

Tire Modeling

Lateral and Longitudinal Tire Forces

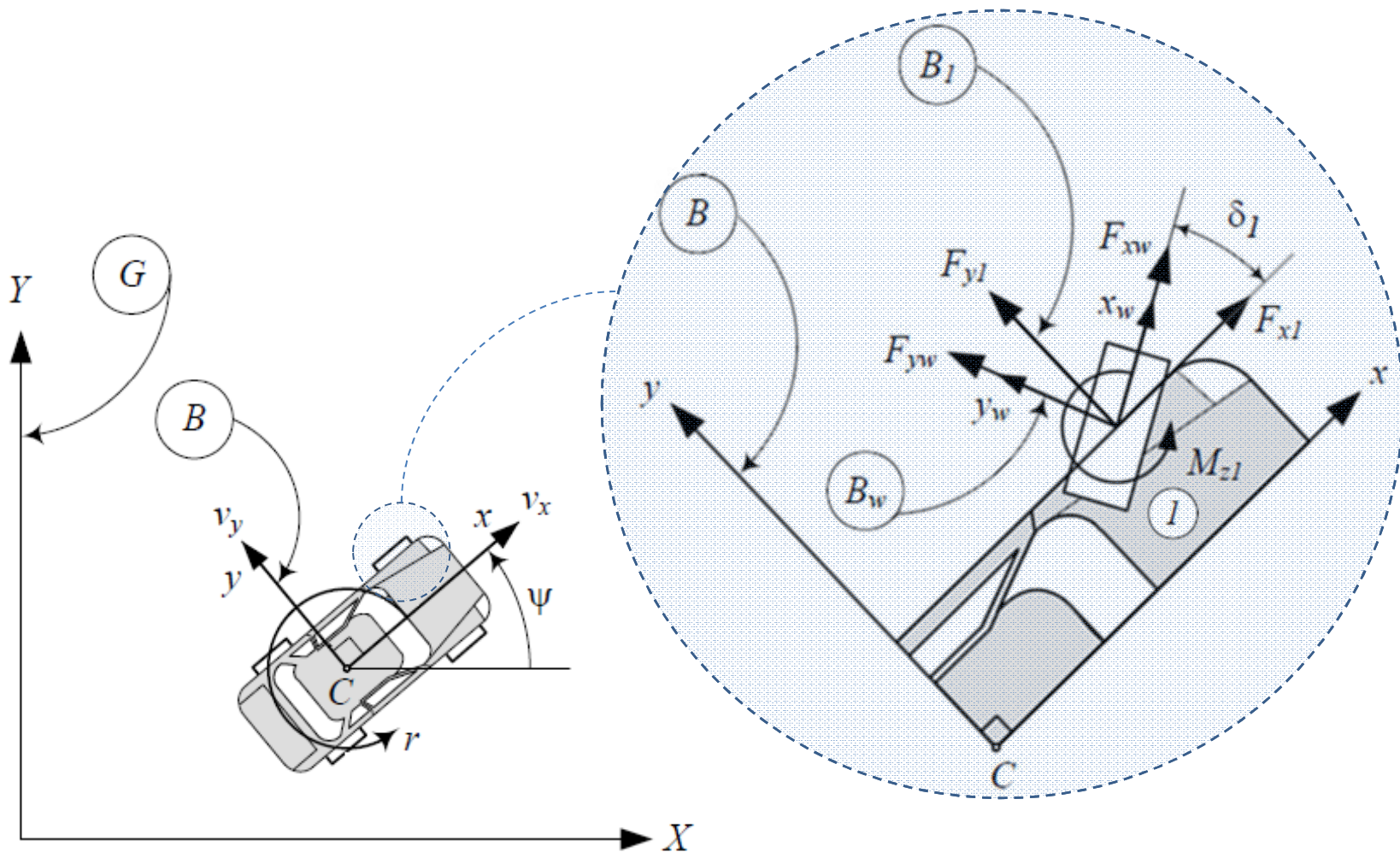
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April 27, 2009

Why Tires are important for Vehicle Control Systems?

- Tires generate the forces that drive and maneuver the vehicle.
- The knowledge of **magnitude**, **direction** and **limit** of the tire forces are essential and valuable for vehicle control systems.
- However, the estimation of these variables in **all driving conditions** and in **real-time** is a very challenging task.

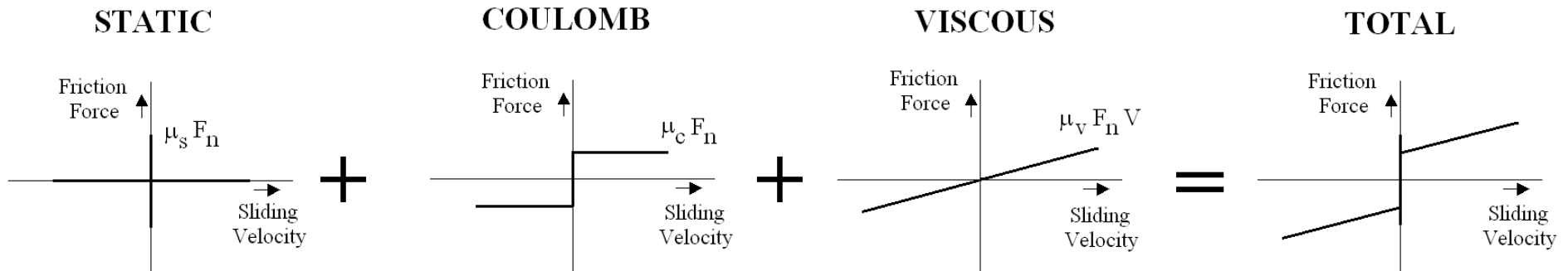
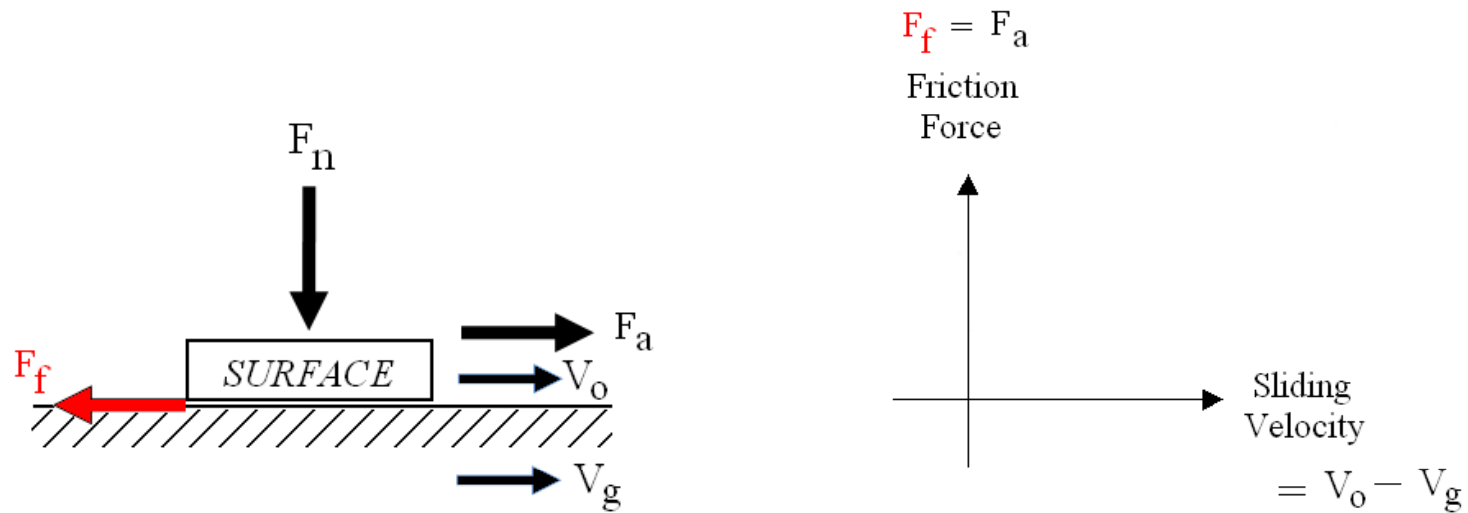
Horizontal Tire Forces



How tire force is generated?

- Tire forces are generated inside the **contact patch**, in other words between the tire and the ground.
- Tire forces are a combination of two factors:
 - **Friction/sliding** in the contact patch, and
 - **Elastic deformations/slipping** of the tire.

Background – Friction Forces



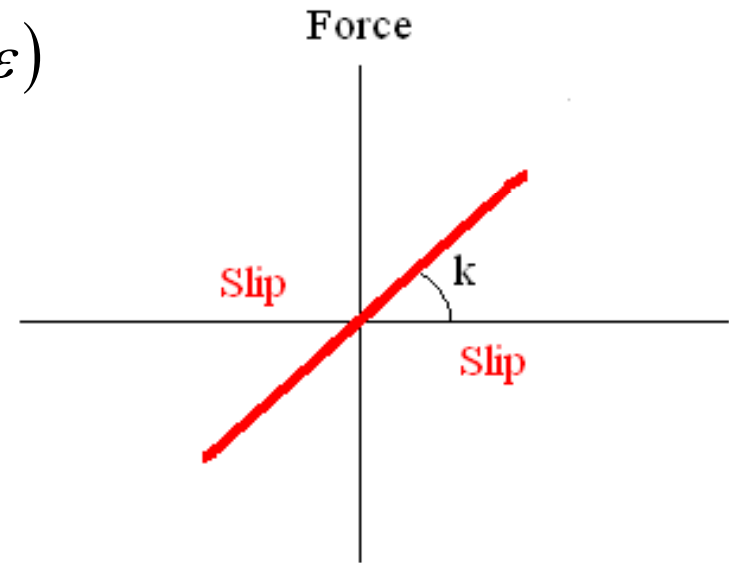
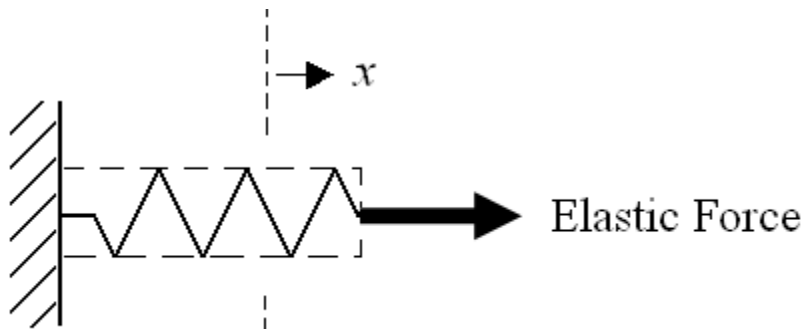
Background – Friction Forces

- Stribeck Effect
 - Stribeck (1902) observed that the friction force is decreasing continuously with increasing velocities *for low velocities*.

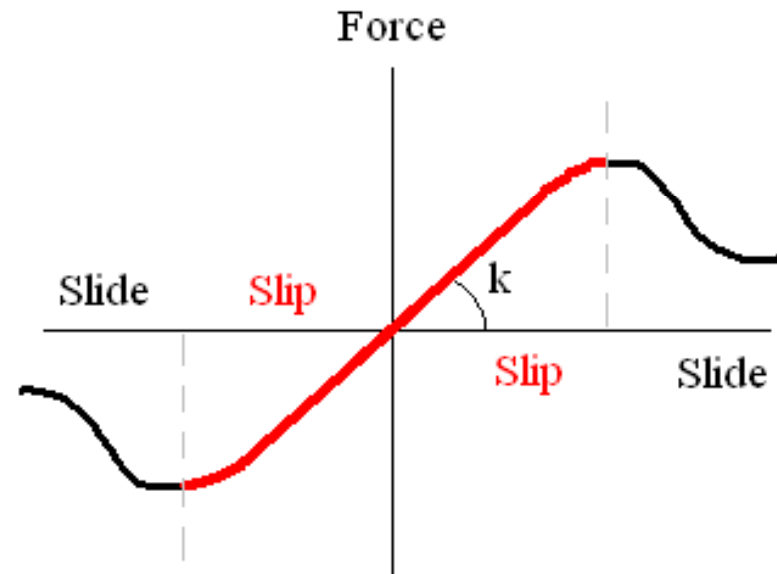
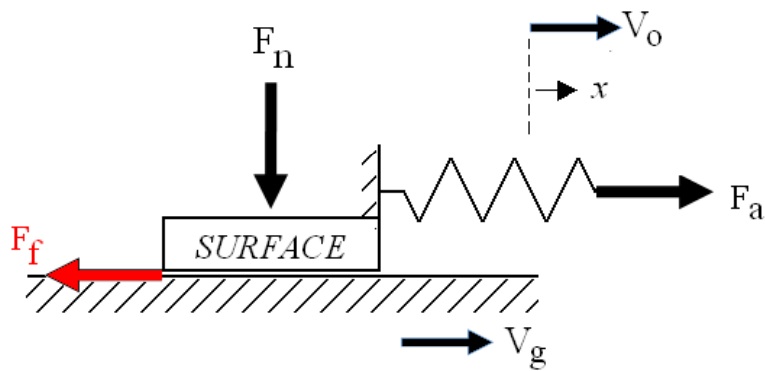


Background – Elastic Force

$$F = k \times x$$
$$(\sigma = E \times \varepsilon)$$



Background – Friction/Elastic Forces

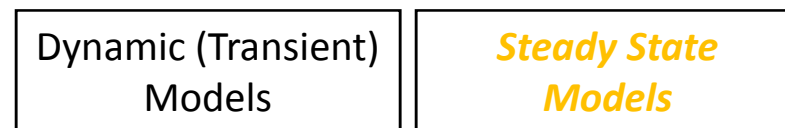


Classification of Tire Mathematical Models

- Based on how you attack the problem...



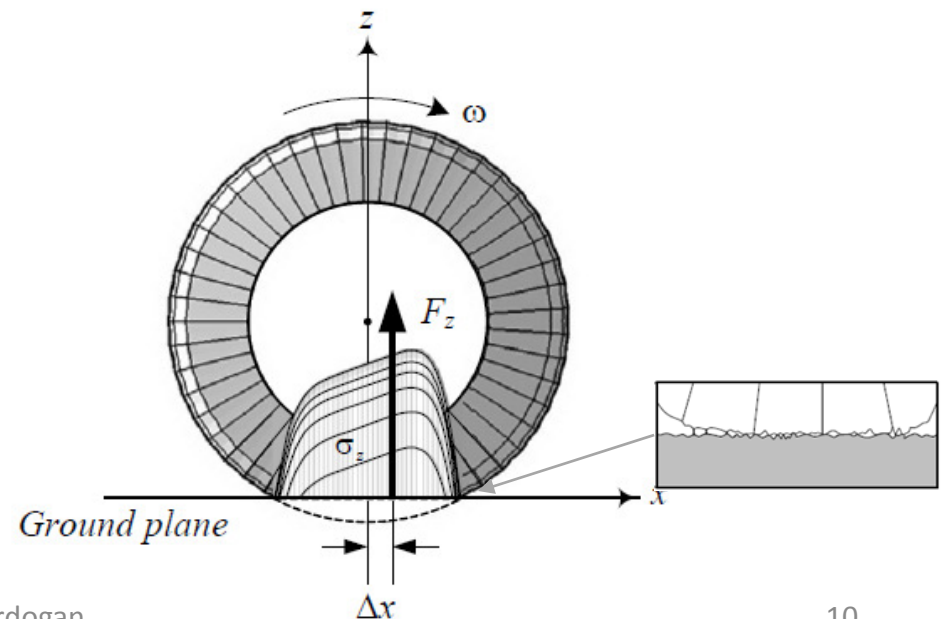
- Based on which time behavior you can capture...



Tire Models

through simple physical models

- There are four main players in tire modeling through simple physical models
 1. Tread deflection (with and w/o)
 2. Carcass/belt deflection (with and w/o)
 3. Distribution of contact pressure (symmetric and asymmetric dist.)
 4. Tire-road friction properties (variable friction)



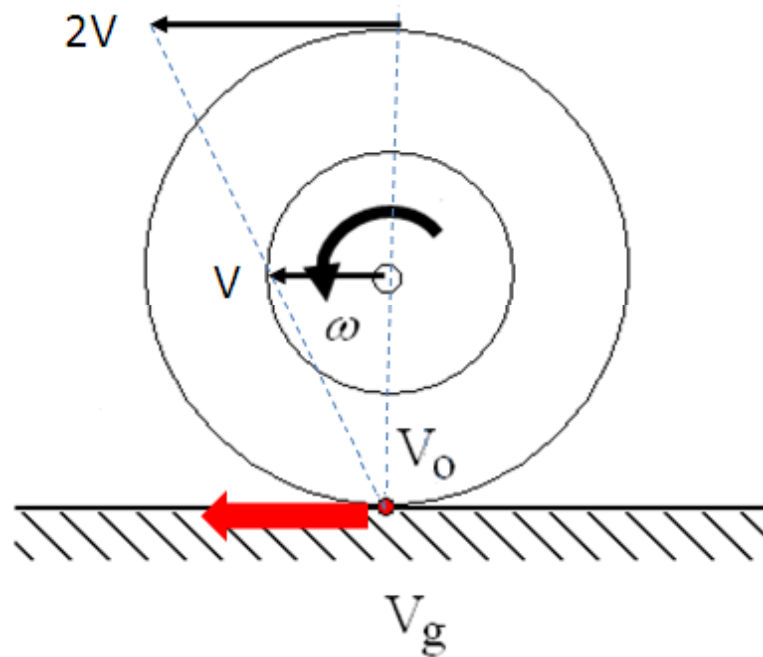
Tire Models

through simple physical models

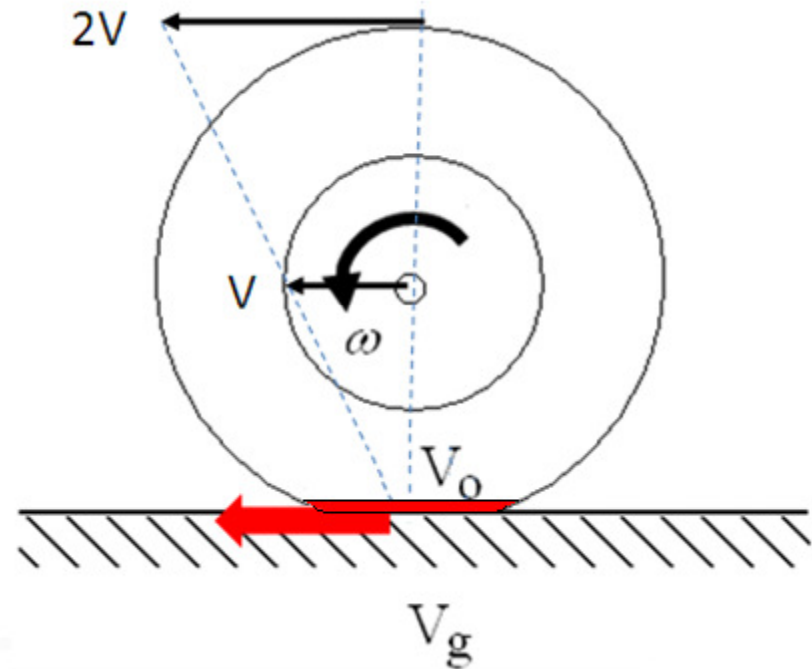
- **Brush Model**
 - **BM (Rigid Carcass)**
 - BM + Linear Carcass Deflection
 - BM + Parabolic Carcass Deflection
 - BM + Asymmetric Carcass Deflection
- **String Model**
 - Stretched String (No Tread Element)
 - BM + Stretched String
- **Beam Model**

Some Concepts - Instantaneous Center of Rotation

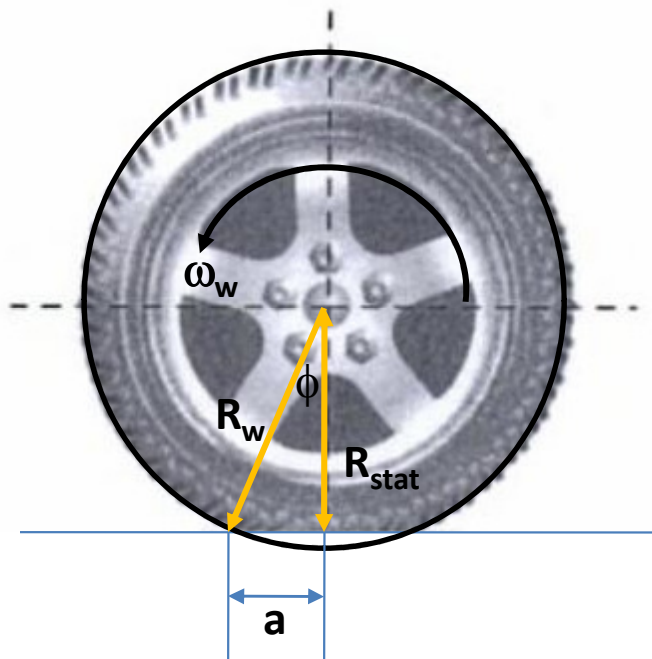
Ideally:



Reality:



Some Concepts – Effective Radius



$$V_{eff} = r_{eff} \omega_w = \frac{a}{t}$$

$$= r_{eff} \frac{\phi}{t}$$

$$r_{eff} = \frac{a}{\phi}$$

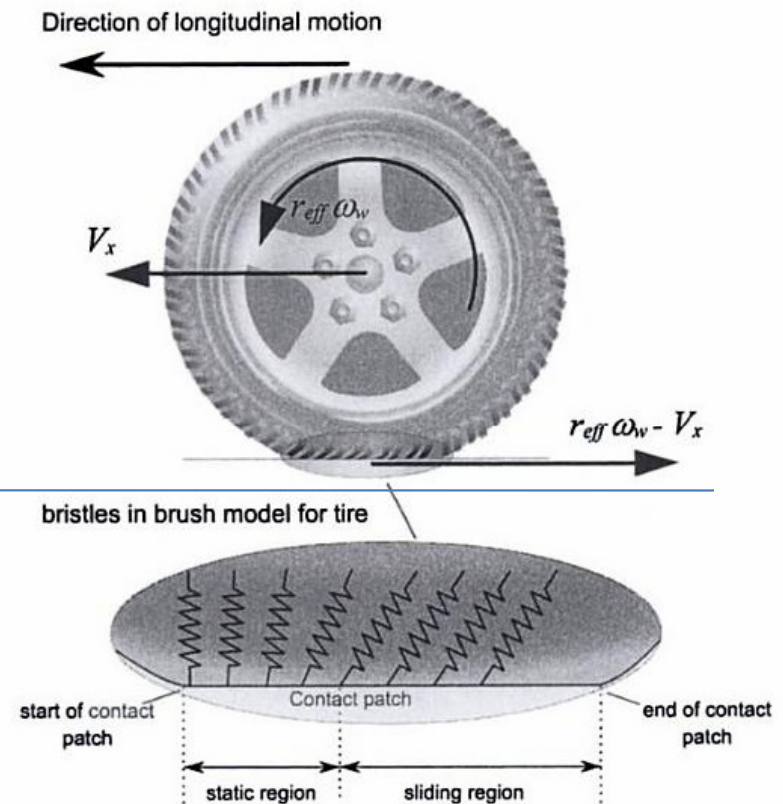
$$R_{stat} < r_{eff} < R_w$$

Brush Model – Pure Longitudinal Slip

through simple physical models

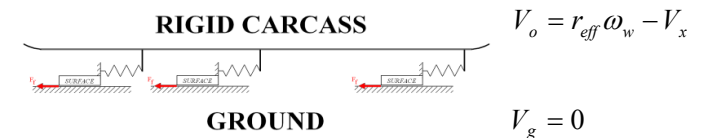
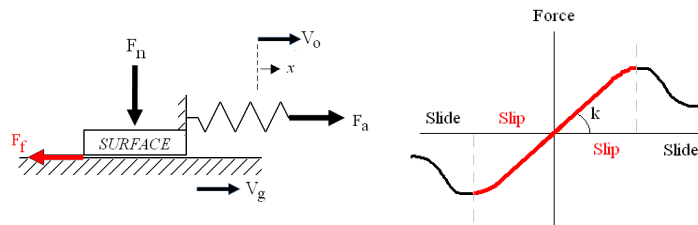
Longitudinal Tire Deformation

Slip Ratio:
$$\sigma_x = \frac{r_{eff} \omega_w - V_x}{\max(V_x, r_{eff} \omega_w)}$$



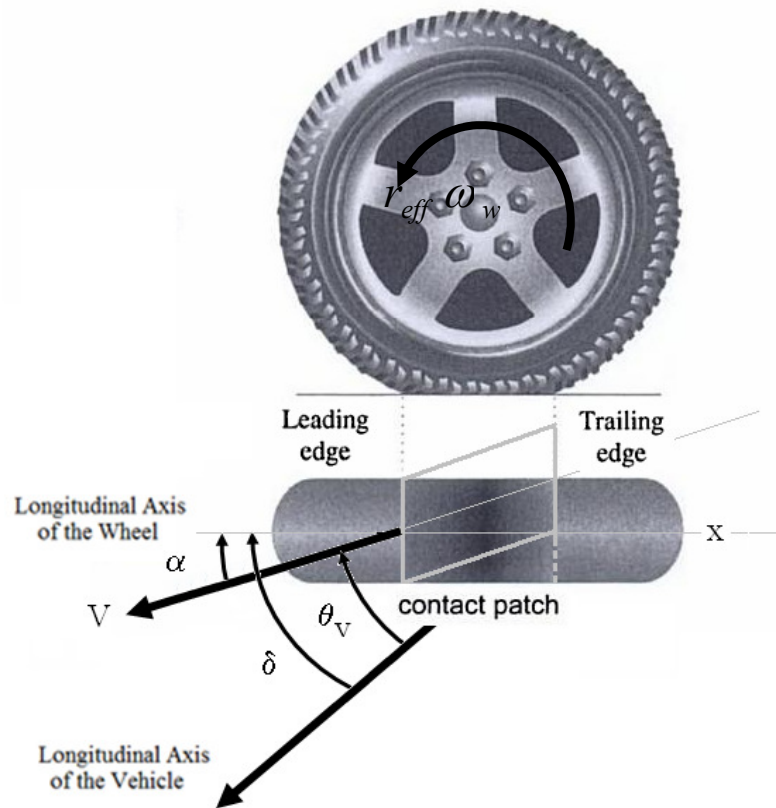
BM – Pure Longitudinal Slip

Remember...

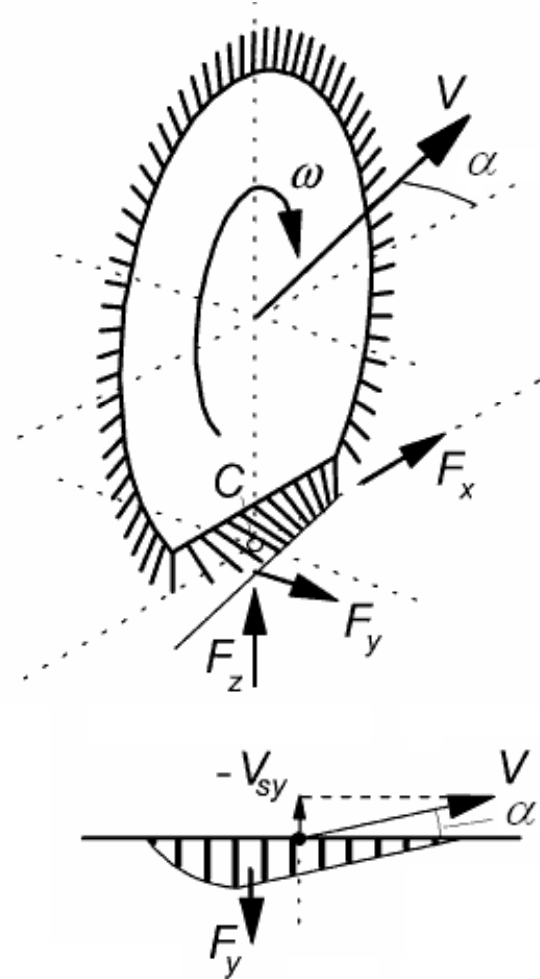


Brush Model – Pure Side Slip

through simple physical models



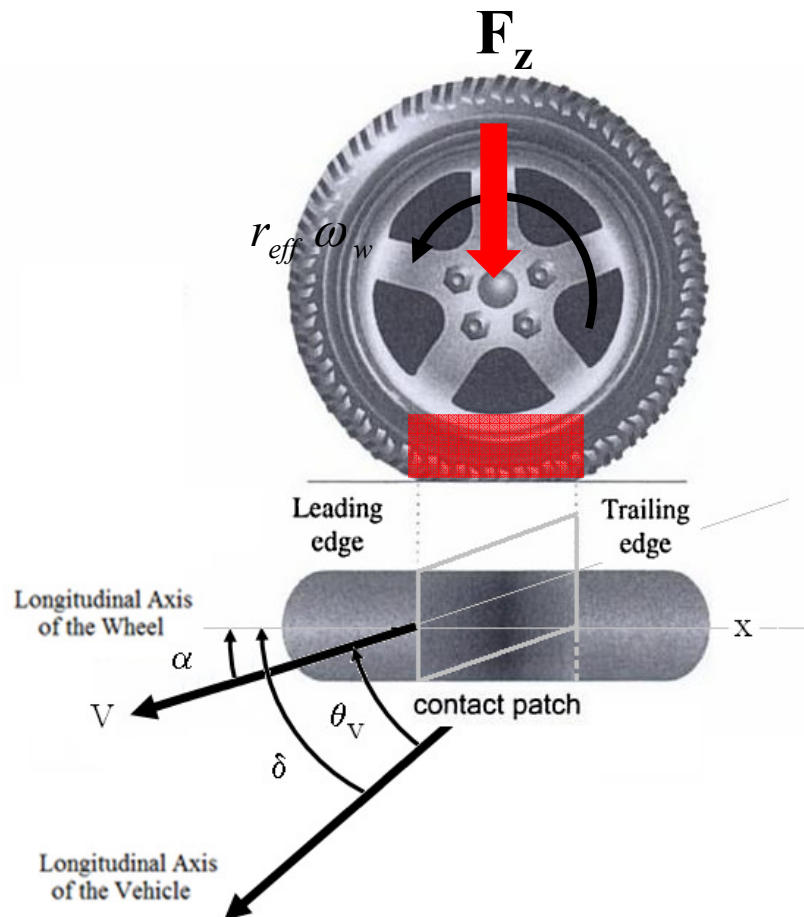
Slip Angle: $\alpha = \delta - \theta_v$



Brush Model – Pure Side Slip

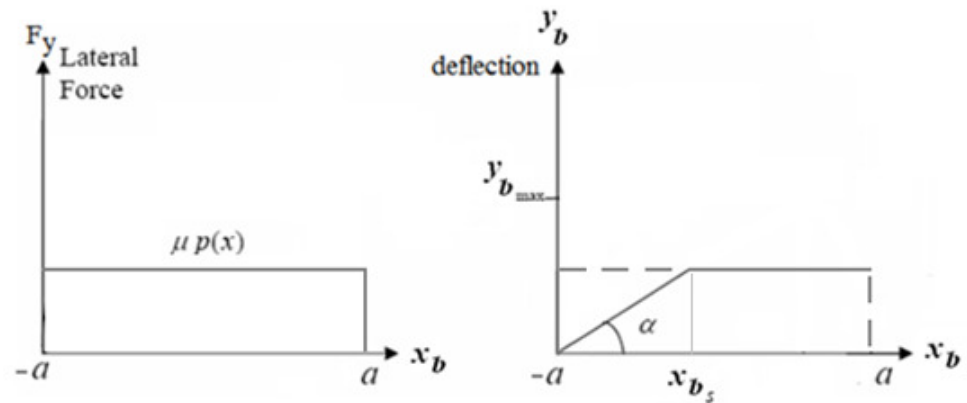
through simple physical models

- **Uniform** Normal Force Distribution



$$p(x) = \frac{F_z}{2a}$$

$$F_z = \int_{-a}^a q_z dx$$



Brush Model – Pure Side Slip

through simple physical models

- Uniform** Normal Force Distribution

Lateral Tire Force :

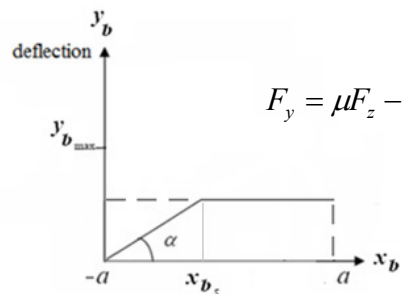
$$F_y = \mu F_z - \frac{(\mu F_z)^2}{c_{py} 8a^2 \tan(\alpha)}$$

Tire Moment:

$$M'_z = \frac{(\mu F_z)^2}{8c_{py} a \tan(\alpha)} - \frac{(\mu F_z)^3}{48c_{py} a^3 \tan^2(\alpha)}$$

Friction Coefficient :

$$\mu = \frac{2c_{py} a \tan(\alpha)}{F_z} x_{bs}$$

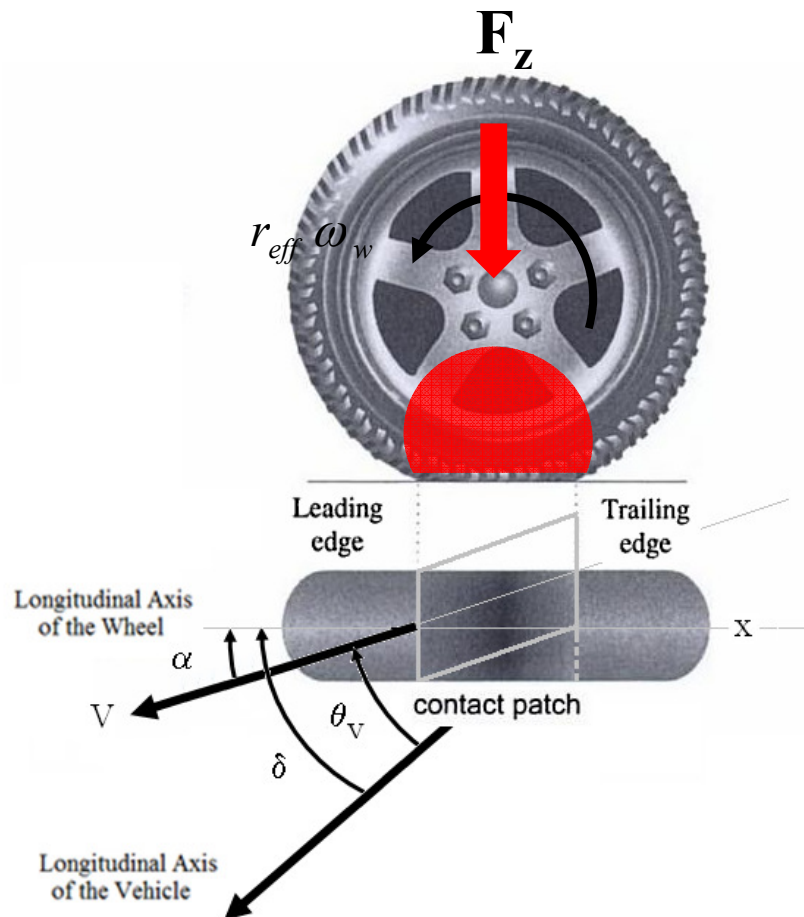


$$F_y = \mu F_z - \frac{y_{b\max} x_{bs}}{2} = \mu F_z - \left(\frac{\mu F_z}{2a} \right) \left(\frac{\mu F_z}{c_{py} 2a \tan(\alpha)} \right) \frac{1}{2}$$

Brush Model – Pure Side Slip

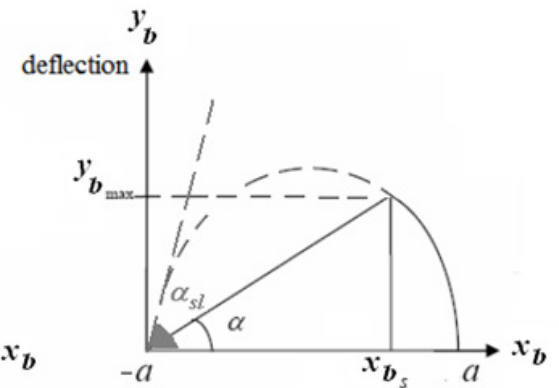
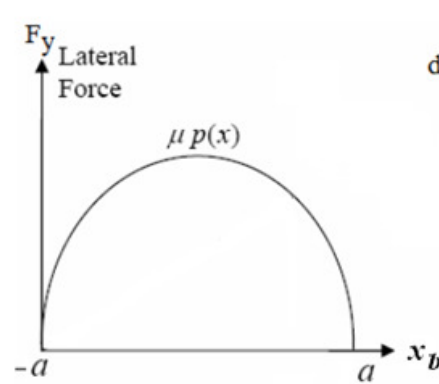
through simple physical models

- **Parabolic** Normal Force Distribution



$$p(x) = \frac{3F_z}{4a} \left(\frac{a^2 - x^2}{a^2} \right)$$

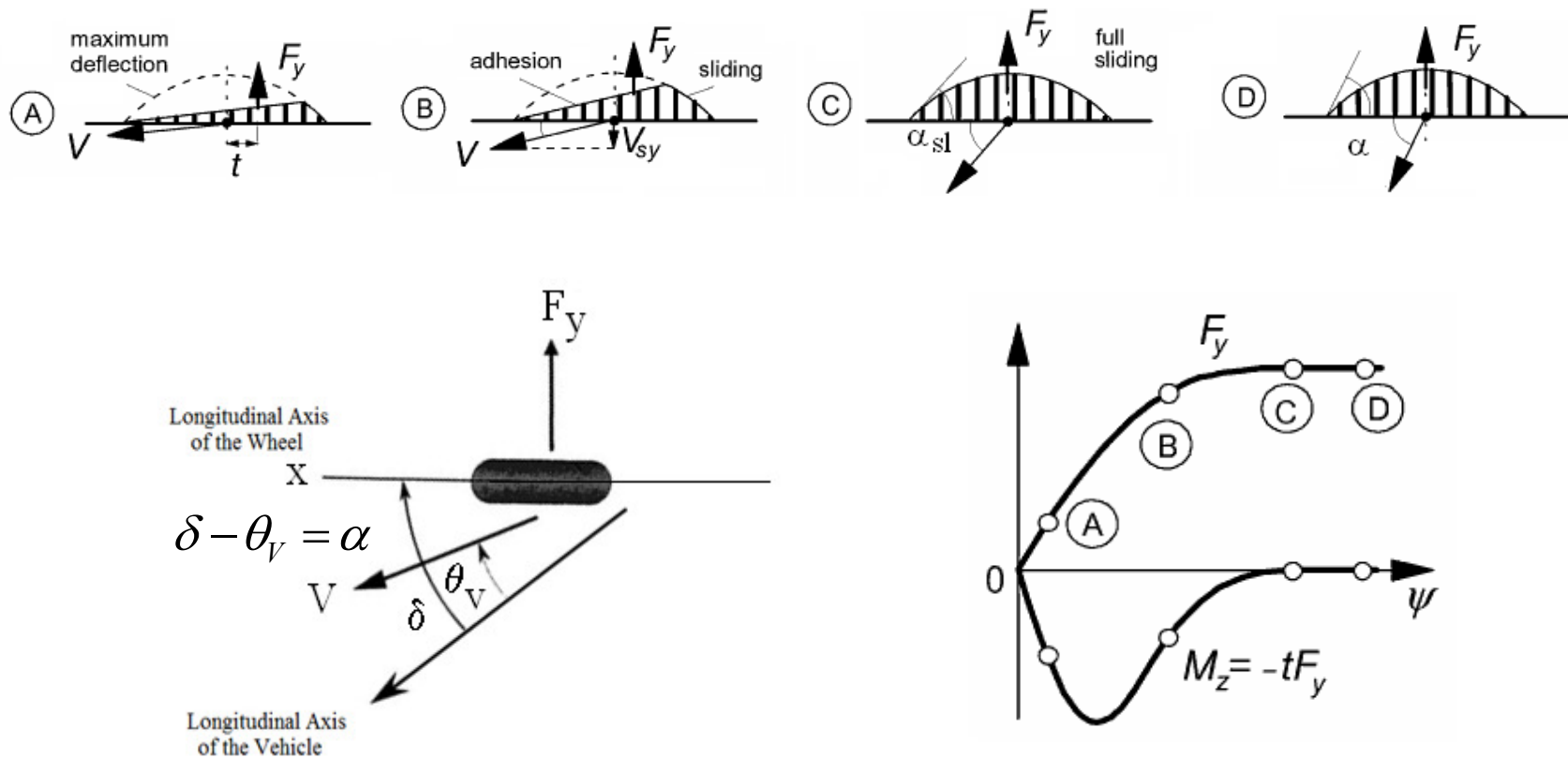
$$F_z = \int_{-a}^a p(x) dx$$



Brush Model – Pure Side Slip

through simple physical models

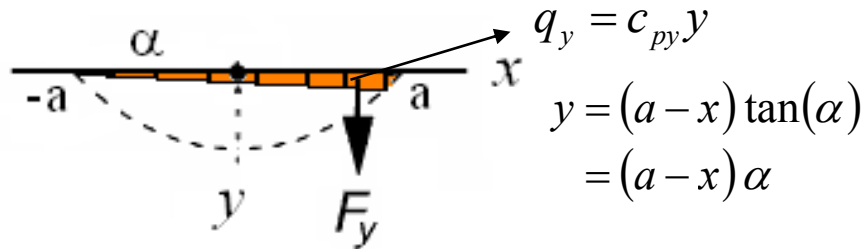
- Parabolic Normal Force Distribution



Brush Model – Pure Side Slip

through simple physical models

- Parabolic Normal Force Distribution
 - **Small Slip Angle** (as $\alpha \rightarrow 0$, $\tan(\alpha) \rightarrow \alpha$)



$$F_y = \int_{-a}^a q_y dx$$

$$= c_{py} \alpha \int_{-a}^a (a - x) dx$$

$$= c_{py} 2a^2 \alpha$$

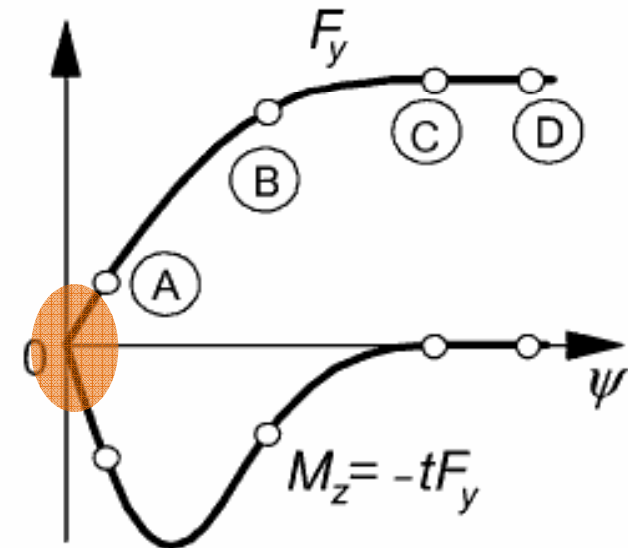
$$= C_{F\alpha} \alpha$$

$$M_z = \int_{-a}^a q_y x dx$$

$$= c_{py} \alpha \int_{-a}^a (a - x) x dx$$

$$= -c_{py} 2a^2 \frac{a}{3} \alpha$$

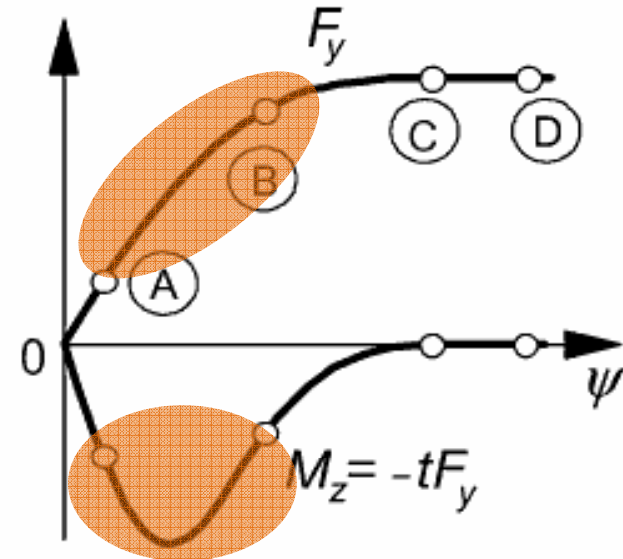
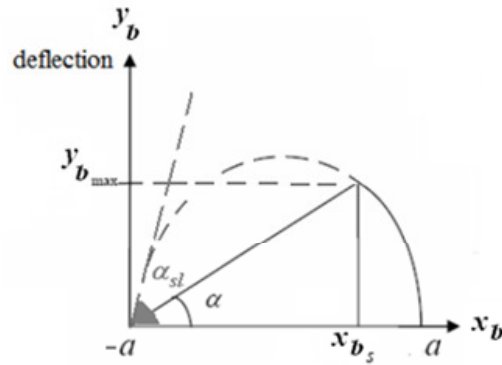
$$= -\frac{a}{3} F_y$$



Brush Model – Pure Side Slip

through simple physical models

- Parabolic Normal Force Distribution
 - Large Slip Angles



Lateral Tire Force :

$$F_y = 3\mu F_z \frac{\tan(\alpha)}{\tan(\alpha_{sl})} \left(1 - \left| \frac{\tan(\alpha)}{\tan(\alpha_{sl})} \right| + \frac{1}{3} \frac{\tan^2(\alpha)}{\tan^2(\alpha_{sl})} \right)$$

Tire Moment (Lateral):

$$M'_z = -\mu F_z a \frac{\tan(\alpha)}{\tan(\alpha_{sl})} \left\{ 1 - 3 \left| \frac{\tan(\alpha)}{\tan(\alpha_{sl})} \right| + 3 \left(\frac{\tan(\alpha)}{\tan(\alpha_{sl})} \right)^2 - \left| \frac{\tan(\alpha)}{\tan(\alpha_{sl})} \right|^3 \right\}$$

Friction Coefficient :

$$\mu = \frac{2c_{py}a^2}{3F_z} \tan(\alpha_{sl})$$

Brush Model – Combined Slip

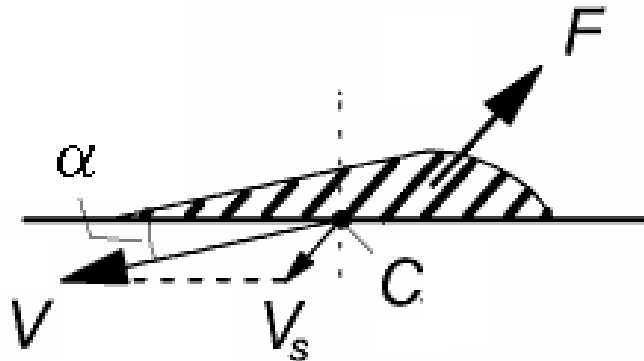
through simple physical models

- Theoretical Slips

$$\sigma_x = \begin{cases} \kappa = \frac{V_r - V_x}{V_x} = -\frac{V_{sx}}{V_x} & \text{brake} \\ \frac{\kappa}{1 + \kappa} = \frac{V_r - V_x}{V_r} = -\frac{V_{sx}}{V_r} & \text{drive} \end{cases}$$

$$\sigma_y = \begin{cases} \tan(\alpha) = -\frac{V_{sy}}{V_x} & \text{brake} \\ \frac{\tan(\alpha)}{1 + \kappa} = -\frac{V_{sy}}{V_r} & \text{drive} \end{cases}$$

$$V_r = r_{eff} \omega_w$$



$$u = (a - x)\sigma_x$$

$$v = (a - x)\sigma_y$$

$$\sigma = \sqrt{\sigma_x^2 + \sigma_y^2}$$

Brush Model – Combined Slip

through simple physical models

Tire Force :

$$F = 3\mu F_z \frac{\sigma}{\sigma_m} \left(1 - \frac{\sigma}{\sigma_m} + \frac{1}{3} \frac{\sigma^2}{\sigma_m^2} \right)$$

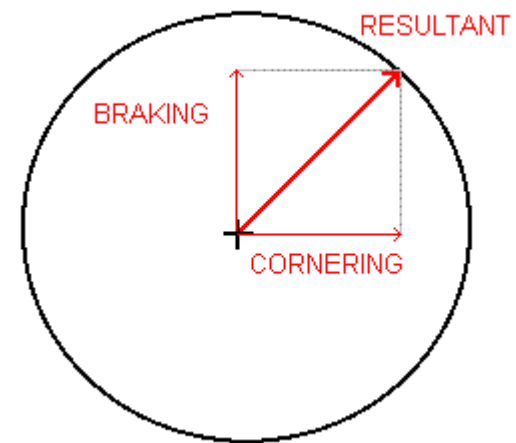
Tire Moment:

$$M'_z = -\mu F_z a \frac{\sigma}{\sigma_m} \left\{ 1 - 3 \frac{\sigma}{\sigma_m} + 3 \frac{\sigma^2}{\sigma_m^2} - \frac{\sigma^3}{\sigma_m^3} \right\}$$

Friction Coefficient :

$$\mu = \frac{2c_p a^2}{3F_z} \sigma_m$$

Friction Circle:



Brush Model – Combined Slip

through simple physical models

- Dugoff's Model

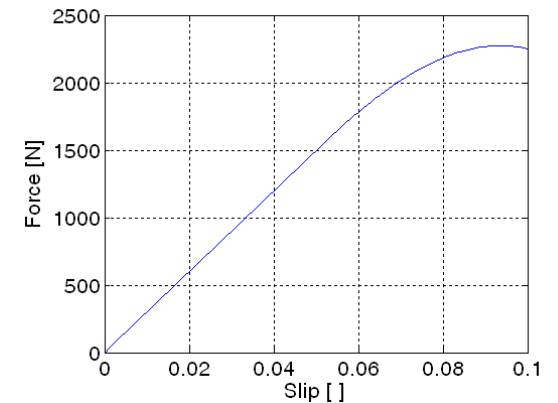
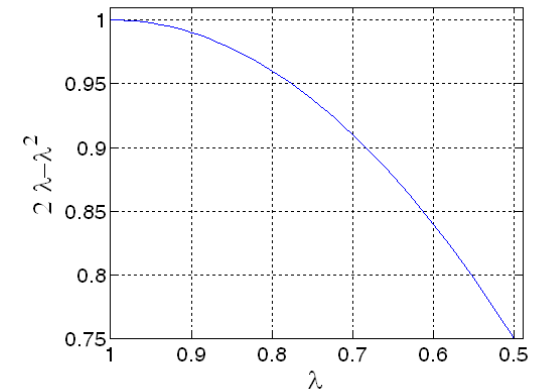
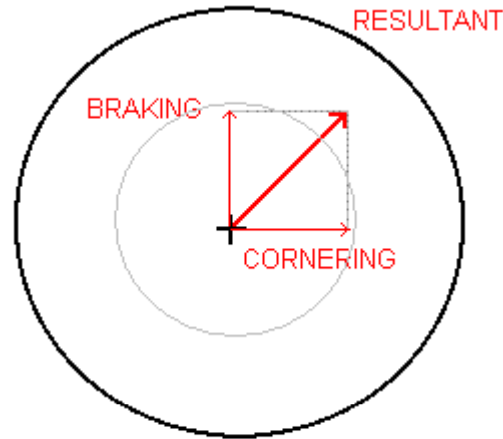
$$F_{x_lin} = C_\kappa \sigma_x$$

$$F_{y_lin} = C_\alpha \sigma_y$$

$$\text{if } \sqrt{F_{x_lin}^2 + F_{y_lin}^2} \leq \frac{\mu F_z}{2}, \quad \begin{aligned} F_x &= F_{x_lin} \times 1 \\ F_y &= F_{y_lin} \times 1 \end{aligned}$$

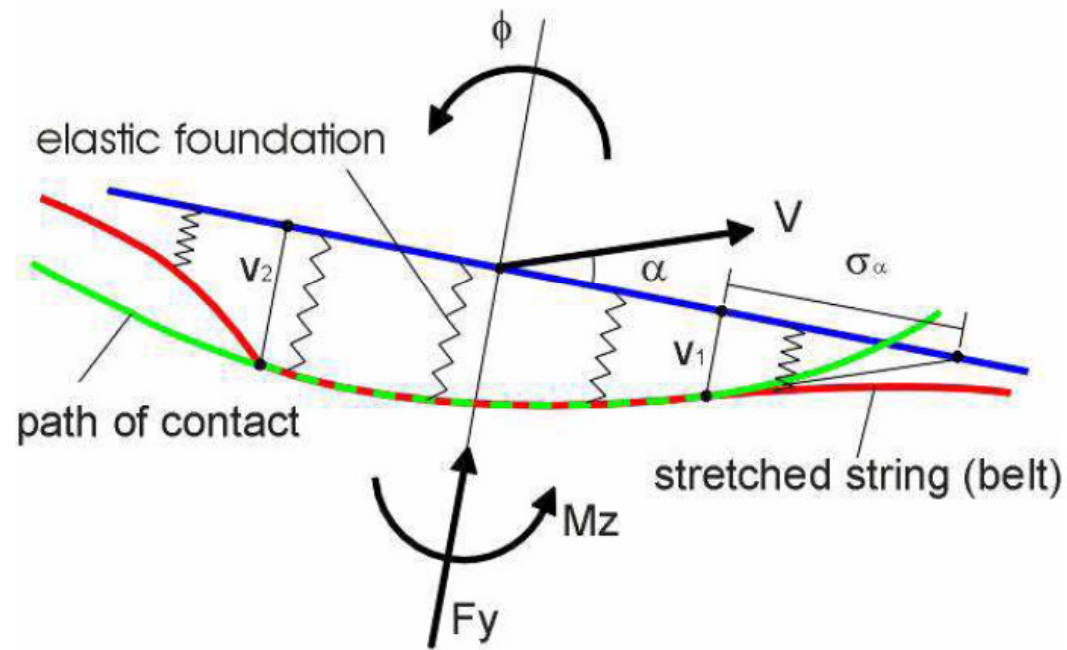
$$\text{if } \sqrt{F_{x_lin}^2 + F_{y_lin}^2} > \frac{\mu F_z}{2}, \quad \begin{aligned} F_x &= F_{x_lin} \times (2\lambda - \lambda^2) \\ F_y &= F_{y_lin} \times (2\lambda - \lambda^2) \end{aligned}$$

$$\lambda = \frac{\frac{\mu F_z}{2}}{\sqrt{F_{x_lin}^2 + F_{y_lin}^2}}$$



String Model

through simple physical models



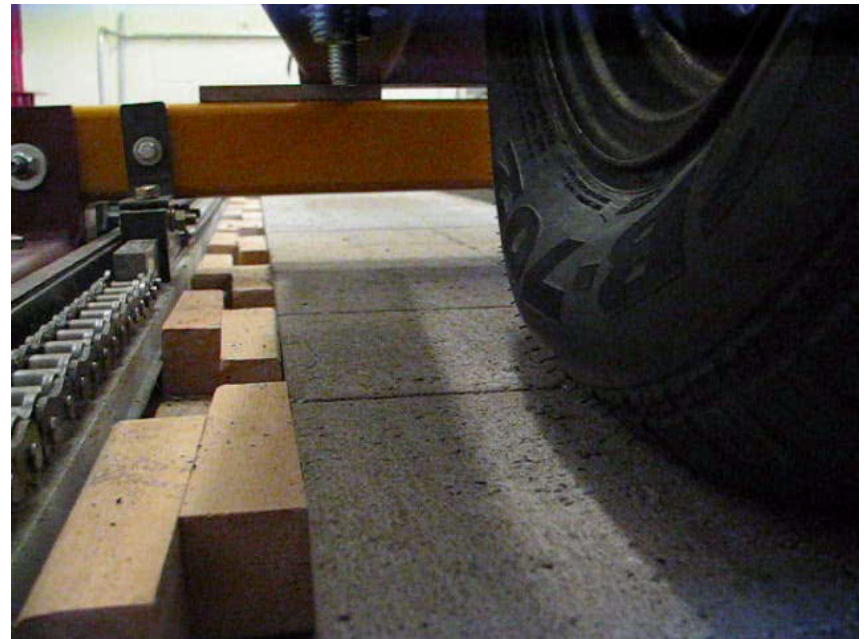
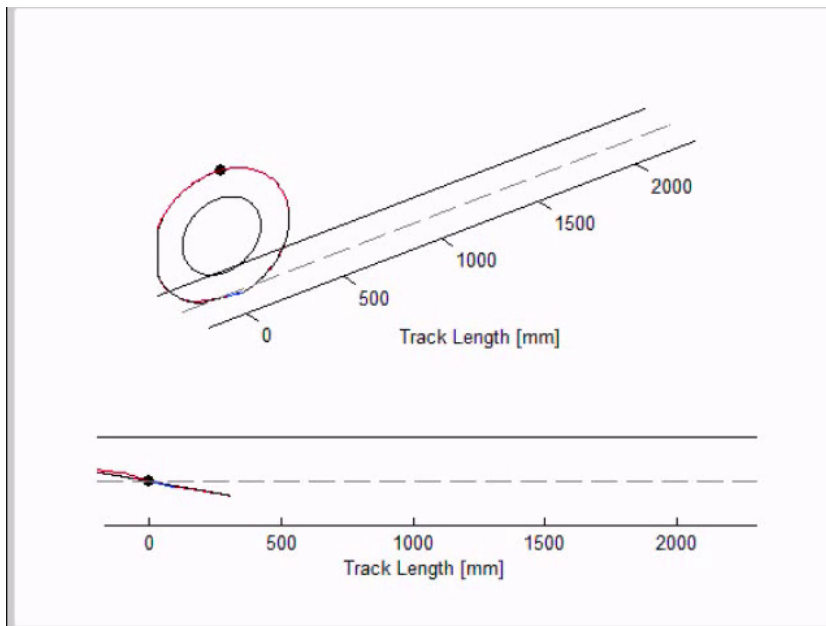
Dynamic (Transient) Tire Models

through simple physical models

- The steady state tire models are handy when we have constant linear and angular velocities.
- Experimental data used to validate the slip/force curves are obtained using specialized equipment that allows independent linear and angular velocity modulation so as to cover the whole slip range.
- This steady-state point of view is rarely true in reality, especially when the vehicle goes through continuous successive phases between acceleration and braking.
- Dynamic models capture the transient behavior of the tire-road contact forces **under time-varying** velocity conditions.
 - Bliman
 - Kinematic TM
 - **Dahl TM**
 - **LuGre TM**

Dynamic Models – Relaxation Length

- **Relaxation length**
 - is related to the distance needed by the tire to reach a the steady state situation after a step change in slip.
 - is the distance needed to build up the steady state tire forces.



Dynamic Models – Dahl Models

through simple physical models

The Dahl model is essentially **Coulomb friction with a lag**.

$$F_{\text{deformation}} = F_{\text{friction}}$$

$$\sigma_o z = F_{\text{coulomb}} \left(1 - e^{\frac{-\sigma_o |x|}{F_{\text{coulomb}}}} \right) \text{sgn}(v)$$

$$\dot{z} = v - \frac{\sigma_o |v|}{F_{\text{coulomb}}} z$$

Derivation

$$\begin{aligned} \frac{dF_{\text{deformation}}}{dt} &= \frac{dF_{\text{friction}}}{dt} \\ \dot{z} &= e^{\frac{-\sigma_o |x|}{F_{\text{coulomb}}}} |v| \text{sgn}(v) \\ e^{\frac{-\sigma_o |x|}{F_{\text{coulomb}}}} &= \frac{\dot{z}}{|v| \text{sgn}(v)} \end{aligned}$$

Steady State:

$$\begin{aligned} \dot{z} &= 0 \Rightarrow z_{ss} \\ 0 &= v - \frac{\sigma_o |v|}{F_{\text{coulomb}}} z_{ss} \\ z_{ss} &= \frac{F_{\text{coulomb}}}{\sigma_o} \text{sgn}(v) \end{aligned}$$

Dynamic Models –LuGre Models

through simple physical models

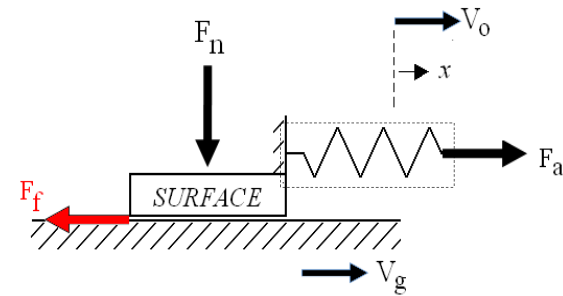
$$F_{deformation} = F_{friction}$$

$$\sigma_o z = F_{coulomb} \left(1 - e^{\frac{-\sigma_o |x|}{g(v)}} \right) \text{sgn}(v), \quad \text{or}$$

$$\sigma_o z + \sigma_1 \dot{z} + f(v) = F_{coulomb} \left(1 - e^{\frac{-\sigma_o |x|}{g(v)}} \right) \text{sgn}(v)$$

$$g(v) = F_{coulomb} + (F_{static} - F_{coulomb}) e^{-|v/v_{striebeck}|^\alpha}$$

$$f(v) = \sigma_2 v$$

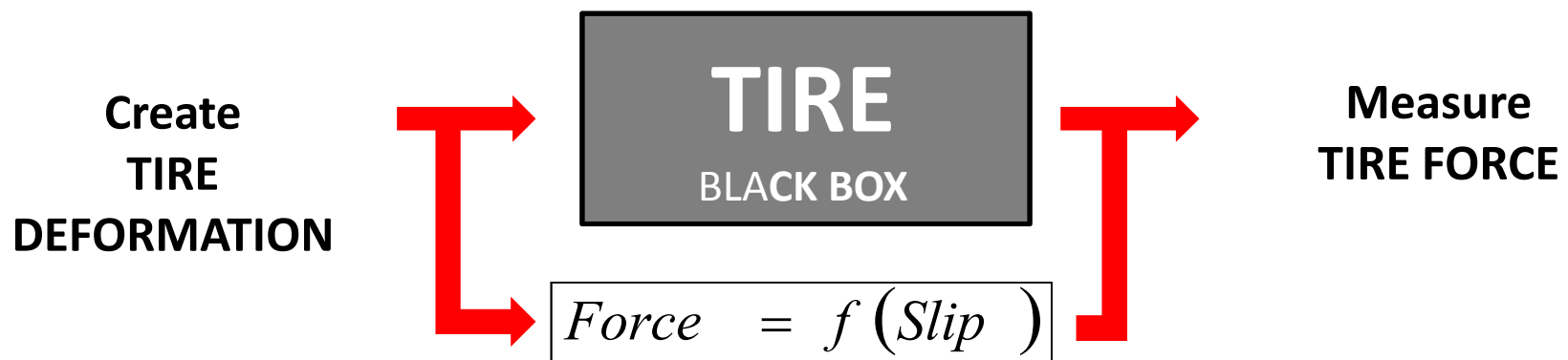


$$\dot{z} = v - \frac{\sigma_o |v|}{g(v)} z$$

Tire Models

from experimental data only

- Pacejka TM
- Burckhardt TM
- Kiencke and Daiss TM



Pacejka Tire Model (Magic Formula)

from experimental data only

$$a_1 \ a_2 \ a_3 \ a_4 \ a_5 \ a_6 \ a_7 \ a_8 \quad F_z$$

$$D = a_1 F_z^2 + a_2 F_z$$

$$BCD = a_3 \sin(a_4 \arctan(a_5 F_z)) \quad (\text{lateral force})$$

$$BCD = \frac{a_3 F_z^2 + a_4 F_z}{e^{a_5 F_z}} \quad (\text{longitudinal force})$$

$$E = a_6 F_z^2 + a_7 F_z + a_8$$

$$C = \frac{2}{\pi} \sin^{-1} \left(\frac{y_s}{D} \right)$$

$$x = X - S_h$$

$$y = D \sin \left[C \arctan \{ Bx - E(Bx - \arctan Bx) \} \right]$$

$$Y(X) = y(x) + S_v$$

B stiffness factor

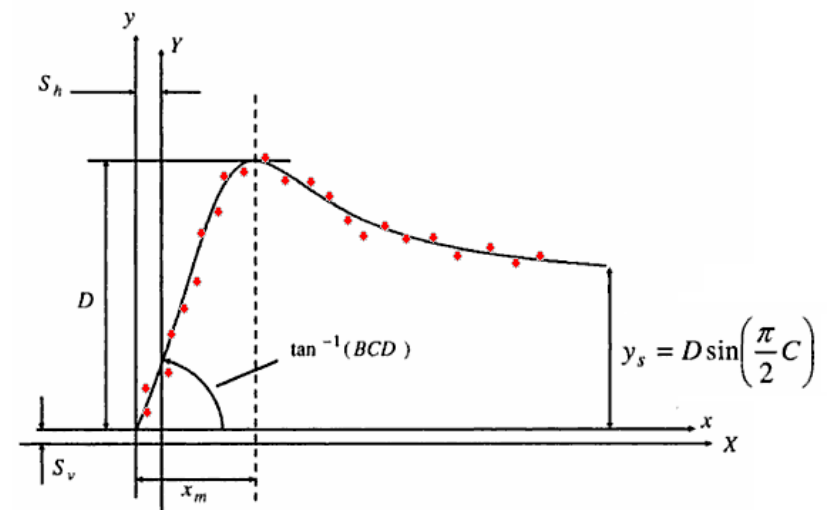
C shape factor

D peak value

E curvature factor

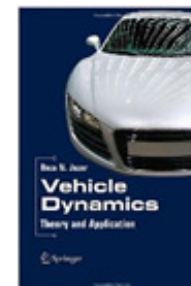
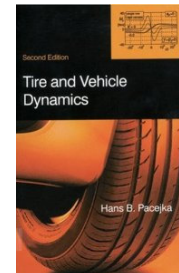
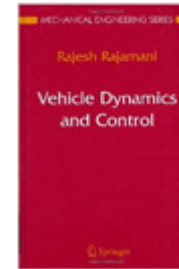
S_h horizontal shift

S_v vertical shift



References

- Vehicle Dynamics and Control, 2005, R. Rajamani
- Tire and Vehicle Dynamics, 2005, H.B. Pacejka
- Contact Mechanics, 1987, K.L. Johnson
- Vehicle Dynamics: Theory and Application, 2009, R. N. Jazar



THANKS ...