- **Problem 1:** A gas is confined in a vertical 0.47 m diameter cylinder by a piston. On the piston rests a weight and the combined mass of the piston and weight is 150 kg. The local acceleration of gravity is 9.81 m.s $^{-2}$  and the ambient pressure is 101.57 kPa.
  - (a) What is the total force exerted on the gas by the atmosphere, the piston and the weight assuming no friction between the piston and the cylinder?
  - (b) What is the pressure of the gas?
  - (c) The gas in the cylinder is heated and expands pushing the piston and weight upward. Calculate the work done by the gas if the piston and weight are raised 0.83 m. What is the change in potential energy of the piston and weight?

**Problem 2:** In a closed system (kinetic and potential energy are constant) three consecutive processes are done by an ideal gas (10 moles,  $MW = 24.945 \text{ g.gmol}^{-1}$ ):

Initial conditions:	$P_1 = 1 \text{ bar, } T_1 = 300 \text{K}$
Process $1\rightarrow 2$ :	Reversible isothermal compression, $V_2 = 0.1 \text{m}^3.\text{kg}^{-1}$
Process $2\rightarrow 3$ :	Isochoric colling, $P_3 = 2$ bar
Process $3\rightarrow 4$ :	Isobaric heating, $T_4 = 600 \text{ K}$

- (a) Calculate the initial volume  $V_1^t$  and specific volume  $V_1$  of the gas.
- (b) Calculate the pressure  $P_2$  after the first process.
- (c) Calculate the temperature  $T_3$  after the second process.
- (d) Calculate the final specific volume V<sub>4</sub>.
- (e) What forms of energy are present in transit across the system's boundary during the first process? Calculate the values.
- (f) Which kind of process can we use to reach the initial state?
- (g) Draw a PV diagram with all processes  $1 \rightarrow 2 \rightarrow 3 \rightarrow 4 \rightarrow 1$ .

**Problem 3:** One mole of an ideal gas with  $C_P = (7/2)R$  and  $C_V = (5/2)R$  expands form  $P_1 = 8$  bar and  $T_1 = 600$  K to  $P_2 = 1$  bar by each of the following paths:

- (a) Constant volume.
- (b) Constant temperature.
- (c) Adiabatically.

Assuming mechanical reversibility, calculate W, Q,  $\Delta U$ ,  $\Delta H$  for each process. Sketch each path on a single PV diagram.

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- **Problem 4:** A Carnot engine receives 250 kJ.s<sup>-1</sup> of heat from a heat-source reservoir at 525°C and rejects heat to a heat-sink reservoir at 50°C. What are the power developed and the heat rejected?
- **Problem 5:** An ideal gas at 2500 kPa is throttled adiabatically to 150 kPa at the rate of 20 gmol.s<sup>-1</sup>. Determine the rate of entropy generation if the surrounding temperature is  $T_0 = 300 \text{ K}$ .
- **Problem 6:** One kilogram of water  $\left(V_1 = 1003 \text{ cm}^3.\text{kg}^{-1}\right)$  in a piston/cylinder device at 25°C and 1 bar is compressed in a mechanically reversible, isothermal process to 1500 bar. Determine  $Q, W, \Delta U, \Delta H$  and  $\Delta S$  given that  $\beta = 250 \times 10^{-6} \text{ K}^{-1}$  and  $\kappa = 45 \times 10^{-6} \text{ bar}^{-1}$ . A satisfactory assumption is that V is at its arithmetic average value. As a PVT equation of state use:

$$\frac{\mathrm{d}V}{V} = \beta \mathrm{d}T - \kappa \mathrm{d}P$$

**Problem 7:** Assuming S = S(P, V) and taking into consideration that,

$$\left(\frac{\partial S}{\partial T}\right)_V = \frac{C_V}{T}$$
 and  $\left(\frac{\partial S}{\partial T}\right)_P = \frac{C_P}{T}$ 

Prove that

$$dS = \frac{C_V}{T} \left( \frac{\partial T}{\partial P} \right)_V dP + \frac{C_P}{T} \left( \frac{\partial T}{\partial V} \right)_P dV$$

- **Problem 8:** Large quantities of liquefied natural gas (LNG) are shipped by ocean tanker. At the unloading port provision is made for vaporisation of the LNG so that it may be delivered to pipelines as gas. The LNG arrives in the tanker at atmospheric pressure and 113.7 K, and represents a possible heat sink for use as the cold reservoir of a heat engine. For unloading of LNG as a vapour at the rate of 9000  $m^3.s^{-1}$ , as measured at 298.15 K and 1.0133 bar, and assuming the availability of an adequate heat source at 303.15 K, what is the maximum possible power obtainable and what is the rate of heat transfer from the heat source? Assume that LNG at 298.15 K and 1.0133 bar is an ideal gas with the molar mass of 17. Also assume that the LNG vaporises only, absorbing only its latent heat of 512 kJ/kg at 113.7 K.
- **Problem 9:** Given saturated ammonia vapour at  $P_1 = 200kPa$  compressed by a piston to  $P_2 = 1.6MPa$  in a reversible adiabatic process, (a) find the work done per unit mass; (b) sketch the T-s and P-v diagrams. Given:

T	$P_{sat}$	$v_f$	$v_g$	$u_f$	$u_g$	$h_f$	$h_g$	$s_f$	$s_g$
-20	190.2	$1.504 \times 10^{-3}$	0.62334	88.76	1299.5	89.05	1418.0	0.3657	5.6155
-15	236.3	$1.519 \times 10^{-3}$	0.50838	111.3	1304.5	111.66	1424.6	0.4538	5.5397

with 
$$[T] = {}^{o}C$$
;  $[P] = kPa$ ;  $[v] = \frac{m^{3}}{kg}$ ;  $[u] = [h] = \frac{kJ}{kg}$ ,  $[s] = \frac{kJ}{kg.K}$ 

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## Sutorial 02

## Problem 03

(a) Finston = 
$$mng = 150 \text{ Mg} \times 9.81 \frac{m}{5^2} = 9471.5 \text{ N}$$

(b) 
$$P_{go} = F = \frac{19092.81 \text{ N}}{7/4} = \frac{110051.78 \text{ N/m}^2}{110.051.78} = \frac{110.051.78}{110.05 \text{ N/g}}$$

piston displacement

piston displacement

The potential energy is.

$$\Delta E_{p} = mg \Delta d = 150 \text{ Kg} \times 9.81 \frac{m}{S^{2}} \times 0.83 \text{ m}$$

$$\Delta E_{p} = 1271.35 \text{ kgm}^2 = 1271.355$$

Moblem 92 (a)  $P_s \sqrt{\frac{1}{s}} = mRT_s = \frac{m}{Mul}RT_s$  $\frac{\sqrt{3}}{m} = \sqrt{3} = \frac{RT_3}{MW_{\times}R_3} = 8.314 \underbrace{5}_{\text{grad},W} \times \frac{300W_{\times}}{24.945g} \underbrace{\frac{1}{945g}}_{\text{grad}} \times \frac{1}{24.945g}$ × 1/sban  $\sqrt{1 - 99.97} \approx \frac{1 \text{N.m.}}{1 \text{Mgmn/s}^2} \times \frac{1 \text{Mgmn/s}^2}{1 \text{Mgmm/s}^2} \times \frac{1 \text{Mgmn/s}^2}{1 \text{Mgmm/s}^2} \times \frac{1 \text{Mgmn/s}^2}{1 \text{Mgm/s}^2} \times \frac{1 \text{Mgm/s}^2}{1 \text{Mgm/s}^$ [m3/K]  $V_{1} = 0.9997 \text{ m}^{3}/\text{KJ}$ and  $\sqrt{1/m} = \sqrt{1} = \sqrt{1 \times m} = \sqrt{1 \times m} \times MW$  $V_1 = 0.9997 \, \text{m}^3 \times 10 \, \text{gmod} \times 24.945 \, \text{g}$  $V_{1}^{t} = 0.24945 \, \text{m}^{3} \, \frac{1 \, \text{Mg}}{1000 \, \text{g}}$ (b) Reversible volthermal compression: (1-02) PV: constant (To=Tz)  $P_{3}\sqrt{1-P_{2}\sqrt{2}}$ .  $P_{2}=\frac{P_{3}\sqrt{1}}{\sqrt{2}}=1$  box  $\frac{0.9997 \text{ m}^{3}/\text{kg}}{0.1 \text{ m}^{3}/\text{kg}}$ Pz = 9,997 ban

(c) Isochonic earling: 
$$(2-p3)$$
  
P/T: constant  $(\sqrt{2}=\sqrt{3})$ 

$$\frac{P_2}{T_2} = \frac{P_3}{T_3}$$
 i.  $T_3 = \frac{P_3 T_2}{P_2} = \frac{0.5 ch}{9.997 bh} \times 300 K$ 

$$\sqrt{3} = 60.02 \text{ K}$$

$$\frac{\sqrt{3}}{T_3} = \frac{\sqrt{4}}{T_4} \cdot \cdot \cdot \sqrt{4} = \frac{\sqrt{3}T_4}{T_3} = 0.1 \, \text{m}^3/\text{ky} \times \frac{600 \, \text{K}}{60.02 \, \text{K}}$$

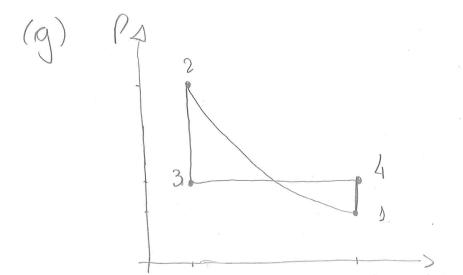
$$\sqrt{4} = 0.9997 \text{ m}^3/\text{K}_1$$

(e) Reversible isothermal process (1-02):

$$\omega = -PdV = -\frac{RT}{V}dV = -\frac{RT}{V_1} \ln \frac{\sqrt{2}}{V_2}$$

this will en me that the whole term is in ]

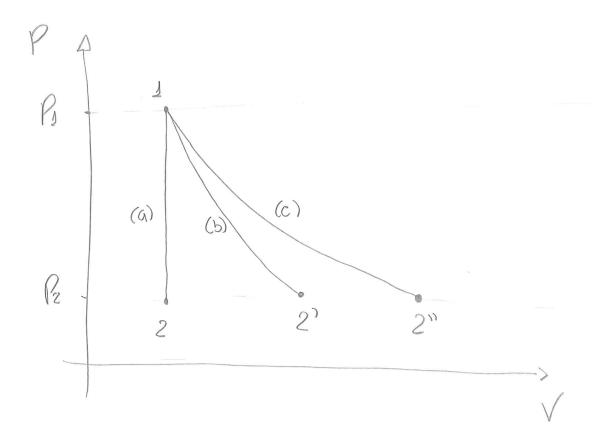
(g) Isochouic cooling



Problem 03 Ideal gas / R=8ban => Pz=1ban Cp=7/2 R and Cv=5/2R (a) Constant volume (dV=0) T2=P2 T3 = 1 x 600 = 75K ΔU= Q= C, ΔT= 5 × 8.314 J × (75-600) K DU=-10912,13 5/grof = Q DH = Cp ST = 7 × 8.314 5 × (75-600) K DM=-15276.985/gwol/ (b) Constant temperature (dT=0)  $\Delta U = 0 = \Delta H$  $\Theta = -W = -RT_s lm (R/R_s)$ 

M = -W = -10373.095/gwol

$$8 = C_p/C_J$$
;  $\sqrt{12} = \sqrt{11} \left( \frac{12}{12} \right) \frac{8-1}{8} = 600 \left( \frac{1}{8} \right) \frac{1.4-3}{1.4} = 331.23K$ 



## Problem 04 Caunot engine

$$\frac{1}{(60+273.15)K} = 1 - \frac{(50+273.15)K}{(525+273.15)K} = 0.5951$$

$$\frac{59.5}{59.5}$$

$$W_{cycle} = Q_{in} N_{canol} = 250 \frac{K5}{s} \times 05951 = 148.775 \frac{K5}{s}$$

Problem 05 Ideal Gas

 $R_1 = 2500 \, \text{MR} = 3 \, \text{R} = 150 \, \text{MR} = \frac{98}{5}$   $m = 30 \, \text{gmol/s}$  $T_0 = 300 \, \text{K}$ ;  $S_g = ?$ 

 $\Delta S = -R lm (R/R) = -8.314 \frac{J}{gwl. K} \times lm (150/2500)$ 

AS = 23.39 5 gmol. K

S=mAS=20 gmol x 23:39 <u>J</u> = 467.8 <u>J</u> K.s

Sg = To S = 300 K x 467.8 I - 140340 I

Sg = 140.3 KW

Roblem 06 (VI= 1003 cm3/Kg) 1Kg H20 P1=15on reversible

T1=75°C isothorn Pz=1500 ban Q, W, DU, DH, B= 250×10-6K-1 1 1K=45×10-6 ban-1 ) dv = BdT - [IXdP : lm V / = - IX (R-P3)  $= O(ipothermal) \qquad lm(V_2/V_1) = -1K(P_2 - P_3)$  $V_2 = V_1 \exp[-1K(R_2 - R_3)] = 1003 \text{ cm}^3 \exp[-45 \times 10^5 \text{ sa}^{-3}(1500 - 1) \text{ bal}$ V2= 937.57 cm3/Kg Vanage =  $\frac{\sqrt{1+\sqrt{2}}}{2}$  = 970. 29cm<sup>3</sup>/Kg  $dH = \frac{CpdT}{G=0} + (1-\beta T)\sqrt{dP} = \sqrt{average} (1-\beta T)(R-R)$ (instrumed) M= 970.29em3 (1-250×156/2-1 298.15 K) (1500-1) ban AU= 134.6052.54 ban.cm3 W5N/m² x 1003 cm3 X JN/m² X JN

AU = AU - (Pz /2 - Ps /s) AU=134.6×10<sup>3</sup>5 - [1500 ban 937,57 cm<sup>3</sup> - 1 ban x 1003 cm<sup>3</sup> kg] DU=134.6×1035 - 1405352 ben Cm3 x 105x1/m² x 1003 am3 11/m 140535.25/Kg AU=-5935.25/14 dS=CpdT-BVdP=-BVava (P2-P3). dS=-250×10-6 N-1, 970.29cm3 x (1500-1)ban dS = -363.61 bacom<sup>3</sup> = -36.36  $5/k_{J.}$  K J/KgK] Q = TDS. Q = - W841.21 5/kg W=/AU-Q= 4906.025/Kg

$$dS = \left(\frac{\partial S}{\partial P}\right)_{V} dP + \left(\frac{\partial S}{\partial V}\right)_{P} dV$$

) using chain sule

$$dS = \left(\frac{\partial S}{\partial T}\right) \left(\frac{\partial T}{\partial P}\right) dP + \left(\frac{\partial S}{\partial T}\right) \left(\frac{\partial T}{\partial V}\right) dV$$

$$C_{P}/T$$

Moblem 08 ING

MW= 17 g/gmol

P=1.0133ban

U = 9000 m3/s

V= 298.15 K

Calculating the mass flow nate of 2NB, assuming it behaves like an ideal gas

PV= MINET = MINERT. .. MINE = PV MW MW

m) = 1.0133 ban × 9000 m3 × 17g × 8.3145/ 298.15K

Mine = 62.54 g.bar.om³ x 105H/m² x 15 x 1000g

[Kg/s] [mine = 6254 Kg/s]

M= 303.15K

Tc = 113.7 K

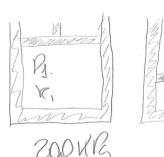
 $R_{c} = 512 \frac{K5}{K_{h}} \times m_{2N6} = 3202048 \frac{K5}{5}$ 

Marcimum pown of a thurnal cycle is introduced by a Carmot engine:

Thus, the work combe computed as
$$(W = Ac \left(\frac{T_H}{T_C} - I\right) = 3202048 \text{ KS} \left(\frac{303.15}{113.7} - I\right)$$
(a)  $W = 5335338.55 \text{ KS/s}$ , Marc Power

and the heat:

Reversible and adiabatic Compussion implies in somhopic moass





It 200 KPa, by linear interpolation in the fiven themodynamic table saturated vapour (vg)

(236.3-190.2) VIPa \_\_\_ (0.50838-062334) m3/Kg (236.3-200) MPa —  $(0.50838-7 g^*)$  m<sup>3</sup>/M<sub>1</sub>

 $V_g^* = 05989 \text{ m}^3/\text{KJ} = V_a$ 

With the same interpolation moredure,

T\*= T1=-18.94°C Mg= M, = 1300.56 KJ/kg

 $S_g^{\dagger} = S_1 = 5.5994 \text{ KJ/Kj.K}$ 

Do the mocess is isentropic

Sz= S1 = 5.5994 KJ/KJ.K

Of Pz=1.6MPa=1600KPa=16ban, the vaturation table
for ammonia (<u>Kevet-books</u>) indicales that

5g = 4.8086 K5/WK < 52

This means that the ammonia is at sevenheated 15 state. Knowing P2 and S2, we can check the superheated ammonia table (120 < T 2140°C) T(°C) M(KS/Kg) & (m3/Kg) | S(K5/KgK) 120 1516.34 011268 5.5008 140 1556.14 011974 5.6276 By linear interpolation for Sz= 5.5994 KJ/KK  $T_2 = 135.55$ °C  $v_2 = 0.11817 \text{ m}^3/4$ Uz= 1547.29 KJ/K T2 > Tc (= 132.4°C) but P2 < Pc (112.8 ban). Also  $v_z < v_s$ . From  $J^{s+}$  law o (isenthoric)  $\Delta u = q^- \omega = \mathcal{U}_z - \mathcal{U}_s : \omega = \mathcal{U}_1 - \mathcal{U}_z$  $\omega = 1300.56 - 1547.29 = -246.73 \text{ KS/KJ}$ 

