

Aufgabe 1

a) Stationärer Fließprozess um Masse im Reaktor:

$$\dot{m} (h_{\text{ein}} - h_{\text{aus}}) = \dot{Q}_{\text{aus}} + Q_R$$

$$\Rightarrow \dot{Q}_{\text{aus}} = \dot{m} (h_{\text{ein}} - h_{\text{aus}}) + Q_R$$

W/W

$$h_{\text{ein}} (70^\circ\text{C}) = h_f (70^\circ\text{C}) + x \cdot (h_g (70^\circ\text{C}) - h_f (70^\circ\text{C}))$$

Mit Tabelle A-2:

$$= 292,98 + 0,005 (2626,8 - 292,98)$$

$$= 304,65 \frac{\text{kJ}}{\text{kg}}$$

$$h_{\text{aus}} (100^\circ\text{C}) = h_f (100^\circ\text{C}) + x \cdot (h_g (100^\circ\text{C}) - h_f (100^\circ\text{C}))$$

Mit Tabelle A-2:

$$= 419,04 + 0,005 (2676,1 - 419,04)$$

$$= 430,33 \frac{\text{kJ}}{\text{kg}}$$

$$\dot{Q}_{\text{aus}} = 0,3 \frac{\text{kg}}{\text{s}} \left[304,65 \frac{\text{kJ}}{\text{kg}} - 430,33 \frac{\text{kJ}}{\text{kg}} \right] + 100 \text{ kW}$$

=

b) mit $\dot{Q}_{\text{aus}} = 65 \text{ kW}$

Entropiebilanz um Kühlwasserflüssigkeit:

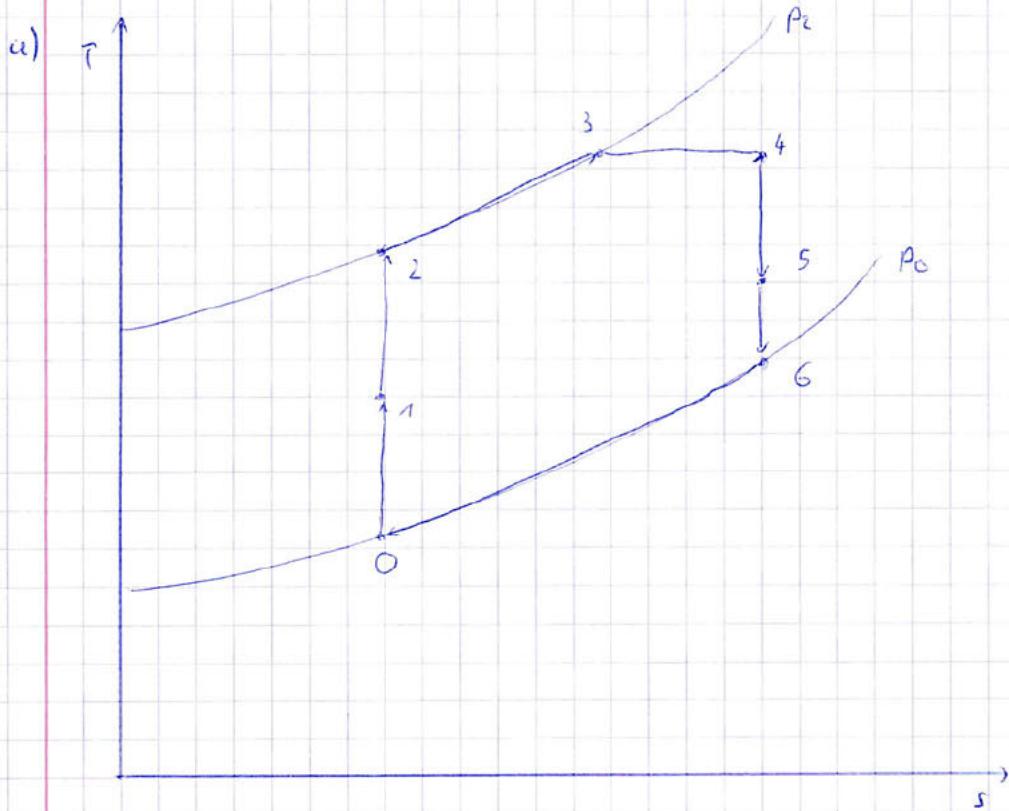
$$\dot{m} (s_{\text{ein}} - s_{\text{aus}}) + \sum \frac{\dot{Q}_i}{T_i} + \dot{S}_{\text{env}}$$

$$\frac{\int_e^u T ds}{s_a + s_e} = \bar{T}$$

c) $O = m [s_{\text{ein}} - s_{\text{aus}}] + \frac{-\dot{Q}_{\text{aus}}}{T} + \frac{\dot{Q}_R}{T} + s_{\text{ev2}}$

d)

Aufgabe 2



b) reversibel adiabate Schubdüse \rightarrow isentrop m.t. $n=1,4$

$$\frac{T_e}{T_s} = \left(\frac{P_e}{P_s} \right)^{\frac{n-1}{n}} \Rightarrow T_e = T_s \left(\frac{P_e}{P_s} \right)^{\frac{n-1}{n}}$$

$$\Rightarrow T_e = 431,9 \left(\frac{0,191}{0,5} \right)^{\frac{1,4-1}{1,4}}$$

$$= 328,07 \text{ K}$$

stationärer Fließprozess um Schubdüse:

$$O = m \left[(h_e - h_a) + \frac{w_e^2 - w_a^2}{2} \right]$$

$$\Rightarrow O = q_s + q_b + \frac{w_s^2 - w_b^2}{2}$$

$$\Rightarrow \frac{w_e^2 - w_s^2}{2} = c_p (T_s - T_e)$$

$$\Rightarrow w_e = \sqrt{2c_p (T_s - T_e) + w_s^2}$$

$$= \sqrt{2 \cdot 1,006 \frac{\text{kg}}{\text{kgK}} (431,9 - 328,07 \text{ K}) + 220 \frac{\text{m}^2}{\text{s}^2}}$$

$$= 507,25 \frac{\text{m}}{\text{s}}$$

$$c) e_{x, \text{str}} = h - h_0 - T_0 (s - s_0) + \cancel{\rho c \ln \frac{T_0}{T} \left(h_e + p_e \right)}$$

$$\Delta e_{\text{str}} = h_0 - h_0 - T_0 (s_0 - s_0) + \left(\frac{w_0^2}{2} - \frac{w_0^2}{2} \right)$$

$$= c_p (T_0 - \bar{T}_0) - \bar{T}_0 \cdot \left(c_p \cdot \ln \frac{T_0}{\bar{T}_0} - R \underbrace{\ln \frac{P_0}{P_0}}_{=0} \right) + \frac{w_0^2}{2} - \frac{w_0^2}{2}$$

$$= 108745 \frac{J}{kg}$$

$$= 108,745 \frac{kJ}{kg}$$

d) Stationärer Fließprozess um ganze Turbine:

$$0 = -\Delta E_{x, \text{str}} + \sum_j \dot{E}_{x, 0,j} - \sum \dot{W}_{t,n} - \dot{E}_{x, \text{vert}}$$

$$\Rightarrow e_{x, \text{vert}} = -\Delta e_{x, \text{str}} + e_{x, 0} - 0$$

Energie des Wärmestroms q_B :

$$\dot{E}_{x, 0} = ((1 - \frac{T_0}{\bar{T}}) \dot{Q}) , \quad Q_B = q_B \cdot m_K$$

$$\rightarrow m e_{x, 0} = (1 - \frac{T_0}{\bar{T}}) \cdot q_B \cdot m_K$$

$$\Rightarrow e_{x, 0} = \left(1 - \frac{-30-273,15K}{1289K} \right) \cdot 1195 \frac{kJ}{kg}$$

$$= 969,58 \frac{kJ}{kg}$$

$$\Rightarrow e_{x, \text{vert}} = -108,745 + 969,58$$

$$= 860,835 \frac{kJ}{kg}$$

Aufgabe 3

a) $p_{\text{ig}} = p_{\text{amb}} + p_{\text{ew}} + p_k$

$$p_{\text{amb}} = 1 \text{ bar} = 10^5 \text{ Pa}$$

$p_{\text{ew}} =$

Fläche der Membran und des Kolbens.

$$A = 2\pi r^2 = 2 \cdot \pi \cdot 0,05^2$$

$$= 0,0157 \text{ m}^2$$

$$p_{\text{ew}} = \frac{F}{A} = \frac{0,1 \cdot 9,81}{0,0157} = 62,48 \text{ Pa}$$

$$p_k = \frac{F}{A} = \frac{32 \cdot 9,81}{0,0157} = 19994,90 \text{ Pa}$$

$$\begin{aligned} p_{\text{ig}} &= 10^5 \text{ Pa} + 62,48 \text{ Pa} + 19994,9 \text{ Pa} \\ &= 120057,38 \text{ Pa} \\ &\approx 1,2 \text{ bar} \end{aligned}$$

perfektes Gas: $pV = mRT \Rightarrow m = \frac{pV}{RT}$

$$R = \frac{\bar{R}}{M} = \frac{8,314}{50} = 0,16628$$

$$m = \frac{120057,38 \text{ Pa} \cdot 0,00316 \text{ m}^3}{0,16628 \frac{\text{J}}{\text{kg K}} \cdot (500+273,15) \text{ K}}$$

$$= 2,93 \text{ g}$$

$$= 2,93 \text{ g}$$

b) p_{ig}

c) Innere Energie des Gases:

$$\begin{aligned}\Delta U &= m u_2 - m u_1 \\&= m (u_2 - u_1) \\&= m \cdot c_v (T_2 - T_1) \\&= 0,00293 \text{ kg} \cdot 0,633 \frac{\text{J}}{\text{kgK}} \cdot (0,003 + 273,15 - (500 + 273,15) \text{ K}) \\&= -0,927 \text{ J}\end{aligned}$$

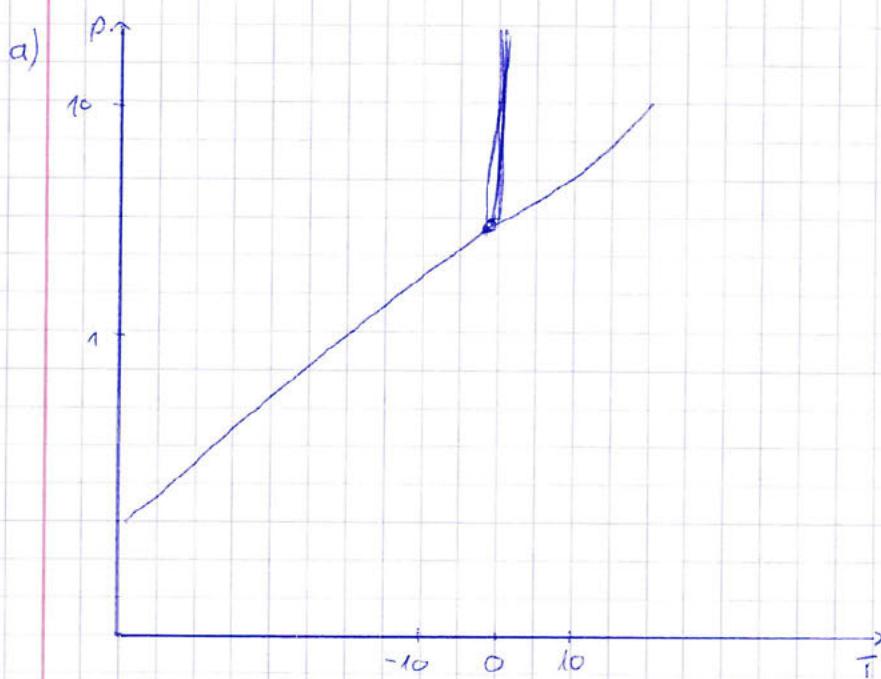
$$W_{v1,2} = m \int_{T_1}^{T_2} p \, dv$$

$$n = \frac{c_p k_u}{c_v} = \frac{R + c_v}{c_v}$$

~~$\int_{T_1}^{T_2} \frac{dp}{R + cp}$~~ = 1,263

$$\begin{aligned}W_{v1,2} &= m \int_{T_1}^{T_2} \frac{R(T_2 - T_1)}{1 - n} \\&= 0,926 \text{ J}\end{aligned}$$

Aufgabe 4



b) Flüssig process um Verdichter:

$$m(h_1 - h_3) \neq -w_k = 0$$

$$\Rightarrow m = \frac{w_k}{h_1 - h_3}$$

isenthalpe Drossel: $h_4 = h_1$

$$p_3 = p_4$$

$$\Rightarrow h_1 = h_4 = h_f \text{ (8 bar)}$$

$$= 93,42 \frac{\text{kJ}}{\text{kg}} \text{ (Tabelle A-11)}$$

$$c) m(l_4 - l_1) = 0$$

$$\Rightarrow l_4 = l_1$$

$$\Rightarrow \text{fl}_4 \approx l_1 = \cancel{162,88} \frac{l_2}{l_3} \quad \text{m.t. Tabelle A-11}$$

93,42

$$T_4 = T_1$$