m}^2/\text{sec}$   $\frac{k}{hL}\Big|_{1, 2} = 6.035$   $\frac{k}{hL}\Big|_{3} = 2.01$   $\frac{\alpha\tau}{L^2}\Big|_{1, 2} = 9.00$   $\frac{\alpha\tau}{L^2}\Big|_{3} = 1.00$   $\frac{\theta_0}{\theta_i}\Big|_{1, 2} = 0.25$   $\frac{\theta_0}{\theta_i}\Big|_{3} = 0.7$  Center  $\frac{\theta_0}{\theta_i} = (0.25)^2(0.07) = 0.0438$   $T = 39.6^{\circ}\text{C}$ 

### 4-58

$$T_{\infty} = 30^{\circ}\text{C} \qquad \tau = 120 \text{ sec} \qquad T_{i} = 220^{\circ}\text{C} \qquad h = 570 \frac{\text{W}}{\text{m}^{2} \cdot {}^{\circ}\text{C}}$$

$$\alpha = 1.17 \times 10^{-5} \text{ m}^{2}/\text{s} \qquad k = 43 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \qquad L_{1} = L_{2} = 0.025$$

$$L_{3} = 0.075$$

$$\frac{\alpha \tau}{L_{1}^{2}} = \frac{(1.17 \times 10^{-5})(120)}{(0.025)^{2}} = 2.246$$

$$\frac{\alpha \tau}{L_{3}^{2}} = 0.25$$

$$\frac{k}{hL_{1}} = \frac{43}{(570)(0.025)} = 3.02$$

$$\frac{k}{hL_{3}} = 1.01$$

$$\left(\frac{\theta_{0}}{\theta_{i}}\right)_{L_{1}} = 0.54 \qquad \left(\frac{\theta_{0}}{\theta_{i}}\right)_{L_{3}} = 0.92 \qquad \left(\frac{\theta_{0}}{\theta_{i}}\right)_{\text{bar}} = (0.54)^{2}(0.92) = 0.268$$

$$T_{0} = 30 + (0.268)(220 - 30) = 81^{\circ}\text{C}$$

$$L = 5 \text{ cm} T_i = 300^{\circ}\text{C} T_{\infty} = 100^{\circ}\text{C} h = 900 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}} \tau = 60 \text{ sec}$$

$$k = 204 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \alpha = 8.42 \times 10^{-5} \text{ m}^2/\text{s} \frac{k}{hL} = 4.53 \frac{\alpha \tau}{L^2} = 2.02$$

$$\frac{\theta_0}{\theta_i} = 0.7 \frac{\theta_L}{\theta_0} = 0.9 \text{Center of face: } \frac{\theta}{\theta_i} = (0.7)(0.9) = 0.63$$

$$T = (0.63)(300 - 100) + 100 = 226^{\circ}\text{C}$$

$$r_0 = 7.5 \text{ cm}$$
  $L = 15 \text{ cm}$   $T_i = 25^{\circ}\text{C}$   $T_{\infty} = 0^{\circ}\text{C}$   $T_0 = 6^{\circ}\text{C}$   
 $h = 17 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $\alpha = 7 \times 10^{-7} \text{ m}^2/\text{s}$   $k = 1.37 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\frac{k}{hL} = 0.54$   
 $\frac{k}{hr_0} = 1.075$   $\frac{\theta_0}{\theta_i} = \frac{6 - 0}{25 - 0} = 0.24 = \left(\frac{\theta_0}{\theta_i}\right)_{\text{cyl}} \left(\frac{\theta_0}{\theta_i}\right)_{\text{plate}}$ 

**Iterative Solution:** 

| τ    | $\frac{\alpha \tau}{{r_0}^2}$ | с    | $\frac{\alpha \tau}{L^2}$ | ρ   | СР    |
|------|-------------------------------|------|---------------------------|-----|-------|
| 3600 | 0.448                         | 0.65 | 0.112                     | 1.0 | 0.65  |
| 7200 | 0.896                         | 0.28 | 0.224                     | 0.9 | 0.252 |

$$\tau = 7200 \text{ sec} = 2 \text{ hr}$$

#### 4-61

$$\frac{1}{R_{m+1}} = \frac{1}{R_{m-1}} = \frac{kA}{\Delta x} = \frac{(0.8)\pi(0.02)^2}{(4)(0.01)} = 0.02513$$

$$\frac{1}{R_{\infty}} = hA = (50)\pi(0.02)(0.01) = 0.031416$$

$$\sum \frac{1}{R} = 0.08168$$

$$C_m = (2700)(840)\pi(0.01)^2(0.01) = 7.125$$

$$\Delta \tau_{\text{max}} = \frac{7.125}{0.08168} = 87.2 \text{ sec}$$

$$T_m^{p+1} = \frac{\Delta \tau}{7.125} [0.025(T_{m-1}{}^p - T_m{}^p) + (0.025)(T_{m+1}{}^p - T_m{}^p) + 0.03142(35 - T_m{}^p)] + T_m^p$$

$$k = 290 \qquad \frac{h(V/A)}{k} = \frac{(120)(0.04)^3}{(6)(0.04)^2(240)} = 3.3 \times 10^{-3} < 0.1$$
Lumped capacity:  $\rho = 2707$   $c = 896$ 

$$\frac{hA}{\rho cV} = \frac{(120)(6)(0.04)^2}{(2707)(896)(0.04)^3} = 7.42 \times 10^{-3}$$

$$\frac{250 - 100}{450 - 100} = e^{-7.42 \times 10^{-3}\tau} \qquad \tau = 114 \text{ sec}$$

#### 4-63

$$L = 5.5 \text{ cm} T_i = 400^{\circ}\text{C} T_{\infty} = 85^{\circ}\text{C} h = 1100 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}} \tau = 60 \text{ sec}$$

$$k = 204 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}} \alpha = 8.4 \times 10^{-5} \text{ m}^2/\text{s} \frac{k}{hL} = \frac{204}{(1100)(0.055)} = 3.37$$

$$\frac{\alpha \tau}{L^2} = \frac{(8.4 \times 10^{-5})(60)}{(0.055)^2} = 1.67 \frac{\theta_0}{\theta_i} = 0.7$$
at  $\frac{x}{L} = 1.0 \frac{\theta}{\theta_0} = 0.86 \frac{\theta}{\theta_i}$  at center of face  $= (0.7)^3 (0.86) = 0.295$ 

$$T = (0.295)(400 - 85) + 85 = 178^{\circ}\text{C}$$

#### 4-64

$$L = 0.025 T_i = 100^{\circ}C T_{\infty} = 25^{\circ}C h = 20 \frac{W}{m^2 \cdot {}^{\circ}C} T_0 = 50^{\circ}C$$

$$k = 204 \frac{W}{m \cdot {}^{\circ}C} \alpha = 8.4 \times 10^{-5} \text{ m}^2/\text{s}$$

$$\frac{h(V/A)}{k} = \frac{(20)(0.05)^3}{(6)(0.05)^2(204)} = 8.16 \times 10^{-4}$$
Lumped Capacity:  $\frac{50 - 25}{100 - 25} = \exp\left[\frac{-(20)(6)(0.05)^2\tau}{(2707)(896)(0.05)^3}\right]$ 

# 4-65

 $\tau = 11111 \, \text{sec}$ 

$$T_{i} = 200^{\circ}\text{C} \qquad T_{\infty} = 30^{\circ}\text{C} \qquad \tau = 600 \text{ sec} \qquad h = 200 \frac{\text{W}}{\text{m}^{2} \cdot {}^{\circ}\text{C}} \qquad d = 10 \text{ cm}$$

$$L = 15 \text{ cm} \qquad T_{0} = 100^{\circ}\text{C} \qquad k = 16.3 \qquad \alpha = 0.44 \times 10^{-5} \qquad \rho = 7817$$

$$c = 460$$

$$\frac{k}{hr_{0}} = \frac{16.3}{(200)(0.05)} = 1.63 \qquad \frac{k}{hL} = \frac{16.3}{(200)(0.075)} = 1.09$$

$$\frac{\alpha\tau}{r_{0}^{2}} = 1.056 \qquad \frac{\alpha\tau}{L^{2}} = 0.47$$

$$\frac{\theta_{0}}{\theta_{i}}\Big|_{c} = 0.45 \qquad \frac{\theta_{0}}{\theta_{i}}\Big|_{p} = 0.9 \qquad \frac{\theta_{0}}{\theta_{i}} = (0.45)(0.9) = 0.405$$

$$T = (0.405)(200 - 30) + 30 = 98.8^{\circ}\text{C}$$

$$\frac{hL}{k} = 0.92 \qquad \frac{h^{2}\alpha\tau}{k^{2}} = 0.397$$

$$\frac{Cyl}{hr_0} = 0.61$$

$$\frac{Q}{Q_0}\Big|_{cyl} = 0.55 \qquad \frac{Q}{Q_0}\Big|_{plate} = 0.2$$

$$\frac{Q}{Q_0}\Big|_{total} = 0.55 + 0.2(1 - 0.55) = 0.64$$

$$Q_0 = \rho c V \theta_i = (7817)(460)\pi(0.05)^2(0.15)(200 - 30) = 0.72 \text{ MJ}$$

$$Q = (0.64)(0.72) = 0.46 \text{ MJ}$$

$$L = 0.15 r_0 = 0.075 T_i = 300^{\circ}C T_{\infty} = 20^{\circ}C h = 35 \frac{W}{m^2 \cdot {}^{\circ}C}$$

$$T = 120^{\circ}C k = 2.3 \frac{W}{m \cdot {}^{\circ}C} \rho = 300 \text{ kg/m}^3 c = 840 \frac{J}{\text{kg} \cdot {}^{\circ}C}$$

$$\frac{k}{hL} = \frac{2.3}{(35)(0.15)} = 0.44 \frac{k}{hr_0} = 0.88$$

$$\frac{\theta}{\theta_i} = \frac{120 - 20}{300 - 20} = 0.36 \alpha = \frac{k}{\rho c} = 9.12 \times 10^{-6}$$

### Geometric Center

At 
$$\tau = 300 \text{ sec}$$
 
$$\frac{\alpha \tau}{L^2} = \frac{(9.12 \times 10^{-6})(300)}{(0.15)^2} = 0.12$$
 
$$\frac{\alpha \tau}{r_0^2} = 0.36$$
 
$$(\theta_0/\theta_i)_{\text{cyl}} = 0.7$$
 
$$(\theta_0/\theta_i)_{\text{plate}} = 0.96$$
 
$$\frac{\theta_i}{\theta_i} = 0.67 \text{ therefore } \tau \text{ is too small}$$
 At  $\tau \approx 500 \text{ sec}$  
$$\frac{\alpha \tau}{r_0^2} = 0.6$$
 
$$\frac{\theta}{\theta_i} \approx 0.4$$

Therefore  $\tau \approx 500 \text{ sec}$ 

### Center of Face

$$\frac{x}{L} = 1.0 \qquad \frac{\theta}{\theta_0} = 0.43$$

$$\left(\frac{\theta_0}{\theta_i}\right)_{\text{cyl}} \times \left(\frac{\theta_0}{\theta_i}\right)_{\text{plate}} \times 0.43 = 0.36 \qquad \left(\frac{\theta_0}{\theta_i}\right)_{\text{cyl}} \times \left(\frac{\theta_0}{\theta_i}\right)_{\text{plate}} = 0.84$$

$$\tau \approx 250 \text{ sec}$$

$$\frac{1}{R_{12}} = \frac{kA}{\Delta x} = \frac{(20)(1)}{0.0025} = 8000 = \frac{1}{R_{23}}$$

$$\frac{1}{R_{1-\infty}} = hA = 70(1) = 70$$

$$\frac{1}{R_{34}} = \frac{(1.2)(1)}{0.0075} = 160 = \frac{1}{R_{45}}$$

$$\frac{1}{R_{56}} = \frac{(0.5)(1)}{0.01} = 50 = \frac{1}{R_{67}}$$

$$C_1 = (7800)(1)\left(\frac{0.005}{4}\right)(460) = 4485$$

$$C_2 = (2)(4485) = 8970$$

$$C_3 = 4485 + (1600)(1)\left(\frac{0.015}{4}\right)(850) = 9585$$

$$C_4 = (2)(5100) = 10,200$$

$$C_5 = 5100 + (2500)(1)(0.005)(800) = 15,100$$

$$C_6 = (2)(10,000) = 20,000$$

$$C_7 = 10,000$$

$$\sum \frac{1}{R_1} = 8070$$

$$\sum \frac{1}{R_2} = 16,600$$

$$\sum \frac{1}{R_3} = 8000 + 160 = 8160$$

$$\sum \frac{1}{R_4} = (2)(160) = 320$$

$$\sum \frac{1}{R_5} = 160 + 50 = 210$$

$$\sum \frac{1}{R_6} = (2)(50) = 100$$

$$\sum \frac{1}{R_7} = 50$$

$$\frac{C_i}{\sum \frac{1}{R_i}}$$

$$1 \qquad 4485/8070 = 0.5558 \text{ sec}$$

$$2 \qquad 8970/16,000 = 0.5606$$

$$3 \qquad 9585/8160 = 1.175$$

$$4 \qquad 10,200/320 = 31.88$$

Use  $\Delta \tau = 0.5558$  sec

5

6

7

Compute for 2, 20, 120 time increments.

15,100/210 = 71.9

20,000/100 = 200

10,000/50 = 200

# The Equations

|   | Α   | В | С      | D   |
|---|-----|---|--------|---|
| 1 | T1= |   |        | =(70*(10-C1)+8000*(C2-C1))*\$C\$9/4485+C1   |
| 2 | T2= |   |        | =(8000*(C1-C2)+8000*(C3-C2))*\$C\$9/8970+C2 |
| 3 | T3= |   |        | =(8000*(C2-C3)+160*(C4-C3))*\$C\$9/9585+C3  |
| 4 | T4= |   |        | =(160*(C3-C4)+160*(C5-C4))*\$C\$9/10200+C4  |
| 5 | T5= |   |        | =(160*(C4-C5)+50*(C6-C5))*\$C\$9/15100+C5   |
| 6 | T6= |   |        | =(50*(C5-C6)+50*(C7-C6))*\$C\$9/2000+C6     |
| 7 | T7= |   |        | =(50*(C6-C7))*\$C\$9/2000+C7                |
| 8 |     |   |        |   |
| 9 | Dt= |   | 0.5558 |   |

| _  | I 0                | T 14                     | ,                        |                       | l k                          |                                    |                          | N                                   |
|--|--------------------|--------------------------|--------------------------|-----------------------|------------------------------|------------------------------------|--------------------------|-------------------------------------|
| H  | Time               | Ti-                      | 17-                      | 73-                   | T#                           | T3=                                | TV-                      | 17-                                 |
| 7  | -                  | 99,21928                 | 100                      | 100                   |                              | 100                                | 100                      | К                                   |
| 3  | 2                  | 99.21933                 | 99.613<br>99.60969       | 100                   | 100                          | 100                                | 100                      | 10                                  |
| 7  | - 3                | 98.83241                 | 99.33049<br>99.27883     | 99.72436              | 99.99843                     | 100                                | 100                      | 10                                  |
| 9  | 6                  | 98,50442                 | 99.05187                 | 99.54419<br>99.42529  | 99.99215                     | 99.99999<br>99.99997               | 100                      | 10                                  |
| 19<br>11<br>12                           | - 4                | 98.27941<br>98.1939      | 98.77006                 | 99.25732<br>99.12877  | 99.98103                     | 99.99992<br>99.99985               | 100                      | 10                                  |
| 13                                       | 10                 | 98.00005<br>97.8932      | 98.66227<br>98.48669     | 98.97027<br>98.8367   | 99,96524                     | 99.99974<br>99.99958               | 100<br>99.99999          | 10                                  |
| 15                                       | 12                 | 97.71913<br>97.59949     | 98.366<br>98.20338       | 98.6848<br>98.5487    | 99.9557<br>99.945            | 99.99938<br>99.99913               | 99.99999<br>99.99998     | 10<br>10                            |
| 16<br>17                                 |                    | 97.43828<br>97.31123     | 98.07521                 | 98.40146<br>98.26433  | 99.9333<br>99.92051          | 99.99881<br>99.99843               | 99.99997<br>99.99995     | 10                                  |
| 끊  | 15                 | 97.15856<br>97.02743     | 97.78893<br>97.64083     | 98.12053<br>97.98327  | 99.90675<br>99.89197         | 99.99797<br>99.99744               | 99.99993<br>99.9999      | 10                                  |
| 20<br>21                                 | 17                 | 96.88061                 | 97.50652<br>97.36262     | 97.84212<br>97.70531  | 99.87625<br>99.85957         | 99.99682<br>99.99612               | 99.99987<br>99.99983     | 10:                                 |
| 72                                       | 19                 | 96.60482                 | 97.22756                 | 97.56633<br>97.43029  |                              | 99.99532                           |                          | 99.99999                            |
| 24<br>25                                 | 21<br>22           | 96.33138<br>96.19754     | 96.95178<br>96.81347     | 97.29315<br>97.15809  | 99.8041                      |                                    |                          | 99.9999                             |
| 26<br>27                                 | 23                 |                          | 96.67898<br>96.54269     | 97.02258<br>96.88861  | 99.76278                     | 99.99111<br>99.99978               |                          | 99.9999                             |
| 28<br>29                                 | 25<br>26           | 95,792                   | 96.40902<br>96.27447     | 96.7546<br>96.62179   | 99.71819                     |                                    | 99,99924                 | 99.9999<br>99.9999                  |
| 30<br>31                                 | 27                 |                          | 96.14179<br>96.0088      | 96.48918<br>96.35755  | 99.67046                     | 99.98506<br>99.98324               | 99.99894                 | 99.9999                             |
| 32<br>33                                 | 29                 | 95.26274                 | 95.87721                 | 96.22627              | 99.61975                     | 99.98127                           | 99.99876<br>99.99856     | 91.9991                             |
| 3  | 31                 | 95.00187                 | 95.61519                 | 95.96583              | 99.56618                     | 99.97918<br>99.97694<br>99.97456   |                          | 99.99947<br>99.99947                |
| 36<br>37                                 | 33                 | 94.74347                 | 95.35568                 | 95.70782              | 99.50991                     | 99.97203                           | 99.99753                 | 99.99904<br>99.99902                |
| 38                                       | 35                 |                          | 95.09863                 | 95.45219              | 99.45103                     | 99.96653                           | 99.99686                 | 99.99970<br>99.99975                |
| 9  | 37                 | 94.23389                 | 94.84397                 | 95.1989               | 99.38969                     | 99.96042                           | 99.99606                 | 99,99971<br>99.99966                |
| 3  |                    | 93.98264                 | 94.59167                 | 94.94791              | 99.326                       | 99.95366                           |                          | 99.99961<br>99.99956                |
| 4  | 41                 | 93.73368                 | 94.34167                 |                       | 99.26005                     | 99.94626                           |                          | 99,9995<br>99,99943                 |
| 9  | 43                 | 93.48699                 | 94.09393                 | 94.45266              | 99.19197                     |                                    | 99.99285                 | 99,99935<br>99,99927                |
| 4  | 45                 | 93.24251                 | 93.84842                 | 94,20631              |                              |                                    | 99.99147                 | 99.99918<br>99.9 <del>9909</del>    |
| 3  |                    | 93.00021                 | 93.60508                 | 3.96611               | 99.04977                     | 9.91996                            | 99.99071<br>99.98991     | 79.57000<br>79.57006                |
| 3  |                    | 92.76005                 | 93,36388                 | 93.726                | 98.97585                     | 9.90979                            |                          | 2.59474<br>2.59451                  |
|  | 51                 | 92.52199                 | 3.12478 9                | 9.60672               | 98.93822 9<br>98.90017       | 99.8989                            | 99.98723                 | 99.9983                             |
| 闔  | 53                 |                          | 2.88774 9                | 73.36969<br>73.25193  |                              | 9.89317 9<br>9.88727 9             | 99.98519 9<br>99.98409 9 | 9.99814<br>9.997%                   |
| 3  | 55                 |                          |                          |                       | 98.78351 5<br>98.74383       | 9.88118 9<br>99.8749 9             |                          | 9.99776<br>9.99736                  |
| 응  |                    |                          | 2.53598 9                | 2.90163<br>2.78584    | 98.70377 9                   |                                    |                          | 9,99734<br>99,9971                  |
| 9  |                    | 91.70479 9<br>91.59002 9 |                          | 2.67053 9<br>2.55569  |                              | 9.85494 9                          |                          | 9.99685                             |
| 63<br>64                                 |                    |                          |                          | 2.44134               | 98.5399 9                    | 9.84069 9                          | 9.97481 9                | 9.99631                             |
| 181                                      | 63 9               |                          | 1.84568 9                | 2.21402 9             |                              | 9.82567 9                          |                          | 9.99569<br>9.99536                  |
| 67                                       | 64 5               | 1.02333 9                |                          |                       |                              |                                    | 9.96817                  | 99.995                              |
| 68<br>69<br>70<br>71                     |                    | 0.79992 9<br>0.68889 9   | 1.39492 9                | 1.76491 5             | 8.28417 9<br>8.24049 9       |                                    | 9.96445 9                | 9.99424                             |
| .72                                      | 69 9               |                          | 1.17229 9<br>1.06165 9   |                       | 0.19652 9                    | 9.77398 9                          |                          | 9,99339                             |
| 7  |                    |                          | 0.95145 9                |                       | 8.10778 9                    | 9.75786 9                          | 9.95617 9                | 9.99245<br>9.99195                  |
| 윊  |                    | 0.14045 9<br>0.03207 9   |                          |                       | 8.01799 9<br>7.97272 9       | 9.73295 9                          | 9.95159 9                | 9.99142                             |
| 77 79 79 79 79 79 79 79 79 79 79 79 79 7 | 74 8               | 9.92413 9<br>9.81661 9   |                          |                       | 7.92721 9                    | 7.71927 9                          | 9.94671 9                | 9.990 <u>29</u><br>9.9 <b>09</b> 68 |
| 22                                       | 76 8               | 9.70951 9                |                          |                       | 7.83549                      | 9.6988 9                           | 9.94152 9                | 9.90905<br>9.90039                  |
| 出  |                    | 9.49657                  | 90.0854 9                | 0.45966 9             | 7.74287 9                    | 67755 9                            | 9.93602                  | 9.9377                              |
| 낊  | 80 8<br>81 8       | 9.28529 85<br>9.18026 85 | 9.87309 90<br>9.76755 90 | .24798                |                              | .65552 9                           | 9,93019 9                |                                     |
| 麗  | 83                 | 9.07563 85<br>88.9714 85 | 0.55768 85               | 93346                 | 7.55513   99<br>97.5077   99 | 63271 9                            | 9,92403 95<br>9,92082 9  | 9.58464<br>9. 0838                  |
| H  | 84 B               | 8.86758 89<br>8.76414 8  | 9.45334 B5               | .72575                | 7.46009 99<br>97.4123 99     | 59703 99                           | 91753 95                 | 98293                               |
| 8  | 86<br>87 8         | 88.6611 89<br>8.55845 85 | 0.24585 89<br>0.14269 89 | 62248 9               | 7.36433 99<br>7.31619 99     | 58474 99                           | 91069 9                  | 98107                               |
| 92                                       | 88 8               | 8.45619 85<br>8.3543 88  | 0.03991 / 89             | 41708 Q               | 7 76780 0                    | 9.5596 5                           | 9.9035 99                |                                     |
| 83<br>84<br>85                           | 91 8               | 8.2528 84<br>8.15168 84  | .83552 8<br>.73389 89    | 9.2132 9              | 97.1708 99<br>7.12202 99     | 53368 99                           | .89596 99                | 97695                               |
| 261                                      | 92 85<br>93 87     | 1.05093 88<br>7.95056 88 | .63263 89<br>.53175 88   | .91018 97             | 7.07309 99<br>7.02402 99     | .50699 99<br>.49336 99             | .88805 99<br>.88396 99   | 97466                               |
| 97<br>98                                 | 941 87             | 7.85055 88<br>7.75092 8  | 43124 22                 | 80991 9               | .97481 99                    | 47953 99                           | .87977 99<br>9.8755 99   | 97221                               |
| 99<br>100                                |                    |                          |                          |                       | .87398 99<br>.82637 99       |                                    | 87113 9                  | 9.9696                              |
| 101<br>102                               | 98   87            | .45418 88<br>.35599 87   | .03286   88              | 41243 96              | 77664 99                     | 42234 9                            | 9.8621 99                | 96682<br>9674                       |
| 103<br>104                               | 100 87             | .25815 87<br>.16066 87   | 83582 88                 | 21583 96              |                              | 3926 99                            | 85260 90                 | 96.384                              |
| 105<br>106                               |                    | .06352 8<br>.96674 87    | 7.6402 88<br>54291 87    | 02061 96<br>92352 04  | .57652 99.                   | 36212 9<br>3.3466 99               | 9.8429 99                | 96073                               |
| 107                                      | 104 86             | 77419 87                 | 44597 87<br>34937 87     | 82678 9               | 6.4758 9                     | 3309 99.                           | .83271 99.<br>82747 99.  | 95741                               |
| 109                                      | 106 86             | .67843 87                | 25311 B                  | 7.6343 96             |                              | 29891 99                           | 82214 99.                | 95389                               |
| 110<br>111<br>112                        | 109 86             | 48792 87.<br>39317 86    | 06161 27.<br>96637 27    | 44316 96<br>34889 96  | .27317 99.<br>.22228 95      | 26623 99.                          | 9.8167 99.<br>81116 99.  | 95018                               |
| 113                                      | 110 86             | 29875 86.                | 87145 87.<br>77687 87.   | 25334 9               | 6.1713 99                    | .2328 99.                          |                          | 94627                               |
| 114<br>113<br>116                        | 112 86             |                          | 68361 87.                | 06483 9               | 6.0691 99.                   | 21581 99.<br>19863 99.<br>1813 99. | 78799 99.                | 94214                               |
| 1176                                     | 114 85.<br>115 85. | 92433 86.<br>83154 86.   | 49507 86.1<br>40178 86.1 | 87761 95.<br>78448 95 | 96659 99.                    | 6377 99.                           | 77579 95                 | 99.94<br>1.9378<br>93555            |
| 119<br>119<br>120                        | 116 B5             | 73906 86.<br>5.6469 86.  | 30881 86.0<br>21616 86.0 | 9166 95.              | 86378 99.<br>81228 99.       | 2819 99.                           | 76318 99                 | 93325                               |
| 121<br>122                               | 118 85.            | 55905 86.<br>46352 86.   | 2383 86.                 | 50697 95.             | 76071 99                     | .0919 99.                          | 75016 99.                | 72846                               |
| 23                                       | 120 1              | 3723 85                  | .9401 86.                | 2352 95               | 70907 99<br>65737 99.0       | .0735 99.°<br>2492 99.°            | 74349 99.9<br>73672 99.9 | 7345                                |

$$\rho = 2000 \text{ kg/m}^3 \qquad c = 960 \frac{J}{\text{kg} \cdot {}^{\circ}\text{C}} \qquad k = 1.04 \frac{W}{\text{m} \cdot {}^{\circ}\text{C}}$$

$$\frac{1}{R_{12}} = \frac{kA}{\Delta x} = \frac{(1.04)(0.005)}{0.002} = 0.26$$

$$\frac{1}{R_{13}} = \frac{(1.04)(0.02)}{0.01} = 2.08$$

$$C_i = \rho_i c_i V_i$$

| Node | $V_{i}$ | $C_i$ | $\sum rac{1}{R_{ij}}$ | $\Delta	au_{ m max}$ |
|------|---------|-------|------------------------|----------------------|
| 1    | 0.0001  | 192   | 3.6                    | 53.3                 |
| 2    | 0.00005 | 96    | 2.05                   | 46.8                 |
| 3    | 0.0002  | 384   | 5.2                    | 73.8                 |
| 4    | 0.0001  | 192   | 3.1                    | 61.9                 |

$$\frac{1}{R_{1-\infty}} = (50)(0.02) = 1.0$$

$$\frac{1}{R_{2-\infty}} = (50)(0.015) = 0.75$$

$$\frac{1}{R_{4-\infty}} = (50)(0.01) = 0.5$$

$$\frac{1}{R_{34}} = \frac{(1.04)(0.01)}{0.02} = 0.52$$

$$\frac{1}{R_{24}} = \frac{(1.04)(0.01)}{0.01} = 1.04$$

$$k = 204 c = 896 \rho = 2707 T_{\infty} = 20^{\circ}\text{C} d = 2.5 \text{ cm}$$

$$\frac{\Delta x = 4 \text{ cm}}{R_{m-1}} = \frac{kA}{\Delta x} = \frac{(204)\pi (0.0125)^2}{0.04} = 2.503$$

$$\frac{1}{R_{\infty}} = hA = 50 \left[ \pi \left( \frac{0.04}{2} \right) (0.025) + \pi (0.0125)^2 \right] = 0.1031$$

$$\sum \frac{1}{R} = 2.6065$$

$$C = \rho c \Delta V = (2707)(896)\pi (0.0125)^2 (0.02) = 23.812$$

$$\Delta \tau_{\text{max}} = \frac{23.812}{2.6065} = 9.1356 \text{ sec}$$

$$T_m^{p+1} = \frac{\Delta \tau}{23.812} [2.503T_{m-1}^p + 0.1031(20)] + \left(1 - \frac{\Delta \tau}{9.1356}\right) T_m^p$$

$$\frac{1}{R_{31}} = \frac{kA}{\Delta x} = \frac{(2.32)(0.01)}{0.01} = 2.32$$

$$\frac{1}{R_{35}} = \frac{(0.48)(0.01)}{0.01} = 0.48$$

$$\frac{1}{R_{3-\infty}} = hA = (50)(0.01) = 0.5$$

$$\sum \frac{1}{R_3} = 2.32 + 0.48 + 0.5 = 3.3$$

$$C_3 = (3000)(0.005)(0.01)(840) + (1440)(0.005)(0.01)(1000) = 198$$

$$\Delta \tau_{\text{max}} = \frac{198}{3.3} = 60 \text{ sec}$$

$$T_3^{p+1} = [2.32(T_1^p - T_3^p) + 0.48(T_5^p - T_3^p) + 0.05(40 - T_3^p)] \frac{\Delta \tau}{198} + T_3^p$$

$$\frac{1}{R_{m+}} = \frac{kA}{\Delta x} = \frac{1}{2}k = \frac{1}{R_{m-}}$$

$$\frac{1}{R_{n-}} = k \qquad \frac{1}{R_{n+}} = hA = h\Delta x$$

$$T_{m, n}^{p+1} = \frac{\Delta \tau}{C_{m, n}} \left[ \frac{k}{2} (T_{m-1, n}^p + T_{m+1, n}^p + 2T_{m, n-1}^p) + h\Delta x T_{\infty} \right]$$

$$+ \left[ 1 - \frac{\Delta \tau}{\Delta \tau_{\text{max}}} \right] T_{m, n}^p$$

$$\frac{1}{R_{12}}\Big|_{A} = \frac{kA}{\Delta x} = \frac{(20)(0.02)}{0.02} = 20 \qquad T_{\infty} = 30^{\circ}\text{C} \qquad \frac{1}{R_{13}} = \frac{(20)(0.01)}{0.04} = 5$$

$$\frac{1}{R_{12}}\Big|_{B} = \frac{(1.2)(0.02)}{0.02} = 1.2 \qquad \frac{1}{R_{14}} = \frac{(1.2)(0.01)}{0.04} = 0.3$$

$$\frac{1}{R_{1-\infty}} = hA = (40)(0.02) = 0.8$$

$$\sum \frac{1}{R_{1-j}} = 27.3$$

$$C_{1} = \sum \rho c\Delta V = (7800)(460)(0.01)(0.02) + (1600)(850)(0.01)(0.02) = 989.6$$

$$\Delta \tau_{\text{max}} = \frac{989.6}{27.3} = 36.25 \text{ sec}$$

$$T_{1}^{p+1} = \frac{\Delta \tau}{C_{1}} [5T_{3}^{p} + 21.2T_{2}^{p} + 0.3T_{4}^{p} + (0.8)(30)] + \left[1 - \frac{\Delta \tau}{36.25}\right] T_{1}^{p}$$

$$\frac{1}{R_{13}} = \frac{(1.2)(0.0225)}{0.02} = 1.35$$

$$\frac{1}{R_{1-7}}\Big|_{B} = \frac{(1.2)(0.01)}{0.03} = 0.4$$

$$\frac{1}{R_{1-7}}\Big|_{C} = \frac{(0.5)(0.005)}{0.03} = 0.0833$$

$$\frac{1}{R_{12}}\Big|_{B} = \frac{(1.2)(0.01)}{0.015} = 0.8$$

$$\frac{1}{R_{1-2}}\Big|_{A} = \frac{(20)(0.05)}{0.015} = 6.6667$$

$$\frac{1}{R_{1-4}}\Big|_{C} = \frac{(0.5)(0.015)}{0.01} = 15.0$$

$$\sum \frac{1}{R_{1}} = 25.05$$

$$C = C_{A} + C_{B} + C_{C} = (7800)(460)(0.005)(0.0075) + (1600)(850)(0.0225)(0.01)$$

$$+ (2500)(800)(0.005)(0.015)$$

$$= 590.55$$

$$\Delta \tau_{\text{max}} = \frac{590.55}{25.05} = 23.57 \text{ sec}$$

$$T_{1}^{P+1} = \frac{\Delta \tau}{590.55} [(T_{3}^{P} - T_{1}^{P})(1.35) + (T_{7}^{P} - T_{1}^{P})(0.4833) + (7.4667)(T_{2}^{P} - T_{1}^{P})$$

 $+(15.75)(T_4^p-T_1^p)]+T_1^p$ 

$$\frac{\text{Node } 1}{R_{12}} = \frac{(1.04)(0.02)}{0.01} = 2.08$$

$$\frac{1}{R_{13}} = \frac{(1.04)(0.01)}{0.02} = 0.52$$

$$\sum \frac{1}{R} = (2)(2.08) + (2)(0.52) = 5.2$$

$$C_1 = (2000)(960)(0.01)(0.02) = 384$$

$$\frac{\text{Node } 2}{R_{2}}$$

$$C_2 = \frac{384}{2} = 192$$

$$\frac{1}{R_{2-\infty}} = (60)(0.02) = 1.2$$

$$\frac{1}{R_{24}} = \frac{(1.04)(0.005)}{0.02} = 0.26$$

$$\sum \frac{1}{R} = 2.08 + (2)(0.26) + 1.2 = 3.8$$

$$\frac{\text{Node } 3}{C_3 = (2000)(960)(0.01)(0.015)} = 288$$

$$\frac{1}{R_{34}} = \frac{(1.04)(0.015)}{0.01} = 1.56$$

$$\frac{1}{R_{35}} = \frac{(1.04)(0.01)}{0.01} = 1.04$$

$$\sum \frac{1}{R} = (2)(1.56) + 1.04 + 0.52 = 4.68$$

$$\frac{\text{Node } 4}{C_4 = (2000)(960)[(0.005)(0.015) + (0.005)(0.01)] = 240}$$

$$\frac{1}{R_{4+}} = \frac{(1.04)(0.005)}{0.02} = 0.26$$

$$\frac{1}{R_{4-\infty}} = (60)(0.02) = 1.2$$

$$\frac{1}{R_{46}} = \frac{(1.04)(0.015)}{0.01} = 1.56$$

$$\sum \frac{1}{R} = 0.26 + 0.26 + 1.56 + 1.56 + 1.2 = 4.84$$

$$\frac{\text{Node } 5}{\text{Node } 5}$$
Take all  $\frac{1}{R} = \frac{(1.04)(0.01)}{0.01} = 1.04$ 

$$\sum \frac{1}{R} = 4.16$$

| Node | С   | $\sum \frac{1}{R}$ | $\Delta	au_{ m max, sec.}$ |
|------|-----|--------------------|----------------------------|
| 1    | 384 | 5.2                | 73.85                      |
| 2    | 192 | 3.8                | 50.53                      |
| 3    | 288 | 4.68               | 61.54                      |
| 4    | 240 | 4.84               | 49.59                      |
| 5    | 192 | 4.16               | 46.15                      |

 $C_5 = (2000)(960)(0.01)(0.01) = 192$ 

$$\frac{1}{R_{35}} = \frac{(15)(0.0025)}{0.02} = \frac{1}{R_{31}} = 1.875$$

$$\frac{1}{R_{34}} = \frac{(15)(0.02)}{0.005} = 60$$

$$\frac{1}{R_{4-\infty}} = (25)(0.02) = 0.5$$

$$\sum \frac{1}{R} = 64.25$$

$$T_3 = \frac{(1.875)(T_1 + T_5) + 60T_4 + 0.5T_{\infty}}{64.25}$$

Fraction liquified =  $(1/u_{if}\rho\Delta V)\sum [(T_i - T_i)/R_{ij}]$ 

### 4-84

$$\frac{1}{R_{76}} = \frac{(16)(0.0125)}{0.01} = 20 \qquad \frac{1}{R_{74}} \bigg|_{A} = \frac{(16)(0.005)}{0.01} = 8$$

$$\frac{1}{R_{78}} = \frac{(100)(0.0125)}{0.02} = 62.5 \qquad \frac{1}{R_{74}} \bigg|_{B} = \frac{(100)(0.01)}{0.01} = 100$$

$$\frac{1}{R_{7-10}} \bigg|_{A} = \frac{(16)(0.005)}{0.015} = 5.333 \qquad \frac{1}{R_{7-10}} \bigg|_{B} = \frac{(100)(0.01)}{0.015} = 66.667$$

$$\sum \frac{1}{R_{7-j}} = 262.5$$

$$C_{7} = (7800)(800)(0.005)(0.0125) + (2600)(500)(0.01)(0.0125) = 390 + 162.5$$

$$= 552.5$$

$$\Delta \tau_{\text{max}} = \frac{552.5}{262.5} = 2.1048 \text{ sec}$$

$$\frac{1}{R_{21}} = \frac{(10)(0.005)}{0.02} = 2.5 \qquad \frac{1}{R_{23}} = \frac{2}{4} = 0.5 \qquad \frac{1}{R_{25}} = 10 + 2 = 12$$

$$\frac{1}{R_{2-\infty}} = (40)(0.02) = 0.8 \qquad \sum \frac{1}{R} = 15.8$$

$$C_2 = (6500)(300)(0.01)(0.005) + (2000)(700)(0.01)(0.005) = 167.5$$

$$\Delta \tau_{\text{max}} = 10.601 \text{ sec}$$

$$T_2^{p+1} = [2.5T_1^p + 0.5T_3^p + 12T_5^p + (0.8)(20)] \frac{\Delta \tau}{167.5} + \left(1 - \frac{\Delta \tau}{10.601}\right) T_2^p$$

$$\frac{1}{R_{42}} = \frac{(20)(0.005)}{0.01} = 10 \qquad \frac{1}{R_{43}} = \frac{(20)(0.01)}{0.01} = 20$$

$$\frac{1}{R_{45}} = \frac{(2)(0.005)}{0.02} = 0.5 \qquad \frac{1}{R_{47}} = 10 + \frac{(2)(0.01)}{0.01} = 12$$

$$\frac{1}{R_{4-\infty}} = (50)(0.01 + 0.005) = 0.75 \qquad \sum \frac{1}{R} = 43.25$$

$$C_4 = (7800)(500)(0.01)(0.005) + (1600)(800)(0.005)(0.01) = 259$$

$$\Delta \tau_{\text{max}} = \frac{259}{43.25} = 5.988 \text{ sec}$$

$$T_4^{p+1} = [10T_2^p + 20T_3^p + 0.5T_5^p + 12T_7^p + (0.75)(50)] \frac{\Delta \tau}{C_4} + \left(1 - \frac{\Delta \tau}{5.988}\right) T_4^p$$

$$\frac{1}{R_{14}} = \frac{(200)(0.005)}{0.01} = 100$$

$$\frac{1}{R_{15}} = \frac{(30)(0.005)}{0.015} = 10$$

$$\frac{1}{R_{12}} = \frac{(200)(0.005)}{0.01} + \frac{(30)(0.0075)}{0.01} = 122.5$$

$$\frac{1}{R_{1-\infty}} = hA = (50)(0.0125) = 0.625$$

$$\sum \frac{1}{R_1} = 233.125$$

$$C_1 = (2700)(900)(0.005)(0.005) + (7800)(800)(0.005)(0.0075) = 294.75$$

$$\Delta \tau_{\text{max}} = \frac{294.75}{233.125} = 1.264 \text{ sec}$$

$$T_1^{p+1} = \frac{\Delta \tau}{294.75} [100(T_4^p - T_1^p) + 10(T_5^p - T_1^p) + 122.5(T_2^p - T_1^p) + 0.625(10 - T_1^p)] + T_1^p$$

$$\frac{1}{R_{21}}\Big|_{A} = \frac{(2)(0.005)}{0.02} = 0.5$$

$$\frac{1}{R_{23}}\Big|_{B} = \frac{(20)(0.005)}{0.01} = 10$$

$$\frac{1}{R_{25}}\Big|_{A} = \frac{(2)(0.01)}{0.01} = 2$$

$$\frac{1}{R_{2-\infty}} = hA = (120)(0.005) = 0.6$$

$$\frac{1}{R_{2-j}} = 23.1 \text{ W/°C}$$

$$C_{2} = (1600)(800)(0.005)(0.01) + (7800)(500)(0.005)(0.005) = 161.5 \text{ J/°C}$$

$$\Delta \tau_{\text{max}} = \frac{161.5}{23.1} = 6.991 \text{ sec}$$

$$T_{2}^{p+1} = \frac{\Delta \tau}{161.5} [0.5(T_{1}^{p} - T_{2}^{p}) + 10(T_{3}^{p} - T_{2}^{p}) + 12(T_{5}^{p} - T_{2}^{p}) + 0.6(10 - T_{2}^{p})] + T_{2}^{p}$$

$$k = 16.3$$
  $\rho = 7817$   $C = 460$  see Table 4–2(d)  
 $Bi = \frac{h\Delta x}{k} = \frac{(60)(0.01)}{16.3} = 0.0368$   $F_0 = \frac{\alpha \Delta \tau}{(\Delta x)^2}$   $F_0(3 + Bi) \le \frac{3}{4}$ 

$$\alpha = \frac{16.3}{(7817)(460)} = 4.53 \times 10^{-6}$$

$$F_0 < \frac{\frac{3}{4}}{3.0368} = 0.24697$$

$$\Delta \tau \le \frac{(0.24697)(0.01)^2}{4.53 \times 10^{-6}} = 5.452 \text{ sec}$$

# 4-91

For  $\Delta \tau = 1942$  sec

$$T_1 = 11.912$$

$$T_2 = 11.097$$

$$T_4 = 22.532$$

$$T_5 = 20.329$$

# The Equations

|    | Α   | В | C    | D   |
|----|-----|---|------|---|
| 1  | T1= |   |      | =(((2.6*C2+2.6*C4)*\$C\$7)/14175+(1-\$C\$7/1942)*C1)        |
| 2  | T2= |   |      | =(((2.6*C1+26+5.2*C5)*\$C\$7)/28350+(1-\$C\$7/1942)*C2)     |
| 3  |     |   |      | (1-90 31 1742) (2)  |
| 4  | T4= |   |      | =(((2.6*C1+2.6*38+5.2*C5)*\$C\$7)/28350+(1-\$C\$7/2726)*C4) |
| 5  | T5= |   |      | =(5.2*((C2+C4+38+10)*\$C\$7)/56700+(1-\$C\$7/2726)*C5)      |
| 6  |     |   |      | 7   |
| _7 | Dt= |   | 1942 |   |

|     | G    | 11       | <del>- , -</del> |   |          |          |
|-----|------|----------|------------------|---|----------|----------|
| 1   | Time | H<br>T1= | I                | J | K        | L        |
| 1 2 | incr | 111=     | T2=              |   | T4=      | T5=      |
| 3   | 0    | 10       |                  |   | -        |          |
| 14  |      |          | 10               |   | 10       | +        |
| 5   | 1    | 7.124092 |                  |   | 14.98696 |          |
| 6   | 2    | 7.87606  |                  |   | 17.68539 | 16.7972  |
| 1 7 | 3    | 9.287557 | 9.167008         |   | 19.24021 | 18.02358 |
|     | 4    | 10.11878 | 9.85524          |   | 20.3756  |          |
| 8   | 5    | 10.76837 | 10.27696         |   | 21.12387 | 19.33766 |
| 9   | 6    | 11.18512 | 10.58706         |   | 21.64916 | 19.703   |
| 10  | 7    | 11.48269 | 10.79142         |   | 22.0046  | 19.95685 |
| 11  | 8    | 11.68209 | 10.93484         |   | 22.25025 | 20.12956 |
| 12  | 9    | 11.82068 | 11.03187         |   | 22.41793 | 20.24853 |
| 13  | 10   | 11.91497 | 11.09893         |   | 22.53321 | 20.32989 |
| 14  | 11   | 11.97992 | 11.14471         |   | 22.61214 | 20.38577 |
| 15  | 12   | 12.02434 | 11.17618         |   | 22.66631 | 20.42405 |
| 16  | 13   | 12.05485 | 11.19773         |   | 22.70344 | 20.45031 |
| 17  | 14   | 12.07575 | 11.21251         |   | 22.72891 | 20.46831 |
| 18  | 15   | 12.09009 | 11.22265         |   | 22.74637 | 20.48066 |
| 19  | 16   | 12.09992 | 11.2296          |   | 22.75834 | 20.48913 |
| 20  | 17   | 12.10666 | 11.23437         |   | 22.76655 | 20.49493 |
| 21  | 18   | 12.11128 | 11.23764         |   | 22.77218 | 20.49891 |
| 22  | 19   | 12.11445 | 11.23988         |   | 22.77604 | 20.50164 |
| 23  | 20   | 12.11663 | 11.24141         |   | 22.77869 | 20.50351 |
| 24  | 21   | 12.11812 | 11.24247         |   | 22.7805  | 20.5048  |
| 25  | 22   | 12.11914 | 11.24319         |   | 22.78175 | 20.50568 |
| 26  | 23   | 12.11984 | 11.24368         |   | 22.7826  | 20.50628 |
| 27  | 24   | 12.12032 | 11.24402         |   | 22.78318 | 20.50669 |
| 28  | 25   | 12.12065 | 11.24426         |   | 22.78359 | 20.50698 |
| 29  | 26   | 12.12087 | 11.24442         |   | 22.78386 | 20.50717 |
| 30  | 27   | 12.12103 | 11.24453         |   | 22.78405 | 20.50731 |
| 31  | 28   | 12.12113 | 11.2446          |   | 22.78418 | 20.5074  |
| 32  |      |          | 11.24465         |   | 22.78427 | 20.50746 |
| 33  | 30   | 12.12126 | 11.24469         |   | 22.78433 | 20.5075  |

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# The Equations

|   | Α   | В | С | D               |
|---|-----|---|---|-----------------|
| 1 | T1= |   |   | =(1100+C3+C4)/4 |
| 2 | T2= |   |   | =(600+C3+C4)/4  |
| 3 | T3= |   |   | =(900+C1+C2)/4  |
| 4 | T4= |   |   | =(800+C1+C2)/4  |

| 2 incr 3 0 4 1 5 2 6 3 7 4 5 8 5 5         | 1000<br>775<br>631.25<br>559.375<br>23.4375<br>05.4688 | 1000<br>650<br>506.25<br>434.375<br>398.4375 | J T3= 1000 725 581.25 509.375 | 1000<br>700<br>556.25 |
|--|--|--|-------------------------------|-----------------------|
| 3 0<br>4 1<br>5 2<br>6 3<br>7 4 5<br>8 5 5 | 775<br>631.25<br>559.375<br>23.4375                    | 650<br>506.25<br>434.375                     | 1000<br>725<br>581.25         | 1000<br>700<br>556.25 |
| 4 1 5 2 6 3 7 4 5 8 5 5                    | 775<br>631.25<br>559.375<br>23.4375                    | 650<br>506.25<br>434.375                     | 725<br>581.25                 | 700<br>556.25         |
| 5 2<br>6 3<br>7 4 5<br>8 5 5               | 631.25<br>559.375<br>23.4375                           | 506.25<br>434.375                            | 581.25                        | 556.25                |
| 6 3<br>7 4 5<br>8 5 5                      | 559.375<br>23.4375                                     | 434.375                                      |                               |                       |
| 7 4 5<br>8 5 5                             | 23.4375  |  | 509.375                       | 404.075               |
| 8 5 5                                      |  | 398.4375                                     |                               | 484.375               |
|  | 05.4688  |  | 473.4375                      | 448.4375              |
| 0 4  |  | 380.4688                                     | 455.4688                      | 430.4688              |
| 0 4  | 96.4844  | 371.4844                                     | 446.4844                      | 421.4844              |
| 10 7 4                                     | 91.9922  | 366.9922                                     | 441.9922                      | 416.9922              |
| 11 8 4                                     | 89.7461  | 364.7461                                     | 439.7461                      | 414.7461              |
| 12 9                                       | 488.623  | 363.623                                      | 438.623                       | 413.623               |
| 13 10 4                                    | 88.0615  | 363.0615                                     | 438.0615                      | 413.0615              |
| 14 11 4                                    | 87.7808  | 362.7808                                     | 437.7808                      | 412.7808              |
| 15 12 4                                    | 87.6404  | 362.6404                                     | 437.6404                      | 412.6404              |
| 16 13 4                                    | 87.5702  | 362.5702                                     | 437.5702                      | 412.5702              |
| 17 14 4                                    | 87.5351  | 362.5351                                     | 437.5351                      | 412.5351              |
| 18 15 48                                   | 87.5175  | 362.5175                                     | 437.5175                      | 412.5175              |
| 19 16 48                                   | 87.5088  | 362.5088                                     | 437.5088                      | 412.5088              |
| 20 17 48                                   | 87.5044  | 362.5044                                     | 437.5044                      | 412.5044              |
| 21 18 4                                    | 87.5022  | 362.5022                                     | 437.5022                      | 412.5022              |
|  | 37.5011  | 362.5011                                     | 437.5011                      | 412.5011              |
| 23 20 48                                   | 37.5005  | 362.5005                                     | 437.5005                      | 412.5005              |
| 24 21 48                                   | 37.5003  | 362.5003                                     | 437.5003                      | 412.5003              |
| 25 22 48                                   | 37.5001  | 362.5001                                     | 437.5001                      | 412.5001              |
| 26 23 48                                   | 37.5001  | 362.5001                                     | 437.5001                      | 412.5001              |
| 27 24 4                                    | 187.500  | 362.500                                      | 437.500                       | 412.500               |
| 28 25 4                                    | 187.500  | 362.500                                      | 437.500                       | 412.500               |
| 29 26 4                                    | 187.500  | 362.500                                      | 437.500                       | 412,500               |
| 30 27 4                                    | 87.500   | 362.500                                      | 437.500                       | 412.500               |
| 31 28 4                                    | 87.500   | 362.500                                      | 437.500                       | 412.500               |
| 32 29 4                                    | 87.500   | 362.500                                      | 437.500                       | 412.500               |
| 33 30 4                                    | 87.500   | 362.500                                      | 437.500                       | 412.500               |

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|                   | $\Delta 	au_{	ext{max}}$ |
|-------------------|--------------------------|
| $C_1 = 89.7$      | 3.5666                   |
| $C_2 = 44.85$     | 3.8114                   |
| $C_3 = 179.4$     | 3.5880                   |
| $C_4 = 89.7$      | 3.5455                   |
| $C_5 = 179.4$     | 3.5880                   |
| $C_6 = 89.7$      | 3.5455                   |
| $C_7 = 179.4$     | 3.5880                   |
| $C_8 = 89.7$      | 3.5455                   |
| $C_9 = 179.4$     | 3.5880                   |
| $C_{10} = 224.25$ | 6.6527                   |
| $C_{11} = 224.25$ | 10.5737                  |
| $C_{12} = 89.7$   | 8.8374                   |
| $C_{13} = 179.4$  | 3.5880                   |
| $C_{14} = 358.8$  | 7.6885                   |
| $C_{15} = 448.5$  | 10.7639                  |
| $C_{16} = 179.4$  | 8.9700                   |
|                   |                          |

# The Equations

| _  | I A  | В | Гс     | T D   |
|----|------|---|--------|---|
| 1  | T1=  |   |        | =C1+(\$C\$18/89.7)*(((C3-C1)/0.2)+2*((C2-C1)/0.1)+((10-C1)/6.67))                                     |
| 2  | T2=  |   | 1      | =C2+(\$C\$18/44.85)*(((C1-C2)/0.1)+((C4-C2)/0.4)+((10-C2)/4.44))                                      |
| 3  | T3=  |   |        | =C3+(\$C\$18/179.4)*(((C1-C3)/0.2)+2*((C4-C3)/0.05)+((C5-C3)/0.2))                                    |
| 4  | T4=  |   |        | =C4+(\$C\$18/89.7)*(((C2-C4)/0.4)+((C3-C4)/0.05)+((C6-C4)/0.4)+((10-C4)/3.33))                        |
| 5  | T5=  |   |        | -C5+(\$C\$18/179.4)*(((C3-C5)/0.2)+2*((C6-C5)/0.05)+((C7-C5)/0.2))                                    |
| 6  | T6=  |   |        | =C6+(\$C\$18/89.7)*(((C4-C6)/0.4)+((C5-C6)/0.05)+((C8-C6)/0.4)+((10-C6)/3.33))                        |
| 7  | T7=  |   |        | -C7+(\$C\$18/179.4)*(((C5-C7)/0.2)+2*((C8-C7)/0.05)+((C9-C7)/0.2))                                    |
| 8  | T8=  |   |        | -C8+(\$C\$18/89.7)*(((C6-C8)/0.4)+((C7-C8)/0.05)+((C10-C8)/0.4)+((10-C8)/3.33))                       |
| 9  | T9=  |   |        | =C9+(\$C\$18/179.4)*(((C7-C9)/0.2)+2*((C10-C9)/0.05)+((C13-C9)/0.2))                                  |
| 10 | T10- |   |        | -C10+(\$C\$18/224.25)*(((C8-C10)/0.4)+((C9-C10)/0.05)+((C14-C10)/0.1)+((C11-C10)/0.3)+((10-C10)/2.67) |
|    | T11- |   |        | =C11+(\$C\$18/224.25)*(((C10-C11)/0.3)+((C15-C11)/0.08)+((C12-C11)/0.2)+((10-C11)/2.67))              |
|    | T12= |   |        | -C12+(\$C\$18/89.7)*(((C11-C12)/0.2)+((C16-C12)/0.2)+((10-C12)/6.67))                                 |
|    | T13= |   |        | -C13+(\$C\$18/179.4)*(((C9-C13)/0.2)+2*((C14-C13)/0.05)+((200-C13)/0.2))                              |
|    | T14= |   |        | -C14+(\$C\$18/358.8)*(((C10-C14)/0.1)+((C13-C14)/0.05)+((C15-C14)/0.15)+((200-C14)/0.1))              |
|    | T15= |   |        | =C15+(\$C\$18/448.5)*(((C11-C15)/0.08)+((C14-C15)/0.15)+((C16-C15)/0.1)+((200-C15)/0.08))             |
|    | T16= |   |        | =C16+(\$C\$18/179.4)*(((C12-C16)/0.2)+((C15-C16)/0.1)+((200-C16)/0.2))                                |
| 17 |      |   |        |   |
| 18 | Dt=  | L | 3.5455 |   |

|   | E          | G        |     | H<br>Ti=               | T2-                      | ]<br> T3=  | K<br>T4=             | L<br>TS=    | M          | N                        | 0                        | P                        | Q                        | R                        | S                    | Ţ                      | Ü                      | Ιv                       | w        |
|---|------------|----------|-----|------------------------|--------------------------|------------|----------------------|-------------|------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|----------------------|------------------------|------------------------|--------------------------|----------|
| 1   |            |          |     | 100                    |                          |            |                      |             | T6-        | T7-                      | T9-                      | T9=                      | T10=                     | T11=                     | T12=                 | T13-                   | T14-                   | T15=                     | T16=     |
| 1   |            | 4.       | 1   |                        |                          |            |                      |             |            |                          |                          |                          |                          |                          |                      |                        |                        |                          | 200      |
| 1   |            |          |     |                        |                          |            |                      | 198.2172    | 197.2991   | 198.2172                 | 197.4108                 | 199.1106                 | 198.2455                 |                          | 197.9775             |                        |                        |                          |          |
| 1   |            | 7        | 4   | 192.8196               | 191.6322                 | 195.6559   | 194.4343             | 196.1444    |            |                          |                          |                          |                          |                          |                      |                        |                        |                          | 199.7109 |
| 10  |            |          |     |                        |                          |            |                      |             |            | 195.6088                 | 194.0394                 | 197.216                  | 196.4878                 | 196.1256                 | 196.0903             | 199.4523               | 199.3775               |                          | 199.2623 |
| 1   |            |          | 7   | 188.316                |                          | 191.7774   | 190.3809             | 192.8584    | 191.4944   | 193.7171                 |                          |                          |                          |                          |                      |                        |                        |                          | 199.0236 |
| 1.   1.   1.   1.   1.   1.   1.   1.   |            | 2        | 9   | 185.4894               | 184.1606                 | 189.1676   |                      |             |            |                          |                          |                          | 194.995                  | 194.858                  | 194.8206             | 198.7626               | 198.7015               | 198.5758                 | 198.5558 |
| 1.  |            |          |     |                        |                          |            | 186.5606             | 189.5742    | 188.2024   | 191.0215                 | 189.7815                 |                          |                          |                          |                      |                        |                        |                          |          |
| 1   |            | 5        | 12  | 181.5175               | 180.2337                 |            |                      |             |            |                          | 188.899                  |                          |                          |                          |                      | 198.0613               | 198.0072               | 197.9355                 | 197.9176 |
| 1   |            |          |     |                        |                          |            | 182.8592             |             |            | 188.6542                 | 187.3232                 | 193.3448                 | 192.8754                 | 193.2882                 | 193.2989             | 197.6078               |                        |                          |          |
| 1   | 11         | 1        | 15  | 177.7869               | 176.5383                 | 181.7969   | 180.4968             |             |            |                          |                          |                          |                          |                          |                      |                        |                        |                          | 197.3669 |
| 1   |            |          |     |                        |                          |            |                      |             | 182.0046   |                          | 185.1017                 | 192.1215                 | 191.7407                 | 192.5341                 | 192.5889             | 196.9653               | 196.9359               |                          |          |
| 12   12   12   12   12   13   13   13   | 2          | 1        | 18  | 174.2686               | 173.0282                 | 178.3544   | 177.1115             | 181.3661    | 180.0625   |                          |                          |                          |                          |                          |                      |                        |                        |                          |          |
| 13  | 23         | 9        |     |                        |                          |            |                      |             |            |                          | 182.9467                 | 190.9793                 | 190.6995                 | 191.8779                 | 191.9824             | 196.3741               | 196.3586               |                          |          |
| 1.   1.   1.   1.   1.   1.   1.   1.   | 24         | 1        | 21  | 170.909                | 169.7179                 | 175.1107   | 173.8597             | 178.5246    | 177.2884   |                          |                          |                          |                          |                          |                      |                        |                        |                          |          |
| 1   |            |          | -   |                        |                          |            |                      |             |            | 182.1641                 | 180.9557                 | 189.928                  | 189.7344                 | 191.3007                 | 191.457              | 195.8295               | 195.8297               | 196.1904                 |          |
| 18  | 27         |          |     |                        | 166.5478                 | 171.9954   | 170.7996             | 175.8662    | 174.6116   |                          | 179.6779                 | 189.2671                 | 189.1323                 | 191.1233                 | 191.1439             | 195.6586               |                        |                          |          |
| 15  | 29         |          | 26  |                        |                          |            |                      |             |            | 180.263                  | 179.0447                 | 188.9465                 | 188.8435                 | 190.7885                 | 190.9972             | 195.33                 | 195.3445               | 195.8402                 | 195.9206 |
| 12   15   15   15   15   15   15   15   |            |          |     |                        |                          |            | 167.8607             | 173.3084    | 172.106    | 179.0454                 | 177.8408                 |                          |                          |                          |                      |                        |                        |                          |          |
| 12   13   14   14   15   15   15   15   15   15   | 32         |          | 19  |                        |                          |            |                      |             |            |                          |                          |                          |                          | 190.3307                 | 190.5912             | 194.8698               | 194.8991               | 195.5283                 | 195.6345 |
| 15   15   15   15   15   15   15   15   |            |          | -   |                        |                          | 166.2524   | 165.0979             | 170.9122    | 169.6997   | 177.2964                 | 176.1288                 | 187.4666                 | 187.4975                 | 190.0515                 | 190.346              |                        |                        |                          |          |
| 13  | 35         | 3        | 2   | 160.0139               | 158.8776                 | 164.4658   | 163.324              |             |            |                          |                          | 187.1893                 | 187.2483                 | 189.9189                 |                      |                        | 194.489                | 195.2488                 | 195.3805 |
| 13   19   19   19   19   19   19   19   | 37         | 1 3      |     |                        |                          |            |                      |             |            | 175.6638                 | 174.4959                 | 186.6568                 | 186.7664                 | 189.6667                 | 90.0107              |                        |                        |                          |          |
| March   Marc  | 38         | 3        |     | 157.3642               | 156.2742                 | 161.9115   | 160.7631             | 167.1589    |            |                          |                          | 186.4007                 | 186.5334                 | 189.5466                 |                      |                        |                        |                          |          |
| 14   15   15   15   15   15   15   15   |            |          |     |                        |                          |            |                      |             |            | 174.1064                 | 172.9699                 | 185.9035                 | 186.0846                 | 189.3175                 | 89.7093              | 93.8092                | 193.8746               | 194.8424                 | 95.0829  |
| 4. 4   15   15   17   17   18   18   18   18   18   18  |            |          | 8   | 154.873                | 153.7766                 | 159.4629   | 158.3566             | 165.0802    | 163.9154   |                          |                          | 185.6623                 | 185.8683                 | 189.2081 1<br>189.1021 1 |                      |                        | 193.761                |                          |          |
| 44   15,4640   31,4292   17,1617   15,6098   10,0095   16,1690   17,1617   17,987   17,1617   18,1618   18,1617   17  |            |          |     |                        |                          | 158.6899   |                      |             |            | 172.6532                 | 171.5171                 | 185.1978                 | 85.4495                  | 188.9991 1               | 89.4368              | 93.4644                | 93.5421                |                          |          |
| 44   150,9575   150,7575   151,7575   152,7576   153,7577   152,7577   153,7577   152,7577   153,75  |            | 4        | 1   | 52.4843                | 151.4292                 | 157.1617   | 156.0508             | 63.0925     | 161.9609   |                          |                          | 184.7535                 | 85.0494                  |                          |                      |                        |                        |                          |          |
| 14   15,02,092   14,04,096   15,05,096   15,05,096   16,05,097   16,05,097   16,05,097   16,05,007  |            |          |     |                        |                          |            |                      |             |            |                          | 170.157                  | 184.5394                 | 84.8557                  | 88.7077 1                | 89.1891 1            | 93.1437                | 93.2335                | 94.4325                  | 94.6507  |
| 46   464   7994   177968   157597   152295   100000   197407   18850   187707   18850   18850   18860   192405   192407   18950   18  |            |          |     |                        | 149.1792                 | 154.9584   | 153.884              | 61.2266     | 160.093    | 70.3927                  |                          | 84.1233 1                | 84.4815                  | 88.5267 1                | 89.1115<br>89.0361 1 |                        |                        |                          |          |
| 10   14   147   148   158   | 49         |          |     |                        |                          |            | 153.1741<br>152.4952 | 60.6168 1   | 59.5028 1  |                          |                          | 83.9212 1                | 84.3009                  | 88.4398                  | 188.963 1            | 92.8454                | 92.9465                | 94.2532 1                | 94.4928  |
| 14   14   15   15   15   15   15   15   |            |          |     |                        | 147.0648                 | 152.8874   | 51.8102 1            | 59.4447     | 58.3391    | 69.1439                  | 68.0443 1                | 83.5311 1                | 83.9505                  | 188.273 1                | 88.8229 1            | 92.6578 1              |                        |                          |          |
| 1.50   166.6674   145.9661   145.967   195.8661   157.771   156.6669   157.967   167.771   157.967   187.972   187.973   186.0577   187.972   187.973   18  | 52         | 45       | 9 1 | 46.7234                | 145.7092                 | 151.5606   | 50.4939 1            | 58.3146 1   |            |                          |                          | 83.3429 1                | 83.7807                  |                          | 88.7557              | 92.5671                | 192.679 1              | 94.0882 1                | 94.3482  |
| 55 . 39 144.7722 143.7553 149.6447 167.757 145.7570 153.6264 175.757 145.047 175.757 145.157 145.157 145.247 1  |            |          |     |                        | 145.0403                 | 50.9067    | 49.8611              | 157.771 1   | 56.6649 1  | 67.9567                  | 66.8767 1                | 82.9768 1                | 83.4524 1                | 88.0387 1                |                      |                        |                        |                          |          |
| Section   18.1577   148.0447   147.977   151.741   155.092   166.0425   167.056   182.453   187.255   187.265   187.265   197.277   197.860   157.277   197.265   197.277   197.265   197.277   197.265   197.277   197.265   197.277   197.265   19  | 55         | 52       | 1   | 44.7722                | 143.7553 1               | 49.6494    | 48.6127 1            |             |            |                          |                          |                          |                          |                          |                      |                        |                        |                          |          |
| Section   14,900   14,900   14,900   14,900   14,900   15,161   15,161   15,161   15,161   15,161   15,161   16,065   16,000   16,000   16,000   17,175   18,000   18,000   19,000   19,000   19,000   10,000   |            | 54       |     |                        |                          |            |                      |             | 155.092 1  | 66.8425                  | 65.7667 1                | 82.4551 1                | 82.9854 1                | 87.8215 1                | 88.4462 1            | 92.1434                | 192.272 1              | 93.8408 1                |          |
| Column   C  |            |          | 1   | 42.9059                | 141.9187                 | 47.8526 1  | 46.8149              | 155.161 1   | 54.0863 1  | 66.1318 1                |                          |                          |                          |                          |                      |                        |                        |                          |          |
| 52. 39   141.151   140.1629   146.183   145.1247   153.7139   135.1249   145.1247   145.0242   145.7241   145.7241   153.044   137.047   145.9242   144.7241   153.044   137.047   145.0242   144.7241   153.044   137.047   145.0442   144.041   157.048   157.048   157.048   147.047   145.048   145.  | 60         | 57       | 1   | 41.7211                | 140.7424 1               | 46.7024 1  |                      |             |            |                          |                          |                          | 82.5465 1                | 87.6198 11               | 8.2791 19            | 91.9106 1              | 92.0486 1              | 93.7068 19               | H.0163   |
| 50   140,002   195,048   145,049   145,049   145,049   145,049   152,789   157,722   184,4657   163,469   181,577   182,772   173,772   181,772   181,772   193,973   193,742   193,772   183,797   143,797   143,797   143,797   143,797   143,797   143,797   143,797   143,797   143,797   153,797   143,797   143,797   153,797   143,797   143,797   153,797   143,797   153,797   143,797   143,797   143,797   143,797   143,797   143,797   143,997   |            |          | -   |                        |                          | 46.1363 1  | 45.1247 1            | 53.7139 1:  | 52.6399 1  | 65.1122 1                | 54.0597 1                | 81.6553 1                | 82.2687 1                |                          |                      |                        |                        |                          |          |
| 195   195   1348   1341   1377   143.999   144.999   144.999   151.979   195.979   1  | 63         | 60       | Ĺ   | 140.028                | 139.0483                 | 45.0469    | 144.043 1.           | 52.7889 1   | 51.7223 1  | 64.7886 16<br>64.4657 16 | 63.7339 11<br>63.4196 11 | 81.5044 18<br>81.3572 18 | 82.1342 1:<br>82.0021 1: |                          |                      | 1.6925                 | 91.8393 1              | 93.5822 19               | 3.9086   |
| 66   53   138,4107   137,4356   143,5429   141,5429   151,0572   151,0572   161,0572   1  |            |          |     |                        |                          | 44.5224 1  | 43.5108 1:           | 52.3345 1:  | 51.2803    | 164.154 H                | 53.1059 1                | 81.2123 11               | 81.8729                  | 187.314                  | 88.027 19            | 1.5545                 | 191.707 1              | 93.5039 19               |          |
| 13,7896   15,7896   16,2982   141,991   151,0974   149,946   162,2432   162,2697   181,900   187,997   191,391   1  | 66         | 63       | 1   | 38.4107                | 37.4556 1                | 43.4898 1  | 42.4863 1:           | 51.4592 1   |            | 63.5428                  |                          |                          |                          |                          |                      |                        |                        |                          |          |
| 69   156.8989   155.9947   142.0043   141.0222   150.2085   149.1527   162.6555   165.077   165.077   165.077   167.073   181.2658   187.0741   187.0831   191.2381  | 68         |          |     | 137.384 I              | 36.4363 1                |            |                      |             |            |                          | 52.2093 11               | 0.7957 18                | 11.5001 1                | 7.1467 18                | 7.8897 19            | 1.3581 19              | 1.5188 1               | 93.3931 19               | 3.7457   |
| 77  | 69         |          | 13  | 6.8898                 | 35.9347 1                | 42.0043 1  | 1.0222 1             | 50.2085 14  | 19.1622 16 | 52.6659 16               | 1.6373 11                |                          |                          |                          |                      |                        |                        |                          |          |
| 12  | 71         | 68       | 13  | 5.9168 1               | 34.9693 1                | 41.0612 1  | 10.0859 14           | 9.4095 14   | B 3695 14  |                          |                          |                          | 1.1493 18                | 6.9901 18                | 7.7616 19            | 1.1736 15              | 1.3419 19              | 3.2896 19                | 3.6568   |
| 14  |            | 69<br>70 | 13  | 5.4383 1<br>4.9782 1   | 34.5045 14               | 40.6068 13 | 10 6258              | 0 0173 14   | 7 0022     | /1 041 1                 |                          |                          |                          |                          |                      |                        | 1.2298 19              | 73.2366 19<br>73.2243 19 | 3.6285   |
| 73   133,048   132,7072   138,8516   137,8482   147,5322   146,5313   160,8079   159,794   179,6422   180,006   187,7559   190,8364   191,0189   193,1019   193,9461   175,9472   147,9482   175,948  | 74.1       | 71       | 13  | 4.5168 1               | 33.5896 13               | 9.7133 13  | 8.7392 14            | 8.2612 14   | 7.2367 16  | 51.3148 16               | 0.5557 18<br>0.2958 17   | 0.0325 18                | 0.8184 18                | 6.8435 18                | 7.6419 19            | 0.9999 19              | 1.1755 19              | 3.1927 19                | 3.5738   |
| 77  | 1761       | 73       | , 1 | 33.628   1             | 32 7072   13             | 18 8516 15 | 7 8642 14            | 7 5222 1    | 46 610 10  |                          |                          | 7.777                    | 0.0007 10                | 0.7307 10                | 7.3000 17            | U.8676                 | 171.0/1 15             | 9.1315  19               | 3.52148  |
| 79   76   132,3577   131,448   131,0353   137,6177   136,6632   146,490   185,4753   160,0005   159,0773   179,3574   180,1181   180,5356   187,391   190,6823   190,891   190,981   190,9  | 77         | 74       | 13  | 3.1998 1               | 32.2735 13               | 8.4285 13  | 7.4721 14            | 7.1806 14   | 6.1581 16  | 0.5598 15                | 9.5519 17                | 9.5711 18                | 0.4065 18                | 6.6621 18                | 7.5299 19            | 0.8364 19<br>90.784 19 | 1.0189 19<br>0.9687 19 | 3.1019 19                | 3.4961   |
| 131   134   131   10333   137   139   136   13  | 70         | 76       | 13  | 2.3577                 | 131.438 13               | 7 6127 13  | 6 6621 14            | 6 4904 14   | 5 4723 16  | 0.9195 15                | 9.3108 17                | 9.40UY 18                | 0.3086                   | 86.619 18                | 7.4591 19            | 0.7327 19              | 0.9196 19              | 3.0445 19                | 3.4471   |
| 19   13   1468   130   2438   136   2445   135   2478   145   2489   145   2499  | 80         | 77       | 13  | 1.9441 1               | 31.0353 13               | 7.2192 13  | 6.2646 1             | 46.152 14   | 5.1429 1   | 59.849 1                 | 58.845 17                | 9.2474 18                | 0.1181 18                | 6.5356 18                | 7.3914 1             | 0.6823 19<br>90.633 19 | 0.8714 19<br>0.8241 19 | 3.0167 19<br>2.9895 19   | 3.4234   |
| 34         81         130.378         12.4400         135.704         134.7385         144.8604         143.887         182.988         157.959         178.842         179.852         182.787         179.2894         190.2874         190.2481         190.2871         190.3333           85         32         130.0072         129.1058         133.3395         134.4018         144.8664         143.8876         157.559         178.7847         179.7534         186.7877         177.6661         193.312         190.0003         190.0003         190.0641         192.8861         193.312         190.0003         190.0003         190.001         1  | 82         | 79       | 13  | 1.1468 1               | 30 2438 13               | 6 4465 12  | 5 4070 14            | S 4000 14   | 4 4046 15  | 7.010/ []                | 8.0201 17                | 9.1439 18                | 0.0255 18                | 6.4952 18                | 7.3586 190           | 0.5846 19              | 0.7778 19              | 2.9629 19:               | 3.3774   |
| \$\frac{8}{8}\$ \frac{8}{12}\$ \frac{190.0072}{129.1058}\$ \frac{135.3359}{134.0018}\$ \frac{144.5654}{144.5654}\$ \frac{143.5594}{143.2572}\$ \frac{152.755}{157.7682}\$ \frac{17.5755}{175.7682}\$ \frac{17.56725}{175.6725}\$ \frac{18.2587}{184.1872.359}\$ \frac{190.0053}{190.0053}\$ \frac{190.0053}{190 | 湖          | 80       | 13  | 0.7624 1:<br>30.378 1: | 29.8551 13<br>29.4805 13 | 6.0674 1   | 35.128 14            | 5.1837 14   | 4.1768 15  | 9.1738 15                | 8.1795 17                | 8.9423 17                | 9.8456 18                | 6.4167 18                | 7.2949 190           | 0.4906 19              | 0.6878 19              | 2.9112 19                | 3.3333   |
| 84   129.279   128.3832   134.5906   135.7016   143.5695   142.772   183.319   175.3459   178.5371   179.3681   185.3049   187.3043   190.3546   190.5599   192.2705     85   152   152   152   152.6346   134.5020   133.7016   143.5695   142.772   183.319   177.3459   178.5470   179.4521   185.2341   187.1469   192.2711   190.4777   192.7006     85   128.7572   127.5686   133.5025   133.0622   133.9471   142.6866   158.1322   177.1459   178.4704   179.4572   185.2341   187.1469   192.2711   190.4777   192.7008   192.2009     96   177.5975   176.56903   132.7322   132.5694   143.1133   142.1265   137.7413   155.7389   178.2001   179.2861   187.1873   190.1891   190.3291   192.2716     97   127.2467   156.6903   132.9782   132.0564   142.5695   141.3262   157.3646   156.3661   177.812   178.0401   179.0412   186.1232   187.0583   190.1492   190.3591   192.7345   193.1313     94   91   126.9565   126.0599   132.5773   131.4602   142.0585   141.3262   157.1604   156.0066   178.0463   187.0389   190.0441   190.2351   190.0341   190.2351   190.0341   190.2351     95   92   126.56171   137.7419   132.053   131.4402   141.7521   140.8117   156.0341   155.3631   178.0415   179.0421   186.1023   187.0381   190.0441   190.3251   192.6619   193.1381     96   126.5065   126.5444   131.7365   130.8462   141.7521   140.8117   156.0341   155.3631   177.809   178.9051   186.9034   189.9071   190.0441   190.0250   192.6614   193.1209     97   98   126.5106   136.4444   131.1361   130.0441   130.0441   190.0441   | 85         | 82       | 13  | 0.0072 12              | 29.1058 13               | 5.3359 13  | 4 4018 14            | 4 5654 14   | 2 5624 15  | 9 7461 1                 | 57 766 17                | 0.0441 17                | 2.7300 10                | 0.3/8/ 18                | .2041 1              | 90.445 19              | 0.6441 19              | 2.8861 19                | 73.312   |
| 8   128 2716   128 0346   134 2902   133 381   143 5773   142 6864   181 1322   157 1489   177 1489   181 139   191   |            | 84       | 1   | 29.279 12              | 28.3832 13               | 4 6306 13  | 3 7016 14            | 3 0602      | 42 072 16  | 0.3376 13                | 7.34/3 1/                | 8.6537 17                | 9.3886 18                | 6.3049 187               | 2043 190             | 0.3564 196             | 0.5593 19              | 2.8375 193               | .2706    |
| 90 87 128.3222 177.3502 33.6222 122.6955 143.1133 142.1265 157.7413 165.7899 177.2513 179.2673 186.1658 187.0918 190.1891 190.3991 192.7461 193.2116 193.211  | 388        | 85       | 12  | 8.9216 12              | 8.0346 13                | 4.2902 13  | 3.3582 14            | 3.6773 14   | 2.6864 15  | 8.1322 15                | 7.1458 17                | 8.4704 179               | 79.306 18<br>9.4252 1    | 6.2691 187<br>86.234 187 | 11753 190            | 0.3133 190             | 0.5181 19:             | 2.8139 193<br>2.7908 193 | 2505     |
| 91   88   127,8996   177,0145   33,2948   123,7755   142,800   141,852   177,5075   186,5789   178,206   178,207   186,1838   187,918   190,1891   190,3991   192,7499   193,1997   92   99   127,2467   126,5669   122,772   126,5609   122,772   142,800   141,852   177,506   156,5719   178,206   178,124   179,1164   186,1003   187,0389   190,1101   190,3235   192,7023   193,1801   93   126,6717   156,5666   122,6565   131,4787   142,9584   141,9565   157,0016   155,2058   178,1019   179,0477   186,6885   167,032   190,0717   190,286   192,6819   193,1839   95   92   126,6717   157,419   132,035   311,4427   141,9565   141,9564   141,9565   177,8016   178,206   178,207   179,047   186,6817   179,033   190,101   190,286   122,6819   193,1839   95   93   126,6171   157,419   132,035   311,4427   141,9721   40,3117   156,824   158,836   177,803   178,9705   186,9374   186,9631   190,034   190,256   192,6614   193,1209   96   93   126,903   125,404   131,7586   130,8462   141,5401   40,5469   156,6518   155,6605   177,803   178,8705   186,9534   189,997   190,1215   192,6413   193,1038   97   94   126,010   125,136   134,4651   130,5794   141,0554   140,5469   156,6518   155,6407   155,131   177,7562   178,7617   185,974   186,9155   199,923   100,1468   192,6022   191,0707   98   95   125,726   124,4888   131,1814   130,2774   140,0314   139,144   153,146   153,146   177,5762   178,6917   185,974   186,9155   199,353   100,1468   192,6022   191,0707   99   95   125,726   124,4888   131,1814   130,2774   140,0314   139,144   153,146   153,146   177,5762   178,6917   185,9474   186,9155   199,3521   100,007   172,5647   193,0384   100   97   125,1381   124,7478   130,6249   139,7817   139,8447   155,1308   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   139,0344   134,534   130,0344   134,534   130,0344   134,534   130,0344   134,544   130,0344   134,544   130,0344   134,544   130,0344   134,  | 9          | 87       | 12  | 3.2322 12              | 7.3502 13                | 3.6222 13  | 2 6054 14            | 11133 14    | 1266 16    | 7.7412 16                | 2.7317 170               | 8.3813 17                | 7.5457 18                | 1996 187                 | .1191 190            | 2297 19                | 0.438 19               | 2.7681 193               | .2116    |
| 93 90 127.2467 126.3666 122.6266 131.7477 142.3068 141.3254 157.1804 155.2254 178.121 179.0427 186.0681 187.0389 190.1101 190.3225 192.7028 193.1561 178.122 179.0427 186.0681 187.0389 190.1101 190.3225 192.7028 193.1561 178.122 179.0427 186.0681 187.0389 190.1101 190.3225 192.7028 193.1561 193.1029 194.1102   |            | 88       | 12  | 7.8996 12              | 7.0145 13                | 3 2948 13  | 2 3755 14            | 9409 14     | 1 9633 16  | 7.5500 35                | 5.7389 1                 | /8.294 17                | 9.25/8 180               | 5.1638 187               | .0918 190            | 1891 190               | 0.3991 192             | 2.7459 193               | .1927    |
| 94 91 126.995 126.6517 135.7419 132.053 131.4402 142.045 141.0565 157.0016 156.0656 177.0505 178.0705 186.0837 185.981 190.0341 190.0341 190.2988 192.089 195.1889 19  | 93         | 90       | 12  | 7.2467 12              | 6.3666 13                | 2.6626 13  | 7478 14              | 3068 14     | 1 2224 15  | 7.1004 144               | 0.3861 1                 | 78.124 175               | 1164 186                 | . 1003 187               | .0389 190            | 1101 190               | .3235 192              | 2.7028 193               | .1561    |
| 95 93 125.008 125.4404 131.7586 130.8462 141.5401 140.5469 156.6518 155.6605 177.809 178.80 185.9768 185.992 189.9097 190.2155 193.6413 193.1038 197.979 180.008 193.6518 185.6618 177.7562 178.80 185.9768 185.992 189.909 190.1080 1852.616 193.0977 190.2155 189.8092 193.008 193.0  | 95         | 91       | 120 | 6.9265 12              | 6.0539 13                | 2.3573 13  | 1.4402 14            | 2.0454 141  | .0665 15   | 7.0016 150               | 0268 17                  | 7.9603 178               | 19705 186                | .0374 186                | .9881 190            | 0341 190               | .2868 192<br>.2508 192 | 1.6614 193               | .1383    |
| 29 59 52 125 7736 [3 4488] 311.844 [3 10.3597] 141.2959 [40.3193] 156.4807 [155.313] 77.7522 [78.7617] 185.9474 [186.9155] 189.9253 [90.1468] 922.6022 [93.0707] 99 69 [125.4269] [124.5589] 130.8967 [129.987] 140.8175 [139.8447] 154.1488 [15.1846] 155.1468 [17.5096] 177.5096 [17.5029] 183.8907 [189.8267] 189.8267 [199.8007] 199.967 [40.8175] 139.8447 [154.1488] 155.1468 [155.1468] 177.5096 [17.5029] 183.8907 [189.8027] 189.8007 [17.5026] 189.8007   | 96         | 93       | 126 | 3085 12                | 5.4404 13                | 1.7586 130 | 8467 141             | 5401 140    | 1.664D 144 | 6610 166                 | 0.803 17                 | 1.8809 178               | 1.8995 180               | .0068 186                | 9634 189             | 9971 190               | 2155 192               | .6413 193                | .1038    |
| 99   96   125.4249   124.5589   130.8987   129.9967   40.8175   139.6447   156.1498   155.1853   177.5772   178.6289   185.8952   189.8955   190.1134   195.833   193.0346   100   97   125.1381   124.2785   130.6249   129.7212   140.5834   139.6153   155.9896   155.0251   177.5772   178.6289   185.8953   186.894   189.8552   190.0807   192.5464   193.0384   101   98   124.8666   123.999   130.3524   129.4544   140.3564   139.8971   155.8398   155.8251   177.4336   178.501   185.8252   186.8471   189.8277   190.0485   192.5464   193.0234   102   99   124.8667   137.7861   137.0861   137.7861   137.0861   137.7861   137.0861   137.78  | 97<br>98   | 95       | 125 | 7126 12                | 3.1396 131<br>4.8488 131 | 1.4653 130 | 0.5592 141           | .2959 140   | 0.3193 156 | 5.4807 15                | 5.513 177                | 7.7262 178               | 1.7617 183               | 9474 186                 | 9155 189             | .9253   190            | .1468 192              | .6022 193                | .0707    |
| [101] 98 [124.8866] [23.999] [103.524, [23.546] [103.554  | 99         | 96       | 125 | 4249 12                | 4.5589 130               | 1 8987 120 | 9967 140             | 8175 130    | 0017 130   | .3140 133                | .3408 1//                | .6309 178                | 1.0947 183               | .9186 186                | 8922 189             | 8905 190               | 1134 192               | .5833 193                | .0546    |
| 102 99 124-5842 123-7286 130 0884 120 1889 140 1207 120 150 150 150 150 150 150 150 150 150 15  | 101        | 98       | 124 | 8606 1                 | 73 999 136               | 3574 190   | 4544 140             | 3664 130    | 2001 100   | .7070 133                | .0251 177                | .3046 1/8                | .3644 183                | .8623 186                | 8471 189             | 8227 190               | .0485  192             | 5464 193                 | 0234     |
| 192,9787   145,7210   137,7117   158,946   155,5234   154,565   177,2953   178,3779   185,7824   186,7825   189,7256   189,9557   192,4938   192,9787   | 102<br>103 | 100      | 124 | 3166 17                | 3.7286 130               | 0.0884 129 | 1888 140             | 1307 13     | 9.166 155  | 6765 154                 | 7151 177                 | 3637 178                 | .4389 185                | .8086 186.               | 8036 189.            | 7573 18                | 9.986 19               | .5286 193.<br>2.511 192  | 9933     |
|   |            |          |     |                        | /01 167                  |            | .2310( 139           | .21 (2) 138 | .×1011 155 | .34341 154               | .36311 177               | 2953  178                | 3779 185                 | 7824 186.                | 7825 189.            | 7256 189               | 9557 192               | 4938 192                 | 9787     |

4-95

|                 | $\Delta 	au_{	ext{max}}$ |
|-----------------|--------------------------|
| $C_1 = 37,500$  | 6912                     |
| $C_2 = 75,000$  | 6912                     |
| $C_3 = 75,000$  | 6912                     |
| $C_4 = 75,000$  | 16,304                   |
| $C_5 = 150,000$ | 16,304                   |
| $C_6 = 150,000$ | 16,304                   |
| $C_7 = 75,000$  | 16,304                   |
| $C_8 = 150,000$ | 16,304                   |
| $C_9 = 150,000$ | 16,304                   |

The Equations

| <u> </u> | The Equations |   |          |  |  |  |  |  |
|----------|---------------|---|----------|--|--|--|--|--|
|          | A             | В | C        | D  |  |  |  |  |
| 1        | T1=           |   |          | =((5*(5-C1)+1.15*(C2-C1)+1.15*(C4-C1))*\$C\$11)/37500+C1                 |  |  |  |  |
| 2        | T2=           |   |          | =((1.15*(C1-C2)+1.15*(C3-C2)+6.25*(5-C2)+2.3*(C5-C2))*\$C\$11/75000+C2)  |  |  |  |  |
| 3        | T3=           |   |          | =((1.15*(C2-C3)+1.15*(100-C3)+6.25*(5-C3)+2.3*(C6-C3))*\$C\$11/75000+C3) |  |  |  |  |
| 4        | T4=           |   |          | =((1.15*(C1-C4)+1.15*(C7-C4)+2.3*(C5-C4))*\$C\$11/75000+C4)              |  |  |  |  |
| 5        | T5=           |   |          | =((2.3*(C2+C4+C6+C8-4*C5))*\$C\$11)/150000+C5                            |  |  |  |  |
| 6        | T6=           |   |          | =((2.3*(C3+C5+100+C9-4*C6))*\$C\$11)/150000+C6                           |  |  |  |  |
| 7        | T7=           |   |          | =((1.15*(C4-C7)+1.15*(100-C7)+2.3*(C8-C7))*\$C\$11/75000+C7)             |  |  |  |  |
| 8        | T8=           |   |          | =((2.3*(C5+C7+100+C9-4*C8))*\$C\$11)/150000+C8                           |  |  |  |  |
| 9        | T9=           |   | <u> </u> | =((2.3*(C6+C8+200-4*C9))*\$C\$11)/150000+C9                              |  |  |  |  |
| 10       |               |   |          | (** (** 50)) \$66(1)(15000010)   |  |  |  |  |
| 11       | Dt=           |   | 6912     |  |  |  |  |  |

|    | G    | Н        | 1        | J        | K        | L        | М        | N        | 0        | P        |
|----|------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 1  |      | T1=      | T2=      | T3=      | T4=      | T5=      | T6=      | T7=      | T8=      | T9=      |
| 2  | Time |          |          |          |          |          |          |          |          |          |
| 3  | incr | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      |
| 4  | 0    | 12.448   | 45.28    | 45.28    | 100      | 100      | 100      | 100      |          | 100      |
| 5  | 1    | 31.10148 | 30.19794 | 39.47705 | 90.72089 | 94.20056 | 94.20056 | 100      | 100      | 100      |
| 6  | 2    | 19.49224 | 30.32963 | 36.64893 | 86.1232  | 87.66316 | 89.63004 | 99.01656 | 99.38535 | 99.38535 |
| 7  | 3    | 22.557   | 27.41379 | 35.6939  | 80.7543  | 82.87434 | 85.93939 | 97.83247 | 98.16904 | 98.48173 |
| 8  | 4    | 19.74192 | 26.62213 | 34.60251 | 76.84571 | 78.71756 | 83.10881 | 96.32353 | 96.73957 | 97.44113 |
| 9  | 5    | 19.71833 | 25.32695 | 33.91854 | 73.25473 | 75.37334 | 80.81171 | 94.73702 | 95.20534 | 96.39018 |
| 10 | 6    | 18.69077 | 24.54301 | 33.29432 | 70.30658 | 72.52294 | 78.95012 | 93.1173  | 93.68756 | 95.3787  |
| 11 | 7    | 18.25474 | 23.7637  | 32.8166  | 67.7235  | 70.12722 | 77.40228 | 91.55006 | 92.23226 | 94.43787 |
| 12 | 8    | 17.69269 | 23.15899 | 32.40588 | 65.51535 | 68.0725  | 76.10637 | 90.06499 | 90.87419 | 93.5776  |
| 13 | 9    | 17.29066 | 22.62032 | 32.06707 | 63.59082 | 66.30944 | 75.00737 | 88.6876  | 89.62552 | 92.80076 |
| 14 | 10   | 16.90746 | 22.16806 | 31.77701 | 61.91986 | 64.78394 | 74.06918 | 87.42549 | 88.49104 | 92.10443 |
| 15 | 11   | 16.58981 | 21.77331 | 31.53019 | 60.45955 | 63.46045 | 73.2625  | 86.28086 | 87.46826 | 91.48363 |
| 16 | 12   | 16.30636 | 21.43293 | 31.31735 | 59.1828  | 62.30754 | 72.56557 | 85.24991 | 86.5517  | 90.93211 |
| 17 | 13   | 16.06152 | 21.13593 | 31.13353 | 58.06362 | 61.30099 | 71.9609  | 84.32643 | 85.7338  | 90.4434  |
| 18 | 14   | 15.84594 | 20.87712 | 30.97387 | 57.08173 | 60.42029 | 71.43462 | 83.50245 | 85.00628 | 90.0111  |
| 19 | 15   | 15.65744 | 20.65066 | 30.83488 | 56.21924 | 59.64858 | 70.97537 | 82.76952 | 84.3607  | 89.62919 |
| 20 | 16   | 15.49175 | 20.45235 | 30.71352 | 55.46115 | 58.97152 | 70.57381 | 82.11905 | 83.78886 | 89.29209 |
| 21 | 17   | 15.34628 | 20.2784  | 30.60738 | 54.79443 | 58.37696 | 70.22214 | 81.54278 | 83.28302 | 88.99473 |
| 22 | 18   | 15.21835 | 20.1257  | 30.51439 | 54.20784 | 57.85448 | 69.91378 | 81.03293 | 82.83602 | 88.73255 |
| 23 | 19   | 15.10584 | 19.99152 | 30.43284 | 53.69158 | 57.39508 | 69.64313 | 80.5823  | 82.44132 | 88.50146 |
| 24 | 20   | 15.00685 | 19.87357 | 30.36124 | 53.23712 | 56.99099 | 69.40539 | 80.18433 | 82.09301 | 88.29783 |

# 4-96

|                 | <u>Node</u> | $\Delta 	au_{	ext{max}}$ |
|-----------------|-------------|--------------------------|
| $C_1 = 70,312$  | 1           | 11,719                   |
| $C_2 = 70,312$  | 2           | 11,719                   |
| $C_3 = 140,625$ | 3           | 23,438                   |
| $C_4 = 140,625$ | 4           | 23,438                   |
| $C_5 = 140,625$ | 5           | 23,438                   |
| $C_6 = 140,625$ | 6           | 23,438                   |

|   | Α   | В | С     | D  |
|---|-----|---|-------|--|
| 1 | T1= |   |       | =((0.75*(C2-C1)+3*(15-C1)+0.75*(50-C1)+1.5*(C3-C1))*\$C\$8)/70312+C1 |
| 2 | T2= |   |       | =((0.75*(C1-C2)+3*(15-C2)+0.75*(50-C2)+1.5*(C4-C2))*\$C\$8)/70312+C2 |
| 3 | T3= |   |       | =(1.5*(C1+C4+C5+50-4*C3)*\$C\$8)/140625+C3                           |
| 4 | T4= |   |       | =(1.5*(C2+C3+C6+50-4*C4)*\$C\$8)/140625+C4                           |
| 5 | T5= |   |       | =(1.5*(C3+C6+100-4*C5)*\$C\$8)/140625+C5                             |
| 6 | T6= |   |       | =(1.5*(C4+C5+100-4*C6)*\$C\$8)/140625+C6                             |
| 7 |     |   |       |  |
| 8 | Dt= |   | 11719 |  |

# The Solution

|    | G    | Н        | Ī        | Ī        | K        | , <u>, , , , , , , , , , , , , , , , , , </u> | 14       |  |
|----|------|----------|----------|----------|----------|---|----------|--|
| T  | T1=  |          | T2=      | T3=      |          |   | M        |  |
| 2  | Time | -        | 12-      | 13-      | T4=      | T5=   | T6=      |  |
|    |      |          |          |          |          |   |          |  |
| 3  | incr | 50       | 50       | 50       | 50       | 50  | 50       |  |
| 4  | 1    | 32.4995  | 32.4995  | 50       | 50       | 50  | 50       |  |
| 5  | 2    | 30.31238 | 30.31238 | 47.81239 | 47.81239 | 50  | 50       |  |
| 6  | 3    | 29.49212 | 29.49212 | 46.17176 | 46.17176 | 49.72654                                      | 49.72654 |  |
| 7  | 4    | 28.97944 | 28.97944 | 45.00966 | 45.00966 | 49.35055                                      | 49.35055 |  |
| 8  | 5    | 28.62483 | 28.62483 | 44.17227 | 44.17227 | 48.97029                                      | 48.97029 |  |
| 9  | 6    | 28.37116 | 28.37116 | 43.55704 | 43.55704 | 48.62796                                      | 48.62796 |  |
| 10 | 7    | 28.18565 | 28.18565 | 43.09803 | 43.09803 | 48.3371                                       | 48.3371  |  |
| 11 | 8    | 28.04771 | 28.04771 | 42.75161 | 42.75161 | 48.09794                                      | 48.09794 |  |
| 12 | 9    | 27.94386 | 27.94386 | 42.48795 | 42.48795 | 47.90516                                      | 47.90516 |  |
| 13 | 10   | 27.86497 | 27.86497 | 42.28609 | 42.28609 | 47.75171                                      | 47.75171 |  |

### 4-98

$$\rho = 7600 \qquad C = 450 \qquad k = 35$$

$$C_1 = (7600)(450)\pi(0.01)^2(0.02) = 21.488 = C_2 = C_3 = C_4$$

$$C_5 = 10.744$$

$$\Delta \tau_{\text{max}, 1} = \frac{21.488}{1.1499} = 18.687 \text{ sec}$$

$$\Delta \tau_{\text{max}, 5} = \frac{10.744}{0.5875} = 18.288 \text{ sec}$$

|   | Α  | В | С | D  |
|---|----|---|---|--|
| 1 | T1 |   |   | =(0.5498*(200-C1)+0.5498*(C2-C1)+0.05027*(25-C1)+3.142)*\$C\$7/21.488+C1 |
| 2 | T2 |   |   | =(0.5498*(C1-C2)+0.5498*(C3-C2)+0.05027*(25-C2)+3.142)*\$C\$7/21.488+C1  |
| 3 | T3 |   |   | =(0.5498*(C2-C3)+0.5498*(C4-C3)+0.05027*(25-C3)+3.142)*\$C\$7/21.488+C3  |
| 4 | T4 |   |   | =(0.5498*(C3-C4)+0.5498*(C5-C4)+0.05027*(25-C4)+3.142)*\$C\$7/21.488+C4  |
| 5 | T5 |   |   | =(0.5498*(C4-C5)+0.0377*(25-C5)+1.571)*\$C\$7/10.744+C5                  |
| 6 |    |   |   | (======================================                                  |
| 7 | Dt |   |   |  |

|    | G    | Н        | I        | J        | К        | 1.       | М             | N            | 0            | P            |      |   |            |
|----|------|----------|----------|----------|----------|----------|---------------|--------------|--------------|--------------|------|---|------------|
|    |      | TI       | T2       | T3       |          | T5       | 144           | - 1          | - 0          | - P          | 9    | R | S          |
| 2  | Time |          |          |          |          |          |               | <del> </del> | <del> </del> |              |      |   |            |
| 3  | Incr | 200      | 200      | 200      | 200      | 200      |               | <del> </del> |              | <del></del>  |      |   |            |
| 4  | 1    | 195.1869 | 195.1869 | 195.1869 |          | 191,4441 |               | ļ            | <del></del>  |              |      | ļ |            |
| 5  | 2    | 192.8319 | 190.5798 | 190.5798 | 188.8284 | 186.94   |               |              |              |              |      | ļ |            |
| 6  | 3    | 190.6258 | 187.2236 | 185.3502 | 184.4292 | 180.9895 |               |              |              |              |      |   |            |
| 7  | 4    | 189.0082 | 183.6725 | 181.6095 | 179.1037 | 176.8725 |               |              |              | Dt=18.2      | 88 s |   | -          |
| 8  | 5    | 187.312  | 181.0894 |          | 175.3132 |          |               |              |              |              |      |   | <u> </u>   |
| 9  | 6    |          |          |          |          |          | $\overline{}$ |              |              |              |      |   | -          |
| 10 | 7    | 184.7163 | 176.1787 |          | 167.7276 |          |               | 200 T.       |              |              |      |   | ¬ ⊦        |
| 11 | 8    | 183.7138 | 173.8898 | 168.3166 |          | 161.2427 |               | 90           |              |              |      |   | J -        |
| 12 | 9    | 182.6213 | 172.1829 | 165.5046 | 161.4594 |          | — I ,         | 80           |              |              |      |   |            |
| 13 | 10   | 181.7993 | 170.3194 |          | 158.5082 |          |               |              | _            |              |      | _ | 1 F        |
| 14 | 11   | 180.9097 | 168.9099 | 161.1016 | 156.2938 | 152.615  | - 1           | 70           |              |              |      |   | 1  -       |
| 15 | 12   | 180.2312 | 167.3883 | 159.3567 | 153.8789 | 150.5426 | I             | 60           | <i>—</i>     |              |      |   | 4 F        |
| 16 |      | 179.5047 | 166.2218 | 157.4775 | 152.0412 | 148.2827 | 1             | 50           |              |              |      | - | J. H       |
| 17 |      |          |          | 156.0316 |          | 146.5629 | $\neg \neg$ , | 40           | 11/-         |              |      |   | 1 H        |
| 18 |      |          |          | 154.4938 | 148.5415 | 144.7136 |               |              |              |              |      |   | 1 H        |
| 19 |      |          | 162.9936 |          | 146.9241 | 143.2879 |               | 30 +         |              |              |      |   | <b>√</b> H |
| 20 |      | 177.3982 |          | 152.0373 | 145.662  | 141.7742 | 1             | 20 +         |              |              |      |   | 1 H        |
| 21 |      | 177.0136 | 161.3602 | 151.0456 | 144.3377 | 140.5931 | i             | 10           |              |              |      |   | l H        |
| 22 |      |          |          | 150.0146 | 143.2927 | 139.3538 |               | 00           |              |              |      |   | 1 H        |
| 23 |      |          | 160.0155 | 149.194  | 142.208  | 138.3758 |               |              |              |              |      |   | 1 H        |
| 24 |      | 175.9707 | 159.468  | 148.3493 | 141.3432 | 137.3608 |               | 0            | 20           | No of time   | 60   | 1 | 30 H       |
| 25 | 22   | 175.7076 | 158.9084 | 147.6705 | 140.4546 | 136.5515 |               |              |              | (40 OI CHINE | IBCT |   | H          |

|                 | <u>Node</u> | $\Delta 	au_{ m max}$ |
|-----------------|-------------|-----------------------|
| $C_1 = 600$     | 1           | 600                   |
| $C_2 = 1200$    | 2           | 1200                  |
| $C_3 = 1800$    | 3           | 1500                  |
| $C_4 = 2400$    | 4           | 1714                  |
| $C_5 = 2400$    | 5           | 1714                  |
| $C_6 = 1200$    | 6           | 800                   |
| $C_7 = 2400$    | 7           | 2400                  |
| $C_8 = 3600$    | 8           | 4000                  |
| $C_9 = 4800$    | 9           | 6000                  |
| $C_{10} = 4800$ | 10          | 6000                  |
| $C_{11} = 1200$ | 11          | 800                   |
| $C_{12} = 2400$ | 12          | 2400                  |
| $C_{13} = 1200$ | 13          | 800                   |
| $C_{14} = 2400$ | 14          | 2400                  |
|                 |             |                       |

# The Equations

|    | Α    | В | С            | D D  |
|----|------|---|--------------|--|
| 1  | T1=  |   |              |  |
| 2  | T2=  |   |              | =((0.2*(C2-C1)+0.05*(C6-C1)+0.75*(20-C1))*\$C\$16)/600+C1  |
| 3  | T3=  | 1 | <del> </del> | =((0.2*(C1-C2)+0.2*(C4-C2)+0.1*(C7-C2)+0.5*(20-C2))*\$C\$16)/1200+C2   |
|    | T4=  |   | <del> </del> | -(10.2°(C2-C3)+0.1°(C4-C3)+0.15°(C8-C3)+0.75°(20-C3))*\$C\$16\/1800+C3   |
| _  |      | ļ |              | -((0.1 (C3-C4)+0.1 (C3-C4)+0.2 (C9-C4)+(20-C4)) (\$C\$16\/2400+C4  |
|    | T5=  |   |              | =((0.2*(C4-C5)+0.2*(C10-C5)+(20-C5))*\$C\$16)/2400+C5  |
| 6  | T6=  |   |              | =((0.05*(C1-C6)+0.05*(C11-C6)+0.4*(C7-C6)+(20-C6))*\$C\$16)/1200+C6  |
|    | T7=  |   |              | =((0.4*(C6-C7)+0.4*(C8-C7)+0.1*(C2-C7)+0.1*(C12-C7))*\$C\$16)/2400+C7  |
| 8  | T8=  |   |              | =((0.4*(C7-C8)+0.15*(C3-C8)+0.2*(C0-C8)+0.15*(C30-C8)+0.2*(C0-C8)+0.15*(C3-C8)+0.2*(C0-C8)+0.15*(C30-C8)+0.2*(C0-C8)+0.15*(C30-C |
| 9  | T9=  |   |              | =((0.4*(C7-C8)+0.15*(C3-C8)+0.2*(C9-C8)+0.15*(500-C8))*\$C\$16)/3600+C8  |
| 10 | T10= |   |              | =((0.2*(C8-C9)+0.2*(C4-C9)+0.2*(C10-C9)+0.2*(500-C9))*\$C\$16)/4800+C9   |
|    | T11= |   |              | =((0.4*(C9-C10)+0.2*(C5-C10)+0.2*(500-C10))*\$C\$16)/4800+C10  |
|    | T12= |   |              | =((0.4*(C12-C11)+0.05*(C6-C11)+0.05*(C13-C11)+(20-C11))*\$C\$16)/1200+C11  |
|    | T13= |   |              | -(0.4*(C11-C12)+0.1*(C7-C12)+0.1*(C14-C12)+0.4*(500-C12))*\$C\$16\/2400+C12  |
| _  |      |   |              | (0.8 (C14-C13)+0.4*(C14-C13)+(20-C13))*\$C\$16\/1200+C13   |
|    | T14= |   |              | =((0.4*(C13-C14)+0.2*(C12-C14)+0.4*(500-C14))*\$C\$16)/2400+C14  |
| 15 |      |   |              | (550-614)) \$6\$10)24007614  |
| 16 | Dt=  |   | 600          |  |

# The Solution

| _  | G    | Н                        | 1        | J        | K        | L        | M                    | N        | 0        | P         | 0         | R        |          |          |          |
|----|------|--------------------------|----------|----------|----------|----------|----------------------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| 1  |      | T1=                      | T2=      | T3=      | T4-      | T5=      | T6=                  | T7=      | T8-      | T9-       |           |          | S        | T        | U        |
|    | Time |                          |          |          |          |          |                      | 1,-      | 110-     | 17-       | T10-      | T11=     | T12=     | T13=     | T14=     |
| 3  | incr | 500                      | 500      | 500      | 500      | 500      | 500                  | 500      | 600      | 500       |           |          |          |          |          |
| 4  | 1    | 140                      | 380      | 380      | 380      | 380      |                      |          |          |           |           | 500      | 200      | -        |          |
| 5  | 2    | 104                      | 272      | 296      | 296      | 296      |                      | 473      | 500      |           | 500       | 260      |          | 260      | 50       |
| 6  | 3    | 78.65                    | 204.65   | 235.45   | 237.05   | 237.05   | 158.15               | 441.65   | 497      |           |           | 188      |          | 188      | 470      |
| 7  | 4    | 63.8375                  | 160.9775 | 192.3375 | 195.4975 | 195.5375 | 143.8719             | 412.4519 | 490.45   | 492.05    | 492.05    | 161.525  |          | 161.6    | 449.     |
| 8  | 5    | 54.38909                 | 132,0448 | 161.7066 | 166.0619 | 166.1679 | 133.7613             |          | 481.1138 | 485.8338  | 485.8738  | 148.28   |          | 148.37   | 425.836  |
| 9  | 6    | 48.09703                 | 112.3926 | 139.8597 | 145.0777 | 145.2606 |                      | 386.5013 | 469.9464 | 478.8125  | 478.9665  | 139.4915 | 404.9683 | 139.6423 | 405.4931 |
| 10 | 7    | 43.7579                  | 98,69738 | 124.1308 | 129.9938 | 130.2565 | 125.5876<br>118.6513 | 363.6721 | 457.7243 | 471.3056  | 471.6647  | 32.7016  | 387.4753 | 132.931  | 388.3324 |
| 11 | 8    | 40.67204                 | 88.90296 | 112.6423 | 119.0325 | 119.3762 |                      | 343.582  | 445.0171 | 463.5367  | 464.195   | 127.1334 | 372.6767 | 127.454  | 373.9162 |
| 12 | 9    | 38.41317                 | 81.71382 | 104.0912 | 110.9547 | 111.3816 | 112.6515             | 325.8377 | 432.2245 | 455.6632  | 456.7088  | 122.4713 | 360.1583 | 122.8912 | 361.8164 |
| 13 | 10   | 36.71321                 |          | 97.58171 | 104.8972 | 105.411  | 107.409              | 310.0924 | 419.6182 | 447.796   | 449.30-4  | 118,5381 | 349.5572 | 119.0627 | 351.6593 |
| 14 | 11   |                          | 72.11289 | 92.50101 | 100.2587 |          | 102.7945             | 296.0538 | 407.3771 | 440.0134  | 442.04.72 | 115.2078 | 340.5655 | 115.8408 | 343.1286 |
| 15 | 12   |                          | 68.79621 |          |          | 100.8645 | 98,70741             | 283.4791 | 395.6141 | 432.3701  | 434.9803  | 112.3809 | 332.9245 | 113.1247 | 335.9588 |
| 16 | 13   | ** * * * * * *********** | 66.10435 | 85.08535 | 93.6926  | 97.32387 |                      | 272.1674 |          | 424.9044  | 428.1224  | 109.9759 | 326.4174 | 110.8317 | 329 9278 |
| 17 | 14   | 32.8113                  | 63.8703  |          |          |          |                      |          |          | 417.6425  | 421.4884  | 107.9249 | 320.863  | 108,8928 | 324.8499 |
| 18 |      | 32.21799                 | 61,9782  | 79.847   |          | 92.18254 |                      |          | 363.7037 | 410.6016  | 415.0842  | 106.1714 | 316.1098 | 107.2507 | 320.5699 |
| 19 | 16   |                          |          |          |          | 90.23645 |                      | 244.2787 | 354.2379 | 403.7929  | 408.9104  | 104.668  | 312.0311 |          | 316.9579 |
| 20 | -    |                          |          | 77.72591 |          | 88.56012 |                      | 236.6064 | 345.3434 | 397.2::28 | 402.9649  | 103.3755 | 308.5211 |          | 313.9058 |
| 21 |      | 30.86641                 |          |          | 85.85006 |          |                      |          |          | 390.5941  | 397.2436  | 102.2608 | 305,4911 |          | 311.3227 |
| 22 | 19   |                          |          | -        |          |          |                      |          | 329.1817 | 384.807   | 391.741   | 101.2965 | 302.8674 | 102.8025 | 309.133  |
| 23 |      | -                        |          |          | 83.11115 |          | 77.85624             | 217.277  | 321.8631 | 378.9599  | 386.4512  |          | 300.5878 |          | 307.2733 |
| -1 | 20   | 30.13323                 | 55.48237 | 71.19256 | 81.8991  | 83.43666 | 76.19379             | 211.8572 | 315.0158 | 373.3495  |           |          |          |          | 305.6909 |

|               | Node | $\Delta 	au_{	ext{max}}$ |
|---------------|------|--------------------------|
| $C_1 = 412.5$ | 1    | 23.23                    |
| $C_2 = 412.5$ | 2    | 23.23                    |
| $C_3 = 825$   | 3    | 24.26                    |
| $C_4 = 825$   | 4    | 24.26                    |
| $C_5 = 412.5$ | 5    | 24.26                    |
| $C_6 = 412.5$ | 6    | 24.26                    |

# The Equations

| Г | A   | В | С     | D  |
|---|-----|---|-------|--|
| 一 | T1= |   |       | =((0.5*(C2-C1)+16*(C3-C1)+0.5*(100-C1)+0.75*(0-C1))*\$C\$8)/412.5+C1 |
| 2 | T2= |   |       | =((0.5*(C1-C2)+16*(C4-C2)+0.5*(100-C2)+0.75*(0-C2))*\$C\$8)/412.5+C2 |
| 3 | T3= |   |       | =((C4-C3+100-C3+16*(C5-C3)+16*(C1-C3))*\$C\$8)/825+C3                |
| 4 | T4= |   |       | =((C3-C4+100-C4+16*(C6-C4)+16*(C2-C4))*\$C\$8)/825+C4                |
| 5 | T5= |   |       | =((0.5*(C6-C5)+0.5*(100-C5)+16*(C3-C5))*\$C\$8)/412.5+C5             |
| 6 | T6= |   |       | =((0.5*(C5-C6)+0.5*(100-C6)+16*(C4-C6))*\$C\$8)/412.5+C6             |
| 7 |     |   |       |  |
| 8 | Dt= |   | 23.23 |  |

# The Solution

|    | G    | Н        | I        | J        | K        | L        | M        |  |
|----|------|----------|----------|----------|----------|----------|----------|--|
| 1  |      | T1=      | T2=      | T3=      | T4=      | T5=      | T6=      |  |
| 2  | Time |          |          |          |          |          |          |  |
| 3  | incr | 100      | 100      | 100      | 100      | 100      | 100      |  |
| 4  | 1    | 95.77636 | 95.77636 | 100      | 100      | 100      | 100      |  |
| 5  | 2    | 95.65572 | 95.65572 | 98.09716 | 98.09716 | 100      | 100      |  |
| 6  | 3    | 93.93774 | 93.93774 | 97.90809 | 97.90809 | 98.28546 | 98.28546 |  |
| 7  | 4    | 93.7183  | 93.7183  | 96.34828 | 96.34828 | 97.99371 | 97.99371 |  |
| 8  | 5    | 92.30658 | 92.30658 | 96.00754 | 96.00754 | 96.5676  | 96.5676  |  |
| 9  | 6    | 91.95924 | 91.95924 | 94.70492 | 94.70492 | 96.15961 | 96.15961 |  |
| 10 | 7    | 90.7756  | 90.7756  | 94.2724  | 94.2724  | 94.95701 | 94.95701 |  |
| 11 | 8    | 90.35207 | 90.35207 | 93.16672 | 93.16672 | 94.48215 | 94.48215 |  |
| 12 | 9    | 89.34371 | 89.34371 | 92.6837  | 92.6837  | 93.45226 | 93.45226 |  |
| 13 | 10   | 88.87968 | 88.87968 | 91.73122 | 91.73122 | 92.94412 | 92.94412 |  |

# 4-102

|                  | Node | $\Delta 	au_{	ext{max}}$ |
|------------------|------|--------------------------|
| $C_1 = 87.4$     | 1    | 4.263                    |
| $C_2 = 174.8$    | 2    | 4.263                    |
| $C_3 = 174.8$    | 3    | 4.263                    |
| $C_4 = 174.8$    | 4    | 4.37                     |
| $C_5 = 349.6$    | 5    | 4.37                     |
| $C_6 = 349.6$    | 6    | 4.37                     |
| $C_7 = 174.8$    | 7    | 4.37                     |
| $C_8 = 349.6$    | 8    | 4.37                     |
| $C_9 = 349.6$    | 9    | 4.37                     |
| $C_{10} = 87.4$  | 10   | 4.37                     |
| $C_{11} = 174.8$ | 11   | 4.37                     |
| $C_{12} = 174.8$ | 12   | 4.37                     |

|    | A    | В | С     | D  |
|----|------|---|-------|--|
| 1  | Tl=  |   |       | =((10*(C2-C1)+10*(C4-C1)+0.5*(20-C1)+2250)*\$C\$14)/87.4+C1          |
| 2  | T2=  |   |       | =((10*(C1-C2)+10*(C3-C2)+20*(C5-C2)+(20-C2)+4500)*\$C\$14)/174.8+C2  |
| 3  | T3=  |   |       | =((10*(C2-C3)+10*(100-C3)+20*(C6-C3)+(20-C3)+4500)*\$C\$14)/174.8+C3 |
| 4  | T4=  |   |       | =((20*(C5-C4)+10*(C1-C4)+10*(C7-C4)+4500)*\$C\$14)/174.8+C4          |
| 5  | T5=  |   |       | =(20*(C2+C4+C6+C8-4*C5+450)*\$C\$14)/349.6+C5                        |
| 6  | T6=  |   |       | =(20*(C3+C5+100+C9-4*C6+450)*\$C\$14)/349.6+C6                       |
| 7  | T7=  |   |       | =((20*(C8-C7)+10*(C4-C7)+10*(C10-C7)+4500)*\$C\$14)/174.8+C7         |
| 8  | T8=  |   |       | =(20*(C5+C7+C9+C11-4*C8+450)*\$C\$14)/349.6+C8                       |
| 9  | T9=  |   |       | =(20*(C6+C8+100+C12-4*C9+450)*\$C\$14)/349.6+C9                      |
| 10 | T10= |   |       | =((10*(C11-C10)+10*(C7-C10)+2250)*\$C\$14)/87.4+C10                  |
| 11 | T11= |   |       | =((10*(C10-C11)+10*(C12-C11)+4500)*\$C\$14)/174.8+C11                |
| 12 | T12= |   |       | =((10*(C11-C12)+10*(100-C12)+4500)*\$C\$14)/174.8+C12                |
| 13 |      |   |       |  |
| 14 | Dt=  |   | 4.263 |  |

| Г  | G    | Н        | ı        | J        | K        | L.       | M        | N        | 0        | P        | Q        | R        | S        |
|----|------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| ī  |      | Tl=      | T2=      | T3=      | T4=      | T5-      | T6=      | T7=      | T8-      | T9-      | T10=     | T11-     | T12=     |
| 2  | Time |          |          |          |          |          |          |          |          |          |          |          |          |
| 3  | incr | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      | 100      |
| 4  | 1    | 207.7944 | 207.7944 | 207.7944 | 209.7454 | 209.7454 | 209.7454 | 209.7454 | 209.7454 | 209.7454 | 209.7454 | 209.7454 | 209.7454 |
| 5  | 2    | 313.9115 | 313.9115 | 287.6228 | 319.015  | 319.015  | 292.2505 | 319.4908 | 319.4908 | 292.7263 | 319.4908 | 319.4908 | 292.7263 |
| 6  | 3    | 418.9784 | 412.5671 | 353.7527 | 427.6319 | 421.1046 | 360.6248 | 429.1202 | 422.5929 | 361.8811 | 429.2363 | 422.709  | 361.9972 |
| 7  | 4    | 520.0872 | 504.1228 | 411.1692 | 532.4461 | 515.973  | 420.1895 | 535.3472 | 518.7892 | 422.2876 | 535.7413 | 519.2399 | 422.6534 |
| 8  | 5    | 615.878  | 589.0655 | 462.5564 | 631.8501 | 604.1731 | 473.5189 | 636.405  | 608.4612 | 476.5462 | 637.2459 | 609.4543 | 477.2659 |
| 9  | 6    | 705.8037 | 667.9876 | 509.2889 | 725.3115 | 686.1659 | 522.0996 | 731.6148 | 692.0467 | 526.0685 | 733.0256 | 693.7396 | 527.2421 |
| 10 | 7    | 789.8938 | 741.3159 | 552.2365 | 812.7431 | 762.4467 | 566.7599 | 820.8674 | 769.9421 | 571.7017 | 822.9209 | 772.4608 | 573.3975 |
| 11 | 8    | 868.3139 | 809.5113 | 591.9073 | 894.365  | 833.4091 | 608.0596 | 904.2931 | 842.5468 | 613.9641 | 907.0524 | 845.9651 | 616.2386 |
| 12 | 9    | 941.396  | 872.9303 | 628.6868 | 970.4467 | 899.4628 | 646.3588 | 982.173  | 910.2095 | 653.2258 | 985.6561 | 914.583  | 656.1098 |
| 13 | 10   | 1009.446 | 931.9475 | 662.8376 | 1041.344 | 960.9432 | 681.9505 | 1054.807 | 973.2781 | 689.7527 | 1059.036 |          | 693.268  |
| 14 | 11   | 1072.819 | 986.8653 | 694.5941 | 1107.377 | 1018.193 | 715.0525 | 1122.534 | 1032.057 | 723.7703 | 1127.498 | 1038,389 | 727.9206 |
| 15 | 12   | 1131.82  | 1037.995 | 724.1362 | 1168.891 | 1071.5   | 745.866  | 1185.663 | 1086.846 | 755.4621 | 1191.359 | 1094.149 | 760.2461 |
| 16 | 13   | 1186.768 | 1085.594 | 751.638  | 1226.183 | 1121.153 | 774.5545 | 1244.509 | 1137.912 | 784.9983 | 1250.911 | 1146.17  | 790.4035 |
| 17 | 14   | 1237.935 | 1129.926 | 777.2423 | 1279.556 | 1167.4   | 801.2767 | 1299.353 | 1185.513 | 812.5265 | 1306.446 | 1194.696 | 818.5381 |
| 18 | 15   | 1285.596 | 1171.21  | 801.0901 | 1329.274 | 1210.486 | 826.1675 | 1350.474 | 1229.88  | 838.1878 | 1358.225 | 1239.958 | 844.7843 |
| 19 | 16   | 1329.988 | 1209.669 | 823.3015 | 1375.598 | 1250.625 | 849.359  | 1398.119 | 1271.238 | 862.1076 | 1406.504 | 1282.172 | 869.2671 |
| 20 | 17   | 1371.346 | 1245.494 | 843.9949 | 1418.756 | 1288.027 | 870.9663 | 1442.53  | 1309.788 | 884.4064 | 1451.515 | 1321.54  | 892.1032 |
| 21 | 18   | 1409.874 | 1278.874 | 863.273  | 1458.973 | 1322.877 | 891.1018 | 1483.923 | 1345.724 | 905.1927 | 1493.482 | 1358.253 | 913.4021 |
| 22 | 19   | 1445.775 | 1309.973 | 881.2366 | 1496,447 | 1355,353 | 909.8646 | 1522.507 | 1379.221 | 924.5706 | 1532.606 | 1392.488 | 933.2658 |
| 23 | 20   | 1479.226 | 1338.953 | 897.9745 | 1531.371 | 1385.617 | 927.3511 | 1558.471 | 1410.446 | 942.6344 | 1569.082 | 1424.411 | 951.7901 |

$$k = 43 \qquad \rho = 7800 \qquad C = 470 \qquad \Delta x = 5 \text{ cm} \qquad h = 35 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$$

$$\frac{d = 0.0125}{0 \quad 1 \quad 2 \quad 3 \quad 4}$$

$$\frac{1}{R_{12}} = \frac{kA}{\Delta x} = \frac{(43)\pi (0.0125)^2}{(4)(0.05)} = 0.1055$$

$$\frac{1}{R_{1-\infty}} = hA = (35)\pi (0.0125)(0.05) = 0.0687$$

$$\frac{1}{R_{4-\infty}} = (35)[\pi (0.00625)^2 + \pi (0.025)(0.0125)] = 0.0387$$

$$C_1 = \frac{(7800)(470)\pi (0.0125)^2 (0.05)}{4} = 22.494$$

$$C_4 = \frac{C_1}{2} = 11.247$$

| Node | $\sum \frac{1}{R}$ | $\frac{C}{\sum \frac{1}{R}}$ |
|------|--------------------|------------------------------|
| 1    | 0.2797             | 80.42                        |
| 2    | 0.2797             | 80.42                        |
| 3    | 0.2797             | 80.42                        |
| 4    | 0.1442             | 78.00                        |

Excel solution for  $\Delta \tau = 25$  sec and 75 sec shown below  $T_2 = 190$ °C occurs at six, 25 sec time increments.

Time = (25)(6) = 150 sec

Steady state reached at about (30)(75) = 2250 sec

### The Equations

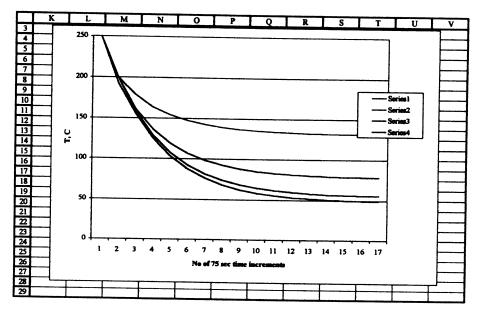
|   | Α   | В   | С   |
|---|-----|-----|---|
| 1 | T1= | 250 | =(0.1055*(250-B1)+0.1055*(B2-B1)+0.0687*(30-B1))*\$E\$1/22.494+B1 |
| 2 | T2= | 250 | =(0.1055*(B1-B2)+0.1055*(B3-B2)+0.0687*(30-B2))*\$E\$1/22.494+B2  |
| 3 | T3= | 250 | =(0.1055*(B2-B3)+0.1055*(B4-B3)+0.0687*(30-B3))*\$E\$1/22.494+B3  |
| 4 | T4= | 250 | =(0.1055*(B3-B4)+0.0387*(30-B4))*\$E\$1/11.247+B4                 |

# The Solution $\Delta \tau = 25 \text{ sec}$

|    | E  | F           | G       | Н       | 1       | J        |
|----|----|-------------|---------|---------|---------|----------|
| 1  | 25 | T1=         | T2=     | T3=     | T4=     | NO. time |
| 2  |    | 250         | 250     | 250     | 250     | 0        |
| 3  |    | 233.2021872 | 233.202 | 233.202 | 231.075 | 1        |
| 4  |    | 219.6565517 | 217.687 | 217.438 | 214.277 | 2        |
| 5  |    | 208.5025058 | 203.558 | 202.785 | 199.166 | 3        |
| 6  |    | 199.1591519 | 190.795 | 189.258 | 185.462 | 4        |
| 7  |    | 191.2238042 | 179.318 | 176.833 | 172.979 | 5        |
| 8  |    | 184.4095428 | 169.022 | 165.462 | 161.584 | 6        |
| 9  |    | 178.5062724 | 159.794 | 155.081 | 151.174 | 7        |
| 10 |    | 173.3560731 | 151.525 | 145.625 | 141.666 | 8        |
| 11 |    | 168.8373313 | 144.114 | 137.025 | 132.989 | 9        |
| 12 |    | 164.8543305 | 137.469 | 129.211 | 125.076 | 10       |
| 13 |    | 161.3302817 | 131.506 | 122.119 | 117.867 | 11       |
| 14 |    | 158.2025554 | 126.152 | 115.688 | 111.306 | 12       |
| 15 |    | 155.4193442 | 121.341 | 109.858 | 105.339 | 13       |
| 16 |    | 152.9372761 | 117.017 | 104.577 | 99.9179 | 14       |
| 17 |    | 150.7196685 | 113.126 | 99.7953 | 94.996  | 15       |
| 18 |    | 148.7352253 | 109.624 | 95.4665 | 90.5303 | 16       |
| 19 |    | 146.9570465 | 106.47  | 91.5491 | 86.4809 | 17       |
| 20 |    | 145.3618616 | 103.629 | 88.0049 | 82.8108 | 18       |
| 21 |    | 143.9294278 | 101.069 | 84.7989 | 79.4859 | 19       |
| 22 |    | 142.6420506 | 98.7601 | 81.8995 | 76.4749 | 20       |
| 23 |    | 141.4841976 | 96.6784 | 79.2777 | 73.7491 | 21       |
| 24 |    | 140.4421843 | 94.8006 | 76.9072 | 71.2822 | 22       |
| 25 |    | 139.5039146 | 93.1064 | 74.7642 | 69.0501 | 23       |
| 26 |    | 138.6586669 | 91.5776 | 72.827  | 67.0309 | 24       |
| 27 |    | 137.8969134 | 90.1977 | 71.0759 | 65.2046 | 25       |

The Solution  $\Delta \tau = 75 \text{ sec}$ 

|    | F           | G       | Н       | I       | J          |
|----|-------------|---------|---------|---------|------------|
| 1  | T1=         | T2=     | T3=     | T4=     | NO. time i |
| 2  | 250         | 250     | 250     | 250     | 0          |
| 3  | 199.6065617 | 199.607 | 199.607 | 193.225 | 1          |
| 4  | 178.4827185 | 160.756 | 158.511 | 155.591 | 2          |
| 5  | 163.3926051 | 136.251 | 128.837 | 125.235 | 3          |
| 6  | 153.7552402 | 118.852 | 107.538 | 103.192 | 4          |
| 7  | 146.9853904 | 106.797 | 92.2282 | 87.3609 | 5          |
| 8  | 142.2884591 | 98.2178 | 81.3868 | 75.9821 | 6          |
| 9  | 138.9538804 | 92.1736 | 73.6354 | 67.9179 | 7          |
| 10 | 136.60297   | 87.8665 | 68.15   | 62.1549 | 8          |
| 11 | 134.9294051 | 84.8196 | 64.2379 | 58.0744 | 9          |
| 12 | 133.7448107 | 82.6494 | 61.4671 | 55.1655 | 10         |
| 13 | 132.9015472 | 81.1117 | 59.4936 | 53.1044 | 11         |
| 14 | 132.3038016 | 80.0172 | 58.0947 | 51.6368 | 12         |
| 15 | 131.8785075 | 79.2411 | 57.0992 | 50.5963 | 13         |
| 16 | 131.5768177 | 78.689  | 56.393  | 49.8559 | 14         |
| 17 | 131.3622656 | 78.2972 | 55.8908 | 49.3307 | 15         |
| 18 | 131.2100006 | 78.0187 | 55.5343 | 48.9572 | 16         |
| 19 | 131.1017517 | 77.821  | 55.2809 | 48.6921 | 17         |
| 20 | 131.0249059 | 77.6804 | 55.1011 | 48.5036 | 18         |
| 21 | 130.9702875 | 77.5806 | 54.9732 | 48.3698 | 19         |
| 22 | 130.931506  | 77.5097 | 54.8824 | 48.2748 | 20         |
| 23 | 130.9039466 | 77.4594 | 54.8179 | 48.2072 | 21         |
| 24 | 130.8843754 | 77.4236 | 54.7721 | 48.1593 | 22         |
| 25 | 130.8704692 | 77.3982 | 54.7395 | 48.1252 | 23         |
| 26 | 130.8605927 | 77.3801 | 54.7164 | 48.101  | 24         |
| 27 | 130.8535756 | 77.3673 | 54.7    | 48.0838 | 25         |
| 28 | 130.8485916 | 77.3582 | 54.6883 | 48.0716 | 26         |
| 29 | 130.8450507 | 77.3517 | 54.68   | 48.0629 | 27         |
| 30 | 130.8425356 | 77.3471 | 54.6742 | 48.0567 | 28         |
| 31 | 130.8407489 | 77.3439 | 54.67   | 48.0523 | 29         |
| 32 | 130.8394797 | 77.3415 | 54.667  | 48.0492 | 30         |
| 33 | 130.8385781 | 77.3399 | 54.6649 | 48.047  | 31         |
| 34 | 130.8379376 | 77.3387 | 54.6634 | 48.0455 | 32         |
| 35 | 130.8374826 | 77.3379 | 54.6623 | 48.0443 | 33         |
| 36 | 130.8371594 | 77.3373 | 54.6616 | 48.0435 | 34         |
| 37 | 130.8369298 | 77.3369 | 54.661  | 48.043  | 35         |
| 38 | 130.8367668 | 77.3366 | 54.6606 | 48.0426 | 36         |
| 39 | 130.8366509 | 77.3364 | 54.6604 | 48.0423 | 37         |



$$\frac{\alpha \Delta \tau}{(\Delta x)^2} = \frac{1}{4} \qquad \Delta \tau_{\text{max}} = \frac{\frac{(0.15)^2}{4}}{1.29 \times 10^{-5}} = 436 \text{ sec}$$

$$C_1 = C_2 = C_3 = C_4 = 78,488$$
The Equations

|   | A   | В | С   | D   |
|---|-----|---|-----|---|
| 1 | T1= |   |     | =(45*(C2+C3+100+30-4*C1)*\$C\$6)/78488+C1 |
| 2 | T2= |   |     | =(45*(C1+C4+30+100-4*C2)*\$C\$6)/78488+C2 |
| 3 | T3= |   |     | =(45*(C1+C4+200-4*C3)*\$C\$6)/78488+C3    |
| 4 | T4= |   |     | =(45*(C2+C3+200-4*C4)*\$C\$6)/78488+C4    |
| 5 |     |   |     |   |
| 6 | Dt= |   | 436 |   |

|    | G    | H        | I        | J        | K        |
|----|------|----------|----------|----------|----------|
| 1  |      | T1=      | T2=      | T3=      | T4=      |
| 2  | Time |          |          |          |          |
| 3  | intr | 500      | 500      | 500      | 500      |
| 4  | 1    | 282.5222 | 282.5222 | 300.0204 | 300.0204 |
| 5  | 2    | 178.1463 | 178.1463 | 195.6463 | 195.6463 |
| 6  | 3    | 125.9535 | 125.9535 | 143.4535 | 143.4535 |
| 7  | 4    | 99.85439 | 99.85439 | 117.3544 | 117.3544 |
| 8  | 5    | 86.80353 | 86.80353 | 104.3035 | 104.3035 |
| 9  | 6    | 80.27743 | 80.27743 | 97.77743 | 97.77743 |
| 10 | 7    | 77.01405 | 77.01405 | 94.51405 | 94.51405 |
| 11 | 8    | 75.38219 | 75.38219 | 92.88219 | 92.88219 |
| 12 | 9    | 74.56618 | 74.56618 | 92.06618 | 92.06618 |
| 13 | 10   | 74.15813 | 74.15813 | 91.65813 | 91.65813 |

# 4-106

|              | Node | $\Delta 	au_{	ext{max}}$ |
|--------------|------|--------------------------|
| $C_1 = 350$  | 1    | 16.83                    |
| $C_2 = 700$  | 2    | 17.16                    |
| $C_3 = 700$  | 3    | 17.16                    |
| $C_4 = 350$  | 4    | 16.83                    |
| $C_5 = 700$  | 5    | 17.16                    |
| $C_6 = 1400$ | 6    | 17.16                    |
| $C_7 = 1400$ | 7    | 17.5                     |
| $C_8 = 700$  | 8    | 17.5                     |

|   | A   | В | С | D   |
|---|-----|---|---|---|
| 1 | T1= |   |   | =((10*(C2-C1)+10*(C5-C1)+0.8*(300-C1))*\$C\$8)/350+C1 |
| 2 | T2= |   |   | =((10*(C1-C2)+20*(C5-C2)+0.8*(300-C2))*\$C\$8)/700+C2 |
| 3 |     |   |   |   |
| 4 |     |   |   |   |
| 5 | T5= |   |   | =((10*(C1-C5)+20*(C6-C5)+10*(50-C5))*\$C\$8)/700+C5   |
| 6 | T6= |   |   | =((20*(C2-C5)+50-3*C6)*\$C\$8)/1400+C6                |
| 7 |     |   |   |   |
| 8 | Dt= |   |   |   |

The Solution 10 sec

|    | G        | Н        | I        | J | K  | T L      | T 14         |
|----|----------|----------|----------|---|--|----------|--------------|
| 1  | Dt= 0.25 | T1=      | T2=      |   |  | T5=      | T6=          |
| 2  | Time     |          |          |   |  | 113-     | 10=          |
| 3  | incr     | 50       | 50       |   |  | 50       |              |
| 4  | 1        |          | 50.07143 |   |  | 50       |              |
| 5  | 2        | 50.2841  |          |   |  | 50.00038 |              |
| 6  | 3        | 50.42376 |          |   | <del></del>                                      | 50.00038 | +            |
| 7  | 4        | 50.56185 |          |   | <del></del>                                      | 50.00226 | <del></del>  |
| 8  | 5        | 50.69841 | 50.35439 |   |  | 50.00220 |              |
| 9  | 6        | 50.83345 | 50.42444 |   | <del> </del>                                     | 50.00556 | ·            |
| 10 | 7        | 50.96699 | 50.49422 |   |  | 50.00772 |              |
| 11 | 8        | 51.09907 | 50.56372 |   |  | 50.00772 |              |
| 12 | 9        | 51.2297  | 50.63294 |   | <del>                                     </del> | 50.01302 | <del> </del> |
| 13 | 10       | 51.3589  | 50.70189 |   |  | 50.01502 |              |
| 14 | 11       | 51.48669 | 50.77057 |   |  | 50.01957 |              |
| 15 | 12       | 51.61311 | 50.83897 |   | <b>†</b>   | 50.0233  |              |
| 16 | 13       | 51.73816 | 50.9071  |   | <del></del>                                      | 50.02732 |              |
| 17 | 14       | 51.86186 | 50.97495 |   | <del>                                     </del> | 50.03162 |              |
| 18 | 15       | 51.98425 | 51.04253 |   | <b>†</b>   | 50.0362  |              |
| 19 | 16       | 52.10533 | 51.10984 |   |  |          | 49.74471     |
| 20 | 17       | 52.22513 | 51.17687 |   |  |          | 49.73081     |
| 21 | 18       | 52.34366 | 51.24363 |   |  | 50.05152 |              |
| 22 | 19       | 52.46095 | 51.31012 |   |  | 50.05713 | 49.70368     |
| 23 | 20       | 52.57701 | 51.37633 |   |  | 50.06299 | 49.69046     |
| 24 | 21       | 52.69186 | 51.44227 |   |  | 50.06908 | 49.67746     |
| 25 | 22       | 52.80552 | 51.50794 |   |  | 50.0754  | 49.66468     |
| 26 | 23       | 52.91801 | 51.57334 |   |  | 50.08195 | 49.65212     |
| 27 | 24       | 53.02933 | 51.63847 |   |  | 50.08872 | 49.63977     |
| 28 | 25       | 53.13952 | 51.70333 |   |  | 50.0957  | 49.62765     |
| 29 | 26       |          | 51.76792 |   |  | 50.10288 | 49.61573     |
| 30 | 27       | 53.35654 | 51.83224 |   |  | 50.11027 | 49.60402     |
| 31 | 28       |          | 51.89629 |   |  | 50.11785 | 49.59253     |
| 32 |          |          | 51.96007 |   |  | 50.12563 | 49.58124     |
| 33 |          | 53.67392 |          |   |  | 50.13359 | 49.57016     |
| 34 | 31       |          | 52.08682 |   |  | 50.14173 | 49.55928     |
| 35 |          | 53.88025 | 52.1498  |   |  | 50.15005 | 49.54861     |
| 36 |          |          | 52.21251 |   |  | 50.15854 | 49.53814     |
| 37 |          |          | 52.27496 |   |  | 50.1672  | 49.52786     |
| 38 |          |          | 52.33713 |   |  | 50.17602 | 49.51779     |
| 39 |          |          | 52.39905 |   |  | 50.185   | 49.5079      |
| 40 |          | 54.37855 | 52.4607  |   |  |          | 49.49822     |
| 41 |          |          | 52.52208 |   |  |          | 49.48873     |
| 42 |          | 54.57116 | 52.5832  |   |  |          | 49.47942     |
| 43 | 40       | 54.66607 | 52.64406 |   |  | 50.2224  | 49.47031     |

The Solution 1 min

|    | G    | Н        | I        | J | K | L        | M        |
|----|------|----------|----------|---|---|----------|----------|
| 1  | Dt=5 | T1=      | T2=      |   |   | T5=      | T6=      |
| 2  | Time |          |          |   |   |          |          |
| 3  | incr | 50       | 50       |   |   | 50       | 50       |
| 4  | 1    | 52.85714 | 51.42857 |   |   | 50       | 49.64286 |
| 5  | 2    | 55.06939 | 52.74694 |   |   | 50.15306 | 49.39158 |
| 6  | 3    | 56.83448 | 53.95515 |   |   | 50.38451 | 49.22623 |
| 7  | 4    | 58.28076 | 55.0567  |   |   | 50.65229 | 49.13243 |
| 8  | 5    | 59.4929  | 56.05746 |   |   | 50.93347 | 49.09918 |
| 9  | 6    | 60.528   | 56.96481 |   |   | 51.21614 | 49.11769 |
| 10 | 7    | 61.42553 | 57.78686 |   |   | 51.49463 | 49.18062 |
| 11 | 8    | 62.21358 | 58.53195 |   |   | 51.76664 | 49.2817  |
| 12 | 9    | 62.91278 | 59.20827 |   |   | 52.03167 | 49.41549 |
| 13 | 10   | 63.53868 | 59.8236  |   |   | 52.29003 | 49.57722 |
| 14 | 11   | 64.10342 | 60.38518 |   |   | 52.54239 | 49.76272 |
| 15 | 12   | 64.61663 | 60.89959 |   |   | 52.78948 | 49.96832 |

The Solution 1 sec

|   | G        | Н        | I        | J | K | L        | M        |
|---|----------|----------|----------|---|---|----------|----------|
| 1 | Dt= 0.25 | T1=      | T2=      |   |   | T5=      | T6=      |
| 2 | Time     |          |          |   |   |          |          |
| 3 | incr     | 50       | 50       |   |   | 50       | 50       |
| 4 | 1        | 50.14286 | 50.07143 |   |   | 50       | 49.98214 |
| 5 | 2        | 50.2841  | 50.14258 |   |   | 50.00038 | 49.96455 |
| 6 | 3        | 50.42376 | 50.21346 |   |   | 50.00114 | 49.94722 |
| 7 | 4        | 50.56185 | 50.28406 |   |   | 50.00226 | 49.93015 |

The Solution Steady state

|            | G              | н                           | 1                             | 7            | K            | L                                    | м                    |
|------------|----------------|-----------------------------|-------------------------------|--------------|--------------|--------------------------------------|----------------------|
| 1/2        | De- 15<br>Time | Ti-                         | T2=                           |              |              | TS-                                  | T6-                  |
| 3          | incr           | 50                          | 50                            |              | <del> </del> | 50                                   | 5                    |
| 1 3        | 1 1/2          | 58.57143<br>61.33878        |                               |              |              | 50<br>51.37755                       |                      |
| 6          | 3              | 63.64127                    | 59.88289                      |              |              | 52.11651                             | 49.1057              |
| 7          | 5              | 65.19508<br>66.35762        | 61.4761<br>62.66179           | <del> </del> |              | 52.84225<br>53.54526                 | 49.7273<br>50.5147   |
| 9<br>10    | 6              | 67.29328<br>68.09796        | 63.61532<br>64.43446          |              |              | 54.23228                             | 51.3803              |
| 11         | 8              | 68.82336                    | 65.17237                      |              |              | 54.90189<br>55.55348                 |                      |
| 12<br>13   |                | 69.49762<br>70.13612        | 65.85796<br>66.50702          |              |              | 56.18693<br>56.80237                 | 54.0610<br>54.9314   |
| 14<br>15   | 11             | 70.74738                    | 67.12829                      |              |              | 57.40015                             | 55.7811              |
| 16         | 13             | 71.33619<br>71.90536        | 67.72669<br>68.30511          |              |              | 57.98065<br>58.54433                 | 56.60847<br>57.41306 |
| 17<br>18   | 14             | 72.45663<br>72.99113        | 68.86531<br>69.40848          |              |              | 59.09165<br>59.62306                 | 58.1949:<br>58.95447 |
| 19<br>20   | 16             | 73.5097<br>74.01296         | 69.93544                      |              |              | 60.13902                             | 59.69209             |
| 21         | 18             | 74.50148                    | 70.44685<br>70.94327          |              |              | 60.63998                             | 60.40836             |
| 22<br>23   | 19<br>20       | 74.97572<br>75.43612        | 71.42518<br>71.89304          |              |              | 61.59859<br>62.05708                 |                      |
| 24<br>25   | 21             | 75.88312                    | 72.34727                      |              |              | 62.50223                             | 63.07138             |
| 26         | 22<br>23       | 76.3171<br>76.73 <b>844</b> | 72. <b>788</b> 27<br>73.21643 |              |              | 62.93444<br>63.35406                 | 63.68945             |
| 27<br>28   | 24<br>25       | 77.14753<br>77.54471        | 73.63214<br>74.03574          |              |              | 63.76148<br>64.15704                 | 64.87217             |
| 29         | 26             | 77.93033                    | 74.42761                      |              |              | 64.54109                             | 65.43785<br>65.98707 |
| 30<br>31   | 27             | 78.30474<br>78.66825        | 74.80807<br>75.17746          |              |              | 64.91397<br>65.276                   | 66.52031<br>67.03803 |
| 32<br>33   | 29<br>30       | 79.02118<br>79.36384        | 75.5361<br>75.88431           |              |              | 65.6275                              | 67.54069             |
| 34         | 31             | 79.69653                    | 76.22239                      |              |              | 66.3001                              | 68.02873<br>68.50257 |
| 35<br>36   | 32<br>33       | 80.01955<br>80.33316        | 76.55063<br>76.86932          |              |              | 66.6218                              | 68.96262<br>69.40928 |
| 37<br>38   | 34<br>35       | 80.63765                    | 77.17873<br>77.47915          |              |              | 67.23739                             | 69.84295             |
| 39         | 36             | 81.22031                    | 77.77082                      |              |              | 67.53182<br>67.81768                 | 70.264<br>70.6728    |
| 49         |                |                             | 78.05401<br>78.32896          |              |              | 68.09522<br>68.36469                 | 71.06971<br>71.45506 |
| 42         | 39             | 82.03226                    | 78.5959<br>78.85508           |              |              | 68.62632                             | 71.82921             |
| 44         | 41             | 82.53494                    | 79.10672                      |              |              | 68.88033<br>69.12696                 | 72.19246<br>72.54515 |
| 45<br>46   | 42             | 82.77537<br>83.0088         | 79.35104<br>79.58825          |              |              | 69.3664<br>69.59889                  | 72.88758<br>73.22005 |
| 47<br>48   |                | 83.23544                    | 79.81856                      |              |              | 69.8246                              | 73.54284             |
| 49         | 46             | 83.66913                    | 80.04216<br>80.25926          |              |              |                                      | 73.85623<br>74.16051 |
| 50<br>51   |                | 83.87656<br>84.07795        | 80.47005                      |              |              |                                      | 74.45594<br>74.74277 |
| 52<br>53   | 49             | 84.27348                    | 80.87339                      |              |              | 70.85842                             | 75.02126             |
| 54         | 51             | 84.64764                    | 81.06631<br>81.25361          |              |              |                                      | 75.29164<br>75.55416 |
| 55<br>56   | 52             |                             | 81.43546<br>81.61202          |              |              | 71.40928                             | 75.80903<br>76.0565  |
| 57<br>58   |                | 85.16904                    | 81.78345<br>81.94988          |              |              | 71.75033                             | 76.29676             |
| 59         | 56             | 85.49185                    | 82.11147                      |              |              |                                      | 76.53003<br>76.75651 |
| 60<br>61   |                |                             | 82.26837<br>82.42069          |              |              | 72.22559 1<br>72.37488               | 76.97641<br>77.1899  |
| 62<br>63   |                |                             | 82.56859<br>82.71218          |              |              | 72.51983                             | 77.39719<br>77.59844 |
| 64         | 61 1           | 86.22018 8                  | 32.85159                      |              | - 7          | 2.79719                              | 77.79384             |
| 65<br>66   |                |                             | 32.98695<br>33.11837          |              |              |                                      | 77.98355<br>78.16774 |
| 67<br>68   |                |                             | 3.24596<br>3.36985            |              | 7            | 3.18371 7<br>3.30512                 | 78.34657<br>78.5202  |
| 69         | 66 8           | 86.84855 8                  | 3.49012                       |              |              | 73.423                               | 78.68878             |
| 3          | 68 8           |                             | 83.6069<br>3.72028            |              |              |                                      | 78.85245<br>79.01136 |
| 73         |                |                             | 3.83037<br>3.93724            |              |              | 3.75646 7                            | 79.16565<br>79.31545 |
| 74<br>75   | 71 8           | 7.39067 8                   | 4.04101                       |              | 7            | 3.96291 7                            | 9.46009              |
| 76         | 73 8           | 7.58607 8                   | 4.23958                       | $=\pm$       | 7            | 4.06165<br>4.15752                   | 79.6021<br>79.7392   |
| 78         |                |                             | 4.33455<br>4.42676            |              |              |                                      | 9.87231<br>0.00154   |
| 79<br>80   | 76 8           | 7.85837 8                   | 4.51629                       |              | 7            | 4.42872 8                            | 0.12702              |
| 81         | 78 8           | 8.02696                     | 84.6876                       |              | 7            | 4.59662 8                            |                      |
| 82<br>83   |                |                             | 4.76954                       |              |              | 4.67692 8<br>4.75489 8               | 0.48197<br>0.59346   |
| 84<br>85   | 81 8           | 8.26189 8                   | 4.92633<br>5.00132            |              | 7            | 4.83059 8                            | 0.70172              |
| 86         | 83 8           | 8.40733 8                   | 5.07413                       |              |              | 4.90408 8<br>4.97544 8               | 0.80682<br>0.90887   |
| 87<br>88   |                |                             | 5.14482<br>5.21346            |              |              | 5.04472 <b>8</b><br>5.11199 <b>8</b> |                      |
| 89<br>90   | 86 8           | 8.61001 8                   | 5.28009                       |              |              | 75.1773 8                            | 1.19754              |
| 91         | 88             | 88.7355 8                   | 5.34479<br>5.40761            |              | 7:           | 75.2407 8<br>5.30227 8               | 1.37626              |
| 92<br>93   |                |                             | 5.46859<br>5.52781            | $-\Gamma$    |              | 5.36204 B<br>5.42007 B               |                      |
| 94<br>95   | 91 8           | 8.91036                     | 85.5853                       | _            | 7:           | 5.47642                              | 81.6253              |
| 96         | 93 8           | 9.01862 8                   | 5.69531                       |              | 7:           | 5.53112 8<br>5.58424 8               |                      |
| 97<br>98   |                |                             | 5.74792<br>5.79901            |              | 7:           | 5.63581 8                            | 1.85324              |
| 99<br>100  | 96 8           |                             | 5.84861                       |              | 7:           | .73448 8                             | 1.99435              |
| 101        | 98 89          | 9.26288 85                  | 5.94352                       | =            | 7            | 5.8275 82                            | 2.06185<br>2.12738   |
| 102<br>103 |                | 9.30755 85<br>9.35092 86    |                               | $=$ $\top$   |              | .87199<br>.91519 87                  | 82.191               |
| _          |                |                             |                               |              |              |                                      |                      |

#### 4-112

Wall thickness = 0.25 m 
$$T_{\infty} = 600^{\circ}\text{C}$$
  $h = 100 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   
 $k = 0.16 \frac{\text{W}}{\text{m} \cdot {}^{\circ}\text{C}}$   $\alpha = 3.5 \times 10^{-7} \text{ m}^2/\text{s}$ 

Approximate as inf. plate with 2L = 0.5

Center plane is insulated

$$\frac{k}{hL} = \frac{0.16}{(100)(0.25)} = 6.4 \times 10^{-3} \qquad A = (6)(1.0) = 6.0 \text{ m}^2$$

$$V = 1.0 - (0.5)^3 = 0.875 \text{ m}^3$$

$$\frac{h(V/A)}{k} = 546.9 \qquad \text{Not lumped capacity}$$

$$\frac{\theta_0}{\theta_i} = \frac{150 - 600}{30 - 600} = 0.789 \qquad \frac{\alpha \tau}{L^2} = 0.2$$

$$\tau = \frac{(0.25)^2 (0.2)}{3.5 \times 10^{-7}} = 3.57 \times 10^4 \text{ sec} = 9.92 \text{ hr}$$

$$k = 1.07$$
  $\alpha = 5.4 \times 10^{-7}$   $T_i = 20^{\circ}$ C  $x = 2.0 \text{ cm}$ 

$$\frac{q}{A} = 4500 \text{ W/m}^2$$
  $T_0 = T_i + \frac{\left(2\frac{q_0}{A}\right)\sqrt{\frac{\alpha\tau}{\pi}}}{k}$ 

| τ    | $T_{0}$ |
|------|---------|
| 0    | 20      |
| 100  | 54.87   |
| 300  | 80.4    |
| 900  | 124.61  |
| 1500 | 155.05  |
| 1400 | 150.47  |
| 1390 | 150     |
| 2000 | 175.94  |

at 
$$x = 2$$
 cm  $\tau = 1390$   

$$\frac{q}{A} = -k \frac{\partial T}{\partial x}$$

$$= \frac{2q_0}{A} \sqrt{\frac{\alpha \tau}{\pi}} \left( \frac{-x^2}{4\alpha \tau} \right) \exp\left( \frac{-x^2}{4\alpha \tau} \right) \left( \frac{-2x}{4\alpha \tau} \right) - \frac{q_0}{A} x \left[ -\exp\left( \frac{-x^2}{4\alpha \tau} \right) \left( \frac{1}{2\sqrt{\alpha \tau}} \right) \right]$$

$$- \frac{q_0}{A} \left[ 1 - \operatorname{erf} \left( \frac{x}{2\sqrt{\alpha \tau}} \right) \right]$$

$$= 1180 \text{ W/m}^2$$

$$\frac{k}{hr_0} = \frac{3.2}{(350)(0.075)} = 0.122 \qquad \frac{\alpha\tau}{r_0^2} = \frac{(13\times10^{-7})(21)(60)}{(0.075)^2} = 0.291$$

$$\frac{r}{r_0} = \frac{4.5}{7.5} = 0.6 \qquad \frac{\theta_0}{\theta_i} = 0.65 \qquad \frac{\theta}{\theta_0} = 0.59$$

$$T = (0.65)(0.59)(120 - 30) + 30 = 64.5^{\circ}\text{C}$$

$$\frac{hr_0}{k} = 8.2 \qquad \frac{h^2\alpha\tau}{k^2} = \frac{(350)^2(13\times10^{-7})(21)(60)}{(3.2)^2} = 19.6$$

$$\frac{Q}{Q_0} = 0.92 \qquad \rho c = \frac{k}{\alpha}$$

$$Q = \frac{(0.92)(3.2)}{13\times10^{-7}}(120 - 30)\frac{4}{3}\pi(0.075)^3 = 3.6\times10^5 \text{ J}$$

$$\frac{1}{R} = \frac{kA}{\Delta x} = \frac{(20)(0.01)}{0.01} = 20 \qquad \alpha = \frac{k}{\rho c} = 5 \times 10^{-6}$$

$$\sum \frac{1}{R} = (4)(20) = 80 \qquad C = \rho c \Delta V = \frac{k}{\alpha} (\Delta x)^2 = \frac{(20)(0.01)^2}{5 \times 10^{-6}} = 400$$

$$\Delta \tau_{\text{max}} = \frac{C}{\sum \frac{1}{R}} = \frac{400}{80} = 5 \text{ sec}$$

$$T_i = 100^{\circ}\text{C} \qquad \frac{\Delta \tau}{C} = \frac{5}{400} = \frac{1}{80}$$

Excel solution shown for  $\Delta \tau = 5$  sec 1 minute = 12 time increments

|    | Α                | В               | С                 | D                | E                | F                |
|----|------------------|-----------------|-------------------|------------------|------------------|------------------|
| 1  | T1=              | T2=             | T3=               | T4=              | T5=              | T6=              |
| 2  | 100              | 100             | 100               | 100              | 100              | 100              |
|    | =(140+B2+C2)/4   | =(40+A2+D2)/4   | =(100+A2+E2+D2)/4 | =(B2+C2+F2)/4    | =(200+C2+F2)/4   | =(100+D2+E2)/4   |
| 4  | =(140+B3+C3)/4   | -(40+A3+D3)/4   | =(100+A3+E3+D3)/4 | -(B3+C3+F3)/4    | =(200+C3+F3)/4   | =(100+D3+E3)/4   |
| 5  | 7                | =(40+A4+D4)/4   | =(100+A4+E4+D4)/4 | =(B4+C4+F4)/4    | =(200+C4+F4)/4   | =(100+D4+E4)/4   |
| -  | =(140+B5+C5)/4   | =(40+A5+D5)/4   | =(100+A5+E5+D5)/4 | =(B5+C5+F5)/4    | =(200+C5+F5)/4   | =(100+D5+E5)4    |
| 7  |                  | =(40+A6+D6)/4   | =(100+A6+E6+D6)/4 | =(B6+C6+F6)/4    | =(200+C6+F6)/4   | =(100+D6+E6)4    |
|    | =(140+B7+C7)/4   | =(40+A7+D7)/4   | =(100+A7+E7+D7)/4 | =(B7+C7+F7)/4    | =(200+C7+F7)/4   | =(100+D7+E7)4    |
| 9  | =(140+B8+C8)/4   | =(40+A8+D8)/4   | =(100+A8+E8+D8)/4 | =(B8+C8+F8)/4    | =(200+C8+F8)/4   | =(100+D8+E8)/4   |
| _  | =(140+B9+C9)/4   | =(40+A9+D9)/4   | =(100+A9+E9+D9)/4 | =(B9+C9+F9)/4    | =(200+C9+F9)/4   | =(100+D9+E9)/4   |
|    | =(140+B10+C10)/4 | =(40+A10+D10)/4 | =(100+A10+E10+D10 |                  | =(200+C10+F10)/4 | =(100+D10+E10)/4 |
| -  | =(140+B11+C11)/4 | =(40+A11+D11)/4 | =(100+A11+E11+D11 | =(B11+C11+F11)/4 | =(200+C11+F11)/4 | =(100+D11+E11)/4 |
|    | =(140+B12+C12)/4 | =(40+A12+D12)/4 | =(100+A12+E12+D12 | =(B12+C12+F12)/4 | =(200+C12+F12)/4 | =(100+D12+E12)/4 |
| _  | =(140+B13+C13)/4 | =(40+A13+D13)/4 | =(100+A13+E13+D13 | =(B13+C13+F13)/4 | =(200+C13+F13)/4 | =(100+D13+E13)/4 |
|    | =(140+B14+C14)/4 | =(40+A14+D14)/4 | =(100+A14+E14+D14 | =(B14+C14+F14)/4 | =(200+C14+F14)/4 | =(100+D14+E14V4  |
| _  | =(140+B15+C15)/4 | =(40+A15+D15)/4 | =(100+A15+E15+D15 | =(B15+C15+F15)/4 | =(200+C15+F15)/4 | =(100+D15+E15)/4 |
|    | =(140+B16+C16)/4 | =(40+A16+D16)/4 | =(100+A16+E16+D16 | =(B16+C16+F16)/4 | =(200+C16+F16)/4 | =(100+D16+E16)/4 |
|    | =(140+B17+C17)/4 | =(40+A17+D17)/4 | -(100+A17+E17+D17 | =(B17+C17+F17)/4 | -(200+C17+F17)/4 | =(100+D17+E17)/4 |
|    | =(140+B18+C18)/4 | =(40+A18+D18)/4 | =(100+A18+E18+D18 | =(B18+C18+F18)/4 | =(200+C18+F18)/4 | =(100+D18+E18)/4 |
|    | =(140+B19+C19)/4 | =(40+A19+D19)/4 | =(100+A19+E19+D19 | =(B19+C19+F19)/4 | =(200+C19+F19)/4 | =(100+D19+E19)/4 |
| 21 |                  | =(40+A20+D20)/4 | =(100+A20+E20+D20 | =(B20+C20+F20)/4 | =(200+C20+F20)/4 | =(100+D20+E20)/4 |
| 22 | =(140+B21+C21)/4 | =(40+A21+D21)/4 | =(100+A21+E21+D21 | =(B21+C21+F21)/4 | =(200+C21+F21)/4 | =(100+D21+E21)/4 |
|    |                  |                 | =(100+A22+E22+D22 | =(B22+C22+F22)/4 | =(200+C22+F22)/4 | =(100+D22+E22)/4 |
|    | =(140+B23+C23)/4 | =(40+A23+D23)/4 | =(100+A23+E23+D23 | =(B23+C23+F23)/4 | =(200+C23+F23)/4 | =(100+D23+E23)/4 |
|    |                  | =(40+A24+D24)/4 | -(100+A24+E24+D24 | -(B24+C24+F24)/4 | =(200+C24+F24)/4 | =(100+D24+E24)/4 |
|    |                  | =(40+A25+D25)/4 | =(100+A25+E25+D25 | =(B25+C25+F25)/4 | =(200+C25+F25)/4 | =(100+D25+E25)/4 |
| _  |                  | =(40+A26+D26)/4 | =(100+A26+E26+D26 |                  | -(200+C26+F26)/4 | =(100+D26+E26)/4 |
|    |                  | =(40+A27+D27)/4 | =(100+A27+E27+D27 |                  | =(200+C27+F27)/4 | =(100+D27+E27)/4 |
| 29 | =(140+B28+C28)/4 | =(40+A28+D28)/4 | =(100+A28+E28+D28 | =(B28+C28+F28)/4 |                  | =(100+D28+E28)/4 |

### The Solution

|    | Α       | В       | С        | D       | Е       | F       |
|----|---------|---------|----------|---------|---------|---------|
| 1  | T1=     | T2=     | T3=      | T4=     | T5=     | T6=     |
| 2  | 100     | 100     | 100      | 100     | 100     | 100     |
| 3  | 85      | 60      | 100      | 75      | 100     | 75      |
| 4  | 75      | 50      | 90       | 58.75   | 93.75   | 68.75   |
| 5  | 70      | 43.4375 | 81.875   | 52.1875 | 89.6875 | 63.125  |
| 6  | 66.3281 | 40.5469 | 77.96875 | 47.1094 | 86.25   | 60.4688 |
| 7  | 64.6289 | 38.3594 | 74.92188 | 44.7461 | 84.6094 | 58.3398 |
| 8  | 63.3203 | 37.3438 | 73.49609 | 42.9053 | 83.3154 | 57.3389 |
| 9  | 62.71   | 36.5564 | 72.38525 | 42.0447 | 82.7087 | 56.5552 |
| 10 | 62.2354 | 36.1887 | 71.86584 | 41.3742 | 82.2351 | 56.1884 |
| 11 | 62.0136 | 35.9024 | 71.46118 | 41.0607 | 82.0135 | 55.9023 |
| 12 | 61.8409 | 35.7686 | 71.27197 | 40.8165 | 81.8409 | 55.7686 |
| 13 | 61.7601 | 35.6643 | 71.12456 | 40.7023 | 81.7601 | 55.6643 |
| 14 | 61.6972 | 35.6156 | 71.05564 | 40.6133 | 81.6972 | 55.6156 |
| 15 | 61.6678 | 35.5776 | 71.00194 | 40.5717 | 81.6678 | 55.5776 |
| 16 | 61.6449 | 35.5599 | 70.97683 | 40.5393 | 81.6449 | 55.5599 |
| 17 | 61.6342 | 35.546  | 70.95727 | 40.5241 | 81.6342 | 55.546  |
| 18 | 61.6258 | 35.5396 | 70.94813 | 40.5123 | 81.6258 | 55.5396 |
| 19 | 61.6219 | 35.5345 | 70.941   | 40.5068 | 81.6219 | 55.5345 |
| 20 | 61.6189 | 35.5322 | 70.93767 | 40.5025 | 81.6189 | 55.5322 |
| 21 | 61.6175 | 35.5304 | 70.93507 | 40.5005 | 81.6175 | 55.5304 |
| 22 | 61.6164 | 35.5295 | 70.93386 | 40.4989 | 81.6164 | 55.5295 |
| 23 | 61.6158 | 35.5288 | 70.93291 | 40.4982 | 81.6158 | 55.5288 |
| 24 | 61.6154 | 35.5285 | 70.93247 | 40.4976 | 81.6154 | 55.5285 |
| 25 | 61.6152 | 35.5283 | 70.93213 | 40.4974 | 81.6152 | 55.5283 |
| 26 | 61.6151 | 35.5282 | 70.93197 | 40.4972 | 81.6151 | 55.5282 |
| 27 | 61.615  | 35.5281 | 70.93184 | 40.4971 | 81.615  | 55.5281 |
| 28 | 61.615  | 35.528  | 70.93178 | 40.497  | 81.615  | 55.528  |
| 29 | 61.615  | 35.528  | 70.93174 | 40.497  | 81.615  | 55.528  |

#### 4-134

$$\frac{\overline{hV}}{kA} = \frac{h(2LA)}{kA} = \frac{2hL}{k} < 0.1$$
From figure  $\frac{\theta}{\theta_0} = 0.98$  for  $\frac{k}{hL} = 20$  and  $\frac{x}{L} = 1.0$  worst case

Cylinder
$$\frac{hV}{kA} = \frac{1}{2} \frac{hr_0}{k} < 0.1$$
From figure  $\frac{\theta}{\theta_0} = 0.91$  for  $\frac{k}{hr_0} = 5$  and  $\frac{r}{r_0} = 1.0$  worst case

#### **Sphere**

$$\frac{hV}{kA} = \frac{1}{3} \frac{hr_0}{k} < 0.1$$

$$\frac{hr_0}{k} < 0.3$$
From figure  $\frac{\theta}{\theta_0} = 0.85$  for  $\frac{k}{hr_0} = 3.333$  and  $\frac{r}{r_0} = 1.0$  worst case

#### 4-135

Aluminum 
$$k = 204$$
  $\alpha = 8.4 \times 10^{-5} \text{ m}^2/\text{s}$   $T_i = 200^{\circ}\text{C}$   
 $T_{\infty} = 25^{\circ}\text{C}$   $h = 5000 \frac{\text{W}}{\text{m}^2 \cdot {}^{\circ}\text{C}}$   $T_0 = 90^{\circ}\text{C}$   $L = 5 \text{ cm} = 0.05 \text{ m}$ 

$$\frac{\theta_0}{\theta_i} = \frac{90 - 25}{200 - 25} = 0.37$$
  $\frac{k}{hL} = \frac{204}{(5000)(0.05)} = 0.82$ 

From chart 
$$\frac{\alpha \tau}{L^2} = 1.3$$
  $\tau = \frac{(1.3)(0.05)^2}{8.4 \times 10^{-5}} = 38.7 \text{ sec}$ 

#### 4-136

$$\frac{k}{hL} = 0 \text{ for } h \to \infty$$

$$\frac{\theta_0}{\theta_i} = 0.37 \qquad \text{From chart } \frac{\alpha \tau}{I_i^2} = 0.5 \qquad \tau = \frac{(0.5)(0.05)^2}{8.4 \times 10^{-5}} = 14.9 \text{ sec}$$

### 4-137

Lumped capacity 
$$\rho = 2707 \text{ kg/m}^3$$
  $c = 896 \frac{\text{J}}{\text{kg} \cdot {}^{\circ}\text{C}}$   

$$\frac{hA}{\rho cV} = \frac{(5000)A}{(2707)(896)A(0.05)} = 0.041$$

$$90 - 25 = e^{-0.041\tau} = 0.27$$

$$\frac{90 - 25}{200 - 25} = e^{-0.041\tau} = 0.37$$

$$\tau = 24.2 \text{ sec}$$

#### 4-138

### Suddenly exposed plate

$$\frac{90 - 25}{200 - 25} = 0.37 = \text{erf}\left(\frac{x}{2\sqrt{\alpha\tau}}\right) \qquad \frac{x}{2\sqrt{\alpha\tau}} = 0.34$$

$$\tau = \frac{\left[\frac{0.05}{(2)(0.34)}\right]^2}{8.4 \times 10^{-5}} = 64.4 \text{ sec}$$

Convectively exposed plate
$$\frac{hx}{k} = \frac{(5000)(0.05)}{204} = 1.22$$

$$\tau = \frac{(7)(0.05)^2}{8.4 \times 10^{-5}} = 208 \text{ sec}$$

#### 4-139

$$h = 23$$
  $k = 1.37$   $\alpha = 7.5 \times 10^{-7}$   $L = 18$  cm  
 $T_i = 30$ °C  $T_{\infty} = 0$ °C  $T_{x=0} = 5$ °C

a. Back side insulated

$$\frac{\theta_L}{\theta_i} = \frac{5-0}{30-0} = 0.167$$
  $\frac{k}{hL} = \frac{1.37}{(23)(0.18)} = 0.331$   
At  $\frac{x}{L} = 1.0$ , using infinite plate Heisler chart  $\frac{\theta}{\theta_0} = 0.355$ 

By iteration, 
$$F_0 = \frac{\alpha \tau}{L^2} = 0.7$$
  $\tau = 8.4 \text{ h}$ 

**b.** Semi-infinite solid Iterative solution of Eq. (4–15) yields  $\tau = 13.7$  h

#### 4-140

$$T_1 = 70^{\circ}\text{F}$$
  $T_{\infty} = 350^{\circ}\text{F}$   $h = 2.5$   $k_w = 0.395$   $\rho = 59.6$   $c_p = 1.0$   $\alpha = 0.00663$   $V = 0.084 \text{ ft}^3 \text{ (assume spherical roast)}$   $r = 0.271 \text{ ft} = r_0$   $\frac{k}{hr_0} = 0.583$   $\frac{\theta_0}{\theta_i} = 0.536$   $\frac{\alpha \tau}{r_0^2} = 0.3$ 

#### 4-145

$$r_0 = 1.5 \text{ in} = 3.81 \text{ cm}$$
  $k = 0.585$   $\alpha = 1.4 \times 10^{-7}$   $\rho = 999$   $c = 4195$ 

Take T = 3°C at outside of orange to prevent frostbite

$$\frac{k}{hr_0} = \frac{0.585}{(45)(0.0381)} = 0.34 \qquad \frac{\theta}{\theta_0} = 0.33$$

$$\frac{\theta}{\theta_i} = \frac{3 - 0}{25 - 0} = 0.12 = \frac{\theta_0}{\theta_i} (0.33)$$

$$\frac{\theta_0}{\theta_i} = 0.364 \rightarrow \frac{\alpha \tau}{r_0^2} = 0.35$$

$$\tau = \frac{(0.35)(0.0381)^2}{1.3 \times 10^{-7}} = 3888 \text{ sec}$$

$$\frac{hr_0}{\theta_0} = 2.93 \qquad \frac{h^2 \alpha \tau}{\theta_0} = \frac{(45)^2 (1.3 \times 10^{-7})(388)^2}{1.3 \times 10^{-7}}$$

$$\frac{hr_0}{k} = 2.93 \qquad \frac{h^2 \alpha \tau}{k^2} = \frac{(45)^2 (1.3 \times 10^{-7})(3888)}{(0.585)^2} = 2.99$$

$$\frac{Q}{Q_0} = 0.84$$

For 100 oranges:

$$Q = (100)(999)(4195)\frac{4}{3}\pi(0.0381)^3(0.84)(25-0) = 1.19 \times 10^6 \text{ J} = 1125 \text{ Btu}$$

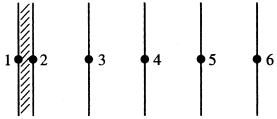
#### 4-147

The thermal resistance between the slab in contact with the ground may be determined from the shape factors of table 3–1. This information may be used in conjunction with properties of the insulation to determine the steady state temperature distribution. For the transient analysis a numerical model must be formulated.

#### 4-149

Polyethylene 
$$k = 0.33$$
  $\rho = 960$   $c = 2100$   $\alpha = 1.64 \times 10^{-7}$   
Particle board  $k = 0.17$   $\rho = 1000$   $c = 1300$   $\alpha = 1.31 \times 10^{-7}$ 

Assume all heat flux absorbed



2 mm 2.5 cm

Because polyethylene is so thin it can be neglected in comparison to other material

#### Node 2

$$1300 + \frac{0.17}{0.025} (T_3^p - T_2^p) = (1000)(1300)(0.0125) \frac{T_2^{p+1} - T_2^p}{\Delta \tau}$$
$$= 16,250 \frac{T_2^{p+1} - T_2^p}{\Delta \tau}$$

 $\Delta \tau_{\rm max} = 2390~{\rm sec}$ , and the same value results for other nodes. Choosing  $\Delta \tau = 2390~{\rm sec}$  for the time increment, the nodal equations are

$$T_2^{p+1} = 191.2 + T_3^p$$

$$T_3^{p+1} = \frac{(T_2^p + T_4^p)}{2}$$

$$T_4^{p+1} = \frac{(T_3^p + T_5^p)}{2}$$

$$T_5^{p+1} = \frac{(T_4^p + T_6^p)}{2}$$

$$T_6^{p+1} = T_5^p$$

Time to reach  $50^{\circ}\text{C} = 5.8$  time increments = (5.8)(2390) = 13,860 sec = 3.85 h

### 4-150

 $A_r$  = surface area for radiation

 $A_c$  = surface area for convection

m = mass

c = specific heat

$$h = A(T - T_{\infty})^n$$

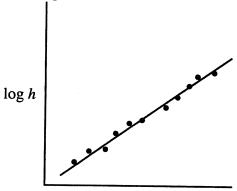
$$q_{\rm rad} = \sigma \varepsilon A_r (T^4 - T_{\infty}^4)$$

$$q_{\rm conv} = hA_c(T - T_{\infty})$$

$$q_r + q_c = -mc\frac{dT}{d\tau}$$

$$\sigma \varepsilon A_r [(T^p)^4 - T_{\infty}^4] + h A_c (T^p - T_{\infty}) = \frac{T^{p+1} - T^p}{\Lambda \tau}$$
 (1)

 $T^p$  measured as function of time during cooling process. Calculate values of h from Eq. (1) for time increments. Plot



 $\log (T - T^{\circ})$ 

Determine values of A and n from graph or from least squares analysis of  $\log h = \log A + n \log(T - T_{\infty})$