

\* Review: A general angle modulation signal is given by  $\varphi(t) = A \cos(\theta_i(t))$

where  $A$  is the amplitude of the carrier, and  $\theta_i(t)$  is the instantaneous phase (in rad) of the signal that carries the message signal  $m(t)$ .

\* The instantaneous frequency  $f_i(t)$  Hz or  $\omega_i(t)$  rad/sec is given by  $\omega_i(t) = \frac{d}{dt} \theta_i(t) \Leftrightarrow \theta_i(t) = \int_0^t \omega_i(\tau) d\tau + \theta_0$

$\theta_0$  is the instantaneous phase at  $t=0$  (usually  $\theta_0=0$ )

$$f_i(t) = \frac{1}{2\pi} \omega_i(t) = \frac{1}{2\pi} \frac{d}{dt} \theta_i(t) \quad (\text{Hz})$$

### Angle Modulation

#### Phase Modulation (PM)

In phase modulation, the instantaneous phase  $\theta_i(t)$  is varied as a linear function of the message  $m(t)$ .

$$\theta_i(t) = \underline{\omega_c t} + \underline{k_p m(t)} + \theta_0$$

carrier freq.      phase constant

Thus,

$$\varphi_{PM}(t) = A \cos[\omega_c t + k_p m(t) + \theta_0]$$

\* Peak phase deviation  $\Delta\theta$ : the largest deviation of  $\theta_i(t)$  from  $(\omega_c t + \theta_0)$ . Hence,  $\Delta\theta = k_p \max\{|m(t)|\}$

We refer to the peak phase deviation as the modulation index,  $\beta_{PM} = \Delta\theta$

#### Angle Modulation

#### Frequency Modulation (FM)

In frequency modulation, the instantaneous frequency  $\omega_i(t) / f_i(t)$  is varied as a linear function of the message  $m(t)$ .

$$\omega_i(t) = \omega_c + k_\omega m(t)$$

or

$$f_i(t) = f_c + k_f m(t)$$

As a result,

$$\theta_i(t) = \omega_c t + k_\omega \int_0^t m(\tau) d\tau + \theta_0$$

Thus,

$$\varphi_{FM}(t) = A \cos[\omega_c t + k_\omega \int_0^t m(\tau) d\tau + \theta_0]$$

\* Peak frequency deviation  $\Delta\omega$ , the largest deviation of  $\omega_i(t)$  from  $\omega_c$ .  $\Delta\omega = k_\omega \max\{|m(t)|\}$

\* Since the instantaneous phase is:

$$\theta_i = \omega_c t + K_\omega \int_0^t m(\tau) d\tau + \theta_0$$

the peak phase deviation ( $\Delta\theta$ ) is given by:  $B: \text{message bw}$

$$\Delta\theta = K_\omega \max\left\{\left|\int_0^t m(\tau) d\tau\right|\right\}, \quad \beta_{FM} = \frac{\Delta\omega}{2\pi B} = \frac{\Delta f}{B}$$

For example, let us consider the single tone modulation  $m(t) = A_m \cos \omega_m t$

$$\varphi_{PM}(t) = A \cos [\omega_c t + K_p A_m \cos \omega_m t + \theta_0]$$

$$\Delta\theta = K_p A_m$$

$$\beta = K_p A_m$$

$$\varphi_{FM}(t) = A \cos [\omega_c t + K_w A_m \int_0^t \cos \omega_m \tau d\tau + \theta_0]$$

$$\Delta\omega = K_w A_m$$

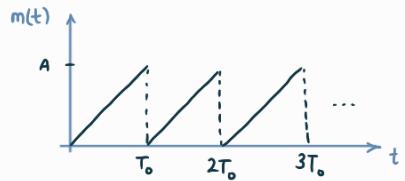
$$\Delta\theta = \max \left\{ \left| \frac{K_w A_m}{\omega_m} \sin(\omega_m t) \right| \right\} = \frac{K_w A_m}{\omega_m}$$

$$\beta = \frac{K_w A_m}{\omega_m} = \frac{\Delta\omega}{\omega_m} = \frac{\Delta f}{f_m}$$

**Ex.** Sketch the PM and FM waves produced by the sawtooth wave shown below.

SOL: The mathematical expression of  $m(t)$  is :

$$m(t) = \frac{A}{T_0} (t - nT_0), \quad nT_0 \leq t < (n+1)T_0 \quad \text{for } n=0,1,2,\dots$$



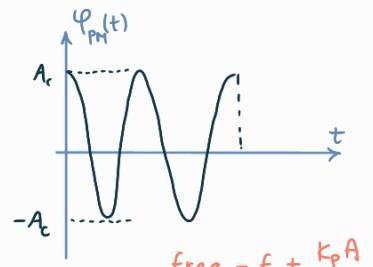
The PM signal is  $\varphi_{PM}(t) = A_c \cos (\omega_c t + K_p m(t))$ . In the interval  $0 \leq t < T_0$ ,  $m(t) = \frac{At}{T_0}$ . Hence, in this

$$\varphi_{PM}(t) = A_c \cos \left[ \omega_c t + K_p \frac{At}{T_0} \right] = A_c \cos \left[ \left( \omega_c + \frac{K_p A}{T_0} \right) t \right], \quad 0 \leq t < T$$

Thus, in  $0 \leq t < T$ ,  $\varphi_{PM}(t)$  is just a cosine signal with frequency  $\frac{1}{2\pi} \left( \omega_c + \frac{K_p A}{T_0} \right) = f_c + \frac{K_p A}{2\pi T_0}$  and  $\theta_0 = 0$ .

In the next interval,  $T_0 \leq t < 2T_0$ ,  $m(t) = \frac{At}{T_0} - A$ . Thus,

$$\varphi_{PM}(t) = A_c \cos \left[ \omega_c t + K_p \left( \frac{At}{T_0} - A \right) \right] = A_c \cos \left[ \left( \omega_c + \frac{K_p A}{T_0} \right) t - AK_p \right], \quad T_0 \leq t < 2T_0$$

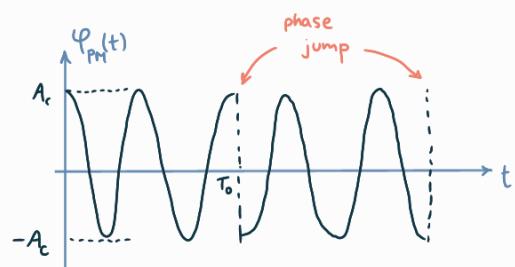


Thus,  $\varphi_{PM}(t)$  is still a cosine signal with frequency  $f_c + \frac{K_p A}{2\pi T_0}$ , but at  $t=T_0$ , there

is a phase shift (jump) of  $(AK_p)$  rad. Similarly,  $\varphi_{PM}(t)$  will still be a cosine signal but at  $t=2T_0, 3T_0, \dots$  the

phase will be changed by  $-AK_p$  rad. In this case the phase of the signal is

discontinuous as the message signal  $m(t)$  is discontinuous.



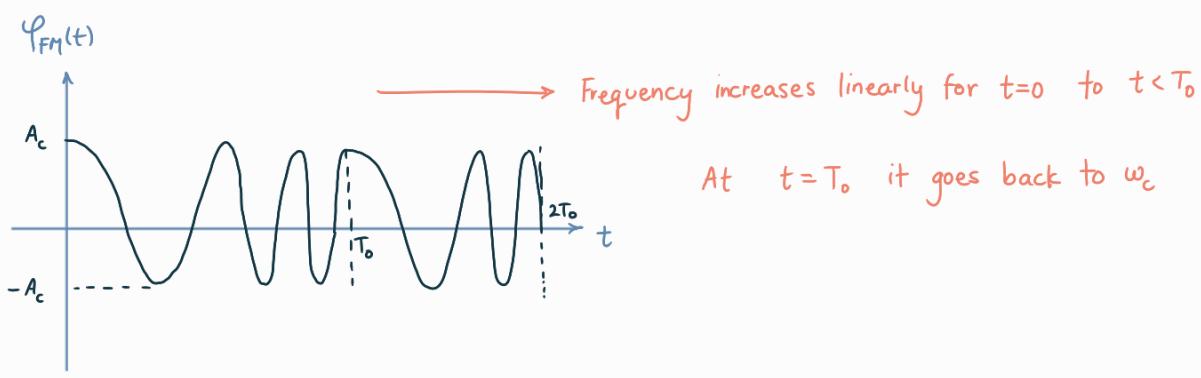
In the FM signal, the phase is proportional to the integral of  $m(t)$ ,

Here we illustrate with  $AK_p = \pi$  rad

and hence is continuous. In FM, the instantaneous frequency is  $\omega_i = \omega_c + K_w m(t)$

Hence,  $\omega_i$  will increase from  $\omega_c$  to  $\omega_c + K_w A$  between  $t=0$  and  $t < T_0$ . Then at  $t=T_0$ ,  $\omega_i$  goes back down to  $\omega_c$ .

and starts increasing again. An illustrative example is given below:



**Ex.** Find the modulation index for each of the following cases. Assume that  $K_p = 1$  and  $\theta_0 = 0$ .

(a) PM,  $m(t) = a(t)$

(b) PM,  $m(t) = b(t)$

SOL :

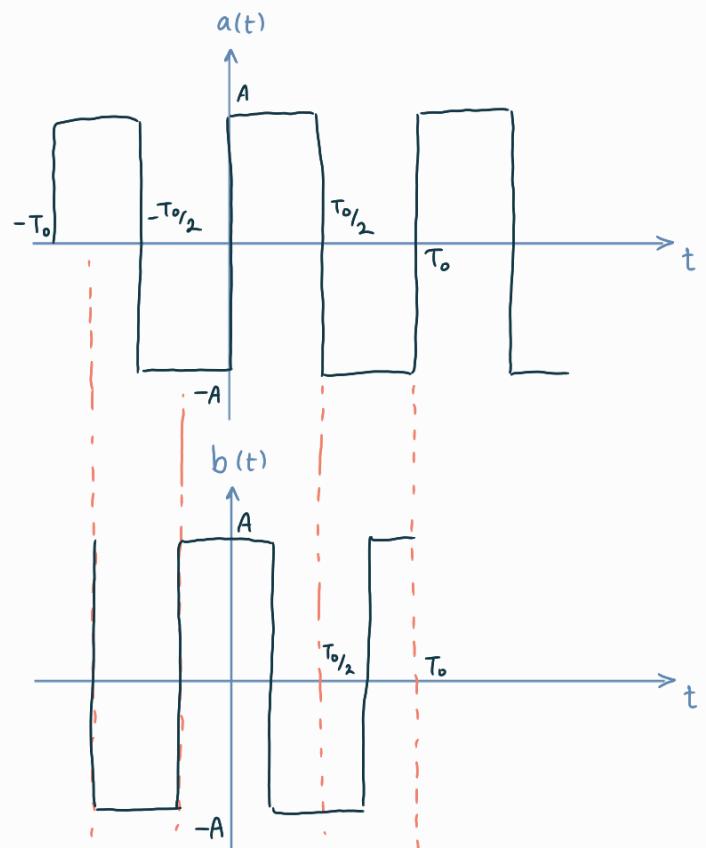
(a) In PM, the modulation index (peak phase

deviation)  $\beta$  is given by  $\beta = K_p \cdot \max \{ |m(t)| \}$ .

Note that  $\max \{ |m(t)| \} = A$  for  $a(t)$ .

Hence,  $\beta = K_p \cdot A = A$

(b) Note that  $b(t)$  is just a shifted (time)



version of  $a(t)$ , and it does not affect the maximum amplitude. Hence,  $\beta = A$ .

**Ex.** Consider the following modulated signal:  $\varphi(t) = 5 \cos [\omega_c t + \cos \omega_m t]$  for some  $\omega_c, \omega_m$ .

(a) If it is a PM signal with  $K_p = 2$ , then what is the message  $m(t)$ ?

(b) If it is an FM signal with  $K_\omega = 0.2$ , then what is  $m(t)$ ?

SOL : (a) Since  $\varphi_{PM}(t) = 5 \cos [\omega_c t + 2m(t) + \theta_0] = 5 \cos (\omega_c t + \cos \omega_m t)$ , we find  $\theta_0 = 0$  and  $m(t) = \frac{1}{2} \cos \omega_m t$

(b) Since  $\varphi_{FM}(t) = 5 \cos [\omega_c t + 0.2 \int_0^t m(\tau) d\tau + \theta_0] = 5 \cos (\omega_c t + \cos \omega_m t)$ , we have  $0.2 \int_0^t m(\tau) d\tau + \theta_0 = \cos (\omega_m t)$

$$\frac{d}{dt} \Rightarrow 0.2 m(t) = -\omega_m \sin(\omega_m t) \Rightarrow m(t) = -5 \omega_m \sin(\omega_m t).$$

Also, using this  $m(t)$ , one can find that  $\theta_0 = 1$  rad.

### ANGLE MODULATION REVIEW

Recall that an FM signal is given by:

$$\varphi(t) = A \cos \left[ \omega_c t + k_\omega \int_0^t m(\tau) d\tau \right]$$

Important parameters

where,  $A$  = carrier amplitude,  $\omega_c$  = carrier frequency (rad/sec),  $k_\omega$  = frequency sensitivity,  $m(\tau)$  = message signal.

Peak phase deviation / modulation index:

$$\beta = k_\omega \cdot \max \left| \int_0^t m(\tau) d\tau \right|$$

NBFM :  $\beta \ll 1$

WBFM

(sometimes we take  $\beta < 0.3$  as a threshold)

Roughly  $\beta > 0.3$

The FM signal can be approximated as:

$$\varphi_{NB}(t) = A \cos \omega_c t - A k_\omega \int_0^t m(\tau) d\tau \cdot \sin \omega_c t$$

By inspection we can notice that  $\varphi_{NB}(t)$  is similar to

DSB-LC where a carrier  $A \cos \omega_c t$  is added to/ subtracted

from function  $m(t)$  multiplied by a carrier  $\sin(\omega_c t)$ .

Based on this, BW of  $\varphi_{NB}(t)$  is  $2 \times \text{BW}(m(t))$

Ex.  $m(t) = a \cos \omega_m t$ ,

$$\varphi_{NB}(t) = A \cos \omega_c t - \frac{A \cdot k_\omega \cdot a}{\omega_m} \sin \omega_m t \cdot \sin \omega_c t,$$

$$\beta = k_\omega \cdot \max \left| \frac{a}{\omega_m} \sin \omega_m t \right| = \frac{a \cdot k_\omega}{\omega_m}$$

We do not have a simple approximation of  $\varphi(t)$ .

Also, analyzing a general message signal  $m(t)$  becomes

mathematically intractable. We study WBFM for

$m(t) = a \cos \omega_m t$ , then WBFM can be expressed in its

"Bessel form":

$$\varphi_{WB}(t) = A \sum_{n=-\infty}^{\infty} J_n(\beta) \cos \left[ (\omega_c + n \omega_m) t \right]$$

Here,  $J_n(\beta)$  is the  $n^{\text{th}}$  order Bessel function of the first

kind. We do not need to study it in details. This is sufficient:

(a)  $J_n(\beta)$  is real.

(d)  $\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$

(b)  $J_n(\beta) = (-1)^n J_{-n}(\beta)$

(c) For  $\beta \ll 1$ ,  $J_0(\beta) = +1$ ,  $J_1(\beta) = \beta/2$ ,  $J_n(\beta) = 0$   $n \geq 2$

Bandwidth: due to the similarity between the  $\varphi_{NB}$  &  $\varphi_{DSB}$ ,

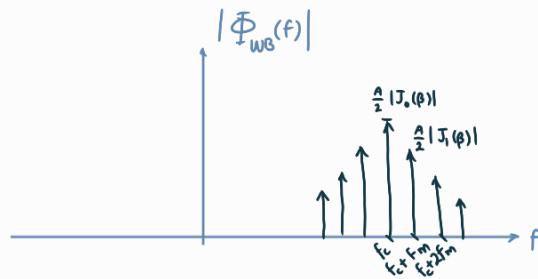
the bandwidth of  $\varphi_{NB} = 2 \times$  bandwidth of the message signal.

Spectrum of WBFM:

$$\Phi_{WB}(f) = \mathcal{F} \left\{ A \sum_{n=-\infty}^{\infty} J_n(\beta) \cdot \cos[(\omega_c + n\omega_m)t] \right\}$$

$$= A \sum_{n=-\infty}^{\infty} J_n(\beta) \mathcal{F} \left\{ \cos[(\omega_c + n\omega_m)t] \right\}$$

$$= \frac{A}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [ \delta(\omega - \omega_c - n\omega_m) + \delta(\omega + \omega_c + n\omega_m) ]$$



$$@ f_c : \frac{A}{2} |J_0(\beta)| \quad @ f_c \pm f_m : \frac{A}{2} |J_1(\beta)|$$

Bandwidth of WBFM:

(a) The 1% Rule: Among all the delta functions in  $|\Phi_{WB}(\omega)|$ , keep the ones that have a magnitude  $\geq 0.01$ ,

and ignore the rest. Specially choose  $n_0$  such that  $|J_n(\beta)| \geq 0.01$  for  $n \leq n_0$  and  $|J_n(\beta)| < 0.01$  for  $n > n_0$ . Then the bandwidth is:  $BW = 2n_0\omega_m$  rad/sec

(b) Carson's Rule:  $BW = 2\omega_m(1+\beta)$  rad/sec OR  $BW = 2f_m(1+\beta)$  This works well for large  $\beta$ .

**Ex.** A carrier  $c(t) = 100 \cos \omega_c t$  is frequency modulated by the message  $m(t) = 100 \cos(\omega_m t)$  where  $f_c = 100 \text{ KHz}$ ,  $f_m = 1 \text{ KHz}$ .

The frequency sensitivity  $K_\omega = 32\pi$ .

(a) Using the 1% rule, find the approximate BW of  $\varphi(t)$ . Which frequency components fall within this BW?

(b) Sketch the magnitude spectrum of  $\varphi(t)$  [only positive frequencies]. Include only the frequency components that are centered within the approximation.

(c) Find the BW of  $\varphi(t)$  using Carson's rule. Which frequency components fall within this BW? How do they compare to those in part (a)?

SOL: (a) According to the 1% rule, we need to find  $n_0$  such that  $|J_n(\beta)| \geq 0.01$  for  $|n| \leq n_0$  and  $|J_n(\beta)| < 0.01$

for  $|n| > n_0$ . First we find  $\beta$ .

$$\beta = \frac{\Delta\omega}{\omega_m} = \frac{a \cdot k\omega}{\omega_m} = \frac{32\pi \times 100}{2\pi \times 10^3} = 1.6$$

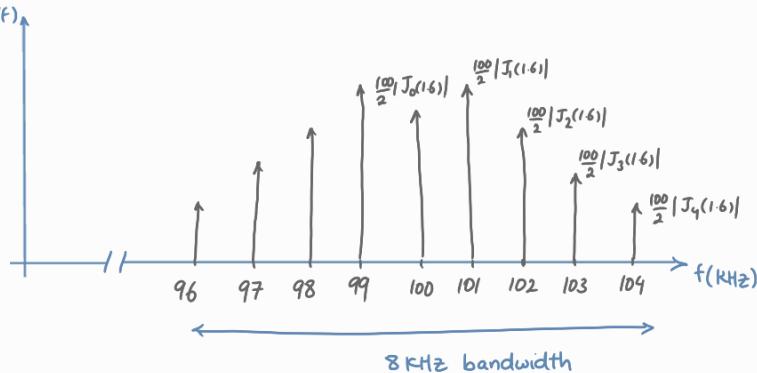
Now, let's look at the Bessel function table for  $\beta = 1.6$ :

$\beta$	$J_0(\beta)$	$J_1(\beta)$	$J_2(\beta)$	$J_3(\beta)$	$J_4(\beta)$	$J_5(\beta)$
1.6	0.455	0.570	0.257	0.073	0.015	0.002
Frequency	$f_c$	$f_c \pm f_m$	$f_c \pm 2f_m$	$f_c \pm 3f_m$	$f_c \pm 4f_m$	$f_c \pm 5f_m$

We note that  $n_0 = 4$ , since  $J_4(\beta) \geq 0.01$  but  $J_5(\beta) < 0.01$ . Thus the BW is  $2 \times n_0 \times \omega_m = 2\pi \times 8 \text{ rad/sec}$  or  $8 \text{ kHz}$ .

The frequency components contained within this bandwidth:  $f_c$ ,  $f_c \pm f_m$ ,  $f_c \pm 2f_m$ ,  $f_c \pm 3f_m$  and  $f_c \pm 4f_m$ .

(b)  $\Phi(f)$



(c) Using Carson's rule,  $BW = 2f_m(1+\beta) = 2(1+1.6) \text{ kHz} = 5.2 \text{ kHz}$ . The largest  $n_0$  that satisfies  $2n_0 f_m \leq 5.2 \text{ kHz}$  is  $n_0 = 2$ .

Hence, the frequency components that fall within this bandwidth are  $f_c$ ,  $f_c \pm f_m$  and  $f_c \pm 2f_m$ .

Thus Carson's rule includes only 5 frequency components whereas the 1% rule includes 9.

Ex.

A certain sinusoid of frequency  $f_m$  (Hz) is used as the message in a DSB-LC and an FM signal. When modulated the peak

frequency deviation of the FM signal is set to 3 times the bandwidth of the AM signal. Also, the magnitudes of the sidebands spaced

at  $\pm f_m$  (Hz) from the carrier are equal in both systems. Determine the modulation index of the FM and AM systems.

FM signal:  $\varphi_f(t) = A_1 \sum J_n(\beta) \cos[(\omega_c + n\omega_m)t]$

Assume that the AM signal has form:  $\varphi_A(t) = (A_2 + A_m \cos(\omega_m t)) \cos \omega_c t$

SOL : We know that  $\Delta f$  is 3 times the bandwidth of the AM system:

$$\Delta f = 3 \cdot \text{BW(AM)} , \text{ BW of AM} = 2f_m \Rightarrow \Delta f = 3 \times 2f_m = 6f_m , \text{ by definition } \beta = \frac{\Delta f}{f_m} = \frac{6f_m}{f_m} = 6 \Rightarrow \boxed{\beta = 6}$$

Next, we know that the power in the two systems are equal. The power of the FM signal is  $A_1^2/2$ .

Calculating the power of AM :  $\varphi_{\text{AM}}(t) = [A_2 + A_M \cos(\omega_m t)] \cos(\omega_c t) = A_2 \cos(\omega_c t) + \frac{A_M}{2} \cos(\omega_c - \omega_m)t + \frac{A_M}{2} \cos(\omega_c + \omega_m)t$

$$\text{Power } \varphi_{\text{AM}}(t) = \frac{A_2^2}{2} + \frac{A_M^2}{8} + \frac{A_M^2}{8} = \frac{A_2^2}{2} + \frac{A_M^2}{4} \Rightarrow A_1^2 = A_2^2 + \frac{A_M^2}{2} \quad (1)$$

Now the modulation index of the AM signal is  $\mu = \frac{A_M}{A_2}$ . Hence from (1),  $A_1^2 = A_2^2 (1 + \mu^2/2)$

\* We are also given that the magnitude of sidebands at frequencies spaced  $\pm f_m$  from the carrier frequency are equal in both systems.

$$\varphi_{\text{AM}}(t) = A_2 \cos(\omega_c t) + \frac{\mu A_2}{2} \cos[(\omega_c - \omega_m)t] + \frac{\mu A_2}{2} \cos[(\omega_c + \omega_m)t]$$

Thus, the magnitude in question is at frequency  $\pm f_m$ .  $\frac{\mu A_2}{4}$

The magnitude of the frequency components located at  $f_c \pm f_m$  is:  $\frac{A_1}{2} |J_1(\beta)| = \frac{A_1}{2} |J_1(6)|$ .

$$\text{As a result, } \frac{A_1}{2} |J_1(6)| = \frac{\mu A_2}{4} \Rightarrow A_1^2 J_1^2(6) = \frac{\mu^2 A_2^2}{4} \quad (2)$$

Thus from (1) and (2)  $\mu \approx 0.6 A_M$

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