

# Designing a Kalman Filter for a Maxon EC 8 mm Brushless DC Motor with Hall Sensors

## 1. Introduction

This report describes a Kalman filter design for estimating and controlling the state of a Maxon EC (Electronically Commutated) brushless DC motor with an 8 mm diameter. This small-diameter motor is often equipped with integrated Hall effect sensors for commutation and basic speed measurement. The high-speed, compact nature of this motor makes reliable state estimation crucial, especially when sensor resolution is limited.

Key objectives include:

- Accurate real-time estimation of rotor position and speed.
- Compensation for noise in Hall sensor signals.
- Robust feedback for motor control loops.

## 2. Motor and Hall Sensor Characteristics

### 2.1 Electrical Model

A simplified voltage equation for each phase can be written as:

$$V(t) = Ri(t) + L \frac{di(t)}{dt} + e_{\text{back}}(t),$$

where

- $V(t)$  is the phase voltage,
- $i(t)$  is the phase current,
- $R$  and  $L$  are the phase resistance and inductance,
- $e_{\text{back}}(t)$  is the back-EMF voltage proportional to rotor speed.

**Typical Values (Approximate):**

- $R \approx 5.5 \, \Omega$ ,
- $L \approx 0.2 \, \text{mH}$ ,
- Back-EMF constant  $K_e \approx 2.5 \, \frac{\text{mV}}{\text{rpm}}$ ,
- Torque constant  $K_t \approx 2.4 \, \frac{\text{mN}\cdot\text{m}}{\text{A}}$ ,
- *(Exact values depend on the specific EC 8 mm variant; consult the Maxon datasheet.)*

## 2.2 Mechanical Model

The motor's rotor dynamics:

$$J \frac{d\omega}{dt} = K_t i(t) - B \omega(t) - \tau_{\text{load}}(t),$$

where

- $J$  is the rotor inertia,
- $\omega(t)$  is the angular velocity,
- $B$  is the viscous friction coefficient,
- $\tau_{\text{load}}(t)$  is the load torque.

**Typical Values:**

- $J \approx 3 \times 10^{-7} \text{ kg} \cdot \text{m}^2$  (small rotor inertia for 8 mm motor),
- $B \approx 1 \times 10^{-5} \text{ N} \cdot \text{m} \cdot \text{s/rad}$  (estimated),
- (*Exact values from the motor's official datasheet.*)

## 2.3 Hall Effect Sensors

- **Resolution:** Typically 1–3 Hall sensors yield 6 or more electrical transitions per electrical revolution (commutation signals).
- **Noise/Uncertainty:** Mechanical tolerances can cause jitter or phase error in Hall signals.
- **Measurement Rate:** Hall transitions may be measured at microcontroller interrupt level. The motor speed must be inferred from time between transitions.

# 3. State-Space Model and Kalman Filter Setup

## 3.1 State Variables

Let the state vector be

$$x(t) = \begin{bmatrix} \theta(t) \\ \omega(t) \\ i(t) \end{bmatrix},$$

where

- $\theta$  [rad] is the estimated rotor angle,
- $\omega$  [rad/s] is the angular speed,
- $i$  [A] is the phase or transformed current (e.g., in a  $dq$  reference frame).

Input  $u(t)$  can be the applied phase voltage (or  $dq$ -axis voltages).

## 3.2 Discrete-Time Approximation

For a sampling time  $\Delta t$ , the model converts to:

$$x_{k+1} = A x_k + B u_k + w_k, \quad z_k = H x_k + v_k,$$

with  $w_k$  and  $v_k$  representing process and measurement noise. Noise covariances  $Q$  and  $R$  define the filter's trust in the model vs. measurements.

### 3.3 Measurement Vector

Hall sensors can directly provide coarse rotor angle increments or speed estimates. One approach is to measure:

$$z_k = \begin{bmatrix} \theta_{\text{Hall},k} \\ i_{\text{meas},k} \end{bmatrix},$$

where  $\theta_{\text{Hall},k}$  is extracted from Hall transitions, and  $i_{\text{meas},k}$  is current sensor data. Then

$$H = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

## 4. Kalman Filter Design Steps

### 4.1 Predict

$$\begin{aligned} \hat{x}_{k|k-1} &= A \hat{x}_{k-1|k-1} + B u_{k-1}, \\ P_{k|k-1} &= A P_{k-1|k-1} A^\top + Q. \end{aligned}$$

### 4.2 Update

$$\begin{aligned} K_k &= P_{k|k-1} H^\top (H P_{k|k-1} H^\top + R)^{-1}, \\ \hat{x}_{k|k} &= \hat{x}_{k|k-1} + K_k (z_k - H \hat{x}_{k|k-1}), \\ P_{k|k} &= (I - K_k H) P_{k|k-1}. \end{aligned}$$

## 5. Filter Tuning and Implementation

### 5.1 Process Noise ( $Q$ )

Set  $Q$  to account for:

- Load torque variations on the motor shaft.
- Uncertainty in phase inductance/resistance at different temperatures.
- Rotor friction modeling errors.

### 5.2 Measurement Noise ( $R$ )

- **Hall Sensor Noise:** Incorporate the quantization and possible jitter in Hall transitions.
- **Current Sensor Noise:** Determine from specifications (e.g.,  $\pm 2\%$  measurement error).
- Adjust  $R$  values if the filter either over-trusts or under-trusts measurements.

### 5.3 Sampling Time

Because Hall sensors give updates at discrete transitions, the effective sampling rate for the filter can vary with motor speed. A separate high-frequency loop (e.g.,  $> 1$  kHz) can integrate and estimate speed. The KF can be updated either every fixed  $\Delta t$  or upon Hall transitions using event-based processing.

## 6. Practical Considerations

### 6.1 Limited Angle Resolution

Hall sensors offer coarse electrical angle increments (e.g., 6 or 12 transitions per electrical revolution). High mechanical speed can result in minimal resolution for advanced, high-precision servo tasks. The Kalman filter helps interpolate or smooth these coarse measurements.

### 6.2 Nonlinearities

A plain linear KF may still suffice if the operating range is near linear regions. For wider speed/flux range, consider using Extended Kalman Filter (EKF) or Unscented Kalman Filter (UKF) to handle back-EMF nonlinearities.

### 6.3 Real-Time Constraints

- Embedded microcontrollers must compute the Kalman update in  $\approx \mu\text{s}$ –ms timescales.
- Evaluate memory usage for state covariance matrices and matrix operations.

## 7. Example Flowchart

1. **Initialization:** Set  $\hat{x}_{0|0}$ ,  $P_{0|0}$ , guess  $Q$ ,  $R$ .
2. **Motor Voltage Input:** Apply  $u_k$  from higher-level controller (e.g., PID or FOC).
3. **KF Predict Step:** Compute  $\hat{x}_{k|k-1}$ ,  $P_{k|k-1}$ .
4. **Measurement Acquisition:** Read Hall sensor transitions and current sensor data (forming  $z_k$ ).
5. **KF Update Step:** Calculate  $K_k$ , correct state estimate  $\hat{x}_{k|k}$ .
6. **Feedback to Controller:** Use  $(\hat{\theta}, \hat{\omega}, \hat{i})^\top$  in real-time control loop.
7. **Repeat:** Continue predict–update cycles.

## 8. Conclusion

Designing a Kalman filter for a small-diameter Maxon EC BLDC motor with integrated Hall sensors involves:

- Formulating an appropriate state model (angle, speed, current).
- Accommodating coarse angle measurements from Hall signals.
- Tuning process and measurement noise covariances to balance model fidelity with sensor noise.
- Implementing the filter on an embedded platform with careful consideration of real-time constraints.

The resultant system provides more stable angle and speed estimates, better utilization of limited Hall sensor resolution, and robust performance under load variations. When properly integrated with a motor controller, the Kalman filter significantly enhances precision and responsiveness of the EC 8 mm motor drive.

## References

- Maxon Motor AG. “EC 8 mm DC Motor Specifications,” <https://www.maxongroup.com/>
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