

Optimized MPPT implementation for Dye-sensitized Solar cells

Maximum Power Point Tracking for DCSs

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ABSTRACT

(Filler text not actual text) During recent years, for photovoltaic (PV) systems, many maximum power point tracking (MPPT) algorithms have been proposed and developed to maximize the produced energy. Regarding the design manner, these methods vary in many aspects as: implementation simplicity, power or energy efficiency, convergence speed, sensors required, cost effectiveness. Some comparative studies, based on widely-adopted MPPT algorithms, presented in the literature give results obtained either from simulation tool, which provide simultaneous operating systems, or using real PV test bench under solar simulator in order to reproduce the same operating solar conditions. This work presents an experimental comparison, under real solar irradiation, of four most used MPPT methods for PV power systems: Perturb and Observe (P&O) and Incremental Conductance, as tracking step constant, and improved P&O and Fuzzy Logic based MPPT, as variable tracking step. Using four identical PV, under strictly the same set of technical and meteorological conditions, an experimental comparison of these four algorithms is done. Following two criteria, energy efficiency and cost effectiveness, this comparison shows the advantage of use of a MPPT with a variable tracking step. The extracted energies by all four methods are almost identical with a slight advantage for improved P&O algorithm.

Keywords: DSC, MPPT, PnO.

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ACRONYMS

DSCs	Dye-Sensitized Solar Cells.....	1
MPPT	Maximum power Point Tracking	1
CdTe	cadmium telluride	1
CIGS	copper-indium-gallium selenide.....	1
CIS	copper-indium sulphide.....	1
a-Si	amorphous silicon	1
FTO	fluorine-doped tin oxide	9
WE	Working Electrode	9
CE	Counter Electrode.....	9
HOMO	Highest Occupied Molecular Orbital	10
LUMO	Lowest Unoccupied Molecular Orbital	10
MPP	Maximum Power Point	3
PnO	Perturb and Observe.....	6
FOCV	fractional open circuit voltage.....	6
ICM	Incremental Conductance Method	6
F.F	Fill Factor.....	12
DSP	Digital Signal Processor.....	38
VAL	voltage approximation line.....	38
LED	Light Emitting Diode	25

1

INTRODUCTION

This chapter gives a basic introduction to Dye-Sensitized Solar Cells ([DSCs](#)) and Maximum power Point Tracking ([MPPT](#)). It also defines the scope, Goals, Objective and the Research Methodology for the thesis.

1.1

BACKGROUND

Our ever increasing reliance on electrical and electronic equipment intensified our search for new sources of energy. Dwindling fossil-fuel reserves are not something we can rely on in the long-term. Alternate energy sources must be efficient, cost-effective and ecologically friendly. The Harnessing of solar energy becomes a very attractive proposition. A moderately efficient solar cell array (8%-10% efficiency) Covering a small portion of the earth's surface would be able to provide an enormous amount of electric power and thus reduce greenhouse-gas emissions [[kalyanasundaram2010dye](#)]. However, the current high cost of solar panels made from traditional inorganic semiconductors imposes a restriction on their mass usage. **picture about the losses Solar energy intercepting Earth [[toivola2010dye](#)]**

1.1.1

Dye-Sensitized Solar Cells(DSCs)

Photovoltaic devices are based on the concept of charge separation at an interface of two materials of different conduction mechanism. To date this field has been dominated by solid-state junction devices, usually made of silicon, and profiting from the experience and material availability resulting from the semiconductor industry. The dominance of the photovoltaic field by inorganic solid-state junction devices is now being challenged by the emergence of a third generation of cells, based, e.g. on nano-crystalline oxide and conducting polymers films [[gratzel2004conversion](#)]. Crystalline silicon being the first; and thin film technologies such as cadmium telluride ([CdTe](#)), copper-indium-gallium selenide ([CIGS](#)), copper-indium sulphide ([CIS](#)) and amorphous silicon ([a-Si](#)) being examples of the second generation [[toivola2010dye](#)].

Solar energy can be converted into electricity by a variety of technologies that can also be divided into four classes: Concentrator systems, wafer-based crystalline silicon, thin-film technologies, and emerging technologies [[wenger2010strategies](#)].

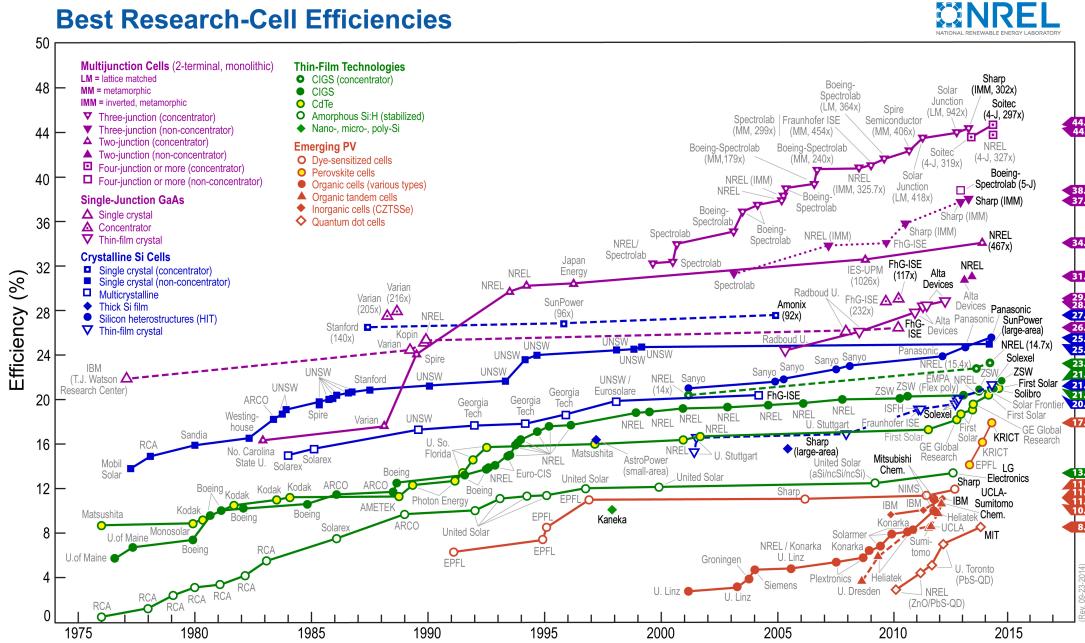


Figure 1.1: Research Cell Efficiency Records [nrel_Research_Cell]

Dye-sensitized solar cells(DSCs) are the most promising of the third and latest generation of solar cells. Under development for the last 20 years, this technology is ready for large scale commercialization to provide robust, efficient, and affordable solar energy to the masses. unlike previous generation cells, DSCs is a Photo-electrochemical device whose principal of operation is similar to Photosynthesis seen in plants.

1.1.2 Advantages of DSCs

The *** of solar cells is slow **.A major contributing factor for this is the predominant type of solar cells used today -ones made from silicon, which are quite expensive and are complex to manufacture. This has lead to intensive research in to alternative solar cells in the past decade. DSCs have many advantages over their 1st and 2nd generation counterparts. They offer transparency, low cost, and high power conversion efficiencies under cloudy and artificial light conditions.DSCs work even in low-light conditions such as non-direct sunlight and cloudy skies.They are easy and economical to manufacture,with the major constituent materials available in abundance in most counties. **This availability of Raw material also enables us to scale the manufacturing to Tera-Watts levels relatively simple.Since raw-materials are non-toxic and there are no noxious emissions during manufacturing-Sustainable**

		Performance			
		World record efficiency	Module efficiency	Sensitivity to light angle and condition	Sensitivity to temperature fluctuations
1 st generation PV	Mono-crystalline silicon	30.0%	19.5%	High	- 0.53% / °C
	Multi-crystalline silicon	18.0%	13.0-15.0%	High	- 0.44% / °C
2 nd generation PV	Cadmium telluride	17.3%	13.5%	Medium	- 0.27% / °C
	CIGS	20.3%	15.1%	Medium	- 0.42% / °C
3 rd gen.	Amorphous silicon	13.0%	5.0-7.0%	Medium	- 0.20% / °C
	DSCs	14.14% (15%)	10.3%	Low	+ 0.1% / °C

Figure 1.2: Three generations of cells – Performance

**Add more details about Advantage of DSC over conventional cells **

1.2 MAXIMUM POWER POINT TRACKING(MPPT)

A photovoltaic (PV) array that functions under uniform radiation and temperature conditions presents an I-V and P-V characteristic as the one shown in Figure 1.3 and Figure 1.5, respectively. As can be observed, there is a single point, called Maximum Power Point (MPP), where the array provides the maximum power possible for these environmental conditions (radiation and temperature), and so functions with the maximum performance. When a load is connected directly to a PV array (direct coupling), the operation point is defined by the intersection of its I-V characteristics, as shown in Figure 1.3. In general, this operation point does not coincide with the MPP. Thus, in direct coupling systems, the array must be over-dimensioned to guarantee the power demand of the load. Obviously, this implies a more expensive system. To solve this problem, a DC/DC converter with an algorithm for the automatic control of its duty cycle “ δ ” is inserted between the photovoltaic array and the load , resulting in what is known as MPPT system. The MPPT must control the voltage or current (through the δ the converter) of the PV array regardless of the load, trying to place it in the MPP. Therefore, the MPPT must find the optimal δ for the operation point of the PV array to coincide with the MPP[enrique2010reliable].

Although the solution to operating in the MPP may seem immediate, it is not. This

4 | MAXIMUM POWER POINT TRACKING(MPPT) 1.2

is because the location of the **MPP** in the I-V curve of the PV array is not known a priori. This point must be located, either by mathematical calculations over a valid model, or by using some search algorithm. This implies even more difficulty if we consider the fact that the **MPP** presents non-linear dependencies with temperature and radiation[enrique2010reliable]

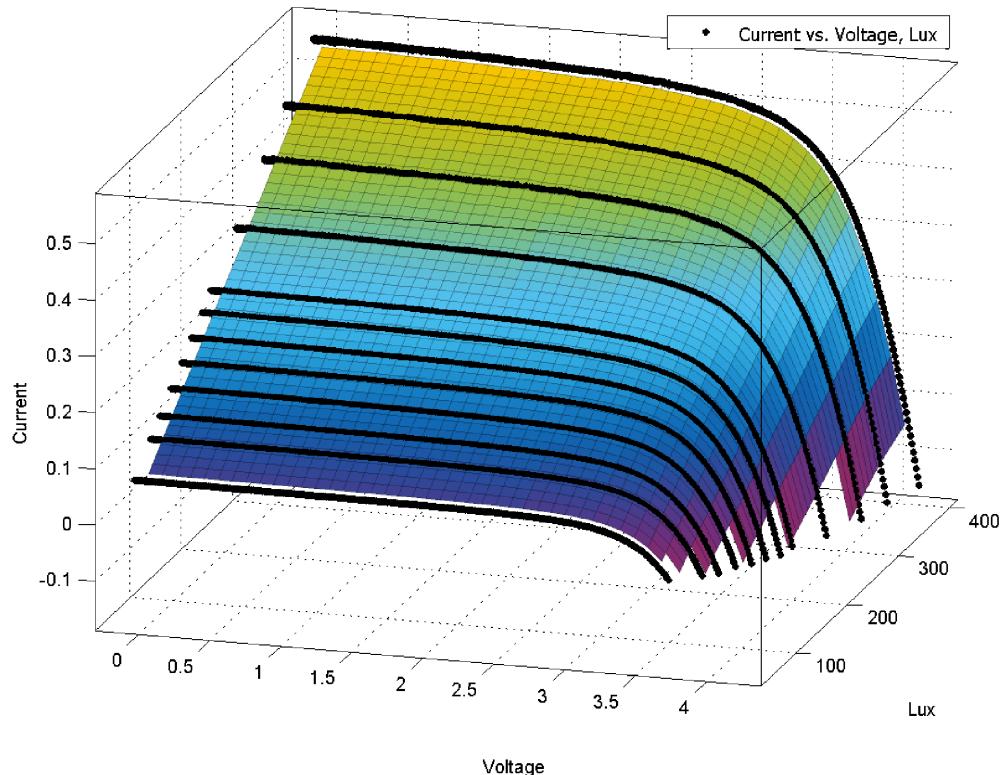


Figure 1.3: I-V-Lux

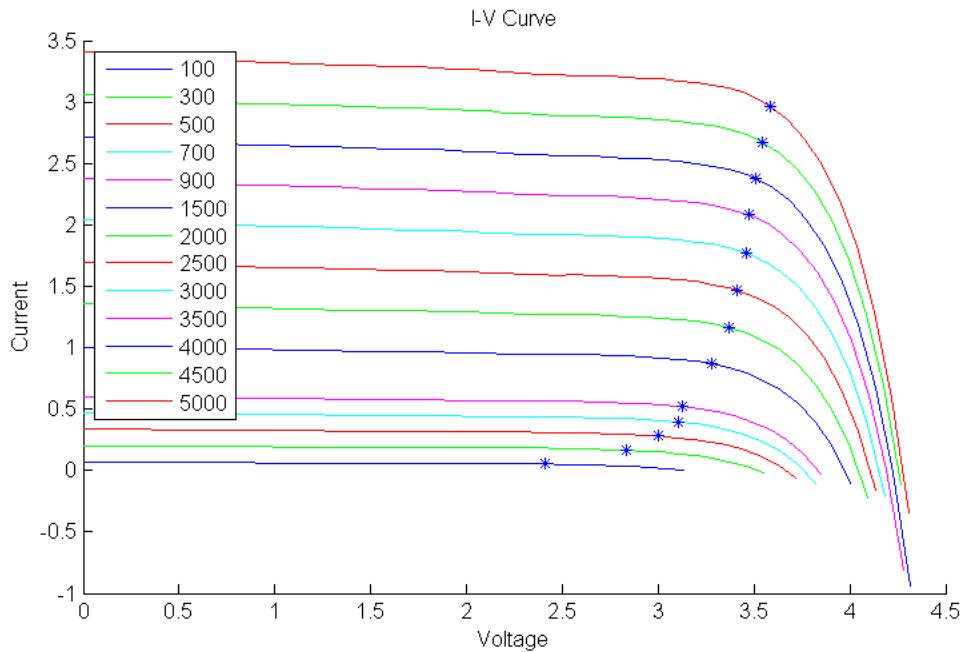


Figure 1.4: I-V Graph, MPPT marked with '*'.

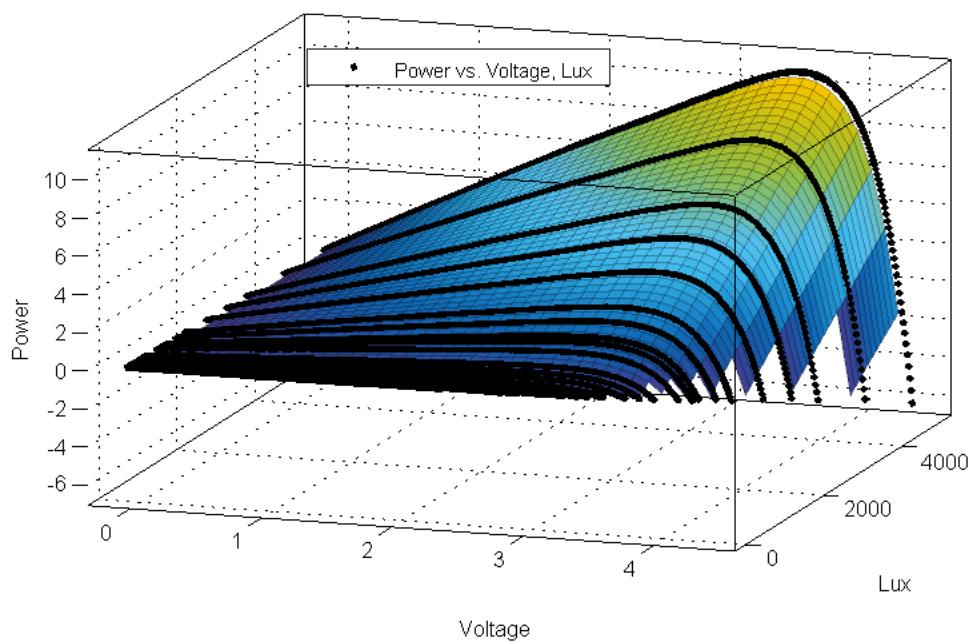


Figure 1.5: P-V Lux

As such, many **MPPT** methods have been developed and implemented. The methods vary in complexity, sensors required, convergence speed, cost, range of effectiveness,

6 | SCOPE, THESIS GOALS AND OBJECTIVES 1.3

implementation hardware, popularity, and in other respects. They range from the almost obvious (but not necessarily ineffective) to the most creative (not necessarily most effective). In fact, so many methods have been developed that it has become difficult to adequately determine which method, newly proposed or existing, is most appropriate for a given PV system. Some of the most popular being:

- Perturb and Observe Method
- Incremental Conductance Method
- fractional open circuit voltage Method
- Fixed duty cycle Method
- Pilot cell Method
- Pilot cell Method
- Fractional short-circuit current Method
- Fuzzy logic controller

1.3 | SCOPE, THESIS GOALS AND OBJECTIVES

This thesis focuses on the finding a practically **optimal** and usable MPPT algorithm that is optimised to be used with the current DSCs.

The objectives of the thesis can be summarized as:

- Develop an Electrical model for DSCs and verify the accuracy of said model.
- Compare and optimize the following Maximum power point tracking (MPPT) algorithms for compatibility with the above Model using MATLAB® and Simulink®.
 1. Perturb and Observe ([PnO](#)) Method.
 2. Incremental Conductance Method ([ICM](#)).
 3. fractional open circuit voltage ([FOCV](#)) Method.
- Setting up the test environment
- Execution of test cases on prototype developed, based on two of the best optimized algorithm, with recordable test results.
- Develop Reference designs for production.
- Internal report.
- Master thesis report.

1.4 | THESIS OUTLINE

- Chapter 1 Presents the background and the main objectives of this thesis
- Chapter 2 Contains the prior research and literature that this thesis was based on, it also discusses the principle of operating principles/state-of-the-art of **DSCs** and of **MPPT**
- Chapter 3 concerns the research methods, measurement techniques and implementation of the thesis.
- Chapter 4 Gives a summary of the results.
- The thesis is Concluded and Future Work talked about in Chapter 5

1.5 | RESEARCH METHODOLOGY

The implementation of the thesis is **

- Develop a suable model for the **DSCs** based on either:
 1. the single diode equation for **DSCs**.
 2. based on experimental modelling Methods .
- objective study of current algorithms; weigh their pros vs cons.
- Validation of the Model and algorithm in MATLAB® and Simulink®.
- Implementation in test Hardware .

2 | RELATED LITERATURE

****This chapter reviews the relevant literature's to establish the research context necessary for the thesis.** OR **This section explores contemporary academic/scientific papers and research that forms the basis for this thesis. ****

2.1 DYE-SENSITIZED SOLAR CELLS(DSCS)

****Move part of the text and pictures from introduction to here **** The basic structure of DSCs is represented in the Figure 2.1 on page 9.

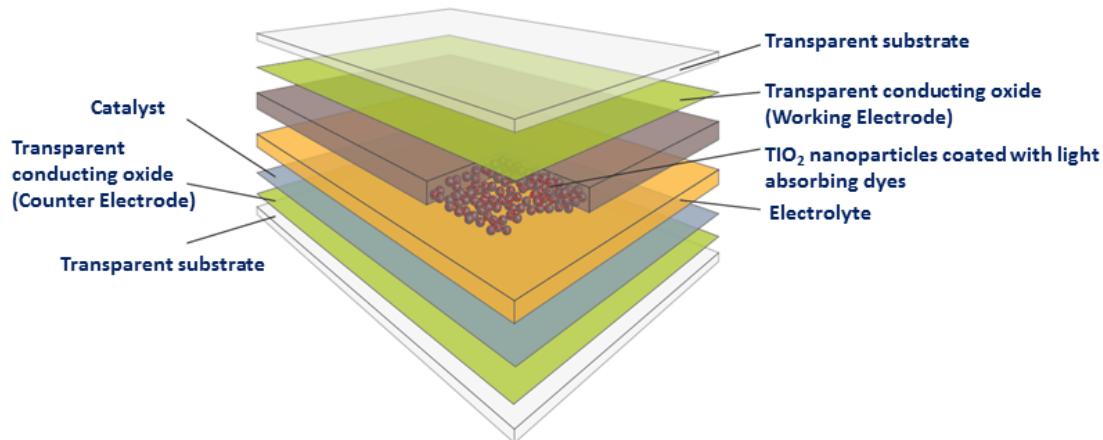


Figure 2.1: Structure of a DSC

The most commonly used substrate is glass coated with fluorine-doped tin oxide (**FTO**). Attached to the surface of the nano-crystalline particles of Titanium dioxide(TiO_2) is a mono-layer of the light-sensitive-charge-transfer dye. The dye absorbed photons of incoming light and uses this energy to release free electrons to the TiO_2 layer acting as the Working Electrode (**WE**) and then onto metal contacts. An electrolyte is filled between the electrodes and helps transfer electrons from the Counter Electrode (**CE**) to the dye particle which is in an oxidized state due to a loss of electron to reduce it back to its ground state. The most commonly used redox couple, and the one that gives the best cell efficiencies when combined with TiO_2 , is iodide/triiodide (I^-/I_3^-). The oxidized dye gets electrons from the iodide ions which, in turn, get oxidized to triiodide in the process. The triiodide ions then diffuse to the counter electrode, where they get reduced back to iodide by the electrons returning from the external load. Thus,

the cell operation is based on consecutive reduction/oxidation cycles and, in an ideal cell, no chemical substances are permanently transmuted. The most often used counter electrode catalyst for the triiodide/iodide reduction reaction is platinum, though also carbon materials and certain conductive polymers have been successfully employed in this function.

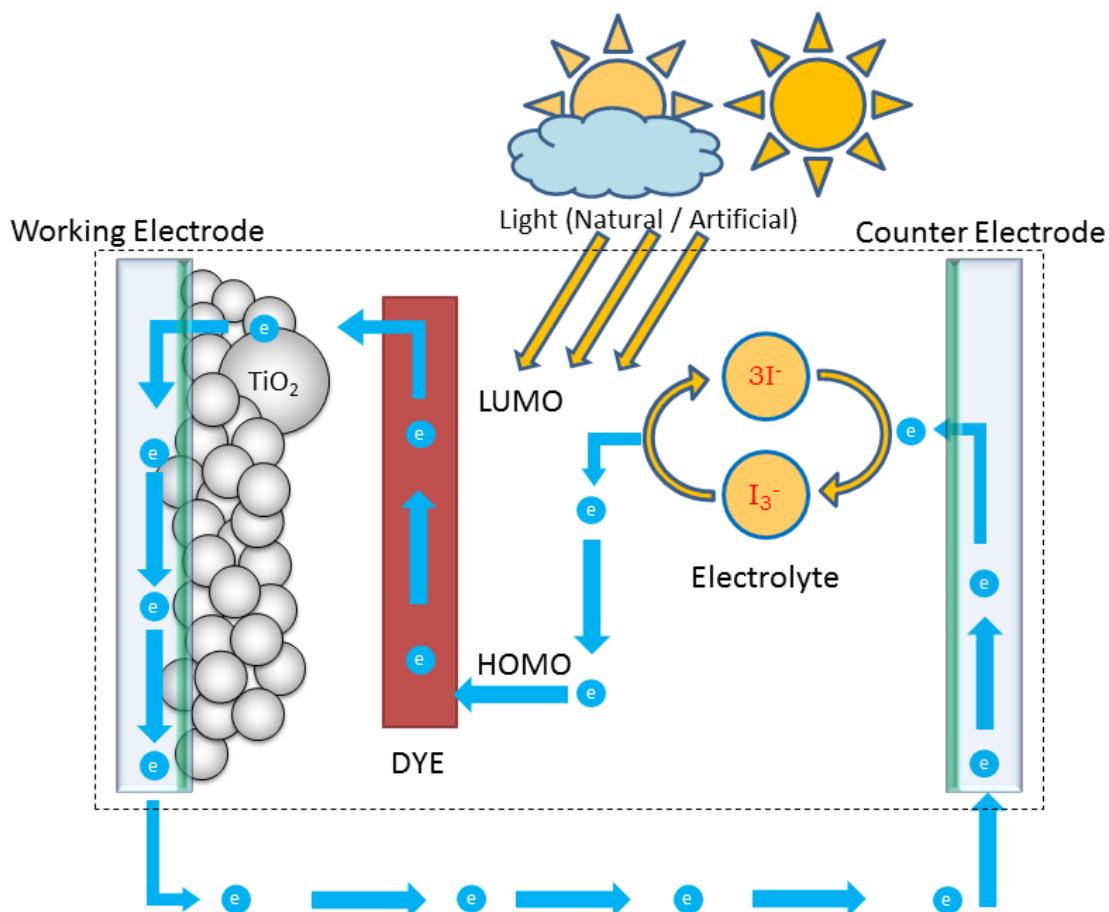


Figure 2.2: The structure and operating principle of a DSC (adapted from [toivola2010dye][lgcell_DSSC_cycle])

The amount of current that the cell is able to generate is determined by the energetic distance of the Highest Occupied Molecular Orbital (HOMO) and Lowest Unoccupied Molecular Orbital (LUMO) of the dye, which equals the band gap in inorganic semiconductors. The maximum voltage, on the other hand, is defined as the difference between the redox level of the electrolyte and the Fermi level of the TiO₂. With iodide/triiodide redox couple, this difference is 0.9 V, though slight variation is caused by the electrolyte composition due to species adsorbed on the TiO₂ surface, which may alter the Fermi level position somewhat. Also, there is always some recombination in the cell which lessens the amount of electrons in the TiO₂ film, thus lowering the Fermi level and decreasing the cell voltage. [toivola2010dye]. This operating principle of DSCs is

depicted in the Figure 2.2 on page 10.

Info about single diode model of DSCs Pictures etc

2.1.1 Single diode model

The simplest equivalent circuit of a generic solar cell is a Single diode model comprising of a current source in parallel with a diode. A slightly more detailed model includes a shunt resistance of the cell which takes into account the parallel resistive losses representing leakage current across the junction in the cell. This model is sometimes referred to as a single exponential five-parameter model[vignati2012solutions]. Like before, the incident photons induces a current in the active area that is proportional to the intensity of the light falling on the cell.

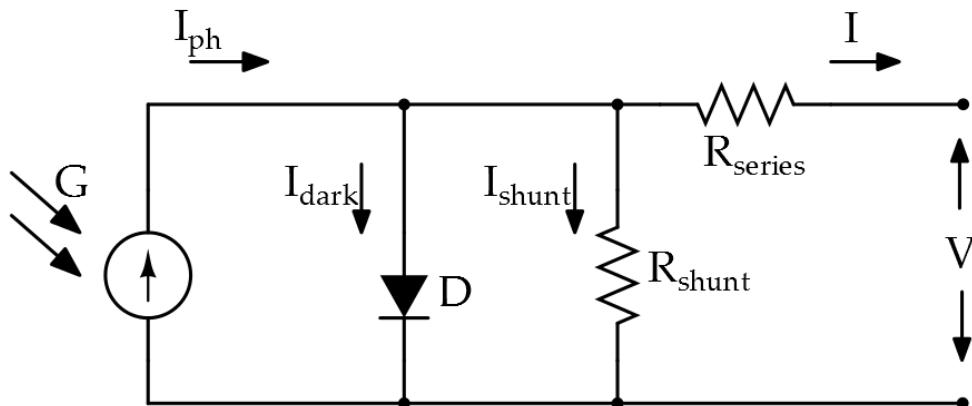


Figure 2.3: Single diode model for a solar cell

Change text The power conversion efficiency of a solar cell is determined from the current versus applied voltage (I-V) characteristics under illumination. The I-V curve and device efficiency are reported with respect to a standard reference spectral irradiance distribution, the air mass 1.5 global (AM 1.5G) spectrum[wenger2010strategies]. The I-V characteristics of a solar cell are well described by an equivalent electric circuit in Figure 2.3 on page 11 . Under illumination, a constant photo current (I_{ph}) is generated. If a forward voltage bias is applied, a dark diode current (I_{dark}) flows in the opposite direction. A shunt resistance (R_{shunt}) may arise from charge recombination in the photo-active layer and induce a shunting current(I_{shunt}).The series resistance (R_{series}) includes the contact resistance at interfaces, the bulk resistance, and the sheet resistance of the transparent electrodes. The total measured current then is:

$$I = I_{ph} - I_{dark} - I_{shunt} = I_{ph} - I_s(e^{\frac{eV}{mkT}} - 1) - \frac{V + IR_{series}}{R_{shunt}} \quad (2.1)$$

where I_s is the diode saturation current, V is the applied bias voltage, m is an ideality factor ($m = 1$ for an ideal cell), k is the Boltzmann constant, and T is the device temperature[pointwenger2010strategies]. For small forward bias voltages the numerical value of the exponential is very large and the thermal voltage very small, therefore the '-1' in the diode equation can be safely neglected and the forward diode current can be written as[pv_education_org]:

$$I_{dark} = I_s(e^{\frac{eV}{mkT}}) \quad (2.2)$$

Substituting the value of I_{dark} back in equation 2.1 and neglecting the shunt resistance we can simplify the equation to as below (equation 2.3) can be schematically depicted as Figure 2.4 on page 12. The simplified equation suffices for most modelling applications.

$$I = I_{ph} - I_{dark} - I_{shunt} = I_{ph} - I_s(e^{\frac{eV}{mkT}}) \quad (2.3)$$

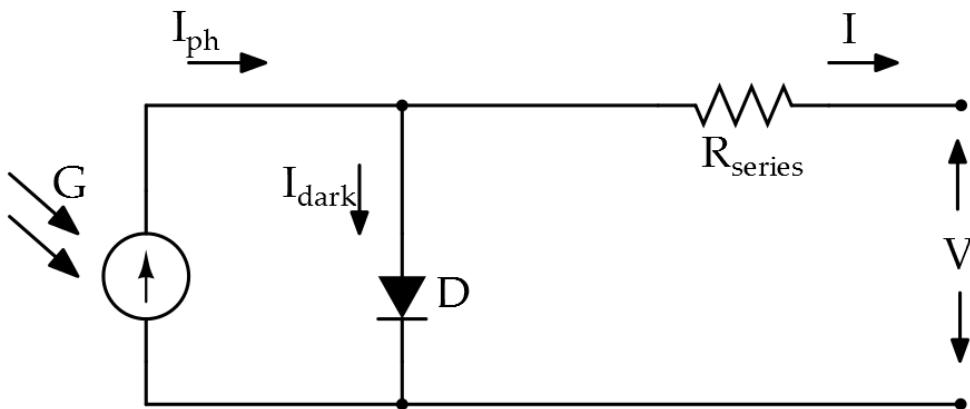


Figure 2.4: Simplified single diode model for a solar cell

The maximum-power operating point defines the condition at which the power output ($P_{max} = I_{max}V_{max}$) of the device is maximal. The so-called Fill Factor (FF) is often used to characterize the maximum power ,

$$FF = \frac{I_{max}V_{max}}{I_{sc}V_{oc}} \quad (2.4)$$

The accuracy and complexity of the model can be increased by including Temperature dependence of the photo current and diode saturation current; Shunt resistance in

parallel with the diode; Accommodating for variance in the quality factor of the diode either by having a variable parameter or introduction of an additional diode in to the circuit as done in the Double Diode Model.

2.1.2 | Double diode model

The single diode equation assumes a constant value for the ideality factor n . In reality the ideality factor is a function of voltage across the device. At high voltage, When the recombination in the device is dominated by the surfaces and the bulk regions the ideality factor is close to one. However at lower voltages, recombination in the junction dominates and the ideality factor approaches two. The junction recombination is modelled by adding a second diode in parallel with the first and setting the ideality factor typically to two(ideality factor, m for $D_1 = 1$ and $D_2 = 2$)[[pv_education_org](#)].

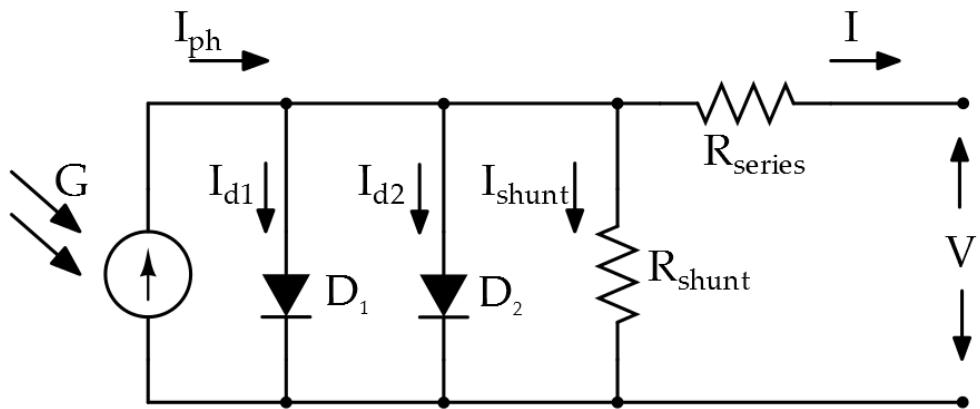


Figure 2.5: Double diode model for a solar cell

The equation of the double diode model under illumination is given by:

$$I = I_{ph} - I_{dark} - I_{shunt} = I_{ph} - I_{s1}(e^{\frac{eV}{kT}} - 1) - I_{s2}(e^{\frac{eV}{2kT}} - 1) - \frac{V + IR_{series}}{R_{shunt}} \quad (2.5)$$

2.1.3 | Equivalent DSCs model

It has normally been found that [DSCs](#) do not conform to the typical I-V curves obtained from transmission line model and ladder circuit[[yong2008modeling](#)].[DSCs](#) are often modelled with circuits similar to conventional pn -junction solar cell (Section 2.1.1 and 2.1.2),however even these representations fail to correspond to experimentally obtained

values.

A standard DSCs typically contains three interfaces formed by FTO/TiO₂, TiO₂/dye/electrolyte, and electrolyte/Pt-FTO as depicted in the Figure 2.2 on page 10. The equivalent circuit below (Figure 2.6) accounts for these interfaces. The interfacial charge transfer at the TiO₂/ dye/ electrolyte is represented by a rectifying diode(D₁) and a double-layer capacitance (C_i).A recombination diode D₂ is employed to denote the interfacial charge recombination losses to both the dye cation and the redox electrolyte.Parallel resistive losses across the cell including leakage current is indicated by R_{Shunt}. The photo-generated current I_{ph} is in parallel with the Diodes and C_i. An inductive recombination pathway as a result of a charge-transfer current is incorporated into the circuit, consisting of a recombination resistance(R_{rec})in series with the an inductor (L).The charge-transfer resistance and interfacial capacitance at the FTO electrode and electrolyte/Pt-FTO interface are represented by R_E and C_E, and R_{CE} and C_{CE} respectively.The Nernst diffusion of the carrier transport by ions within the electrolyte is denoted by the Warburg impedance (W). A resistance element R_{Series} designates the bulk and contact resistive losses present in a practical DSCs,such as the sheet resistance of the FTO glass,Contact resistance etc. The I-V characteristics based on the equivalent circuit model in figure 2.6 is described in equations 2.6 [yong2008modeling].

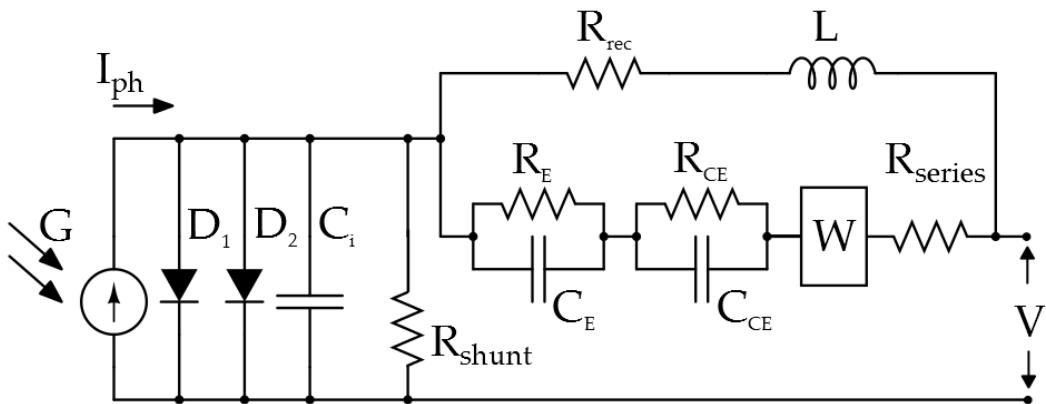


Figure 2.6: Equivalent circuit for DSCs

$$I = I_{ph} - I_{s1}(e^{\frac{eV}{mkT}} - 1) - I_{s2}(e^{\frac{eV}{2mkT}} - 1) - (V + IZ)(j\omega C_i + \frac{1}{R_{Shunt}}) \quad (2.6)$$

$$I_{ph} = \int qF(\lambda)[1 - r(\lambda)]IPCE(\lambda)d\lambda = \int qF(\lambda)\Phi(\lambda)d\lambda \quad (2.7)$$

$$Z = \frac{1}{(R_{rec} + j\omega L)} + \frac{1}{Z_S} \quad (2.8)$$

$$Z_S = \frac{1}{j\omega C_E + \frac{1}{R_E}} + \frac{1}{j\omega C_{CE} + \frac{1}{R_{CE}}} + W + R_S \quad (2.9)$$

$$W = \sigma\omega^{-1/2}(1-j) \quad (2.10)$$

Where T is the absolute temperature, ω is the angular frequency, σ is the Warburg coefficient, $F(\lambda)$ and $IPCE(\lambda)$ are the incident photon flux density and the incident photon-to-current conversion efficiency at wavelength λ respectively, $r(\lambda)$ is the incident light losses due to the light absorption and reflection by the FTO glass, and $\Phi(\lambda)$ is the quantum yield [yong2008modeling].

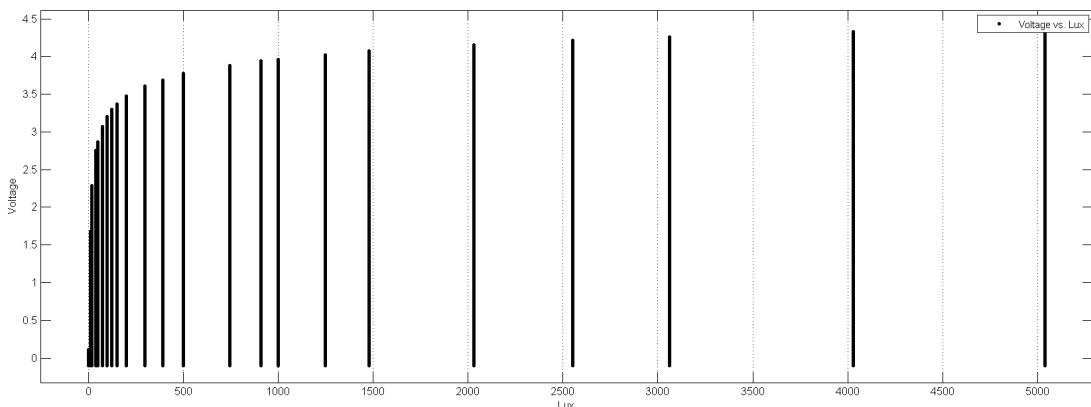


Figure 2.7: spread of measured illumination vs Voltage

However due to the near impossibility of accurately measuring all the variables of a unknown cell for this research work,a model was constructed by placing a the test cell under a battery of varied illuminations (0 Lux - 5050 Lux) shown in figure 2.7 . Which resulted in a surface that closely resembles the cell's operation in real world conditions. particular attention was paid to low light conditions which is to be expected for indoor illuminations (< 2000 Lux).As DSCs display are very stable output across a large temperature range, the above model was made independent of temperature variations.

**Pictures and text about losses in the light absorption in the cell **

**talk ABOUT STABILITY OF dcs with change in temperature **

Despite all the advantages presented by the generation of energy through the use of PVs, the efficiency of energy conversion is currently low and the initial cost for its implementation is still considered high, and thus it becomes necessary to use techniques to extract the maximum power from these panels, in order to achieve maximum efficiency in operation. It should be noted that there is only one maximum power point (MPP), and this varies according to climatic and irradiation conditions[[eltawil2013mppt](#)].

To overcome this problem, several methods for extracting the maximum power have been proposed in literature **citations **

[2.2.1](#) | Perturb and Observe Method



Figure 2.8: Black box model for the Perturb and Observe Algorithm

The [PnO](#) Method is most widely used in [MPPT](#) because of its simple structure and it requires only few parameters. Figure [2.9](#) shows the flow chart of [PnO](#) method. It perturbs the PV array's terminal voltage periodically, and then it compares the PV output power with that of the previous cycle of perturbation. When PV power and PV voltage increase at the same time and vice versa, a perturbation step size, ΔD will be added to the duty cycle, D to generate the next cycle of perturbation in order to force the operating point moving towards the [MPP](#). When PV power increases and PV voltage decreases and vice versa, the perturbation step will be subtracted for the next cycle of perturbation. This process will be carried on continuously until [MPP](#) is reached. However, the system will oscillate around the [MPP](#) throughout this process, and this will result in loss of energy. These oscillations can be minimized by reducing the perturbation step size but it significantly slows down the [MPP](#) tracking system also leading to loss of energy.[[ngan2011study](#)].[PnO](#) is also not suable when the light intensity changes rapidly.

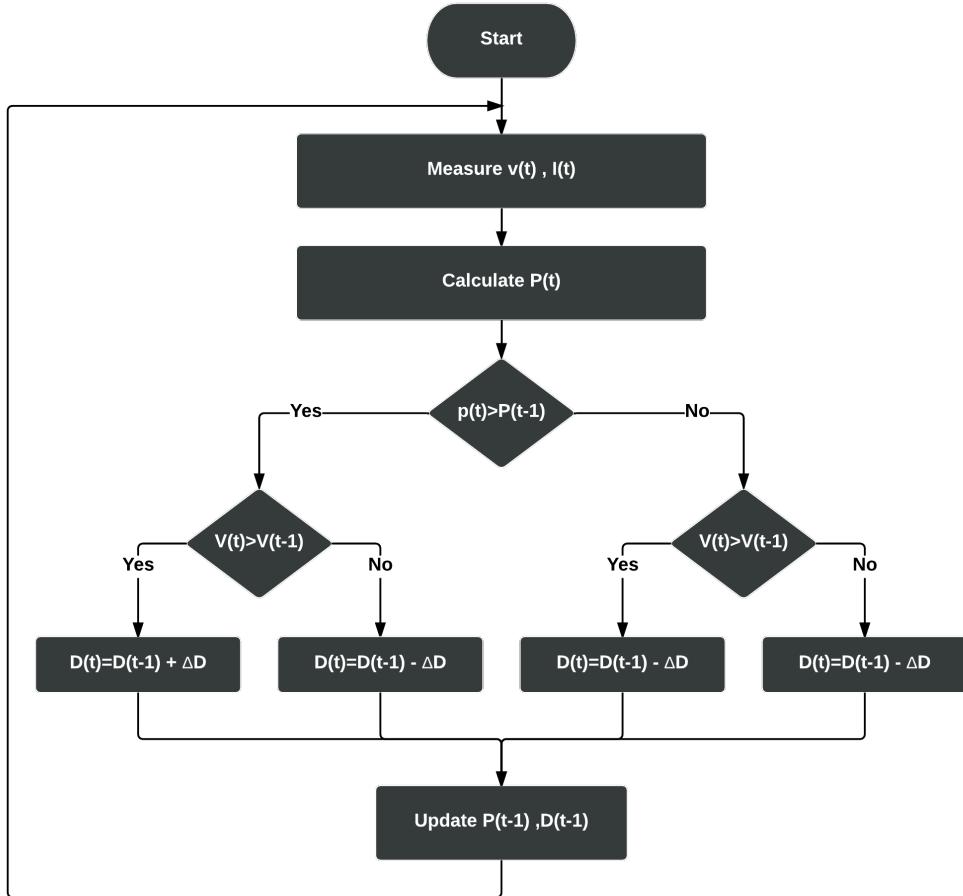


Figure 2.9: Flow chart for the Perturb and Observe Method

2.2.2 Incremental Conductance Method



Figure 2.10: Black box model for the Incremental Conductance Algorithm

The solar array terminal voltage can be adjusted relative to the MPP voltage by measuring the incremental and instantaneous array conductance (dI/dV and I/V , respectively).

18 | MAXIMUM POWER POINT TRACKING(MPPT) 2.2

The Algorithm is based on the fact that at the **MPP** the derivative of the cell's power is zero. Although the incremental conductance method offers good performance under rapidly changing atmospheric conditions, four sensors are required to perform the computations. The drawback is that sensor devices require more conversion time thus result in a large amount of power loss[**gomathy2012design**].In addition to the above drawback, the **ICM** suffers the same limitations as **PnO** method namely,for rapid tracking larger step sized must be utilized which results in the oscillation around the **MPP**.

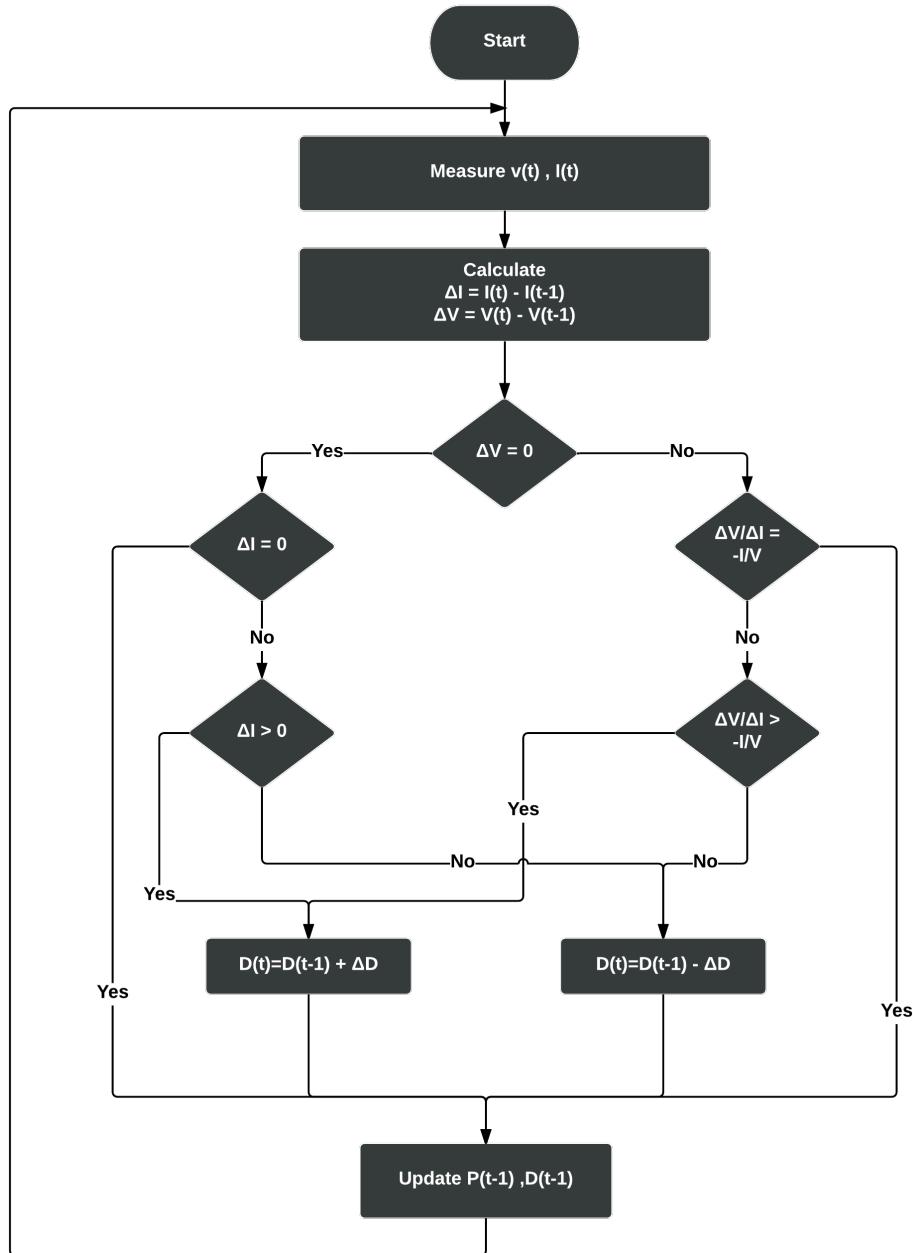


Figure 2.11: Flow chart for the Incremental Conductance Method



Figure 2.12: Black box model for the Incremental Conductance Algorithm

This is a method based on the linear relationship between output voltage of the PV array at the **MPP**, V_{MPP} and the PV array's open circuit voltage, V_{OC} in under varying temperature and solar irradiance.

$$V_{MPP} \approx k_i V_{OC} \quad (2.11)$$

Constant value of k_i is dependent on the characteristics of PV array. Generally, it has to be computed empirically in order to determine the V_{MPP} and V_{OC} for varied temperatures and solar irradiances. The value of k_i ranges from 0.73 to 0.80 for most PV modules over a temperature range of 0 to 60°C. Figure 2.13 describes the operation of a **FOCV**, the PV array is temporarily isolated from **MPPT**, then the open circuit voltage, V_{OC} is measured periodically by shutting down the power converter momentarily. The **MPPT** calculates V_{MPP} from the pre-set value of k_1 and the calculated value of V_{OC} . Then, the array's voltage is varied until V_{MPP} is reached. The shut-down of power converter periodically will incur temporary loss of power which results in power extracted will not be the maxima. Since is an approximation, the PV array will never reach the **MPP**. Even though this technique is very easy and cheap for implementation, yet since true **MPP** is never reached there is always a loss in power during operation [ngan2011study].

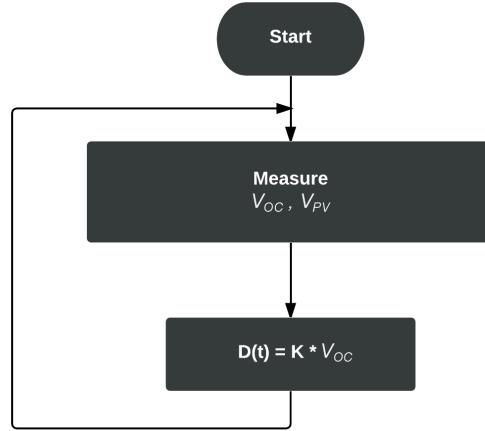


Figure 2.13: Flow chart for the fractional open circuit voltage Method Method

2.2.4 | Other Algorithms

- **Fixed duty cycle** The fixed duty cycle represents the simplest of the methods and it does not require any feedback, where the load impedance is adjusted only once for the maximum power point and it is not adjusted again.
- **Pilot cell** In the pilot cell MPPT algorithm, the constant voltage or current method is used, but the open-circuit voltage or short-circuit current measurements are made on a small solar cell, called a pilot cell, that has the same characteristics as the cells in the larger solar array. The pilot cell measurements can be used by the MPPT to operate the main solar array at its MPP, eliminating the loss of PV power during the V_{OC} or I_{SC} measurement.
- **Fractional short-circuit current** under varying atmospheric conditions, I_{MPP} is approximately linearly related to the I_{SC} of the PV array.

$$I_{MPP} \approx k_j I_{SC} \quad (2.12)$$

- **Fuzzy logic controller (FLC)** have the advantages of working with imprecise inputs, it does not need an accurate mathematical model and it can handle non-linearity as well [messai2011maximu]. However their effectiveness depends a lot on the presence of an expert knowledge; conversely, in the absence of such knowledge, their design is usually slow and not optimized.

2.3 | MACHINE LEARNING ???

This section discusses about Search optimization in order to lock on the V_{MP} and I_{MP} as efficiently as possible.

We use regression analysis when we want to predict one variable from another. The most basic form of regression is called simple regression, where We have 1 independent variable and 1 dependent variable and where we are predicting a linear trend. In regression, we attempt to determine the magnitude of the relationship between a set of independent variables and the dependent variable. Independent variable(X), Also called the predictor variable, that we believe influences our Dependent variable(Y),Also called the response variable[[lenarreg2006](#)].

A regression model is a formal way of stating:

- The tendency of the response variable(Y) to vary with the predictor variable(X).
- A scattering of points around some statistical relationship.

Equation for a line can be written as:

$$y = mx + b \quad (2.13)$$

The linear regression model(for observation $i = 1, \dots, N$) can we written as:

$$Y_i = \beta_0 + \beta_1 X_i + \epsilon_i \quad (2.14)$$

- β_0 is the mean of the population when X is zero -the Y intercept.
- β_1 is the slope of the line, the amount of increase in Y brought about by a unit increase ($X' = X + 1$) in X.
- ϵ_i is the random error, specific to each observation.

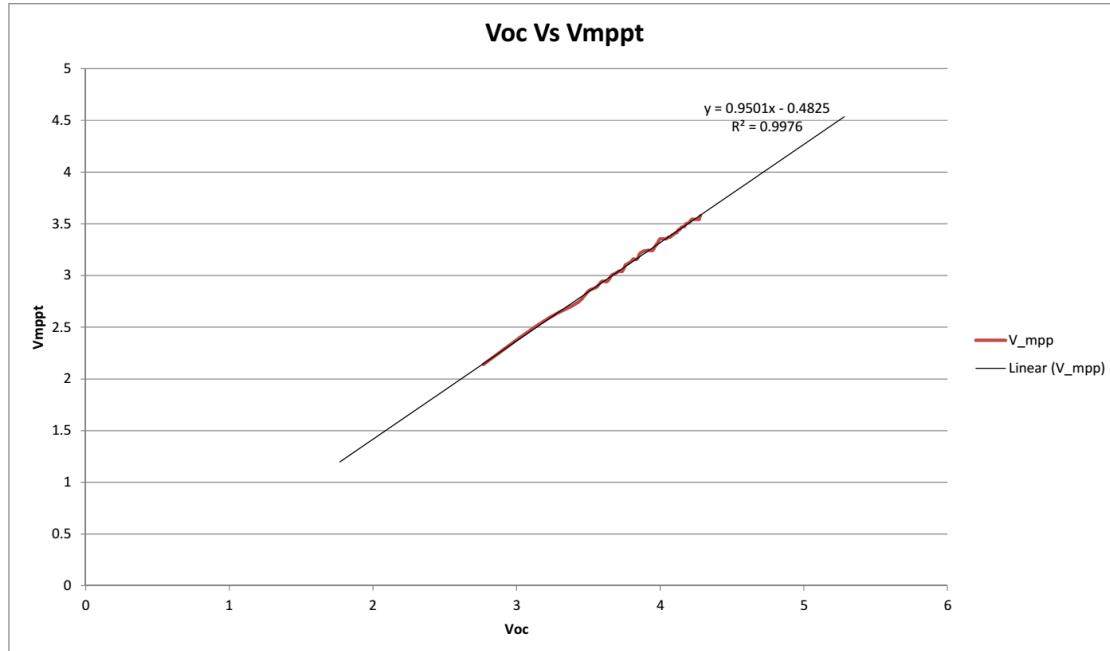


Figure 2.14: Example for linear regression

**add more text about line Linear Regression **

2.3.2 | Pattern search

Seiler, Mary C., and Fritz A. Seiler. "Numerical recipes in C: the art of scientific computing.- 10.2 Golden Section Search in One dimension" Risk Analysis 9.3 (1989): 415-416.

Finding the Maxima or minima of a first order single variable function can easily be found by equating the derivative of this function to zero. However finding the derivative of certain functions is not always easy or possible. In such conditions Search techniques are used to find the Maxima or minima in a uni-modal((A uni-modal function contains only one minimum or maximum on the specified interval) continuous function over an interval without using derivatives. Golden Section search Algorithm is one such search method. The Algorithm derives its name from the Golden ratio(0.61803...)

Two numbers are said to be in the golden ratio if their ratio is same as the ratio of their sum to the larger of the two quantities. Assuming $b > a$ then this can be expressed as:

$$\frac{a+b}{b} = \frac{b}{a} = \phi \quad (2.15)$$

where ϕ is the golden ratio whose value is given by:

$$\phi = \frac{\sqrt{5} - 1}{2} = 0.61803398874989..... \quad (2.16)$$

**add more text about Golden search **

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Figure 2.15: Golden Section search Algorithm

3

METHODOLOGY AND IMPLEMENTATION

This chapter covers the implementation details of the concept, the algorithms. All the simulations were first carried out in MATLAB® and Simulink®, testing and verifying; then implementing the same in Hardware.

3.1 CELL CHARACTERISATION

In this section, Model of two types of cells ([a-Si](#) and [DSCs](#)) is discussed. There are several Models that have been analysed in literature which are usually variations of the Single Diode model or the Double Diode model (discussed in section [2.1.1](#) and [2.1.2](#)).

3.1.1 Test Setup

in **furtherance of** creating a working solar cell model and to validate the algorithm several measurements would need to be performed. The Test-rig consisted of a blacked out enclosure to prevent **interference** from ambient light. The Test-rig is fitted with an array of evenly spaced White-Light Emitting Diode ([LED](#)s) to provide uniform illumination on the Test subject. The [LED](#)-array are calibrated and temperature controlled so as to provide white light with a known spectra. A high precision Lux Meter([GOSSEN Mavolux 5032B](#)) is used to measure the intensity of the light, as perceived by the human eye. The Light chamber is also routinely calibrated against a reference cell to factor-in the variations and degradation of the [LEDs](#). The intensity of light is varied using a High-Voltage power source. A pictorial representation of the above description can be seen in figure [3.1](#) on page [26](#).

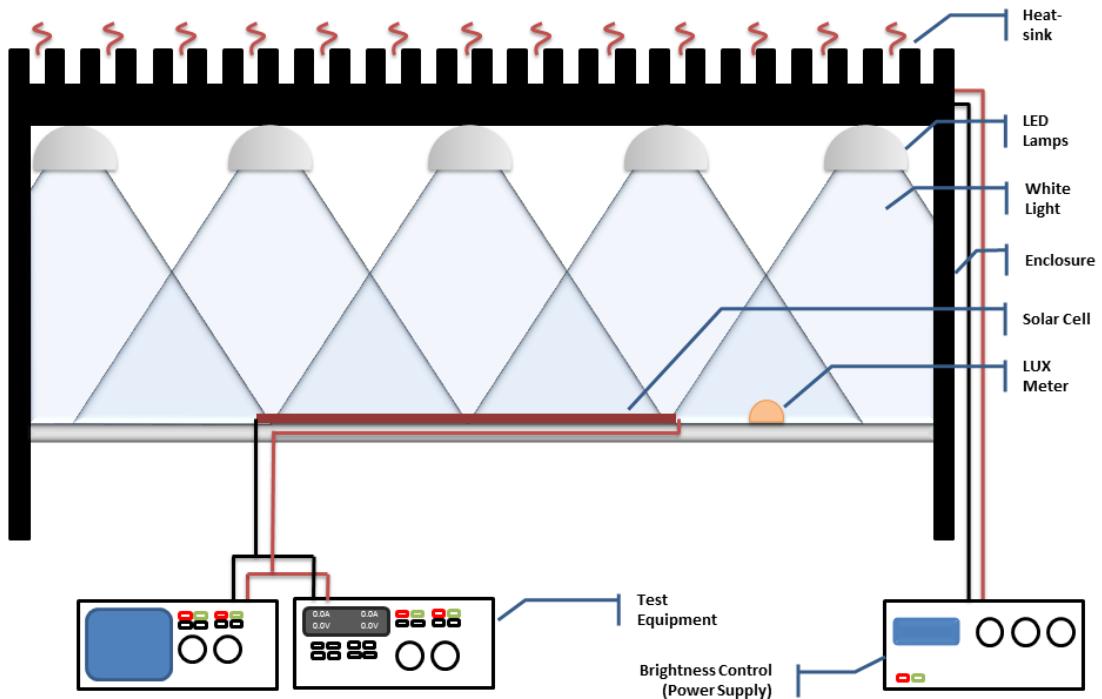


Figure 3.1: Test Setup

As the Sink Voltage is increased in small steps from 0 V to V_{OC} and beyond the cell is forced to operate at the Sink Voltage resulting in the I-V graph depicted in figure 3.3 on page 27. When the above is repeated for several different light intensities we get a three-dimensional surface shown in figure 3.4 on page 28

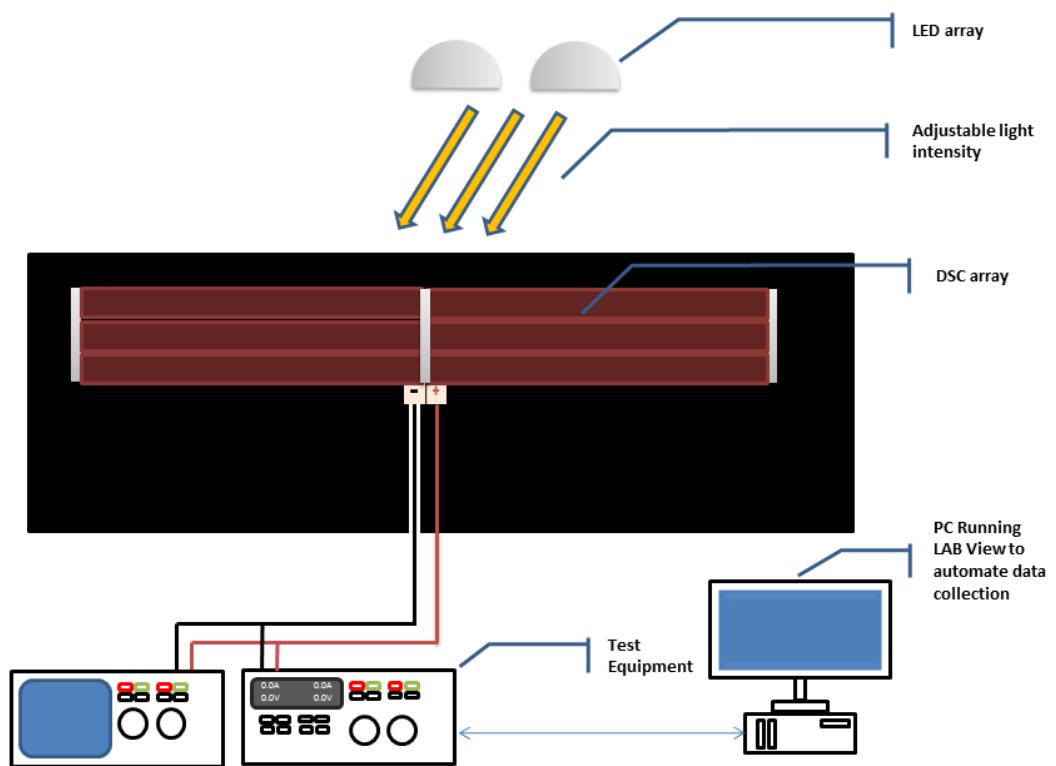


Figure 3.2: Cell Characterisation

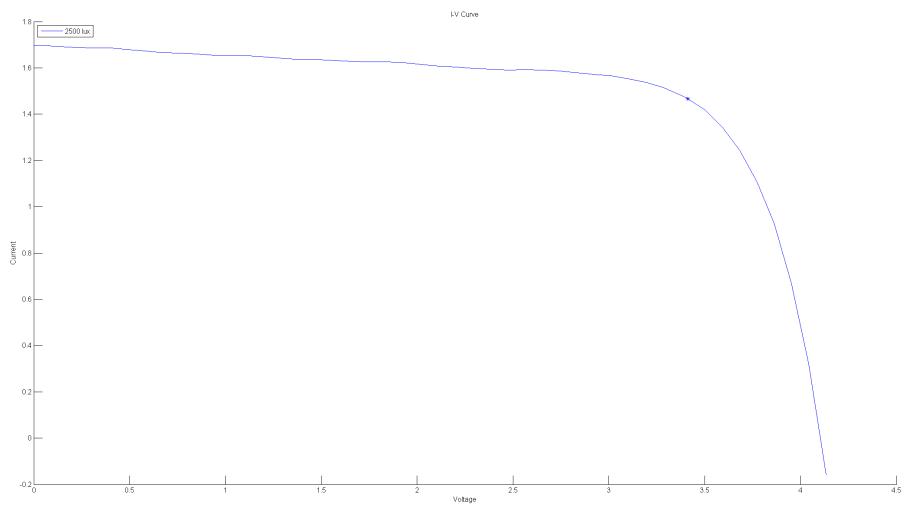


Figure 3.3: I-V curve for the array at steady illumination

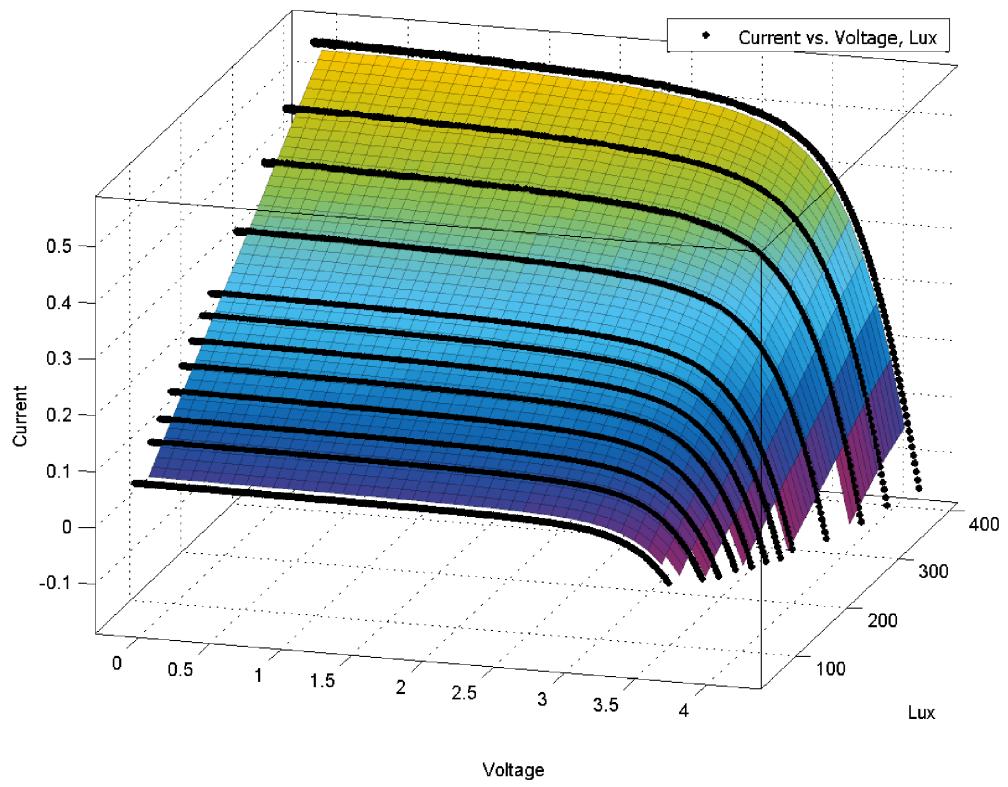


Figure 3.4: I-V curve for the array at varying illumination

3.2 MODELLING AND SIMULATIONS

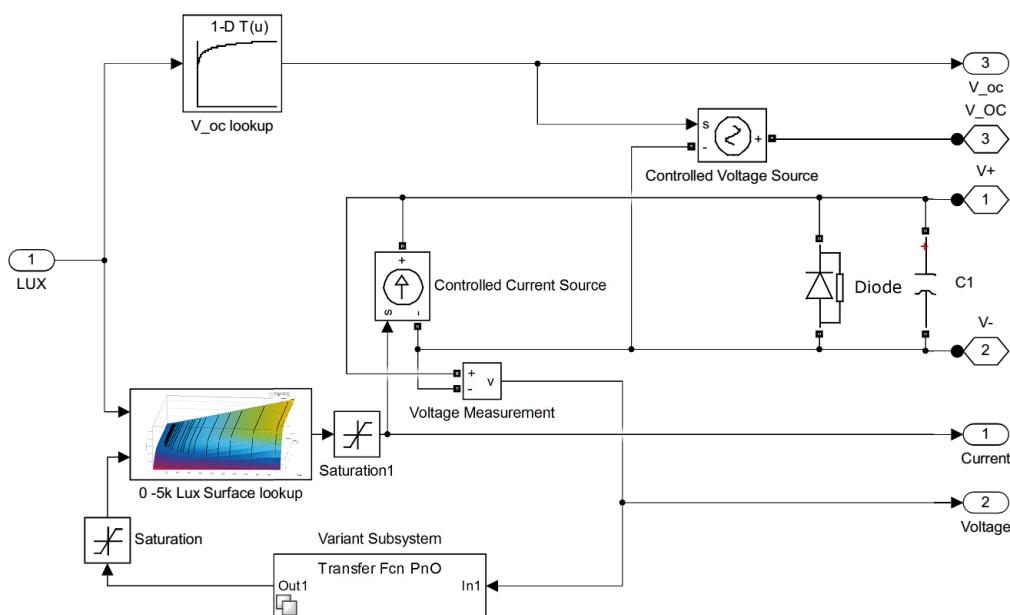


Figure 3.5: Modelling of the DSC Subsystem

3.3 VALIDATION IN MATLAB®

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4 RESULT DISCUSSION

4.1 PERTURB AND OBSERVE METHOD

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Figure 4.1: Perturb and Observe Method on implementation

4.2 INCREMENTAL CONDUCTANCE METHOD

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Figure 4.2: Incremental Conductance Method on implementation

4.3 FRACTIONAL OPEN CIRCUIT VOLTAGE METHOD

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Figure 4.3: fractional open circuit voltage on implementation

4.4 | PROPOSED METHOD

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Figure 4.4: Flow chart for Proposed MPPT Algorithm

5 CONCLUSION AND FUTURE WORK

This final chapter concludes the results obtained from the thesis and also the vast scope for future work in this area.

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5.0.1 **text**[ngan2011study]

Ngan, Mei Shan, and Chee Wei Tan. "A study of maximum power point tracking algorithms for stand-alone photovoltaic systems." Applied Power Electronics Colloquium (IAPEC), 2011 IEEE, IEEE, 2011.

**Text about the paper **

5.0.2 | **text[ngan2011study]**

Ngan, Mei Shan, and Chee Wei Tan. "A study of maximum power point tracking algorithms for stand-alone photovoltaic systems." Applied Power Electronics Colloquium (IAPEC), 2011 IEEE. IEEE, 2011.

**Text about the paper **

5.0.3 | **text[esram2007comparison]**

Esram, Trishan, and Patrick L. Chapman. "Comparison of photovoltaic array maximum power point tracking techniques." IEEE TRANSACTIONS ON ENERGY CONVERSION EC 22.2 (2007): 439.

**almost all the Work in eltawil2013mppt is derived from this paper including pictures and text **

5.0.4 | **text[eltawil2013mppt]**

Eltawil, Mohamed A., and Zhengming Zhao. "MPPT techniques for photovoltaic applications." Renewable and Sustainable Energy Reviews 25 (2013): 793-813.

This article aims to assess different MPPT techniques, provide background knowledge, implementation topology, grid interconnection of PV and solar microinverter requirements presented in the literature, doing in depth comparisons between them with a brief discussion. The MPPT merits, demerits and classification, which can be used as a reference for future research related to optimizing the solar power generation, are also discussed.

**Text about the paper **

5.0.5 | **text[reza2013classification]**

Reza Reisi, Ali, Mohammad Hassan Moradi, and Shahriar Jamasb. "Classification and comparison of maximum power point tracking techniques for photovoltaic system: A review." Renewable and Sustainable Energy Reviews 19 (2013): 433-443.

5.0.6 | **text**[faranda2008energy]

Faranda, Roberto, and Sonia Leva. "Energy comparison of MPPT techniques for PV Systems." WSEAS transactions on power systems 3.6 (2008): 446-455.

This paper presents a comparative study of ten widely-adopted MPPT algorithms; their performance is evaluated on the energy point of view, by using the simulation tool Simulink®, considering different solar irradiance variations.

My thesis borrows some of the algorithms/Flow Chart mentioned in the above four papers.

5.0.7 | **text**[houssamo2013experimental]

Houssamo, Issam, Fabrice Locment, and Manuela Sechilariu. "Experimental analysis of impact of MPPT methods on energy efficiency for photovoltaic power systems." International Journal of Electrical Power & Energy Systems 46 (2013): 98-107.

This work presents an experimental comparison; Using four identical PV, under strictly the same set of technical and meteorological conditions, an experimental comparison of four most used MPPT methods for PV power systems is done. This comparison shows the advantage of use of a MPPT with a variable tracking step.

5.0.8 | **text**[jain2004new]

Jain, Sachin, and Vivek Agarwal. "A new algorithm for rapid tracking of approximate maximum power point in photovoltaic systems." Power Electronics Letters, IEEE 2.1 (2004): 16-19.

This paper presents a new algorithm for tracking maximum power point in photovoltaic systems. This is a fast tracking algorithm, where an initial approximation of MPP quickly achieved using a variable step-size. Subsequently, the exactMPP can be targeted using any conventional method like the hill-climbing or incremental conductance method. Thus, the drawback of a fixed small step-size over the entire tracking range is removed, resulting in reduced number of iterations and much faster tracking compared to conventional methods.

My implementation draws inspiration for the above article for its two-stage algorithm to reduce the number of iterations but deviates significantly in the implementation and algorithms used to identify the MPP

Liu, Yi-Hua, and Jia-Wei Huang. "A fast and low cost analog maximum power point tracking method for low power photovoltaic systems." Solar Energy 85.11 (2011): 2771-2780.

**add TEXT important RESEARCH *

Typically, MPPT methods utilized in medium and high power PV systems uses measured cell characteristics (current, voltage, power) along with an online search algorithm to compute the corresponding MPP. Due to the complexity of the required mathematical operations, a Digital Signal Processor (DSP) or a relatively powerful micro-controller is typically needed, which increases the cost of the system. Moreover, it consumes significant portion of the generated power. Therefore, aMPPT circuit with low-cost and fast-tracking features is essential .

It has already established that there exists a relation between V_{MPP} and V_{OC} in equation 2.12 and is famously used in the FOCV method. However we see that this does not hold true for all illumination conditions and certainly not for low-light(less than 1500 Lux) as compared to higher insolation. Since V_{OC} is a logarithmic function of I_{ph} , the relationship between V_{MP} and I_{MP} .with respect to irradiation is not linear. However, it is possible to linearize this relationship for an interval where the value of V_{OC} is sufficiently insensitive to irradiation. That is, the voltage approximation line (VAL) can be calculated as the tangent line of the MPP locus where the sensitivity of V_{OC} to I_{ph} is lower than a pre-defined threshold. This relationship is illustrated in Figure 5.1 on page 39.

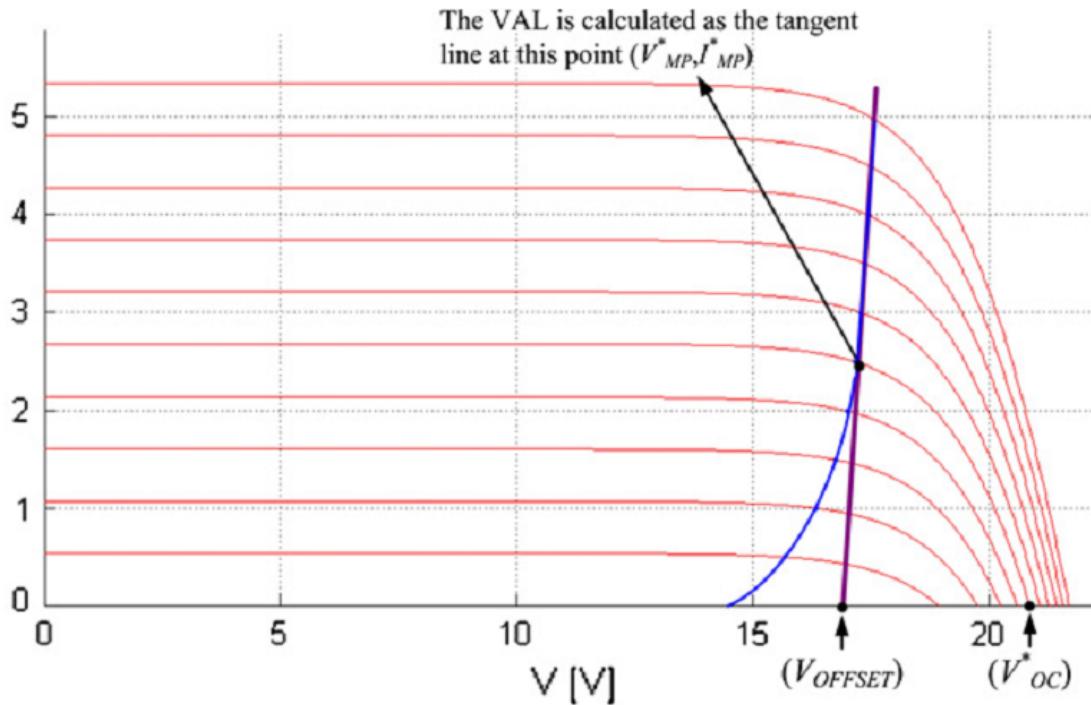


Figure 5.1: I-V curves of the solar panel under different irradiation levels and the voltage approximation line. [liu2011fast]

The same trend can be seen on the I-V curves for the DSCs under test (Figure 5.2).

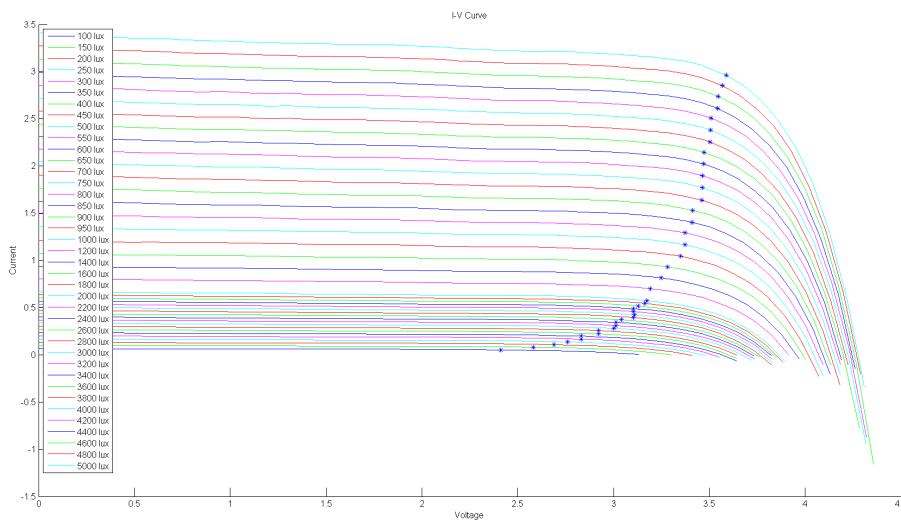


Figure 5.2: Variation of V_{MPP} for different illumination observed **in/on** the DSC under test

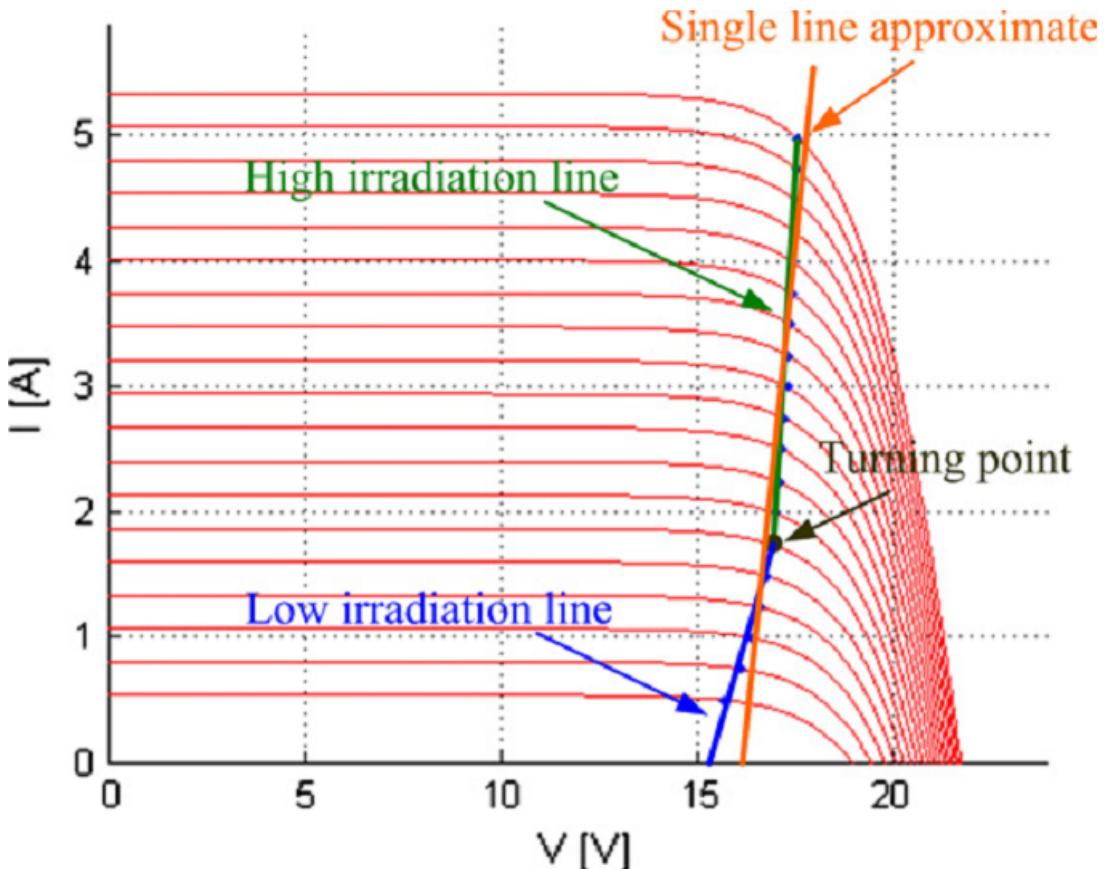


Figure 5.3: Research Cell Efficiency Records [liu2011fast]

insert pictures

5.0.10 | **text**[dondi2008modeling]

Dondi, Denis, et al. "Modeling and optimization of a solar energy harvester system for self-powered wireless sensor networks." Industrial Electronics, IEEE Transactions on 55.7 (2008): 2759-2766.

**Initial modelling strategies were based on this paper, improving the efficiency. # discrete components# **

5.0.11 | **text**[chu2009robust]

Chu, Chen-Chi, and Chieh-Li Chen. "Robust maximum power point tracking method for photovoltaic cells: A sliding mode control approach." Solar Energy 83.8 (2009): 1370-1378.

5.0.12 | **text**[urayai2011single]

Urayai, Caston, and G. Amaratunga. "Single sensor boost converter-based maximum power point tracking algorithms." Applied Power Electronics Conference and Exposition (APEC), 2011 Twenty-Sixth Annual IEEE. IEEE, 2011.

Two new maximum power point tracking algorithms are presented: the input voltage sensor, and duty ratio maximum power point tracking algorithm (ViSD algorithm); and the output voltage sensor, and duty ratio maximum power point tracking algorithm (VoSD algorithm). unlike the incremental conductance algorithm which requires two sensors (the voltage sensor and current sensor), the two algorithms are more desirable because they require only one sensor: the voltage sensor.

5.0.13 | **text**[clark2006power]

Clark, C., and A. Lopez. "Power system challenges for small satellite missions." Proceedings of the 2006 Small Satellites, Systems and Services Symposium, D. Danesy, Ed. The Netherlands: ESA. 2006.

TExt Inspiration for use of multiple power buses