a) Energie bilanz für stationäres System:

$$dE^{0} = 2m \ln(t) + ke; \tau pet + EQ - EW$$
 $0 = m (hein - kous) + EQ - EW$
 $Q = m (hans - kein)$

A

a) Energie bilanz für stationäres System

 $0 = m (hein - kaus) + EQ - EW$
 $Q = m (hein - kaus) + EQ - EW$
 $Q = m (hous - hein) + 10064$

A-2

b) (mit Quus = 6
$$\Gamma$$
 EW)

$$T = \int_{Sa-Se}^{a} T ds$$

$$= \int_{Sa-Se}^{a} \frac{dH}{dt} - \int_{Sa-Se}^{a} \frac{dT}{dt} = \frac{e^{-t} \cdot T_{u} - T_{e}}{e^{t} \cdot T_{e}}$$

$$= \int_{Sa-Se}^{a} \frac{dH}{dt} - \int_{Sa-Se}^{a} \frac{dT}{dt} = \frac{e^{-t} \cdot T_{u} - T_{e}}{e^{t} \cdot T_{e}}$$

$$= \frac{288 \cdot 15}{(a)(\frac{298 \cdot 15}{289 \cdot 15})} = 293.12 K_{u}$$

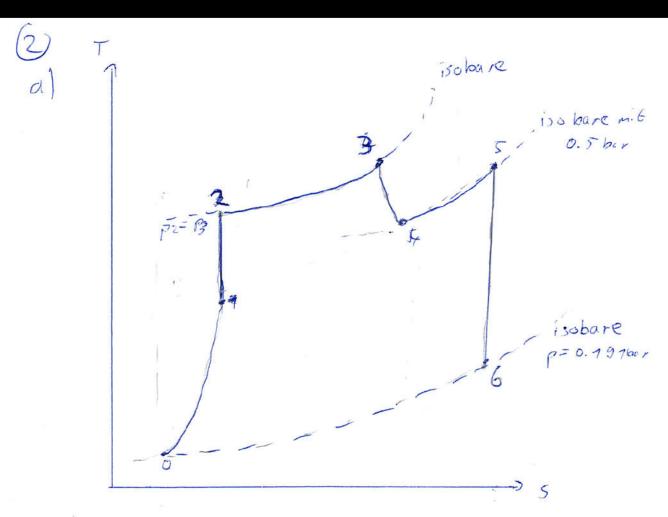
c) stationairer Flie Aprozess:

$$0 = m(s_e - s_a) + EQ + Serz$$

=) Serz = $m(s_a - s_e) - Quu$

d) Halboffenes System

$$m_2 \cdot u_2 - m_1 \cdot u_1 + \Delta KE + DPZ = \sum \Delta m_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{2}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i \cdot (u_i + \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2}) + \sum \Delta u_i$$



b) Schub düse = isemt rop

$$T_6 = \left(\frac{p_6}{p_5}\right)^{\frac{1}{n-1}} = 3 T_6 = T_5 \left(\frac{p_6}{p_5}\right)^{\frac{1}{n-1}}$$

$$T_6 = 431.9 \times \left(\frac{0.791bar}{0.5bar}\right)^{\frac{1}{n-1}} = 328.075 \times 10^{-1}$$

$$stat FP:$$

$$0 = m(L_5 - L_6 + \frac{w_5^2 - w_6^2}{2}) + 50^7 - 50^7$$

$$= \sqrt{2(L_5 - L_6) + w_5^2}$$

$$= \sqrt{2 \cdot C_p(T_5 - T_6) + 70^3 + (220m/s)^2}$$

$$= 507.24 m/s$$

$$= (h_6 - h_0 - T_0(s_6 - s_0) + \frac{w_6^2}{2} - \frac{w_0^2}{2})$$

$$= c_p^{19}(T_6 - T_0) - T_0(c_p \cdot l_n(\frac{T_6}{T_0}) - R \cdot l_n(\frac{F_6}{P_0}) + \frac{w_6}{2} - \frac{w_0^2}{2}$$

$$= T_6 = 2328.07T \times T_0 = 2 \times 3.75 \times 6$$

$$c_p = 7.006 \quad w_s = 507.28 \text{ m/s} \quad w_0 = 200 \text{ m/s}$$

A) From

$$e_{xverL} = -\Delta e_{xx} + (1 - \frac{T_0}{T_0}) - q_b$$
 $= 848.78 \text{ kf}$
 $= 848.78 \text{ kf}$

a) prod Pan - mew of + mk. g + Pamb. Pay = me + mx og + Pamb = 0.7/cq + 32thg . 4-9.81m/s2 + 1.705 N/m = 1.40 bar PV=mRT=> m= PV. Mw = 1.4.702 KPa - 3.74.70-3m3 - 50 100 kmei = 3.664 9/ b) Druck bleist Konstant pag = 160 Gar

IZ= FM W =

Druck bleist konstant bei pzig = 1.40bar was sich durch die oben genutzte Formel was sich durch die oben genutzte Formel für Pra erklären lässt, denn es verändern sich köhe der derg genutzten Größen.

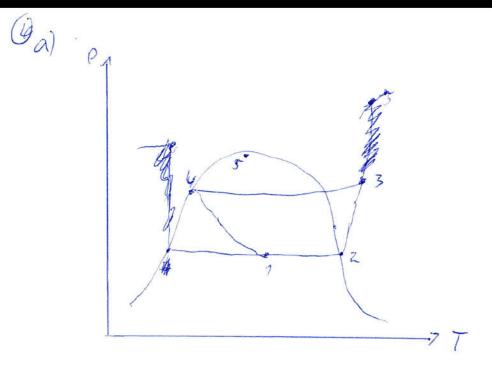
$$m_{\nu}(u_2 - u_1) + m_{\underline{c}} \cdot (\overline{T_2} - \overline{T_1}) = Q$$
 $m_{\overline{c}} \cdot (u_2 - u_1) + m_{\underline{c}} \cdot (\overline{T_1} - \overline{T_2}) = Q$
 $m_{\overline{c}} \cdot (u_2 - u_1) + m_{\underline{c}} \cdot (\overline{T_1} - \overline{T_2}) = Q$

$$u_1 = U_F \tilde{u}_{5} \tilde{s}_{1} \tilde{g}_{1} + \chi_{E;_{5,7}} \left(u_{fest} - u_{f} \tilde{u}_{5} \tilde{s}_{1} \tilde{g}_{1} \right)$$

$$= -3.0 \, 45 + 0.6 \left(-333.4 \, 49 + 0.045 \right) = -760.09 \, \frac{k_{5}}{k_{5}}$$

$$u_{2} = -700.09 \, \frac{k_{5}}{k_{5}} + \frac{7.5 \, k_{5}}{0.1 \, k_{5}} = -785.09$$

• \$



 $\frac{5}{5} = \frac{5}{3}$ is antrop

Zu stand	·p(bur]	IT	×	15	1.	
1					147	
7			1	12-17		
3	8					
4	8		0		h-hy	

=) X3=

A-17: hy=hf(8621) = 93.42/ff = h1

c) $7_2 = 22^{\circ}$ C m = 4/cf $k_1 = \frac{h_2 - h_4}{h_8 - h_4}$ $k_2 = 26/c + 3 \frac{c_4}{l_2}$ $T_2 = 22^{\circ}$ C $P_2 = \frac{(6.4566 - 1.706)^{10}}{(24 - 20)^{\circ}}(22 - 20)^{\circ}$ + 5. 7. 16 $= 6.0863 km^{\circ} 6 \text{ for}$ $h_4 = 6.0863 km^{\circ} 6 \text{ for}$

x= 0.0776

 $d) = \frac{|Q_{zq}|}{|w_{t}|} = \frac{|Q_{k}|}{|w_{k}|} = \frac{|Q_{k}|}{|w_$

hz = 258.36+260.45 let = 259.41 leg