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**Problem 4.1**

1) Since  $\mathcal{F}[\text{sinc}(400t)] = \frac{1}{400}\Pi(\frac{f}{400})$ , the bandwidth of the message signal is  $W = 200$  and the resulting modulation index

$$\beta_f = \frac{k_f \max[|m(t)|]}{W} = \frac{k_f 10}{W} = 6 \Rightarrow k_f = 120$$

Hence, the modulated signal is

$$\begin{aligned} u(t) &= A \cos(2\pi f_c t + 2\pi k_f \int_{-\infty}^t m(\tau) d\tau) \\ &= 100 \cos(2\pi f_c t + 2\pi 1200 \int_{-\infty}^t \text{sinc}(400\tau) d\tau) \end{aligned}$$

2) The maximum frequency deviation of the modulated signal is

$$\Delta f_{\max} = \beta_f W = 6 \times 200 = 1200$$

3) Since the modulated signal is essentially a sinusoidal signal with amplitude  $A = 100$ , we have

$$P = \frac{A^2}{2} = 5000$$

4) Using Carson's rule, the effective bandwidth of the modulated signal can be approximated by

$$B_c = 2(\beta_f + 1)W = 2(6 + 1)200 = 2800 \text{ Hz}$$

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**Problem 4.2**

1) The maximum phase deviation of the PM signal is

$$\Delta\phi_{\max} = k_p \max[|m(t)|] = k_p$$

The phase of the FM modulated signal is

$$\begin{aligned} \phi(t) &= 2\pi k_f \int_{-\infty}^t m(\tau) d\tau = 2\pi k_f \int_0^t m(\tau) d\tau \\ &= \begin{cases} 2\pi k_f \int_0^t \tau d\tau = \pi k_f t^2 & 0 \leq t < 1 \\ \pi k_f + 2\pi k_f \int_1^t d\tau = \pi k_f + 2\pi k_f (t - 1) & 1 \leq t < 2 \\ \pi k_f + 2\pi k_f - 2\pi k_f \int_2^t d\tau = 3\pi k_f - 2\pi k_f (t - 2) & 2 \leq t < 3 \\ \pi k_f & 3 \leq t \end{cases} \end{aligned}$$

The maximum value of  $\phi(t)$  is achieved for  $t = 2$  and is equal to  $3\pi k_f$ . Thus, the desired relation between  $k_p$  and  $k_f$  is

$$k_p = 3\pi k_f$$

2) The instantaneous frequency for the PM modulated signal is

$$f_i(t) = f_c + \frac{1}{2\pi} \frac{d}{dt} \phi(t) = f_c + \frac{1}{2\pi} k_p \frac{d}{dt} m(t)$$

For the  $m(t)$  given in Fig. P-4.2, the maximum value of  $\frac{d}{dt} m(t)$  is achieved for  $t$  in  $[0, 1]$  and it is equal to one. Hence,

$$\max(f_i(t)) = f_c + \frac{1}{2\pi}$$

For the FM signal  $f_i(t) = f_c + k_f m(t)$ . Thus, the maximum instantaneous frequency is

$$\max(f_i(t)) = f_c + k_f = f_c + 1$$


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### Problem 4.3

For an angle modulated signal we have  $x(t) = A_c \cos(2\pi f_c t + \phi(t))$ , therefore The lowpass equivalent of the signal is  $x_l(t) = A_c e^{j\phi(t)}$  with Envelope  $A_c$  and phase  $\pi(t)$  and in phase an quadrature components  $A_c \cos(\phi(t))$  and  $A_c \sin(\phi(t))$ , respectively. Hence we have the following

PM $\begin{cases} A_c & \text{envelope} \\ k_p m(t) & \text{phase} \\ A_c \cos(k_p m(t)) & \text{in-phase comp.} \\ A_c \sin(k_p m(t)) & \text{quadrature comp.} \end{cases}$	FM $\begin{cases} A_c & \text{envelope} \\ 2\pi k_f \int_{-\infty}^t m(\tau) d\tau & \text{phase} \\ A_c \cos(2\pi k_f \int_{-\infty}^t m(\tau) d\tau) & \text{in-phase comp.} \\ A_c \sin(2\pi k_f \int_{-\infty}^t m(\tau) d\tau) & \text{quadrature comp.} \end{cases}$
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### Problem 4.4

1) Since an angle modulated signal is essentially a sinusoidal signal with constant amplitude, we have

$$P = \frac{A_c^2}{2} \Rightarrow P = \frac{100^2}{2} = 5000$$

The same result is obtained if we use the expansion

$$u(t) = \sum_{n=-\infty}^{\infty} A_c J_n(\beta) \cos(2\pi(f_c + n f_m)t)$$

along with the identity

$$J_0^2(\beta) + 2 \sum_{n=1}^{\infty} J_n^2(\beta) = 1$$

2) The maximum phase deviation is

$$\Delta\phi_{\max} = \max |4 \sin(2000\pi t)| = 4$$

3) The instantaneous frequency is

$$\begin{aligned} f_i &= f_c + \frac{1}{2\pi} \frac{d}{dt} \phi(t) \\ &= f_c + \frac{4}{2\pi} \cos(2000\pi t) 2000\pi = f_c + 4000 \cos(2000\pi t) \end{aligned}$$

Hence, the maximum frequency deviation is

$$\Delta f_{\max} = \max |f_i - f_c| = 4000$$

4) The angle modulated signal can be interpreted both as a PM and an FM signal. It is a PM signal with phase deviation constant  $k_p = 4$  and message signal  $m(t) = \sin(2000\pi t)$  and it is an FM signal with frequency deviation constant  $k_f = 4000$  and message signal  $m(t) = \cos(2000\pi t)$ .

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## Problem 4.6

1) If the output of the narrowband FM modulator is,

$$u(t) = A \cos(2\pi f_0 t + \phi(t))$$

then the output of the upper frequency multiplier ( $\times n_1$ ) is

$$u_1(t) = A \cos(2\pi n_1 f_0 t + n_1 \phi(t))$$

After mixing with the output of the second frequency multiplier  $u_2(t) = A \cos(2\pi n_2 f_0 t)$  we obtain the signal

$$\begin{aligned} y(t) &= A^2 \cos(2\pi n_1 f_0 t + n_1 \phi(t)) \cos(2\pi n_2 f_0 t) \\ &= \frac{A^2}{2} (\cos(2\pi(n_1 + n_2)f_0 t + n_1 \phi(t)) + \cos(2\pi(n_1 - n_2)f_0 t + n_1 \phi(t))) \end{aligned}$$

The bandwidth of the signal is  $W = 15$  KHz, so the maximum frequency deviation is  $\Delta f = \beta_f W = 0.1 \times 15 = 1.5$  KHz. In order to achieve a frequency deviation of  $f = 75$  KHz at the output of the wideband modulator, the frequency multiplier  $n_1$  should be equal to

$$n_1 = \frac{f}{\Delta f} = \frac{75}{1.5} = 50$$

Using an up-converter the frequency modulated signal is given by

$$y(t) = \frac{A^2}{2} \cos(2\pi(n_1 + n_2)f_0 t + n_1 \phi(t))$$

Since the carrier frequency  $f_c = (n_1 + n_2)f_0$  is 104 MHz,  $n_2$  should be such that

$$(n_1 + n_2)100 = 104 \times 10^3 \Rightarrow n_1 + n_2 = 1040 \text{ or } n_2 = 990$$

2) The maximum allowable drift ( $d_f$ ) of the 100 kHz oscillator should be such that

$$(n_1 + n_2)d_f = 2 \Rightarrow d_f = \frac{2}{1040} = .0019 \text{ Hz}$$

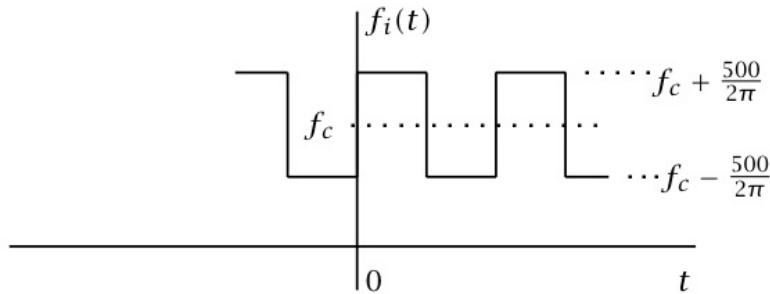
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**Problem 4.8**

1) The instantaneous frequency is given by

$$f_i(t) = f_c + \frac{1}{2\pi} \frac{d}{dt} \phi(t) = f_c + \frac{1}{2\pi} 100m(t)$$

A plot of  $f_i(t)$  is given in the next figure



2) The peak frequency deviation is given by

$$\Delta f_{\max} = k_f \max[|m(t)|] = \frac{100}{2\pi} 5 = \frac{250}{\pi}$$

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**Problem 4.9**

1) The modulation index is

$$\beta = \frac{k_f \max[|m(t)|]}{f_m} = \frac{\Delta f_{\max}}{f_m} = \frac{20 \times 10^3}{10^4} = 2$$

The modulated signal  $u(t)$  has the form

$$\begin{aligned} u(t) &= \sum_{n=-\infty}^{\infty} A_c J_n(\beta) \cos(2\pi(f_c + n f_m)t + \phi_n) \\ &= \sum_{n=-\infty}^{\infty} 100 J_n(2) \cos(2\pi(10^8 + n 10^4)t + \phi_n) \end{aligned}$$

The power of the unmodulated carrier signal is  $P = \frac{100^2}{2} = 5000$ . The power in the frequency component  $f = f_c + k10^4$  is

$$P_{f_c+kf_m} = \frac{100^2 J_k^2(2)}{2}$$

The next table shows the values of  $J_k(2)$ , the frequency  $f_c + kf_m$ , the amplitude  $100J_k(2)$  and the power  $P_{f_c+kf_m}$  for various values of  $k$ .

Index $k$	$J_k(2)$	Frequency Hz	Amplitude $100J_k(2)$	Power $P_{f_c+kf_m}$
0	.2239	$10^8$	22.39	250.63
1	.5767	$10^8 + 10^4$	57.67	1663.1
2	.3528	$10^8 + 2 \times 10^4$	35.28	622.46
3	.1289	$10^8 + 3 \times 10^4$	12.89	83.13
4	.0340	$10^8 + 4 \times 10^4$	3.40	5.7785

As it is observed from the table the signal components that have a power level greater than 500 (= 10% of the power of the unmodulated signal) are those with frequencies  $10^8 + 10^4$  and  $10^8 + 2 \times 10^4$ . Since  $J_n^2(\beta) = J_{-n}^2(\beta)$  it is conceivable that the signal components with frequency  $10^8 - 10^4$  and  $10^8 - 2 \times 10^4$  will satisfy the condition of minimum power level. Hence, there are four signal components that have a power of at least 10% of the power of the unmodulated signal. The components with frequencies  $10^8 + 10^4$ ,  $10^8 - 10^4$  have an amplitude equal to 57.67, whereas the signal components with frequencies  $10^8 + 2 \times 10^4$ ,  $10^8 - 2 \times 10^4$  have an amplitude equal to 35.28.

2) Using Carson's rule, the approximate bandwidth of the FM signal is

$$B_c = 2(\beta + 1)f_m = 2(2 + 1)10^4 = 6 \times 10^4 \text{ Hz}$$


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### Problem 4.11

1) The PM modulated signal is

$$\begin{aligned} u(t) &= 100 \cos(2\pi f_c t + \frac{\pi}{2} \cos(2\pi 1000t)) \\ &= \sum_{n=-\infty}^{\infty} 100 J_n \left(\frac{\pi}{2}\right) \cos(2\pi(10^8 + n10^3)t) \end{aligned}$$

The next table tabulates  $J_n(\beta)$  for  $\beta = \frac{\pi}{2}$  and  $n = 0, \dots, 4$ .

$n$	0	1	2	3	4
$J_n(\beta)$	.4720	.5668	.2497	.0690	.0140

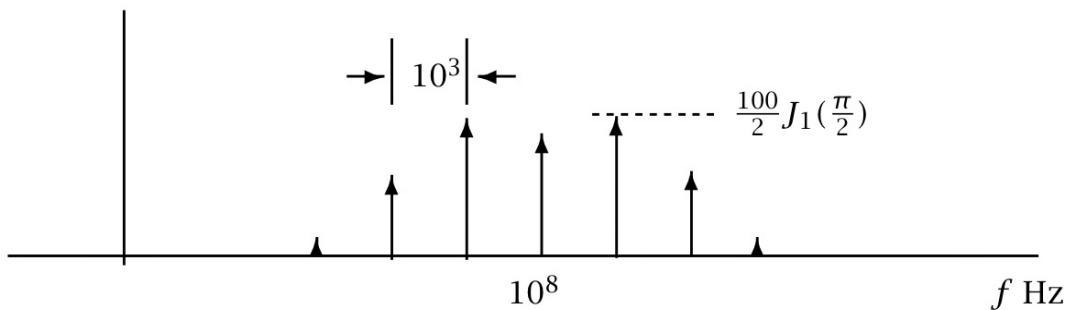
The total power of the modulated signal is  $P_{\text{tot}} = \frac{100^2}{2} = 5000$ . To find the effective bandwidth of the signal we calculate the index  $k$  such that

$$\sum_{n=-k}^k \frac{100^2}{2} J_n^2 \left(\frac{\pi}{2}\right) \geq 0.99 \times 5000 \Rightarrow \sum_{n=-k}^k J_n^2 \left(\frac{\pi}{2}\right) \geq 0.99$$

By trial end error we find that the smallest index  $k$  is 2. Hence the effective bandwidth is

$$B_{\text{eff}} = 4 \times 10^3 = 4000$$

In the next figure we sketch the magnitude spectrum for the positive frequencies.



2) Using Carson's rule, the approximate bandwidth of the PM signal is

$$B_{\text{PM}} = 2(\beta_p + 1)f_m = 2\left(\frac{\pi}{2} + 1\right)1000 = 5141.6$$

As it is observed, Carson's rule overestimates the effective bandwidth allowing in this way some margin for the missing harmonics.

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**Problem 4.13**

1) If the signal  $m(t) = m_1(t) + m_2(t)$  DSB modulates the carrier  $A_c \cos(2\pi f_c t)$  the result is the signal

$$\begin{aligned} u(t) &= A_c m(t) \cos(2\pi f_c t) \\ &= A_c(m_1(t) + m_2(t)) \cos(2\pi f_c t) \\ &= A_c m_1(t) \cos(2\pi f_c t) + A_c m_2(t) \cos(2\pi f_c t) \\ &= u_1(t) + u_2(t) \end{aligned}$$

where  $u_1(t)$  and  $u_2(t)$  are the DSB modulated signals corresponding to the message signals  $m_1(t)$  and  $m_2(t)$ . Hence, AM modulation satisfies the superposition principle.

2) If  $m(t)$  frequency modulates a carrier  $A_c \cos(2\pi f_c t)$  the result is

$$\begin{aligned} u(t) &= A_c \cos(2\pi f_c t + 2\pi k_f \int_{-\infty}^{\infty} (m_1(\tau) + m_2(\tau)) d\tau) \\ &\neq A_c \cos(2\pi f_c t + 2\pi k_f \int_{-\infty}^{\infty} m_1(\tau) d\tau) \\ &\quad + A_c \cos(2\pi f_c t + 2\pi k_f \int_{-\infty}^{\infty} m_2(\tau) d\tau) \\ &= u_1(t) + u_2(t) \end{aligned}$$

where the inequality follows from the nonlinearity of the cosine function. Hence, angle modulation is not a linear modulation method.

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**Problem 4.17**

Using Carson's rule we obtain

$$B_c = 2(\beta + 1)W = 2\left(\frac{k_f \max[|m(t)|]}{W} + 1\right)W = \begin{cases} 20020 & k_f = 10 \\ 20200 & k_f = 100 \\ 22000 & k_f = 1000 \end{cases}$$

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