

Wolfgang Torge
Jürgen Müller

Geodesy

4th Edition

DE GRUYTER

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Preface to the Fourth Edition

The origin of this introductory textbook goes back to the booklet “Geodäsie”, prepared by the first author and published in 1975 by Walter de Gruyter and Co. The English translation (1980) was well accepted by the geodetic and surveying community, which led to revised and extended editions in 1991 and 2001, as well as to translations into Spanish, Chinese, and Greek. Recognizing the continuing interest in the “Geodesy”, the publisher and the authors, both professors at the Institut für Erdmessung (IfE), Leibniz Universität Hannover, decided to prepare a fourth edition which is presented here. It is based on the third edition, and keeps the basic subdivision into eight chapters. An extensive revision was necessary in the chapters dealing with reference systems, methods of measurement and modeling, and geodetic contribution to recent geodynamics research. This reflects the central role which geodesy has achieved in the past 10 years, within the joint effort of the geosciences at monitoring and interpreting the global change of our planet. The Global Geodetic Observing System established by the International Association of Geodesy represents the outstanding example for the geodetic part of this interdisciplinary concert, with an overwhelming contribution of geodetic space techniques.

The “Introduction” again contains the definition and an overview of about 2000 years of the history of geodesy, with the current change to a four-dimensional concept, and strong connections to astronomy, physics, and the other geosciences. The chapter on “Reference Systems and Reference Frames” has been revised thoroughly. It includes the recent definition and realization of celestial and terrestrial reference systems, and emphasizes the fundamental role of Earth’s rotation. Updating of “The Gravity Field of the Earth” concentrated on the geoid and mean sea level, with discussion of the manifold problems at realizing these surfaces. Only minor changes were necessary in the chapter on “The Geodetic Earth Model”, which now also contains some definitions and parameters for optimum Earth models. The chapters on “Methods of Measurement” and “Methods of Positioning and Gravity Field Modeling” again comprise the core of the book, and required extensive revision and completion. This is due to the overwhelming contribution of geodetic space methods in solving the three basic problems of geodesy, i.e., the determination of the surface, the gravity field, and the rotation of the Earth. Sufficient space has been given to the description of Global Navigation Satellite Systems like GPS and to sophisticated space systems such as laser ranging and Very Long Baseline Interferometry, the successful gravity space missions are also explained in more detail. The present state of terrestrial positioning and gravimetry is again discussed in some detail, as these methods still play an important role on a local scale, and serve for densification and validation of satellite-derived results. The progress in gravity field modeling is demonstrated by some examples of recent global and local gravity field models, including GRACE- and GOCE-based satellite models, the Earth Gravitational Model EGM2008, and gravimetric geoid models for the U.S.A. and for Europe. The transition from classical geodetic control networks

to three-dimensional reference frames embedded in the global terrestrial reference system is treated in the chapter on “Geodetic and Gravimetric Networks”, where the impact of absolute gravimetry on the establishment of gravity networks also becomes visible. The final chapter “Structure and Dynamics of the Earth” had to be extended significantly, in order to adequately consider the geodetic contribution to the investigation and modeling of geodynamic processes of global to local scale. The present state of research is shown by several case studies, referring to, e.g., sea level change, glacial isostatic adjustment, plate tectonics, seismic and volcanic activity, hydrological circulation, and Earth tides.

The text is illustrated by numerous figures, depicting either fundamental relations, or showing geodetic techniques, reference systems, gravity field models and examples of geodynamics research. The book’s revision led to a volume increase of about 25%, the number of figures (now partly in color) increased even more. The reference list contains more than 900 entries, with about 500 of them published since 2000.

The book is especially addressed to graduate students in the fields of geodesy, geophysics, surveying engineering, and geomatics, as well as to students of terrestrial and space navigation. It should also serve as a reference for geoscientists and engineers facing geodetic problems in their professional work.

The contents of the book are partly based on lectures given by the authors at the Leibniz Universität Hannover, Germany, and on guest lectures given abroad. The authors are indebted to individuals and institutions for providing illustrations, due credit is given in the figure captions. Valuable information on dedicated problems was given by Prof. Matthias Becker, Technische Universität Darmstadt, Prof. Christopher Jekeli, Ohio State University, Dr. Corinna Kröner, PTB Braunschweig, Dipl.-Ing. Alexander Schunert, Institut für Photogrammetrie und GeoInformation, Leibniz Universität Hannover, and Prof. Florian Seitz, Technische Universität München. The staff of the Institut für Erdmessung assisted in manifold ways, by discussion and by preparing geodetic products. We especially mention Dipl.-Ing. Philip Brieden, Dr.-Ing. Heiner Denker, Prof. Jakob Flury, Dr.-Ing. Olga Gitlein, Prof. Steffen Schön, Dr.-Ing. Ludger Timmen, and Dr.-Ing. Sybille Vey. M.Sc. Manuel Schilling handled the technical preparation of the manuscript, and assisted in text storage and proof-reading. All this is gratefully acknowledged. The good cooperation with the publisher, proven over nearly 40 years association, continued, cordial thanks go to Dr. Christoph von Friedeburg, Mrs. Hella Behrend, Mrs. Sabina Dabrowski, and the staff at De Gruyter. Finally, our gratitude goes to our wives Renate and Sieglinde for their understanding and continuous encouragement, especially during the last year of increased activity.

Wolfgang Torge, Jürgen Müller
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1 Introduction

1.1 Definition of geodesy

According to the classical definition of Friedrich Robert Helmert (1880), “*geodesy* ($\gamma\eta$ = Earth, $\delta\alpha\omega$ = I divide) *is the science of the measurement and mapping of the Earth’s surface.*” Helmert’s definition is fundamental to geodesy even today. The surface of the Earth, to a large extent, is shaped by the Earth’s gravity, and most geodetic observations are referenced to the Earth’s gravity field. Consequently, the above definition of geodesy includes the determination of the Earth’s *external gravity field*. Since ancient times, the reference system for the survey of the Earth has been provided by extraterrestrial sources (stars). This demands the Earth’s orientation in space to be implied into the focus of geodesy. In recent time, the objective of geodesy has expanded to include applications in ocean and space research. Geodesy, in collaboration with other sciences, is also now involved in the determination of the surfaces and gravity fields of *other celestial bodies*, such as the moon (lunar geodesy) and planets (planetary geodesy). Finally, the classical definition has to be extended to include *temporal variations* of the Earth’s figure, its orientation and its gravity field.

With this extended definition, geodesy is part of the *geosciences* and *engineering sciences*, including navigation and geomatics (e.g., Nat. Acad. Sciences, 1978; Herring, 2009; Plag and Pearlman, 2009). Geodesy may be divided into the areas of global geodesy, geodetic surveys (national and supranational), and plane surveying. *Global geodesy* includes the determination of the shape and size of the Earth, its orientation in space, and its external gravity field. A *geodetic survey* deals with the determination of the Earth’s surface and gravity field over a region that typically spans a country or a group of countries. The Earth’s curvature and gravity field must be considered in geodetic surveys. In *plane surveying* (topographic surveying, cadastral surveying, engineering surveying), the details of the Earth’s surface are determined on a local level, and thus curvature and gravity effects are most often ignored.

There is a close relation between global geodesy, geodetic surveying, and plane surveying. Geodetic surveys are linked to reference frames (networks) established by global geodesy, and they adopt the parameters for the figure of the Earth and its gravity field. On the other hand, the results of geodetic surveys contribute to global geodesy. Plane surveys, in turn, are generally referenced to control points established by geodetic surveys. They are used extensively in the development of national and state map-series, cadastral and geoinformation systems, and in civil engineering projects. The measurement and data evaluation methods applied in national geodetic surveys nowadays mostly are similar to those used in global geodetic work. In particular, space methods (satellite geodesy) which have long been a dominant technique in global geodesy, are now also commonly employed in regional and local surveys. This also requires a more detailed knowledge of the gravity field at regional and local scales.

With the corresponding classification in the English and French languages, the concept of “*geodesy*” (la géodésie, “*höhere Geodäsie*” after *Helmert*) in this text

refers only to global geodesy and geodetic surveying. The concept of “*surveying*” (la topométrie, Vermessungskunde or “niedere Geodäsie” after Helmert) shall encompass plane surveying.

In this volume, geodesy is treated only in the more restrictive sense as explained above (excluding plane surveying), and is limited to the planet Earth. Among the numerous textbooks on surveying we mention Anderson and Mikhail (1998), Johnson (2004), and Kahmen (2006). For lunar and planetary geodesy see Nothnagel et al. (2010, p. 53 ff.) with respect to reference systems, and Wieczorek (2007) for gravity fields, see also Zumberge et al. (2009). Numerical values of astrometric and geodetic parameters are given by Yoder (1995) and Shirley and Fairbridge (1997, sections on gravitation and gravity field of the terrestrial planets). For the planet Earth, we refer to Groten (2004) and Petit and Luzum (2010).

1.2 The objective of geodesy

Based on the concept of geodesy defined in [1.1], the objective of geodesy with respect to the planet Earth may be described as follows:

“The objective of geodesy is to determine the figure and external gravity field of the Earth, as well as its orientation in space, as a function of time, from measurements on and exterior to the Earth’s surface.”

This *geodetic boundary-value problem* incorporates a geometric (figure of the Earth) and a physical (gravity field) part; both are closely related.

By the *figure of the Earth* we mean the physical and the mathematical surface of the Earth as well as a geodetic reference model (e.g., Moritz, 1990).

The *physical surface* of the Earth is the border between the solid or fluid masses and the atmosphere. The *ocean floor* may be included in this definition, being the bounding surface between the solid terrestrial body and the oceanic water masses. The irregular surface of the solid Earth (continental and ocean floor topography) cannot be represented by a simple mathematical (analytical) function. Continental topography is therefore described point wise by *coordinates of control* (reference) *points*. Given an adequately dense control network, the detailed structure of this surface can be determined by interpolation of data from spatial and terrestrial topographic and photogrammetric surveying and from hydrographic surveys (e.g., Kraus and Schneider, 1988/90; Hake et al., 2002; McGlone et al., 2004; Luhmann et al., 2006; Kraus, 2007; Konecny, 2009). On the other hand, the *ocean surface* (70% of the Earth’s surface) is easier to represent. If we neglect the effects of ocean currents and other “disturbances” like ocean tides, it forms a part of a level or equipotential surface of the Earth’s gravity field (surface of constant gravity potential). We may think of this surface as being extended under the continents and identify it as the *mathematical figure of the Earth*, which can be described by a condition of equilibrium (Helmert, 1880/1884). J. B. Listing (1873) designated this level surface as *geoid*.

The great mathematician, physicist, astronomer and geodesist Carl Friedrich Gauss (1777–1855) had already referred to this surface: “*Was wir im geometrischen Sinn Oberfläche der Erde nennen, ist nichts anderes als diejenige Fläche, welche überall die Richtung der Schwere senkrecht schneidet, und von der die Oberfläche des Weltmeers einen Theil*

ausmacht...", which reads in English translation: "What we call surface of the Earth in the geometrical sense is nothing more than that surface which intersects everywhere the direction of gravity at right angles, and part of which coincides with the surface of the oceans" (C. F. Gauss: Bestimmung des Breitenunterschiedes zwischen den Sternwarten von Göttingen und Altona, Göttingen 1828. C. F. Gauss Werke, Band IX, Leipzig 1903, p. 49, see also Moritz, 1977).

The description of the external gravity field including the geoid represents the physical aspect of the problem of geodesy. In solving this problem, the Earth's surface and the geoid are considered as bounding surfaces in the Earth's gravity field. Based on the law of gravitation and the centrifugal force (due to the Earth's rotation), the *external gravity field* of the Earth can be modeled analytically and described by a large number of model parameters. A geometric description is given by the infinite number of *level surfaces* extending completely or partially exterior to the Earth's surface. The geoid as a physically defined Earth's figure plays a special role in this respect.

Reference systems are introduced in order to describe the orientation of the Earth in space (celestial reference system) as well as its surface geometry and gravity field (terrestrial reference system). The definition and realization of these systems has become a major part of global geodesy; the use of three-dimensional Cartesian coordinates in Euclidean space is adequate in this context. However, due to the demands of users, *reference surfaces* are introduced. We distinguish between curvilinear surface coordinates for horizontal positioning, and heights above some zero-height surface for vertical positioning. Because of its simple mathematical structure, a rotational *ellipsoid*, flattened at the poles, is well suited for describing horizontal positions, and consequently it is used as a reference surface in geodetic surveying. In plane surveying, the *horizontal plane* is generally a sufficient reference surface. Because of the physical meaning of the geoid, this equipotential surface is well suited as a reference for heights. For many applications, a *geodetic reference Earth* (Earth model, normal Earth) is needed. It is realized through a *mean-Earth ellipsoid* that optimally approximates the geometry (geoid) and the gravity field of the Earth. Fig. 1.1 shows the mutual location of the surfaces to be determined in geodesy.

The body of the Earth, its gravity field and its orientation are subject to *temporal variations* of secular, periodic, and episodic nature; these changes can occur globally, regionally, and locally. Geodetic measurement and evaluation techniques are now able to detect partly these variations to a high level of accuracy. Accordingly, geodetic

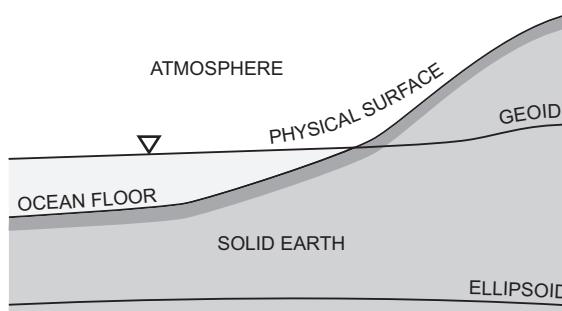


Fig. 1.1: Physical surface of the Earth, geoid, and ellipsoid.

observations and derived parameters must be considered as time-dependent quantities. If time-independent results are required, the observations must be corrected for temporal variations, and the final results have to be referred to a specified epoch. On the other hand, by determining temporal variations, geodesy contributes to the investigation of the kinematics and dynamics of the Earth.

1.3 Historical development of geodesy

The formulation of the objective of geodesy as described in [1.2] did not fully mature until the nineteenth century. However, the question of the figure of the Earth was contemplated already in antiquity. In fact, geodesy together with astronomy and geography are among the oldest sciences dealing with the planet Earth. Superseding the use of the *sphere* as a model for the Earth [1.3.1], the oblate *rotational ellipsoid* became widely accepted as the model of choice in the first half of the eighteenth century [1.3.2]. The significance of the *gravity field* was also recognized in the nineteenth century, leading to the introduction of the geoid [1.3.3]. In the second half of the twentieth century, satellite techniques permitted the realization of the *three-dimensional* concept of geodesy [1.3.4]. At the same time, a drastic increase in the accuracy of geodetic observations required that time variations be taken into account. This led to the concept of *four-dimensional* geodesy [1.3.5].

Extensive material on geodetic history is found in Todhunter (1873), Perrier (1939), Fischer (1975), Bialas (1982), and Smith (1986), while Levallois (1988) and Torge (2009) concentrate on the history of geodesy in France and in Germany, respectively.

1.3.1 The spherical Earth model

Various opinions about the figure of the Earth prevailed in the past, e.g., the notion of an *Earth disk* encircled by oceans (*Homer's Iliad* around 800 B.C., *Thales of Milet* about 600 B.C.). Considering the sphere aesthetically appealing, *Pythagoras* (around 580–500 B.C.) and his school proposed a spherical shaped Earth. By the time of *Aristotle* (384–322 B.C.), the spherical concept was generally accepted and even substantiated by observations. For example, observers noted the round shadow of the Earth in lunar eclipses and the apparent rising of an approaching ship at the horizon. In China the spherical shape of the Earth was also recognized in the first century A.D.

Eratosthenes of Alexandria (276–195 B.C.) was the first who, based on the assumption of a spherical Earth, deduced the Earth's radius from measurements (Schwarz, 1975; Lelgemann, 2010); he is often regarded as the founder of geodesy. The principle of the *arc-measurement* method developed by him was applied until modern times: from geodetic measurements, the length ΔG of a meridian arc (or any other great circle) is determined; astronomical observations furnish the associated central angle ψ (Fig. 1.2). The radius of the Earth is then given by

$$R = \frac{\Delta G}{\psi}. \quad (1.1)$$

Eratosthenes found that the rays of the sun descended vertically into a well in Syene (modern day Assuan), at the time of the summer solstice. Whereas in Alexandria

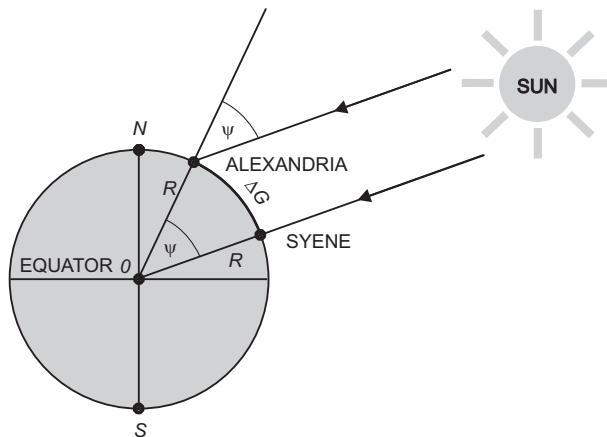


Fig. 1.2: Arc measurement of Eratosthenes.

(approximately on the same meridian as Syene), the sun's rays formed an angle with the direction of the plumb line. From the length of the shadow of a vertical staff ("gnomon") produced in a hemispherical shell ("skaphe"), Eratosthenes determined this angle as 1/50 of a complete circle, i.e., $\psi = 7^\circ 12'$ (Lelgemann, 2000). From Egyptian cadastre maps, which were based on the information of "bematists" (step counters), Eratosthenes probably estimated the distance from Syene to Alexandria to be 5000 stadia. With the length of the Eratosthenes stadium assumed as 158.7 m (Egyptian norm), the Earth's radius is computed to be about 6300 km, which is close to the real value of 6370 km. Another ancient determination of the Earth's radius is attributed to *Posidonius* (135–51 B.C.). Using the (approximate) meridian arc from Alexandria to Rhodes, he observed the star Canopus to be on the horizon at Rhodes, while at a culmination height of $7^\circ 30'$ at Alexandria, this again corresponds to the central angle between the two sites. *Klaudios Ptolemaios* (around 100–160 A.D.) finally established the geocentric world system of *Aristotle*, by fundamental publications on astronomy (commonly cited with the Arabian naming "Almagest") and geography ("Geographike hyphegesis"). These works included star catalogs, maps and lists with geographical coordinates of many places; they dominated the view of the world until the beginning of modern times (e.g. Kleinberg et al., 2011).

During the middle ages in Europe, the question of the figure of the Earth was not pursued further, although the knowledge of the Earth's spherical shape was not lost and especially kept in the monasteries. Documentation from China shows that an astrophysical-geodetic survey between the 17° and 40° latitude was carried out by the astronomers *Nankung Yüeh* and *I-Hsing* c. 725 A.D. in order to determine the length of a meridian. A meridian arc of 2° extension was measured directly with ropes by the Arabs (c. 827 A.D.) northwest of Bagdad, during the caliphate of *Al-Mámún*. At the beginning of the modern age, the French physician *J. Fernel* (1525) described an arc measurement between Paris and Amiens, at which the geographical latitudes were determined using a quadrant, and the length of the arc was computed from the number of rotations of a wagon wheel.

Later arc measurements based on the spherical Earth model benefited from fundamental advances in instrumentation technology, especially by the invention of the

telescope in the Netherlands (c. 1600), and its modification and application in astronomy by *Galilei* and *Kepler* (1610/1611). Equally important was the progress in methodology by the development of the *triangulation*. With this method, the hitherto tedious and inaccurate direct length measurement or even estimation of a spherical arc was replaced by an indirect procedure. The angles in a chain of triangles following the arc (triangulation network) were observed with angle measuring devices of high precision (the quadrant and later the theodolite), and the scale of the network was derived from one (or more) short baselines measured with high precision. With proper reduction of the observations to the meridian, the length of the arc then is provided by trigonometric formulae, cf. [7.1]. After the initial application of *triangulation* by *Gemma Frisius* (1508–1555) in the Netherlands, and by *Tycho Brahe* (1546–1601) in Denmark, the Dutchman *Willebrord Snell van Royen*, called *Snellius* (1580–1626), conducted a first triangulation (1614/15) in order to determine the radius of the Earth from the meridian arc between Bergen op Zoom and Alkmaar (Holland), (Haasbroek, 1968).

Although triangulation combined with astronomic positioning soon proved as an economic and accurate method of arc measurement, other strategies for determining the Earth radius were also pursued. *A. Norwood*, for example, still employed a direct length measurement using a chain when determining the meridian arc between London and York (1633–1635). The method of *reciprocal zenith angles* is another technique that has been used to determine the central angle between points on a meridian arc. Already proposed by *Kepler* (1607), the Italian priests *F. Grimaldi* and *G. B. Riccioli* used this method in 1645, between Bologna and Modena (Fig. 1.3). The central angle may be computed from the zenith angles z_1 and z_2 observed at locations P_1 and P_2 according to

$$\psi = z_1 + z_2 - \pi. \quad (1.2)$$

This procedure makes an arc measurement independent of astronomic observations, but it does not yield satisfactory results due to the inaccurate determination of the curvature of light rays (refraction anomalies) affecting the observed zenith angles.

Through the initiative of the French Academy of Sciences (founded in Paris, 1666), France assumed the leading role in geodesy in the seventeenth and eighteenth centuries.

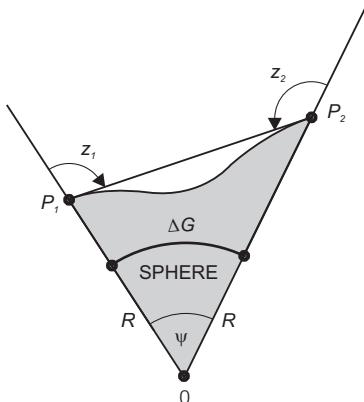


Fig 1.3: Central angle and reciprocal zenith angles.

In 1669/70 the French abbot *J. Picard* measured the meridian arc through Paris between Malvoisine and Amiens with the aid of a triangulation network; he was the first to use a telescope with cross hairs as part of the quadrant employed for the measurement of the angles. The value Picard obtained for the radius of the Earth (deviation from the exact value only +0.01%) aided *Newton* in the verification of the law of gravitation, which he had formulated already in 1665/66.

1.3.2 The ellipsoidal Earth model

In the sixteenth and seventeenth centuries, new observations and ideas from astronomy and physics decisively influenced the perception of the figure of the Earth and its position in space. *Nicolaus Copernicus* (1473–1543) achieved the transition from the *geocentric* universe of *Aristotle* and *Ptolemy* to a *heliocentric* system (1543: "De revolutionibus orbium coelestium"), which *Aristarchos of Samos* (about 310–250 B.C.) had already postulated. *Johannes Kepler* (1571–1630) discovered the laws of planetary motion (1609: "Astronomia nova...", 1619: "Harmonices mundi"), in which the planets followed elliptical orbits in a systematic manner. Finally, *Galileo Galilei* (1564–1642) established the fundamentals for mechanical dynamics (law of falling bodies and law of pendulum motion), and strengthened the idea of a heliocentric world system by a multitude of astronomic observations of high accuracy. Being a strong advocate of the new system, he decisively contributed to its final success, notwithstanding the long-lasting opposition of the Catholic Church.

In 1666, the astronomer *J. D. Cassini* observed the flattening of the poles of Jupiter. On an expedition to Cayenne to determine martian parallaxes (1672/73), the astronomer *J. Richer* discovered that a one-second pendulum regulated in Paris needed to be shortened in order to regain oscillations of one second. From this observation, and on the basis of the law of pendulum motion, one can infer an increase in gravity from the equator to the poles. This effect was confirmed by the English astronomer *E. Halley* when comparing pendulum measurements in St. Helena to those taken in London (1677/78).

Founded on these observations and his theoretical work on gravitation and hydrostatics, *Isaac Newton* (1643–1727) developed an Earth model based on physical principles, and presented it in his famous "Philosophiae Naturalis Principia Mathematica" (1687). Based on the law of gravitation, Newton proposed a rotational ellipsoid as an equilibrium figure for a homogeneous, fluid, rotating Earth. The flattening

$$f = \frac{a - b}{a} \quad (1.3)$$

(with semi-major axis a and semi-minor axis b of the ellipsoid) of Newton's ellipsoid was 1/230. He also postulated an increase in gravity acceleration from the equator to the poles proportional to $\sin^2\varphi$ (geographical latitude φ). At the same time, the Dutch physicist *Christian Huygens* (1629–1695), after having developed the principle of the pendulum clock and the law of central motion, also calculated an Earth model flattened at the poles ("Discours de la Cause de la Pesanteur," 1690). Shifting the source of the Earth's attractive forces to the center of the Earth, he obtained a rotationally-symmetric equilibrium-surface with a meridian curve of fourth order and flattening of 1/576.

Arc measurements at various latitudes were now required to verify the proposed ellipsoidal Earth-models. Theoretically, the length of a 1° arc (meridian arc for a difference

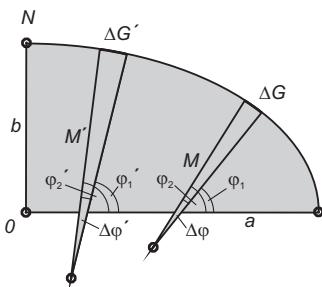


Fig. 1.4: Latitude arc measurement.

of 1° in latitude), in the case of flattened poles, should increase pole-ward from the equator. The ellipsoidal parameters a, b or a, f then can be computed from two arc measurements.

We distinguish between arc measurements along an ellipsoidal meridian (latitude arc measurement), along a parallel (longitude arc measurement), and arc measurements oblique to the meridian.

For the computations in a *latitude arc measurement* (Fig. 1.4), the angles $\Delta\varphi = \varphi_2 - \varphi_1$ and $\Delta\varphi' = \varphi'_2 - \varphi'_1$ are formed from the observed geographical latitudes $\varphi_1, \varphi_2, \varphi'_1$ and φ'_2 . The corresponding meridian arcs ΔG and $\Delta G'$ are obtained from triangulation networks. For short arcs, one can replace the meridian ellipse by the osculating circle having the meridian radius of curvature $M = M(\varphi)$ evaluated at the mean latitude $\varphi = \frac{1}{2}(\varphi_1 + \varphi_2)$, where M is also a function of the ellipsoidal parameters a, f . From $\Delta G = M\Delta\varphi$ and $\Delta G' = M'\Delta\varphi'$, a and f may be determined. The larger the latitude interval $\varphi' - \varphi$, the more accurate the computed flattening; whereas, the accuracy of the semi-major axis length a depends in particular on the lengths of the meridian arcs.

For *longitude arc measurements*, corresponding relations are used between the arc lengths measured along the parallels and the difference of the geographical longitudes observed at the end points of the arcs. Arc measurements *oblique to the meridian* require a proper azimuth determination for reduction to the meridian.

Initial evaluations of the older arc measurements (*Snellius, Picard*, among others) led to an Earth model elongated at the poles. The same result was obtained by *La Hire, J. D.* and *J. Cassini*. They extended the arc of Picard north to Dunkirk and south to Collioure (1683–1718), with a latitude difference of $8^\circ 20'$. Dividing the arc into two parts, the separate computation of the northern and the southern segment yielded a “negative” flattening of $-1/95$, which may be attributed primarily to uncertainties in the astronomic latitudes. The intense dispute between the supporters of Newton (flattening at the poles) and those of the Cassinis (elongation at the poles) over the figure of the Earth was resolved by two further arc measurement campaigns sponsored by the French Academy of Sciences.

P. Maupertuis and *A.-C. Clairaut*, among others, participated in the expedition to Lapland (1736–1737). The Lapland arc measurement (average latitude $66^\circ 20'$ and latitude interval $57.5'$) was compared with the arc measurement through the meridian of Paris, revised by *Cassini de Thury* and *La Caille*, (1739–1740). The result confirmed the polar flattening, with a flattening value of $1/304$. On a second expedition (1735–1744) to the Spanish Vice-Kingdom of Peru (modern day Ecuador), an arc at an average latitude of

$1^{\circ}31'$ south and with $3^{\circ}7'$ amplitude was determined by *P. Bouguer*, *C. de La Condamine* and *L. Godin*, supported by the Spanish navy officers *J. Juan* and *A. de Ulloa*. Combining the results with the Lapland arc led to a flattening of $1/210$. The flattening of the Earth at the poles was thereby demonstrated by *geodetic* measurements.

A *synthesis* between the physical and the geometric evidence of the ellipsoidal shape of the Earth was finally achieved by *A.-C. Clairaut* (1713–1765). The theorem (1743), which bears his name, permits the computation of the flattening from two gravity measurements at different latitudes, cf. [4.2.2]. A first application of Clairaut's theorem was by virtue of *P. S. Laplace* (1799), who derived a flattening of $1/330$ from only 15 gravity values. The wider application of this “*gravimetric method*” suffered from the lack of accurate and well-distributed gravity measurements and from the difficulty of reducing the data to the Earth ellipsoid. Such problems were not overcome until the twentieth century. The theoretical basis, on the other hand, for physical geodesy was laid down between the middles of the eighteenth and the nineteenth century. It is related to the development of potential theory and connected with the names of the French mathematicians *J.-B. d'Alembert*, *J. L. Lagrange*, *A. M. Legendre* and *P. S. Laplace*, followed later by *C. F. Gauss* and the British scientists *G. Greene* and *G. G. Stokes*.

With the rotational ellipsoid commonly accepted as a model for the Earth, numerous *arc measurements* were conducted up to the twentieth century. These measurements generally served as a basis for national geodetic surveys, see [1.3.3]. For example, the meridian arc through Paris was extended by *Cassini de Thury* and included in the first triangulation of France (1733–1750). A geodetic connection between the astronomical observatories in Paris and Greenwich (1784–1787) was the beginning of the national survey of Great Britain, with the final extension of the Paris meridian arc to the Shetland Islands. Particular significance was attained by a new measurement on the meridian through Paris, between Barcelona and Dunkirk (1792–1798), commissioned by the French National Assembly and carried out by *J. B. Delambre* and *P. F. A. Méchain*. The results served for the definition of the meter as a natural unit of length (1799). Combined with the Peruvian arc measurement, these observations yielded an ellipsoidal flattening of $1/334$.

1.3.3 The geoid, arc measurements and national geodetic surveys

As recognized by *P. S. Laplace* (1802), *C. F. Gauss* (1828), *F. W. Bessel* (1837), and others, the assumption of an ellipsoidal-Earth model is no longer tenable at a high level of accuracy. The deviation of the physical plumb line, to which the measurements refer, from the ellipsoidal normal can no longer be ignored. This deviation is known as the *deflection of the vertical*. While adjusting several arc measurements for the determination of the ellipsoidal parameters, contradictions were found which greatly exceeded the observational accuracy. An initial adjustment of sections of the Paris meridian arc was carried out in 1806 by *A. M. Legendre* in his treatise “*Sur la méthode des moindres carrées*”. The least-squares method of adjustment applied by him was also independently developed by *C. F. Gauss*. Gauss successfully used the method for the orbit calculation of the asteroid “*Ceres*” (1802), and also for early adjustments of the Paris meridian arc and of a triangulation network in and around the dukedom of Brunswick (1803–1807).

This led to the refined definition of the “figure of the Earth” by *Gauss* and *Bessel*, who clearly distinguished between the physical surface of the Earth, the geoid as the mathematical surface, and the ellipsoid as a reference surface approximating it,

cf. [1.2]. With the definition of geodesy [1.1], *F. R. Helmert* made the transition to the actual concept of the figure of the Earth (Moritz, 1990).

Friedrich Robert Helmert (1843–1917), one of the most distinguished geodesists of modern times, was professor of geodesy at the Technical University at Aachen, Germany, and later director of the Prussian Geodetic Institute in Potsdam and of the Central Bureau of the ‘Internationale Erdmessung’. Through his work, geodesy has experienced decisive impulses, the effects of which are still felt today. In his fundamental monograph (1880/1884), *Helmert* established geodesy as a proper science (Wolf, 1993).

Despite the discrepancies found from the adjustments of different arcs, this method continued to be used to determine the dimensions of the Earth ellipsoid. However, the deflections of the vertical were still treated as random observational errors in the adjustments. As a consequence, this calculation method provided parameters for *best-fitting* ellipsoids, approximating the geoid in the area of the triangulation chains. The method failed to deliver a globally best-approximating ellipsoid, which is also due to the lack of data on the oceans. Many of these best-fitting ellipsoids have been introduced as “*conventional*” ellipsoids for calculating the national geodetic surveys, and thus arc measurements increasingly became part of the geodetic surveys. Established by triangulation, these national surveys provided control points for mapping, which remained the basis for many national geodetic reference systems until recent time. Gravity observations by pendulum measurements started in the eighteenth century. Observations were carried out in connection with arc measurements and in dedicated campaigns, especially after the foundation of the “Mitteleuropäische Gradmessung”, cf. [1.4.2].

We mention the historically important arc of *Gauss* (arc measurement between Göttingen and Altona 1821–1824, invention of the Heliotrope, adjustment according to the method of least squares) and its extension to the triangulation of the kingdom of Hannover (until 1844). Initiated by the Danish astronomer *H. C. Schumacher*, this arc should become part of a central European network, running from Denmark to Bavaria (triangulation by *J. G. Soldner*, 1808–1828) and further southwards. *Bessel* and *Baeyer* carried out an arc measurement oblique to the meridian in East Prussia (1831–1838), which connected the Russian triangulations (*W. Struve*, *C. Tenner*) with the Prussian and Danish networks and finally with the French–British arc along the meridian of Paris. The extension of a triangulation chain from the observatory in Tartu/Estonia northwards to the Arctic Ocean and southwards to the Black Sea (1816–1852) led to the “*Struve Geodetic Arc*”, stretching over more than 2800 km around the 27°E meridian. In 2005, this international geodetic enterprise was inscribed on the World Heritage List of UNESCO.

Further *long arcs* linking national triangulation-chains were built up over the next 100 years. Some of these were not completed until the 1950s, while others were never finished, owing to the replacement of classical geodetic observation techniques by satellite surveying methods. These long arcs include the American meridian arc (Alaska–Tierra del Fuego), the North American longitude arc along the 39° parallel between the Atlantic and the Pacific Oceans, the West European–African arc along the meridian of Paris (Shetlands–Algeria), the Arctic Ocean to Mediterranean Sea meridian arc (Hammerfest–Crete) as an extension of the “*Struve Arc*”, and the African 30° East meridian arc (Cairo–Cape Town) tied to it, the European–Asiatic longitude arc measurements at 48° (Brest–Astrachan) and at 52° latitude (Ireland–Ural Mountains), as well as the latitude and longitude arc measurements in India (*G. Everest*, *W. Lambdon*).

Since the 1880s, *vertical control networks* were established by geometric leveling within the frame of the national geodetic surveys but *independently* from the horizontal control systems. Heights were referred to a level surface close to the geoid and defined by the mean sea level as observed with a tide gauge. The accurate knowledge of the geoid was not needed in this separate treatment of horizontal position and height, as it was required only for the reduction of horizontal positioning.

An inevitable presupposition for the evaluation of large-scale measurements was the introduction of a standard for length. But it was only about one century after the introduction of the *meter* in France that representatives of a large number of countries met at the International Meter Convention in Paris in 1875, and agreed upon a new definition for the meter and its realization through a standard meter bar. There was also an urgent need to introduce a world time system, and a common zero meridian for the geographical longitude. Following a recommendation of the “Europäische Gradmessung” in 1883, the International Meridian Conference met in Washington, D. C. (1884). The Conference adopted the *Greenwich meridian* as the initial meridian for longitude, and the universal day (mean solar day) as the *time* unit referenced to this zero meridian.

1.3.4 Three-dimensional geodesy

The three-dimensional concept of geodesy consists of the common treatment of horizontal and vertical positioning within the same mathematical model. This was suggested already by Bruns (1878), who proposed to determine the surface of the Earth pointwise using a spatial polyhedron together with all exterior level surfaces. However, three-dimensional computations were not carried out in practice due to the problems associated with the inclusion of height measurements into the model. Trigonometrically derived height differences over large distances suffered from refraction anomalies, and geometric leveling could not be reduced to the ellipsoid as accurate geoid heights above the ellipsoid were not available.

The concept of three-dimensional geodesy was revived by Marussi (1949) and Hotine (1969), while in 1945 Molodensky demonstrated that the physical surface of the Earth and its external gravity field can be determined from surface measurements only, without needing the geoid (Molodenski, 1958).

Väisälä (1946) introduced *Stellar triangulation* from high altitude balloons as a first step to realize the three-dimensional concept. This technique was followed by *electromagnetic distance measurements* in the 1950s and 1960s, using both terrestrial and airborne methods. Satellite geodesy provided a technological breakthrough after the launch of the Russian satellite Sputnik I in 1957. Observations to orbiting satellites were used to establish control points in a three-dimensional system, and provided global gravity field information. Beginning in the 1980s, the NAVSTAR *Global Positioning System (GPS)* today dominates geodetic measuring techniques. Since the 1990s, global geodetic networks have been built up by different space techniques, and are regularly maintained by international services. Among the practical problems which geodesy is facing today is the connection of classical horizontal and vertical control networks to the global system, and their transformation into three-dimensional nets. This includes the determination of the geoid with respect to a global reference ellipsoid, with high accuracy and spatial resolution.

Recently, *kinematic methods* have gained great importance, especially with the extensive use of Global Navigation Satellite Systems (GNSS) like GPS. The measuring systems are carried on moving platforms (e.g., satellite, airplane, ship, car) and provide data referring to the geodetic reference system by continuous positioning (navigation).

1.3.5 Four-dimensional geodesy

The beginning of four-dimensional geodesy (Mather, 1973) may be reckoned from the detection of *polar motion* by F. Küstner (1884/85) and first observations of the *Earth tides* by E.v. Rebeur-Paschwitz (1889–1893), at the Geodetic Institute Potsdam. Monitoring of *crustal deformations* related to seismic activities began in Japan and the U.S.A. about 100 years ago. Interest in these phenomena was motivated by disastrous seismic events, such as the San Francisco Earthquake of 1906. In Fennoscandia, precise leveling and tide gauge registrations started in the 1880s and were used to determine the region's large-scale *vertical uplift* caused by postglacial rebound.

Today, the variations of the *Earth's rotation* and the movements of the *tectonic plates* are regularly observed through global networks. In addition, a number of regional control networks has been set up, especially at tectonic plate boundaries. *Gravity field variations* with time are derived from the analysis of satellite orbits and from dedicated satellite gravity missions (global and regional scale), as well as from terrestrial gravity measurements (local scale). The *Earth tides* have also been modeled successfully using terrestrial and satellite methods.

Worldwide, large efforts are nowadays made to measure and analyze all types of geodynamic phenomena, with geodetic methods playing a significant role, e.g. NASA (1983), Lambeck (1988), Herring (2009). With a further increase in accuracy of geodetic observations and a better resolution in space and time, geodesy now more than ever contributes to the understanding of the Earth system dynamics and global change processes. A long-term enterprise directed to this objective is the Global Geodetic Observing System (GGOS) of the International Association of Geodesy (Plag and Pearlman, 2009), cf. [1.4.2]. The time-variability of geodetic products (geometric and gravimetric networks, gravity field, Earth's orientation) also increasingly forces geodetic *practice* to take temporal changes into account, and to present geodetic products accordingly.

1.4 Organization of geodesy, literature

1.4.1 National organizations

The problems of *global geodesy* may be solved only by international cooperation of research institutions and national agencies, within the framework of international organizations and services, cf. [1.4.2].

University institutes and departments pursue fundamental and applied *research* in the fields of geodesy and remote sensing, geophysics, astronomy and space sciences, geomatics and surveying engineering. Worldwide, there is a multitude of corresponding institutions engaged in this research, which cannot be listed here explicitly (see Geodesist's Handbook 2004, J. Geod. 77, No. 10–11).

In several countries, *academy* or *governmental* institutes are also engaged in geodetic research.

Examples are found in Austria (Institute of Space Research, Academy of Sciences, Graz), China (Institute of Geodesy and Geophysics, Wuhan), Czech Republic (Research Institute of Geodesy, Topography and Cartography), Finland (Finnish Geodetic Institute), Germany (Deutsches Geodätisches Forschungsinstitut DGFI, München), Deutsches Geoforschungszentrum GFZ, Potsdam), Japan (National Research Institute for Earth Science and Disaster Prevention), Poland (Institute of Geodesy and Cartography, Space Research Center, Warsaw), Russia (Institute of Physics of the Earth, Moscow).

The national *geodetic surveys* are carried out according to the guidelines of the national survey authority, organized either as a central agency or in decentralized institutions.

As examples, we mention Australia (Geoscience Australia, Geospatial and Earth Monitoring Division), Austria (Bundesamt für Eich- und Vermessungswesen), Brazil (Instituto Brasileiro de Geografia e Estatística IBGE), Canada (Geodetic Survey Division/Geomatics, National Resources Canada), China (National Bureau of Surveying and Mapping with affiliated Chinese Academy of Surveying and Mapping), Denmark (Kort og Matrikelstyrelsen), France (Institut Géographique National), Germany (State geodetic surveys in cooperation with the Federal Bundesamt für Kartographie und Geodäsie BKG), Great Britain (Ordnance Survey), India (Survey of India), Italy (Istituto Geografico Militare), Japan (Geospatial Information Authority GSI), Norway (Statens Kartverk), Russia (Roskartografiya/Federal Service of Geodesy and Cartography), South Africa (Chief Directorate: Surveys and Mapping, Mowbray), Spain (Instituto Geográfico Nacional), Sweden (Landmäteriet), Switzerland (Bundesamt für Landestopographie), The Netherlands (Kadaster en Openbare Registers), and the U.S.A. (National Geodetic Survey/National Oceanic and Atmospheric Administration NGS/NOAA, formerly U.S. Coast and Geodetic Survey).

In addition to these, a number of non-geodetic institutions, in the course of their special tasks and projects, are also concerned with geodetic problems. These groups develop theories, measuring systems and methods, and in particular are involved with the collection and evaluation of geodetic data.

We mention *space agencies* (e.g., Agenzia Spaziale ASI, Matera; Centre National d'Etudes Spatiales, Toulouse; Deutsches Zentrum für Luft- und Raumfahrt; Goddard Space Flight Center of NASA, Greenbelt, MD, U.S.A.), *space observatories* (Astro-Geodynamics Observatory, Mizusawa, Japan; Geodätisches Observatorium Wettzell, Germany; Observatoire de Paris; Observatoire Royal de Belgique; Onsala Space Observatory, Sweden; Pulkovo Observatory, Russia; Royal Greenwich Observatory; Shanghai Observatory; U. S. Naval Observatory), *geologic and hydrographic services* (China: State Seismological Bureau; France: Bureau des Recherches Géologiques et Minières; Germany: Alfred-Wegener-Institut für Polar- und Meeresforschung (AWI), Bundesanstalt für Geowissenschaften und Rohstoffe, Bundesamt für Seeschiffahrt und Hydrographie; Great Britain: Institute of Geological Sciences, Institute of Oceanographic Sciences; U.S.A.: U.S. Geological Survey), and *military agencies* (e.g., U.S.A.: National Geospatial-Intelligence Agency NGA, formerly National Imagery and Mapping Agency NIMA and Defense Mapping Agency DMA). More details may be found in Journal of Geodesy 74 (2000, p. 142 ff.).

1.4.2 International collaboration

At the beginning of the arc measurement in the kingdom of Hannover (1821), *C. F. Gauss* had already expressed his desire for international collaboration. According to Gauss, this geodetic network would be connected to neighboring triangulation

networks, aiming toward an eventual merger of the European observatories. Organized international collaboration originated with the memorandum by the Prussian general J. J. Baeyer (1794–1885): “Über die Größe und Figur der Erde, eine Denkschrift zur Begründung einer Mitteleuropäischen Gradmessung” (1861). In 1862, the “Mitteleuropäische Gradmessung” was founded in Berlin and was being among the first international scientific associations of significance; Baeyer became its first president. After expanding to the “Europäische Gradmessung” (1867) and to the “Internationale Erdmessung” (“Association Géodésique Internationale,” 1886), the association engaged in fruitful activity, which was especially inspired by the works of Helmert as director of the Central Bureau (Levallois, 1980; Torge, 1996, 2005; Ádam, 2008).

After the dissolution of the “Internationale Erdmessung” during the first World War, the “International Union of Geodesy and Geophysics” (IUGG) was founded in 1919. In 2011, this organization had a membership of 65 countries. It consists of one geodetic and seven geophysical associations, dealing with the cryosphere, with geomagnetism, hydrology, meteorology, oceanography, seismology, and volcanology. The “International Association of Geodesy” (IAG) is led by a President who is elected every four years, and who is assisted by a Vice President and a General Secretary, together they form the IAG Bureau. The Executive Committee coordinates the IAG’s work and formulates the general policy, while the Council (delegates from the membership countries) is responsible for governance, strategic policy and direction. The IUGG and IAG meet at General Assemblies at four-year intervals. In addition, numerous symposia and scientific conferences are organized to treat special themes; among these are the IAG Scientific Assemblies, which are held between the General Assemblies.

The scientific work of the IAG is performed by Commissions, Services, Inter-commission Committees, the Communication and Outreach Branch, and IAG Projects (Beutler et al., 2004, The Geodesist’s Handbook 2008, J. Geod. 82, No. 11). Currently there are four *Commissions* established for long-term problems (Reference Frames, Gravity Field, Earth Rotation and Geodynamics, Positioning and Application), which may set up Study Groups or Working Groups for topics of limited scope. A focal point for theoretical geodesy is the *Inter-commission Committee* on Theory. The “*Global Geodetic Observing System (GGOS)*” was established in 2003, as an integral IAG component along with Services and Commissions (Plag and Pearlman, 2009). It “works with the other IAG components to provide the geodetic infrastructure necessary for monitoring the Earth system and global change research” (Drewes, 2005; Terms of Reference 2007, J. Geod. 82 (2008), No. 11: 826–829).

An important part of the IAG work is done by *Services*, through collecting and analyzing observations in order to generate products relevant to geodesy and other sciences and applications.

We currently have the following Services partly maintained in collaboration with other scientific organizations: International GNSS Service (IGS) with the Central Bureau at the NASA Jet Propulsion Laboratory, Pasadena, California; International VLBI Service for Geodesy and Astrometry (IVS); International Laser Ranging Service (ILRS); International Gravimetric Bureau (BGI), Toulouse; International Geoid Service (IGeS), Milano; International Centre for Earth Tides (ICET), France; International Earth Rotation and Reference Systems Service (IERS) with the Central Bureau at the Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt, a.M.; International DORIS Service, France; International Gravity Field Service with the Central Bureau at the National Geospatial-Intelligence Agency NGA, U.S.A.; International Centre for Global Earth

Models, GFZ Potsdam; International Digital Elevation Model Service, U.K.; Permanent Service for Mean Sea Level, Proudman Oceanographic Laboratory, Liverpool, U.K.; Bureau International des Poids et Mesures-Time, Frequency and Gravimetry Section, Sèvres, France; International Altimetry Service IAS (to be confirmed); IAG Bibliographic Service, Leipzig, Germany.

1.4.3 Literature

References to textbooks and journals for geodesy and related fields (mathematics, physics, astronomy, geophysics, surveying engineering, mapping and geomatics) will be found in the running text. A list of geodetic and geodetically relevant publication series is given in Journal of Geodesy 77 (2004): 742–748, and a revised version is available at the IAG Website <http://www.iag-aig.org>.

We mention in particular the Journal of Geodesy (formerly Bulletin Géodésique and Manuscripta Geodaetica, Springer: Berlin-Heidelberg-New York), which is the official journal of the IAG. The results of each General Assembly of the IAG are compiled in the Travaux (Proceedings). National reports are collected and stored at the Central Bureau of the IAG. The proceedings of IAG symposia are published in a separate series (Springer).

Among the recent *scientific-technical journals* in the field of geodesy, geophysics, navigation, and surveying, we mention in particular:

Acta Geodaetica et Geophysica Hungarica (Hungary), Acta Geodaetica et Cartographica Sinica (China), Acta Geophysica (Springer), Advances in Space Research (Elsevier), Allgemeine Vermessungsnachrichten (Germany), Annals of Geophysics (Italy), Artificial Satellites (Poland), Australian Journal of Geodesy, Photogrammetry and Surveying, The Australian Surveyor, Bollettino de Geodesia e Scienze Affini (Italy), Bollettino die Geofisica Teorica ed Applicata (Italy), Earth, Planets and Space (Japan), EOS Transactions (American Geophysical Union AGU, U.S.A.), Geodesia (The Netherlands), Geodeticky a kartograficky obzor (Czech Republic), Geomatica (Canada), Geodesy and Cartography (Poland), Geodeziya i Aeroseymka, Geodeziya i Kartografiya (Russia), Geomatik Schweiz: Geoinformation und Landmanagement (Switzerland), Geophysical Journal International (Wiley, U.K.), Geophysical Journal of the Royal Astronomical Society (U.K.), Geophysical Research Letters (AGU, U.S.A.), Geophysics (U.S.A.), GPS World (U.S.A.), GPS Solutions (Springer), Inside GNSS (U.S.A.), Izvestiya, Physics of the Solid Earth (Russia/Springer), Journal of Applied Geodesy (Germany), Journal of Earthquake Prediction Research (China/Russia), Journal of Geodynamics (Elsevier), Journal of the Geodetic Society of Japan, Journal of Geophysical Research (AGU, U.S.A.), Journal of Surveying Engineering (U.S.A.), Kart og plan (Norway), Marine Geodesy (U.K.), Monthly Notices of the Royal Astronomical Society (U.K.), Navigation (U.S.A.), Österreichische Zeitschrift für Vermessungswesen und Geoinformation (Austria), Physics and Chemistry of the Earth A: Solid Earth and Geodesy (The Netherlands), Reviews of Geophysics and Space Physics (U.S.A.), Revista Cartografica (Mexico), Space Science Reviews (Springer), Surveying and Land Information Systems (U.S.A.), Studia Geophysica et Geodaetica (Czech Republic), Survey Review (U.K.), Surveys in Geophysics (Springer), Tectonophysics (The Netherlands), Zeitschrift für Geodäsie, Geoinformation und Landmanagement zfv (Germany).

Technical Reports are issued by university and research institutes, as well as by some governmental agencies. We mention here:

Astron.-geodätische Arbeiten in der Schweiz (Schweiz. Geod. Komm.); Bull. d'Inf. Marées Terrestres, Brussels; Bull. Earthquake Research Inst., Univ. of Tokyo; Bull. Geograph. Survey Inst., Tokyo; Geod. Geophys. Arb. in der Schweiz; Geowiss. Mittl. Studieng. Verm.wesen,

TU Wien; IERS Techn. Notes, Frankfurt a.M.; IGS Techn. Reports JPL, Pasadena, U.S.A.; Journal of Wuhan Technical University of Surveying and Mapping; Metrologia (Inst. of Physics/BIPM, France); Mitt. Bundesamt Kart. u. Geod., Frankfurt a.M.; Mitt. Geod. Inst. Univ. Bonn; Mitt. Geod. Inst. TU Graz; Mitt. Inst. Geod. Photogr. ETH Zürich; NASA Goddard Space Flight Center Rep., Greenbelt, Md.; Nat. Survey and Cadastre, Geod. Div. Techn. Rep., Copenhagen; Nederlands Geod. Comm. Publ.; Newton's Bulletin (formerly Bull. D'Inf. Bureau Gravimetrique International, Toulouse); NGA/NIMA Techn. Rep., Washington D.C.; NOAA-NOS-National Geod. Survey Techn. Rep., Rockville, Md.; Publ. on Geodesy, Delft; Publ./Rep. Finnish Geod. Inst. Helsinki; Publ. Division of Geomatics, Univ. of Calgary; Rep. Dep. of Geodetic Science and Surveying, The Ohio State Univ., Columbus, Ohio; Rep. on Geodesy, Inst. of Geodesy and Geod. Astronomy, Warsaw Univ. of Technology; Math. and Phys. Geodesy, TH Delft; Schriftenreihe d. Institute d. Fachber. Vermessungswesen, Univ. Stuttgart; Univ. Rep. School of Geomatic Engineering, Univ. of New South Wales, Sydney; Veröff. Bayer. Komm. für die Internationale Erdmessung, München; Veröff. Deutsche Geod. Komm., München; Wiss. Arb. Fachr. Geodäsie und Geoinformatik (formerly Fachrichtung Vermessungswesen), Leibniz Univ. Hannover.

2 Reference Systems and Reference Frames

Reference systems are required in order to describe the position and motion of the Earth and other celestial bodies including artificial satellites, positions and movements on the surface of the Earth, and the stationary and time-variable parts of the Earth's gravity field. They are represented by *coordinate systems*, which – in Newtonian space – are three-dimensional in principle, and defined with respect to origin, orientation, and scale. A fourth dimension, time, enters through the mutual motion of the Earth and other celestial bodies and through the temporal variations of the Earth's shape, its gravity field and its orientation. Present-day measurement accuracy even requires a four-dimensional treatment in the framework of general relativity, with rigorous coupling of space and time. Reference systems are realized through *reference frames* consisting of a set of well-determined fixed points or objects, given by their coordinates and (if necessary) velocities at a certain epoch. They serve for modeling geodetic observations, as a function of a multitude of geometric and physical parameters of interest in geodesy and other geosciences.

Basic units and constants are fundamental to the geodetic measurement and modeling processes [2.1]. Time systems are based either on processes of quantum physics, on motions in the solar system, or on the daily rotation of the Earth [2.2]. The geometric properties of reference systems are provided by three-dimensional coordinates, here we distinguish between a space-fixed celestial and an Earth-fixed terrestrial reference system [2.3]. Conventional reference systems and corresponding reference frames are provided by the International Earth Rotation and Reference Systems Service IERS [2.4]. In addition, gravity field-related local level systems have to be introduced, as most geodetic observations refer to gravity [2.5].

Fundamentals on three-dimensional and surface geodetic coordinates are provided by Heitz (1988), while Kovalevsky et al. (1989) and Nothnagel et al. (2010) in detail describe global reference systems and reference frames used in astronomy and geodesy. The impact of relativity on geodesy and reference systems is discussed in Soffel (1989) and Moritz and Hofmann-Wellenhof (1993). For reference systems and frames defined for the moon and the planets, see Seidelmann et al. (2007).

The treatment of *height* and *gravity* requires the introduction of dedicated reference systems. *Vertical Reference Systems* are based on the gravity field of the Earth and will be discussed in [3.4.3] and [7.2]. Gravity measurements apply different techniques and deliver various gravity field quantities. As a consequence, a *Gravity Reference System* has to be introduced in order to consistently evaluate the heterogeneous gravity data, cf. [5.4.3].

2.1 Basic units and constants

Time, length, and mass are basic quantities used in geodesy. The units for these quantities are the second (s), the meter (m), and the kilogram (kg), respectively. They are

defined through the International System of Units (Système International d'Unités SI), established in 1960 by the eleventh General Conference of Weights and Measures (CGPM) in Paris (BIPM 2006), see also Markowitz (1973), Drewes (2008). The definitions of these international standards are as follows:

- The *second* is the duration of 9 192 631 770 periods of the radiation corresponding to the transition between the two hyperfine levels of the ground state of the cesium-133 atom (CGPM 1967).
- The *meter* is the length of the path traveled by light in vacuum during a time interval of 1/299 792 458 of a second (CGPM 1983).
- The *kilogram* is the unit of mass; it is equal to the mass of the international prototype of the kilogram (CGPM 1901).

According to these definitions, the second and the kilogram are independent units. The meter, on the other hand, depends on the fixed value of the velocity of light (see below).

The establishment and maintenance of the reference standards for these units is the task of the *Bureau International des Poids et Mesures* (BIPM), located in Sèvres, France. BIPM cooperates with the national laboratories of standards under the guidelines of the International Meter Convention (1875). These national laboratories include the National Institute of Standards and Technology, Gaithersburg, MD, U.S.A., the National Physical Laboratory, Teddington, U.K., and the Physikalisch-Technische Bundesanstalt, Braunschweig, Germany.

The *realization* of the *meter* is based on interferometric measurements (relative uncertainty 10^{-12}) using light with highly stable frequencies (stabilized lasers). The international *kilogram* prototype has been kept in BIPM since 1889; national prototypes are related to it with an uncertainty of 10^{-9} . The BIPM Time, Frequency and Gravimetry Section (until 1987: Bureau International de l'Heure BIH, Paris) defines the *second* (uncertainty now reaching 10^{-17}) and the atomic time scale, cf. [2.2.1].

Previous definitions of the meter and the second were based on natural measures. The *meter* was intended to be one ten-millionth part of the meridian quadrant passing through Paris. Its length was derived from a dedicated arc measurement, cf. [1.3.2], and realized in 1799 by a prototype meter bar called "mètre des archives". Following the International Meter Convention, a more stable version (platinum-iridium bar) was manufactured (international meter). It has been preserved since 1889 at the BIPM, and copies have been distributed to the participating countries. This improved realization (uncertainty 10^{-7}) was valid until 1960 when, for the first time, the wavelength of a certain spectral line of light became the defining quantity.

Since ancient times, the natural measure for *time* has been the daily rotation of the Earth about its axis. The mean solar day, cf. [2.2.2], was determined by astronomic observations, and the second was defined as 1/86400 part of that day, according to the subdivision of the day into 24 hours, with the hour 60 minutes and the minute comprises 60 seconds. From the 1930s on, it became obvious that this definition was uncertain by about 10^{-7} due to irregularities of the Earth's rotation, cf. [2.3.4]. Time measurements based on atomic clocks became possible in 1955, with a cesium standard constructed at the National Physical Laboratory (UK), Guinot and Arias (2005).

As a supplementary SI unit, the *radian* (rad) is used for *plane angles*:

- The radian is the plane angle between two radii of a circle subtended by an arc on the circumference having a length equal to the radius.

Geodesy, astronomy, and geography also use the *sexagesimal graduation* with 1 full circle = 360° (degrees), $1^\circ = 60'$ (arcminutes), and $1' = 60''$ (arcseconds, also arcsec, with the milli- and micro-subdivisions mas and μ as). With 2π rad corresponding to 360° , an angle α is transformed from radian to degree by

$$\alpha^\circ = \rho^\circ \alpha \text{rad}, \quad \rho^\circ = 180^\circ/\pi. \quad (2.1)$$

Among the fundamental *physical constants* used in geodesy is the *velocity of light* in vacuum, which is (exactly!) by the above definition (1983)

$$c = 299\,792\,458 \text{ ms}^{-1}, \quad (2.2)$$

and the *gravitational constant* (CODATA System of Physical Constants 2006, Mohr et al., 2008), which is given by

$$G = (6.674\,28 \pm 0.000\,67) \times 10^{-11} \text{ m}^3\text{kg}^{-1}\text{s}^{-2}, \quad (2.3)$$

with a relative uncertainty of 1×10^{-4} .

While the IERS Standards (1992) still recommended the former CODATA (1986) value of $6.67259 \times 10^{-11} \text{ m}^3\text{kg}^{-1}\text{s}^{-2}$ for the constant of gravitation, the Numerical Standards given in the IERS Conventions (2010) contain the value given in (2.3), Petit and Luzum (2010). It should be noted that the uncertainty of G directly affects the calculation of mass and mean density of the Earth, and of its moments of inertia, cf. [8.1], [3.3.4].

Henry Cavendish carried out the first experimental determination of G in 1798 with a torsion balance. Current work concentrates on increasing the relative accuracy of G to better than 10^{-4} . This includes investigations into dependence of G on material, external influences, distance and direction, as well as non-inverse-square properties of gravitation (as the “fifth force” discussed for a while), Gillies (1987), Fischbach and Talmadge (1999). The results obtained vary strongly, but a significant accuracy increase has not been achieved, and evidence for deviations from Newton’s law have not been found. The limited accuracy obtained is due to the fact that only very weak gravitational forces can be produced experimentally, and that gravitation, unlike other forces, cannot be screened.

Other units and constants used in geodesy, astronomy, and geophysics, will be introduced in the corresponding chapters. IERS and other services generally adopt corresponding parameter values for a certain time period as standards (Petit and Luzum, 2010), see also Ahrens (1995), Burša (1995a) and Grotens (2004).

2.2 Time systems

Time plays a fundamental role in geodesy. This is, on the one hand, due to the fact that most geodetic observation methods use time or frequency measurements of electromagnetic waves for positioning (this is especially valid for space geodetic methods), and that a uniform time scale is also needed in order to model the motion of artificial satellites. On the other hand, a time system is required for describing the relative motion of the Earth in the solar system with respect to inertial space and for dating all measurements and results.

Relativistic effects close to the Earth are at the order of 10^{-9} in a relative sense, which is at the order of accuracy at present-day geodetic measurements. This fact requires a relativistic

treatment of measurements using electromagnetic signals, and of reference systems moving with high velocities and in the neighbourhood of massive bodies. According to Einstein's theory of General Relativity, systems of (four-dimensional) space-time coordinates within the gravitational field have to be defined and used for modeling (e.g. Damour, 2007). Consequently, the IAU (International Astronomical Union) introduced corresponding celestial and terrestrial reference systems in 2000, and IUGG and IAG followed the relevant resolutions (Petit and Luzum, 2010). Reference systems are now defined within the frame of relativity theory, and satellite orbits and space geodetic observation are modeled and analyzed in the context of post-Newtonian formalism. On the other hand, at most geodetic applications and at modeling geodynamic phenomena, relativistic effects (being proportional to $1/c^2$) can still be taken into account by corresponding reductions, and geodetic calculations may take place in Newtonian space, with Euclidian geometry and absolute time. Therefore, time and coordinate systems are treated separately in the following, with proper reference to the space-time relation (Müller et al., 2008).

Time systems are defined by the unit for a time interval (scale) and by a time epoch. They are based either on the definition of the SI second and on orbital motions in the solar system [2.2.1], or on the diurnal rotation of the Earth about its axis [2.2.2]. Fundamental descriptions of time systems are found in Moritz and Mueller (1987), and McCarthy and Seidelmann (2009), see also Nothnagel et al. (2010). For transformations between different time scales see, e.g., Soffel et al. (2003) and Guinot (2005), and the IAU2000/2006 resolutions (McCarthy and Petit, 2004; Petit and Luzum, 2010).

2.2.1 Atomic time, dynamical time systems

A uniform time scale of high accuracy is given by the *International Atomic Time* (Temps Atomique International TAI). It corresponds to the definition of the SI second, cf. [2.1], which has been made approximately equal to the second of the formerly used *Ephemeris Time* (see below). The origin of TAI was chosen so that its epoch (January 1, 1958, 0 h) coincided with the corresponding epoch of Universal Time UT1, cf. [2.2.2]. The TAI day comprises 86400 s, and the Julian Century has 36 525 TAI days. TAI is regarded as a realization of Terrestrial Time TT (see below).

TAI is *provided* by the BIPM Time, Frequency and Gravity Section, from the readings of a large set (presently more than 350) of atomic clocks (mostly cesium beam frequency standards including about ten primary standards providing long-term stability, and a few hydrogen masers) maintained at over 50 national laboratories (Börger, 2005). Clock comparisons are performed at a number of timing centers, employing mainly GPS and geostationary telecommunication satellites for synchronization (Petit and Jiang, 2008), cf. [5.2.5]. From these local determinations, a weighted mean is calculated and disseminated at the BIPM. TAI stability is better than 10^{-15} (over minutes to several months) and decreases with time, it can be accessed by time transfer techniques with an accuracy of 1 ns and better, e.g., Weyers et al. (2001). A relative uncertainty of 10^{-17} and better is expected through the development of new atomic clock technologies (laser-cooled cesium fountains, optical clocks using light instead of microwaves at the atomic transition process), and will strengthen the relativistic aspects of geodesy (Shen et al., 2011).

According to the theory of General Relativity, the definition of a time system depends on the choice of the respective reference system; velocity and gravity potential at the clock's site play an important role under this aspect. As a consequence, the readings of the atomic clocks are

reduced to a non-moving clock at sea level, introducing a standard potential value for the geoid (SI second “on the geoid”), see below and [3.4.1].

Dynamical time scales have been introduced early, in order to provide an independent and uniform time argument of barycentric ephemerides and equations of motion. This was achieved by time systems, based on the orbital motion of bodies in the solar system.

The *Ephemeris Time* (ET) was introduced by IAU in 1952. It was realized through long-term astronomical observations to the sun. Ephemeris Time was followed by *dynamical time* scales, referring either to the barycenter of the solar system or to the geocenter. Temps Dynamique Barycentrique (TDB), for instance, was used in celestial mechanics as an independent time argument for the barycentric ephemerides of the solar system bodies (sun, moon and planets).

In 1991, the IAU introduced general relativity as the basis of four-dimensional space-time reference systems, with a corresponding “*coordinate time*” for the individual system (Müller, 1999; Petit and Luzum, 2010; p. 151 ff.). We distinguish between barycentric and geocentric coordinate time. *Barycentric Coordinate Time* (Temps Coordonné Barycentrique TCB) refers to a reference system located at the center of mass of the solar system, and is used for the ephemerides of bodies moving in this system (planets, moon, interplanetary satellites). It replaces TDB (see above) which can be expressed as a linear function of TCB. *Geocentric Coordinate Time* (Temps Coordonné Geocentrique TCG) is the coordinate time of a reference system with origin at the Earth’s center of mass (Geocentric Celestial Reference System). It is based on the SI second, and of special importance for the equations of motion and ephemerides of artificial Earth satellites. The transformation between TCB and TCG is given by a four-dimensional transformation, which depends on geometry, kinematics, and potential in the solar system, cf. [2.4.1].

Terrestrial Time (TT) has been introduced as a coordinate time no longer based on celestial dynamics. It serves for dating events observed at the surface of the Earth or close to it, and thus it is the primary time scale for the relativistic treatment of space geodetic techniques. The definition of this time coordinate implies that TT (previously called Temps Dynamique Terrestre TDT) would be measured by an atomic clock located on the rotating geoid. TT differs from TCG only by a constant rate, $d(TT)/d(TCG) = 1 - L_G$, with the unit of TT being chosen so that it agrees with the SI second on the geoid, and the defining constant $L_G = W_0/c^2 = 6.969\,290\,134 \times 10^{-10}$ (W_0 geoid potential, c velocity of light in vacuum), Fukushima (2009), Petit and Luzum (2010). As a consequence, although TAI and TT are independent time scales, the TT unit is practically equivalent to TAI, with a constant difference resulting from the epoch definition of TAI:

$$TT = TAI + 32.184 \text{ s.} \quad (2.4)$$

2.2.2 Sidereal and Universal Time

The diurnal rotation of the Earth provides a natural measure for time. Corresponding time systems are introduced in order to relate Earth-based observations to a space-fixed system: Sidereal and Universal (solar) Time. Hereby, two periodic motions of the Earth play a role (Fig. 2.1):

- The *diurnal rotation* (spin) of the Earth about its polar axis. This rotational axis approximately coincides with the axis of maximum moment of inertia, and it passes

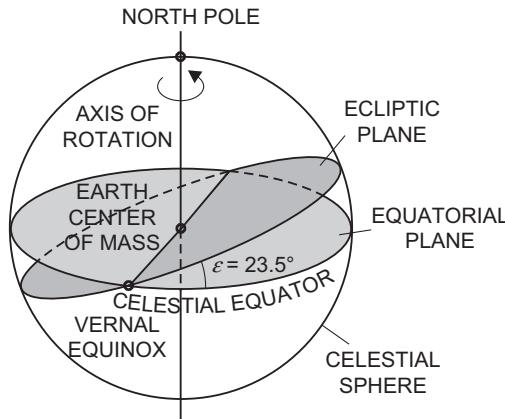


Fig. 2.1: Earth rotation, equatorial plane, and ecliptic plane.

through the Earth's center of mass, cf. [2.3.4]. The *equatorial plane* is perpendicular to the axis of rotation.

- The *annual revolution* of the Earth around the sun. Following Kepler's laws, the Earth describes an ellipse with the sun at one of its focal points. Minor perturbations arise due to the gravitation of the moon and other planets. The plane of the Earth's orbit is called the *ecliptic plane*; it has an obliquity ε of about 23.5° with respect to the equatorial plane.

By circumscribing the unit sphere (celestial sphere) around the center of the Earth, simple geometric relations are obtained. The *celestial equator* and the *ecliptic* are defined by the intersections of the sphere with the corresponding planes. The *vernal equinox* (also First Point of Aries) is the intersection of the ecliptic and the equator where the sun passes from the southern to the northern hemisphere, it serves as the origin of the right ascension α . This classical equator–ecliptic system will be introduced in [2.3.1].

With the IAU2000/2006 resolutions, a slightly modified definition of the origin of the right ascension has been introduced (within the frame of a more fundamental updating of the astronomic reference system), this will be discussed in [2.4.1]. Here and in the following, the classical system is still treated in some detail, as it certainly will be of practical relevance for a longer time span.

Sidereal time is directly related to the rotation of the Earth. *Local Apparent* (or true) *Sidereal Time* (LAST) refers to the observer's (local) meridian; it is equal to the hour angle h of the (true) vernal equinox (Fig. 2.2), cf. [2.3.1]. The vernal equinox is affected by precession and nutation in longitude, and thus experiences long and short-periodic variations, cf. [2.3.2]. If nutation is removed, we obtain *Local Mean Sidereal Time* (LMST), referring to the mean vernal equinox. For the Greenwich meridian the corresponding hour angles are called *Greenwich Apparent Sidereal Time* (GAST) and *Greenwich Mean Sidereal Time* (GMST), the symbol θ is also often used for GAST. With the IAU2000/2006 resolutions, GAST has been replaced by the *Earth Rotation Angle*, see [2.4.2]. The astronomic longitude Λ is the angle between the meridian planes of the observer and Greenwich. It is given by, cf. [2.5]:

$$\Lambda = \text{LAST} - \text{GAST} = \text{LMST} - \text{GMST}. \quad (2.5)$$

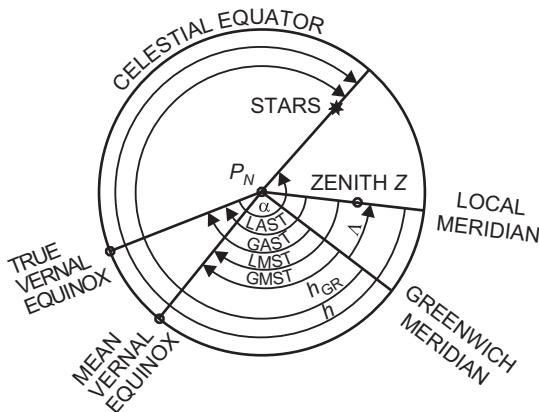


Fig. 2.2: Rectascension, sidereal time, hour angle, and longitude.

LAST is used at the evaluation of astronomical observations to fixed stars and extra-galactic radio sources, cf. [5.3.2], [5.3.4]. The mean sidereal time scale is still affected by precession (long-periodic). The *mean sidereal day* is the fundamental unit; it corresponds to the time interval of two consecutive transits of the mean vernal equinox through the meridian.

For practical reasons, *solar time* is used in everyday life. It is related to the (apparent) diurnal motion of the sun about the Earth. Since this revolution is not uniform, a fictitious “mean” sun is introduced which moves with constant velocity in the equatorial plane and coincides with the true sun at the vernal equinox. *Mean solar time* is equal to the hour angle of the mean sun plus 12 h, the beginning of the day is thus shifted to midnight. If referred to the Greenwich mean astronomical meridian, cf. [2.3.4], it is termed *Universal Time* (UT). Its fundamental unit is the *mean solar day*, being the interval between two transits of the mean sun through the meridian.

The conversion of Universal Time to Greenwich Mean Sidereal Time is rigorously possible and is given by a series development with time defined by the International Astronomical Union (Seidelmann, 1992/2006). Since the orbital motion of the Earth is about 1° per day (360°/365 d), the year has 1 day more in sidereal days than in solar days. We have the following approximation:

$$1 \text{ mean sidereal day} = 1 \text{ mean solar day} - 3 \text{ m } 55.90 \text{ s} = 86164.10 \text{ s.} \quad (2.6)$$

The Earth's rotation rate is 15.04107"/s, and its angular velocity is

$$\omega = 2\pi/86164.10 \text{ s} = 7.292115 \times 10^{-5} \text{ rad s}^{-1}. \quad (2.7)$$

Universal time is obtained from a network of space geodetic stations operating within the frame of the IERS, with the main contribution coming from Very Long Baseline Interferometry, cf. [2.4.4]. The observed local time UT0 refers to the instantaneous rotation axis, which is affected by polar motion, cf. [2.3.4]. In order to compare the results of different stations, reductions to a *Conventional Terrestrial Pole* are applied. The reduction in astronomic longitude $\Delta\Lambda_p$ corresponds to a change in time, cf. [5.3.3]. It transforms UT0 to UT1, which refers to the conventional terrestrial system, cf. [2.4.2]:

$$\text{UT1} = \text{UT0} + \Delta\Lambda_p \quad (2.8)$$

From a historical point of view, solar time UT1 has been the most important time-scale for human life, but it still contains all variations of the Earth's rotation with time, the same is valid for Greenwich Mean Sidereal Time.

A practical time scale, as needed in navigation for instance, has to provide a *uniform* unit of time and maintain a close relationship with UT1, i.e., to Earth rotation. In 1972, this led to the introduction of the *Coordinated Universal Time* (UTC), as a compromise between TAI and UT1. The time interval of UTC exactly corresponds to atomic time TAI, cf. [2.2.1], and its epoch differs by not more than 0.9 s from UT1. In order to keep the difference

$$|\Delta\text{UTI}| = |\text{UT1} - \text{UTC}| < 0.9 \text{ s}, \quad (2.9)$$

"leap seconds" are introduced in UTC when necessary. In 2011, we have a difference $\text{UTC} - \text{TAI} = -34$ s, and no positive leap second has been introduced at the end of December 2011.

Like TAI, UTC is provided by the BIPM time, frequency and gravity section, while ΔUT is calculated and distributed by the IERS, cf. [2.4.4]. UT1 is now primarily regarded as the time-variable rotation angle of the Earth about its polar axis, containing a multitude of information on geodynamic processes, and serving as one orientation parameter between the terrestrial and the celestial reference systems, cf. [2.4.3], [8.3.2].

UTC is disseminated through the Internet (e.g. U.S. National Institute of Standards and Technology, U.S. Naval Observatory), via radio, telephone, and GPS. Among the continuously broadcasting time stations are DCF77/Mainflingen (77.5 kHz), HBG/Prangins (75 kHz); MSF/Rugby (60 kHz) in Europe; WWV resp. WWVB/Ft. Collins, Colorado (2,5 to 20 MHz resp. 60 kHz); and WWVH/Kauai, Hawaii (2,5 to 15 MHz).

2.3 Reference coordinate systems: fundamentals

Reference systems in astronomy and geodesy are four-dimensional in principle, containing a set of three-dimensional geometric coordinates and the time coordinate. Restricting ourselves on the geometry in Newtonian space, the systems are defined by the origin and orientation of the fundamental planes or axes of a Cartesian coordinate system. For practical reasons, spherical (polar) coordinates are also introduced at both systems. We distinguish between the space-fixed celestial reference system [2.3.1] and the terrestrial reference system fixed to the Earth's body [2.3.3]. The equatorial plane (or the Earth rotation axis, respectively) provides a common orientation for both systems which differ by their conventional orientation on that plane. The Earth rotation axis experiences a multitude of variations with time, with respect to an inertial system as well as to the solid Earth, and so do the reference systems related to it [2.3.2], [2.3.4].

In this chapter, we discuss the fundamentals of celestial and terrestrial reference systems, following the classical definitions in astronomy. As mentioned already in [2.2.2], a number of IAU resolutions since the 1990s significantly modified and refined the concepts and definitions in fundamental astronomy in order to cope with the increased accuracy of the observations. As a consequence, the internationally adopted reference systems experienced some important changes, while the accuracy of the reference frames improved remarkably. The new definitions and the corresponding realizations will be introduced in [2.4], together with the relations between the classical and the modern systems, which will exist simultaneously for a certain transition time.

The fundamentals of reference systems in astronomy are given in textbooks or monographies as Eichhorn (1974), Schödlbauer (2000), Kovalevsky (2002), and Kovalevsky and Seidelmann (2004). For reference systems in geodesy see textbooks as Hofmann-Wellenhof and Moritz (2005) and the publications on the actual International Terrestrial Reference Frame, cf. [2.4.2].

2.3.1 Celestial Reference System

An inertial system is needed in order to model the ephemerides of celestial bodies in space, including those of artificial satellites. At the classical point of view, such a system is characterized by Newton's laws of motion; it is either at rest or in the state of a uniform rectilinear motion without rotation. A *space-fixed* system (Celestial Reference System CRS) represents an approximation to an inertial system. We distinguish between a dynamical and a kinematic CRS.

A *dynamical* CRS is based on the ephemerides of solar system bodies (planets, moon, artificial satellites) and possibly also on the proper motion of stars. Dynamical reference systems have been realized through various optical measurements and radio data. The corresponding reference frames have been used for aligning star catalogues, but are of limited accuracy and not very practical for astronomical routine observations. Lunar laser ranging will provide a corresponding reference frame with an accuracy of $0.01''$ and long-time stability, in contrast to satellite techniques which only allow a reference time stability of a few days. A *kinematic* CRS is defined by the positions and (if necessary) proper motions of stars or quasars. It is represented by the IAU *International Celestial Reference System*, and its realization is of extreme significance for geodesy, cf. [2.4.1].

The coordinates of the classical celestial reference system are defined by the *equatorial system* of spherical astronomy. We introduce a three-dimensional Cartesian coordinate system with the origin at the center of mass of the Earth (geocenter). The Z-axis coincides with the rotational axis of the Earth. The X- and Y-axis span the equatorial plane, with the X-axis pointing to the vernal equinox (First Point of Aries) and the Y-axis forming a right-handed system (Fig. 2.3), cf. [2.2.2]. As already mentioned above,

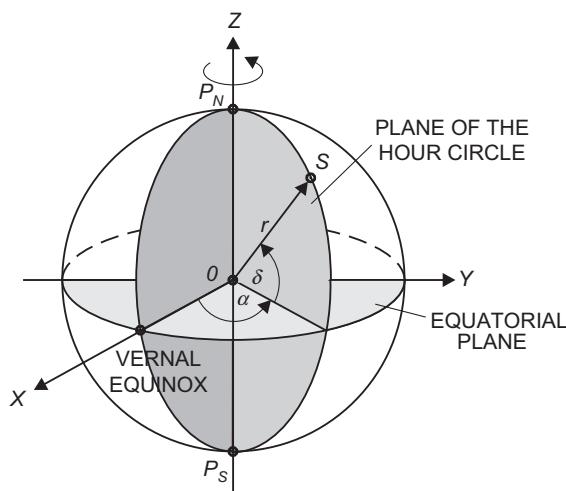


Fig. 2.3: Astronomic equatorial system.

we here concentrate on the classical (and still wide-spread) definition of the equator/ecliptic-system, the recent modification based on the IAU2000 definitions will be discussed in [2.4].

In the sequel, we shall also shift the origin of this system to the position of an observer on the Earth (topocenter) or to the barycenter of the solar system. The directions to celestial bodies then vary with different definitions of the origin (parallaxes). Since the Earth's radius is negligibly small compared to the distances to stars and extragalactic radio sources, no distinction is necessary between a topocentric and a geocentric system, i.e. the daily parallax can be neglected, cf. [5.3.3].

We circumscribe the unit sphere (celestial sphere) about the Earth. The rotational axis meets the sphere at the *celestial* north and south *poles* P_N and P_S . The great circles perpendicular to the celestial equator, which contain the celestial poles, are called *hour circles*, and the small circles parallel to the equator are termed *celestial parallels*.

Star positions are usually given as spherical coordinates right ascension and declination: α, δ -system, (Fig. 2.3). The *right ascension* α is the angle measured in the plane of the equator between the planes of the hour circles passing through the vernal equinox and the celestial body S ; it is reckoned from the vernal equinox anticlockwise. The *declination* δ is the angle measured in the plane of the hour circle between the equatorial plane and the line OS (positive from the equator to P_N and negative to P_S).

The *position* of a *celestial body* S now can be described either by the Cartesian coordinates X, Y, Z , or by the spherical coordinates α, δ, r (r distance from the origin O). We have the transformation

$$\mathbf{r} = \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = r \begin{pmatrix} \cos \alpha \cos \delta \\ \sin \alpha \cos \delta \\ \sin \delta \end{pmatrix}. \quad (2.10)$$

In geodesy, only directions are important for stars and extragalactic sources. With $r = 1$, α and δ describe the position of S on the unit sphere. These angles can also be expressed by the lengths of the corresponding arcs on the equator and the hour circle.

We finally introduce the local *meridian plane* of the observer, spanned by the local vertical (direction of the plumb line) and the rotational axis, after a parallel shift from the geocenter to the topocenter. The *zenithal point* Z and the *nadir point* Z' are the intersections of the vertical with the unit sphere, and the *celestial meridian* is the great circle through Z and the poles (Fig. 2.4). The *hour angle* h is measured in the equatorial plane between the celestial meridian through Z and the hour circle of S , reckoned from the upper meridian toward west. The great circles perpendicular to the horizon and running through Z and Z' are called *vertical circles*, and the small circle through S , parallel to the horizon, is termed *almucantar*. Because of the Earth's rotation, the hour angle system (h, δ -system) depends on time. It is rotated, with respect to the (α, δ) -system, about the polar axis by the angle of sidereal time LAST, cf. [2.2.2]. We have the relation (Fig. 2.2)

$$\text{LAST} = h + \alpha, \quad (2.11)$$

which is used with time determination, cf. [5.3.2].

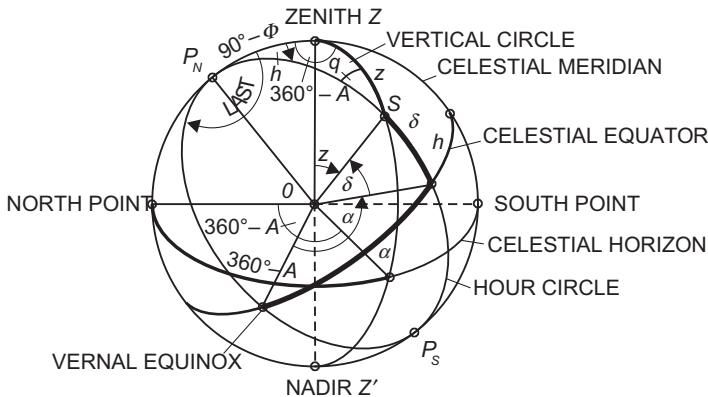


Fig. 2.4: Astronomic equatorial and horizon system.

2.3.2 Precession, nutation

The Earth's axis of rotation which has been introduced as the Z -axis experiences long-term and periodic changes, with respect to a space-fixed (quasi-inertial) system, cf. [2.3.1]: *Precession and nutation* (Moritz and Mueller, 1987; Seidelmann, 1992/2006; Schuh and Böhm, 2011). This is due to gravitational torques exerted by the moon, the sun and the planets on the flattened Earth. The effect of precession and nutation on the position (α, δ) of celestial bodies has to be taken into account by corresponding reductions, based on precession-nutation models and observations; this will be discussed below and in [2.4.3].

The *lunisolar precession* is a secular effect caused by the gravitation of the moon and the sun on the equatorial bulge of the Earth. This creates a torque which tends to turn the equatorial plane into the plane of the ecliptic (Fig. 2.5). In combination with the moment of the Earth's rotation, the Earth's axis describes a gyration of a cone with a generating angle of $23^{\circ}26'21.4''$ at J2000.0 (corresponding to the obliquity of the ecliptic ε), about the northern pole of the ecliptic E_N . As a consequence, the vernal equinox

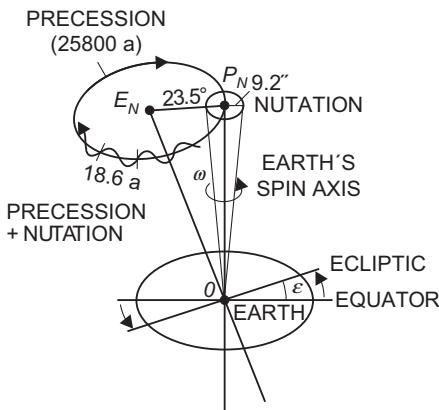


Fig. 2.5: Precession and nutation.

moves clockwise along the ecliptic. The gravitation of the planets causes an additional slow dislocation of the Earth's orbit and thereby an additional migration of the vernal equinox and a change in ε : *planetary precession*. The sum of the lunisolar and the planetary precession is termed *general precession*. With a rate of $5029.7962''/\text{century}$ along the ecliptic (general precession in longitude for J2000.0, also *constant of precession*), a complete revolution is performed in about 25 770 years.

The precession is superimposed by periodic effects, known as *nutation*, which can be described by a rotation of the true pole about the cone of precession. Lunisolar nutation results from the periodic position changes of the moon and the sun relative to the Earth. The nutation periods range from short-periodic (a few days) to long-periodic (mainly 18.6, 1.0, 0.5 years and 14 days). The 18.6 years period is caused by the inclination of the lunar orbit (approximately 5°) with respect to the ecliptic. This results in a corresponding movement of the orbital node along the ecliptic, where the semi-major axis of the 18.6 a-nutation ellipse (constant of nutation) amounts to $9.2025''$ for J2000.0. Semi-annual and semi-monthly periods stem from the oscillations of the sun and moon between the Earth's northern and southern hemisphere.

The instantaneous position of a celestial body, cf. [2.3.1], is called *true position* at the epoch t . By accounting for nutation, we obtain the *mean position* at epoch t , which refers to the mean celestial equator and the mean vernal equinox, cf. [2.2.2]. If precession is also taken into account, we get the mean position at the reference epoch J2000.0.

Precession has been known already since antiquity (*Hipparcos*, 2nd century B.C.), and nutation was found in 1748 by *James Bradley*. Based on long-term astronomic observations and the ephemerides of moon, sun, and planets, a sequel of precession and nutation models have been developed in recent times. We mention the IAU1976 theory of precession, which used three time-dependent rotation angles for the reduction to a mean reference pole at epoch J2000.0 (Julian epoch January 1, 2000, 12h), Lieske et al. (1977). It was followed by the IAU1980 theory of nutation which described the deviation of the true pole from the mean pole by series expansions of two time-dependent parameters: "nutation in obliquity of ecliptic" and "nutation in ecliptic longitude" (Seidelmann, 1982). At this model, the Earth was regarded as an elliptical, rotating, elastic and ocean-free body with solid inner and liquid outer core (Wahr, 1981a).

Nowadays, VLBI measurements to quasars and lunar laser ranging mainly contribute to the development of precession-nutation models, based on more recent geophysical Earth models. The recent IAU2000/2006 precession-nutation model will be introduced in [2.4.1].

2.3.3 Terrestrial Reference System

An *Earth-fixed* reference system, rotating with the Earth, is introduced for describing positions and movements of objects on and close to the Earth's surface, thus providing the basis for national surveys, geoinformation systems and navigation. It also serves as geometric frame for the determination of the Earth's gravity field and other space dependent geophysical/geological properties of the Earth, as well as for modeling deformations of the Earth's body and other terrestrial variations with time. As with the celestial reference system, we introduce a three-dimensional geocentric Cartesian coordinate system, realized through the coordinates of a set of fundamental stations of a global geodetic network.

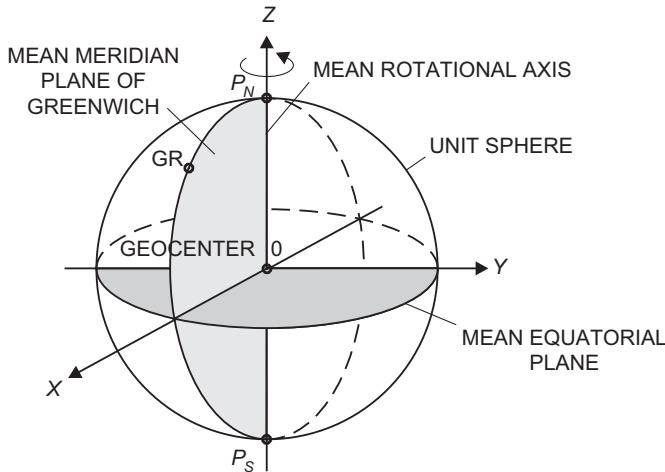


Fig. 2.6: Earth-fixed geocentric Cartesian system.

The origin of this system of spatial Cartesian coordinates X , Y , Z (Fig. 2.6) is located at the Earth's center of mass (geocenter), being defined for the whole Earth including oceans and atmosphere. The Z -axis is directed towards a conventional "mean" terrestrial (north) pole, and should coincide with a corresponding "mean" rotational axis. The "mean" equatorial plane is perpendicular to it and contains the X - and Y -axis. A "mean" rotational axis and equatorial plane have to be introduced because the rotation of the Earth changes with respect to the Earth's body over time, this will be discussed in [2.3.4]. The X , Z -plane is generated by the conventional "mean" meridian plane of Greenwich, which is spanned by the mean axis of rotation and the Greenwich zero meridian, to which Universal Time refers, cf. [2.2.2]. The Y -axis is directed so as to obtain a right-handed system. For the definition of the *International Reference System* see [2.4.2].

Comparing the definitions of the celestial and the terrestrial reference systems we recognize that the instantaneous axis of rotation is the common starting point for defining the Z -axis of both systems. The directions of the X -axis of the systems differ by the angle of Greenwich apparent sidereal time GAST, cf. [2.2.2]. With the recent IAU2000 system, GAST has been superseded by the Earth Rotation Angle, cf. [2.4.2].

In order to describe analytically certain physical properties of the Earth (gravity field, magnetic field, topography, etc.), *spherical coordinates* r , ϑ , λ are employed. Here, r is the radial distance from the geocenter, ϑ the polar distance (co-latitude), and λ the geocentric longitude. Instead of ϑ , the geocentric latitude

$$\bar{\varphi} = 90^\circ - \vartheta \quad (2.12)$$

can be used (Fig. 2.7). The position of the point P is then given by the position vector

$$\mathbf{r} = \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = r \begin{pmatrix} \sin \vartheta \cos \lambda \\ \sin \vartheta \sin \lambda \\ \cos \vartheta \end{pmatrix}. \quad (2.13)$$

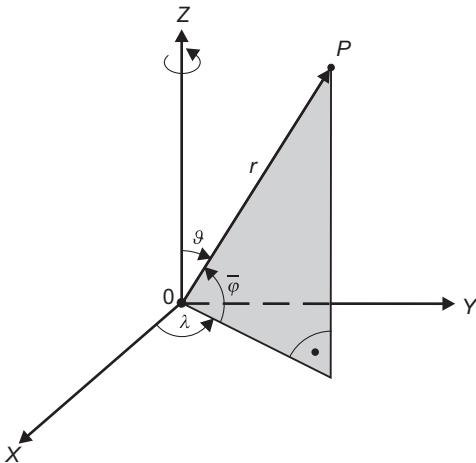


Fig. 2.7: Cartesian and spherical coordinates.

2.3.4 Polar motion, Earth rotation

The rotation of the Earth can be described by a vector directed to the north pole of the instantaneous axis of rotation and by the angular velocity ω , see (2.7). The direction of the (space-fixed) rotational axis is given by the Celestial Pole, cf. [2.3.1]. Among the standard reference books on Earth rotation are the monographs by Lambeck (1980) and by Moritz and Mueller (1987), also Schuh and Böhm (2011). For the relations between Earth rotation and global geodynamic processes, as well as for measuring and modeling techniques see Plag and Pearlman (2009, p. 123 ff.), Gross (2009), and Seitz and Schuh (2010), cf. also [8.3.2].

Direction and magnitude of the rotational axis vector (and the equatorial plane attached to it) change with time with respect to the solid Earth, which is due to external gravitational forces and to internal geodynamical processes. Going more into details, we have the time-variable lunar, solar and planetary gravitation, on the one hand, and a multitude of variations in the Earth's body on the other, ranging from mass redistributions in the atmosphere and the hydrosphere over tectonic plate movements, post-glacial isostatic adjustment and mantle convection to liquid core motion. The changes are secular, periodic or quasi-periodic, and irregular in nature, and they are clearly visible in the Earth rotation parameters *polar motion* and *Earth rotation angle*.

We here neglect the fact that there is a small deviation between the instantaneous axis of rotation and the angular momentum axis, which conserves its direction in space. This deviation is less than 0.001" with periods <1 day.

The observation of the *Earth rotation parameters* consequently provides information about the physical properties of the Earth's interior and on mass transport in the geo-physical fluids, which include the atmosphere and the oceans, continental water, and the mantle and core (Dehant and Mathews, 2009), cf. [8.3.2]. On the other hand, these parameters are part of the *Earth Orientation Parameters* (EOP), which provide the transformation from the International Terrestrial Reference System to the International Celestial Reference System as a function of time, and vice versa [2.4.3].

Polar motion for a rigid Earth was already predicted in 1765 by *Leonhard Euler*. In 1884/85, *F. Küstner* observed corresponding latitude variations, with a period found in 1891 by *S.C. Chandler*, valid for a more realistic non-rigid Earth. International activities of monitoring polar motion date back to 1899, when the *International Latitude Service* (ILS) started latitude observations at five observatories located around the globe on the $39^{\circ}08''$ northern parallel (Höpfner, 2000). The *rotational velocity* of the Earth was considered to be constant until the 1930s. Improved astrometric observations then revealed seasonal variations (N. Stoyko, 1937), and since the 1950s atomic clocks offered new possibilities to identify temporal variations of the Earth's angular velocity. After extension (1962) of the ILS to the *International Polar Motion Service* (IPMS), and in cooperation with the *Bureau International de l'Heure* (BIH) established in 1919, finally about 50 astronomical observatories contributed to the determination of polar motion and time (Höpfner, 2000). Using classical astrometric techniques, an accuracy of $0.02''$ resp. 1 ms was reached for mean values over 5 days (Yokohama et al., 2000; Guinot, 2000). Starting in the 1960s, polar motion and Earth rotation are now determined regularly by geodetic space techniques, within the frame of the IERS, cf. [2.4.4]. The results are provided with daily (and partly sub-daily) resolution and an accuracy improved by about two to three orders of magnitude with respect to classical techniques.

Polar motion (or wobble) is the motion of the Earth's rotation (spin) axis with respect to the Earth-fixed reference system. It directly affects the coordinates of stations on the Earth's surface and the gravity vector. Polar motion consists of several components:

- A free oscillation with a period of about 435 days (*Chandler period*), with a variable amplitude of $0.1''$ to $0.2''$, in a counter-clockwise (prograde) sense as viewed from the north pole. The Chandler wobble is due to the fact that the spin axis of the Earth does not coincide exactly with the (polar) axis of maximum moment of inertia (figure axis). For a *rigid* Earth, this would lead to a gyration of the rotational axis about the principal axis of inertia with a period of $A/(C - A) = 305$ days (*Euler period*). Here C is the Earth's polar moment of inertia, and A is the mean equatorial moment (rotational symmetry assumed). The difference between the Chandler and the Euler period results from the non-rigidity of the Earth, and is a function of the internal structure and rheology. The elasticity of the Earth's mantle should lead to internal friction with corresponding dissipation of energy, and result in a damping of the Chandler wobble with time. In reality, the wobble is continuously excited by atmospheric and oceanic processes, with minor contributions from continental hydrosphere and cryosphere, and no damping has been observed (Gross et al., 2003; Seitz et al., 2004).
- An *annual wobble*, superposing the Chandler wobble, and caused by mass redistributions and mass motions in the Earth. This includes the seasonal displacements of air and water masses, at which the annual high pressure system over Siberia plays a significant role. The annual oscillation proceeds in the same direction as the Chandler wobble with nearly a constant amplitude of about $0.1''$, and the superposition of the annual and the Chandler wobble leads to an oscillation of 6.3 years, with $0.25''$ amplitude (Höpfner, 2004).
- A *secular motion* of the pole as observed for more than 100 years. The motion consists of an irregular drift of about $0.003''$ to $0.004''$ /year (corresponding to about 10 cm/year on the Earth's surface) in the direction of 76° to 79° western longitude. Secular motion is mainly due to glacial isostatic adjustment in Canada and Fennoscandia, but sea-level changes, large-scale tectonic movements, mass shifts in the Earth's interior and polar ice melting may also contribute to this trend.

Correlated with tectonic plate motions, secular motions of the pole attain large amounts over geological epochs: *polar wander* (Steinberger and Torsvik, 2008).

- *Periodic, quasiperiodic* and more *irregular variations* occurring at time scales from days to decades, with amplitudes of $0.03''$ and more (decadal variations). Their origin reaches from ocean tides and ocean-tide loading (diurnal and semi-diurnal frequencies) over atmospheric and hydrologic processes (few days to few years) to oceanic and continental water variations (on inter-annual time scales from 1 year to 6 years and more), but is partly still unknown.
- Other *free motions* in addition to the Chandler wobble, due to misalignments of rotational axis and figure axes related to the flattened Earth's mantle, and inner and outer core (Dehant and Mathews, 2009).

The *nearly diurnal free wobble* (NDFW) is caused by the misalignment of the figure axis of the mantle and the rotation axis of the fluid outer core. As seen from the terrestrial reference system, this mantle-core interaction results in a retrograde (opposite to the diurnal Earth rotation) motion of the Earth rotation axis with nearly diurnal frequency. In space it corresponds to a retrograde motion of the rotation axis with respect to the angular momentum axis, with a period of about 430 sidereal days (*free core nutation FCN*). The inner core reaction with the mantle should lead to another nearly diurnal retrograde period motion (seen from mantle-fixed frame), and prograde decadal variations (space-fixed frame). Again, these free motions are excited by geophysical processes. They reach only the order of a few 0.1 mas, and are still under discussion (Greiner-Mai et al., 2003).

The superposition of all these polar motion components results in a slightly perturbed spiral like curve of the instantaneous pole with a slowly advancing mean position (Fig. 2.8).

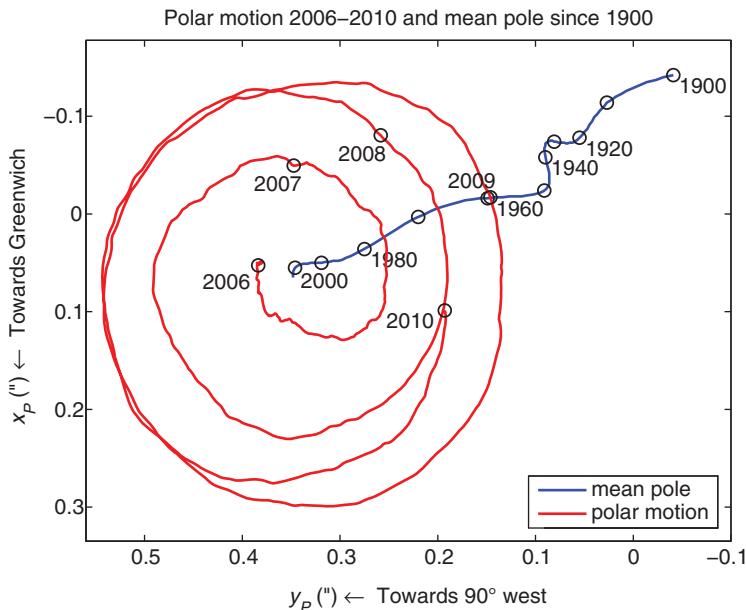


Fig. 2.8: Polar motion 2006–2010, and mean pole displacement 1900–2006, with data from IERS (<http://hpiers.obspm.fr/eop-pc>).

Over 1 year, the deviations from the mean position remain $< 0.3''$, corresponding to approximately 9 m on the Earth's surface.

The reference for describing the actual position of the celestial pole with respect to the solid Earth is provided by a Conventional Terrestrial Pole. The corresponding IERS Reference Pole, cf. [2.4.3], agrees within $0.03''$ with the former *Conventional International Origin*, which was defined by the mean direction of the Earth rotation axis as determined between 1900.0 and 1906.0. The position of the instantaneous pole, with respect to the terrestrial reference pole is given by the rectangular coordinates x_p, y_p , which are defined in the plane tangential to the pole. The x-axis is in the direction of the Greenwich mean meridian (consistent with the previous BIH zero meridian), and the y-axis is directed along the 90°W longitude meridian. These plane coordinates are usually expressed as spherical distances (in units of arcsec) on the unit sphere, which corresponds to rotations around the respective axis of the geocentric coordinate system. The direction of the zero longitude meridian (*Greenwich Mean Observatory*) was fixed indirectly through the longitudes of the observatories determining Universal Time within the frame of the BIH time service.

The angular velocity ω of the Earth's rotation, as monitored from the Earth, changes with time. Relative changes may reach several 10^{-8} , which corresponds to several ms for 1 day. The variations are generally described by the excess revolution time with respect to the nominal *Length-Of-Day* (LOD) comprising 86 400 s, and then called excess of length-of-day:

$$\Delta\text{LOD} = \text{LOD} - 86400 \text{ s.} \quad (2.14a)$$

They are derived by comparing astronomical time determinations, which deliver Universal Time UT1, with the uniform time scales TAI or UTC, generally through the difference $\Delta\text{UT} = \text{UT1} - \text{UTC}$, cf. [2.2.2]:

$$\Delta\text{LOD} = -\frac{d}{dt}(\Delta\text{UT}) 86400 \text{ s.} \quad (2.14b)$$

The following components of LOD variations have been identified, exploiting ancient records of lunar and solar eclipses, lunar occultation observations, and in modern times optical astrometric and VLBI measurements (Brosche and Sündermann, 1990; Morrison and Stephenson, 2001; Gross, 2009), see Fig. 2.9:

- A *secular decrease* in the angular velocity of the Earth's rotation, caused mainly by tidal dissipation. It lengthens the day by about 2 ms/century (Brosche and Sündermann, 1978/1982).

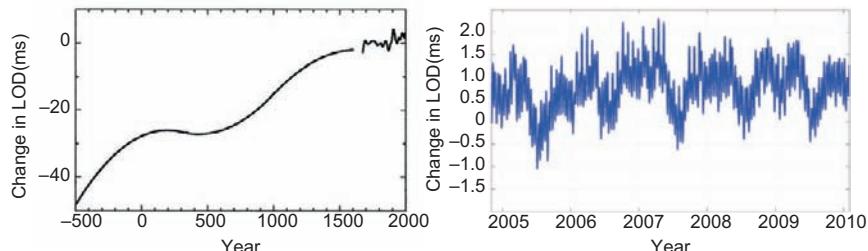


Fig. 2.9: Observed LOD variations over the past 2500 years (left, after Morrison and Stephenson, 2001) and 2005–2010 (right: with data from IERS, <http://hpiers.obspm.fr/eop-pc>).

- Fluctuations over *decades* (amplitude of a few ms), due to motions in the Earth's interior (core-mantle coupling) and to slow climatic variations.
- Tidal variations due to solid Earth and ocean tides (about 1 ms amplitude), with long- (annually) and short- (monthly, fortnightly, and especially diurnal and semi-diurnal) periodic parts.
- *Seasonal* effects (amplitude less than one ms), explained mainly by annual and semiannual atmospheric excitation, with contributions from water and ice budget variations, and continental hydrology, Gross et al. (2004).
- More *irregular* oscillations ranging from days to several years and including interannual and intraseasonal variations. They are predominantly of atmospheric origin, and caused by changes in the angular momentum of the zonal winds, as for instance connected with the El Niño Southern Oscillation phenomenon. Terrestrial mass displacements (Earthquakes) may also play a certain role.

While the effect of polar motion on observations depends on location, LOD changes act uniformly on all points on the Earth. The pole coordinates and UT1-UTC as well as LOD are nowadays provided by the IERS, cf. [2.4.3], [2.4.4]. More details on recent results of geodynamics research based on Earth rotation changes are given in [8.3.2].

2.4 International reference systems and reference frames

Conventional celestial and terrestrial reference systems are nowadays defined by the International Astronomical Union (IAU) and the International Union of Geodesy and Geophysics (IUGG), they are realized by corresponding reference frames. Here again we distinguish between the International *Celestial* Reference System/Frame (ICRS/ICRF) [2.4.1] and the International *Terrestrial* Reference System/Frame (ITRS/ITRF) [2.4.2]. The transformation rules between the systems employ the Earth orientation parameters, with the Earth rotation parameters as subset [2.4.3]. Realization and maintenance of the reference frames is the duty of the International Earth Rotation and Reference Systems Service (IERS) [2.4.4]. We especially refer to the IERS Conventions (Petit and Luzum, 2010) and to the detailed explanations given by Seidelmann (1992/2006), Seidelmann and Kovalevsky (2002) and Kaplan (2005).

2.4.1 International Celestial Reference System and Frame

Celestial reference systems are based on the positions of a set of selected celestial bodies. These spatial coordinate systems have the barycenter of the solar system as origin, and the directions of the system axis are defined either by the equatorial plane and the ecliptic (classical strategy: stellar system) or by the positions of extragalactic radio sources (IAU2000 radio source system). Measured right ascension and declination are related to the respective system, and refer to a specified date (epoch), cf. [2.3.1] and below.

Stellar reference systems have been provided by astronomy since antiquity, through the observation of fixed stars. They were realized by star catalogues containing the star positions for a certain epoch. Temporal variations of the system as the precession were early

recognized and taken into account. We mention the (lost) star catalogue of the Greek astronomer *Hipparchos* (2nd century B.C.) which was used and extended by *Ptolemaios* (1st to 2nd century), and the more recent catalogues of *Tycho Brahe* (16th century) and (now based on telescope observations) *Flamsteed* (17th century), *Bessel* (19th century), and many others. In the 1880s, a first “Fundamental Catalogue” of selected stars was compiled, followed by a series of further catalogues providing a uniform celestial reference frame.

Special importance among the *stellar* reference frames obtained the *Fundamental Catalogue* FK5 (Fricke et al., 1988), which is considered as *provisional realization* of the *International Celestial Reference System* ICRS (see below), and which was valid between 1988 and 1997. This *optical* frame was provided by the mean positions (α, δ) and the proper motions (generally $<1''/\text{year}$) of 1535 bright stars (up to an apparent magnitude of 7.5) for the epoch J2000.0 (Julian epoch January 1, 2000, 12h TT), with a precision of $0.01'' \dots 0.03''$ and $0.05''/\text{century}$, respectively. A supplement to FK5 contained additional stars up to a magnitude of 9.5. The mean equator (and mean pole) and the mean vernal equinox for J2000.0 were defined by the FK5 star positions, with an accuracy of $0.05''$. Due to refraction uncertainties, *Earth-based* astrometry can hardly improve this accuracy.

Astromonic space missions meanwhile could significantly improve the realization of a stellar reference system. The Hipparcos astrometry satellite (ESA, 1989–1993) was used to construct a network by measuring large angles between nearly 120 000 stars (up to an apparent magnitude of 11) covering the entire sky. The reference frame (about 100 000 stars) thus established provides an accuracy of better than $0.001''$ (epoch 1991.25) and $0.0006''/\text{year}$ for proper motion (Hipparcos, 1995; Kovalevsky et al., 1997), which leads to a typical accuracy of $0.005'' \dots 0.01''$ for J2000.0. The Hipparcos catalogue is now regarded by IAU as the *primary realization* of ICRS at *optical* wavelengths.

From improved FK5 data and HIPPARCOS results, an FK6 catalogue has been developed for a small number of stars (340 “astrometrically excellent”), resulting in an improvement of proper motion ($0.0003''$) as compared to the HIPPARCOS catalogue (Wielen et al., 1999). Upcoming optical astrometry space missions such as GAIA (*Global Astrometric Interferometer for Astrophysics*) and SIM Lite Astrometric Observatory (formerly Space Interferometer Mission) should significantly increase the quality of the optical catalogues (Klioner, 2003). The ESA mission GAIA (launch scheduled for 2012) will employ two telescopes on a rotating spacecraft and survey about one billion stars down to 20^{mag} , a positional accuracy of $20 \mu\text{as}$ is expected at 15^{mag} . The NASA space telescope mission SIM (launch planned for 2015) will use a 6 m-baseline Michelson interferometer and strive for μas -accuracy.

Starting in the 1990s, the IAU developed a new strategy for the definition and realization of a *four-dimensional* celestial reference system, and for the relation between the celestial and the terrestrial reference system. This was due to the rapid development of VLBI and geodetic space methods, with a significant increase of observational accuracy and the availability of time series of high resolution. The *International Celestial Reference System* (ICRS) finally introduced in 2000 is based on the theory of general relativity (Klioner et al., 2010). It is a *radio source* system, being accessible by the equatorial coordinates of extragalactic radio sources determined from VLBI observations, see below (ICRF), Petit and Luzum (2010), also Kaplan (2005) and Seidelmann (1992/2006).

ICRS is defined as a *Barycentric Celestial Reference System* (BCRS), with the origin located at the barycenter of the solar system; its time coordinate is the Barycentric Coordinate Time (TCB), Soffel et al. (2003), cf. [2.2.1]. The orientation of ICRS is realized by the adopted coordinates of the defining radio sources. The system no longer depends on the epoch, the Earth's pole of rotation and the pole of the ecliptic, as at the former equator/ecliptic system. For continuity with previous reference systems, the orientation has been chosen as close as possible to the mean equator and dynamic equinox at J2000.0, as given by the FK5. The system is kinematically non-rotating with respect to the defining extragalactic sources. This assumption is realistic, as the selected radio sources generally do not show a measurable proper motion, due to the large distances from the Earth (>1.5 billion light years).

The link (parallelism of axes) between the (previous) stellar and the radio source system is given with an accuracy of 0.05...0.1" (epoch J2000.0), this is within the uncertainty of the FK5. This connection has been improved by the results of the astrometric space mission HIPPARCOS to 0.001" or better for the epoch of observation, exploiting optical signals from a limited number of radio sources.

A *Geocentric Celestial Reference System* (GCRS) is introduced in order to realize the transformation between the celestial and the terrestrial (Earth-fixed) reference system, its coordinate time is Geocentric Coordinate Time (TCG), cf. [2.2.1]. The transition from the barycentric to the geocentric system requires taking effects like annual aberration and annual parallax into account, cf. [5.3.3]. The relation between BCRS and GCRS is given by relativistic (post-Newtonian) transformations, which include position, velocity and acceleration of the Earth, as well as the gravitational potential at the geoid. GCRS moves with the geocenter and is non-rotating with respect to BCRS, its axes are parallel to those of the BCRS.

The subsequent *transformation* from the celestial to the terrestrial reference system and vice versa includes a rotation around the polar axis, and has to take temporal variations of the reference pole into account, referring either to the space-fixed reference system (precession/nutation, cf. [2.3.2]) or to the Earth-fixed reference system (polar motion and Earth rotation, cf. [2.3.4]). The classical (equator/ecliptic-based) and the IAU2000 transformation procedure differ partly, this will be further discussed in [2.4.3]. With the IAU2000 resolution, an *intermediate reference system* has been introduced for this transformation, leading to a clear separation between precession/nutation and polar motion. The intermediate reference system is regarded either as space-fixed (*celestial*) or as Earth-fixed (*terrestrial*).

The *Celestial Intermediate Reference System* (CIRS) is related to GCRS by a time-dependent rotation taking precession and nutation into account (Capitaine and Wallace, 2006; Capitaine, 2007). It is defined by the intermediate equator of the *Celestial Intermediate Pole* (CIP) and the *Celestial Intermediate Origin* (CIO) on a specific date (Fig. 2.10). The position of celestial bodies in this system is now described by the *intermediate* right ascension and declination at a specified date, which corresponds to the "apparent" equinox right ascension and declination of the classical equator/ecliptic system, cf. [2.3.2], [5.3.2].

The position of the *Celestial Intermediate Pole* (CIP) in the GCRS is defined by the part of the precession-nutation with periods greater than 2 days, and the retrograde

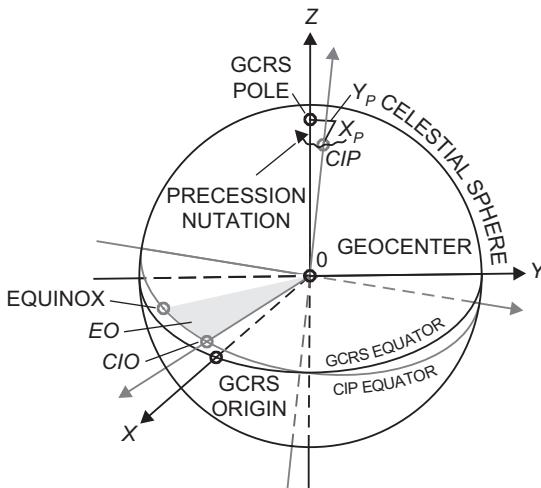


Fig. 2.10: Geocentric Celestial Reference System (GCRS) and Celestial Intermediate Reference System (CIP/CIO system), equation of the origins (EO), and motion of CIP in the GCRS (precession–nutation).

diurnal part of polar motion including free core nutation; the omitted nutation terms are included in the polar motion, cf. [2.4.3]. The motion of the CIP is primarily realized by the IAU2000/2006 precession–nutation model, and described by the X_p - and Y_p -components of the CIP unit vector (Fig. 2.10). Time-dependent corrections ΔX , ΔY (*nutation or celestial pole offsets*) are provided by the IERS. They are regularly derived from VLBI and LLR, and now also GPS observations (Rothacher et al., 1999). Corresponding corrections are given for use with the IAU1976/1980 precession–nutation model, as offsets in nutation in obliquity and in ecliptic longitude. These small effects are mainly due to the fact that the free core nutation is not included into the IAU nutation model; other unpredictable geophysical processes in the Earth’s atmosphere, oceans and solid body also contribute, cf. [2.3.4].

The IAU2000/2006 *Precession–Nutation Model* is based on the P03 precession theory (Capitaine et al., 2003) and the IAU 2000A/2000B nutation model (Mathews et al., 2002), see IERS Conventions 2010 (Petit and Luzum, 2010; p. 61 ff.). It replaced the IAU (1976/1980) models for precession and nutation, which used the Celestial Ephemeris Pole (CEP) as the reference pole for the International Celestial Reference Frame, cf. [2.3.2]. The new precession model provides polynomial expressions up to the 5th degree in time, while the nutation series includes 678 lunisolar and 687 planetary terms of nutation in longitude and obliquity. Model parameters have been derived through a fit of geophysical models to nutation–precession data derived from VLBI data sets. The underlying non-rigid Earth model takes mantle inelasticity and ocean tides into account, as well as electromagnetic couplings between the fluid outer core and the mantle, and between the solid inner core and the outer core. The IAU2000A nutation model delivers a precision of 0.1 to 0.2 mas at a one day resolution, an abbreviated version (IAU 2000B) is at the 1 mas accuracy level (Capitaine et al., 2009). The CIP coordinates (X_p, Y_p) are given as time-dependent polynomials, depending on the arguments of the precession–nutation model.

The *Celestial Intermediate Origin* (CIO) is the non-rotating origin for right ascension on the intermediate equator, it replaces the former equinox. The distance between the CIO and the equinox along the intermediate equator (i.e., the difference between the Earth Rotation Angle, see [2.4.2], and GAST) is called *equation of the origins* (Fig. 2.10).

The ICRS is realized through the *International Celestial Reference Frame* (ICRF), established and maintained by IERS. There exist two main realizations of the frame, the ICRF1 (1995 and later extensions, Ma et al., 1998; Fey et al., 2004) and the ICRF2 (Ma et al., 2009). ICRF1 contains the coordinates (equatorial system, epoch J2000.0) of some 600 radio sources. About 300 of them are well observed “defining sources” (high positional stability, no proper motion) establishing the orientation, and 100 more are used for densification and connection to the stellar-fixed reference system. The southern sky is not as well covered, as the radio telescopes are concentrated in the northern hemisphere. The coordinates of the radio sources are determined by radio astronomy (VLBI observations), with a precision of better than 1 mas on the average and 0.1 mas for the most precisely observed objects. ICRF2 utilizes more than 3400 compact radio astronomical sources, including 295 defining sources (Fig. 2.11). The corresponding observations stem from about 4550 VLBI sessions of 18 h or more duration, carried out between 1979 and 2009. This data set is rather heterogeneous with respect to the number of participating stations and global distribution, about 1400 multi-session sources contribute to at least two observing sessions. The average precision has improved to about 0.05 mas, and is 0.02 mas at best.

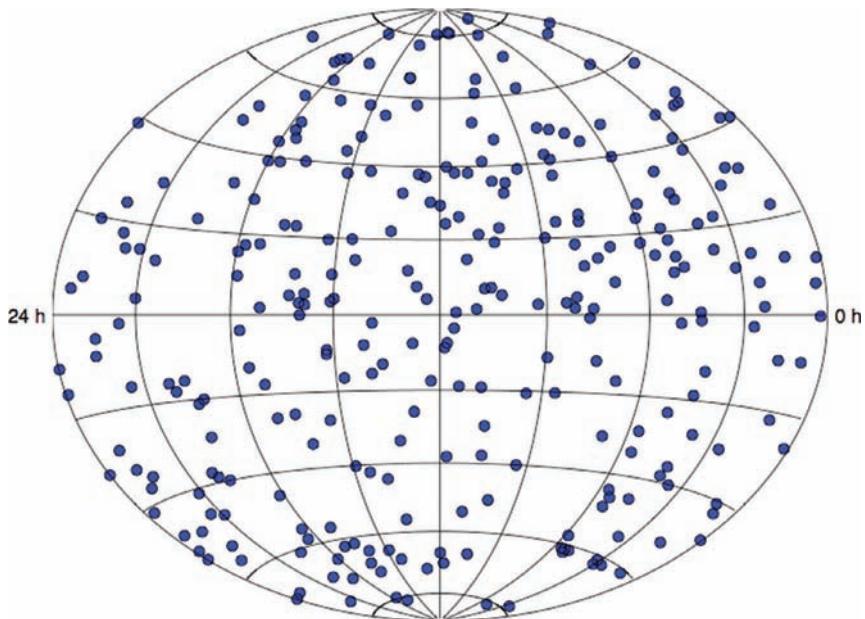


Fig. 2.11: International Celestial Reference Frame (ICRF2), from Fey et al. (2009).

2.4.2 International Terrestrial Reference System and Frame

The *International Terrestrial Reference System* (ITRS) is a geocentric terrestrial reference system (GTRS) co-rotating with the Earth in its diurnal motion in space, i.e., with the axis fixed to the solid Earth. The ITRS *origin* is the Earth's center of mass, including oceans and atmosphere. The *unit of length* is the meter (SI), which is consistent with the coordinate time TCG resp. TT, cf. [2.2.1]. The *orientation* of the axis is maintained in continuity with past international agreements (BIH orientation). Consequently, the pole of the ITRS (*IERS Reference Pole*) agrees within the accuracy of realization with the former *Conventional International Origin*, defined as the mean direction of the Earth's rotation axis between 1900 and 1905. This is also valid for the *IERS Reference Meridian*, which points to the zero longitude on the equator and coincides with the former BIH Greenwich Mean Observatory, cf. [2.3.4]. The time evolution of the ITRS orientation is ensured by a no-net-rotation condition with regard to horizontal motions at the Earth's surface, i.e., a global residual rotation is not allowed (Schuh et al., 2003; Petit and Luzum, 2010; p. 31 ff.).

The connection of the ITRS to the ICRS is given through the *Terrestrial Intermediate Reference System* (TIRS), as defined by the *Celestial Intermediate Pole* (CIP) resp. the intermediate equator, and the *Terrestrial Intermediate Origin* (TIO), Fig. 2.12, cf. also [2.4.3].

TIRS is related to ITRS by polar motion (i.e., the motion of CIP with respect to the ITRS). The *pole coordinates* x_p, y_p are derived from observations. They are regularly published by the IERS, together with additional components due to ocean tides (diurnal and semi-diurnal variations) and to nutation (with periods less than 2 days in space, which are not included in the nutation model).

The relation of ITRS to the Geocentric *Celestial* Reference System (GCRS) is given by the CIP (which is identical in both systems), and by a rotation around the CIP-axis which takes the Earth rotation into account. The rotation angle is called *Earth Rotation Angle* (ERA), and its time derivative is the Earth's angular velocity. ERA is measured along the

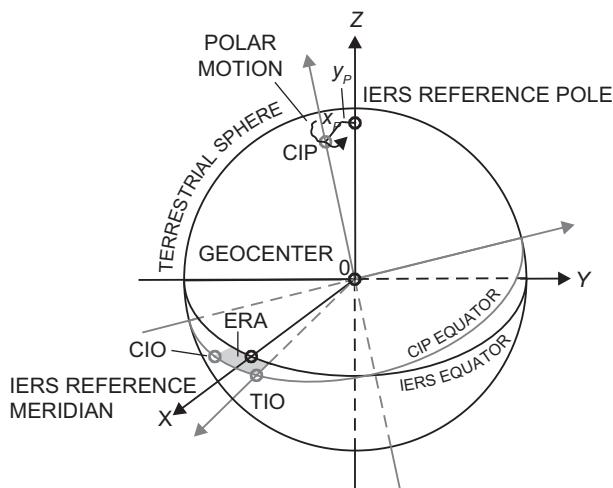


Fig. 2.12: International Terrestrial Reference System (IERS-Reference System) and Terrestrial Intermediate Reference System (CIP/TIO system), with Earth Rotation Angle (ERA) and motion of CIP in the ITRS (polar motion).

intermediate equator of the CIP between the Celestial Intermediate Origin (CIO) and the *Terrestrial Intermediate Origin* (TIO), positively in the retrograde direction. It substitutes Greenwich Apparent Sidereal Time (GAST) introduced in the classical equator/ecliptic system as rotation angle between the true vernal equinox and the Greenwich Meridian, cf. [2.2.2]. ERA is connected with UT1 by a simple linear relation, given by Capitaine et al. (2000). It can be calculated from the UT1 values published by the IERS, where similarly to polar motion (see above) small sub-daily ocean tides and nutation effects should be added as corrections. The TIO represents the origin of longitude in the Terrestrial Intermediate Reference System (TIRS), and remains within 0.1 mas of the ITRF zero meridian.

Realizations of ITRS are provided by the IERS, through the (regularly updated) *International Terrestrial Reference Frame* (ITRF). An ITRF solution comprises a global set of space geodetic observing stations with their geocentric Cartesian coordinates and the horizontal velocities of the observing sites, where a site is defined as a cluster of neighboring stations. GPS-stations prevail in the ITRF, followed by other space techniques; the corresponding networks as for example the IGS Global Tracking Network are described in [5.2], [5.3]. The high-precision (and expensive) VLBI and SLR stations are heterogeneously distributed over the Earth, while the GPS and DORIS networks cover the Earth's surface rather homogeneously, with extension into remote and ocean areas (Fig. 2.13). The stations participating to the ITRF carry out observations either continuously or at certain time intervals. As the observation sites are distributed over a larger number of tectonic plates, the detection of station movements due to plate tectonics becomes possible, see below and [8.2.3].

The combination of the networks observed with *different* techniques is carried out by local tie measurements ("mm"accuracy) at stations, where different techniques are employed, see Fig. 2.13. These *co-location* sites are of special value

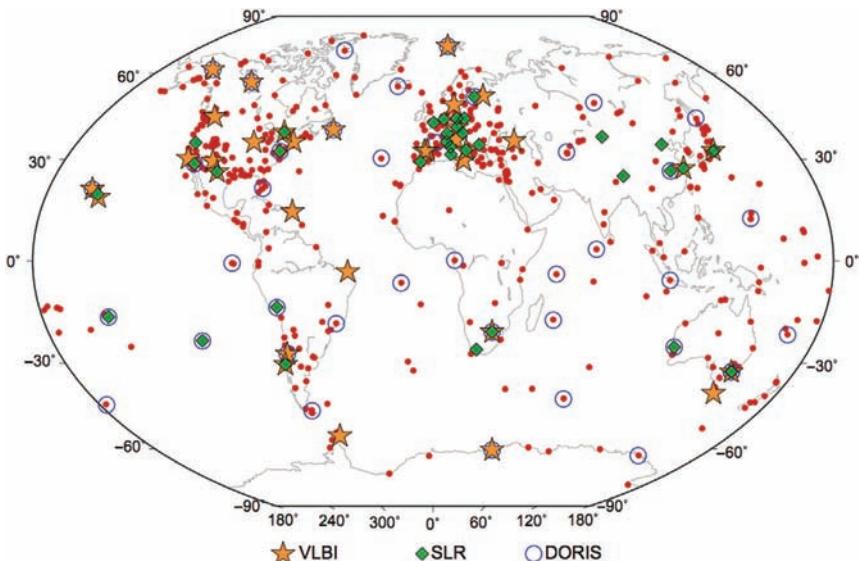


Fig. 2.13: International Terrestrial Reference Frame 2008 (ITRF2008) sites, with highlighting of VLBI, SLR and Doris sites co-located with GPS, from Altamini et al. (2011).

also for detecting systematic differences between the methods (Ray and Altamini, 2005). Several time variable effects are also taken into account at the evaluation, including local station displacements due to the solid Earth tides (using the tide-free model), polar motion, ocean and atmospheric loading effects, postglacial rebound, and shifts of instrumental reference points (Petit and Luzum, 2010; pp. 99–122).

The input data used for the ITRF are weekly time series of station positions derived from the individual satellite techniques (GPS, SLR, DORIS), 24-hours VLBI-session solutions, and daily Earth orientation parameters (now also directly included into the adjustment), as provided by the IERS Technique Centers. After reprocessing the input data (now covering a time span between 12 and 29 years) with partly improved reduction models, the individual solutions are combined by least-squares adjustment.

The ITRF-coordinates are given for a reference epoch (t_0), and refer to the IERS Reference Pole and the IERS Reference Meridian, see above. The current position vector \mathbf{r} (given in three-dimensional Cartesian Coordinates for the time t) of a point on the Earth's surface is derived from its position at the reference epoch by

$$\mathbf{r}(t) = \mathbf{r}_0 + \dot{\mathbf{r}}_0(t - t_0) + \Delta\mathbf{r}(t). \quad (2.14)$$

Here, \mathbf{r}_0 and $\dot{\mathbf{r}}_0$ are the position and velocity respectively at t_0 , and $\Delta\mathbf{r}(t)$ represents periodic and episodic station variations of geophysical origin for which conventional models are available, see above.

New versions of the ITRF are published every few years by the IERS, with the ITRF2005 and ITRF2008 as the most recent solutions obtained at the ITRS Combination Centres IGN and DGFI [2.4.4], cf. Altamini et al. (2007), Angermann et al. (2009), Altamini et al. (2011). The *ITRF2008* is comprised of the geocentric positions (X , Y , Z) for 934 stations, located at 580 sites (including about 90 co-location sites) and the corresponding horizontal velocities (Figs. 2.13, 2.14). The results refer to the epoch J2000.0, but in future, weekly solutions may provide a quasi-continuous monitoring of station movements.

Different computation strategies are applied at the combination centres. IGN is estimating similarity transformation parameters between epoch respectively per-technique solutions and the combined frame, along with the adjustment of station positions, velocities and

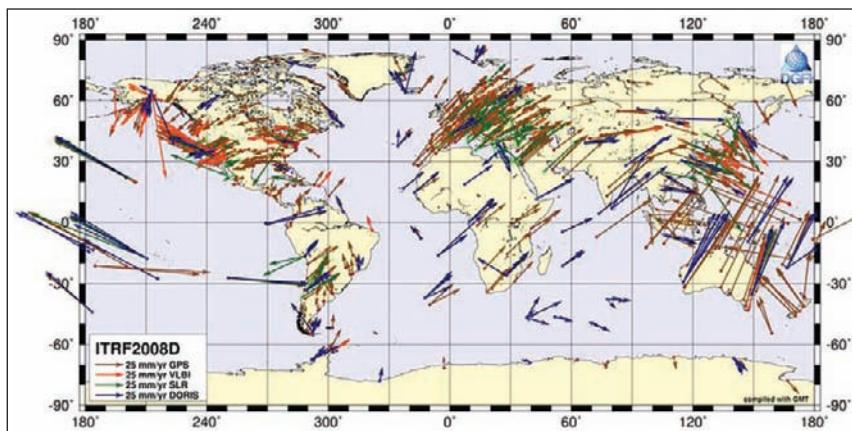


Fig. 2.14: ITRF2008 horizontal station velocities, from DGFI Website (<http://www.dgfi.badw.de>).

Earth Orientation Parameters. The epoch solution is based on seven transformation parameters (shift of origin, change of orientation, scale factor, cf. [6.2]), while the per-technique solution is extended by including linear parameter changes with time. DGFI, on the other hand, accumulates the normal equations of the different time series and techniques, without any transformation (Seitz et al., 2010). This method delivers corrections to the original observations, while the combination of the individual solutions results in corrections to the adjustment unknowns. Recent computation strategies employ a *common* adjustment for the determination of station positions and velocities, together with the Earth orientation parameters, based on the original observation time series. This is connected with a unification of standards, partly reprocessing of observations (GPS), and improvements in modelling (Angermann et al., 2010).

The *accuracy* of the ITRF solutions depends on the observation techniques and the quality and time span of the data. The accuracy of station positions and velocities is now at the order of a few mm and 0.1 to 0.5 mm/year, respectively. The ITRF origin (Earth's mass center) is in principle accessible through all dynamical satellite techniques but realized primarily by the SLR network. The scale, with the SI meter as length unit, is provided by SLR and VLBI observations, and naturally depends on the speed of light. These techniques also secure the long-term stability of the ITRF, as the corresponding observation series already cover several decades.

Geocenter variations with respect to the monitoring stations have been found from the analysis of space geodetic data. Annual and seasonal variations of several mm are caused primarily by mass redistributions in the atmosphere and the oceans and by continental water variations (Dong et al., 1997; Feissel-Vernier et al., 2006). These geometrically derived movements of the geocenter should correspond to the results obtained from the variations of the degree—one spherical harmonic coefficients of recent gravity models [3.3.4].

The no-net rotation condition of the ITRS (see above) is achieved by aligning the velocity-field to the horizontal movements of a plate tectonics model, vertical movements are not allowed at all.

Here, the IGN solution is based on the geological-geophysical plate tectonics model NNR-NUVEL1A (DeMets et al., 1994, cf. [8.2.4]), which uses geological time scales. DGFI, on the other hand, utilizes the plate rotation and deformation model APKIM (Drewes, 2009a). This model comprises 17 rigid plates and five plate boundary deformation zones, taken from the geophysical model PB2002 (Bird, 2003), and utilizes geodetically observed station velocities. Plate motion is modeled by one rotation vector per plate, and inter-plate deformations are computed assuming a visco-elastic-plastic continuum.

ITRF practically agrees with the *World Geodetic System WGS84*, maintained by the U.S. National Imagery and Mapping Agency. The coincidence is within the one meter-level for the former WGS84-Doppler realization, and at the few cm-level or better for the GPS realizations of WGS84, transformation parameters between the systems are no longer significant, cf. [5.2.5].

2.4.3 Transformation between terrestrial and celestial reference systems, Earth orientation parameters

The transformation between the terrestrial and the celestial reference systems (and vice versa) could, in principle, be carried out by rotations through three independent

(Eulerian) angles, under the assumption that the origin of the celestial system had been shifted to the geocenter (Richter, 1995). The latter requirement can easily be fulfilled through the shift from the barycentric to the geocentric celestial reference system, cf. [2.4.1]. The rotation based on Eulerian angles would, on the other hand, lead to a series of time-consuming matrix-operations, and a rather unwieldy transformation procedure. This is due to the rapid temporal change of the Eulerian angles which may reach large values.

As a consequence, the terrestrial-to-celestial (and vice-versa) transformation – by convention – has been split into two parts, separating the motion of the pole in the celestial system (precession and nutation, cf. [2.3.2]) from its motion in the terrestrial system (polar motion, cf. [2.3.4]). An intermediate (celestial resp. terrestrial) reference system relates the two systems to each other, which are distorted by a spin (rotation angle GAST resp. ERA) around the common pole axis (Petit and Luzum, 2010; p. 43 ff.).

The transformation is performed through a sequence of rotation matrices, with precession-nutation, Earth rotation angle and polar motion as time-dependent arguments, contingently supplemented by small correction angles. There exist two transformation strategies (the classical equinox-based and the CIO-based, as recommended by IAU2000 resolutions) which differ by the adopted origin on the CIP equator, and the transformation matrices for precession-nutation and Earth rotation. The transformation matrix for polar motion, on the other hand, is common to the two procedures. Using the same input data, both transformation models should deliver identical results.

The *equinox-based transformation* from the Earth-fixed terrestrial reference system ITRS to the space-fixed geocentric reference system GCRS reads as

$$\mathbf{r}_{\text{GCRS}} = \mathbf{P}(t) \mathbf{N}(t) \mathbf{R}_3(-\theta(t)) \mathbf{R}_2(x_p(t)) \mathbf{R}_1(y_p(t)) \mathbf{r}_{\text{ITRS}}, \quad (2.15)$$

where the \mathbf{R}_i ($i = 1, 2, 3$) represent rotation matrices of the corresponding angle around the i -axis, and t is the observation time in Terrestrial Time TT. \mathbf{r}_{GCRS} and \mathbf{r}_{ITRS} are the direction vectors in the space-fixed and the Earth-fixed system, respectively, i.e., the coordinates for points on the celestial resp. terrestrial (unit) sphere. Polar motion is taken into account by the product $\mathbf{R}_2(x_p)\mathbf{R}_1(y_p)$. It follows from rotations about the Y- and X-axis, computed as functions of the pole coordinates x_p and y_p (regarded as small rotation angles) of CIP within the ITRS, cf. [2.3.4]. This transformation step performs the transition from the ITRS to the Terrestrial Intermediate Reference System (TIRS). The Earth's rotation is described by the matrix $\mathbf{R}_3(-\theta)$ containing the rotation angle θ resp. GAST (Greenwich Apparent Sidereal Time), it transforms from the TIRS to the true equinox and equator of date system:

$$\begin{aligned} \mathbf{R}_1(y_p(t)) \mathbf{R}_2(x_p(t)) &= \left(\begin{array}{ccc} 1 & 0 & -x_p \\ 0 & 1 & y_p \\ x_p & -y_p & 1 \end{array} \right) \Bigg\} \\ \mathbf{R}_3(-\theta) &= \left(\begin{array}{ccc} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{array} \right) \Bigg\}. \end{aligned} \quad (2.16a)$$

The nutation matrix \mathbf{N} then transforms from the true equator and vernal equinox to the mean equator and equinox. It contains the obliquity of the ecliptic ε and the nutation angles in obliquity $\Delta\varepsilon$ and in ecliptic longitude $\Delta\psi$, as modeled through series expansions with time (IAU1980 Nutation Theory):

$$\mathbf{N}(t) = \mathbf{R}_1(-\varepsilon(t)) \mathbf{R}_3(\Delta\psi(t)) \mathbf{R}_1(\varepsilon(t) + \Delta\varepsilon(t)). \quad (2.16b)$$

Finally, the precession matrix \mathbf{P} performs the transition to the reference epoch (J2000.0), the corresponding rotation angles again are given by series expansions, which depend on the lunisolar and planetary precession constants (Lieske et al., 1977; see also McCarthy and Petit, 2004; p. 45). By applying the rotations for precession and nutation, the transition from the intermediate reference system to the celestial reference system is completed.

The *CIO-based transformation* (IAU 2000 Resolutions) reads as follows:

$$\mathbf{r}_{\text{GCRS}} = \mathbf{Q}(X_p(t), Y_p(t)) \mathbf{R}_3(s(t)) \mathbf{R}_3(-ERA) \mathbf{R}_3(-s'(t)) \mathbf{R}_2(x_p(t)) \mathbf{R}_1(y_p(t)) \mathbf{r}_{\text{ITRS}}. \quad (2.17)$$

Again, t is the time of observation in TT. The classical polar motion rotation is now supplemented by a very small correction angle s' (TIO locator, $s' = 0$ for J2000.0, and changing about -50 mas/century). It provides the TIO position on the equator corresponding to the definition of the “non-rotating” origin, taking polar motion and polar motion rate into account. The Earth rotation angle ERA is now defined as the angle measured along the CIP equator, between the Celestial and the Terrestrial Intermediate Origin (CIO resp. TIO), cf. [2.4.2]. Precession and nutation have been combined now, and are expressed by a common matrix \mathbf{Q} , containing the CIP coordinates X_p, Y_p in the geocentric celestial reference system, cf. [2.4.1]. Again there is a small correction term s (CIO locator), describing the CIO position on the CIP equator for a CIP moving due to precession and nutation. It can be calculated from the CIP coordinates and coordinate rates in the GCRS.

Summarizing the terrestrial-to-celestial (and vice-versa) transformation procedure, we recognize that there is a fundamental difference in our knowledge of the parameters required at the different steps of rotation. Precession and nutation can be modeled to a high degree, and only small corrections have to be determined by observations: *Celestial Pole Offsets*. The *Earth Rotation Angle* has to be derived from observations of UT1, but can be expressed also by the small difference $\Delta\text{UT} = \text{UT1} - \text{UTC}$, cf. [2.2.2]. *Polar motion*, on the other hand, cannot be modeled, but the corresponding rotation angles are small *a priori*. Consequently, the time-dependent *Earth Orientation Parameters* (EOP) to be determined from observations and published as part of the IERS products [2.4.4] consist of the celestial pole offsets $\Delta X_p, \Delta Y_p$, the pole coordinates x_p and y_p in the terrestrial system, and the Earth rotation angle, provided by UT1-UTC. In addition, the IERS also publishes the observed time rates (linear changes with time) of polar motion and UT1 (length of day excess ΔLOD). The subset of the pole coordinates and the Earth rotation angle is designated also as *Earth Rotation Parameters*. As discussed in this chapter, the Earth orientation parameters are of fundamental importance for metrology, geodesy and navigation. In addition, the observed EOP time series represent an important source of information for geosciences and astronomy, as they contain a multitude of time-variable effects produced by gravitational and geodynamic processes in the Earth system (Schuh et al., 2003; Seitz and Schuh, 2010), cf. [8.3.2].

As already mentioned in [2.4.2], the *space geodetic techniques* exploited at the IERS contribute in different ways to the determination of the Earth orientation parameters. The direct connection to quasars favors VLBI at deriving corrections for *nutation*, which is also the only technique for the determination of *Universal Time*. The long observation series available for Lunar Laser Ranging (LLR) contribute to the evaluation of the long-periodic precession and nutation part, while GPS as realization of a dynamic reference system can only detect short-periodic terms. *Polar motion* can be determined by VLBI and by all satellite techniques, where GPS and DORIS are preferred due to global station coverage and weather independence. Satellite-based techniques are not able to directly determine UT1 and nutation offsets, due to the necessity of estimating simultaneously the satellites' orbital elements. On the other hand, GPS and SLR can be evaluated with respect to the time rate of UT1 (LOD) and of nutation (Rothacher et al., 2001; Schmidt et al., 2010). Polar motion and UT1 are now determined with an accuracy of about 0.1 mas and better for polar motion, and 0.01 ms for UT1, with daily and even subdaily (down to one hour) resolution. Nutation offsets are available every 5 to 7 days, with an accuracy of 0.3 mas and better.

Continuous observations with *ring laser gyroscopes* offer an additional opportunity to particularly monitor short-periodic parts (from hours to days) of the Earth rotation variations, and thus contribute to the detection of regional crustal deformations, among others. This technique is based on two laser beams which propagate in opposite direction around a ring. The effective paths' lengths of the two beams differ due to the co-rotating of the gyroscope with the Earth, which leads to an interference of the corresponding frequencies (Sagnac-effect). The observed beat frequency is proportional to the Earth's rotation vector component normal to the plane of the ring, thus realizing an "absolute" rotation measurement; an external reference frame is not required. With a current sensitivity of 10^{-11} rad/s/ $\sqrt{\text{Hz}}$ and better promising results have been obtained with this technique, e.g., at the Geodetic Observatory Wettzell, Germany (Schreiber et al., 2009).

2.4.4 International Earth Rotation and Reference Systems Service

The International Earth Rotation and Reference Systems Service (IERS) is in charge of defining conventional celestial and terrestrial reference systems as ICRS and ITRS, based on resolutions of the International Astronomical Union (IAU) and the International Union of Geodesy and Geophysics (IUGG). The IERS also provides and maintains the corresponding reference frames ICRF and ITRF as realization of the systems, and it is responsible for the determination of the Earth orientation parameters (EOP), which relate the two frames to each other and which are required to study Earth orientation variations. Finally, IERS collects and releases data related to global geophysical fluids, for interpretation and modeling of time/space variations in the ICRF, ITRF, and EOP. The IERS products are based on models, procedures and constants which follow the research developments and the recommendations of the international scientific unions. Conventions and standards are updated from time to time, keeping continuity with previous rules. The current issue is called IERS Conventions (2010), Petit and Luzum (2010).

Established by the IAU and IUGG, the IERS started operation on January 1, 1988. It replaced the International Polar Motion Service IPMS and the Earth rotation section of BIH, cf. [2.3.4]. The IERS accomplishes its mission through a number of components, which partly are structurally independent but cooperate with IERS.

We especially mention the technique centers, the product centers, and the ITRS combination centers. The *technique centers* comprise several IAG Services specialized on data collection, analyzing and modeling, using a dedicated space geodetic observation technique. The techniques involved include Very Long Baseline Interferometry, Satellite and Lunar Laser Ranging, Global Navigation Satellite Systems (GNSS, today primarily GPS) and DORIS, cf. [5.2] and [5.3]. Data are collected through technique-specific networks, with stations operating either permanently or for a certain time span, containing some hundred observation sites. The individual solutions (ICRF and ITRF coordinates, EOP) are analyzed and further processed by the *product centers*, responsible for the maintenance of the reference frames and for a continuous monitoring and publication of the EOP. The ITRS *combination centers* (Institut Géographique National, Deutsches Geodätisches Forschungsinstitut) combine the ITRF results of the individual technique centers by adjustment, and prepare an updated version of the International Terrestrial Reference Frame, which is released every few years (since 1988, more than ten versions of the ITRF have been published, the last one being ITRF, 2008). The EOP are regularly published by the IERS product center, located at the Observatoire de Paris, and by the U.S. Naval Observatory (Rapid Service with real-time results, Prediction Center); they result from a combination of the time series provided by the individual technique centers.

The IERS *Central Bureau* is located (since 2001) at Bundesamt für Kartographie und Geodäsie BKG, Frankfurt a.M., Germany. The *results* of the IERS are regularly disseminated through bulletins, annual reports, and technical notes. They especially comprise the ICRF and ITRF solutions, which contain the positions of the extragalactic radio sources and the terrestrial stations with station velocities, respectively. Earth orientation data are provided from rapid service and predictions to monthly and long-term results, cf. [2.4.1] to [2.4.3]. Finally, IERS is also responsible for the announcement of UT1 – UTC and the introduction of leap seconds, cf. [2.2.2].

2.5 Local level systems

The majority of classical geodetic and astronomic observations (and naturally also gravity measurements) on or close to the Earth's surface refer to the Earth's gravity field, by orientation along the direction of the plumb line at the point of observation, i.e., the local vertical. An exception is distance measurements (including satellite-based positioning) and very long baseline interferometry, which are independent of the gravity field. Thus, most observations establish local level systems, and modeling requires the relations between these systems and the global geocentric system [2.3.3], Heck (2003a), Hofmann-Wellenhof and Moritz (2005, p. 208 ff.).

The *orientation* of the local system with respect to the global geocentric reference system is given by two angles, defining the direction of the plumb line (Fig. 2.15). The *astronomic (geographic) latitude* Φ is the angle measured in the plane of the meridian between the equatorial plane and the local vertical through the point P . It is reckoned positive from the equator northward and negative to the south. The angle measured in the equatorial plane between the Greenwich meridian plane and the plane of the meridian passing through P is the *astronomic (geographic) longitude* Λ ; it is reckoned positive toward the east. The *gravity potential* W locates P in the system of level surfaces

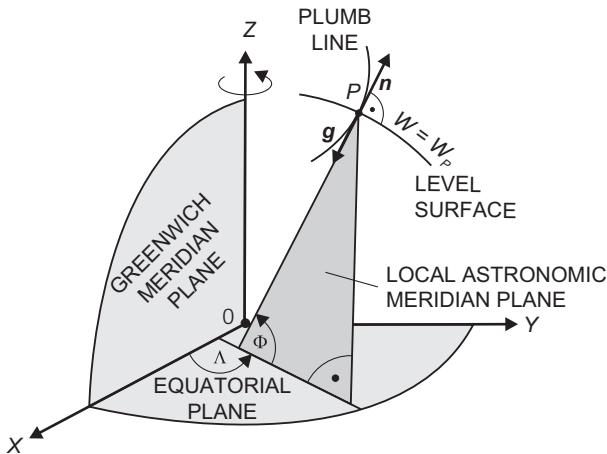


Fig. 2.15: Astronomic latitude and longitude.

$W = \text{const.}$, cf. [3.2.1]. The *local astronomic meridian plane* is spanned by the local vertical at P and a line parallel to the rotational axis, cf. [2.3.1].

We introduce the outer surface normal \mathbf{n} (unit vector), which is normal to the level surface $W = W_p$ and passes through P . It is directed to the zenith, which is opposite of the direction of the gravity vector \mathbf{g} . From Fig. 2.15, we see that

$$\mathbf{n} = -\frac{\mathbf{g}}{g} = \begin{pmatrix} \cos\Phi \cos\Lambda \\ \cos\Phi \sin\Lambda \\ \sin\Phi \end{pmatrix}. \quad (2.18)$$

Latitude Φ and longitude Λ can be determined by the methods of geodetic astronomy, cf. [5.3]. Together with the potential W , they form a triple of three-dimensional coordinates defined in the gravity field, cf. [3.2.3].

We now establish a local three-dimensional Cartesian coordinate system with origin at the point of observation P . The z -axis coincides with the local vertical and points toward the zenith. The x -axis (north) and the y -axis (east) span the horizontal plane, which is tangent to the level surface $W = W_p$; *Local level system*. As the orientation of this left-handed system is given by astronomic quantities (latitude and longitude provide the direction of the z -axis, and the azimuth realizes the x -axis, see below), this system is also called *local astronomic system*.

The *geometric quantities* which can be *observed* within the frame of the local system (representing three-dimensional polar coordinates) include astronomic azimuths, horizontal directions and angles, zenith angles, spatial distances, and leveled height differences.

The *astronomic azimuth* A is the angle measured in the horizontal plane between the astronomic meridian of P and the vertical plane spanned by the vertical through P and the target point P_i . It is positive as measured from the x -axis in a clockwise direction. *Horizontal directions and angles* may be regarded as azimuths lacking orientation, or as azimuth differences. The *zenith angle* (also *zenith distance*) z is the angle measured in the vertical plane between the local vertical and the line joining P and P_i . It is positive

as measured from the outer surface normal (the symbol z is used for the zenith angle and for the zenith-directed coordinate axis of the local level system, this should not lead to confusion). The *spatial distance* s is the length of the straight line joining P and P_i . *Geometric leveling* also refers to the local vertical, providing a height difference with respect to $W = W_p$ over a very short distance. It may be regarded as the boundary case for trigonometric heighting, with a zenith angle of 90° . Finally, we mention *gravity measurements* and measurements of *gravity gradients*, which also refer to the local level system.

According to Fig. 2.16, the position vector between P and P_i is given by

$$\mathbf{x} = \begin{pmatrix} x \\ y \\ z \end{pmatrix} = s \begin{pmatrix} \cos A \sin z \\ \sin A \sin z \\ \cos z \end{pmatrix}. \quad (2.19)$$

This provides the transformation between the local polar and the local Cartesian coordinates.

The local level system is the starting-point for modeling classical *astronomic* and *geodetic* observations.

In *geodetic astronomy*, only direction measurements (zenith angles and azimuths) to celestial bodies are performed. The local system is called the *horizon system*, and the origin is named topocenter. The points of intersection of the plumb-line direction with the celestial sphere are known as the zenithal point Z and the nadir point Z' . The intersection of the horizontal plane with the celestial sphere is the celestial horizon. The azimuth in astronomy is usually reckoned from the south point and is considered positive westward to the north. In the following, the azimuth A will be reckoned in the geodetic sense, i.e., positive from the north. The relation between the horizon system and the equatorial hour angle system, cf. [2.3.1], is given by the astronomic triangle (Fig. 2.17), see also Fig. 2.4. It is formed on the celestial sphere by the vertices P_N (north pole), Z (zenithal point),

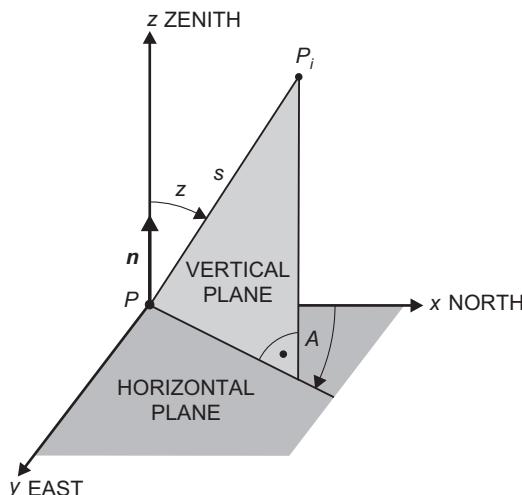


Fig. 2.16: Local level system.

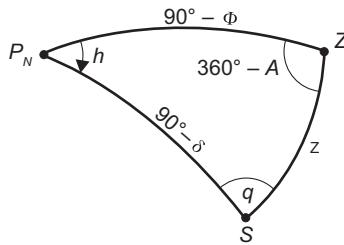


Fig. 2.17: Astronomic triangle.

and S (celestial body). The triangle contains the complements to declination ($90^\circ - \delta$) and astronomic latitude ($90^\circ - \Phi$), the hour angle h , the zenith angle z , the explement of the azimuth ($360^\circ - A$), and the parallactic angle q . From spherical trigonometry we obtain

$$\left. \begin{aligned} \cos A \sin z &= \sin \delta \cos \Phi - \cos \delta \cosh \sin \Phi \\ \sin A \sin z &= -\cos \delta \sinh \\ \cos z &= \sin \delta \sin \Phi + \cos \delta \cosh \cos \Phi \end{aligned} \right\}. \quad (2.20)$$

The transition to the α, δ -system (right ascension α) is given by the local apparent sidereal time LAST, see (2.12):

$$\alpha = \text{LAST} - h. \quad (2.21)$$

Astronomic longitude Λ is obtained by comparing LAST with the Greenwich sidereal time (2.5):

$$\Lambda = \text{LAST} - \text{GAST}. \quad (2.22)$$

Equations (2.20) to (2.22) are the fundamental equations for determining Φ , Λ and A from measurements of z and GAST at given α, δ , cf. [5.3.2]. Equation (2.20) also follows from (2.19) if we take (2.10) and (2.28) into account. Here again we remember the modified definitions of the right ascension and the Earth rotation angle as introduced with the IAU2000 resolutions, cf. [2.4]. These modifications do not affect the transformation procedures described in this chapter.

For geodetic applications, the observations carried out in the local level systems have to be transformed into the global geocentric system for further use in establishing geodetic control networks. Due to the non-parallelism of the plumb lines, the orientation of the local level systems depends on position and thus changes rapidly from place to place. Computations in one individual system are therefore admissible only in very limited areas when applying formulas of plane geometry.

As we have seen, the plumb line direction can be referred to the global geocentric system by means of the “orientation” parameters astronomic latitude Φ and longitude Λ (Fig. 2.18). After a parallel shift of the global system into the local one (Fig. 2.16), we transform the latter one to a right-handed system by applying the reflection matrix

$$\mathbf{S}_2 = \begin{pmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix}. \quad (2.23)$$

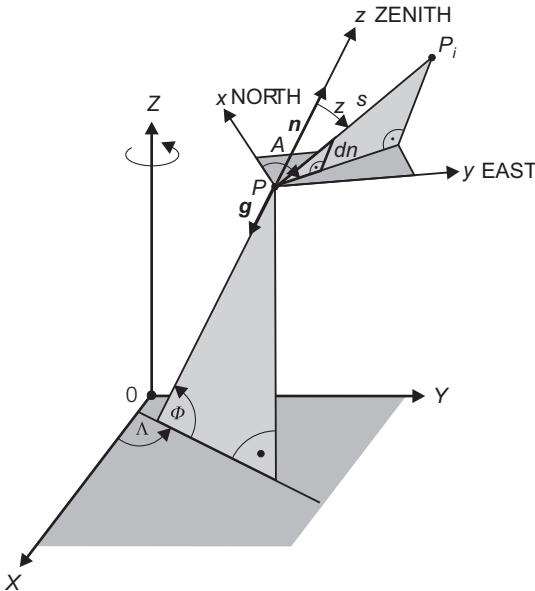


Fig. 2.18: Local level and global geocentric system.

We then rotate the local system by $90^\circ - \Phi$ around the (new) y -axis and by $180^\circ - \Lambda$ around the z -axis with the rotation matrices

$$\mathbf{R}_2(90^\circ - \Phi) = \begin{pmatrix} \sin\Phi & 0 & -\cos\Phi \\ 0 & 1 & 0 \\ \cos\Phi & 0 & \sin\Phi \end{pmatrix} \text{ and}$$

$$\mathbf{R}_3(180^\circ - \Lambda) = \begin{pmatrix} -\cos\Lambda & \sin\Lambda & 0 \\ -\sin\Lambda & -\cos\Lambda & 0 \\ 0 & 0 & 1 \end{pmatrix}. \quad (2.24)$$

Coordinate differences between P_i and P in the geocentric system are thus obtained by

$$\Delta \mathbf{x} = \mathbf{A} \mathbf{x}, \quad (2.25)$$

with \mathbf{x} given by (2.19) and

$$\Delta \mathbf{x} = \begin{pmatrix} \Delta X \\ \Delta Y \\ \Delta Z \end{pmatrix}. \quad (2.26)$$

The transformation matrix reads as

$$\mathbf{A} = \mathbf{R}_3(180^\circ - \Lambda) \mathbf{R}_2(90^\circ - \Phi) \mathbf{S}_2 = \begin{pmatrix} -\sin\Phi \cos\Lambda & -\sin\Lambda & \cos\Phi \cos\Lambda \\ -\sin\Phi \sin\Lambda & \cos\Lambda & \cos\Phi \sin\Lambda \\ \cos\Phi & 0 & \sin\Phi \end{pmatrix}. \quad (2.27)$$

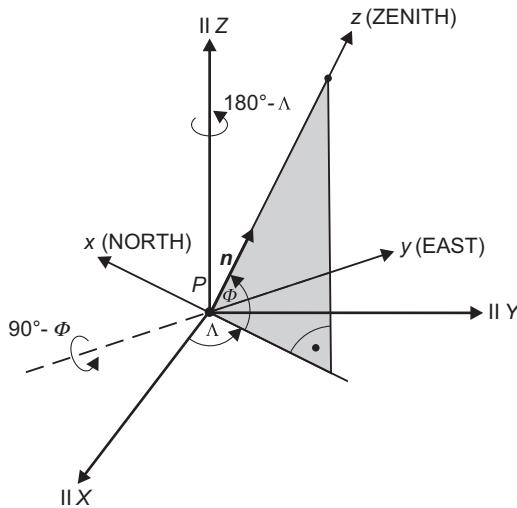


Fig. 2.19: Transformation between the local level and the global geocentric system.

The inversion of (2.25) is performed easily considering that \mathbf{A} is orthonormal:

$$\mathbf{A}^{-1} = \mathbf{A}^T.$$

We obtain

$$\mathbf{x} = \mathbf{A}^{-1} \Delta \mathbf{x}, \quad (2.28)$$

with

$$\mathbf{A}^{-1} = \begin{pmatrix} -\sin\Phi \cos\Lambda & -\sin\Phi \sin\Lambda & \cos\Phi \\ -\sin\Lambda & \cos\Lambda & 0 \\ \cos\Phi \cos\Lambda & \cos\Phi \sin\Lambda & \sin\Phi \end{pmatrix}. \quad (2.29)$$

Equations (2.25) to (2.29) are the basic equations for the evaluation of local geodetic measurements within the three-dimensional reference frame, cf. [6.2.1].

3 The Gravity Field of the Earth

The external gravity field plays a fundamental role in geodesy. The figure of the Earth has evolved primarily under the effect of gravity, and most geodetic observations refer to the gravity field. Geodetic modeling thus requires consideration of gravity, this includes satellite orbit calculations and geoid determination. In addition, the analysis of the (time-variable) external gravity field yields information on the distribution and movement of the Earth's masses; in this way geodesy significantly contributes not only to solid Earth physics and oceanography, but also to atmospheric sciences and hydrology.

The fundamental quantities gravitation and gravity, together with their corresponding potentials, are introduced in [3.1], where the main properties of the gravity field are also described. The geometry of the gravity field is especially important for local applications [3.2], while the spherical harmonic expansion provides a powerful tool for a global gravity-field representation [3.3]. The geoid, as a physically defined figure of the Earth and reference surface for heights, is of basic interest in geosciences and engineering [3.4]. Gravity variations with time can be modeled in part (e.g., tidal effects), but to a large degree monitoring and modeling of these effects is still in the research stage [3.5].

The theory of the gravity field is extensively treated in geodetic and geophysical literature, e.g., Heiskanen and Moritz (1967), Jeffreys (1970), Hofmann-Wellenhof and Moritz (2005), Lowrie (2007), also Jekeli (2009).

3.1 Fundamentals of gravity field theory

A body on the Earth's surface experiences the gravitational force of the masses of the Earth, [3.1.1] to [3.1.3], and other celestial bodies as well as the centrifugal force due to the Earth's rotation [3.1.4]. The resultant is the force of gravity [3.1.5]. In the case of artificial satellites, it is noted that a satellite does not rotate with the Earth; hence, only gravitation acts on the satellite, neglecting non-gravitational forces as atmospheric air drag for the moment.

3.1.1 Gravitation, gravitational potential

According to Newton's Law of Gravitation (1687), two point masses m_1 and m_2 attract each other with the gravitational force (attractive force)

$$\mathbf{K} = -G \frac{m_1 m_2}{l^2} \frac{\mathbf{l}}{l'} \quad (3.1)$$

where G is the gravitational constant, cf. [2.1],

$$G = 6.674 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2}, \quad (3.2)$$

(G -value according to the IERS Conventions, Petit and Luzum, 2010), and l is the distance between the masses. The vectors \mathbf{K} and \mathbf{l} point in opposing directions. The SI unit of \mathbf{K} is m kg s^{-1} .

By setting the mass at the attracted point P to unity, (3.1) transforms into the gravitational acceleration (henceforth also termed gravitation):

$$\mathbf{b} = -G \frac{m \mathbf{l}}{l^2} \quad (3.3)$$

\mathbf{b} originates at P and is directed towards the source point P' with mass m . The distance vector \mathbf{l} may be expressed by the position vectors \mathbf{r} and \mathbf{r}' (Fig. 3.1), e.g., in the global Cartesian X , Y , Z system:

$$\mathbf{l} = \mathbf{r} - \mathbf{r}' = (X, Y, Z), \text{ and } \mathbf{r}' = (X', Y', Z'), \quad (3.4a)$$

with

$$l = |\mathbf{l}| = \sqrt{(X - X')^2 + (Y - Y')^2 + (Z - Z')^2}. \quad (3.4b)$$

The unit of the acceleration \mathbf{b} is m s^{-2} .

According to (3.3), gravitation depends only on the distance between the attracting mass and the attracted point, it does *not* depend on the coordinate system! While global applications require a geocentric coordinate system, local coordinate systems are useful for solving problems of limited spatial extent.

The *Earth* is composed of an infinite number of differential mass elements dm . The gravitation on the unit mass at P results from the integral over the individual contributions. Equation (3.3) correspondingly transforms to

$$\mathbf{b} = \mathbf{b}(\mathbf{r}) = -G \iiint_{\text{Earth}} \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} dm. \quad (3.5)$$

The mass element dm can also be expressed by the volume density $\rho = \rho(\mathbf{r}')$ and the volume element dv :

$$dm = \rho dv, \quad (3.6)$$

where ρ is expressed in kg m^{-3} .

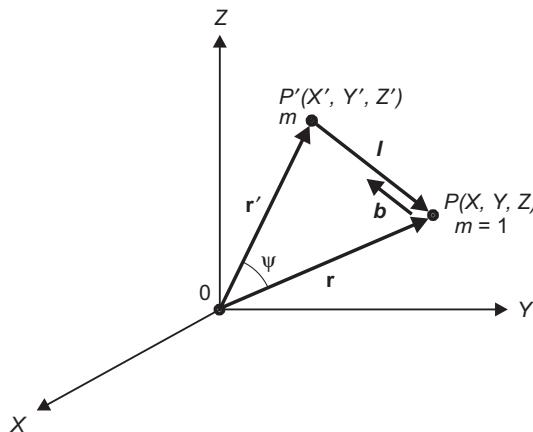


Fig. 3.1: Gravitation.

The representation of gravitational acceleration, the gravity field, and related computations are simplified if the scalar quantity “*potential*” is used instead of the vector quantity “*acceleration*”. Because the gravitational field is invariant to rotations:

$$\operatorname{curl} \mathbf{b} = \mathbf{0}, \quad (3.7)$$

the vector \mathbf{b} may be represented as the gradient of a potential V (e.g., Kellogg, 1929; Sigl, 1985):

$$\mathbf{b} = \operatorname{grad} V. \quad (3.8)$$

For a *point mass* m , see (3.3), we have

$$V = \frac{Gm}{r}, \text{ with } \lim_{r \rightarrow \infty} V = 0. \quad (3.9)$$

For the *Earth*, see (3.5) and (3.6), we obtain

$$V = V(\mathbf{r}) = G \iiint_{\text{Earth}} \frac{dm}{r} = G \iiint_{\text{Earth}} \frac{\rho}{r} dv, \lim_{r \rightarrow \infty} V = 0. \quad (3.10)$$

The potential at P indicates the work that must be done by gravitation in order to move the unit mass from infinity ($V = 0$) to P . The unit of potential is $\text{m}^2 \text{s}^{-2}$.

If the density function $\rho = \rho(\mathbf{r}')$ were known for the Earth, (3.5) resp. (3.10) would permit *calculation* of the gravitation as a function of position. In reality, more detailed density information is available merely for the upper layers of the Earth, while global models generally consider radial density changes only, cf. [3.1.2], [8.1]. Consequently, gravity field *observations* have to be used in order to model the exterior gravity field.

3.1.2 Gravitation of a spherically symmetric Earth

To a first approximation, the Earth can be viewed as a sphere with a centrally symmetric density structure, i.e., composed of spherical shells with constant density, cf. [8.1]. We calculate the gravitation in the interior and exterior of such a shell using the system of spherical coordinates r, ϑ, λ introduced in (2.14). For this purpose, the orientation of the system is changed such that the ϑ -axis coincides with the line joining the coordinate origin O and the calculation point P (Fig. 3.2).

The potential of a homogeneous *spherical shell* of radius r' with infinitesimal thickness dr' , density ρ and surface mass element dm (surface or single layer potential) is now given in analogy to (3.10) by

$$V_s = G \mu \iint_S \frac{dS}{r}. \quad (3.11a)$$

with the constant surface density

$$\mu = \frac{dm}{dS} = \rho dr'. \quad (3.11b)$$

Here, integration is over the surface of the shell S and

$$dS = r'^2 \sin \vartheta' d\vartheta' d\lambda' \quad (3.12)$$

is the surface element. Inserting (3.12) into (3.11) gives

$$V_s = G \mu r'^2 \int_{\lambda'=0}^{2\pi} \int_{\vartheta'=0}^{\pi} \frac{\sin \vartheta'}{r'} d\vartheta' d\lambda'. \quad (3.13)$$

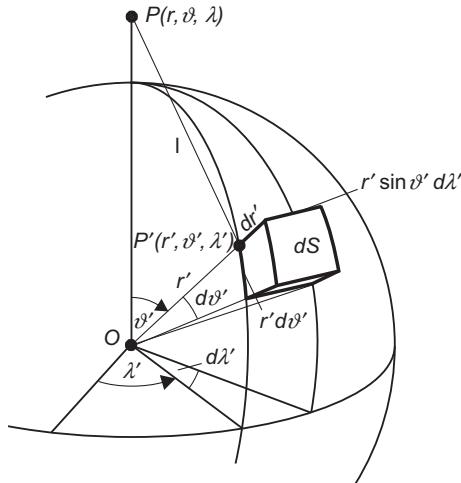


Fig. 3.2: Surface element of a spherical shell.

At integrating (3.13), a distinction has to be made as to whether the attracted point P is exterior or interior to the spherical shell (Fig 3.3). In order to simplify the integration, the variable l is introduced instead of ϑ' , using the triangle POP' (e.g., Sigl, 1985). For an attracted point lying in the exterior ($r > r'$), the potential is then given by

$$V_{se} = 4\pi G \mu \frac{r'^2}{r} = G \frac{m}{r} \quad (3.14)$$

Here,

$$m = 4\pi \mu r'^2 \quad (3.15)$$

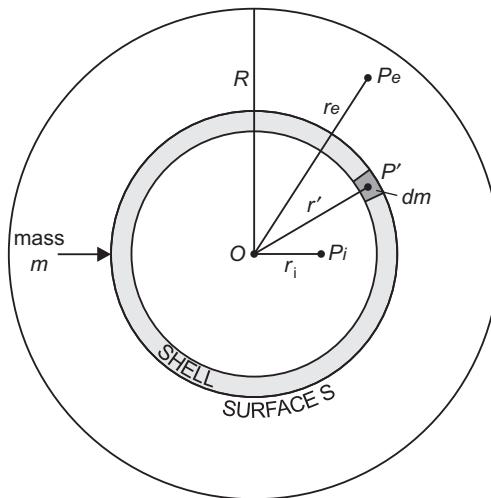


Fig. 3.3: Gravitation exterior and interior of a spherical shell.

represents the mass of the spherical shell. By comparing with (3.9) we recognize that the result is equal to the potential of the mass concentrated in the center of the sphere. The potential of the *spherical Earth* composed of concentric homogeneous shells consequently is

$$V_e = G \iiint_{\text{Earth}} \frac{dm}{r} = \frac{GM}{r}. \quad (3.16)$$

It is equal to the potential of the entire mass M of the Earth concentrated at the center of mass. The gravitation follows from

$$b_e = -\frac{\partial V_e}{\partial r} = \frac{GM}{r^2}. \quad (3.17)$$

With $GM = 398.6 \times 10^{12} \text{ m}^3 \text{ s}^{-2}$ and the radius of the Earth $R = 6371 \text{ km}$, the potential at the surface of the Earth ($r = R$) amounts to $V = 6.26 \times 10^7 \text{ m}^2 \text{ s}^{-2}$, and the gravitation is $b = 9.82 \text{ m s}^{-2}$.

For a point in the *interior* ($r < r'$), we easily obtain from (3.13) for the potential of the spherical shell:

$$V_{si} = 4\pi G\mu r' = \frac{Gm}{r'}. \quad (3.18)$$

Here, V_{si} is constant; therefore, the gravitation is zero:

$$b_{si} = -\frac{\partial V_{si}}{\partial r} = 0. \quad (3.19)$$

The potential inside an *Earth* constructed of homogeneous *shells* includes the contribution of the masses interior to the sphere $r = \text{const.}$ (3.14), and the contribution of the spherical shell having thickness $R - r$ (3.18). After substituting the surface density μ through the volume density ρ , we obtain

$$V_i = \frac{4\pi G}{r} \int_0^r \rho r'^2 dr' + 4\pi G \int_r^R \rho r' dr'. \quad (3.20)$$

For a *homogeneous Earth* ($\rho = \text{const.}$) we have

$$V_i = \frac{4}{3}\pi G\rho r^2 + 2\pi G\rho(R^2 - r^2) = 2\pi G\rho \left(R^2 - \frac{r^2}{3} \right). \quad (3.21)$$

From (3.20) we obtain the gravitation of an Earth composed of spherical *shells*:

$$b_i = -\frac{\partial V_i}{\partial r} = G \frac{M_i}{r^2} \quad (3.22)$$

with

$$M_i = 4\pi \int_0^r \rho r'^2 dr' \quad (3.23)$$

according to (3.15), which represents the mass inside the sphere $r = \text{const.}$ The masses outside this sphere have no effect on the gravitation. For a *homogeneous sphere* ($\rho = \text{const.}$), (3.22) can be written as

$$b_i = \frac{4}{3}\pi G\rho r. \quad (3.24)$$

3.1.3 Properties of the gravitational potential

We now investigate the fundamental properties of the gravitational potential and its first and second derivatives.

Starting from the Earth's potential (3.10)

$$V = G \iiint_{\text{Earth}} \frac{dm}{l}, \quad (3.25)$$

gravitation is given by the gradient (3.8). In the X, Y, Z system, it has the components, see (3.5),

$$\frac{\partial V}{\partial X} = V_x = -G \iiint_{\text{Earth}} \frac{X - X'}{l^3} dm, \text{ etc.} \quad (3.26)$$

The second derivatives read as

$$\frac{\partial^2 V}{\partial X^2} = V_{xx} = -G \iiint_{\text{Earth}} \frac{dm}{l^3} + 3G \iiint_{\text{Earth}} \frac{(X - X')^2}{l^5} dm, \text{ etc.} \quad (3.27)$$

We now again have to distinguish between the cases where the attracted point P lies exterior or interior to the Earth's masses, cf. [3.1.2]. Here, we neglect the mass of the atmosphere (about 10^{-6} of the total mass) and the variations of gravitation with time (maximum relative effect about 10^{-7}). The Earth's surface S then constitutes a boundary surface between the mass-free exterior space and the Earth's interior.

If P lies exterior to the surface S , we have $l > 0$ always. Then according to (3.25)–(3.27), the potential and its first and second derivatives are single-valued, finite and continuous functions, vanishing at infinity.

We now apply the Laplacian differential operator $\Delta = \operatorname{div} \operatorname{grad}$ to V . In the X, Y, Z -system, this reads as

$$\Delta V = V_{xx} + V_{yy} + V_{zz}. \quad (3.28)$$

When introducing (3.27) into (3.28), the first and second terms cancel each other. This leads to *Laplace's differential equation* of second order, which governs the exterior gravitational field:

$$\Delta V = 0. \quad (3.29)$$

Continuous functions, having continuous first and second order derivatives and fulfilling (3.29), are called *harmonic functions*.

If the attracted point lies *inside* the body of the Earth, then the case $l = 0$ is possible. This requires special attention because of the discontinuity of $1/l$.

To this end, we consider P enclosed by a sphere K (center at P_0 , radius p), where p is chosen sufficiently small so that the density $\rho = \text{const.}$ inside K (Fig. 3.4). The potential at P is composed of the contributions from masses lying interior and exterior to K . From (3.10) and (3.21) and using

$$R = p, r = q = \sqrt{(X - X_0)^2 + (Y - Y_0)^2 + (Z - Z_0)^2},$$

we find

$$V = G \iiint_{\text{Earth}-K} \frac{dm}{l} + 2\pi G \rho \left(p^2 - \frac{q^2}{3} \right).$$

In the limits $p \rightarrow 0$ and $q \rightarrow 0$, agreement is obtained with the expression for the exterior potential (3.10). Differentiation yields

$$V_x = -G \iiint_{\text{Earth}-K} \frac{X - X'}{l^3} dm - \frac{4}{3}\pi G \rho (X - X_0), \text{ etc.}$$

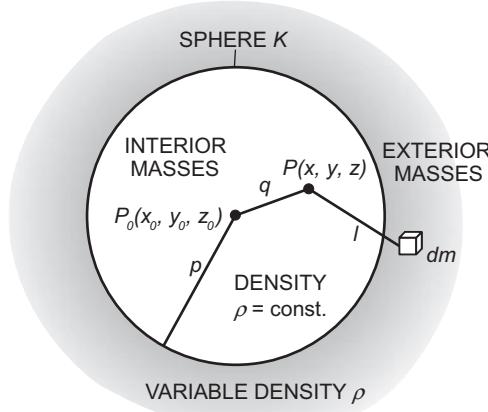


Fig. 3.4: Gravitational potential inside the Earth.

As $q \rightarrow 0$, we also have $X - X_0 \rightarrow 0$, $Y - Y_0 \rightarrow 0$, $Z - Z_0 \rightarrow 0$, so that once again we obtain agreement with the exterior case (3.26). The second derivatives are given by

$$V_{xx} = -G \iiint_{\text{Earth-K}} \frac{1}{l^3} dm + 3G \iiint_{\text{Earth-K}} \frac{(X - X')^2}{l^5} dm - \frac{4}{3}\pi G\rho, \text{ etc.}$$

For $q \rightarrow 0$, the last term does not vanish, and we obtain:

$$V_{xx} = -\frac{4}{3}\pi G\rho, \text{ etc.} \quad (3.30)$$

The gravitational potential and its first derivatives are thus single-valued, finite, and continuous in the interior as well. According to (3.30), the second derivatives exhibit discontinuities at abrupt changes in density. Inserting (3.30) into (3.28), we get *Poisson's differential equation*:

$$\Delta V = -4\pi G\rho. \quad (3.31)$$

Hence, V is *not* a harmonic function in the interior of the Earth.

Finally, we mention *Gauss' integral formula*, which connects the normal derivatives $\partial V / \partial n_s$ on any boundary surface S (which in general is *not* an equipotential surface) and the second derivatives contained in the Laplace operator (3.28):

$$\iint_S \frac{\partial V}{\partial n_s} dS = \iiint_v \Delta V dv. \quad (3.32)$$

Here, v is the volume of the body of surface S (Fig. 3.5). The left-hand term may be interpreted as "gravitational flux" through S . As shown in potential theory, it is proportional to the total mass

$$M = \iiint_v dm = \iiint_v \rho(\mathbf{r}') dv \quad (3.33)$$

according to

$$\iint_S \frac{\partial V}{\partial n_s} dS = -4\pi GM. \quad (3.34)$$

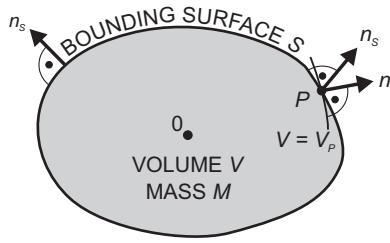


Fig. 3.5: Outer surface normal on the bounding surface and on the equipotential surface.

Taking the limit at the source point P' in (3.34), equation (3.32) reduces to Poisson's differential equation (3.31) and to Laplace's differential equation for the exterior space ($\rho = 0$). Based on Gauss' formula, basic relationships can be established between observations in the gravity field and parameters describing the surface S , cf. [6.5.1].

3.1.4 Centrifugal acceleration, centrifugal potential

The centrifugal force acts on any object of mass of the Earth. It arises as a result of the rotation of the Earth about its axis. We assume here a rotation of constant angular velocity ω about the rotation (or spin) axis, with the axis assumed fixed with the Earth. The small effects of time variations of the rotation vector can be taken into account by reductions, cf. [2.3.4]. The *centrifugal acceleration*

$$\mathbf{z} = (\boldsymbol{\omega} \times \mathbf{r}) \times \boldsymbol{\omega} = \omega^2 \mathbf{p} \quad (3.35a)$$

acting on a unit mass is directed outward and is perpendicular to the spin axis (Fig. 3.6). With the geocentric latitude $\bar{\varphi}$, we have the distance to the rotation axis

$$p = r \cos \bar{\varphi}$$

and the magnitude of the centrifugal acceleration

$$z = |\mathbf{z}| = \omega^2 r \cos \bar{\varphi}. \quad (3.35b)$$

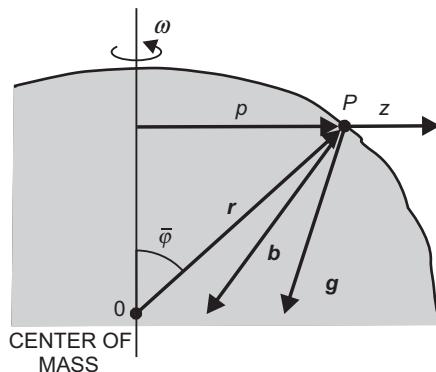


Fig. 3.6: Gravitation, centrifugal acceleration, and gravity.

The angular velocity

$$\omega = 7.292\ 115 \times 10^{-5} \text{ rad s}^{-1} \quad (3.36)$$

is known with high accuracy from astronomy, cf. [2.2.2]. Consequently, the centrifugal acceleration $\mathbf{z} = |\mathbf{z}|$ can be calculated if the position of P is known.

As the Z -axis of the Earth-fixed X, Y, Z -system coincides with the axis of rotation, cf. [2.4.2], we have

$$\mathbf{p} = \begin{pmatrix} X \\ Y \\ 0 \end{pmatrix}, p = |\mathbf{p}| = \sqrt{X^2 + Y^2}.$$

With

$$\mathbf{z} = \text{grad } Z, \quad (3.37)$$

we introduce the *centrifugal potential*

$$Z = Z(p) = \frac{\omega^2}{2} p^2, \lim_{p \rightarrow 0} Z = 0. \quad (3.38)$$

Remark: Here, the symbols z and Z are used for the centrifugal acceleration and potential, respectively. They were introduced earlier for local and global coordinates and will be employed again as such in later sections.

Differentiating twice and applying the Laplacian operator yields

$$\Delta Z = 2 \omega^2. \quad (3.39)$$

Therefore, the analytic function Z , as opposed to V (3.29), is not harmonic.

For points on the equator of the Earth, the centrifugal potential has a value of $1.1 \times 10^5 \text{ m}^2 \text{s}^{-2}$, and the centrifugal acceleration is 0.03 m s^{-2} ($\approx 0.3\%$ of gravitation). At the poles, we have $Z = 0$ and $z = 0$.

3.1.5 Gravity acceleration, gravity potential

The gravity acceleration, or *gravity* \mathbf{g} (Latin: *gravitas*), is the resultant of gravitation \mathbf{b} and centrifugal acceleration \mathbf{z} (Fig. 3.6):

$$\mathbf{g} = \mathbf{b} + \mathbf{z}. \quad (3.40)$$

By multiplying with the mass m of the attracted point, we obtain the force of gravity

$$\mathbf{F} = m\mathbf{g}. \quad (3.41)$$

The direction of \mathbf{g} is referred to as the direction of the *plumb line* (vertical); the magnitude g is called gravity intensity (generally just gravity). With (3.10) and (3.38), the *gravity potential* of the Earth becomes

$$W = W(\mathbf{r}) = V + Z = G \iiint_{\text{Earth}} \frac{\rho}{l} dv + \frac{\omega^2}{2} p^2. \quad (3.42)$$

It is related to the *gravity acceleration* by

$$\mathbf{g} = \text{grad } W. \quad (3.43)$$

In the X, Y, Z -system, we have

$$\mathbf{g}^T = (\text{grad } W)^T = (W_x \ W_y \ W_z). \quad (3.44)$$

Taking (2.18) into account, we obtain the components of gravity expressed by the plumb line parameters astronomical latitude and longitude Φ, Λ :

$$\mathbf{g} = -g\mathbf{n} = -g \begin{pmatrix} \cos\Phi \cos\Lambda \\ \cos\Phi \sin\Lambda \\ \sin\Phi \end{pmatrix}. \quad (3.45)$$

The property

$$\text{curl } \mathbf{g} = \text{curl grad } W = 0 \quad (3.46)$$

follows from the corresponding properties of gravitation and centrifugal acceleration and can also be expressed by the conditions

$$W_{xy} = W_{yx}, \ W_{xz} = W_{zx}, \ W_{yz} = W_{zy} \quad (3.47)$$

W and its first derivatives are single-valued, finite, and continuous in the whole space as a consequence of the characteristics of V and Z . Exceptions are the uninteresting cases $r \rightarrow \infty$ (then also $Z \rightarrow \infty$) and $g = 0$ (direction of the plumb line is not unique). Due to the behavior of V , the second derivatives of W are discontinuous inside the Earth at abrupt density changes. For geodesy, the most important surface of discontinuity is the physical surface of the Earth, with a density jump from 1.3 kg m^{-3} (density of air) to 2700 kg m^{-3} (mean density of the upper crust).

From (3.31) and (3.39), we obtain the generalized Poisson differential equation

$$\Delta W = -4\pi G\rho + 2\omega^2. \quad (3.48)$$

In outer space ($\rho = 0$), it becomes the generalized Laplace differential equation

$$\Delta W = 2\omega^2. \quad (3.49)$$

With the conditions (3.47) and (3.48) resp. (3.49), the gravity potential W possesses only five (out of nine) mutually independent second derivatives. They are closely related to the curvature of the level surfaces and the plumb lines, cf. [3.2.2].

Because of the flattening at the Earth's poles and the centrifugal acceleration, g depends on the latitude. As found in [3.1.2], the gravitation for a *spherical* model is 9.82 m s^{-2} , this value decreases at the equator and increases at the poles of an *ellipsoidal* model. The centrifugal acceleration further diminishes the equatorial value, while gravitation at the poles is not affected by centrifugal acceleration, cf. [3.1.4]. As a result, gravity varies between 9.78 m s^{-2} (equator) and 9.83 m s^{-2} (poles), see also [4.3].

3.2 Geometry of the gravity field

A geometrical representation of the gravity field is given by the level surfaces and the plumb lines [3.2.1]. Local field properties are described by the curvatures of level surfaces and plumb lines [3.2.2], and a system of "natural" coordinates can be based on these properties [3.2.3].

3.2.1 Level surfaces and plumb lines

The surfaces of constant gravity potential

$$W = W(\mathbf{r}) = \text{const.} \quad (3.50)$$

are designated as *equipotential* or *level surfaces* (also geopotential surfaces) of gravity. As a result of an infinitesimal displacement $d\mathbf{s}$, and in view of (3.43), the potential difference of differentially separated level surfaces (Fig. 3.7) is given by

$$dW = \mathbf{g} \cdot d\mathbf{s} = g ds \cos(\mathbf{g}, d\mathbf{s}). \quad (3.51)$$

This means that the derivative of the gravity potential in a certain direction is equal to the component of gravity along this direction. Since only the projection of $d\mathbf{s}$ along the plumb line enters into (3.51), dW is independent of the path. Hence, no work is necessary for a displacement along the level surface $W = \text{const.}$: the level surfaces are *equilibrium* surfaces.

If $d\mathbf{s}$ is taken along the level surface $W = W_p$, then it follows from $dW = 0$ that $\cos(\mathbf{g}, d\mathbf{s}) = \cos 90^\circ = 0$: gravity is normal to $W = W_p$, or, in other words, the level surfaces are intersected at right angles by the *plumb lines*. The tangent to the plumb line is called the *direction* of the plumb line and has been defined already in [3.1.5]. If $d\mathbf{s}$ is directed along the outer surface normal \mathbf{n} , then, because $\cos(\mathbf{g}, \mathbf{n}) = \cos 180^\circ = -1$, the following important differential relationship exists:

$$dW = -g dn. \quad (3.52)$$

It provides the link between the potential difference (a physical quantity) and the difference in height (a geometric quantity) of neighboring level surfaces. According to this relation, a combination of gravity measurements and (quasi) differential height determinations, as provided by geometric leveling, delivers gravity potential differences, cf. [5.5.4].

If g varies on a level surface, then, according to (3.52), the distance dn to a neighboring level surface also changes. Therefore, the level surfaces are not parallel, and the plumb lines are space curves. As a consequence of the gravity increase of 0.05 m s^{-2} from the equator to the poles, the level surfaces of the Earth converge toward the poles by $0.05 \text{ m s}^{-2}/9.8 \text{ m s}^{-2}$, or 5×10^{-3} , in a relative sense. For example, two level surfaces that are 100.0 m apart at the equator are separated by only 99.5 m at the poles (Fig. 3.8).

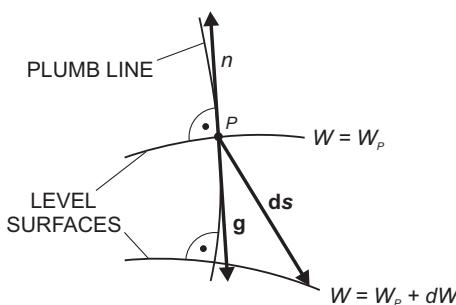


Fig. 3.7: Neighboring level surfaces and plumb line.

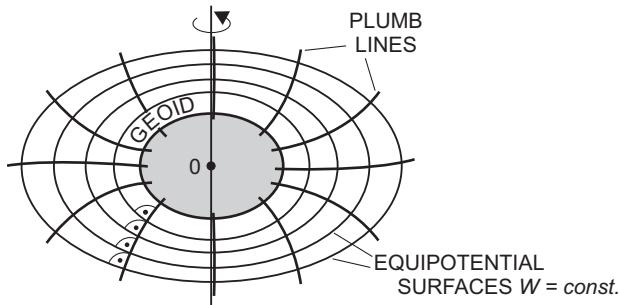


Fig. 3.8: Equipotential surfaces and plumb lines close to the Earth.

The level surfaces inside the Earth and in the exterior space are closed spheroidal surfaces. The geoid is the level surface that approximates mean sea level. Because of its importance as a reference surface for heights, it will be treated separately in [3.4]. As an outer limit in the realm of the definition of gravity, one may consider the level surface for which the gravitation and centrifugal acceleration in the equatorial plane cancel each other. The equatorial radius of this surface would be 42 200 km.

The concept of the level surface was introduced by *MacLaurin* (1742), whereas *Clairaut* (1743) thoroughly discussed level surfaces and plumb lines as a whole. Bruns (1878) included the determination of the exterior level surfaces in their entirety in the fundamental problem of geodesy.

3.2.2 Local gravity field representation

From the properties of the potential function $W = W(\mathbf{r})$, it follows that the level surfaces which lie entirely in the exterior space are analytical surfaces; that is, they have no salient or singular points, cf. [3.1.5], and can be expanded in Taylor series. Level surfaces extending partially or completely inside the Earth exhibit discontinuities in the second derivatives where density jumps occur. These surfaces can thus be constructed from pieces of different analytical surfaces only. Local gravity field observables are obtained with gravity meters and gravity gradiometers, they play an important role at high resolution gravity field modeling (Baeschlin, 1948; Hofmann-Wellenhof and Moritz, 2005).

Using the local astronomic x, y, z -system introduced in [2.5], we develop the potential W in the vicinity of the origin P into a series. This local representation reads as

$$\begin{aligned} W = W_p + W_x x + W_y y + W_z z + \frac{1}{2} (W_{xx} x^2 + W_{yy} y^2 + W_{zz} z^2) \\ + W_{xy} xy + W_{xz} xz + W_{yz} yz + \dots \end{aligned} \quad (3.53)$$

Here, $W_x = \partial W / \partial x$, $W_{xx} = \partial^2 W / \partial x^2$, $W_{xy} = \partial^2 W / \partial x \partial y$, etc. represent the first and second order partial derivatives at P in the local system. If the calculation point is located on the level surface through P , we have

$$W = W_p, W_x = W_y = 0, W_z = -g.$$

By solving for z , we get the equation of the *level surface* in the neighborhood of P :

$$z = \frac{1}{2g} (W_{xx} x^2 + 2W_{xy} xy + W_{yy} y^2) + \dots \quad (3.54)$$

Here, we have neglected terms of third and higher order, taking into account that z is of second order compared to x and y , due to the small curvature of the level surfaces.

The curvature of the *level surface* at P along an azimuth A is described by the curvature of the normal section (intersection of the vertical plane with the surface), which is called normal curvature. We now apply the well-known formula for the depression of a sphere (local approximation to the level surface) with respect to the horizontal x, y -plane

$$z = -\frac{s^2}{2R_A}, \quad (3.55)$$

with distance s from P , and radius of curvature R_A in the azimuth A (Fig. 3.9). By introducing (3.55) into (3.54), and substituting x, y with the local polar coordinates s, A

$$x = s \cos A, \quad y = s \sin A,$$

we obtain the *normal curvature*

$$k = \frac{1}{R_A} = -\frac{1}{g} (W_{xx} \cos^2 A + 2W_{xy} \sin A \cos A + W_{yy} \sin^2 A). \quad (3.56)$$

For the x - and y -directions ($A = 0^\circ$ and $A = 90^\circ$), we obtain the curvatures

$$k_x = \frac{1}{R_x} = -\frac{W_{xx}}{g}, \quad k_y = \frac{1}{R_y} = -\frac{W_{yy}}{g}, \quad (3.57)$$

where R_x and R_y are the corresponding curvature radii. Analogously, the geodetic torsion in the direction of the meridian (expressing the change of direction normal to the meridian) is given by

$$t_x = -\frac{W_{xy}}{g}. \quad (3.58)$$

The normal curvature assumes its extreme values in the mutually perpendicular directions of *principal curvature* A_1 and $A_2 = A_1 \pm 90^\circ$. By considering the extrema, we find

$$\tan 2A_{1,2} = 2 \frac{W_{xy}}{W_{xx} - W_{yy}}. \quad (3.59)$$

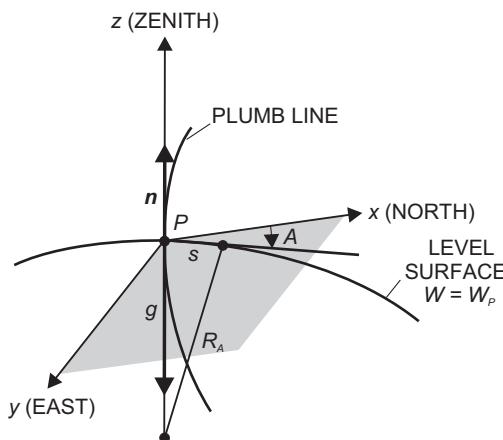


Fig. 3.9: Curvature of level surfaces and plumb lines.

Introducing (3.59) into (3.56) yields the corresponding principal curvatures

$$\frac{1}{R_{A_1}} = -\frac{1}{g}(W_{xx} + W_{xy}\tan A_1), \quad \frac{1}{R_{A_2}} = -\frac{1}{g}(W_{yy} + W_{xy}\cot A_2). \quad (3.60)$$

With $A_2 = A_1 + 90^\circ$, the *mean curvature* of the level surface is given by

$$J = \frac{1}{2}(k_x + k_y) = -\frac{1}{2g}(W_{xx} + W_{yy}). \quad (3.61)$$

Outside the masses of the Earth, the *plumb lines* can also be described analytically. In the local astronomic system, the equation of the plumb line is given by

$$x = x(s), \quad y = y(s), \quad z = z(s), \quad (3.62)$$

where s now is the arc length reckoned in the direction of gravity (Fig. 3.9). The line element along s thus differs from gravity only by the "scale factor" g :

$$g \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix} = \begin{pmatrix} W_x \\ W_y \\ W_z \end{pmatrix}, \quad (3.63)$$

with $x' = dx/ds$, etc. The curvature vector of the plumb line lies in the principal normal through P and thus in the horizontal plane. It reads as

$$\begin{pmatrix} x'' \\ y'' \\ z'' \end{pmatrix} = \kappa \begin{pmatrix} \cos A \\ \sin A \\ 0 \end{pmatrix}, \quad (3.64)$$

where κ is the total curvature, and A is the azimuth of the principal normal. Differentiating (3.63) with respect to s , and considering that at P : $x' = y' = 0$, $z' = -1$, the substitution into (3.64) yields

$$\kappa = -\frac{W_{xz}}{g \cos A} = -\frac{W_{yz}}{g \sin A} \quad (3.65)$$

and

$$A = \arctan \frac{W_{yz}}{W_{xz}}. \quad (3.66)$$

The *curvatures* of the projections of the plumb line on the x , z -plane ($A = 0^\circ$) and y , z -plane ($A = 90^\circ$) follow from (3.65):

$$\kappa_x = -\frac{W_{xz}}{g}, \quad \kappa_y = -\frac{W_{yz}}{g}, \quad (3.67)$$

where

$$\kappa = \sqrt{\kappa_x^2 + \kappa_y^2}.$$

From (3.56) to (3.67), we recognize that the curvatures of the level surfaces and the plumb lines depend on the second derivatives of the gravity potential. Consequently, they experience discontinuities at abrupt density changes, as discussed for the potential function, cf. [3.1.5].

The *gravity gradient tensor* (*Eötvös tensor*, also *Marussi tensor*) is comprised of the second derivatives of W as follows:

$$\text{grad } \mathbf{g} = \text{grad}(\text{grad } W) = \begin{pmatrix} W_{xx} & W_{xy} & W_{xz} \\ W_{yx} & W_{yy} & W_{yz} \\ W_{zx} & W_{zy} & W_{zz} \end{pmatrix}. \quad (3.68)$$

With (3.57), (3.58), (3.67), and $W_z = -g$, it can be transformed into the tensor

$$-\frac{1}{g} \operatorname{grad} \mathbf{g} = \begin{pmatrix} k_x & t_x & \kappa_x \\ t_x & k_y & \kappa_y \\ \kappa_x & \kappa_y & \frac{1}{g} \frac{\partial g}{\partial z} \end{pmatrix}, \quad (3.69)$$

which completely describes the geometry of the gravity field (Graffarend, 1986; Moritz and Hofmann-Wellenhof, 2005). As already stated in [3.1.5], (3.68) resp. (3.69) only contain five independent elements.

The Eötvös tensor (3.68) includes the *gravity gradient*

$$\operatorname{grad} g = - \begin{pmatrix} W_{xz} \\ W_{yz} \\ W_{zz} \end{pmatrix} = \begin{pmatrix} \partial g / \partial x \\ \partial g / \partial y \\ \partial g / \partial z \end{pmatrix}, \quad (3.70)$$

which describes the variation of gravity in the horizontal plane and in the vertical direction. The horizontal gradient is formed by the components $\partial g / \partial x$ and $\partial g / \partial y$, and points in the direction of maximum gravity increase in the horizontal plane. The vertical component (often called vertical gradient) $\partial g / \partial z$ describes the gravity change with height. If we combine the generalized Poisson equation (3.48) with the mean curvature (3.61), we get

$$\Delta W = W_{xx} + W_{yy} + W_{zz} = -2gJ - \frac{\partial g}{\partial z} = -4\pi G\rho + 2\omega^2$$

or

$$\frac{\partial g}{\partial z} = -2gJ + 4\pi G\rho - 2\omega^2. \quad (3.71)$$

This relation was found by Bruns (1878). It connects the vertical gradient with the mean curvature of the level surface and offers a possibility to determine this curvature from gravity measurements, cf. [5.4.5].

3.2.3 Natural coordinates

We introduce a system of non-linear “natural” coordinates Φ, Λ, W defined in the gravity field. Astronomical latitude Φ and astronomical longitude Λ describe the direction of the plumb line at the point P . They have been introduced already in [2.5] as orientation parameters of the local gravity field system with respect to the global geocentric system. The gravity potential W locates P in the system of level surfaces $W = \text{const.}$ (Fig. 2.12). Hence, P is determined by the non-orthogonal intersection of the coordinate surfaces $\Phi = \text{const.}$, $\Lambda = \text{const.}$, and $W = \text{const.}$ The coordinate lines (spatial curves) are called astronomic meridian curve ($\Lambda, W = \text{const.}$), astronomic parallel curve ($\Phi, W = \text{const.}$), and isozenithal line ($\Phi, \Lambda = \text{const.}$).

The natural coordinates can be determined by measurements. Astronomic positioning provides latitude and longitude, cf. [5.3.2]. Although W cannot be measured directly, potential differences can be derived from leveling and gravity measurements and then referred to a selected level surface, e.g., the geoid, cf. [5.5.4].

The relationship between the global X, Y, Z -system and the Φ, Λ, W -system is obtained from (3.45):

$$\mathbf{g} = \operatorname{grad} W = -g \begin{pmatrix} \cos \Phi \cos \Lambda \\ \cos \Phi \sin \Lambda \\ \sin \Phi \end{pmatrix}. \quad (3.72)$$

Solving for the natural coordinates yields the non-linear relations:

$$\left. \begin{aligned} \Phi &= \arctan \frac{-W_z}{\sqrt{W_x^2 + W_y^2}} \\ \Lambda &= \arctan \frac{W_y}{W_x} \\ W &= W(X, Y, Z) \end{aligned} \right\}. \quad (3.73)$$

Differential relations between the *local* Cartesian coordinates x, y, z (local astrometric system) and the *global* Φ, Λ, W -system are given by

$$d\Phi = \frac{\partial \Phi}{\partial x} dx + \frac{\partial \Phi}{\partial y} dy + \frac{\partial \Phi}{\partial z} dz, \text{ etc.,}$$

where dx, dy , and dz can be derived from local measurements, cf. [2.5].

The partial derivatives of Φ and Λ describe the change of the plumb line direction when moving in the gravity field. This corresponds to the curvature of the level surface (when moving in the horizontal plane) and of the plumb line (when moving vertically). We have the following relations:

$$\left. \begin{aligned} \frac{\partial \Phi}{\partial x} &= k_x \frac{\partial \Phi}{\partial y} = \frac{\cos \Phi \partial \Lambda}{\partial x} = t_x \frac{\partial \Phi}{\partial z} = \kappa_x \\ \frac{\cos \Phi \partial \Lambda}{\partial y} &= k_y \frac{\cos \Phi \partial \Lambda}{\partial z} = \kappa_y \\ \frac{\partial W}{\partial x} &= 0, \frac{\partial W}{\partial y} = 0, \frac{\partial W}{\partial z} = -g, \end{aligned} \right\}, \quad (3.74)$$

where the curvature and torsion parameters are given by (3.57), (3.58), and (3.67). Introducing (3.74) into the differential relations leads to the transformation

$$\begin{pmatrix} d\Phi \\ \cos \Phi d\Lambda \\ dW \end{pmatrix} = \begin{pmatrix} k_x & t_x & \kappa_x \\ t_x & k_y & \kappa_y \\ 0 & 0 & -g \end{pmatrix} \begin{pmatrix} dx \\ dy \\ dz \end{pmatrix}, \quad (3.75)$$

which again contains the elements of the Eötvös tensor (3.69), see Grafarend (1975), Moritz and Hofmann-Wellenhof (1993).

As the orientation of the local systems changes from point to point, the differentials dx, dy, dz are imperfect ones (i.e., they are not the differential of a function of position only), with loop closures differing from zero:

$$\oint dx \neq 0, \oint dy \neq 0, \oint dz \neq 0. \quad (3.76)$$

Φ, Λ, W , on the other hand, possess perfect differentials with

$$\oint d\Phi = 0, \oint d\Lambda = 0, \oint dW = 0. \quad (3.77)$$

Equation (3.75) offers the possibility to transform local observable quantities (azimuths, horizontal directions and angles, zenith angles, distances, potential differences from leveling and gravity) to the global system of "natural" coordinates, where the astrometric latitude and longitude coordinates are also observables.

A theory of "intrinsic geodesy" based on the differential geometry of the gravity field has been developed by Marussi (1949, 1985), see also Hotine (1969). Using only observable quantities, reductions to conventional reference systems are completely avoided. On the other hand, in order to practically evaluate (3.75), a detailed knowledge of the curvature of the gravity field would be necessary. This would require a dense survey of the second derivatives of the gravity potential, as the curvature close to the Earth's surface is rather irregular. Present gravity models

already provide this information for the long- and medium-wave part of the gravity field, but a high-resolution would require costly and time consuming terrestrial techniques, cf. [5.2.8], [5.4.5]. Yet even with a better knowledge of the curvature of the gravity field, the transfer of coordinates would hardly be made in the system of natural coordinates, due to the complex structure of the gravity field, and the success of Cartesian coordinate systems based on space geodetic methods, cf. [2.4].

3.3 Spherical harmonic expansion of the gravitational potential

Because the density function $\rho = \rho(\mathbf{r}')$ of the Earth is not sufficiently known, the gravitational potential $V = V(\mathbf{r})$ cannot be computed by Newton's law of gravitation using (3.10). However, a convergent series expansion of V is possible in the exterior space of the Earth as a special solution of Laplace's differential equation (3.29). It can be easily derived from an expansion of the reciprocal distance appearing in Newton's law [3.3.1], [3.3.2], e.g., Hobson (1965), Sigl (1985), Blakeley (1996). This solution corresponds to a spectral decomposition of the gravitational field [3.3.3]. The coefficients of the series expansion provide the amplitudes of the respective spectral parts [3.3.4]. Any observable functional of V can be evaluated for the determination of these coefficients, thus allowing a global analytical representation of the gravitational field, cf. [6.6.1].

3.3.1 Expansion of the reciprocal distance

Applying the law of cosines to the triangle $OP'P$ (Fig. 3.1), we obtain

$$\frac{1}{l} = (r^2 + r'^2 - 2rr' \cos \psi)^{-\frac{1}{2}} = \frac{1}{r} \left(1 + \left(\frac{r'}{r} \right)^2 - 2 \frac{r'}{r} \cos \psi \right)^{-\frac{1}{2}} \quad (3.78)$$

for the reciprocal distance $1/l$ appearing in (3.10), between the attracted point P and the attracting point P' . Here, ψ is the central angle between the directions from O to P and O to P' , respectively. If $1/l$ is expanded in a series converging for $r' < r$, and if the terms are arranged according to increasing powers of r'/r , then it follows

$$\frac{1}{l} = \frac{1}{r} \sum_{l=0}^{\infty} \left(\frac{r'}{r} \right)^l P_l(\cos \psi). \quad (3.79)$$

The $P_l(\cos \psi)$ terms represent polynomials of l^{th} degree in $\cos \psi$. They are known as *Legendre polynomials* (zonal harmonics), and they are computed for the argument $t = \cos \psi$ by means of

$$P_l(t) = \frac{1}{2^l l!} \frac{d^l}{dt^l} (t^2 - 1)^l. \quad (3.80a)$$

A rapid calculation is possible with the recurrence formula (Wenzel, 1985)

$$P_l(t) = \frac{2l-1}{l} t P_{l-1}(t) - \frac{l-1}{l} P_{l-2}(t), \quad l \geq 2, \quad (3.80b)$$

with $P_0 = 1$, $P_1 = t$.

We now introduce the unit sphere σ around the origin of the coordinates O (Fig. 3.10). The projections of OP and OP' on σ , together with the north pole projection N , form a spherical triangle. It contains the spherical coordinates ϑ, λ

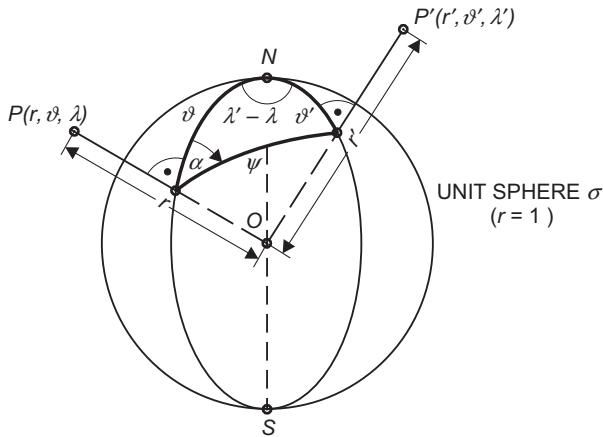


Fig. 3.10: Spherical polar triangle on the unit sphere, spherical coordinates.

and ϑ' , λ' , and the central angle ψ appears as a spherical distance on σ , see also [2.3.3]. Spherical trigonometry provides the following relationship

$$\cos \psi = \cos \vartheta \cos \vartheta' + \sin \vartheta \sin \vartheta' \cos(\lambda' - \lambda).$$

The corresponding decomposition of $P_l(\cos \psi)$ leads to

$$\begin{aligned} P_l(\cos \psi) &= P_l(\cos \vartheta)P_l(\cos \vartheta') \\ &+ 2 \sum_{m=1}^l \frac{(l-m)!}{(l+m)!} (P_{lm}(\cos \vartheta) \cos m\lambda P_{lm}(\cos \vartheta') \cos m\lambda' \\ &+ P_{lm}(\cos \vartheta) \sin m\lambda P_{lm}(\cos \vartheta') \sin m\lambda'). \end{aligned} \quad (3.81)$$

Again, the $P_l(t)$ are the Legendre polynomials with the argument $t = \cos \vartheta$ or $t = \cos \vartheta'$. The *associated* Legendre functions of the first kind, $P_{lm}(t)$ (degree l and order m), are obtained by differentiating $P_l(t)$ m times with respect to t :

$$P_{lm}(t) = (1 - t^2)^{\frac{m}{2}} \frac{d^m}{dt^m} P_l(t). \quad (3.82)$$

Up to degree 3, the Legendre polynomials and the associated Legendre functions are given as follows:

$$P_0 = 1, P_1 = \cos \vartheta, P_2 = \frac{3}{2} \cos^2 \vartheta - \frac{1}{2}, P_3 = \frac{5}{2} \cos^3 \vartheta - \frac{3}{2} \cos \vartheta \quad (3.83a)$$

and

$$\left. \begin{aligned} P_{1,1} &= \sin \vartheta, P_{2,1} = 3 \sin \vartheta \cos \vartheta, P_{2,2} = 3 \sin^2 \vartheta \\ P_{3,1} &= \sin \vartheta \left(\frac{15}{2} \cos^2 \vartheta - \frac{3}{2} \right), P_{3,2} = 15 \sin^2 \vartheta \cos \vartheta, P_{3,3} = 15 \sin^3 \vartheta \end{aligned} \right\}. \quad (3.83b)$$

A series development for the calculation of $P_{lm}(t)$ is given in Hofmann-Wellenhof and Moritz (2005, p. 17). By substituting (3.81) into (3.79), the expansion of $1/l!$ into spherical harmonics is completed.

The functions

$$\left. \begin{aligned} Y_{lm}^c(\vartheta, \lambda) &= P_{lm}(\cos \vartheta) \cos m\lambda \\ Y_{lm}^s(\vartheta, \lambda) &= P_{lm}(\cos \vartheta) \sin m\lambda \end{aligned} \right\} \quad (3.84)$$

contained in (3.81), are called *Laplace's surface spherical harmonics*. They characterize the behavior of the developed function (here $1/l$) on the unit sphere, cf. [3.3.3]. The *orthogonality* relations are valid for these functions, i.e., the integral over the unit sphere of the product of any two different functions is zero:

$$\iint_{\sigma} Y_{lm}^i Y_{nq}^k d\sigma = 0 \quad (3.85)$$

for $n \neq l$, $q \neq m$, or $k \neq i$. For the product of two equal functions Y_{lm}^c or Y_{lm}^s , we have

$$\iint_{\sigma} Y_{lm}^2 d\sigma = \begin{cases} \frac{4\pi}{2l+1} & \text{for } m=0 \\ \frac{2\pi(l+m)!}{(2l+1)(l-m)!} & \text{for } m \neq 0, \end{cases} \quad (3.86)$$

see Hofmann-Wellenhof and Moritz (2005, p. 21).

3.3.2 Expansion of the gravitational potential

We substitute the spherical harmonic expansion of $1/l$, (3.79) and (3.81), into the volume integral (3.10):

$$V = \frac{G}{r} \sum_{l=0}^{\infty} \sum_{m=0}^l k \frac{(l-m)!}{(l+m)!} \times \frac{1}{r^l} \left(\begin{aligned} & P_{lm}(\cos \vartheta) \cos m\lambda \iint_{\text{Earth}} r'^l P_{lm}(\cos \vartheta') \cos m\lambda' dm \\ & + P_{lm}(\cos \vartheta) \sin m\lambda \iint_{\text{Earth}} r'^l P_{lm}(\cos \vartheta') \sin m\lambda' dm \end{aligned} \right), \quad (3.87)$$

$$k = \begin{cases} 1 & \text{for } m=0 \\ 2 & \text{for } m \neq 0 \end{cases}.$$

In abbreviated form this development can be expressed as

$$V = \sum_{l=0}^{\infty} V_l = \sum_{l=0}^{\infty} \frac{Y_l(\vartheta, \lambda)}{r^{l+1}}, \quad (3.88)$$

where the V_l are called *solid spherical harmonics*, they are linear combinations of the surface spherical harmonics (3.84).

For $l=0$, the integration yields the potential of the Earth's mass M concentrated at the center of mass (3.16). We extract this term, introduce the semi-major axis a of the Earth ellipsoid as a constant "scale factor", and denote the mass integrals by C_{lm} , S_{lm} (spherical harmonic coefficients). The gravitational potential expanded in spherical harmonics can then be written as

$$V = \frac{GM}{r} \left(1 + \sum_{l=1}^{\infty} \sum_{m=0}^l \left(\frac{a}{r} \right)^l (C_{lm} \cos m\lambda + S_{lm} \sin m\lambda) P_{lm}(\cos \vartheta) \right). \quad (3.89)$$

The *harmonic coefficients* (also Stokes' coefficients) are given by

$$\left. \begin{aligned} C_{l0} = C_l &= \frac{1}{M} \iiint_{\text{Earth}} \left(\frac{r'}{a} \right)^l P_l(\cos \vartheta) dm \text{ for } m = 0 \text{ and} \\ \begin{cases} C_{lm} \\ S_{lm} \end{cases} &= \frac{2}{M} \frac{(l-m)!}{(l+m)!} \iiint_{\text{Earth}} \left(\frac{r'}{a} \right)^l P_{lm}(\cos \vartheta) \begin{cases} \cos m\lambda' \\ \sin m\lambda' \end{cases} dm \text{ for } m \neq 0 \end{aligned} \right\}. \quad (3.90)$$

The following denotations are also used, particularly in satellite geodesy:

$$J_l = -C_{l0}, J_{lm} = -C_{lm}, K_{lm} = -S_{lm}. \quad (3.91)$$

Calculations in the gravitational field become more convenient with the (fully) *normalized* spherical harmonic functions $\bar{P}_{lm}(\cos \vartheta)$. They are computed from the conventional harmonics, (3.80) and (3.82), according to

$$\bar{P}_{lm}(t) = \sqrt{k(2l+1)(l-m)!/(l+m)!} P_{lm}(t), \quad k = \begin{cases} 1 & \text{for } m = 0 \\ 2 & \text{for } m \neq 0 \end{cases} \quad (3.92)$$

with $t = \cos \vartheta$, etc. Recursive formulas are also available for the calculation of the normalized harmonics and its derivatives (Paul, 1978; Tscherning et al., 1983; Wenzel, 1985):

$$\begin{aligned} \bar{P}_{lm}(t) &= \left[\frac{(2l+1)(2l-1)}{(l+m)(l-m)} \right]^{\frac{1}{2}} t \bar{P}_{l-1,m}(t) - \\ &\quad \left[\frac{(2l+1)(l+m-1)(l-m-1)}{(2l-3)(l+m)(l-m)} \right]^{\frac{1}{2}} \bar{P}_{l-2,m}(t) \end{aligned} \quad (3.93a)$$

for $l > m + 1$

with

$$\begin{aligned} \bar{P}_0 &= 1, \quad \bar{P}_1 = \sqrt{3} \cos \vartheta, \quad \bar{P}_2 = \frac{1}{2} \sqrt{5} (3 \cos^2 \vartheta - 1), \\ \bar{P}_{1,1} &= \sqrt{3} \sin \vartheta, \quad \bar{P}_{2,1} = \sqrt{15} \sin \vartheta \cos \vartheta, \quad \bar{P}_{2,2} = \frac{1}{2} \sqrt{15} \sin^2 \vartheta \end{aligned} \quad (3.93b)$$

and the control formula

$$\sum_{m=0}^l \bar{P}_{lm}(t)^2 = 2l + 1. \quad (3.93c)$$

In addition to the orthogonality relations (3.85), (3.86) for the surface harmonics, we now also have

$$\frac{1}{4\pi} \iint_{\sigma} \left(\bar{P}_{lm} \begin{cases} \cos m\lambda \\ \sin m\lambda \end{cases} \right)^2 d\sigma = 1 \quad (3.94)$$

over the unit sphere σ . According to (3.92), for an expansion of the gravitational potential analogous to (3.89), the harmonic coefficients are now given by

$$\begin{cases} \bar{C}_{lm} \\ \bar{S}_{lm} \end{cases} = \sqrt{\frac{(l+m)!}{k(2l+1)(l-m)!}} \begin{cases} C_{lm} \\ S_{lm} \end{cases}, \quad k = \begin{cases} 1 & \text{for } m = 0 \\ 2 & \text{for } m \neq 0 \end{cases} \quad (3.95)$$

Equation (3.89), or the corresponding equations employing fully normalized harmonics (3.92) and (3.95), represent spherical solutions of Laplace's differential equation (3.29). These solutions can also be derived straightforwardly by the method of

variable separation, after substituting the Cartesian coordinates with spherical coordinates (Hofmann-Wellenhof and Moritz, 2005, p. 9 ff.).

The expansion converges outside a sphere of radius $r = a$, which just encloses the Earth (*Brillouin* sphere). After the theorem of *Runge-Krarup*, an expansion of V into converging spherical harmonics can also be used in the interior of the Earth, down to a sphere completely inside the Earth and close to its surface (*Bjerhammar* sphere), Krarup (1969), Moritz (1980, p. 69). Such an expansion represents an analytical continuation of the outer gravitational field model into the Earth's interior, with arbitrarily good approximation to the outer field. Naturally, this extension does not satisfy the Poisson equation (3.31) which governs the actual gravitational field in the Earth's interior.

With present accuracies of the determination of the Earth's gravity field, the gravitation of the *atmosphere* cannot be neglected. As the density of the atmosphere primarily depends on height, corresponding models can be used to calculate the potential and the gravitation of the atmosphere as a function of height. These calculations are based on the relations derived for the potential inside an Earth constructed of homogeneous spherical shells, cf. [3.1.2]. With an atmospheric mass of about 5.32×10^{18} kg, we get a potential value of $55.6 \text{ m}^2 \text{s}^{-2}$ for $h = 0$, and $54.8 \text{ m}^2 \text{s}^{-2}$ for $h = 100$ km. This effect is taken into account by corresponding reductions, cf. [4.3].

The extension of the spherical harmonic expansion for V to the *gravity potential* W is performed easily by adding the centrifugal potential Z (3.38). If we express the distance p to the rotational axis by spherical coordinates (2.14), the centrifugal potential reads as

$$Z = \frac{\omega^2}{2} r^2 \sin^2 \vartheta \quad (3.96a)$$

or, after introducing the Legendre polynomial P_2 according to (3.83a), as

$$Z = \frac{\omega^2}{3} r^2 (1 - P_2(\cos \vartheta)). \quad (3.96b)$$

By adding (3.96) to (3.89) we get the expansion for the gravity potential.

3.3.3 Geometrical interpretation of the surface spherical harmonics

We now discuss the properties of the surface spherical harmonics (3.84), which describe the behavior of the gravitational potential on the unit sphere. The zero points of these functions divide the surface into regions with alternating signs, bounded by meridians and parallels.

For the order $m = 0$, we obtain the Legendre polynomials $P_l(\cos \vartheta)$. Because of their independence of the geographical longitude λ , they divide the surface into zones of positive and negative signs: *zonal harmonics*. These harmonics possess l real zeros in the interval $0 \leq \vartheta \leq \pi$. For even l , the sphere is divided symmetrically with respect to the equator $\vartheta = 90^\circ$, and the case for odd l results in an asymmetric division. The $P_{lm}(\cos \vartheta)$ for $m \neq 0$ have $(l - m)$ zeros in the interval $0 < \vartheta < \pi$. Because of the multiplication by $\cos m\lambda$ or $\sin m\lambda$, the surface harmonics are longitude dependent, furnishing $2m$ zeros in the interval $0 \leq \lambda \leq \pi$: *tesseral harmonics* (*tessera* means a square or rectangle). Finally, for $m = l$, the dependence on ϑ disappears, and the sphere is divided into sectors of alternating signs: *sectorial harmonics* (Fig. 3.11).

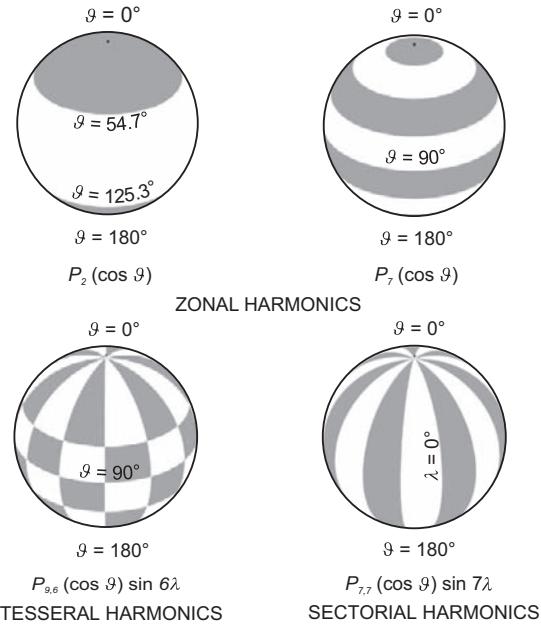


Fig. 3.11: Spherical harmonics on the unit sphere, with alternating positive (gray) and negative (white) sign.

The amplitudes of the individual terms given by the surface harmonics are determined by the harmonic coefficients. For example, the series has only zonal harmonics for an Earth rotationally symmetric with respect to the Z-axis; the coefficients with $m \neq 0$ must all vanish. For a mass distribution symmetric with respect to the equator, the zonal harmonic coefficients with odd l must be absent.

Summarizing, we state that the spherical harmonic expansion of the gravitational potential represents a *spectral decomposition* of the gravitational field. The field is separated into structures of wavelength $360^\circ/l$, corresponding to a spatial resolution of $180^\circ/l$. With increasing height, the field is smoothed by the factor $(a/r)^l$, see (3.89) and the examples in [6.7.3].

3.3.4 Physical interpretation of the spherical harmonic coefficients

The spherical harmonic expansion has transformed the single volume integral over the Earth's masses (3.10) into an infinite series. The harmonic coefficients now carry mass integrals for the individual contribution of the corresponding wavelength to the total potential. The lower degree harmonics have a simple physical interpretation.

As already stated above, the zero degree term ($l = 0$) represents the potential of a homogeneous or radially layered spherical Earth, see (3.16):

$$V_0 = \frac{GM}{r}. \quad (3.97)$$

The terms of degree one and two ($l = 1, 2$) can be calculated from (3.90) by introducing the harmonic functions P_{lm} (3.83) and subsequently transforming the spherical coordinates to Cartesian coordinates using (2.14). For $l = 1$, this yields

$$C_1 = \frac{1}{aM} \iiint_{\text{Earth}} Z' dm, \quad C_{1,1} = \frac{1}{aM} \iiint_{\text{Earth}} X' dm, \quad \text{and} \quad S_{1,1} = \frac{1}{aM} \iiint_{\text{Earth}} Y' dm. \quad (3.98)$$

As known from mechanics, the integrals divided by the mass M are the coordinates of the center of mass of the Earth. Since we have placed the origin of the coordinate system at the center of mass, we have

$$C_1 = C_{1,1} = S_{1,1} = 0. \quad (3.99)$$

For $l = 2$, we obtain

$$\begin{aligned} C_2 &= \frac{1}{a^2 M} \iiint_{\text{Earth}} \left(Z^2 - \frac{X^2 + Y^2}{2} \right) dm, \\ C_{2,1} &= \frac{1}{a^2 M} \iiint_{\text{Earth}} XZ dm, \\ S_{2,1} &= \frac{1}{a^2 M} \iiint_{\text{Earth}} YZ dm, \\ C_{2,2} &= \frac{1}{4a^2 M} \iiint_{\text{Earth}} (X^2 - Y^2) dm, \\ S_{2,2} &= \frac{1}{2a^2 M} \iiint_{\text{Earth}} XY dm. \end{aligned} \quad (3.100)$$

These expressions are functions of the moments of inertia

$$\begin{aligned} A &= \iiint (Y^2 + Z^2) dm, \quad B = \iiint (X^2 + Z^2) dm, \\ C &= \iiint (X^2 + Y^2) dm \end{aligned} \quad (3.101a)$$

and of the products of inertia

$$D = \iiint YZ dm, \quad E = \iiint XZ dm, \quad F = \iiint XY dm \quad (3.101b)$$

with respect to the axes of the global X, Y, Z -system. If we neglect polar motion, the Z -axis coincides with one principal axis of inertia (maximum moment of inertia). Consequently, we have

$$D = E = 0.$$

F , on the other hand, would only become zero if the X -axis coincided with one of the equatorial principal axes of inertia. Due to the conventional definition of the X -axis (Greenwich meridian), F therefore does not vanish.

Using the above expressions for A, B, C , and F , the harmonic coefficients of second degree may also be formulated as follows:

$$\begin{aligned} C_2 &= \frac{1}{a^2 M} \left(\frac{A + B}{2} - C \right), \quad C_{2,1} = S_{2,1} = 0, \\ C_{2,2} &= \frac{B - A}{4a^2 M}, \quad S_{2,2} = \frac{F}{2a^2 M}. \end{aligned} \quad (3.102)$$

$J_2 = -C_2$ is also known as *dynamical form factor*. It characterizes the polar flattening of the Earth's body by the difference between the mean equatorial moment of inertia (with $A \approx B$) and the polar moment of inertia. As this is the largest deviation from a spherical Earth model, the numerical value for C_2 is three orders of magnitude larger than the values of the successive coefficients. Slight contributions to the ellipsoidal form of the Earth also come from the even zonal harmonics of higher degree, mainly $l = 4$ and $l = 6$. The coefficients $C_{2,2}$ and $S_{2,2}$ describe the asymmetry of the equatorial mass distribution in relation to the rotational axis (ellipticity or flattening of the equator) and the torsion of the corresponding principal axes of inertia with respect to the conventional X - and Y -directions. The values obtained for these coefficients have been used for the computation of three-axial ellipsoids, cf. [4.2.1]. If the odd zonal harmonic-coefficients differ from zero, the corresponding terms in the expansion of V represent an asymmetric mass distribution with respect to the equatorial plane, cf. [3.3.3]. The main contribution comes from C_3 , and may be geometrically interpreted as a difference in the flattening for the northern and the southern hemisphere (a "pear-shaped" Earth's figure). Numerical values for the coefficients are given in [6.6.2], and actual values for the derived physical quantities of the Earth will be found in [8.1].

By introducing the coefficients $C_{1,0}$, $C_{1,1'}$, $S_{1,1'}$, and $C_{2,1'}$, $S_{2,1}$ as unknowns into the adjustment of satellite orbit observations, (small) deviations of the Earth's center of mass (geocenter variations) and the polar axis of inertia from the geocentric coordinate system (polar motion) can be detected. This is of importance for the investigation of temporal variations of the Earth's body.

3.4 The geoid

The geoid is of fundamental importance for geodesy, oceanography, and physics of the solid Earth. Due to the present-day demands on accuracy and resolution, the classical definition of the geoid must be reconsidered [3.4.1]. In geodesy and oceanography, the geoid serves as a height reference surface for describing continental and sea surface topography [3.4.2], [3.4.3]. Solid Earth physics exploits the geoid as a gravity field representation revealing the distribution of deeper located masses, cf. [8.2.4].

3.4.1 Definition

The geoid has already been introduced in [1.2] as a refined model of the figure of the Earth. Defined in 1828 by Gauss as the "equipotential surface of the Earth's gravity field coinciding with the mean sea level of the oceans", the name "geoid" was only given in 1873 by Listing.

This physical *definition* considers the waters of the oceans as freely-moving homogeneous matter, subject only to the force of gravity and free from variations with time (as ocean tides and time-variable ocean currents). Upon attaining a state of equilibrium, the surface of such idealized oceans would assume a level surface of the gravity field. This ocean surface may be regarded as being extended under the continents, e.g., by a system of conducting tubes, and will then represent a global realization of the geoid.

With the gravity potential value W_0 , the *equation* of the geoid reads as

$$W = W(\mathbf{r}) = W_0. \quad (3.103)$$

It follows from the properties of the gravity potential W , that the geoid is a closed and continuous surface, cf. [3.1.3]. As it extends partially inside the solid Earth (under the continents), its curvature will display discontinuities at abrupt density changes. Nevertheless, although not being an analytical surface in a global sense, it may be sufficiently well approximated by a spherical harmonic development, cf. [3.3.2]. With respect to a best-fitting reference ellipsoid, cf. [4.3], the geoid r.m.s. deviation amounts to ± 30 m; maximum deviations (geoid heights, also geoid undulations) reach about ± 100 m. The large-scale structures (resolution of about 500 km) of the geoid (geoid heights above a geocentric reference ellipsoid) are shown in Fig. 3.12, for more detailed information see [6.6.3].

The problem of downward continuation of the gravity field into the Earth's masses presupposes knowledge about the density distribution of the atmospheric and topographic masses. Geoid calculations consequently depend on the corresponding assumptions (Strykowski, 1998), cf. [6.5.3].

As is well known from oceanography, *mean sea level* is *not* an equilibrium surface in the Earth's gravity field, due to ocean currents and other quasi-stationary effects. In addition, sea level experiences a variety of *temporal variations*, which cover a wide spectrum. They can be only partially reduced by averaging over time or by modeling. Hence, mean sea level still varies over longer time spans, and a geoid definition has to refer to a certain epoch of mean sea level, cf. [3.4.2], [8.3.3], Bosch (2001b).

The *geoid* as gravity field quantity naturally also is affected by variations with time, and has to be regarded as a time-dependent quantity. We distinguish between the gravimetric tidal effects [3.5.2], and the gravity changes which result from displacements of terrestrial masses [3.5.3], [8.3.5]. The corresponding geoid changes remain at the order

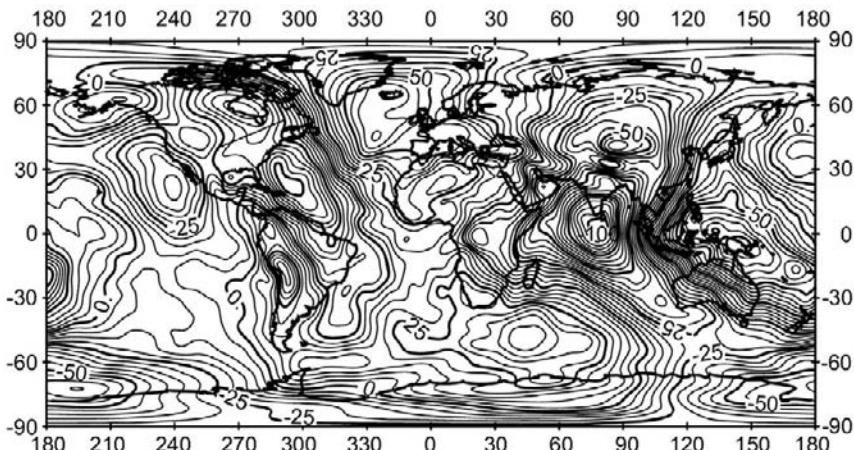


Fig. 3.12: Large scale geoid structures: EGM96 spherical harmonic expansion truncated at degree and order 36, contour line interval 5 m (after Lemoine et al., 1998).

of mm/year, but may reach the centimeter order of magnitude over several years. The definition of a “cm-geoid” has to take this time-dependence into account.

The *gravimetric tides* require special consideration. While the periodic part can be modeled to a high degree of accuracy, the treatment of the *permanent tidal deformation* enters into the definition of the geoid. This effect results from the fact that the mean value (time average) of the zonal tide of degree two is not zero, cf. (3.122). There are three different definitions possible. The *mean geoid* includes the direct effect of attraction *and* the indirect effect of deformation caused by extraterrestrial bodies (mean tidal system). It would coincide with an “undisturbed” mean ocean surface; hence it is of interest for oceanography. For the *non-tidal geoid*, the total tidal-effect would be eliminated (tide-free system). This would agree with the theoretical demand of geodesy to have no masses outside the boundary surface “geoid”, cf. [6.5.3], but would significantly change the shape of the Earth, and consequently the tide-free system is not acceptable from the geophysical point of view. As the response of the Earth to the permanent tidal part (the indirect effect) is not known, the *zero-tide-geoid* is preferred in geodesy (zero tidal system). Here, the attraction part is eliminated but the permanent deformation retained. This definition takes into account the fact that positioning also refers to a tidal-deformed Earth (IAG resolution, General Assembly Hamburg 1983; Rapp, 1983; Ekman, 1989).

In practice, geodetic products may refer to different tidal reductions. The zero tidal system is well established in gravimetry, while three-dimensional reference coordinates generally are given in a conventional tide-free system, and an interdisciplinary approach with oceanography would require the mean tidal system. Careful studies and reductions to a common standard are therefore required at combination solutions (Mäkinen and Ihde, 2009).

Consequently, a *refined geoid definition* is needed at the “cm” accuracy level (Rizos, 1982). By applying a minimum condition on the differences between (global) mean sea level and the geoid (mean sea surface topography, cf. [3.4.2]), the geoid could be defined as the equipotential surface which best fits mean sea level at a certain epoch (Rapp, 1995a), cf. [3.4.3].

Another choice would be to define the geoid as the level surface which optimally fits mean sea level at a selected set of tide gauges used for defining the vertical datum of national or continental height systems (Burša et al., 2002), cf. [7.2]. Such a definition would lead to only small corrections for the existing height systems but not result in a best fit over the open oceans. From the relativistic point of view, another approach would be to define the geoid as the surface where clocks have the same proper time (Müller et al., 2008). As discussed in [2.2.1], the definition of Terrestrial Time TT requires the geopotential value of the geoid, and a corresponding value is provided by the IERS Conventions. As a consequence, optical atomic clocks with a frequency stability of 10^{-17} – 10^{-18} would allow a potential transfer for geoid determination with dm- to cm-accuracy (Burša et al., 2007), cf. also [2.2.1].

3.4.2 Mean sea level

The ocean surface does not coincide with a level surface (e.g., the geoid) of the Earth’s gravity field; the deviations are called *sea surface topography* SST (also ocean surface topography or dynamic ocean topography DOT). *Instantaneous* SST is affected by

temporal variations of long-term, annual, seasonal, and short-term character, occurring at different scales. Averaging the ocean surface over time (at least over one year) and/or modeling ocean tides provides *Mean Sea Level* (MSL) for the corresponding time interval. But, even after reducing all time-dependent parts, a (smooth) quasi-stationary SST would remain (mean sea surface or mean dynamic ocean topography). It is caused by nearly constant oceanographic and meteorological effects, which generate ocean currents and ocean surface slopes. The r.m.s. variation of this mean dynamic ocean topography is ± 0.6 to ± 0.7 m, and the maximum deviation from the geoid is about ± 1 m or more (Bosch et al., 2010).

Short term variations of the sea surface (waves) are averaged out in the mean value over time (e.g., at tide gauge observations over one hour) or by the smoothing effect of the "footprints" in satellite altimetry, with spatial extension of several kilometers, cf. [5.2.7].

Ocean tides contribute about 70% to the variability of the sea surface, with maximum partial tides at daily and half-daily periods (Le Provost, 2001). The tidal effects can deviate considerably between the open ocean and shelf areas, adjacent seas, and coastal zones. This is due to unequal water depths and to the fact that the continents impede the free movement of water. On the open sea, the tidal amplitude is less than one meter (r.m.s. variation ± 0.3 m), while it can amount to several meters in coastal areas (Bay of Fundy, Nova Scotia: more than 15 m). *Oceanic tidal models* are based on Laplace's tidal equations, taking ocean boundaries, bathymetry and tidal friction into account. Early models were constrained to fit tide gauge observations (Schwiderski, 1980, 1983). The results of ocean-wide satellite *altimetry* (Chambers, 2009) allowed the development of *empirical tidal models* (Andersen and Knudsen, 1997; Bosch et al., 2009), and the assimilation of altimetric data into hydrodynamic models (Le Provost et al., 1998). The models solve for about 10 to 15 and more partial tides (annual, semi-annual, monthly, fortnightly, diurnal, semi-diurnal, quarter-diurnal). They are provided either in grid form (from $1^\circ \times 1^\circ$ to $0.25^\circ \times 0.25^\circ$ and $0.125^\circ \times 0.125^\circ$) or as a spherical harmonic expansion. Ocean tide models have also been derived by including tidal parameters into global gravity modeling (Lyard et al., 2006). The accuracy of the oceanic tidal models amounts to ± 1 to 2 cm on the open oceans but is less at shelf areas and close to the coast (Shum et al., 1997).

Sea level fluctuations of annual, semi-annual, and seasonal character are of *meteorological* origin (atmospheric pressure, winds, heat exchange between water masses, atmosphere and land), and of *oceanographic* nature (ocean currents, differences in water density as a function of temperature, salinity and pressure), and are also due to a variable *water budget* (changing water influx, e.g. as a result of polar ice melting, strong precipitation, e.g. through monsoon rains, etc.). The amplitude of these variations is on the order of 0.1 to 1 m, and scales are of a few 100 to 1000 km, e.g. at meandering ocean streams and eddies (Nerem, 1995; Bosch, 2004). We especially mention the annual oscillation (0.1 to 0.2 m) between the water masses of the northern and the southern hemisphere, which is due to different solar heating, and the interannual El Niño phenomenon, cf. [8.3.3]. An interaction between the ocean tides and the ocean circulation has also been found, which is induced by internal tides generated at topographic features as islands or ocean trenches (Garrett, 2003). In addition, a global *secular rise* of about 1 to 2 mm/a has been observed over the last 100 years (e.g., Douglas, 1997). This trend is expected to increase, reaching eventually 0.6 m (or even more?) over the 21st century, due to climate changes producing a thermal expansion of the water masses, a melting of the polar ice caps and the glaciers, changing continental hydrology, and isostatic movements (Church et al., 2008). The current rate of a *global* sea level rise as derived from satellite altimetry is between 3 and 4 mm/year, but this trend is superimposed by strong regional variations of

different sign, reaching the cm-order of magnitude (Bosch et al., 2010, Cazenave and Llovel, 2010), cf. also [8.3.3].).

Mean sea level can be derived from tide gauge records, satellite altimetry, and oceanographic methods.

Tide gauges (mareographs) continuously record the height of the water level with respect to a height reference surface close to the geoid, cf. [3.4.3]. Averaging the results over long time intervals (month, year) eliminates most variations with time. In order to fully remove the tidal period of a complete lunar cycle (nutation), the record should extend over 18.6 years, cf. [2.3.2]. The precision of the mean monthly and annual values is generally better than ± 1 cm. These results may be systematically disturbed if the tide gauge location is not directly linked to the open ocean and data is thereby affected by local sea level anomalies (swell in shallow waters, estuary effects at river mouths). In addition, local or regional vertical crustal movements (land sinking due to water or oil pumping, sedimentary subsidence, postglacial uplift, etc.) may act at the tide gauge location and systematically affect (bias) the sea level registration. These movements may reach a few mm/year (Mitchum, 1994). They are now generally observed by means of geodetic space techniques, especially continuous GPS observations (e.g., Becker et al., 2002), cf. [8.3.3].

Tide gauge data are available for almost 2000 stations worldwide, but only a few stations cover a time span of a few centuries (at Amsterdam registrations go back to 1700). The Global Sea Level Observing System (GLOSS) of the International Oceanographic Commission (IOC) defines a worldwide Core Network of approximately 300 stations, which is densified by regional and national networks (Woodworth and Player, 2003). In the open oceans, pressure tide gauges contribute in monitoring sea surface variability by exploiting the hydrostatic equation (8.5), but lack connection to continental height systems, e.g., Tolkatchev (1996). Tide gauges along the continental coasts generally have been connected to the local geodetic height control system, thus permitting to determine the deviation of MSL from a zero height reference close to the geoid. Sea level slopes up to several 0.1 m/1000 km and more have been detected by this method, cf. [3.4.3].

Satellite altimetry directly delivers sea surface heights with respect to an ellipsoidal reference surface, by regular surveys of the oceans, cf. [5.2.7]. With the exception of the polar regions, satellite altimeters cover the marine areas with repeated tracks (e.g., with a 10 days repetition rate at TOPEX/Poseidon) and permit derivation of mean sea surface heights to an accuracy of 1 to 2 cm. Preprocessed sea surface heights for the individual missions are provided by the responsible space agencies like NASA and ESA. Refined solutions are derived over a certain time period (e.g., one month or one year) and given in grids of a few minutes of arc; they differ with respect to the used data sets, the evaluated time span, and the evaluation method (Tapley and Kim, 2001). Sea surface topography is obtained by referring these results to a geoid model. If the altimetric solutions for different epochs are compared, sea surface variations with time can be determined which are due to redistribution of oceanic water masses (e.g., Minster et al., 1995), see above and [8.3.3].

Oceanographic methods derive sea surface topography from measurements at sea (Rummel and Ilk, 1995). *Steric leveling* assumes that equipotential and isobaric surfaces coincide at a certain depth (e.g., 2000 m): “level of no motion”. Using water density

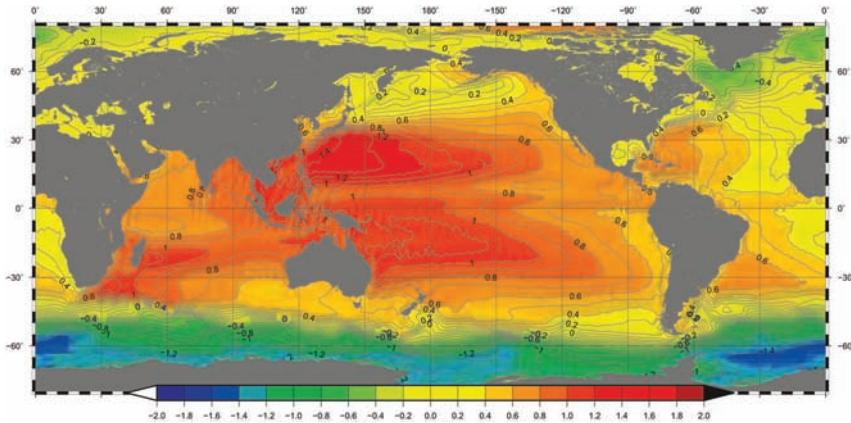


Fig. 3.13: Mean sea surface topography (meter above the geoid) for the period 1993–2008, resolution about 500 km, after Bosch et al. (2010).

values derived from salinity, temperature, and pressure data along vertical profiles, the integration of the hydrostatic equation yields the gravity potential difference (or the dynamic height, also geopotential height, cf. [3.4.3]) between two pressure levels, the ocean surface and the reference “level of no motion”. This method is applicable in the deep oceans and was used to compute mean monthly and annual dynamic heights. *Geostrophic leveling* (dynamic leveling) is based on the hydrodynamic equations and uses observed ocean current velocities. It can also be applied in shelf areas (Sturges, 1974).

Sea surface topography models have been developed by oceanographic and altimetric methods. *Oceanic* models correspond to a spherical harmonic expansion up to degree 36 (or a minimum wavelength of 10°) with an accuracy of a few cm to 0.1 m (Levitus et al., 1994). *Satellite altimetry* solutions are based on subtracting geoid heights from altimetric sea surface heights. This can be done straightforward, comparing the sea surface height data with a global geoid model, or by inclusion of the sea surface topography into a common adjustment, together with gravity field and satellite orbit parameters (e.g., Lemoine et al., 1998; Tapley et al., 2003; Savcenko and Bosch, 2008). In the latter case, the separation of the geoid and the ocean topography poses a special problem, and spherical harmonic developments of the sea surface topography remain significantly below the spatial resolution of (satellite-only) gravity field developments (1° to 2° resolution and cm-accuracy). Fig. 3.13 shows the quasi-stationary sea surface topography as derived for a limited time span, which clearly reveals the main ocean currents, and an equatorial bulge of roughly a half meter with respect to mid-latitudes (Bosch et al., 2010).

3.4.3 The geoid as height reference surface

The geoid is used in geodesy, cartography and geomatics, as well as in geophysics and especially in oceanography as a reference surface for heights and depths (continental and ocean bottom topography, as well as sea surface topography). A point P can be

attributed to a specified level surface by its gravity potential W (Fig. 3.14). With respect to the geoid potential W_0 , the “height” of P is given by the negative potential difference to the geoid, which is called the *geopotential number* C . We get from (3.52)

$$C = W_0 - W_P = - \int_{P_0}^P dW = \int_{P_0}^P g dn. \quad (3.104)$$

The integral is independent of the path. Hence, P_0 is an arbitrary point on the geoid. C can be determined from geometric leveling and gravity measurements along any path between P_0 and P , cf. [5.5.4].

The geopotential number is an ideal measure for describing the behavior of masses (e.g., water masses) in the gravity field, it satisfies the fundamental hydrostatic equation, see [8.1]. It could be used as a “height” in several applications, as in hydraulic engineering, oceanography and meteorology. A more general use is limited by the potential unit $\text{m}^2 \text{s}^{-2}$, which is in contradiction to the obvious demand for a metric height system that employs the “meter” unit.

In order to achieve a certain agreement with the numerical value of the height in meters, the geopotential unit $10 \text{ m}^2 \text{s}^{-2}$, or kGal m , is also used for the geopotential number. With $g \approx 9.8 \text{ m s}^{-2}$, the values of C are about 2% smaller than the corresponding height values.

The *dynamic height* H^{dyn} is obtained by dividing the geopotential number through a constant gravity value. Usually the normal gravity γ_0^{45} calculated for the surface of the level ellipsoid at 45° latitude is used: $\gamma_0^{45} = 9.806\,199 \text{ m s}^{-2}$, cf. [4.3]:

$$H^{\text{dyn}} = \frac{C}{\gamma_0^{45}}. \quad (3.105)$$

The surfaces $H^{\text{dyn}} = \text{const.}$ remain equilibrium surfaces. Hence, points located on the same level surface have the same dynamic height. Unfortunately, a geometric interpretation of the dynamic heights is not possible, and larger corrections are necessary in order to convert leveling results into dynamic height differences, cf. [6.4.1]. Because of this, dynamic heights have not been widely used in geodesy but are used in oceanography,

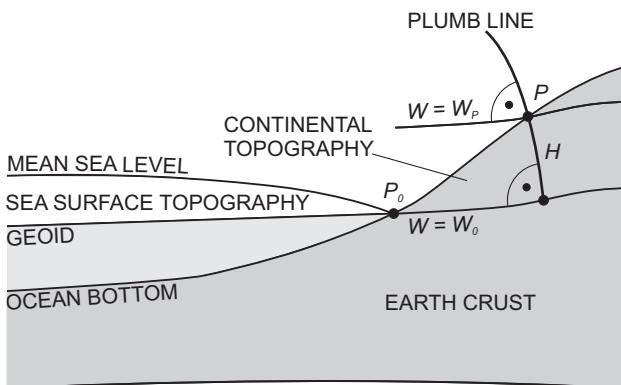


Fig. 3.14: Geoid, mean sea level, continental and sea surface topography.

under the assumption of a hydrostatic equilibrium of the water masses, and also in meteorology, with a standard gravity value at sea level $\gamma_0 = 9.806\,65 \text{ m s}^{-2}$, cf. [3.4.2].

National or continental height systems, and terrain-data based on them (topographic maps, digital terrain models), use either orthometric or normal heights.

The *orthometric height* H is defined as the linear distance between the surface point and the geoid, reckoned along the curved plumb line (Fig. 3.14). This definition corresponds to the common understanding of “heights above sea level”. Expanding the right-hand side of (3.104) in H and integrating along the plumb line from P_0 ($H = 0$) to $P(H)$ we obtain

$$H = \frac{C}{\bar{g}}, \bar{g} = \frac{1}{H} \int_0^H g dH. \quad (3.106)$$

\bar{g} is the mean gravity along the plumb line, with the consequence that gravity values inside the Earth are required for its calculation. This is performed by introducing a model of the density distribution of the topographic masses, see [6.4.1] for corresponding estimates of \bar{g} . As the density distribution is known only imperfectly, the accuracy of computed orthometric heights depends on the accuracy of the density model. In addition, points of equal orthometric height deviate slightly from a level surface, which is due to the non-parallelism of the level surfaces, cf. [3.2.1]. These drawbacks are compensated by the fact that orthometric heights represent the geometry of the topographic masses. In addition, the results of geometric leveling, as the most precise height determination method on land, only need small corrections for the transformation into orthometric height differences, cf. [6.4.1].

In order to avoid any hypothesis on the distribution of the topographic masses, *normal heights* H^N have been introduced and are used in a number of countries. The mean gravity \bar{g} in (3.106) is now replaced by the mean normal gravity $\bar{\gamma}$ along the normal plumb line, which is only slightly curved, cf. [4.2.3]:

$$H^N = \frac{C}{\bar{\gamma}}, \bar{\gamma} = \frac{1}{H^N} \int_0^{H^N} \gamma dH^N. \quad (3.107)$$

$\bar{\gamma}$ can be calculated in the normal gravity field of an ellipsoidal Earth model, cf. [4.2.2]. The reference surface for the normal heights is the *quasigeoid*. It is obtained pointwise by drawing the normal heights from the Earth's surface to the interior. The quasigeoid thus constructed is close to the geoid but not a level surface. It deviates from the geoid on the mm-to-cm order at low elevations and may reach 1 m deviation in the high mountains. On the oceans, geoid and quasigeoid practically coincide, cf. [6.1.1].

A *global vertical reference surface* “geoid” could be based on the determination of a geoid potential value W_0 derived from sea surface topography SST, cf. [3.4.2]. According to Bruns' formula (6.97b), SST is proportional to the difference between the gravity potential values on the geoid W_0 and on the ocean surface W_p , i. e., the geopotential number (3.104): $SST = (W_0 - W_p)/\gamma_p$, with normal gravity γ . A minimum condition applied on SST then serves for estimating W_0 . The “vertical coordinates” in this system are given by the potential values W (calculated in the zero-tidal system, cf. [3.4.1]) or the geopotential numbers. As the result would be derived from data collected over a limited (although as long as possible!) time interval, it should refer to a defined epoch. Using the results of dedicated satellite gravity field missions, cf. [5.2.8], and recent (and future) satellite altimetry, cf. [5.2.7], such a global vertical reference surface could be realized with cm-accuracy.

The realization of the vertical reference system on the *continents* requires special consideration. Presently, the zero height surface (vertical datum) of national height systems is defined by the mean sea level derived from tide gauge records over a certain time interval (the International Hydrographic Organization defines MSL as the average height of the sea surface over a 18.6-year period), and realized through the zero-points of tide gauges. By transferring potential differences (or height differences in the national height system) from the zero-point to the benchmarks of the vertical control network, the vertical datum finally is realized by the set of benchmark heights, cf. [7.2]. These local reference surfaces only approximate the geoid or the quasigeoid, due to the effect of sea surface topography and local sea level anomalies, with deviations up to 1 m and more, cf. [3.4.2].

As a consequence, a *global* vertical reference system is actually defined and realized only at the accuracy level of a few decimeters, through the W_0 -values of different SST evaluations (the IERS Conventions 2010 give the value $W_0 = 62\,636\,856.0 \pm 0.5\text{m}^2\text{s}^{-2}$, as a recent standard). On the continents, the present realization of a global vertical system is even worse. This accuracy is significantly less than that of the global *geometric* reference system, cf. [4.3], and does no longer satisfy the needs of geodesy and oceanography. Basic strategies for the definition and realization of a world height system follow the ideas explained above (Rummel and Teunissen, 1988; Rapp, 1995b). These strategies include the determination of the potential offsets of local vertical height systems from a global system (defined through the geoid potential), exploiting GNSS positioning at bench marks, and provide first results (Ihde and Sánchez, 2005; Sánchez, 2009).

The adjustment of a continental-wide leveling network connected to MSL of *one* tide gauge, provides potential differences or heights that refer to one common level surface. By comparing with the mean sea level obtained at different tide gauges, *sea level slopes* that partially agree with oceanic leveling results have been found. For example, MSL at the Pacific coast of the U.S.A. is about 1 m higher than at the Atlantic coast (Zilkoski et al., 1995), and the mean Baltic Sea level is estimated to be about 0.5 m above MSL of the Mediterranean Sea (Sacher et al., 1999). On the other hand, there are also larger discrepancies of a few 0.1 m between the results of geometric and oceanic leveling. These can be traced back to differently defined reference surfaces, to the particular behaviour of MSL along the coastlines, and to systematic errors in geometric leveling over long distances (Fischer, 1977). It should also be mentioned that older leveling networks have often been adjusted without any gravity reduction, or by substituting actual gravity with normal gravity, thus producing larger systematic errors, cf. [7.2]. A unification of the different vertical datum systems to a world-wide standard thus would also require a uniform treatment of the height measurements, in addition to the vertical shifts to a common global reference surface (see above).

3.5 Temporal gravity variations

Gravity changes with time may be divided into effects due to an eventual time dependent gravitational constant and variations of the Earth's rotation [3.5.1], tidal accelerations [3.5.2], and variations caused by terrestrial mass displacements [3.5.3]. These changes are of global, regional, or local character and occur either at well-known frequencies (tides) or at time scales ranging from secular to episodic (Lambeck, 1988; Mueller and Zerbini, 1989; Timmen, 2010).

3.5.1 Gravitational constant, Earth rotation

Based on cosmological considerations, Dirac (1938) postulated a secular decrease of the gravitational constant G , with relative changes of $\dot{G}/G = -10^{-10}$ to $-10^{-11}/a$ ($\dot{G} = dG/dt$). But even to this day, laboratory experiments and the analysis of long-term observations to artificial satellites and the moon have not supported the assumption $\dot{G} \neq 0$ (Gillies, 1987).

A powerful tool for detecting a secular variation of G is lunar laser ranging, as such a variation would change the Earth-moon distance. Recently, the analysis of 40 years of lunar laser ranging data yielded a relative change of $(-1 \pm 4) \times 10^{-13}/a$ for the gravitational constant, which is not significant (Hofmann et al., 2010).

The Earth's rotational vector $\boldsymbol{\omega}$ is subject to secular, periodic, and irregular variations, leading to changes of the centrifugal acceleration \mathbf{z} , cf. [2.3.4]. In a spherical approximation, the radial component of \mathbf{z} enters into gravity, cf. [3.1.4]. By multiplying (3.35b) with $\cos\bar{\varphi}$ ($\bar{\varphi}$ = geocentric latitude), we obtain

$$z_r = -\omega^2 r \cos^2 \bar{\varphi}. \quad (3.108)$$

Differentiation yields the effect of changes in latitude (polar motion) and angular velocity (length of day) on gravity:

$$\delta z_r = \omega^2 r \sin 2\bar{\varphi} d\bar{\varphi} - 2\omega r \cos^2 \bar{\varphi} d\omega. \quad (3.109)$$

Polar motion does not exceed a few $0.1''/a$, and rotation changes are at the order of a few ms. Hence, corresponding gravity variations on the Earth's surface ($r = 6371$ km) remain less than $0.1 \mu\text{m s}^{-2}$ and $0.01 \mu\text{m s}^{-2}$, respectively. They can be taken into account easily by corresponding models, cf. [5.3.3], [5.4.1].

3.5.2 Tidal acceleration, tidal potential

Tidal acceleration is caused by the difference between lunisolar gravitation (and to a far lesser extent planetary gravitation) and orbital accelerations due to the motion of the Earth around the barycenter of the respective two-body system (Earth-moon, Earth-sun, etc.). The periods of these orbital motions are about 28 days for the moon and 365 days for the sun, and the gravimetric tidal effect is at the order of $10^{-7} g$ (Melchior, 1983; Zürn and Wilhelm, 1984; Wenzel, 1997a).

For a *rigid Earth*, the tidal acceleration at a given point can be determined from Newton's law of gravitation and the ephemerides (coordinates) of the celestial bodies (moon, sun, planets). The computations are carried out separately for the individual two-body systems (Earth-moon, Earth-sun, etc.), and the results are subsequently added, with the celestial bodies regarded as point masses.

We consider the geocentric coordinate system to be moving in space with the Earth but not rotating with it (revolution without rotation). All points on the Earth experience the same orbital acceleration in the geocentric coordinate system (see Fig. 3.15 for the Earth-moon system). In order to obtain equilibrium, orbital acceleration and gravitation of the celestial bodies have to cancel in the Earth's center of mass. Tidal acceleration occurs at all other points of the Earth. The acceleration is defined as the difference between the gravitation \mathbf{b} , which depends on the position of the point, and the constant part \mathbf{b}_0 , referring to the Earth's center:

$$\mathbf{b}_t = \mathbf{b} - \mathbf{b}_0. \quad (3.110)$$

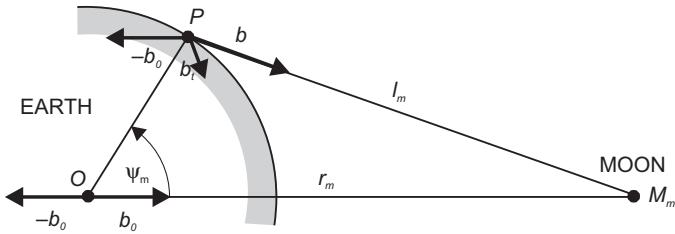


Fig. 3.15: Lunar gravitation, orbital acceleration, and tidal acceleration.

The tidal acceleration deforms the Earth's gravity field symmetrically with respect to three orthogonal axes with origin at the Earth's center. This tidal acceleration field experiences diurnal and semi-diurnal variations, which are due to the rotation of the Earth about its axis.

If we apply the law of gravitation to (3.110), we obtain for the moon (m)

$$\mathbf{b}_t = \frac{GM_m}{l_m^2} \frac{\mathbf{l}_m}{l_m} - \frac{GM_m}{r_m^2} \frac{\mathbf{r}_m}{r_m}. \quad (3.111)$$

Here, M_m is the mass of the moon, and l_m and r_m are the distances to the moon as reckoned from the calculation point P and the Earth's center of mass O , respectively. We have $\mathbf{b}_t = \mathbf{0}$ for $l_m = r_m$. Corresponding relations hold for the Earth-sun and Earth-planet systems.

We now make the transition from the tidal acceleration to the *tidal potential*:

$$\mathbf{b}_t = \text{grad } V_t = \text{grad}(V - V_0). \quad (3.112)$$

In the geocentric system, using spherical coordinates r_m, ψ_m (functions of time!), the law of gravitation yields the potential of a point mass according to (3.9):

$$V = \frac{GM_m}{l_m} \quad (3.113a)$$

with

$$l_m = (r^2 + r_m^2 - 2rr_m \cos \psi_m)^{\frac{1}{2}}. \quad (3.113b)$$

The potential of the homogeneous \mathbf{b}_0 -field is given by multiplying b_0 with $r \cos \psi_m$:

$$V_0 = \frac{GM_m}{r_m^2} r \cos \psi_m. \quad (3.114)$$

Inserting (3.113) and (3.114) into (3.112), and adding an integration constant, so that $V_t = 0$ for $r = 0$ and $l_m = r_m$, we get for the tidal potential

$$V_t = GM_m \left(\frac{1}{l_m} - \frac{1}{r_m} - \frac{r \cos \psi_m}{r_m^2} \right). \quad (3.115)$$

The tidal potential, and functionals thereof, can be calculated either from the ephemerides of the celestial bodies or from a spherical harmonic expansion. Tidal potential catalogues are based primarily on the latter method, as the series expansions converge rapidly close to the Earth's surface ($r = R$), with $r/r_m = 1/60$ for the moon and a corresponding relation of $1/23\,600$ for the sun. The results from calculations employing the ephemerides may serve as a control for the tidal potential catalogues.

We develop (3.113b) into a series according to (3.79). When inserting into (3.115), the terms of degree zero and one cancel and we obtain

$$V_t = \frac{GM_m}{r_m} \sum_{l=2}^{\infty} \left(\frac{r}{r_m}\right)^l P_l(\cos \psi_m), \quad (3.116)$$

where $P_l(\cos \psi_m)$ are the Legendre polynomials of degree l . The development converges rapidly due to the factor r/r_m , with the largest contribution ($\approx 98\%$) originating from degree two. Restricting ourselves now to $l=2$, and inserting P_2 (3.83) in the form

$$\cos^2 \psi_m = \frac{1}{2} (\cos 2\psi_m + 1),$$

we get the *main term* of the tidal potential series

$$V_t = \frac{3}{4} GM_m \frac{r^2}{r_m^3} \left(\cos 2\psi_m + \frac{1}{3} \right). \quad (3.117)$$

For $r=R$, and neglecting the slight variation of r_m , the expression before the parentheses is called *Doodson's tidal constant*. It is $2.628 \text{ m}^2 \text{ s}^{-2}$ for the moon and $1.208 \text{ m}^2 \text{ s}^{-2}$ for the sun. Hence, the solar tides amount to 46% of the lunar tides.

Differentiating (3.117) generates the *tidal acceleration*. The *radial component* (positive outward) is found to be

$$b_r = \frac{\partial V_t}{\partial r} = \frac{3}{2} GM_m \frac{r}{r_m^3} \left(\cos 2\psi_m + \frac{1}{3} \right). \quad (3.118)$$

The *tangential component* (positive in the direction toward the moon) is

$$b_{\psi_m} = -\frac{\partial V_t}{\partial \psi_m} = \frac{3}{2} GM_m \frac{r}{r_m^3} \sin 2\psi_m. \quad (3.119)$$

Equations (3.117) to (3.119) permit calculation of the tidal effects on the level surfaces, on gravity, and on the plumb line direction for a rigid Earth.

Taking the relation (3.52) between a potential change and the vertical shift of a level surface into account, (3.117) delivers the tidal-induced increase of a level surface. This amounts to 0.36 m for the moon and 0.16 m for the sun at $\psi=0^\circ$ and 180° , respectively. At $\psi=90^\circ$ and 270° , we have a decrease of 0.18 m and 0.08 m, respectively. For stationary systems, the level surfaces would experience a corresponding deformation, and freely moving masses of water would assume the form of one of these surfaces (equilibrium tide), Fig. 3.16.

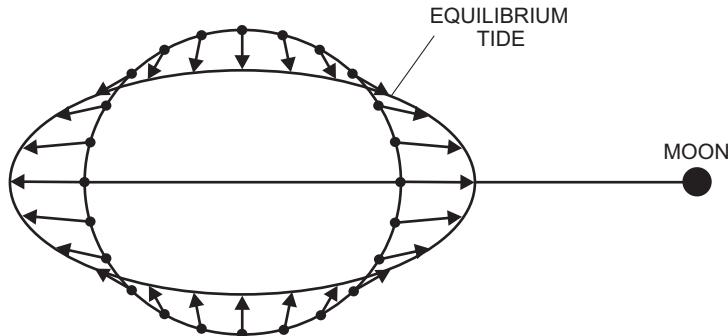


Fig. 3.16: Tidal acceleration and equilibrium tide.

According to (3.118), gravity changes (opposite sign!) would vary between $-1.1 \mu\text{m s}^{-2}$ (moon) and $-0.5 \mu\text{m s}^{-2}$ (sun) for $\psi = 0^\circ$ (zenithal position); and $+0.5 \mu\text{m s}^{-2}$ (moon) and $+0.3 \mu\text{m s}^{-2}$ (sun) for $\psi = 90^\circ$ and 135° . Changes in the direction of the *plumb line* are given by b_ψ/g , see (3.119). There is no tidal effect at $\psi = 0^\circ$ and 90° . Maximum values occur at $\psi = 45^\circ$ and 135° , with fluctuations of $\pm 0.017''$ (moon) and $\pm 0.008''$ (sun).

Equation (3.117) provides the dependence of the tidal potential on the zenith angle (and the distance) to the celestial body. The temporal variation of the tidal potential and acceleration is more easily recognized if we change to the Earth-fixed coordinate system $(\bar{\varphi}, \lambda)$ for the point of calculation and to the equatorial system of astronomy (δ, h) for the celestial body, cf. [2.3.1]. Following (2.21), we have for the moon the relation

$$\cos \psi_m = \sin \bar{\varphi} \sin \delta_m + \cos \bar{\varphi} \cos \delta_m \cosh_{h_m} \quad (3.120)$$

with the hour angle given by (2.22) and (2.23):

$$h_m = \text{LAST} - \alpha_m = \lambda + \text{GAST} - \alpha_m. \quad (3.121)$$

Substituting into (3.117) yields *Laplace's tidal equation* for the moon (a corresponding equation is valid for the sun):

$$V_t = \frac{3}{4} GM_m \frac{r^2}{r_m^3} \left[\left(\frac{1}{3} - \sin^2 \bar{\varphi} \right) (1 - 3 \sin^2 \delta_m) + \sin 2\bar{\varphi} \sin 2\delta_m \cos h_m + \cos^2 \bar{\varphi} \cos^2 \delta_m \cos 2h_m \right]. \quad (3.122)$$

The quantities r_m , δ_m and h_m vary with time, having different periods. The first term, which is independent of the Earth's rotation, exhibits long-periodic variations (14 days for the moon, half a year for the sun). It also contains a non-periodic part, which only depends on latitude, causing a permanent deformation of the level surfaces including the geoid, cf. [3.4.1]. Using (3.52), and taking the inclination of the ecliptic into account, the geoid is thus lowered by 0.19 m at the poles and raised by 0.10 m at the equator (Ekman, 1989). The second term oscillates with diurnal periods because of the daily rotation of the Earth as expressed by the hour angle h , and the third term introduces semi-diurnal periods. Long-periodic terms enter through the declination δ and the right ascension α .

As seen from (3.122), long-periodic and semi-diurnal tides are symmetric about the equator, while the diurnal tides are antisymmetric. The diurnal tide has its maximum at $\varphi = \pm 45^\circ$ and vanishes at the equator and the poles, while the semi-diurnal tide reaches its maximum at the equator and is zero at the poles. The long-periodic tides have a maximum at the poles.

Each of the three tidal constituents in (3.122) varies in a complicated way, since they contain products of different time varying functions. However, the ephemerides of the moon and the sun can be expressed as harmonic functions of five fundamental astronomic quantities, considering that these quantities essentially change uniformly with time (Melchior, 1983). Introducing these harmonic series into (3.122) yields a spectral analysis of the tidal potential, and with (3.118) and (3.119), we get a corresponding spectral analysis of the tidal acceleration. Thus, potential and acceleration are represented by the sum of time-dependent cosine functions having constant periods and amplitudes and phases that depend on latitude and height (partial tides). Tab. 3.1 gives the periods and amplitudes of the main gravimetric partial tides for $\varphi = 45^\circ$.

Tab. 3.1: Principal gravimetric partial tides for $\bar{\varphi} = 45^\circ$, $h = 0$

Symbol	Name	Period (solar days/hours)	Amplitude (nm s ⁻²)
Long-periodic waves			
M0	Const. <i>m</i> tide	∞	102.9
S0	Const. <i>s</i> tide	∞	47.7
Ssa	Declin. tide to S0	182.62 d	14.8
Mm	Ellipt. tide to M0	27.55 d	16.8
Mf	Declin. tide to M0	13.66 d	31.9
Diurnal waves			
O1	Main diurnal <i>m</i> tide	25.82 h	310.6
P1	Main diurnal <i>s</i> tide	24.07 h	144.6
Q1	Ellipt. tide to O1	26.87 h	59.5
K1	Main diurnal/ <i>s</i> decl. tide	23.93 h	436.9
Semi-diurnal waves			
M2	Main <i>m</i> tide	12.42 h	375.6
S2	Main <i>s</i> tide	12.00 h	174.8
N2	Ellipt. tide to M2	12.66 h	71.9
K2	Declin. tide to M2, S2	11.97 h	47.5
Ter-diurnal waves			
M3	Ter-diurn. <i>m</i> tide	8.28 h	5.2

A first expansion for the moon and the sun was carried out by Doodson (1921). The development by Cartwright and Tayler (1971) and Cartwright and Edden (1973) contains 505 partial tides (uncertainty less than 1 nm s⁻²) and was recommended by IAG for the computation of the tides of the rigid Earth (Rapp, 1983). Among the more recent tidal catalogues is the development by Hartmann and Wenzel (1995). It is based on a spherical harmonic development to degree 6 (moon) and degree 3 (sun) and includes the effects of Venus, Mars, and Jupiter (four orders of magnitude smaller than the tidal effects of moon and sun). It also takes the flattening of the Earth into account. This catalogue provides 12 935 partial tides, with an accuracy of 0.001 nm s⁻² for the gravimetric tidal effect (Wenzel, 1996).

As the Earth is not a *rigid* body, it reacts in a different way to the tidal force. The solid Earth behaves mainly as an *elastic* body: *Earth's body tides* (Earth tides). In the oceans, tidal oscillations depend on the ocean-bottom topography, with large differences occurring at the coastlines and at the shelf areas: *ocean tides* (Zahel, 1997; LeProvost, 2001), cf. [3.4.2]. While the measurement of gravimetric tidal effects will be discussed in [5.4.6], the theory of Earth tides and results of Earth-tide observations are given in [8.3.6].

3.5.3 Non-tidal temporal gravity variations

The terrestrial gravity field is affected by a number of variations with time due to mass redistributions in the atmosphere, the hydrosphere, the cryosphere, and the solid Earth's surface, crust, mantle and core (e.g., Ekman, 1989; Dickey, 2002). These processes take place at different time scales and are of global, regional, and local character. The magnitude

of these non-tidal gravity variations depends on the amount of mass shifts and is related to them by the law of gravitation. Generally, gravity variations produced by mass redistributions do not exceed the order of 10^{-9} to 10^{-8} g. Of special interest for geodesy are temporal changes of the geoid. They generally remain less than 1 mm/year, but may reach regionally one centimetre and more within a few years (e.g., Kuhn, 2002).

Long-term global effects include postglacial rebound, melting of the ice caps and glaciers, as well as sea level changes induced by global warming; slow motions of the Earth's core and mantle convection also contribute. Subsidence in sedimentary basins and tectonic uplift are examples of regional effects. Groundwater and soil moisture variations are primarily of seasonal character but may affect larger regions, while volcanic and Earthquake activities are short-term processes of more local extent. Human activities as large building projects, irrigation or the withdrawal of water, oil and gas may also cause gravity changes, but are of a more local character.

Observation and modeling of non-tidal temporal gravity variations started with advanced relative and absolute gravimetry, in the second half of the twentieth century. Repeated satellite orbit analyses early allowed the determination of global gravity field changes, e.g., expressed as a change of the Earth's oblateness. Dedicated gravity field satellite missions are now able to monitor large- and medium-scale variations, of seasonal and long-term character. Small-scale effects still can be detected only by repeated terrestrial gravity measurements (e.g., Torge, 1993; Wahr, 2009). The continuous registration of gravity allows to monitor a multitude of geodynamic phenomena, from the seconds to decades time scale. More details about the measurement and the evaluation of gravity variations with time will be found in the chapters on gravity measurements [5.2.8], [5.4.1], [5.4.6], and on the results obtained by repeated gravity field determination, especially through dedicated satellite missions [8.3.5].

4 The Geodetic Earth Model

A geodetic Earth model is used as a reference for the actual surface and external gravity field of the Earth. It should provide a good fit to the geoid and to the gravity field, and thus allow the linearization of non-linear geodetic problems. On the other hand, the mathematical formation of the model should be simple and possibly permit calculations by closed formulas. The model should serve as a standard for applications not only in geodesy, surveying, navigation, geoinformation and cartography, but also in astronomy and geophysics.

Based on these considerations, the level ellipsoid has been introduced as geodetic Earth model. It possesses a simple geometry, and coordinate systems that refer to it approximate the gravity field related “natural” coordinates sufficiently well [4.1]. The ellipsoid’s mass and rotation provide a “normal” gravity field exterior to the ellipsoid, which can be rigorously calculated if the ellipsoid surface is defined to be in equilibrium [4.2]. State of the art Earth models are recommended from time to time as a standard and are given the name Geodetic Reference System [4.3].

4.1 The rotational ellipsoid

The rotational ellipsoid was introduced as a geometrical figure of the Earth in the eighteenth century, cf. [1.3.2]. By fitting its dimension and orientation to the geoid, it approximates this level surface within about ± 100 m. The geometry of the ellipsoid can be described in a simple manner, together with ellipsoidal surface coordinates and curvature [4.1.1], [4.1.2]. The use of global and local three-dimensional ellipsoidal systems provides an approximation to the corresponding systems of the actual Earth and permits the separation between horizontal position and height [4.1.3].

Geometry and coordinate systems of the ellipsoid are well documented in geodetic literature, e.g., Grossmann (1976), Bomford (1980), Heitz (1988), Heck (2003a).

4.1.1 Parameters and coordinate systems

The rotational ellipsoid is generated by rotating the meridian ellipse about its minor axis. Size and shape of the ellipsoid are described by two geometric parameters, the *semi-major axis* a and the *semi-minor axis* b (Fig. 4.1). Generally, b is replaced by a smaller quantity, describing the (small) polar flattening of the ellipsoid, which is more suitable for series expansions. We especially have the (geometrical) *flattening*

$$f = \frac{a - b}{a}, \quad (4.1a)$$

the *first numerical eccentricity*

$$e = \sqrt{a^2 - b^2} / a, \quad (4.1b)$$

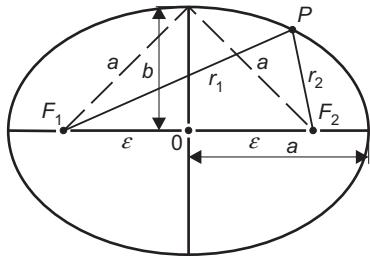


Fig. 4.1: Meridian ellipse.

and the *second numerical eccentricity*

$$e' = \frac{\sqrt{a^2 - b^2}}{b}. \quad (4.1c)$$

The following relations hold among those quantities:

$$\frac{b}{a} = 1 - f = \sqrt{1 - e^2} = \frac{1}{\sqrt{1 + e'^2}} = \frac{e}{e'}. \quad (4.2)$$

From the geometric definition of the ellipse as the curve having a constant value for the sum of the distances r_1 and r_2 to the focal points F (Fig. 4.1)

$$r_1 + r_2 = 2a,$$

we obtain the *linear eccentricity* as another quantity describing the flattening:

$$\varepsilon = \sqrt{a^2 - b^2}. \quad (4.3)$$

We now introduce a spatial Cartesian \bar{X} , \bar{Y} , \bar{Z} -coordinate system (Fig. 4.2). The origin of the system is situated at the center of the ellipsoid O . The \bar{Z} -axis coincides with the minor axis of the ellipsoid. The equation of the surface of the ellipsoid is then given by

$$\frac{\bar{X}^2}{a^2} + \frac{\bar{Y}^2}{b^2} + \frac{\bar{Z}^2}{b^2} - 1 = 0. \quad (4.4)$$

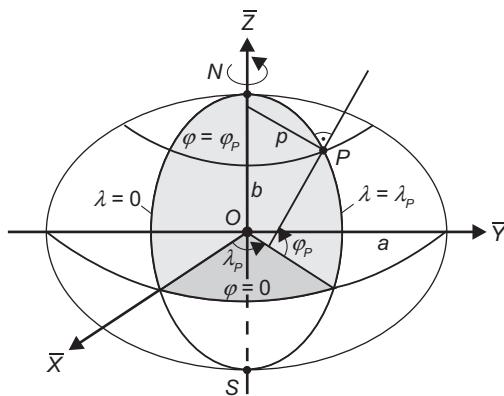


Fig. 4.2: Geodetic coordinates latitude and longitude.

The system of *geodetic surface coordinates* is defined by the ellipsoidal *latitude* φ and *longitude* λ (also *geodetic* latitude and longitude). φ is the angle measured in the meridian plane between the equatorial plane (\bar{X}, \bar{Y} -plane) of the ellipsoid and the surface normal at P . Longitude λ is the angle measured in the equatorial plane between the zero meridian (\bar{X} -axis) and the meridian plane of P . Here, φ is positive northwards and negative southwards, and λ is positive as reckoned towards the east. The ellipsoidal *meridian plane* is formed by the surface normal and the \bar{Z} -axis. φ and λ are defined to have angular values, but they may also be considered as curvilinear surface coordinates. The *coordinate lines* of this orthogonal system are the meridians ($\lambda = \text{const.}$) and the parallels, or circles of latitude, ($\varphi = \text{const.}$). With

$$\bar{X} = p \cos \lambda, \quad \bar{Y} = p \sin \lambda, \quad (4.5)$$

we introduce the radius of the circle of latitude

$$p = \sqrt{\bar{X}^2 + \bar{Y}^2} \quad (4.6)$$

as a new variable (Fig. 4.2). Substituting p into (4.4) and differentiating yields the slope of the ellipsoidal tangent at P (Fig. 4.3):

$$\frac{d\bar{Z}}{dp} = -\left(\frac{b}{a}\right)^2 \frac{p}{\bar{Z}} = -\cot \varphi. \quad (4.7)$$

By combining (4.4) and (4.7), and substituting p with (4.5), the parametric representation of the *meridian ellipse* follows:

$$\begin{aligned} \bar{X} &= \frac{a^2 \cos \varphi \cos \lambda}{(a^2 \cos^2 \varphi + b^2 \sin^2 \varphi)^{\frac{1}{2}}}, & \bar{Y} &= \frac{a^2 \cos \varphi \sin \lambda}{(a^2 \cos^2 \varphi + b^2 \sin^2 \varphi)^{\frac{1}{2}}}, \\ \bar{Z} &= \frac{b^2 \sin \varphi}{(a^2 \cos^2 \varphi + b^2 \sin^2 \varphi)^{\frac{1}{2}}}. \end{aligned} \quad (4.8)$$

Instead of φ , other latitude parameters are used for special applications. The *geocentric latitude* $\bar{\varphi}$ has already been introduced together with the longitude λ and the geocentric distance r as spherical coordinate, cf. [2.5.1]. From Fig. 4.3, the corresponding equation of the *ellipse* is given by

$$p = r \cos \bar{\varphi}, \quad \bar{Z} = r \sin \bar{\varphi}, \quad (4.9)$$

where p follows from (4.5), (4.6).

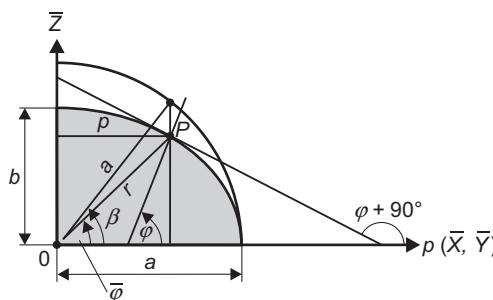


Fig. 4.3: Geodetic, reduced, and geocentric latitude.

The *reduced latitude* β is obtained by projecting (parallel to the \bar{Z} -axis) from the ellipse to the concentric circle of radius a (Fig. 4.3). Since the ratio of the elliptical to the circular coordinates is $\frac{b}{a}$ (ellipse as the affine image of the circle), we have

$$p = a \cos \beta, \quad \bar{Z} = \frac{b}{a} \sin \beta = b \sin \beta. \quad (4.10)$$

Using β instead of φ formally transforms ellipsoidal into spherical formulas, see also [6.3.3].

Comparing (4.9) and (4.10) with (4.7) provides the transformation between φ , $\bar{\varphi}$, and β :

$$\begin{aligned} \tan \bar{\varphi} &= \left(\frac{b}{a}\right)^2 \tan \varphi = (1 - e^2) \tan \varphi, \\ \tan \beta &= \frac{b}{a} \tan \varphi = \sqrt{1 - e^2} \tan \varphi. \end{aligned} \quad (4.11a)$$

A series expansion yields the differences in the angles:

$$\varphi - \bar{\varphi} = \frac{e^2}{2} \sin 2\varphi + \dots = 2(\varphi - \beta). \quad (4.11b)$$

The maximum difference occurs at $\varphi = 45^\circ$, with $(\varphi - \bar{\varphi}) = 690''$.

4.1.2 Curvature

The meridians and parallels are the *lines of curvature* of the rotational ellipsoid. The principal *radii of curvature* are therefore in the plane of the meridian and in the plane of the prime vertical perpendicular to the meridian plane (Fig. 4.4).

The curvature of the *meridian* (curvature radius M) $\bar{Z} = \bar{Z}(p)$ in the \bar{Z}, p -plane is given by

$$\frac{1}{M} = - \frac{\frac{d^2 \bar{Z}}{dp^2}}{\left(1 + \left(\frac{d\bar{Z}}{dp}\right)^2\right)^{\frac{3}{2}}}. \quad (4.12)$$

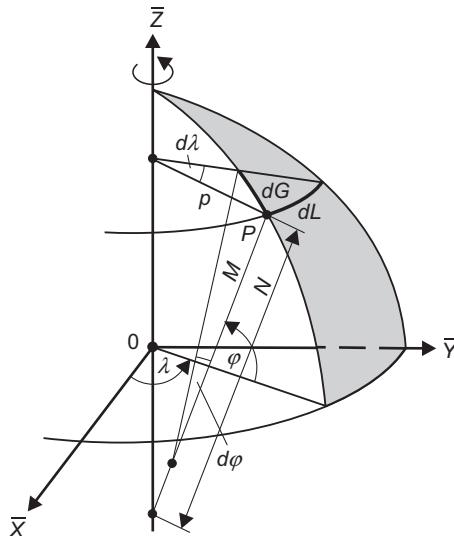


Fig. 4.4: Curvature of the rotational ellipsoid.

With (4.7) and its derivative, and taking (4.2) into account, we obtain the meridian radius of curvature

$$M = \frac{a(1-e^2)}{(1-e^2\sin^2\varphi)^{\frac{3}{2}}}. \quad (4.13)$$

The plane of a parallel circle (oblique section of the rotational ellipsoid) and the vertical plane in the same tangential direction intersect at point P with the angle φ . The theorem of *Meusnier* (regarding surface curvatures, see, e.g., Stoker, 1969) provides the radius of curvature in the *prime vertical*:

$$N = \frac{p}{\cos\varphi}. \quad (4.14)$$

Because of rotational symmetry, the origin of N is on the spin axis. Inserting (4.6) and (4.8) into (4.14), one obtains

$$N = \frac{a}{(1-e^2\sin^2\varphi)^{\frac{1}{2}}}. \quad (4.15)$$

A comparison of (4.13) and (4.15) shows that $N \geq M$. At the poles ($\varphi = \pm 90^\circ$), the polar radius of curvature becomes

$$c = M_{90} = N_{90} = \frac{a^2}{b}. \quad (4.16)$$

At the equator ($\varphi = 0^\circ$) the values are

$$M_0 = \frac{b^2}{a}, \quad N_0 = a. \quad (4.17)$$

The *curvature* of the ellipsoidal *normal section* with the geodetic azimuth α is computed according to *Euler's formula* by

$$\frac{1}{R_\alpha} = \frac{\cos^2\alpha}{M} + \frac{\sin^2\alpha}{N}. \quad (4.18)$$

Here, R_α is the radius of curvature. The *geodetic azimuth* α is defined as the angle measured in the horizontal plane between the ellipsoidal meridian plane of P and the vertical plane containing the normal to P and the target point; α is reckoned from north in the clockwise direction. The *mean curvature* \bar{J} is given by

$$\bar{J} = \frac{1}{2} \left(\frac{1}{M} + \frac{1}{N} \right). \quad (4.19)$$

The *arc lengths* of the *coordinate lines* of the φ, λ -system are computed using M and N . For the arc elements of the meridian and the parallel, respectively, we obtain (Fig. 4.4)

$$dG = M d\varphi, \quad dL = N \cos\varphi d\lambda. \quad (4.20)$$

With (4.13), the length of the *meridian arc* (starting at the equator) becomes

$$G = \int_0^\varphi M d\varphi = a(1-e^2) \int_0^\varphi \frac{d\varphi}{(1-e^2\sin^2\varphi)^{\frac{3}{2}}}. \quad (4.21a)$$

Equation (4.21a) can be reduced to an elliptic integral of the second kind, which cannot be evaluated in a closed form (Kutterer, 1998). Practical computations may be

based on numerical integration (e.g., by Simpson's rule) or on a binomial expansion of the denominator. Subsequent term-by-term integration then yields

$$G = a(1 - e^2) \left(\left(1 + \frac{3}{4}e^2 + \dots \right) \varphi - \left(\frac{3}{8}e^2 + \dots \right) \sin 2\varphi + \dots \right). \quad (4.21b)$$

Short arcs ($\Delta\varphi = \varphi_2 - \varphi_1 < 1^\circ$) can be calculated by a rapidly converging Taylor expansion. Expanding about the middle latitude $\varphi_m = \frac{(\varphi_1 + \varphi_2)}{2}$ yields

$$\Delta G_{1,2} = G_2 - G_1 = \left. \left(\frac{dG}{d\varphi} \right) \right|_{\varphi_m} \Delta\varphi + \dots \quad (4.21c)$$

According to (4.20), the arc length of a *circle of latitude* between the geodetic longitudes λ_1 and λ_2 is given by

$$\Delta L = \int_{\lambda_1}^{\lambda_2} N \cos \varphi d\lambda = N \cos \varphi (\lambda_2 - \lambda_1). \quad (4.22)$$

With $a = 6\ 378\ 137$ m, $b = 6\ 356\ 752$ m, and $e^2 = 0.006\ 694\ 380$ (for numerical values see [4.3]), we get for the radii of curvature at the poles and at the equator

$$c = 6\ 399\ 594 \text{ m}, \quad M_0 = 6\ 335\ 439 \text{ m}, \quad N_0 = a.$$

The arc lengths along the meridian and the parallel for $\varphi = 50^\circ$ are

$$\Delta G(\Delta\varphi = 1^\circ) = 111\ 229 \text{ m}, \quad \Delta L(\Delta\lambda = 1^\circ) = 71\ 696 \text{ m},$$

$$\Delta G(\Delta\varphi = 1') = 1853.8 \text{ m}, \quad \Delta L(\Delta\lambda = 1') = 1194.9 \text{ m},$$

$$\Delta G(\Delta\varphi = 1'') = 30.90 \text{ m}, \quad \Delta L(\Delta\lambda = 1'') = 19.92 \text{ m}.$$

Local approximations to the ellipsoid use the *Gaussian osculating sphere* of radius

$$R_G = \sqrt{M(\varphi)N(\varphi)}. \quad (4.23)$$

At the latitude φ , it has the same Gaussian curvature as the ellipsoid.

Global approximations can be based on a sphere with the *mean radius*

$$R_m = \frac{1}{3}(2a + b), \quad (4.24a)$$

the radius derived from equality of *volumes* (i.e., volume of sphere equals volume of ellipsoid)

$$R_V = \sqrt[3]{a^2 b}, \quad (4.24b)$$

or the radius for a sphere having a *surface area* equal to that of the ellipsoid. The latter one results from an integration over the ellipsoidal surface elements dG and dL (4.20), which after a series expansion yields

$$R_S = b \left(1 + \frac{2}{3}e^2 + \frac{3}{5}e^4 + \dots \right)^{1/2}. \quad (4.24c)$$

The numerical values for these three approaches agree within a few meters, which leads to a mean global value of $R = 6371$ km.

4.1.3 Spatial geodetic coordinates

The ellipsoidal surface coordinate system (φ, λ) can be extended to a spatial system by introducing the height h of the point P above the ellipsoid measured along the surface

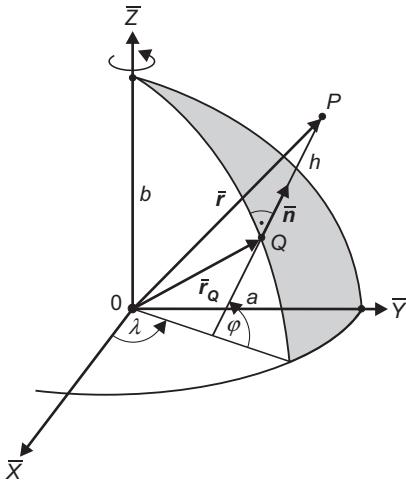


Fig. 4.5: Spatial geodetic coordinates.

normal (Fig. 4.5). The point Q on the ellipsoid thus is obtained by projecting the point P along the ellipsoidal normal: *Helmerit projection* (Grafarend, 2000, 2001). The spatial coordinates φ, λ, h are designated as *geodetic coordinates*.

The *coordinate surfaces* ($\varphi = \text{const.}$, $\lambda = \text{const.}$, $h = \text{const.}$) of this system are orthogonal. The *coordinate lines* (φ -line = geodetic meridian, λ -line = geodetic parallel, h -line = ellipsoidal normal) represent planar curves.

In (4.8) we substitute the first eccentricity e^2 for the semi-minor axis b , taking (4.15) into account; the coordinate vector for the point Q on the ellipsoid (4.8) then transforms into

$$\bar{\mathbf{r}}_Q = \begin{pmatrix} \bar{X}_Q \\ \bar{Y}_Q \\ \bar{Z}_Q \end{pmatrix} = N \begin{pmatrix} \cos \varphi \cos \lambda \\ \cos \varphi \sin \lambda \\ (1 - e^2) \sin \varphi \end{pmatrix}. \quad (4.25)$$

For the point P , we get according to Fig. 4.5

$$\bar{\mathbf{r}} = \bar{\mathbf{r}}_Q + h \bar{\mathbf{n}}, \quad (4.26a)$$

with the surface normal

$$\bar{\mathbf{n}} = \begin{pmatrix} \cos \varphi \cos \lambda \\ \cos \varphi \sin \lambda \\ \sin \varphi \end{pmatrix}, \quad (4.26b)$$

or

$$\bar{\mathbf{r}} = \begin{pmatrix} \bar{X} \\ \bar{Y} \\ \bar{Z} \end{pmatrix} = \begin{pmatrix} (N + h) \cos \varphi \cos \lambda \\ (N + h) \cos \varphi \sin \lambda \\ ((1 - e^2)N + h) \sin \varphi \end{pmatrix}. \quad (4.27)$$

The *inverse problem* can be solved for φ and h only by iterative methods. From (4.27) we get (e.g., Heiskanen and Moritz, 1967, p. 183)

$$h = \frac{\sqrt{\bar{X}^2 + \bar{Y}^2}}{\cos \varphi} - N, \quad \varphi = \arctan \frac{\bar{Z}}{\sqrt{\bar{X}^2 + \bar{Y}^2}} \left(1 - e^2 \frac{N}{N + h} \right)^{-1}$$

$$\lambda = \arctan \frac{\bar{Y}}{\bar{X}}. \quad (4.28)$$

The iteration process may start with $h = 0$, which results in a first approximation for φ , and so on. Close to the Earth's surface ($h \ll N$) the process converges quickly. Closed formulas, with negligible residual errors on the Earth's surface, are given by Bowring (1985). Efficient methods have also been developed for large heights (Borkowski, 1989; Sjöberg, 1999). The transformation (4.28) is a standard problem in satellite geodesy, cf. [6.2.1].

Local ellipsoidal (geodetic) systems are introduced in analogy to the local astronomic systems, cf. [2.5], and represent an approximation to them (Fig. 4.6). With the origin at the point P , the local system is connected to the ellipsoidal vertical (outer surface normal \bar{n} to the ellipsoid) through the geodetic latitude and longitude (4.26b). The \bar{z} -axis is directed towards the ellipsoidal zenith, with the \bar{x} , \bar{y} -plane being perpendicular to it. The \bar{x} -axis points to the ellipsoidal north (direction of the ellipsoidal meridian), and the \bar{y} -axis points towards east (left-handed system).

A target point P_i is described with respect to P by the geodetic (ellipsoidal) azimuth α , introduced in [4.1.2], the ellipsoidal zenith angle ζ , and the straight distance s between P and P_i . The zenith angle is measured in the vertical plane between the ellipsoidal vertical and the connecting line and reckoned positively from the zenith. These polar coordinates can be transformed into the local \bar{x} , \bar{y} , \bar{z} -system by a relation corresponding to (2.20):

$$\bar{x} = \begin{pmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \end{pmatrix} = s \begin{pmatrix} \cos \alpha \sin \zeta \\ \sin \alpha \sin \zeta \\ \cos \zeta \end{pmatrix}. \quad (4.29)$$

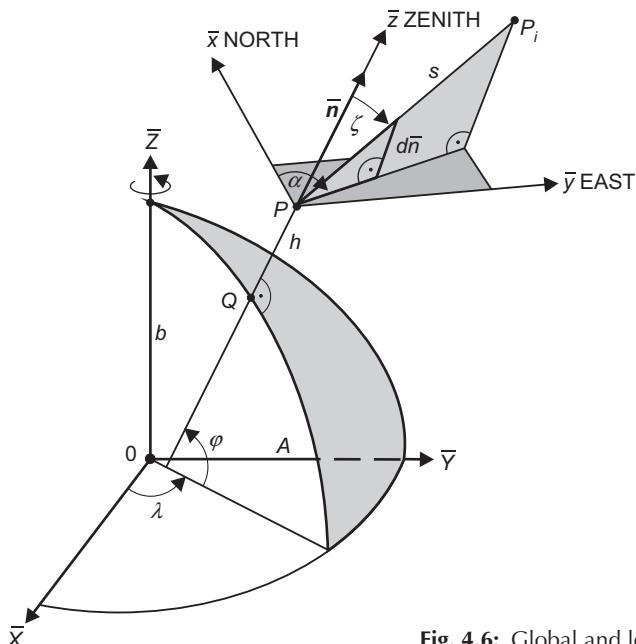


Fig. 4.6: Global and local ellipsoidal system.

After applying the reflection matrix \mathbf{S}_2 (2.23), the local system is transformed to the global $\bar{X}, \bar{Y}, \bar{Z}$ -system by the rotation matrices $\mathbf{R}_2(90^\circ - \varphi)$ and $\mathbf{R}_3(180^\circ - \lambda)$, which correspond to (2.24) and (2.25):

$$\Delta\bar{\mathbf{X}} = \bar{\mathbf{A}}\bar{\mathbf{x}}, \quad (4.30)$$

with

$$\Delta\bar{\mathbf{X}} = (\Delta\bar{X}, \Delta\bar{Y}, \Delta\bar{Z})^T \quad (4.31)$$

and

$$\begin{aligned} \bar{\mathbf{A}} &= \mathbf{R}_3(180^\circ - \lambda)\mathbf{R}_2(90^\circ - \varphi)\mathbf{S}_2 \\ &= \begin{pmatrix} -\sin\varphi\cos\lambda & -\sin\lambda & \cos\varphi\cos\lambda \\ -\sin\varphi\sin\lambda & \cos\lambda & \cos\varphi\sin\lambda \\ \cos\varphi & 0 & \sin\varphi \end{pmatrix} \end{aligned} \quad (4.32)$$

The inversion of (4.32) gives

$$\bar{\mathbf{x}} = \bar{\mathbf{A}}^{-1}\Delta\bar{\mathbf{X}}, \quad (4.33)$$

with

$$\bar{\mathbf{A}}^{-1} = \bar{\mathbf{A}}^T = \begin{pmatrix} -\sin\varphi\cos\lambda & -\sin\varphi\sin\lambda & \cos\varphi \\ -\sin\lambda & \cos\lambda & 0 \\ \cos\varphi\cos\lambda & \cos\varphi\sin\lambda & \sin\varphi \end{pmatrix}, \quad (4.34)$$

which corresponds to (2.28) and (2.29).

4.2 The normal gravity field

A “normal” gravity field may be referenced to the rotational ellipsoid by considering the latter to be a “level” ellipsoid, with mass and rotational velocity. This Earth model is now generally accepted as a geodetic reference system; higher order models generally do not offer any advantage [4.2.1]. The external gravity field of the level ellipsoid can be determined unambiguously from the parameters defining it [4.2.2]. The geometry of the normal gravity field is of special interest for geodetic applications [4.2.3].

4.2.1 The level ellipsoid, level spheroids

We introduce an ellipsoidal gravity field composed of gravitation and centrifugal acceleration: *normal gravity field*. It is based upon four parameters: total mass M and angular velocity ω , and the geometric parameters a and f of the rotational ellipsoid. In addition, we require the surface of this ellipsoid to be a level surface of its own gravity field. According to the theorem of *Stokes-Poincaré*, the gravity field then is uniquely defined in the space exterior to the ellipsoid.

Theorem of Stokes-Poincaré: If a body of total mass M rotates with constant angular velocity ω about a fixed axis, and if S is a level surface of its gravity field enclosing the entire mass, then the gravity potential in the exterior space of S is uniquely determined by M , ω , and the parameters defining S .

The Earth model defined in that way is called a *level* (or equipotential) *ellipsoid*. Instead of a , f , M and ω , other sets of four independent parameters can be used for its definition. If the parameters are given values which correspond to the real Earth, then an optimum approximation to the geometry of the geoid and to the external gravity field is achieved: *mean Earth ellipsoid*, cf. [4.3]. From the physical point of view, an Earth model would be required which is in *hydrostatic equilibrium*. All its level surfaces then coincide with the surfaces of equal density and equal pressure. Deviations from this model would indicate stress in the Earth's body, cf. [8.1].

The theory of the level ellipsoid has been developed by *P. Pizetti* (1894), *C. Somigliana* (1929), and others (Heiskanen and Moritz, 1967, p. 64). Equilibrium figures have been discussed as physical Earth models since the days of *Newton* and *Clairaut*, cf. [1.3.2], see Ledersteger (1956/1969), Moritz (1990).

In the above definition of the level ellipsoid, nothing has been stated regarding the interior mass distribution. But from the theory of equilibrium figures, it follows that only the homogeneous ellipsoids of *MacLaurin* exist in equilibrium. On the other hand, the surface of an equilibrium figure constructed of shells of equal density, and thus corresponding more to the real structure of the Earth, is *not* an ellipsoid. Nevertheless, a layered structure of the interior mass of the level ellipsoid that approximates the actual situation, and reproduces sufficiently well the gravity field of the level ellipsoid, can be found (Moritz, 1968a). The maximum deviation between the level surfaces and the surfaces of equal density are at the order of r^2 only, and the differences in stress remain considerably smaller for the model than for the real Earth. The level ellipsoid thus can also serve as a bounding surface for a *geophysical Earth model* (Marussi et al., 1974).

There have been several attempts to construct Earth models with a better fit to the geoid and the external gravity field than that provided by the level ellipsoid. A physical approximation consists of reference figures derived from truncated spherical harmonic expansions of the gravity potential of the Earth: *level spheroids*, cf. [3.3.2]. By assuming symmetry about the equator and truncating at degree $l = 2$ (*Brun's spheroid*) and $l = 4$ (*Helmert's spheroid*), we obtain surfaces of fourteenth and twenty-second order, respectively. The deviations from the rotational ellipsoid having the same length of the axis are on the order of f^2 for $l = 2$, and f^3 for $l = 4$. From the tesseral harmonics of second degree and order, with the harmonic coefficients $C_{2,2}$ and $S_{2,2}$, the equatorial principal moments of inertia and their directions can be calculated. The results can be used to derive a *triaxial ellipsoid*, as another geometrical approximation to the geoid.

First attempts in this direction were made by *Helmert* (1915) and *Heiskanen* (1924). They were based on the sparse gravity data available at that time, and spherical harmonic expansions of normal gravity derived from them. Recent results stem from Earth gravitational models obtained from satellite methods. They deliver a difference of about 70 m between the radii of the equatorial principal axes of inertia (corresponding to an equatorial flattening of about 1/91 000), where the larger radius is directed to 14.9° W longitude (Burša, 1995a; Marchenko, 2009).

These higher order Earth models do not significantly reduce the deviations to the geoid, as compared to the level ellipsoid. In addition, computations related to these surfaces and their gravity fields become more complicated. Finally, they are generally not suitable as physical normal figures. Although, for instance, triaxial rotational ellipsoids exist

as equilibrium figures (homogeneous ellipsoids of *Jacobi*), such ellipsoids would yield a completely unnatural form when using the actual values for the angular velocity and mass of the Earth.

4.2.2 The normal gravity field of the level ellipsoid

The external gravity field of the level ellipsoid (normal gravity field) can be modeled by *closed formulas* in the system of *ellipsoidal coordinates* β, λ, u . The reduced latitude β and the geodetic longitude λ have been already introduced in [4.1.1]. The third coordinate u is the semi-minor axis of the ellipsoid with constant linear eccentricity ε , see (4.3), which passes through the point P (Fig. 4.7). From (4.8) and (4.10), and putting $\sqrt{u^2 + \varepsilon^2}$ for the semi-major axis, the transformation from the ellipsoidal coordinates to the Cartesian ones is given by

$$\begin{pmatrix} \bar{X} \\ \bar{Y} \\ \bar{Z} \end{pmatrix} = u \begin{pmatrix} \sqrt{1 + \left(\frac{\varepsilon}{u}\right)^2} \cos\beta \cos\lambda \\ \sqrt{1 + \left(\frac{\varepsilon}{u}\right)^2} \cos\beta \sin\lambda \\ \sin\beta \end{pmatrix}. \quad (4.35)$$

For $\varepsilon = 0$, the β, λ, u -system with $\beta = 90^\circ - \vartheta$ and $u = r$ reduces into the system of spherical coordinates (2.13).

We denote the vector of *normal gravity* by γ and the normal gravity *potential* by U . In analogy to (3.43), we have

$$\gamma = \text{grad } U. \quad (4.36a)$$

With respect to the surface normal, γ is given in analogy to (3.72) by

$$\gamma = -\gamma \begin{pmatrix} \cos\varphi \cos\lambda \\ \cos\varphi \sin\lambda \\ \sin\varphi \end{pmatrix}. \quad (4.36b)$$

Corresponding to (3.42), U is composed of the gravitational potential V_E and the potential of the centrifugal acceleration Z_E :

$$U = V_E + Z_E. \quad (4.37)$$

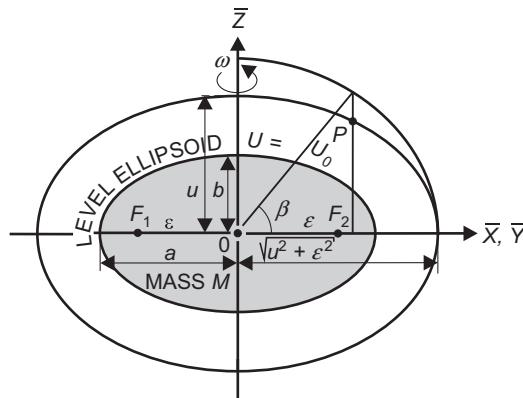


Fig. 4.7: Level ellipsoid and ellipsoidal coordinates.

The gravitational potential satisfies Laplace's differential equation (3.29) in the space exterior to the ellipsoid that contains the total mass.

By expressing Laplace's equation in ellipsoidal coordinates β, λ, u , we get a solution for the potential U , based on ellipsoidal harmonics. Adding the centrifugal potential (3.38), and taking both rotational symmetry and the condition of the ellipsoid surface as a level surface into account, we obtain a closed expression for the normal gravity potential (Heiskanen and Moritz, 1967, p. 64):

$$U = \frac{GM}{\varepsilon} \arctan \frac{\varepsilon}{u} + \frac{\omega^2}{2} a^2 \frac{q}{q_0} \left(\sin^2 \beta - \frac{1}{3} \right) + \frac{\omega^2}{2} (u^2 + \varepsilon^2) \cos^2 \beta. \quad (4.38)$$

Here, q is an auxiliary quantity depending only on the geometric parameters ε and u . On the ellipsoid surface ($u = b$), it is denoted q_0 :

$$q = \frac{1}{2} \left(1 + 3 \frac{u^2}{\varepsilon^2} \right) \arctan \frac{\varepsilon}{u} - 3 \frac{u}{\varepsilon}, \quad q_0 = q_{u=b}. \quad (4.39)$$

Hence, in agreement with the *Stokes-Poincaré* theorem, cf. [4.2.1], the normal gravity potential is determined by the four parameters a, b, M, ω . It does not depend on the geodetic longitude. If one puts $u = b$ and $q = q_0$ in (4.38), the potential of the *level ellipsoid* reads

$$U_0 = \frac{GM}{\varepsilon} \arctan \frac{\varepsilon}{b} + \frac{\omega^2}{3} a^2. \quad (4.40)$$

The normal gravity γ is perpendicular to the level ellipsoid, so that in accordance with (4.36), only the orthogonal component appears in the derivative of U (4.38). If the geodetic latitude φ is used instead of the reduced latitude β , we obtain the formula of *Somigliana* (1929) for the *normal gravity* on the *ellipsoid*

$$\gamma_0 = \frac{a\gamma_a \cos^2 \varphi + b\gamma_b \sin^2 \varphi}{\sqrt{a^2 \cos^2 \varphi + b^2 \sin^2 \varphi}}. \quad (4.41a)$$

For numerical computations, the form

$$\gamma_0 = \gamma_a \frac{1 + k \sin^2 \varphi}{(1 - e^2 \sin^2 \varphi)^{\frac{1}{2}}} \text{ with } k = \frac{b\gamma_b}{a\gamma_a} - 1 \quad (4.41b)$$

is more convenient (Moritz, 2000).

Here, the normal gravity, which depends on latitude only, is represented by the four parameters a, b, γ_a (normal gravity at the equator), and γ_b (normal gravity at the pole). The ellipsoidal parameters $a, b, M, \omega, \gamma_a, \gamma_b$ appearing in (4.38) and (4.41) are interrelated according to the theorem of *Pizetti*

$$2 \frac{\gamma_a}{a} + \frac{\gamma_b}{b} = \frac{3GM}{a^2 b} - 2\omega^2 \quad (4.42)$$

and the theorem of *Clairaut*

$$f + \beta = \frac{\omega^2 a}{\gamma_a} (1 + e'^2)^{-\frac{1}{2}} \left(1 + e' \frac{3 \left(1 + \frac{1}{e'^2} \right) \left(1 - \frac{1}{e'} \arctan e' \right) - 1}{\left(1 + \frac{3}{e'^2} \right) \arctan e' - \frac{3}{e'}} \right). \quad (4.43)$$

Thus, again only four independent parameters remain. In (4.43), besides the second eccentricity e' and the geometric flattening f , there is also the *gravity flattening*

$$\beta = \frac{\gamma_b - \gamma_a}{\gamma_a}. \quad (4.44)$$

Remark: The abbreviation β is used for both the reduced latitude and the gravity flattening; confusion is not to be anticipated.

The normal gravity in the *exterior space* is obtained by partial differentiation of (4.38). Near the ellipsoid, a Taylor series expansion with respect to the ellipsoidal height is sufficient, see below.

Application of normal gravity field formulas, (4.38) to (4.43), is often facilitated by *series expansions* with respect to f , or some other quantity that describes the polar flattening.

We start with the spherical harmonic expansion of the gravitational potential. Due to the symmetry with respect to the rotational axis (tesseral terms are zero) and the equatorial plane (odd zonal terms are zero), we obtain, upon adding the centrifugal potential (3.96a) expressed in spherical coordinates, the *potential* of normal gravity in terms of Legendre polynomials, cf. [3.3.2],

$$U = \frac{GM}{r} \left(1 - \sum_{n=1}^{\infty} \left(\frac{a}{r} \right)^{2n} J_{2n} P_{2n}(\cos \vartheta) \right) + \frac{\omega^2}{2} r^2 \sin^2 \vartheta. \quad (4.45)$$

If P_2 is substituted from (3.83a), the expansion up to $n = 1$ (corresponding to the spherical harmonic degree $l = 2$) yields an approximation linear in f :

$$U = \frac{GM}{r} \left(1 - \left(\frac{a}{r} \right)^2 J_2 \left[\frac{3}{2} \cos^2 \vartheta - \frac{1}{2} \right] + \frac{\omega^2}{2GM} r^3 \sin^2 \vartheta \right). \quad (4.46)$$

Solving for r and setting $U = U_0$ gives the *radius vector* to the level ellipsoid, where we have put $r = a$ on the right-hand side:

$$r = \frac{GM}{U_0} \left(1 - J_2 \left[\frac{3}{2} \cos^2 \vartheta - \frac{1}{2} \right] + \frac{\omega^2 a^3}{2GM} \sin^2 \vartheta \right). \quad (4.47)$$

The *normal gravity* γ follows from the derivative of (4.46) with respect to r :

$$\gamma = \frac{GM}{r^2} \left(1 - 3 \left(\frac{a}{r} \right)^2 J_2 \left[\frac{3}{2} \cos^2 \vartheta - \frac{1}{2} \right] - \frac{\omega^2}{GM} r^3 \sin^2 \vartheta \right). \quad (4.48)$$

If we substitute either $\vartheta = 90^\circ$ (equator) or 0° (pole) in (4.47) and (4.48), then we obtain either the semi-major axis a and the equatorial gravity or the semi-minor axis b and the polar gravity of the ellipsoid. Using these values, the *geometric flattening* f (4.1a) and the *gravity flattening* β (4.44) may be computed according to

$$f = \frac{3}{2} J_2 + \frac{m}{2}, \quad \beta = -\frac{3}{2} J_2 + 2m. \quad (4.49)$$

Here,

$$m = \frac{\omega^2 a}{\gamma_a} \quad (4.50)$$

is the ratio of the centrifugal acceleration to the normal gravity at the equator, a rigorous formula is given by (4.56).

From (4.48) and (4.49), we arrive at an approximation to the theorem of *Pizetti* (4.42)

$$GM = a^2 \gamma_a \left(1 - f + \frac{3}{2} m \right) \quad (4.51)$$

and an approximation to *Clairaut's theorem* (4.43)

$$f + \beta = \frac{5}{2} m. \quad (4.52)$$

Substituting (4.49) and (4.50) into (4.48), we obtain Newton's gravity formula, cf. [1.3.2]:

$$\gamma_0 = \gamma_a(1 + \beta \sin^2 \varphi). \quad (4.53)$$

If two γ_0 gravity values are known on the ellipsoid (gravity reduction problem!) at different geographic latitudes φ , then γ_a and β may be computed from (4.53). With known values for the semi-major axis a and the angular velocity ω , (4.50) supplies the quantity m . Finally, Clairaut's theorem (4.52) yields the geometric flattening f , which thus can be determined from gravity values. Application of this principle to the real Earth – that is, deriving geometric form parameters from physical quantities – leads to the gravimetric method of physical geodesy, cf. [6.5.1].

The relations above (linear in f , β , and m) may also be derived by series expansions of the closed formulas. They had already been found by Clairaut ("Théorie de la Figure de la Terre" 1743). The expansion up to terms of the order f^2 yields (IAG, 1971)

$$f = \frac{3}{2}J_2 + \frac{m}{2} + \frac{9}{8}J_2^2 + \frac{15}{28}J_2m + \frac{3}{56}m^2, \quad (4.54)$$

$$\beta = -f + \frac{5}{2}m - \frac{17}{14}fm + \frac{15}{4}m^2, \quad (4.55)$$

$$m = \frac{\omega^2 a^2 b}{GM}, \quad (4.56)$$

$$\gamma_0 = \gamma_a(1 + \beta \sin^2 \varphi + \beta_1 \sin^2 2\varphi), \quad \beta_1 = \frac{1}{8}f^2 - \frac{5}{8}fm. \quad (4.57)$$

One of the first applications of Clairaut's theorem was made by Helmert (1901). An adjustment of about 1400 free-air reduced gravity values to the gravity formula (4.57) yielded the parameters $\gamma_a = 9.7803 \text{ m s}^{-2}$ and $\beta = 0.005302$, with a flattening of $f = 1/298.3$.

The harmonic coefficients of second and fourth degree may be computed from f and m as follows:

$$J_2 = \frac{2}{3}f - \frac{m}{3} - \frac{1}{3}f^2 + \frac{2}{21}fm, \quad J_4 = -\frac{4}{5}f^2 + \frac{4}{7}fm. \quad (4.58)$$

For today's accuracy requirements, an expansion up to $n = 3$ (corresponding to $l = 6$) is generally adequate. That is, the expansion has to include the terms of the order f^3 (Cook, 1959). Developments up to the order f^5 have been given by Chen (1982).

Near the Earth's surface, a Taylor series expansion with respect to the ellipsoidal height h is sufficient for the derivation of the normal gravity in the exterior space:

$$\gamma = \gamma_0 + \left(\frac{\partial \gamma}{\partial h} \right)_0 h + \frac{1}{2} \left(\frac{\partial^2 \gamma}{\partial h^2} \right)_0 h^2 + \frac{1}{6} \left(\frac{\partial^3 \gamma}{\partial h^3} \right)_0 h^3 + \dots \quad (4.59)$$

The partial derivative $\frac{\partial \gamma}{\partial h}$ is obtained by applying Bruns' equation (3.71) to the exterior space:

$$\frac{\partial \gamma}{\partial h} = -2\gamma\bar{J} - 2\omega^2, \quad (4.60)$$

where \bar{J} is the mean curvature of the ellipsoid (4.19). A series expansion up to the order of f leads to the vertical component of the normal gravity gradient

$$\frac{\partial \gamma}{\partial h} = -2\frac{\gamma}{a}(1 + f + m - 2fs \sin^2 \varphi). \quad (4.61)$$

The second and the third derivative can be derived from a spherical approximation of γ where $\partial\gamma/\partial h = \partial\gamma/\partial r$ etc., see (3.17). With

$$\gamma = \frac{GM}{r^2}, \quad \frac{\partial\gamma}{\partial r} = -2\frac{GM}{r^3} = -2\frac{\gamma}{r}$$

we obtain

$$\frac{\partial^2\gamma}{\partial r^2} = \frac{6GM}{r^4} = 6\frac{\gamma}{r^2}, \quad \frac{\partial^3\gamma}{\partial r^3} = -24\frac{GM}{r^5} = -24\frac{\gamma}{r^3}. \quad (4.62)$$

Inserting the above into (4.59), with $r = a$ and $\gamma = \gamma_0$, leads to the normal gravity as a function of latitude and height:

$$\gamma = \gamma_0 \left(1 - \frac{2}{a} (1 + f + m - 2f \sin^2 \varphi) h + \frac{3}{a^2} h^2 \right) + \dots, \quad (4.63)$$

where the h^3 -term has to be added for higher altitudes. Airborne and satellite applications require rigorous formulas, at which γ is derived by differentiating the normal gravity potential (4.38). The results are given in the β, λ, u -system, and can be easily transformed into a three-dimensional Cartesian coordinate system (4.35), cf. Hofmann-Wellenhof and Moritz (2005, p. 240 ff.).

With $\gamma = 9.81 \text{ m s}^{-2}$ and $a = 6378 \text{ km}$, we get $\frac{\partial\gamma}{\partial h} = -3.086 \mu\text{m s}^{-2}/\text{m}$ and $\frac{\partial^2\gamma}{\partial h^2} = 1.5 \times 10^{-6} \mu\text{m s}^{-2}/\text{m}^2$. More detailed numerical values are given in [4.3]. In gravity reductions the value $-3.086 \mu\text{m s}^{-2}/\text{m}$ is used conventionally.

4.2.3 Geometry of the normal gravity field

The geometry of the normal gravity field is represented by the spheropotential surfaces and the normal plumb lines.

The *spheropotential surfaces* are surfaces of constant normal gravity potential

$$U = U(\mathbf{r}) = \text{const.} \quad (4.64)$$

With the exception of the surface of the level ellipsoid ($U = U_0$), spheropotential surfaces deviate from ellipsoids and are not parallel to each other. The *normal plumb lines* intersect the spheropotential surfaces orthogonally. Due to the non-parallelism of the level surfaces, they are slightly curved in the plane of the meridian (Fig. 4.8).

In order to describe the geometry of the normal gravity field, “normal” geodetic coordinates φ^N, λ^N, U are introduced. They are defined in analogy to the “natural” coordinates ϑ, Λ, W of the actual gravity field, cf. [3.2.3]. The normal geodetic coordinates refer to the point Q , which is related to the surface point $P(\Phi, \Lambda, W)$ by the conditions:

$$\varphi_Q^N = \Phi_p, \quad \lambda_Q^N = \Lambda_p, \quad U_Q = W_p. \quad (4.65)$$

The surface thus defined in a point-wise manner approximates the physical surface of the Earth, with deviations less than 100 m and less than one arcmin, respectively. This surface is called the *telluroid* (Hirvonen, 1960). It is not a level surface of the normal gravity field, but it resembles the Earth’s surface.

The *normal geodetic latitude* φ^N is the angle measured in the meridian plane between the equatorial plane of the ellipsoid and the direction of the normal plumb line. It differs from the geodetic latitude φ , introduced in [4.1.1], by the small angle $\delta\varphi^N$. This difference is a result of the normal plumb line curvature, see below. The *normal geodetic*

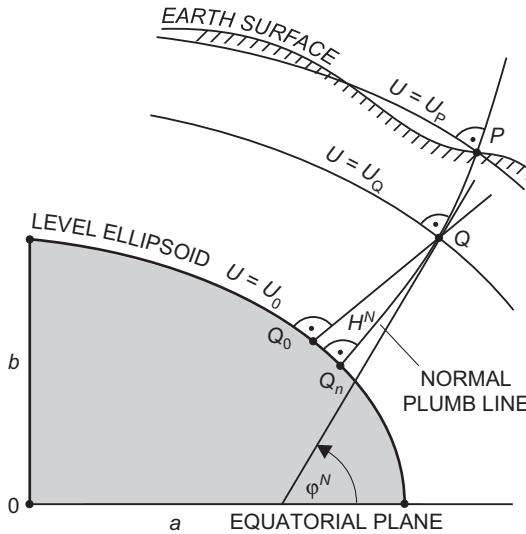


Fig. 4.8: Spheropotential surfaces, normal plumb line, normal height.

longitude λ^N is equal to the geodetic longitude λ . The *normal gravity potential* U relates the point Q to the level surface $U = U_Q$.

Instead of U , the potential difference $U_0 - U_Q$ to the level ellipsoid may be used for that purpose. With $U_Q = W_p$, and the condition $U_0 = W_0$, cf. [6.5.4], we obtain the *normal height* H^N already introduced in [3.4.3]:

$$H^N = \frac{U_0 - U_Q}{\bar{\gamma}} = \frac{W_0 - W_p}{\bar{\gamma}}. \quad (4.66)$$

Hence, H^N is defined as the distance between Q and the level ellipsoid measured along the normal plumb line. To a good approximation, H^N may be measured along the ellipsoidal normal passing through the surface point. According to (3.107), $\bar{\gamma}$ is the mean normal gravity between the ellipsoid and Q . Substituting γ from (4.63) into (3.107) and integrating yields

$$\bar{\gamma} = \gamma_0 \left(1 - \frac{1}{a} (1 + f + m - 2f \sin^2 \phi) H^N \right). \quad (4.67)$$

Hence, $\bar{\gamma}$ may be computed rigorously in an iterative manner. Since C can be derived from measurements, the normal height can be determined without any hypothesis. Extending the normal heights downward from the Earth's surface yields the *quasigeoid*, which is used as a reference surface for heights, cf. [3.4.3].

The normal geodetic coordinates ϕ^N, λ^N, H^N have gained special importance for the direct determination of the physical surface of the Earth according to the theory of Molodensky, cf. [6.5.1], [6.7.2]. Normal heights have been introduced for a number of national height systems, cf. [7.2].

The curvature of the *spheropotential surfaces* is described by the second derivatives of U , in analogy to the actual gravity field, see (3.57), (3.58). In the local

ellipsoidal system, the curvatures in the direction of the meridian and the parallel are given by

$$k_x^N = -\frac{U_{\bar{x}\bar{x}}}{\gamma}, \quad k_y^N = -\frac{U_{\bar{y}\bar{y}}}{\gamma}. \quad (4.68)$$

The geodetic *torsion* is zero due to the rotational symmetry of the level ellipsoid:

$$t_{\bar{x}}^N = -\frac{U_{\bar{x}\bar{y}}}{\gamma} = 0. \quad (4.69)$$

On the ellipsoid, the curvature is given by the principal radii of curvature M and N , see (4.13), (4.14):

$$k_{\bar{x}(0)}^N = \frac{1}{M}, \quad k_{\bar{y}(0)}^N = \frac{1}{N}. \quad (4.70)$$

Following (3.67), and taking the rotational symmetry into account, we get for the curvature of the projections of the *normal plumb line* onto the \bar{x} , \bar{z} - and the \bar{y} , \bar{z} -plane, respectively:

$$\kappa_{\bar{x}}^N = -\frac{U_{\bar{x}\bar{z}}}{\gamma}, \quad \kappa_{\bar{y}}^N = -\frac{U_{\bar{y}\bar{z}}}{\gamma} = 0. \quad (4.71)$$

On the level ellipsoid, we have with (4.20)

$$U_{\bar{x}\bar{z}(0)} = -\left(\frac{\partial \gamma}{\partial \bar{x}}\right)_0 = -\left(\frac{\partial \gamma}{M \partial \varphi}\right)_0. \quad (4.72)$$

Introducing the derivative $\frac{\partial \gamma}{\partial \varphi}$ from (4.53) and inserting into (4.71) yields with sufficient approximation

$$\kappa_{\bar{x}(0)}^N = \frac{\beta}{M} \sin 2\varphi \quad (4.72a)$$

with gravity flattening β (4.44). For the change of the normal gravity along the meridian, we thus get

$$\left(\frac{\partial \gamma}{\partial \bar{x}_0}\right) = \gamma \frac{\beta}{M} \sin 2\varphi = 8.2 \times 10^{-9} \sin 2\varphi \text{ m s}^{-2}/\text{m} \quad (4.72b)$$

which corresponds to $8.2 \text{ nm s}^{-2}/\text{m}$ at $\varphi = 45^\circ$. Together with the relation $U_{\bar{z}\bar{z}} = -\frac{\partial \gamma}{\partial \bar{z}}$, (4.68) to (4.72) completely define the Eötvös tensor (3.69) for the normal gravity field. According to (3.75), the differential transformation from the local to the global geodetic system is also provided by the curvature parameters.

Finally, we derive the differences between the geodetic coordinates φ , λ and the normal geodetic coordinates φ^N , λ^N :

$$\varphi = \varphi^N + \delta\varphi^N, \quad \lambda = \lambda^N. \quad (4.73)$$

From (4.71) and (4.72) we obtain

$$d\varphi^N = - \int_0^{H^N} \kappa_x^N dH^N = -\frac{\beta}{M} \sin 2\varphi H^N.$$

And with $\beta = 0.0053$ and $M \approx a = 6371 \text{ km}$ we get

$$\delta\varphi^N = -0.000 17'' \sin 2\varphi H^N, \quad (4.74)$$

where H^N is in meters.

4.3 Geodetic reference systems, optimum Earth model

Geodetic reference systems provide numerical values for the parameters of a geodetic Earth model. The systems are recommended by the International Union of Geodesy and Geophysics (IUGG) and represent the best parameter values for a designated epoch. The systems generally serve as a standard over a longer time span for geodesy and related disciplines such as astronomy, cartography, geophysics, engineering, and navigation.

All reference systems are supposed to be *geocentric*, with the Z-axis coinciding with the Earth's axis of rotation and the direction of the X-axis pointing to the Greenwich meridian. While the earlier reference systems may have large deviations from the geocentric system, recent reference systems agree at the "cm"-level. The orientation of geodetic systems with respect to the Earth is described by the "Geodetic Datum", cf. [6.2.2].

In the nineteenth and early twentieth century, the geometric parameters of reference ellipsoids were derived from various terrestrial data sets and then introduced as a reference for national geodetic surveys, cf. [1.3.3]. Normal gravity formulae referred to these ellipsoids have been derived since about 1900 and used for national gravimetric surveys. These regional or local reference systems may be regarded as precursors of the present global systems, which are based on the theory of the level ellipsoid.

Geodetic reference systems based on the theory of the level ellipsoid were first introduced in 1924/1930. At the IUGG General Assembly in Madrid 1924, *Hayford's ellipsoid* was introduced as the *International Ellipsoid*, with the parameters

$$a = 6\,378\,388 \text{ m}, f = 1/297.0. \quad (4.75a)$$

The General Assembly in Stockholm (1930) adopted the gravity formula established by *G. Cassinis* for Hayford's ellipsoid:

$$\gamma_0 = 9.780\,49(1 + 0.005\,2884\sin^2\varphi - 0.000\,0059\sin^22\varphi) \text{ m s}^{-2}. \quad (4.75b)$$

This corresponds to the normal gravity formula (4.57), assuming a level ellipsoid.

The geometric parameters a and f were calculated by *J. F. Hayford* (1909) from astrogeodetic observations in the U.S.A. In 1928, *W. A. Heiskanen* determined the equatorial gravity from an adjustment of isostatically reduced gravity values. The international reference system of 1924/1930 is thus defined by the four parameters a , f , γ_0 , ω . The corresponding ellipsoid has been applied in numerous geodetic surveys; also, the normal gravity formula has found broad acceptance.

At the General Assembly of the IUGG in Luzern (1967), the 1924/1930 reference system was replaced by the *Geodetic Reference System 1967* (GRS67), see IAG (1971). It was defined by the following parameters:

$$a = 6\,378\,160 \text{ m}, GM = 398\,603 \times 10^9 \text{ m}^3 \text{ s}^{-2}, J_2 = 1082.7 \times 10^{-6}. \quad (4.76a)$$

The angular velocity of the Earth's rotation

$$\omega = 7.292\,115\,146\,7 \times 10^{-5} \text{ rad s}^{-1}, \quad (4.76b)$$

not mentioned in the IUGG resolution, was adopted as the fourth parameter. The reference ellipsoid corresponding to this definition was declared a level ellipsoid.

The calculation of the semi-major axis was based on astrogeodetic observations collected over the continents, which were transformed into a uniform system by gravimetric methods.

Observations of space probes yielded the geocentric gravitational constant, which includes the mass of the atmosphere. The dynamic form factor was derived from the orbit perturbations of artificial satellites, and the angular velocity of the Earth's rotation was adopted from astronomy. The GRS67 has been used especially for scientific problems and for a few geodetic networks.

At the IUGG General Assembly in Canberra (1979), the *Geodetic Reference System 1980* (GRS80) was introduced. It is also based on the theory of the geocentric equipotential ellipsoid, with the defining parameters (Moritz, 2000):

$$\left. \begin{array}{ll} a = 6\ 378\ 137\ \text{m} & \text{equatorial radius of the Earth} \\ GM = 398\ 600.5 \times 10^9\ \text{m}^3\ \text{s}^{-2} & \text{geocentric gravitational} \\ & \text{constant of the Earth} \\ J_2 = 1082.63 \times 10^{-6} & (\text{including the atmosphere}) \\ & \text{dynamical form factor of the} \\ & \text{Earth (excluding the permanent} \\ & \text{tidal deformation)} \\ \omega = 7.292\ 115 \times 10^{-5}\ \text{rad s}^{-1} & \text{angular velocity of the Earth.} \end{array} \right\} \quad (4.77a)$$

With $M_{\text{atm}} = 0.88 \times 10^{-6}M$, we have $GM_{\text{atm}} = 0.35 \times 10^9\ \text{m}^3\ \text{s}^{-2}$.

With respect to the orientation, it is stated that the minor axis of the reference ellipsoid be parallel to the direction defined by the Conventional International Origin and that the primary meridian be parallel to the zero meridian of the BIH adopted longitudes, cf. [2.3].

The system is consistent with the IAU system of astronomical constants, cf. [2.3.1], [2.3.2]. It is now widely used as a reference for geodetic work, in theory as well as in practice.

The equatorial radius of the GRS80 ellipsoid has been derived from laser distance measurements to satellites, satellite altimetry, and Doppler positioning, with an uncertainty of 0.5 m. The calculation of the geocentric gravitational constant was based on space probes and lunar and satellite laser data ($\pm 0.05 \times 10^9\ \text{m}^3\ \text{s}^{-2}$), while the value for the dynamic form factor was taken from global gravity models ($\pm 5 \times 10^{-9}$). Again, the angular velocity of the Earth is a value derived from annual means over the last decades; velocity variations with time do not affect this rounded value (Burša, 1995a).

Numerical values for derived parameters include (Moritz, 2000):

Geometric constants, cf. [4.1.1], [4.1.2]:

$$\left. \begin{array}{ll} b = 6\ 356\ 752.3141\ \text{m} & \text{semi-minor axis} \\ e = 521\ 854.0097\ \text{m} & \text{linear eccentricity (4.3)} \\ c = 6\ 399\ 593.6259\ \text{m} & \text{polar radius of curvature (4.16)} \\ e^2 = 0.006\ 694\ 380\ 022\ 90 & \text{first eccentricity (e) (4.1b)} \\ e'^2 = 0.006\ 739\ 496\ 775\ 48 & \text{second eccentricity (e) (4.1c)} \\ f = 0.003\ 352\ 810\ 681\ 18 & \text{flattening (4.1a)} \\ 1/f = 298.257\ 222\ 101 & \text{reciprocal flattening} \\ G = 10\ 001\ 965.7293\ \text{m} & \text{meridian quadrant (4.21a)} \end{array} \right\} \quad (4.77b)$$

Physical constants, cf. [4.2.2]:

$U_0 = 62\ 636\ 860.850\ \text{m}^2\text{s}^{-2}$	normal potential at ellipsoid (4.40)	}
$J_4 = -0.000\ 002\ 370\ 912\ 22$	spherical harmonic coefficient (4.45)	
$J_6 = 0.000\ 000\ 006\ 083\ 47$	spherical harmonic coefficient (4.45)	
$J_8 = -0.000\ 000\ 000\ 014\ 27$	spherical harmonic coefficient (4.45)	
$m = 0.003\ 449\ 786\ 003\ 08$	(4.50)	
$\gamma_a = 9.780\ 326\ 771\ 5\ \text{m s}^{-2}$	normal gravity at equator (4.41)	
$\gamma_b = 9.832\ 186\ 368\ 5\ \text{m s}^{-2}$	normal gravity at pole (4.41)	
$\beta = 0.005\ 302\ 440\ 112$	(4.44)	
$k = 0.001\ 931\ 851\ 353$	(4.41b)	

Normal gravity can be computed by the closed formula (4.41) or the series expansion

$$\gamma_0 = \gamma_a \left(1 + 0.005\ 279\ 0414 \sin^2 \varphi + 0.000\ 023\ 2718 \sin^4 \varphi + 0.000\ 000\ 1262 \sin^6 \varphi + 0.000\ 000\ 0007 \sin^8 \varphi \right) \quad (4.78a)$$

which is accurate to $10^{-3}\ \mu\text{m s}^{-2}$. The conventional series (4.57) has an accuracy of $1\ \mu\text{m s}^{-2}$:

$$\gamma_0 = 9.780\ 327 \left(1 + 0.005\ 3024 \sin^2 \varphi - 0.000\ 0058 \sin^2 2\varphi \right) \text{m s}^{-2}. \quad (4.78b)$$

Inserting the values for the GRS80 into (4.63) yields the change of normal gravity with height:

$$\gamma = \gamma_0 - (3.0877 \times 10^{-3} - 4.3 \times 10^{-6} \sin^2 \varphi) h + 0.72 \times 10^{-6} h^2 \text{ m s}^{-2} \quad (4.79)$$

with h in km. A development accurate to $10\ \text{nm s}^{-2}$ for heights up to 10 km is given by Wenzel (1989).

According to the definition of GM , γ_0 refers to the total mass of the Earth including the atmosphere. If normal gravity values are required on the ellipsoid, or within the range of the atmosphere, the effect of the air masses above the calculation point must be subtracted from γ_0 . The corresponding reduction amounts to $-8.7\ \mu\text{m s}^{-2}(h=0)$, $-4.7\ \mu\text{m s}^{-2}(h=5\ \text{km})$, and $-0.1\ \mu\text{m s}^{-2}(h=30\ \text{km})$, cf. Ecker and Mittermayer (1969).

There is a lasting discussion to replace the semi-major axis a as one of the defining (or primary) parameters of the Geodetic Reference System by the normal potential U_0 on the level ellipsoid, set equal to the *geoid potential value* W_0 (Burša, 1992). As W_0 has a physical meaning (contrary to a), the whole set of defining parameters would be physically well-defined. In addition, W_0 is a relevant quantity at recent problems, as the definition of a world height system and as a reference for time definition and precise time keeping, under the aspect of General Relativity, cf. [3.4.3] and [2.2.1], respectively. Finally, W_0 does not depend on the permanent tidal effect, cf. [3.4.1], Burša (1995b). A “geopotential scale factor” $R_0 = GM/W_0$ can be derived from W_0 , and used instead of it. The semi-major axis of a best-fitting ellipsoid can be calculated on the basis of (4.40) and corresponding series developments (Burša et al., 1998). The geopotential value on the geoid is now well determined from long-term satellite altimetry data, cf. [3.4.3].

Optimum values for the *Earth model parameters* are determined at shorter time intervals and published by the International Association of Geodesy and the International Astronomical Union. The values are derived from least-squares adjustments employing satellite tracking, satellite gravity gradiometry, satellite altimetry, and terrestrial

gravimetry, and refer to a level ellipsoid which fits best to the geoid. Of special importance are the IERS numerical standards, given in the IERS Conventions (Groten, 2004; Petit and Luzum, 2010). According to these standards, the currently best estimates for the *defining parameters* of a level ellipsoid are as follows:

- The geocentric gravitational constant $GM = (398\ 600.442 \pm 0.001) \times 10^9 \text{ m}^3 \text{ s}^{-2}$ including the mass of the atmosphere. This value is derived from orbit analyses of satellites and space probes. A variation of GM with time has not been found.
- The *equatorial radius of the Earth* $a = 6\ 378\ 136.6 \pm 0.1 \text{ m}$. The radius is derived from an optimum fit between ellipsoidal heights, as obtained for satellite tracking stations, and from satellite altimetry, applying the minimum condition $\iint N^2 d\sigma = \min$. on the geoid heights. It is valid for the zero-frequency as well as for the tide-free system, cf. [3.4.1], and assumed to be constant with time.
- The second-degree zonal harmonic coefficient (*dynamical form factor*) $J_2 = (1082.6267 \pm 0.0001) \times 10^{-6}$ in the tide-free system, and $J_2 = (1082.6359 \pm 0.0001) \times 10^{-6}$ in the zero-tide system. J_2 is obtained from global gravitational field models. Temporal variations of the dynamical form factor have been significantly determined, cf. [8.3.5].
- The mean angular velocity of the *Earth's rotation* $\omega = 7.292\ 115 \times 10^{-5} \text{ rads}^{-1}$ is provided by the IERS, cf. [2.2.2]. For long-term variations see [8.3.2].

Among the quantities *derived* from the defining parameters we have

- The geoid potential $W_0 = 62\ 636\ 856.0 \pm 0.5 \text{ m}^2 \text{ s}^{-2}$. As discussed above, the potential may also be introduced instead of a as defining parameter, and it is also constant with time.
- The reciprocal *flattening* $1/f = 298.256\ 42 \pm 0.000\ 01$
- The *normal gravity* at the equator $\gamma_a = 9.780\ 328 \pm 0.000\ 002 \text{ m s}^{-2}$, both given in the zero-tide system.

5 Methods of Measurement

Modeling of geodetically relevant quantities (especially coordinates, gravity field quantities, and Earth rotation parameters) is based on observations taken on the Earth's surface and in its exterior space. Different measurement methods are available, delivering geometric or physical quantities. Geometric methods rely primarily on electromagnetic waves and thus are affected by atmospheric refraction [5.1]. The measurement methods may be divided into

- observations employing artificial satellites as targets (including the moon), sensors or carriers of sensors: satellite observations [5.2],
- observations to fixed stars and extragalactic radio sources: geodetic astronomy [5.3],
- terrestrial gravity and gravity gradient measurements: gravimetry [5.4], and
- determination of coordinate differences between points on the surface of the Earth: terrestrial geodetic measurements [5.5].

The measurement methods depend on available technology, where electronics governs data collection and online data-processing (Kahmen, 1978; Schlemmer, 1996). Space techniques now dominate global and regional surveys, while terrestrial methods are mainly used for interpolation in space and time, and at solving more local problems. Accuracy and resolution (spatial and temporal) of the results depend on the state of the art of the respective technique. Limiting factors include calibration errors and instrumental drift, and the elimination or reduction of effects directly disturbing the sensor and the measurement process. We especially mention variations of air temperature, atmospheric pressure, groundwater table, and magnetic field, as well as atmospheric refraction, microseismicity, and local site instabilities. Thus the inherent precision of the respective technique may deteriorate by a factor of two to three or more, when considering the accuracy obtained. For the physical fundamentals of geodetic measurement methods we refer to Heitz and Stöcker-Meier (1998), while Plag and Pearlman (2009) review the present state and the future directions of geodetic observation techniques.

5.1 Atmospheric refraction

In practically all geodetic measurements, electromagnetic waves serve as signal carriers; this includes the methods of satellite and terrestrial geodesy as well as geodetic astronomy. From the broad spectrum of electromagnetic waves, the visible light (380 to 780 nm, corresponding to 7.9 and 3.8×10^{14} Hz, respectively), the near infrared (up to 1 μm), and the microwave parts (1 mm to 1 m, corresponding to 300 GHz resp. 300 MHz) are used. When propagating through the atmosphere, the signals experience changes in velocity and curvature of the path (refraction), depending on the physical state of the atmospheric

gas masses [5.1.1]. Signal propagation is different in the troposphere and the ionosphere and has to be treated separately [5.1.2], [5.1.3].

Different methods have been developed in order to eliminate or reduce the effects of atmospheric refraction on geodetic measurements. These include instrument design, observation methodology, and the use of atmospheric models based on data collected on the Earth's surface and in space. The individual strategies will be discussed in the chapters that pertain to measurement methods, see also Brunner (1984a), De Munck and Spoelstra (1992), Dettmering et al. (2010).

5.1.1 Fundamentals

According to *Fermat's principle*, the path s of an electromagnetic wave is determined by the condition of a minimum travel time Δt of the wave (Moritz and Hofmann-Wellenhof, 1993, p. 158):

$$\Delta t = \int_{\text{path}} dt = \int_{\text{path}} \frac{ds}{v} = \min. \quad (5.1)$$

The velocity v differs from the velocity in vacuum c (2.2) by the *index of refraction* n (also called refractive index):

$$n = \frac{c}{v}. \quad (5.2)$$

For a gaseous medium, $n > 1$ is proportional to the density of the gas. If the medium is dispersive for a certain spectral domain, n also depends on the wavelength: *dispersion*. An average value for n near the Earth's surface is 1.0003. Instead of n , the *refractivity*

$$N = (n - 1) \times 10^6 \quad (5.3)$$

is frequently used.

Inserting (5.2) into (5.1) yields

$$\Delta t = \frac{1}{c} \int_{\text{path}} n ds = \min. \quad (5.4)$$

By setting

$$nds = d\bar{s},$$

(5.4) can also be expressed as a minimum condition for the "electromagnetic" path length (Fig. 5.1):

$$\bar{s} = \int_{\text{path}} d\bar{s} = \int_{\text{path}} n ds = \min. \quad (5.5)$$

Solving the variational problem (5.5) yields the path \bar{s} , but requires the knowledge of n along the path.

The effect of refraction on the *distance* is given by the difference between the actual path length \bar{s} and the straight-line s (chord):

$$\bar{s} - s = \int_{\text{path}} n ds - \int_0^s ds = \int_0^s (n - 1) ds + \left(\int_{\text{path}} n ds - \int_0^s n ds \right). \quad (5.6)$$

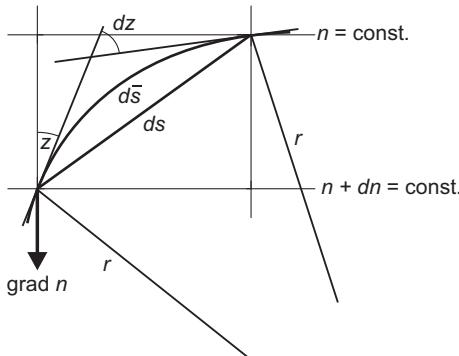


Fig. 5.1: Ray bending in the atmosphere.

The first term on the right side accounts for the difference in length due to the longer travel time in the atmosphere, while the second term represents the effect of the bending of the ray (Janes et al., 1991).

The refraction effect on *curvature* can be estimated by assuming that the air density is stratified horizontally. *Snell's law* describes the bending of the ray as it passes through layers of varying refractive index, which corresponds to Fermat's principle:

$$n \sin z = \text{const.} \quad (5.7a)$$

Or for two points P_1 and P_2 :

$$n_1 \sin z_1 = n_2 \sin z_2. \quad (5.7b)$$

Under the above assumption, the angle between the normal to the surface $n = \text{const.}$ and the tangent to the ray with curvature $1/r$ (the curvature radius r should not be confused with the corresponding spherical coordinate!) is the zenith angle z . Differentiation of (5.7a) yields

$$\sin z \, dn + n \cos z \, dz = 0. \quad (5.7c)$$

With

$$dn = (\text{grad } n) \cdot ds = |\text{grad } n| \cos z \, ds, \quad (5.8)$$

we obtain the curvature

$$\frac{1}{r} = \frac{dz}{ds} = -\frac{|\text{grad } n|}{n} \sin z. \quad (5.9)$$

By separating the horizontal and the vertical component of $\text{grad } n$, we get the curvatures of the ray projected into the horizontal and the vertical planes. The corresponding effects on horizontal and vertical angles are called *horizontal* (lateral) and *vertical* refraction, respectively.

Horizontal refraction is about one to two orders of magnitude less than vertical refraction. Neglecting the latter yields a simplified formula for the curvature of *vertical refraction*:

$$\frac{1}{r} = -\frac{1}{n dh} \sin z, \quad (5.10a)$$

where h is the geodetic height, cf. [4.1.3].

In terrestrial geodetic measurements, we have $n \approx 1$ and $z \approx 90^\circ$, which leads to

$$\frac{1}{r} = -\frac{dn}{dh}. \quad (5.10b)$$

Instead of $1/r$, the coefficient of refraction k is often used. It is defined as the ratio between the radius of the Earth R and the curvature radius r :

$$k = \frac{R}{r} = -R \frac{dn}{dh}. \quad (5.11)$$

The vertical refraction angle δ is the effect of refraction on observed zenith angles (Fig. 5.2). It results from integrating $1/r$ resp. dn/dh along the path:

$$\delta = \frac{1}{s_0^s} \int_0^s (s - s_i) \frac{dn}{dh} ds. \quad (5.12a)$$

Here, the local vertical gradient of n is weighted according to the distance from the observer; values from closer distances receive a larger weight. For a spherical arc ($r = \text{const.}$), and taking (5.11) into account, (5.12a) reduces to

$$\delta = \frac{k}{2R} s. \quad (5.12b)$$

In most geodetic applications, the signal is transferred by a modulation of the carrier wave. This can be regarded as a superposition of a group of waves with different frequencies. While phase velocity v_{ph} , introduced in (5.2), refers to the monochromatic carrier wave, the center of a short wave group (signal energy) propagates with the group velocity

$$v_{\text{gr}} = v_{\text{ph}} - \lambda \frac{dv_{\text{ph}}}{d\lambda}. \quad (5.13)$$

In a dispersive medium, we have $n = n(\lambda)$ and the velocity dispersion $dv_{\text{ph}}/d\lambda \neq 0$ (Leick, 2004). Taking (5.2) into account delivers the corresponding group refractive index

$$n_{\text{gr}} = n_{\text{ph}} - \lambda \frac{dn_{\text{ph}}}{d\lambda} = n_{\text{ph}} + f \frac{dn_{\text{ph}}}{df}, \quad (5.14)$$

with frequency f , cf. [5.1.2], [5.1.3].

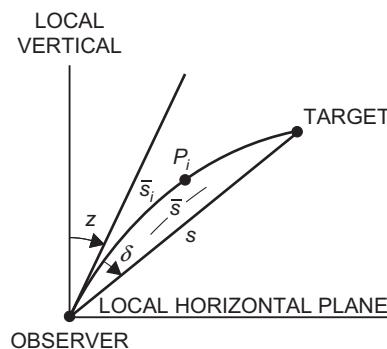


Fig. 5.2: Vertical refraction.

For a *standard atmosphere* with air temperature 273.15 K, air pressure 1013.25 hPa, humidity 0.0 hPa and CO₂ content 0.0375%, the *phase refractivity* may be calculated as follows (IAG resolution, General Assembly Birmingham, 1999; also CODATA, 2006):

$$N_{\text{ph}} = (n_{\text{ph}} - 1)10^6 = 287.6155 + \frac{1.628\ 87}{\lambda^2} + \frac{0.013\ 60}{\lambda^4}, \quad (5.15)$$

where λ is the carrier wave length in μm , and n_{ph} is the corresponding phase refractive index. The *group refractivity* is given by

$$N_{\text{gr}} = (n_{\text{gr}} - 1)10^6 = 287.6155 + \frac{4.886\ 60}{\lambda^2} + \frac{0.068\ 00}{\lambda^4}, \quad (5.16)$$

with the group refractive index n_{gr} .

According to (5.6) and (5.12), the refraction effect on distances and angles depends on the index of refraction and its gradient along the path of the ray, which behave differently in the troposphere than in the ionosphere.

5.1.2 Tropospheric refraction

The *troposphere* is the lower layer of the atmosphere. It extends to a height of about 9 km at the poles and 16 km at the equator. All weather processes take place in this region, where nearly 90% of the atmospheric masses are concentrated. The *tropopause* as a boundary layer separates the troposphere from the *stratosphere*, which extends to about 50 to 60 km. The troposphere, tropopause, and stratosphere are electronically neutral. The index of refraction n depends on temperature T , pressure p and humidity e . For visible light, the troposphere behaves as a dispersive medium, cf. [5.1.1]. The refractive index decreases with height and becomes nearly 1 at about 40 km. Tropospheric refraction is the combined effect from the ground to this “effective” height. Above 70 to 80 km the atmosphere is ionized, cf. [5.1.3].

The *meteorological parameters* T , p , e not only depend strongly on height but also on latitude, land/ocean distribution, topography, vegetation, and local conditions. These variables produce large- to small-scale anomalies of n . Additionally, these parameters experience variations with time which are of long-term, seasonal, daily, and turbulent character. Rapid fluctuations are especially pronounced close to the Earth’s surface, up to 10 to 30 m above the ground (e.g., Bomford, 1980; p. 49 ff.).

Temperature T decreases in the troposphere almost linearly with height h according to $dT/dh \approx -0.0055^\circ\text{C}/\text{m}$, followed by a slight increase in the stratosphere. Horizontal temperature gradients may reach a few $^\circ\text{C}/100\text{ km}$. Within the first few hundred meters above the Earth’s surface and especially close to the ground, temperature variations are pronounced, including temperature inversion during night time and convection at noon. *Air pressure* p decreases exponentially with height. Assuming hydrostatic equilibrium, the vertical pressure gradient depends on density ρ and gravity g . Near the *surface* of the Earth, this leads to $dp/dh = -\rho g = -0.034\ p/T = -0.12\ \text{hPa}/\text{m}$ at standard conditions ($T = 288\ \text{K}$, $p = 1013\ \text{hPa}$). *Humidity* is rather irregularly distributed and concentrated in a layer of a few km above ground, where strong variations also occur with time. It is measured by the water vapour pressure e , which is about 10 to 20 hPa at mid-latitudes close to the surface. It tends to decrease with height, with $de/dh \approx -0.004 \dots 0.008\ \text{hPa}/\text{m}$ at the lower layers, where we also find pronounced differences between dry and damp air regions.

Global *tropospheric models* generally assume concentric spherical layers and azimuthal symmetry and neglect variations with time. They are provided by *standard atmospheres*

in the form of vertical profiles for temperature, pressure, and density. The U.S. standard atmosphere (1976) approximates mean mid-latitude conditions for dry air, latitudinal and seasonal departures are given by supplements, NOAA (1966, 1976). Widely used is the COSPAR International Reference Atmosphere (CIRA), Rees et al. (1990).

Empirical relations have been derived between the index of refraction and the meteorological parameters for both light and microwaves (Bomford, 1980, p. 42 ff.).

With atmospheric conditions different from the standard air, cf. [5.1.1], the *group refractivity* of visible *light* and near *infrared* waves in ambient moist air is (IAG resolution, General Assembly Birmingham, 1999):

$$N_l = (n_l - 1)10^6 = \frac{273.15}{1013.25} \frac{P}{T} N_{gr} - 11.27 \frac{e}{T}, \quad (5.17a)$$

with T in Kelvin, p and e in hPa. Equation (5.17a) is also valid for unmodulated light with the corresponding phase refractivity (5.14).

The refractivity of *microwaves* (independent of the wavelength) is given by the formula of Thayer (1974)

$$N_m = (n_m - 1)10^6 = 77.60 \frac{P}{T} - 13 \frac{e}{T} + 3.78 \times 10^5 \frac{e}{T^2}, \quad (5.17b)$$

which is practically identical with the formula of Essen and Froome (IAG resolution, General Assembly Berkeley, 1963).

The first term on the right side of (5.17a,b) represents a “dry” component of the refractivity. It contributes about 90% to the total tropospheric refraction in the lower 15 km and can be modeled from surface pressure values, assuming hydrostatic equilibrium; these values may be derived from in situ measurements or from numerical weather models. The “wet” component, as expressed by the terms depending on e (especially the last one), is highly variable in space and time and extremely difficult to model, it approaches zero at around a height of 10 km. In order to keep the error in the index of refraction less than 10^{-6} , the meteorological parameters in (5.17a,b) have to be determined to about $\pm 1^\circ\text{C}$ for temperature, ± 3.5 hPa for pressure, and ± 25 hPa (light) resp. ± 0.2 hPa (microwaves) for humidity.

Refraction formulas as (5.17a,b) have been developed originally for the reduction of terrestrial measurements, carried out close to the surface of the Earth and characterized by small elevation angles. With the advent of geodetic space techniques, large elevations (up to zenith directions) had to be considered, and the signal path now passed through the complete troposphere (and the ionosphere, cf. [5.1.3]), Gruber et al. (2009), Dettmering et al. (2010). A number of corresponding *tropospheric refraction models* has been developed since the 1960s (e.g., Hopfield, 1969; Saastamoinen, 1972/1973), employing actual weather data or numerical models as input. Starting from the refraction effect on a measured *distance*, these models concentrate on the first term of (5.6), and distinguish between a “dry” and a “wet” component for the signal delay (see above). The small ray bending effect inherent in (5.6) can easily be taken into account by a “bending function”, see (5.111). As the *dry component* approximately follows hydrostatic equilibrium, it can be modeled as a function of hydrostatic pressure; this “hydrostatic” component is nearly identical for visible light and radio frequencies. As an example, the IERS conventions (Petit and Luzum, 2010, p. 135) provide the following formula (according to Saastamoinen, 1972/1973) for the *zenith hydrostatic delay* of radio waves (in meters):

$$\Delta s(\text{zenith})_{\text{hydr.}} = \frac{0.002 \cdot 277 P}{(1 - 0.002 \cdot 7 \cos 2\varphi - 0.000 \cdot 28 H)}, \quad (5.18a)$$

with p (hPa) atmospheric pressure at the observation site, φ latitude and H (km) height above the geoid. This results in a maximum effect of 2.3 m, and requires the pressure to be determined with ± 0.4 hPa for a reduction accuracy of 1 mm. The zenithal delay contribution of the *wet component* amounts to 0.07 ns for white light, and varies between 0 and 2 ns (about 10% of the dry component) for radio waves. Due to its high variability in space and time, this part is difficult to model, and generally estimated at the evaluation process. Finally, the tropospheric path delay increases strongly with decreasing elevation angles, reaching about 20 to 30 m at an elevation below 5° elevation; this dependence can be modeled by a tropospheric “*mapping function*”. A simple relation is given by $1/\cos z$ for elevation angles that are not too small. Again, the “Saastamoinen-model” offers a good approximation, where the wet component is included now (Hofmann-Wellenhof et al., 2008, p. 135):

$$\Delta s_{\text{trop}} = \frac{0.002\,277}{\cos z} \left(p + \left(\frac{1255}{T} + 0.05 \right) e - \tan^2 z \right). \quad (5.18b)$$

With z zenith angle, p (hPa) pressure, T (°K) temperature, e (hPa) partial pressure of water vapor, the result is given in meters. Improved mapping functions have been developed and are available for optical (laser ranging; Mendes and Pavlis, 2004) and for radio techniques (GPS, VLBI; Niell, 1996; Böhm et al., 2006). The refinements include the separate treatment of the dry and the wet component, and the consideration of horizontal asymmetry of the refraction field.

Differentiating (5.17a,b) with respect to the height h yields the dependence of the rays’ *curvature* on the meteorological parameters. Neglecting minor terms and taking (5.16b) into account, we obtain for the surface near layers

$$\frac{dN_l}{dh} = -78 \frac{p}{T^2} \left(0.034 + \frac{dT}{dh} \right) - \frac{11}{T} \frac{de}{dh} \quad (5.19a)$$

for *light*. For *microwaves*, the last term on the right side (“wet component”) changes to

$$+ \frac{3.7 \times 10^5}{T^2} \frac{de}{dh}. \quad (5.19b)$$

In the layers close to the ground, the strong variations of the meteorological parameters in space and time lead to corresponding changes in the *coefficient of refraction*, with pronounced seasonal and day/night variations (Höpcke, 1966). Under average daytime conditions with a clear sky, and for heights between 40 m and 100 m above the ground, we have for *light*

$$k_l = 0.13 \text{ or } r_l = 8R, \quad (5.20a)$$

and for *microwaves*

$$k_m = 0.25 \text{ or } r_m = 4R, \quad (5.20b)$$

with r_l and r_m being the curvature radii of light and microwaves, respectively, and R the mean Earth’s radius.

According to (5.11), the *coefficient of refraction* k has to be determined for light with an accuracy of 2°C in temperature, 6 hPa in air pressure, and 0.0002°C/m in the temperature gradient in order to achieve a relative accuracy of 1%. For microwaves, the admissible errors may be two times larger. The gradient of the water vapor pressure should be determined with 0.005 hPa/m for light and 0.0001 hPa/m for microwaves. Hence, the most critical parameters are the vertical gradients of temperature and, especially for microwaves, of the water vapor

pressure. According to (5.12b), an error of 1% in k would produce an error in the refraction angle of $0.2''$ over a distance of 10 km and $0.4''$ over 25 km.

The evaluation of space geodetic data (especially VLBI, GPS, DORIS) increasingly contributes to the determination of *atmospheric parameters*, and the improvement of weather models (including latitude and azimuth dependence, MacMillan and Ma, 1997) and weather forecasting (Gendt et al., 2004). The exploitation of GPS signals (carrier phase observations) is of particular importance. *Ground-based* GPS techniques are based on the path delays that the signals experience when passing through the atmosphere (Davis et al., 1996). By separating the "dry" component from the *tropospheric* signal delay, the integrated precipitable *water vapor* content above the observer's site can be estimated from the "wet" component (Bevis et al., 1992). Permanent GPS networks, cf. [5.2.5], [7.3], supply this meteorological information on global and regional scales, with high temporal resolution and nearly on-line (Poli et al., 2007; Heise et al., 2009). The water vapor content can be determined also from ground-based water vapor radiometers, and the results used for calibrating the space-derived "wet" component (Dodson et al., 1996).

Spaceborne GPS receivers allow atmospheric sounding by *radio occultation* (Yunck and Melbourne, 1996). This method became possible through the installation of GPS receivers on board Low Earth Orbiters (LEOs), as *CHAllenging Mini-satellite Payload* (CHAMP), and *Gravity Recovery And Climate Experiment* (GRACE) cf. [5.2.8], and the six satellites of the FORMOSAT-3/COSMIC mission (launched 2006), and is now used operationally by several agencies. Here, the GPS signal is tracked after rising or before setting of the GPS satellite (Fig. 5.3). In connection with a network of ground-based receivers, the observed Doppler shift induced by the relative motion between the LEO and the GPS satellite is used for constructing vertical profiles of atmospheric parameters (from the high atmosphere down to the Earth's surface) on a global scale, including refractivity, bending angles, temperature and water vapor (Wickert et al., 2010).

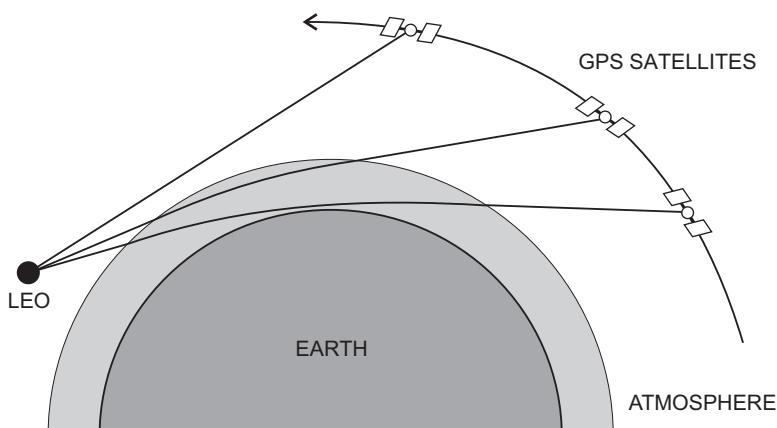


Fig. 5.3: Principle of GPS radio occultation technique.

5.1.3 Ionospheric refraction

As part of the higher atmosphere, the ionosphere is characterized by the presence of free, negatively-charged electrons and positive ions. Ionization is caused primarily by the impact of solar ultraviolet radiation and consequently depends on the density of the atmospheric gas and the intensity of the radiation. The ionosphere covers the region between about 60 km and 1500 km above the Earth, with a maximum electron density at a height of 200 to 300 km.

The ionosphere acts like a mirror at frequencies below 30 MHz. Radio waves of higher frequencies pass through the ionosphere but experience frequency-dependent effects (dispersive medium). Measurements to targets above the ionosphere are also affected by the electron concentration in the plasmasphere, which extends up to a height of several Earth radii above the equator and does not exist at the poles (Wanninger, 1995; Klobuchar, 1996).

The *index of refraction* depends primarily on the number N_e of electrons per m^3 : *electron density*. As a first order approximation, the *phase* refractive index is given by

$$n_{\text{ph}} = 1 - K \frac{N_e}{f^2}, \quad (5.21)$$

with the constant $K = 40.28 \text{ m}^3 \text{s}^{-2}$ and frequency f . Higher terms of the order $1/f^3$ and $1/f^4$ also depend on the intensity of the Earth's magnetic field and the direction of the signal propagation. In daytime, N_e (el/m^3) varies between about $10^8 \dots 10^{10}$ (heights from 60 to 90 km) over 10^{11} (105 to 160 km) to $10^{11} \dots 10^{12}$ (160 to 180 km) and 10^{12} (300 to 400 km).

As seen from (5.2) and (5.21), the phase velocity is larger than the velocity of light in vacuum, which corresponds to a larger wavelength of the signal compared to vacuum. Since signal propagation follows the group velocity, we insert (5.21) into (5.14) and obtain the group refractive index

$$n_{\text{gr}} = 1 + K \frac{N_e}{f^2}. \quad (5.22)$$

Inserting (5.21) resp. (5.22) into (5.6) delivers the difference between the electromagnetic path length \bar{s} and the straight-line connection s . This yields for carrier phase (n_{ph}) and for range (n_{gr}) observations, respectively:

$$(\bar{s} - s)_{\text{ph}} = -(\bar{s} - s)_{\text{gr}} = -\frac{K}{f^2} \int_0^s N_e \, ds, \quad (5.23)$$

where the small effect of the path's bending has been neglected. The signal delay may result in distance errors between a few meters and about 100 meters (Langley, 1998).

The integral of the electron density along the path is called *total electron content* (TEC):

$$\text{TEC} = \int_0^s N_e(s) \, ds. \quad (5.24)$$

It gives the number of electrons along the signal path between the receiver and the satellite, as measured in a cylindrical column with a cross section of 1 m^2 ; its unit is $1 \text{ TECU} = 10^{16} \text{ electrons/m}^2$. TEC values vary between 1 and 10^3 TECU along the radio wave path. For a spherically-layered ionosphere, we may introduce the electron content

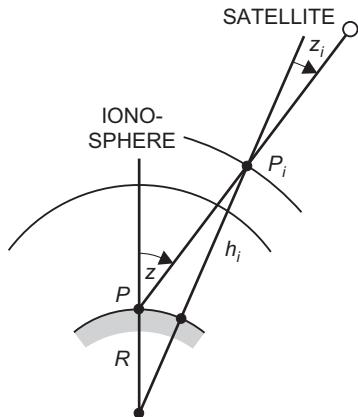


Fig. 5.4: Ionospheric refraction.

along a vertical column of height h and relate it to the TEC along the path by an oblique factor F ("mapping function"):

$$\text{TEC} = F \int_0^h N_e(h) dh. \quad (5.25)$$

For $z < 70^\circ$, we have $F \approx 1/\cos z_i$, with zenith angle z_i at the subionospheric point P_i (Fig. 5.4). P_i is located at the "mean height" h_i of the ionosphere (single-layer model), with, e.g., $h_i = 350$ km. z_i can be calculated from h_i and the zenith angle z measured from the ground:

$$\sin z_i = \frac{R}{R + h_i} \sin z, \quad (5.26)$$

R radius of the Earth.

The electron content in the ionosphere depends on the geographical location (with highest values around the Earth's magnetic equator) and varies strongly with time. There are pronounced variations of daily, seasonal, and about an 11-year (solar activity cycle) period. Superimposed on these more regular variations are irregular disturbances. Short-term scintillations occur primarily in the equatorial zones but also in the polar and auroral regions (magnetic storms). Traveling ionospheric disturbances of wavelike structure proceed with horizontal speeds between 100 and 1000 m/s at scales of some 10 to 1000 km and at periods from several minutes to a few hours. The high spatial and temporal variability of the electron content make modeling and prediction of the ionospheric state difficult.

Ionospheric models describe the distribution of N_e in space and time. They are based on the dependency of the ionospheric state on the position of the sun, and derived from satellite and rocket probes. Assuming a spherical shell distribution, they provide, among others, a smoothly varying TEC along vertical profiles and a mapping function for inclined signal propagation. Among these models are the regularly updated International Reference Ionosphere (IRI) of COSPAR and the MSIS Thermosphere Model of the Naval Research Laboratory (Hedin, 1987, 1991; Bilitza and Reinisch, 2008; Bilitza et al., 2011).

Refined models include actual data from satellites and terrestrial stations, as well as sunspot numbers (e.g., Kleusberg, 1998). These models may deviate from reality by some 10%, due to the ionospheric disturbances.

Ionospheric models are of special importance if only one frequency is used for radio signal propagation. By employing two frequencies most of the ionospheric refraction effects are eliminated, due to the dispersion effect, cf. [5.2.4], [5.2.5], [5.2.7]. Ionospheric models developed for positioning and navigation with GPS and Galileo will be discussed in [5.2.5].

As with the troposphere, the GPS (and other GNSS) signals may be exploited for *ionospheric remote sensing*, as the signal delay provides information on the structure and temporal behavior of the ionosphere. By analyzing the two carrier waves used to eliminate ionospheric refraction, cf. [5.2.5], the total electron content (TEC) along the line of sight from the receiver to the GPS satellite can be measured. The abundance of GPS ground networks (e.g., IGS) and the increasing number of space-based receivers nowadays allows to generate nearly real-time global maps of TEC (Yunck and Melbourne, 1996; Fedrizzi et al., 2001; Schmidt, 2011). The electron content of the upper ionosphere and the plasmasphere can be derived from GPS-signals received by satellite-mounted antennas directed upwards.

5.2 Satellite observations

Satellite geodesy utilizes artificial satellites and the moon as extraterrestrial targets and/or sensors. For a point-mass Earth model, the orbital motion of a satellite is described by Kepler's laws [5.2.1]. The deviations of the actual gravitational field from this model and non-gravitational forces create orbital "perturbations" [5.2.2]. Satellites used for geodetic applications differ in design, equipment, and orbital parameters according to the mission purpose and the respective observation techniques [5.2.3]. Classical measurement methods, introduced and employed from the 1960s to the 1980s, demonstrated the efficiency of satellite geodesy for establishing large-scale geodetic control networks, and for the determination of the long-wave part of the gravitational field. Some of these techniques are still employed at present-day geodetic satellite systems [5.2.4]. Today, the Global Positioning System (GPS) governs three-dimensional positioning at all scales, and further Global Navigation Satellite Systems (GNSS) have been developed or are under construction [5.2.5]. Laser distance-measurements to artificial satellites and to the moon primarily contribute to the establishment and maintenance of global reference systems, but also to the determination of Earth orientation and, with respect to lunar laser ranging, also to lunar sciences and the theory of gravitation [5.2.6]. By monitoring the ocean surface, satellite altimetry is a powerful tool for the survey of the marine gravity field and for geoid determination [5.2.7], while a high-resolution global gravity field recovery including temporal field variations has been obtained by satellite-to-satellite tracking and gravity gradiometry missions [5.2.8].

The theory of satellite orbits and satellite measurement methods are treated in textbooks and monographs on celestial mechanics (Schneider, 1992/1993/1996; Beutler, 2005), orbital theory (Montenbruck and Gill, 2000; Milani and Gronchi, 2009), and satellite geodesy, e.g., Kaula (1966), Schneider (1988), Seeber (2003).

5.2.1 Undisturbed satellite motion

After the satellite has separated from the carrier, it begins its unrestrained revolution about the Earth. We assume the gravitational point mass model (central mass), cf. [3.1.2], and neglect the mass of the satellite with respect to the Earth's mass. If we also neglect perturbations of non-gravitational type and the effect of other celestial bodies (thus restricting ourselves to a two-body problem), Newton's second law of motion provides the *equation of motion* in the gravitational field:

$$\ddot{\mathbf{r}} = \text{grad } V = -\frac{GM}{r^2} \frac{\mathbf{r}}{r}. \quad (5.27)$$

\mathbf{r} is the geocentric position vector of the satellite and $\ddot{\mathbf{r}} = d^2\mathbf{r}/dt^2$ its acceleration, M and V are the mass and the gravitational potential of the Earth, respectively, cf. (3.16). The integration of this vectorial second-order differential equation introduces six integration constants, e.g., position and velocity at a given epoch.

The fundamental theory of the two-body problem is given by celestial mechanics (e.g., Kovalevsky, 1989, for further references see the introduction to this chapter). Such works also address the fundamentals of orbit perturbations, orbit computation, and the treatment of three- and multi-body problems.

Johannes Kepler (1571–1630) derived three laws of planetary motion from the astonomic observations collected by Tycho de Brahe (1546–1601), e.g., Schneider and Müller (2009). When applied to an artificial satellite, these laws provide a geometric description of the satellite's undisturbed central motion around the Earth.

According to Kepler's laws, the satellite moves in an elliptical orbit. One focal point of the ellipse, with semi-major axis a and first numerical eccentricity e (the abbreviations should not be confused with the corresponding parameters of the Earth ellipsoid), coincides with the center of mass of the Earth. In the orbital system (Fig. 5.5), the position of the satellite is described by the distance r from the center of mass and the true anomaly v . The true anomaly is the geocentric angle between the directions to the satellite and perigee. Instead of v , the eccentric anomaly E can be used, with the relations

$$r = a(1 - e \cos E), \tan v = \frac{\sqrt{1 - e^2} \sin E}{\cos E - e}. \quad (5.28)$$

With Kepler's third law, the mean (angular) velocity

$$\bar{n} = \sqrt{\frac{GM}{a^3}} \quad (5.29)$$

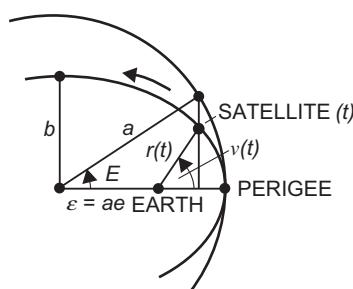


Fig. 5.5: Satellite orbital system.

is introduced, describing a mean orbital motion. The mean anomaly

$$\bar{M} = \bar{n}(t - T) \quad (5.30)$$

represents yet another parameter for describing the satellite's position in the orbit. It is generally preferred because it increases *linearly* with time t . T is the epoch of the passage through the perigee, the closest approach to the Earth. From \bar{M} , E can be computed iteratively using Kepler's equation:

$$\bar{M} = E - e \sin E. \quad (5.31)$$

The orbital system is transformed into the space-fixed equatorial system, cf. [2.3.1], by three rotations (Fig. 5.6). The right ascension of the ascending node Ω and the inclination i provide the orientation of the orbital plane in space. The argument of perigee ω orients the ellipse in the orbital plane. From the result of this transformation, we obtain the geocentric position vector (2.10) as a function of the six Keplerian elements a , e , Ω , i , ω , and ν (or equivalently E , \bar{M} , or T):

$$\mathbf{r} = r \begin{pmatrix} \cos \delta \cos \alpha \\ \cos \delta \sin \alpha \\ \sin \delta \end{pmatrix} = r \begin{pmatrix} \cos(\omega + \nu) \cos \Omega - \sin(\omega + \nu) \sin \Omega \cos i \\ \cos(\omega + \nu) \sin \Omega + \sin(\omega + \nu) \cos \Omega \cos i \\ \sin(\omega + \nu) \sin i \end{pmatrix}, \quad (5.32a)$$

with

$$r = \frac{a(1 - e^2)}{1 + e \cos \nu}. \quad (5.32b)$$

The six Keplerian parameters completely describe the orbital motion of the undisturbed satellite. They correspond to the integration constants of the equation of motion (5.27) and are used for the approximation of satellite orbits.

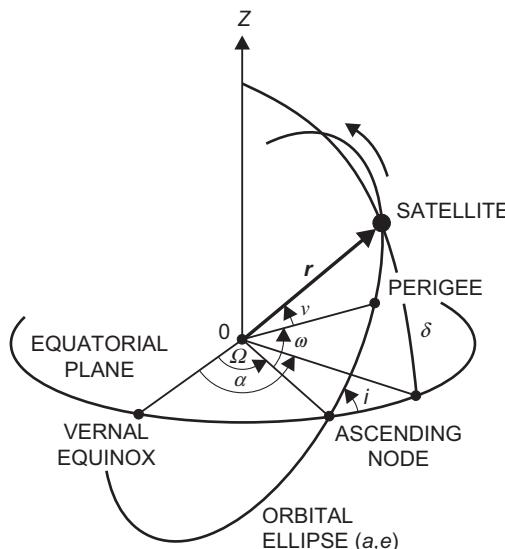


Fig. 5.6: Orbital and equatorial system.

5.2.2 Perturbed satellite motion

The actual orbit of a satellite departs from the Keplerian orbit due to the effects of various "disturbing" forces. This includes the non-spherical parts of the Earth's gravitation, the gravitational effects of moon and sun, atmospheric air drag, and solar radiation pressure, among others. These disturbing forces cause variations in time in the orbital elements (orbital perturbations) of secular, long- and short-periodic nature. The actual orbit can be viewed as the envelope of Keplerian ellipses, which are given at each instant by the actual orbital elements (osculating ellipses).

In order to account for the complete *gravitation* of the Earth, the gravitational potential of a spherically symmetric Earth must be amended by the *perturbing potential* R (not to be confused with the *disturbing potential* introduced in [6.1.1]):

$$V = \frac{GM}{r} + R. \quad (5.33)$$

According to equations (3.89) to (3.91), R can be expressed by a spherical harmonic expansion of the gravitational potential V through the harmonic coefficients J_{lm} , K_{lm} ($l \geq 2$). By substituting (5.33) into (5.27), the *equation of motion* now reads

$$\ddot{\mathbf{r}} = -\frac{GM}{r^2} \frac{\mathbf{r}}{r} + \text{grad } R. \quad (5.34a)$$

The spherical coordinates r , ϑ , λ (2.13) used in the expansion of V can be replaced by the orbital elements according to (5.28) and (5.32), see also Fig. 5.5. R then is described by the time-variable Keplerian orbital parameters and the harmonic coefficients:

$$R = R(a, e, \Omega, i, \omega, \bar{M}, J_{lm}, K_{lm}). \quad (5.34b)$$

The second-order differential equation (5.34) can be transformed into a system of first-order differential equations. They represent the time rates of the orbital parameters as a function of partial derivatives of the perturbing potential (i.e., of the harmonic coefficients) with respect to them. These first-order differential equations are known as Lagrange's perturbation equations (Kaula, 1966, p. 29; Seeber, 2003, p. 85 ff.):

$$\left. \begin{aligned} \frac{da}{dt} &= \frac{2}{na} \frac{\partial R}{\partial \bar{M}} \\ \frac{de}{dt} &= \frac{1-e^2}{na^2 e} \frac{\partial R}{\partial \bar{M}} - \frac{\sqrt{1-e^2}}{na^2 e} \frac{\partial R}{\partial \omega} \\ \frac{d\omega}{dt} &= -\frac{\cos i}{na^2 \sqrt{1-e^2} \sin i} \frac{\partial R}{\partial i} + \frac{\sqrt{1-e^2}}{na^2 e} \frac{\partial R}{\partial e} \\ \frac{di}{dt} &= \frac{\cos i}{na^2 \sqrt{1-e^2} \sin i} \frac{\partial R}{\partial \omega} - \frac{1}{na^2 \sqrt{1-e^2} \sin i} \frac{\partial R}{\partial \Omega} \\ \frac{d\Omega}{dt} &= \frac{1}{na^2 e \sqrt{1-e^2} \sin i} \frac{\partial R}{\partial i} \\ \frac{d\bar{M}}{dt} &= n - \frac{1-e^2}{na^2 e} \frac{\partial R}{\partial e} - \frac{2}{na} \frac{\partial R}{\partial a} \end{aligned} \right\}. \quad (5.35)$$

The influence of the *gravitation of moon and sun* on a satellite can be calculated by corresponding extension of (5.27), which leads to the equation of motion for a

four-body problem. As a result, a satellite orbit experiences secular and long-periodic perturbations, which may reach 100 m and more. In addition, *solid Earth* and *ocean tides*, cf. [8.3.6], especially affect low-orbiting satellites. Corresponding corrections are based on the ephemeris of the moon and sun and on Earth and ocean tide models.

Air drag is caused by friction of the satellite with atmospheric particles. It is proportional to the velocity of the satellite and depends on atmospheric density and the effective cross-sectional area to mass ratio. With increasing altitude, the air drag decreases rapidly and approaches zero at about 1000 km. Air drag effects are corrected using high-altitude atmospheric models such as the COSPAR International Reference Atmosphere, or from on-board accelerometer measurements, cf. [5.1.2], [5.2.8].

High-altitude satellites are especially affected by *solar radiation pressure* due to incident photons. The resulting perturbations depend on the solar flux and the attitude of the satellite with respect to the sun, the area to mass ratio, and the reflectivity. The Earth-reflected solar radiation pressure (albedo) remains significantly smaller than the direct effect. Modeling of the radiation pressure effects is difficult, especially for satellites of complex structure. *Electromagnetic interactions* with the magnetic field of the Earth occur in the ionosphere; however, they are small and can be considered by corrections. At the now reached level of accuracy, *relativistic effects* also have to be taken into account (Ries et al., 1991).

Orbit determinations are based on analytical or numerical methods (Boccaletti and Pucacco, 1996/1999; Milani and Gronchi, 2009). For *analytical solutions*, all acting forces are expressed by rigorous relations and integrated in closed form. A first order approximation is already provided by the solution of (5.35). The position vector at any epoch t is given by the orbital elements at an initial epoch t_0 , the parameters of the gravitational field, and other models of disturbing forces:

$$\mathbf{r} = \mathbf{r}(a_0, e_0, \Omega_0, i_0, \omega_0, \bar{M}_0; GM, J_{lm}, K_{lm}; \dots; t). \quad (5.36)$$

For *numerical methods*, all forces are calculated for a particular position of the satellite and used as a starting condition for a stepwise integration of the equation of motion (5.34a). Classical astronomic methods for orbit determination are used, as developed by *Cowell* (integration of the total force) or *Encke* (integration of the difference to an osculating Kepler ellipse). The numerical integration itself is carried out with conventional methods, fitting a polynomial to a series of consecutive points. The *Runge-Kutta method* as a single-step solution uses a Taylor series for extrapolation, while multi-step methods iteratively improve the prediction results, e.g., through Kalman filter techniques (Montenbruck and Gill, 2000).

The analytical method is rather laborious, and difficulties arise at applying it to non-gravitational forces. It is well suited for estimating the effects of perturbing forces on the satellite's orbit and for the planning of satellite missions and projects. Numerical methods are simple and generally applicable. They are used nearly exclusively today. The arc lengths for orbit modeling (parameter estimation by adjustment) vary from a few days at low orbiting satellites to some weeks at high flying satellites.

Orbit determination is now also *directly* possible by spaceborne packages of satellite navigation and positioning systems as GPS or DORIS (Yunck and Melbourne, 1996), this strategy is applied especially at low Earth orbiters, where modeling of perturbations is difficult. In contrast to the dynamic approach explained above this kinematic orbit

determination does not require any information on the acting forces (gravitation, air drag, solar radiation etc.).

Precise orbit determinations are especially important for positioning and satellite altimetry, but also for satellite gravity missions. With good satellite tracking (within the frame of dedicated networks), and (for the dynamic orbit determination) using precise models of both the gravitational field and the non-gravitational forces, the ephemeris of geodetic relevant satellites can be determined by orbital post-processing with cm-accuracy. By applying adequate models for the perturbing forces, orbit *predictions* can be carried out and extended from several revolutions of the satellite to days and months, with prediction accuracies varying from some centimeters to some meters. Predicted orbits for individual satellites are published by the responsible agencies, while navigation satellites also transmit their own orbital data, cf. [5.2.4], [5.2.5].

An orbital accuracy of better than one mm can be achieved for high-altitude satellites used for positioning, by truncated versions of existing gravitational field models. For the EGM2008 model, cf. [6.6.3], suggested truncation levels are at degree and order 90 for Starlette (orbital radius about 7300 km), 20 for Lageos (12300 km), and 12 for GPS (26600 km), Petit and Luzum (2010).

5.2.3 Artificial Earth satellites

Since the launch of Sputnik I (1957), artificial Earth satellites have been used for geodetic purposes such as positioning and the determination of the Earth's gravity field and rotation parameters. Only a limited number of satellite missions have been designed exclusively for geodetic applications. However, a large number of satellites developed for navigation, remote sensing, and geophysics were and are used extensively also in geodesy.

A satellite can be regarded as a moving *target* at high altitude and then used for positioning. Because the satellite's orbit is affected by the gravitational field of the Earth, the satellite may also serve as a *sensor* for gravitation. Time series of satellite observations finally allow to monitor the time-variable Earth orientation. Satellites may reflect incident light only (passive satellites), or they may carry subsystems on board such as transmitters/receivers, different type sensors, clocks, and computers (active satellites). In the latter case, an energy supply is required, and lifetime is rather limited. Passive satellites have played and play an important role in geodesy, but active satellite missions nowadays support the majority of geodetic applications.

The mean *orbital velocity* of a satellite moving in an approximately circular orbit ($r = a$) is given from (5.29) by

$$\bar{v} = a\bar{n} = \left(\frac{GM}{r} \right)^{1/2}. \quad (5.37)$$

For a satellite close to the Earth ($h = 800$ km), we obtain, with $r = R + h = 7170$ km, a velocity of 7.5 km/s. Kepler's third law yields the period of revolution $U = 2\pi r/\bar{v} = 101$ min. For a high-orbiting satellite ($h = 20\,000$ km) we have 3.9 km/s for velocity and 12 h for the period of revolution. The intersection of the orbital plane with a non-rotating Earth represents a great circle on the Earth's surface: *subsatellite track*. The rotation of

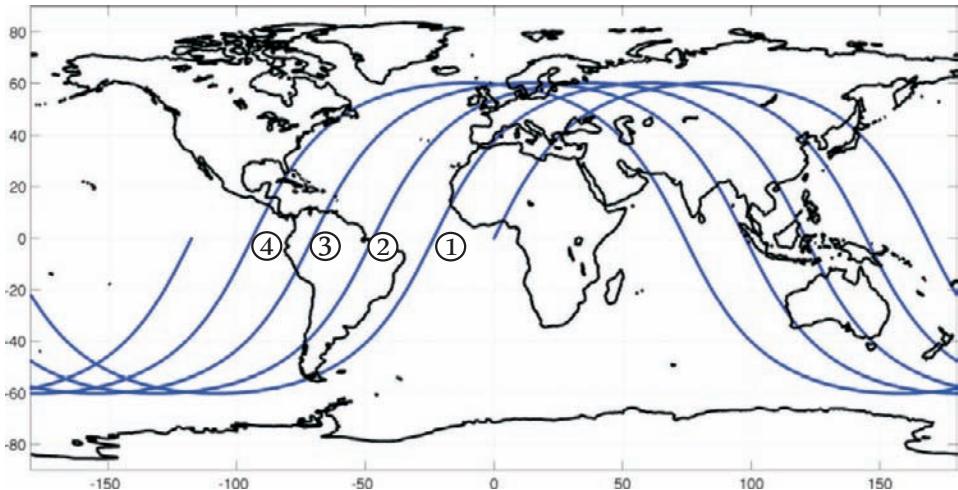


Fig. 5.7: Subsatellite tracks (inclination 60°).

the Earth causes a western displacement of subsequent satellite orbits (Fig. 5.7), with a shift on the equator given by

$$\Delta\lambda = 360^\circ \frac{U}{\text{sidereal day}} = 15^\circ U[h] = 0.25^\circ U[\text{min}]. \quad (5.38)$$

The latitude range of the subsatellite tracks is determined by the inclination of the satellite.

The following aspects have to be considered during the *design* (choice of orbital parameters) of *satellite missions* for geodetic applications:

For *positioning* and determination of Earth rotation, the network geometry of the ground stations and the satellites plays a primary role. Simultaneous direction measurements from two ground stations to a satellite form a plane, and the intersection of planes provides relative positions within a geometric network (satellite triangulation). Range measurements utilize the intersection of spheres (satellite trilateration), whereas range differences, derived from Doppler-frequency shifts, use the intersection of hyperboloids. If the satellite's orbit is known with high accuracy, the absolute position of the ground stations can be derived from these relative measurements. Satellites at high altitudes are preferred for positioning and navigation, as they are less influenced by gravitational and air drag perturbations.

Exact simultaneous measurements of directions or distances were performed from the 1960s to the 1970s, and led to purely geometric satellite networks, without precise knowledge of the satellite orbits. When simultaneousness could be achieved only approximately, a short-arc orbital fitting served for interpolation and improvement of the results, cf. [5.2.4].

The orbital analysis of satellites has been early used for the determination of the Earth's *gravitational field*. As high-orbiting satellites only sense the long-wave parts of the gravity field, low altitude satellites are required for determining the gravitational field at a higher spatial resolution. This is mainly due to the attenuation factor $(a_e/\eta)^l$ in the spherical harmonic expansion of the gravitational potential (semimajor axis of

the Earth ellipsoid a_e), cf. [3.3.2], [6.7.3]. Consequently, the relative errors of the harmonic coefficients increase rapidly at higher degrees l . For $l = 20$, the amplitude of the corresponding structure of wavelength 2000 km is only 5% at a satellite altitude of 1000 km, as compared to the Earth's surface. This attenuation is increased by the fact that the harmonic coefficients become smaller with increasing degree and order, cf. [6.6.2]. In order to resolve the gravitational field from an orbital analysis with a certain degree l at the equator, it follows from (5.38) that the satellite has to perform $2l$ revolutions/day, or a longer observation time is required. As seen from (5.35), the recovery of the harmonic coefficients also strongly depends on the satellite's inclination. Corresponding satellite coverage is needed in order to avoid ill conditioning; too small inclinations and eccentricities should be avoided. An improved resolution of the gravitational field has been achieved by range and range-rate measurements between satellites (low- and high-orbiting) and ground stations, while an even higher resolution can be obtained by gravity gradiometers carried on board low-orbiting satellites. Satellite altimetry finally delivers the distance between the satellite and the ocean surface, and thus a high-resolution approximation to the geoid, cf. [3.4.2]. Dedicated gravity field and satellite altimetry missions require a precise orbit determination and an orientation with respect to the vertical.

Non-gravitational perturbing effects on the satellite can be reduced by a small cross-sectional surface and large mass; a spherical shape offers special advantages. Atmospheric drag and solar radiation pressure may also be compensated by a drag-free system. In such a system, a proof mass is shielded by a shell attached to the satellite. The mass is affected only by gravitation, while surface forces act in addition on the shell. By continuously measuring the position changes between proof mass and shell, a feedback system keeps the satellite centered on the proof mass. In order to detect *variations with time*, in position (station velocities) of observation sites and in the gravitational field, adequate temporal observations series have to be carried out, preferably by the same satellite system.

Satellites used in geodesy may be equipped with the following techniques, of which combinations are used in many missions:

- *Direction* measurements have been made available by a sun-light reflecting skin (early balloon satellites), by flashing light devices, and by mirror arrays, cf. [5.2.4],
- transmitters/receivers serve for the continuous emission/reception of modulated radio waves which are used for *range* and *range rate* (Doppler) measurements between the ground station and the satellite or between satellites, cf. [5.2.4], [5.2.5], [5.2.8],
- retroreflector arrays of fused silica corner cubes reflect laser light pulses and are employed for *laser distance* measurements, cf. [5.2.6],
- vertical distance measurements to the ocean surface are performed by *radar altimeters*, cf. [5.2.7],
- gravity *gradiometers* measure gravitational gradients within the body of the satellite, cf. [5.2.8].

High demands are placed on the determination of *time*. At orbital velocities of several km/s, the time epoch has to be determined to $\pm 1 \mu\text{s}$ in order to keep orbital errors less than 1 cm. Distance measurements to satellites require time interval measurements

to ± 0.1 ns in order to obtain cm-accuracy. Rubidium or cesium frequency standards, which are tied to UTC by time signals, are capable of reaching this level of accuracy. Quartz oscillators can be used in satellite receivers if an external control is provided, e.g., through the satellite system, cf. [5.2.5].

More details on satellites employed in geodesy are given in the following chapters.

5.2.4 Direction, range and range rate (Doppler, DORIS) measurements

Satellite observations began in 1957. They were based partly on methods developed for the observation of the moon and of high-flying balloons. While some of the classical techniques applied up to the 1980s are no longer of importance, other methods have been developed further and are used extensively today. Some results of the early satellite missions are still of relevance for the strengthening and orientation of geodetic networks and for the calculation of Earth models (e.g., Seeger, 2003, p. 158 ff.).

Direction measurements to satellites prevailed until about 1970 and led for the first time to global and regional three-dimensional networks. Orbital analysis also provided the low-degree harmonic coefficients of the gravitational potential development.

For optical direction measurements, an illuminated satellite is photographed on film or glass plates together with the fixed stars.

Balloon satellites reflecting sunlight (e.g., Pageos, 1966–1972, diameter of 30 m, $i = 87^\circ$, $h = 2800$ to 5600 km) and light flashes from active satellites were used. Ballistic cameras (e.g., Wild BC4) mounted azimuthally were easy to operate and had a large field of view. Equatorially-mounted astronomic cameras could follow the motion of the stars. Using a large focal length, even faint stars could thus be detected and observed with high precision. Orbital cameras were designed so that they could also follow the motion of a satellite. Upon developing the photographs and identifying the stars, the satellite and star image points were measured on a precision comparator ($\pm 1 \mu\text{m}$). The plate coordinates of the satellite were then transformed to the spatial directions right ascension and declination, whereby the transformation parameters were derived from the known directions to the stars, cf. [2.4.1]. Since the satellite travels in the atmosphere, astronomic refraction reduction as applied to the stars, cf. [5.3.3], had to be reduced by the satellite refraction (Fig. 5.43), with

$$\Delta z_{\text{sat}} = 0.48'' \frac{\tan z}{h [1000 \text{ km}]} \quad (5.39)$$

The accuracy of the direction measurements was $0.2''$ to $2''$. An increase in accuracy was not possible mainly due to scintillation effects and comparator measuring errors. An outstanding example of a geometric satellite network established by stellar triangulation is the global net (45 stations) of the U.S. National Geodetic Survey (1966–1970). It was constructed by direction measurements with Wild BC4 cameras to the Pageos satellite, and the scale was derived from long traverses measured with electronic distance meters; an accuracy of 4 to 5 m was achieved (Schmid, 1974).

The Japanese satellite EGS (Experimental Geodetic Satellite), also *Ajisai* ($h = 1500$ km, $i = 50^\circ$, nearly circular orbit) is a more recent example of direction measurements. The spherical-shaped (diameter 2.14 m) satellite was launched in 1986. Its surface is equipped with both mirror and laser reflector assemblies. By rotation of the satellite about its axis, incident sunlight is reflected periodically with two flashes per second. The satellite has been used for laser range and for photographic direction measurements, in order to improve the Japanese horizontal control network and to

connect remote islands. Precise orbit determination is also exploited for gravity field improvement.

Microwave distance-measurements started in the 1960s and still play a fundamental role today.

The *Secor* (Sequential Collation of Range) system used modulated microwaves (two frequencies) emitted from ground stations and re-transmitted from transponders on board the satellites. Distances were derived from signal's travel time, using the phase comparison method, cf. [5.5.2]. Using this method and employing spatial *trilateration*, isolated geodetic networks were connected to a global reference system. The precision obtained was a few m, although systematic errors up to several 10 m also occurred.

Starting in the 1970s, *Doppler positioning* (named after the Austrian *Christian Doppler*, 1803–1853) soon became an efficient tool for establishing 3D-networks, or for improving classical geodetic horizontal control. By orbital analysis, it also delivered improved geopotential models and Earth rotation parameters (Seeger, 2003, p. 181 ff.).

With Doppler measurements, a transmitter on-board a satellite S continuously emits a stable frequency f_s (Fig. 5.8). A signal is received at the ground station (distance s to the satellite) with the frequency f_g and a time shift Δt with respect to the transmission time t . f_g is shifted against f_s due to the relative velocity $\dot{s} = ds/dt$ between the satellite and the observer (Doppler effect). Neglecting higher order terms, the Doppler frequency shift for satellites with velocities much smaller than c is given by

$$f_g - f_s = -\frac{\dot{s}}{c} \dot{s}. \quad (5.40)$$

The Doppler shift is proportional to \dot{s} ; a reversal in sign occurs at the time of the closest approach of the satellite to the observer ($\dot{s} = 0$). In principle, a range difference (range rate) can be determined from (5.40) by integration over time. In practice, f_g is compared with a stable reference frequency f_0 generated within the Doppler receiver, with $f_0 \approx f_s$. Integration over a time interval yields the Doppler count

$$N_{ij} = \int_{t_i + \Delta t_i}^{t_j + \Delta t_j} (f_0 - f_g) dt. \quad (5.41)$$

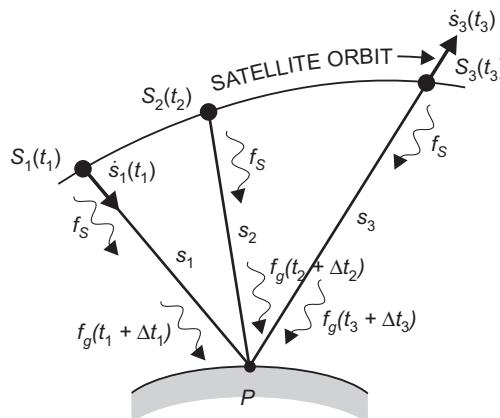


Fig. 5.8: Satellite Doppler positioning.

With (5.40), we obtain the observation equation

$$N_{ij} = (f_0 - f_s)(t_j - t_i) + \frac{f_0}{c}(s_j - s_i), \quad (5.42)$$

which provides the range rate $s_j - s_i$ from the Doppler counts.

As with any microwave technique, Doppler measurements do not depend on weather conditions, and they allow large amounts of data to be accumulated within short time intervals. Today, Doppler measurements are used with several satellite missions and with the DORIS positioning system, see below. Range rate measurements also represent the basic technique for satellite-to-satellite tracking, which is employed for high-resolution gravity field determination, cf. [5.2.8].

The *Navy Navigation Satellite System* (NNSS) or *Transit System* was an important application of Doppler measurements (Anderle, 1986). Developed as a navigation system for the U.S. Navy, it was opened to civil use early on and operated successfully between 1964 and 1996. Positioning was based on four to seven Transit satellites in orbit ($h \approx 1100$ km, $i \approx 90^\circ$), which continuously transmitted frequencies of 150 and 400 MHz. With the orbital planes of the satellites evenly distributed in longitude, and due to Earth rotation, a satellite became visible at least every two hours along the equator. The satellite orbits were determined by Doppler measurements from four tracking stations located in the U.S.A. Initially they referred to the World Geodetic System 1972 (WGS72) and later to WGS84, cf. [5.2.5]. The satellites transmitted their "broadcast ephemeris" at two-minute intervals, together with UTC time signals, with an accuracy of 10 to 20 m. "Precise ephemeris" (± 1 to 2 m) were later made available to authorized users. A number of portable Doppler navigation receivers were commercially produced for geodetic purposes. These contained a reference oscillator, a microprocessor, a data-recording unit, the antenna, and an energy supply. The influence of ionospheric refraction was practically eliminated by the use of two frequencies, cf. [5.1.3], and tropospheric refraction was computed using atmospheric models and observed meteorological data, cf. [5.1.2]. A positional error of 10 to 30 m was obtained at the observation of a single satellite pass. This error could be reduced to 2 to 5 m (broadcast ephemeris) with 30 to 50 passes and to 5 to 1 m using precise ephemeris, the latter being derived from a network of about 20 globally distributed stations. Relative positioning employed simultaneous observations on two or more stations, which strongly reduced orbital and refraction errors and led to baseline accuracies of 0.2 to 0.5 m (Seeber et al., 1982). With GPS becoming operational, the NNSS was no longer maintained.

Another successful application of the Doppler method started in the 1990s with the French DORIS (*Doppler Orbitography and Radio Positioning Integrated by Satellite*) system (Fagard, 2006). In contrast to the Transit system, the radio signals (2.03 and 0.40 GHz) are emitted here continuously by ground beacons, and received and processed as Doppler frequency shifts (integration, e.g., over 10 s) onboard of satellites which also carry an ultra-stable crystal oscillator for time-tagging. The system was originally developed by the French Space Agency CNES, in cooperation with the Institut Géographique National and the Groupe de Recherches de Géodésique Spatiale, in order to support precise orbit determination for altimeter and remote sensing missions. DORIS receivers are flown on a number of satellites, including the altimeter satellites Topex/Poseidon, Jason-2 and Envisat, and remote sensing SPOT satellites (DORIS, 2006).

Meanwhile, a *global network* of 50 to 60 permanently emitting DORIS ground stations has been built up, containing dual-frequency receiver, oscillator, microprocessor, power



Fig. 5.9: DORIS antenna (standard layout 2 m tower), from Fagard (2006).

supply and antenna. The stations are well monumented, for example by concrete pillars or rigid towers (Fig. 5.9), and through co-location well tied to other IERS techniques and to tide gauges. They are evenly distributed around the globe, including oceanic areas (Fig. 5.10), which is an advantage when compared with global networks based on other space techniques. The precise orbit determination also allows the calculation of the

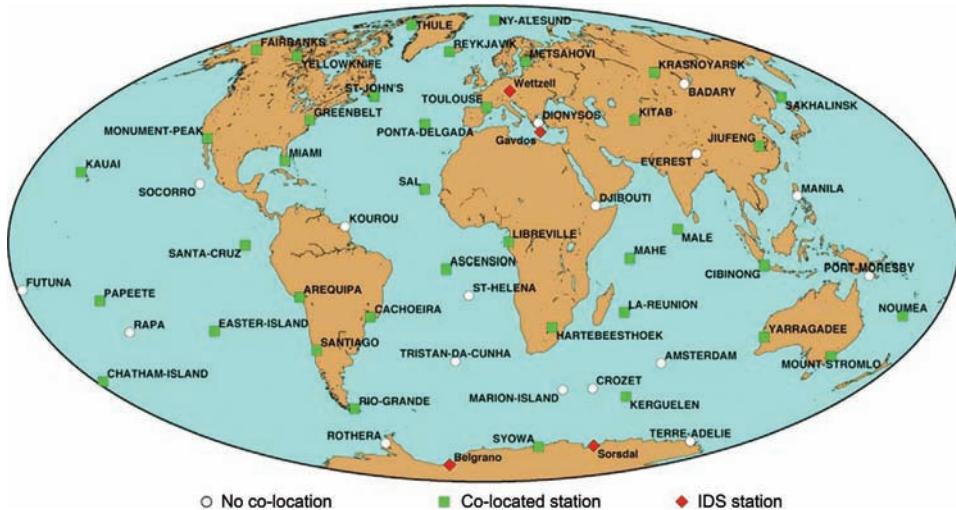


Fig. 5.10: Stations of the DORIS network (status 2006), Tavernier et al. (2006).

coordinates and the velocities of the DORIS global network ground stations, as well as the positioning of dedicated location beacons. Precise orbit determination is now possible with cm-accuracy in post-processing, and the *International DORIS Service* (IDS) of IAG provides coordinates and velocities of the tracking stations with an accuracy of better than 1 cm resp. 2 mm/year, and also UT1 time rates, polar motion and polar motion rates as well as geocenter and scale information of the International Terrestrial Reference Frame (Tavernier et al., 2006).

We finally mention that range rate measurements represent the basic technique for *satellite-to-satellite tracking*, which is employed for high-resolution gravity field determination, cf. [5.2.8].

5.2.5 Global Navigation Satellite Systems GNSS (GPS, GLONASS, Galileo and others)

Global navigation satellite systems have been built up since the 1960s, for world-wide navigation and positioning. Using radio waves as carriers of signals, these systems utilize observed signal travel times in order to derive distances between satellites and ground-based receivers. With the satellites' orbits and time being known, the positions (coordinates) of the terrestrial stations then can be computed within a well-defined terrestrial reference system. Main driver for the development and establishment of these systems came (and to a large part still comes) from military agencies, but the benefit for civilian use was early recognized and proved to become a strong impetus for further development and improvement of the systems.

While ground-based radio navigation systems of regional and global range like DECCA, LORAN and Omega became in use since the 1940s, the U.S. TRANSIT Navy Navigation Satellite System based on Doppler-measurements was the first *satellite-based* system, and was available for civilian users since the 1960s, cf. [5.2.4]. The development of satellite navigation systems using one-way microwave distance measurement between satellites and ground stations started in the 1970s, with the U.S. GPS and the Russian GLONASS systems, both being fully operational now. The European Galileo- and the Chinese COMPASS-system are built up since a couple of years, and will in future enable the joint use of several global satellite navigation systems, with eventual augmentation by regional systems as developed, e.g., in Japan and India. In the following, we concentrate on the description of GPS being the most efficient navigation and positioning system since the 1990s, with widespread application reaching far beyond classical geodetic problems, but also regard the other systems mentioned above.

The NAVSTAR (Navigation System with Time and Range) *Global Positioning System* GPS was the first spaceborne radio navigation system based on timing and ranging, which became operational worldwide. It is under the responsibility of the U.S. Department of Defense (DOD), which started development of the system in 1973. The first GPS satellites were launched in 1978, and the system became fully operational in 1993. GPS provides real time navigation and positioning by one-way microwave distance measurements between the satellites and the GPS receivers. The system was developed and is maintained in order to satisfy the requirements of the U.S. military forces, but early on its use for geodetic applications was investigated (Bossler et al., 1980). Since the 1990s, the U.S. GPS policy strongly encouraged the civilian use of the system, and today GPS positioning is extensively employed in geodesy (and in a multitude of other

geo-referenced applications) at all spatial scales, and also for kinematic positioning and the determination of crustal movements (Evans et al., 2002; Blewitt, 2009).

A large number of textbooks and monographs on GPS (and other global navigation systems) are available. Among the textbooks we have Teunissen and Kleusberg (1998a), Leick (2004), Misra and Enge (2006) and Hofmann-Wellenhof et al. (2008), see also Seeber (2003). A standard reference is given by Parkinson and Spilker (1996), while Kaplan and Hegarty (2006) "provide the reader with a systems engineering treatment", and Xu (2007) concentrates on theory and algorithms. New developments and results are given, among others, in the proceedings of the meetings of the Satellite Division/Institute of Navigation (ION), and in the journals "Navigation", "GPS World" and "GPS Solutions".

The *basic idea* of GPS is to have at least four satellites above the horizon available 24 h everywhere on the Earth. In principle, the position of the receiver's antenna could be derived already from three observed distances, with the computation of three-dimensional coordinates being based on the known ephemerides of the satellites and the intersection of spherical shells. As the clocks of the satellite and the receiver are not synchronized, a fourth distance measurement is necessary in order to determine the clock synchronization error. Therefore, the original distances derived from the travel time of a signal are called *pseudoranges* (Fig. 5.11).

We distinguish between the space, the control, and the user segment of GPS.

The *space segment* consists of 21 active *satellites* (plus three additional spares) arranged in six nearly circular orbits ($i = 55^\circ$, 12 h period of revolution) at an altitude of about 20 200 km (Fig. 5.12, Fig. 5.13). The full satellite constellation provides a global 24-h coverage with four to eight satellites visible above 15° elevation. Due to the limited lifetime of a satellite (10 years on average), some additional active spare satellites are usually in space. In addition, a regular replacement in blocks is taking place which results in a regular constellation of more than 30 satellites. This updating also takes improvements in satellite technology and refined mission strategies into account, as the inclusion of laser retroreflectors for orbit determination (block IIA satellites since 1990), the possibility of distance measurements between satellites (cross links), the on-board computation of ephemeris, and the introduction of new carrier frequencies and ranging codes for military and civilian services.

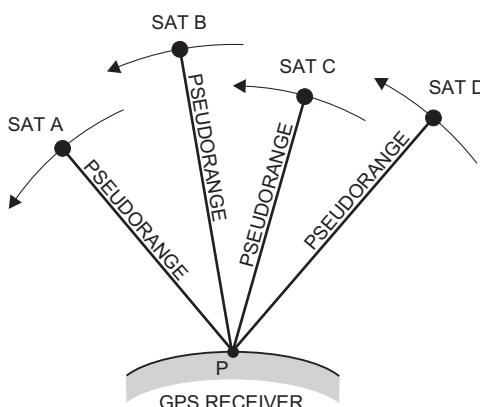


Fig. 5.11: GPS positioning (principle).



Fig. 5.12: GPS IIR-M (Global Positioning System) satellite, from <http://www.gps.gov>.

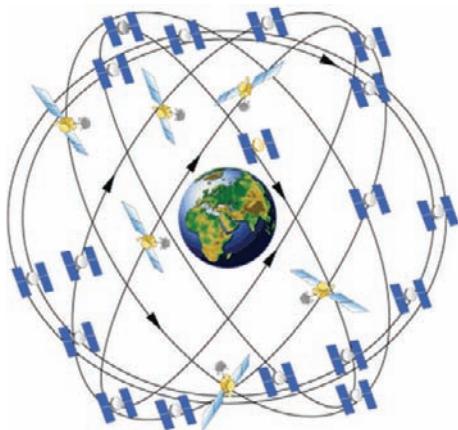


Fig. 5.13: GPS orbit constellation, from <http://www.gps.gov>.

Atomic clocks (two rubidium and two cesium clocks per satellite) provide a high-precision frequency standard, with a few 10^{-13} to 10^{-14} frequency stability over 1 day, and the future hydrogen masers will even reach a stability of 10^{-14} to 10^{-15} , cf. [2.2.1]. These clocks produce the fundamental frequency of 10.23 MHz. By multiplication, the L1 (1575.42 MHz corresponding to 19.0 cm wavelength) and the L2 (1227.60 MHz corresponding to 24.4 cm) *carrier frequencies* have been initially derived and continuously emitted. L1 and L2 serve as carriers for two code modulations and for a data signal (navigation message). The codes are given as binary signals (+1 and -1 sequence) in a pseudo-random noise (PRN) form (Fig. 5.14). The *C/A-code* (coarse/acquisition code) is modulated on L1 only, with a frequency of 1.023 MHz (corresponding to 293 m wavelength) and a repetition rate of 1 ms. The *P-code* (precise code, now available only as encrypted Y-code, see below) is modulated on L1 and L2 and has a frequency of 10.23 MHz (corresponding to 29.3 m wavelength) and a repetition sequence of 266 days. Within the frame of modernization of GPS, the block IIR-M satellites (since 2005) carry a further freely accessible code on L2, and a third

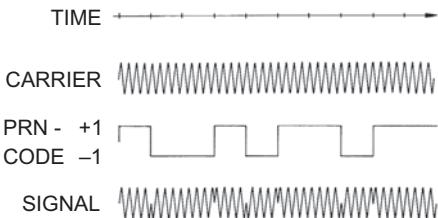


Fig. 5.14: GPS signals (principle).

carrier frequency L5 (1176.45 MHz corresponding to 25.5 cm) is introduced with the block IIF satellites (since 2009).

The GPS *control segment* is responsible for maintaining the operation of the GPS satellites, the determination of GPS time, and the calculation and storage of the navigation data. It consists of the master control station (Schriever AFB, Colorado Springs, Colorado) and a number of globally distributed monitoring stations (originally five stations, with additional 11 stations at the GPS modernization in 2005/2006). The stations are equipped with cesium standards and GPS receivers. They continuously measure pseudoranges to all GPS-satellites in view and transfer the results to the master station. After computation of the satellite orbits and the clock corrections, the (extrapolated) broadcast ephemeris and GPS time are transmitted to the satellites for storage and retransmission by four dedicated ground antennas co-located with monitoring stations. This operational control system is supplemented by the monitor station network of the National Geospatial-Intelligence Agency (NGA), resulting in an accuracy increase of satellite orbits and clock information.

The GPS ephemerides refer to an Earth-fixed system, realized by the coordinates of the monitoring stations: *World Geodetic System* (WGS). WGS has been used by the U.S. Department of Defense since the end of the 1950s, and it has been first realized through the versions WGS60, WGS72 and WGS84 (DMA, 1987). The system was originally derived from Doppler observations from the Transit satellite system, cf. [5.2.4], while the refined versions (since the 1990s) of WGS84 are based on GPS. Defined by NGA, the system is now upgraded at shorter intervals, under the name of WGS84 (Gxxx), where xxx (e.g., 1400) indicates the GPS week number of implementation. The system is intended to serve for mapping, charting, positioning and navigation, following international standards for geodetic reference systems. The defining parameters of the WGS84-ellipsoid (tide-free system) are as follows (Slater and Malys, 1998; NIMA, 2000):

- semi-major axis $a = 6\ 378\ 137\text{ m}$,
- reciprocal flattening $1/f = 298.257\ 223\ 563$,
- geocentric gravitational constant $GM = 398\ 600.4418 \times 10^9\text{ m}^3\text{s}^{-2}$, which includes the atmospheric part $GM_{\text{atm}} = 0.35 \times 10^9\text{ m}^3\text{s}^{-2}$,
- angular velocity of the Earth's rotation $\omega = 7.292\ 115 \times 10^{-5}\text{ rad s}^{-1}$.

The WGS84-ellipsoid thus practically coincides with the parameters of the Geodetic Reference System 1980, cf. [4.3]. The associated gravity field is given by the global geopotential model EGM96 resp. EGM2008, cf. [6.6.3]. The coordinates of the monitoring stations are given for the epoch 1997.0, taking Earth tides (tide-free system), cf. [3.4.1], and plate tectonic motions into account. The accuracy of the recent WGS84 (G1400)-coordinates is at

the cm-order of magnitude, which is also the level of agreement between WGS84 and the International Terrestrial Reference Frame (ITRF, 2008), cf. [2.4.2].

GPS-time (unit SI-second) as a continuous time scale is defined by the cesium clocks of the control segment stations and the satellites. Its initial epoch is January 5, 1980 at 0 h UTC, and since then it differs from UTC because of the UTC “leap seconds”, cf. [2.2.2], and the drift in the GPS clocks. The actual difference between GPS-time and UTC (some 10 s) is part of the GPS navigation message (± 5 ns). GPS thus is also a very efficient system of *time transfer*. An accuracy of some 10 ns can be obtained already with automatically operating single-frequency receivers, while multi-station and multi-satellite constellations allow the time transfer with ± 1 to 0.1 ns (Larson and Levine, 1999).

The *user segment* is composed of the many different type *GPS receivers* operating in navigation, geodesy, and surveying. The main components of a receiver include the antenna, the receiver electronics, the microprocessor, the oscillator, the memory, the user interface, and a power supply. An additional telemetry unit can be used for data transfer between different receivers (differential mode, see below).

The signals transmitted from the satellites are received and amplified by the antenna. After identification (comparison with the receiver’s code copy) the signals are processed to pseudoranges in the channels of the receiver electronics. One channel is generally responsible for the tracking of one satellite. Hence, a minimum of four channels is necessary to determine position and time. Dual-frequency receivers contain 12 or more channels for each frequency (multi-channel technique), which results in a total of 72, 120 or even 220 channels, and enables the simultaneous tracking of a large set of GPS, GLONASS and Galileo satellites. The microprocessor controls the operation of the receiver and calculates the three-dimensional position of the antenna in WGS 84, as well as the velocity and azimuth of moving objects. A quartz oscillator is used for generating the reference frequency, which is approximately synchronized with GPS-time. All data (pseudoranges, phases, time, navigation message) are stored in receiver memory for post-processing, which is typical for multi-station observation sessions often employed in geodesy, cf. [6.2.1]. The user interface includes a keyboard and a display, which provides a communication link between the user and receiver. Power is provided by internal, rechargeable nickel-cadmium batteries.

While GPS *code-signals* (see below) generally are sufficient for *navigation*, *geodetic* GPS receivers use the *carrier phases* as observables which leads to higher accuracies, in the static as well as in the kinematic mode (e.g., Langley, 1997; Seeber, 2003, p. 234 ff.). This is achieved by dual-frequency (L1 and L2) multi-channel instruments and the full carrier wave information available on L1 and L2. Other characteristics include low receiver-noise in code and carrier phase, a high data rate (>1 Hz, and up to a 50 Hz sampling rate), and a large memory capacity. The antenna phase center should be stable and protected against multipath effects (see below).

The Macrometer (1982) was the first GPS receiver for geodetic applications (code-free, single frequency, 6 parallel channels), Counselman and Shapiro (1979). The Texas Instruments TI4100 (1984) provided all geodetically relevant observables (P- and C/A-code pseudoranges, carrier phases on L1 and L2) in a multiplex channel technique (Seeber et al., 1985). Today, a large number of geodetic receivers is available (see the relevant journals as “GPS Solutions”), and their efficiency is discussed in the geodetic literature. Figs. 5.15 to 5.19 show some examples of actual GNSS-receivers. These instruments are generally able to track any combination of GPS, GLONASS and Galileo satellites, where 20 to 30 satellites will be visible with fully deployed

systems. This will improve the satellites-receiver geometry as well as the integrity of the solution, and lead to a higher accuracy for absolute positioning.



Fig. 5.15: GPS continuously operating reference station (CORS) with receiver (Trimble 5700 GPS and GNSS Choke Ring Antenna, courtesy Trimble Navigation Ltd., Sunnyvale, CA, U.S.A.).



Fig. 5.16: Geodetic GNSS two-frequency receiver (Leica Viva GS15), with controller (Leica Viva Controller CS15), courtesy Leica Geosystems AG, Heerbrugg, Switzerland.



Fig. 5.17: JAVAD-TRIUMPH-1 Integrated GNSS receiver with fully integrated GNSS antenna, courtesy JAVAD GNSS, Inc., San Jose, CA, U.S.A.



Fig. 5.18: GPS/GLONASS rover TOPCON HiPer II, courtesy TOPCON Europe B.V., Capelle a/d IJssel, Netherlands.



Fig. 5.19: Septentrio AsteRx3 HDC GPS/Galileo/GLONASS and COMPASS receiver and PolaNt G antenna, courtesy Septentrio Satellite Navigation NV, Leuven, Belgium.

We now discuss in more detail code and carrier phase measurements employed for GPS navigation and positioning.

Code measurements use the travel time Δt of a signal between the satellite and the antenna of the receiver. The time difference is determined by cross-correlating an arriving code sequence with a code copy generated in the receiver. Multiplication of Δt with the velocity of light c gives the distance between the satellite and the antenna, cf. [5.1.1]. Considering the receiver clock synchronization error δt , the *observation equation* for the *pseudoranges* R reads as

$$R = c\Delta t = s + c\delta t \quad (5.43a)$$

The distance is given by

$$s = \left((X_s - X_p)^2 + (Y_s - Y_p)^2 + (Z_s - Z_p)^2 \right)^{\frac{1}{2}}, \quad (5.43b)$$

where X_s , Y_s , Z_s and X_p , Y_p , Z_p are the geocentric coordinates of the satellite and the ground stations, respectively. The *navigation message* needed for the evaluation of (5.43) is transmitted on L1 and L2. It contains the satellite's ephemeris (broadcast ephemeris, accuracy now about ± 1 m) in the form of Keplerian elements and certain time derivatives and orbital corrections, the satellite's clock correction with respect to GPS time, ionospheric correction parameters, and information on the status of the GPS system. Equations (5.43) then provide the coordinates of the ground station and the receiver clock correction from simultaneous measurements to at least four satellites. This presupposes that atmospheric refraction effects are taken into account by proper reductions (see below). The accuracy limit of this method is given by the random noise of the code measurement noise where the noise level may be estimated by 1% of the signal's wavelength. This leads to ± 3 m for the C/A-code and ± 0.3 m for the P-code, and has in geodesy generally led to the use of carrier phase measurements (see below).

GPS provides two different services for navigation (positioning and timing). The *Standard Positioning Service* (SPS) only delivers the C/A-code, and is available for all kind of users. An average positioning accuracy (24 h measurement interval, 95% probability level) of about ± 10 m (horizontal) and ± 20 m (vertical) or better can be achieved, but may be worse by a factor of two or more under unfavourable atmospheric and site conditions. The *Precise Positioning Service* (PPS) uses the P-code (Y-code). It provides all GPS signals and thus the full accuracy of the system, but is reserved to authorized users (U.S. military, U.S. federal agencies, selected allied armed forces). Real-time positional accuracies of better than ± 10 m are attainable with dual-frequency receivers. With GPS being fully operational, an *accuracy deterioration* for civil users had been introduced by DOD consisting of "selective availability" and "Anti-Spoofing".

Under *Selective Availability* (SA), the fundamental frequency of the satellite clocks was destabilized, and the ephemeris data were manipulated. This degraded the absolute accuracy to about 100 m in horizontal position and 150 m in height. SA was applied only between 1990 and 2000, and after suspension the accuracy of positioning and time transfer reached the previous standard. A more rigorous measure was the introduction of *Anti-Spoofing* (AS) in the middle of the 1990s. Since that time, the P-code has been replaced by the encrypted Y-code, which is non-accessible for civilian users.

Pseudorange differences can be derived from integrated *Doppler frequency shifts* (Doppler counts) of the carrier frequency according to (5.41) and (5.42). These differences are used for the determination of velocity in navigation. Doppler solutions also play a

role in the removal of ambiguities, which occur with carrier phase measurements (see below). The method is not suitable for real-time positioning due to the long observation time required.

Geodesy and surveying require accuracies of at least two orders of magnitude better than that required for navigation. This is achieved by *carrier phase measurements*. Due to the shorter wavelength of carrier phases, the random measurement noise is now only about 2 mm or even less (Beutler et al., 1987; Langley, 1997).

The carrier phase is detected by comparing the received carrier signal with the reference frequency generated in the receiver after subtraction of the code. In order to reconstruct L2 under AS conditions (P-code encryption), different techniques have been developed, such as squaring of L2 (eliminates the code signal) and cross-correlation of L1 and L2. The measured phase difference

$$\Delta\varphi = \varphi_c - \varphi_0 \quad (5.44)$$

(φ_c , φ_0 are phase of the carrier and reference waves, respectively) is related to the distance s by the *observation equation*

$$\Delta\varphi = \frac{2\pi}{\lambda}(s - N\lambda + c\delta t), \quad (5.45)$$

which is well known also from terrestrial distance measurements, cf. [5.5.2]. N is an integer number of complete carrier cycles within the range s , and δt is the receiver clock synchronization error. The *ambiguity* introduced by N poses a primary problem for the evaluation of (5.45). Among the algorithms available for ambiguity determination, we have the inclusion of ambiguity-free Doppler solutions, the combination of code and carrier phases, and statistical search methods applied to combinations of L1 and L2. Difficulties arise when the phase lock is lost due to signal obstruction. Such sudden jumps of the carrier phase by an integer number of cycles are called *cycle slips*. They are either removed during pre-processing or taken into account by introducing an additional ambiguity for the affected pseudorange.

The *error budget* of GPS *pseudorange measurements* (as that of other GNSS positioning) contains satellite-specific, signal propagation-specific and user-specific effects, in addition to the random noise. The satellite part contains the satellite's orbit and clock errors, and the signal propagation is affected by ionospheric and tropospheric refraction. Among the user-specific effects are the receiver clock errors and signal propagation delays, antenna phase center variations, multipath effects, and diffraction and signal interference (Seeber, 2003, p. 297 ff.).

Orbital errors are at the order of a few meters for the Standard Positioning Service, while the International GNSS Service (IGS) is able to provide the precise rapid or final (post-processing!) orbits with cm-accuracy (see below). The broadcast *clock error* corresponds to an orbital error of about 1 m, and with the IGS products this error is reduced to the cm-level.

Atmospheric refraction strongly affects the electromagnetic waves while traveling through the atmosphere. *Ionospheric* refraction acts in a different way on the code signal and the carrier phase, causing a *code group delay* (pseudorange too long) and a *phase advance* (pseudorange too short). The effect depends on the (strongly variable) electron content along the signal path and may cause range errors of some meters, reaching eventually some 10 or even 100 m. When only a single-frequency receiver is available, a corresponding reduction has to be based on models of the electron density,

cf. [5.1.3]. Among the ionospheric correction models is the development by Klobuchar (1996), which provides the vertical time delay at GPS measurements by exploiting the GPS ionospheric coefficients broadcast message. Global (IGS) and regional GPS services also offer ionospheric reduction models, containing TEC information with high time resolution and nearly real-time.

The most efficient way to eliminate the largest part of the ionospheric refraction effect is the use of *two-frequency* receivers. The application of (5.23) to the frequencies f_1 and f_2 leads to the reduced distance (for *code* measurements)

$$s = \frac{s_1 f_1^2 - s_2 f_2^2}{f_1^2 - f_2^2}. \quad (5.46)$$

Here, the ionospheric refraction is eliminated, and s_1 and s_2 are the observed distances on L1 and L2 respectively; the residual errors do not exceed the cm-order of magnitude. A corresponding equation can be derived for *carrier phase* observations.

Tropospheric refraction may cause propagation delays of 2.3 m (zenith direction) to about 25 m (at 5° elevation). It is accounted for by tropospheric models and observed surface weather data, cf. [5.1.2]. The “wet” component remains a critical part of these reductions, which may be accurate to a few cm under ideal conditions and large elevation angles, but could reach a meter uncertainty and more at elevations less than 5°. Other strategies for reducing the effect of tropospheric refraction include the estimation of a station dependent “zenith scale factor” for each satellite pass and real-time monitoring in active multiple reference station networks (Bevis et al., 1992), cf. [7.3].

Multipath effects result from signal reflection (at streets, buildings, waterways, etc.) near the antenna. They affect code and carrier phase measurements and can produce errors of a few meters and more at the C/A-code, and of a few cm to dm at carrier phase measurements. Signal diffraction at obstacles and interference with other radiowave sources may also occur. A reduction of these effects is possible by a proper design of the antenna (e.g., at the low-multipath choke-ring antenna used at the IGS stations) and by careful site selection. As the *antenna’s electrical phase center* does not coincide with the geometric center, a phase center offset occurs (a few mm), which is usually provided by the manufacturer. More critical are the phase center variations, which depend on the satellite’s elevation and azimuth and amount to a few mm to cm (up to 10 cm in the vertical). Relative (with respect to a reference antenna) and absolute (using a robot’s rotation and tilting) field calibration methods have been developed in order to model this effect (Görres et al., 2006). These effects also become visible when antennas are changed at continuously operating reference stations, and have to be taken into account accordingly (Wanninger, 2009). Corresponding considerations regarding phase center offsets and variations also have to be made with respect to the satellites’ antennas (Schmid et al., 2005).

The *accuracy* of GPS *positioning* depends, in addition to the accuracy of the pseudorange, on the geometric configuration of the satellites with respect to the receivers and on the duration of the observation time. A longer observation time increases the accuracy, especially for long baselines and for the height component. The accuracy at the kinematic mode (moving GPS antenna) generally is slightly lower than that of the static mode.

The accuracy of an observed pseudorange can be expressed by its standard deviation (also user equivalent range error). The strength of the satellite geometry is characterized by a quantity called

"Positional Dilution of Precision" (PDOP). It is defined as the ratio between the standard deviation of a position σ_p derived from a certain satellite constellation and the standard deviation of an observed pseudorange σ_r according to $\sigma_p = \text{PDOP} \times \sigma_r$ (Langley, 1999). The numerator of this quotient follows from the trace of the coordinates covariance matrix, which depends on the design of the network. PDOP values can be calculated in advance, and then serve for the planning of observations and for rapid information on expected positioning quality. For instance, a PDOP value of 2 (this value is now seldom exceeded) means that the accuracy of positioning is two times worse than the accuracy of the pseudorange observation. If separated into the horizontal and the vertical components, it turns out that the determination of heights is less accurate than horizontal positioning by a factor of about 2. This results from the fact that all observed satellites are *above* the receiver but azimuthally distributed over the *total* horizon, and that the receiver clock corrections are strongly correlated with height (Rothacher, 2002).

With respect to the GPS positioning strategy and the accuracy obtained, we may (like in other geodetic space techniques) distinguish between the absolute and the relative mode.

Absolute positioning employs a single receiver and uses the Standard Positioning Service for determining the station coordinates (see above). The accuracy thus remains restricted and does not significantly increase with the observation time. With the use of precise ephemerides and satellite clock corrections provided by IGS (see below) and exploiting code and carrier phase observations this situation is changing, leading to cm-accuracy at post-processing of longer observation series, cf. [7.3].

For *orbital errors*, a (pessimistic) rule of thumb allows an estimate of the error to be expected in a baseline b from the orbital error dr :

$$\frac{db}{b} = \frac{dr}{s} \quad (5.47)$$

where s is the distance between the satellite and the receiver (maximum 25 000 km). Hence, if an accuracy of 1 cm is required for the baseline, the orbital error should not exceed 2.5 m at $b = 100$ km and 0.25 m at $b = 1000$ km. When the precise ephemerides from the IGS are used, orbital errors no longer play a major role.

Relative positioning is accomplished by simultaneous observations (code and/or phase measurements) on two or more stations, including at least one with known coordinates (reference station). This strategy significantly reduces the distance-dependent effects that occur in the absolute mode (orbital errors as well as ionospheric and tropospheric refraction), due to the high error correlation at neighboring stations.

This strategy has been extended by combining observations of different satellites and at different epochs, and code with carrier phase observations. As a consequence, satellite and receiver clock errors can be eliminated, and rapid ambiguity solutions become possible. Station specific effects, on the other hand, are uncorrelated and cannot be reduced by differencing, they must be kept small by proper selection of the station and corresponding calibration procedures. At post-processing, this relative GPS solution delivers *differences* of coordinates ("baseline vectors") with high accuracy.

Differential GPS (DGPS) has been developed in order to improve the position of a roving station by applying corrections transmitted from a permanently operating reference station to the user in real-time. Corrections may be derived from code observations at the reference station and refer to position or the observed pseudorange. If code-range and (the more precise) carrier phase data are transmitted to the

user station ("rover"), the procedure is called precise DGPS or *Real-Time Kinematic* (RTK) GPS. It delivers the baseline vector in real-time (cm-accuracy over shorter distances) and includes the simultaneous resolution of ambiguities at the rover station. The method can be extended to a network of reference stations (Seeber, 2003, p. 325 ff.; Schön, 2010), cf. [7.3]. For code measurements, the accuracy obtained at relative positioning with good PDOP conditions is $0.25\text{ m} + 1\text{ ppm/horizontal}$, and $0.5\text{ m} + 1\text{ ppm/vertical}$. Carrier phase measurements in the static mode can deliver $5\text{ mm} + 0.5\text{ ppm/horizontal}$ and $10\text{ mm} + 0.5\text{ ppm/vertical}$ in real-time, and could be improved by a factor of about two through post-processing. In the kinematic mode, the accuracy decreases by a factor of about 2. Here and in the following, the distance dependent error part *ppm* is relative to the baseline length. More details on three-dimensional positioning are given in [6.2.1] and [7.3].

The Global Positioning System (and other GNSS) has drastically changed surveying methods in geodesy, navigation, and other applications. This is mainly due to the high accuracy achieved with static and kinematic positioning, real-time evaluation, and operational flexibility. Direct visibility between the ground stations is not necessary any more, only visibility to the satellites is required. The system is weather independent and usable day and night. The use of GPS and other GNSS is still increasing and is strongly supported by global and regional services, cf. [7.3].

High-quality GNSS data and products are available through the *International GNSS Service* (IGS), which operates under the auspices of IAG (Beutler et al., 1999; Dow et al., 2005). Starting as International GPS Service in 1994, more than 200 institutions and agencies now cooperate within this enterprise, with a Central Bureau located at the U.S. Jet Propulsion Laboratory. IGS operates a global network of (today nearly 400) GNSS tracking stations, Fig. 5.20, and some data and data analysis centers, in order to supply observed data and derived products for Earth science research, positioning, navigation



Fig. 5.20: Network stations of the International GNSS Service IGS (status 2010), courtesy IGS (<http://igscb.jpl.nasa.gov/>).



Fig. 5.21: IGS sites HOFN in Höfn, Iceland (left side) and BUCU in Bucharest, Romania (right side), Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt a.M., Germany (<http://www.fs.wettzell.de>).

and timing. The sites have been carefully selected and monumented (Combrinck and Chin, 2001), and use high performance antennas (Fig. 5.21).

The stations are equipped with geodetic two-frequency GPS (GNSS) receivers and generally operate permanently; raw tracking data (phase and pseudorange observations) are provided on hourly basis or even real-time. The IGS products include GPS satellite ephemerides, satellite and station clock parameters, Earth rotation parameters, station coordinates, and ionospheric and tropospheric information. GPS orbits and satellite clock offsets are given on a daily basis, in an ultra rapid (real-time and 3 h delay), rapid and final version. The final “precise” ephemeris (from post-processing) has a precision of about 2 cm, the “rapid” ephemeris is only slightly less precise. Satellite and station clock parameters are precise to 0.05 ns, and the quality of derived Earth orientation parameters (polar motion and LOD) is given by 0.05 mas and 0.02 ms/day, respectively. Weekly solutions for the station coordinates are characterized by a precision of 2 mm (horizontal) resp. 4 mm (vertical), and by 2 resp. 4 mm/year for station velocities (Kouba, 2009). By co-location with other geodetic space techniques, the IGS network is connected to the International Terrestrial Reference Frame (ITRF) and contributes significantly to it; IGS stations also play an important role at densifying ITRF on continental scale, cf. [2.4.2], [7.3].

In addition to GPS, there are a number of other Global Navigation Satellite Systems (GNSS) already operating or in the state of development, at global and regional scale (Fairheller and Clark, 2006; Becker, 2009).

A global navigation satellite system similar to GPS has been developed in the former Soviet Union since the 1970s: GLONASS (Global'naya Navigatsionnaya Sputnikovaya Sistema), Hegarty and Chatre (2008). Like GPS, GLONASS is a military system, but it has been stepwise opened to civilian users since the end of the 1980s. The system became fully operational in 1996, and after some drawbacks (lack of satellites) again in 2010. GLONASS operates as a one-way ranging system, with a space segment comprising 24 (including three spares) satellites, Fig. 5.22.



Fig. 5.22: GLONASS-M satellite, courtesy Russian Federal Space Agency ROSCOSMOS (<http://www.federalspace.ru>).

The satellites are arranged at a regular spacing of 45° in three nearly circular orbits separated 120° apart from each other ($i = 64.8^\circ$, $h = 19\,100$ km, revolution time 11 h 15 min). This configuration assures the simultaneous visibility of six to 11 (minimum five) satellites all over the Earth. The satellites transmit on two carrier frequency bands (G1 around 1602 MHz and G2 around 1246 MHz), but contrary to GPS with *different* frequencies for each satellite. The standard-accuracy C/A-code and the high-accuracy P-code modulated onto the carrier frequencies are the same for all satellites. The GLONASS-K generation (since 2010) provides a third carrier frequency (G3: 1205 MHz) with an additional civil and military ranging code. There is no degradation of the GLONASS signals, but the P-code has not been officially released and may be changed without prior notice. All GLONASS satellites are equipped with laser retroreflectors for laser tracking, and timing is provided by three atomic clocks (cesium standards). The control segment consists of a master control station near Moscow and a large number of secondary tracking stations distributed over the territory of the former Soviet Union. The satellite's navigation message contains the broadcast ephemerides (positions and velocities) and the satellite clock corrections, among others. The accuracy of the predicted orbits and velocities varies between 20 m resp. 0.05 cm/s (along-track) and 5 m resp. 0.3 cm/s (radially), and will increase by a factor of two to three with the GLONASS-M satellites. The GLONASS results refer to the reference system PZ-90, which is based on the former Soviet Geodetic Reference System 1985 (SGS85), Misra and Abbot (1994). The recent realization (2007) agrees within a few decimeters with the World Geodetic System 1984 (WGS84) and with ITRF. GLONASS uses its own time system (UTC + 3 h) which is synchronized to UTC within 1 μ s by the use of leap-seconds.

By combination of GLONASS with GPS, about 12 to 16 satellites are visible at any place of the Earth, which leads to a better coverage of the sky and an improved (with respect to accuracy and surveying of "shadow areas") positioning. Consequently, GNSS

receivers with GPS and GLONASS (and also Galileo and other satellite navigation systems) capability are commercially produced now, where 20 dual frequency channels are required for a GPS/GLONASS combination (Fig. 5.19).

An European navigation satellite system called Galileo started with a definition phase, between 1999 and 2001 (Deisting and Hein, 2006; Hofmann-Wellenhof et al., 2008, p. 341 ff.). The fundamental intention of this enterprise, which is under the supervision of the European Commission and the European Space Agency (ESA), is to establish a global *civilian* navigation and positioning system especially for Europe and surroundings, serving different demands and providing different levels of accuracy and availability. The system shall be independent from GPS and GLONASS, although it should be inter-operable with those systems. In 2007, the European Union took direct control of the Galileo project (Schüler et al., 2009).

The space segment of Galileo shall consist of 27+3 satellites (Fig. 5.23) distributed at 40° distance over three circular Earth orbits which are separated by 120° ($i = 56^\circ$, $h = 23\,260$ km, revolution time 14 h 04 min), Fig. 5.24. Satellite-borne timing is provided



Fig. 5.23: Galileo satellite GIOVE B (Galileo In-Orbit Validation Element), courtesy ESA.

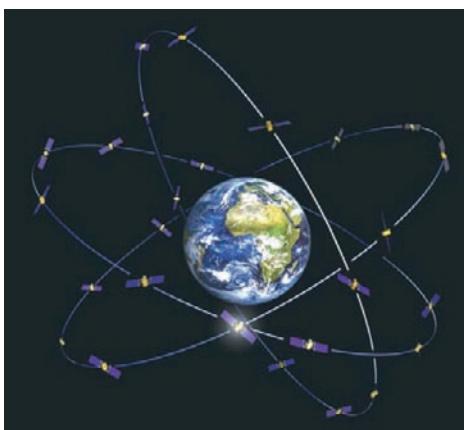


Fig. 5.24: Galileo satellite constellation, courtesy ESA.

by two rubidium frequency standards and two hydrogen masers, with time stability of 10 and 1 ns/day, respectively. All satellites carry laser reflectors in order to support the microwave-based orbit determination.

The following three L-band carrier frequencies bands will be used for navigation and positioning: 1176/1207 and 1192 MHz (E5a, E5b; E5), 1278 MHz (E6), 1575 MHz (E1); the overlay on GPS L1 and L5 and GLONASS G3 frequencies should strengthen the interoperability between the systems. There is an individual code modulation for each satellite (like GPS), and ranging codes and navigation messages will differ according to the application requirements (see below). The system will be operated by three ground control centers, providing orbital data and time synchronization, and supported by about 30 to 40 globally distributed monitoring stations. The “Galileo Terrestrial Reference System” will refer to the actual ITRF. The Galileo system time (GST) is a coordinate time scale, with only small offsets from TAI.

The navigation message, as generated by the ground segment and uploaded to the satellites, will, among others, contain the satellites ephemerides (modified osculating Keplerian elements) and the satellite clock offset GST-TAI. From a total of ten navigation signals, six will be accessible on E5a, E5b and E1 for all users of the Open Service, while two signals on E6 with encrypted ranging codes and correction data are dedicated to users of the Commercial Service. Authorized users of the Public Regulated Service will have access to another two encrypted ranging codes, on E6 and E1. Depending on the carrier frequency, the noise-level of the code-distances is expected to be at the few centimeter to decimeter level, with multipath effects ranging from a few decimeter (open area) to a few meter (urban environment). An accuracy (95% level) of 4 m (8 m) is envisaged for the horizontal (vertical) position, and 50 ns for the time offset.

The Galileo system has been successfully tested by the GIOVE-A/B satellites (Galileo In-Orbit Validation Element) launched in 2005 and 2008. Further satellites followed in 2011, while the full operational capability is expected not before 2020. As with the GPS/GLONASS combination, a joint use of Galileo with these systems will result in an increased accuracy and extended application of satellite navigation and positioning. For instance, fully operational GPS and Galileo would allow simultaneous visibility to 15 or more satellites, resulting in improved geometric configurations ($\text{PDOP} < 1.6$), better ambiguity fixing, and an improvement of position accuracy by a factor of 2 to 3. For the reduction of ionospheric refraction effects at single-frequency positioning, the Nequick model has been proposed. It will employ ionospheric information from the satellite navigation message together with data from a global sensor network, and thus deliver the time-dependent state of electron density (Leitinger et al., 2005).

Regional satellite navigation systems have been developed or are under development also in other parts of the world, and will partly be extended to global systems (Fairheller and Clark, 2006; Hofmann-Wellenhof et al., 2008, p. 406 ff.). As with the European Galileo system, a main impetus for building up these systems is the desire to become independent from the military-managed systems of the U.S.A. and Russia, with a system completely under national control.

China started the development of a regional satellite navigation system under the name of Beidou-1 in the 1970s. Since the 1990s, the system is upgraded to a global one, with one-way distance measurements similar to GPS and GLONASS: Beidou-2/COMPASS.

The system is operated by the China National Space Administration, and designed as a combination of 24+3 satellites in medium height (around 21 500 km), which are evenly arranged in three orbital planes ($i=56^\circ$), with additional five geostationary satellites and three satellites in inclined geosynchronous orbits (36 000 km), Bian et al. (2005). Carrier signals will be emitted in three frequency bands (1575, 1192, 1268 MHz), with satellite-specific codes. The first COMPASS-M1 experimental satellite started in 2007, and further satellites followed in 2009/2010, an operational service is expected for 2020. The accuracy of the system's broadcast information available for civilian use is expected to be at the order of 10 m, 0.2 m/s, and 50 ns for position (geocentric Earth-fixed reference system compatible with ITRF), velocity and time, respectively (Huang and Tsai, 2008).

Further regional navigation satellite systems are under development in Japan and India. The Japanese Quasi-Zenith Satellite System (QZSS) is a proposed satellite system (first satellite launch in 2010), consisting of at least three satellites in orbital planes ($i = 45^\circ$, $a = 42\,160$ km, $e = 0.1$) with geosynchronous periods. The system shall complement GPS, but also serve as an autonomous positioning system for eastern Asia and Oceanica, if necessary. The Indian regional navigation satellite system (first satellite launch planned for 2011, system implementation by 2014) is scheduled for a constellation of seven satellites, three of them in geostationary orbit, and the other four operating in geosynchronous orbits ($i = 29^\circ$). With continuous radio visibility to the Indian control stations, dual-frequency operation should provide a position accuracy of better than 20 m for India and the surrounding areas.

5.2.6 Laser distance measurements

Laser distance measurements are made from ground stations to satellites equipped with corner cube reflectors: *Satellite Laser Ranging* (SLR). This method provides high accuracy due to the favorable propagation of laser light in the atmosphere, and it offers a low-cost, long-lifetime space segment. On the other hand, laser measurements depend on weather conditions and require a considerable operational effort at the ground segment (Combrinck, 2010).

At the ground station, ultra-short laser pulses are emitted at epoch t , reflected at the satellite, and received again at epoch $t + \Delta t$. If refraction effects are sufficiently taken into account by corresponding reductions, the distance is obtained by

$$s = \frac{c}{2} \Delta t, \quad (5.48)$$

it refers to the satellite's position at the time of reflection.

We distinguish between the space and the ground segment of SLR. The *space segment* consists of a laser reflector array arranged on the satellite's surface. Since the 1970s, a large number of *satellites* have been equipped with such arrays, and employed for geodetic positioning and crustal deformation monitoring, determination of Earth rotation parameters, gravity field modeling, and precise orbit determination of dedicated satellite missions.

Dedicated SLR missions for positioning and geodynamic research include the satellites Starlette (France, 1975, $h = 800$ to 1100 km, $i = 50^\circ$), the *Laser Geodynamics Satellites* Lageos 1 and 2 (U.S.A., 1976/1992, $h \approx 5900$ km, $i = 110^\circ/52^\circ$, Cohen et al., 1985; Tapley et al., 1993), Ajisai (Japan, 1986, $h \approx 1500$ km, $i = 50^\circ$), and Etalon 1 and 2 (USSR, 1989, each of the two satellites occupying one of the orbital planes used by GLONASS, Appleby, 1998). These satellites are spherical in shape (diameter 0.2 to



Fig. 5.25: Laser satellite LAGEOS, courtesy National Aeronautics and Space Administration (NASA).

2 m) and heavy, and they possess a favorable surface-to-mass ratio (Fig. 5.25). Satellites employed for altimetry and gravity field missions also carry laser retroreflectors on board as well as the GLONASS and a few GPS satellites, and the future Galileo satellites shall also be equipped correspondingly.

The SLR *ground segment* is represented by the Laser distance *measuring* system. It consists of the laser unit (Nd:Yag-laser = Yttrium-aluminum garnet crystal doped with neodymium ions), the transmitting and receiving optics (telescopes), and the receiver electronics (secondary-electron photomultiplier). The mechanical mounting provides an automatic tracking (required pointing accuracy 1" and better) of the satellite's pre-calculated orbit, with proper on-line corrections. The travel time is measured by a time-interval counter, controlled by an atomic clock, which is regularly compared to UTC. A process computer controls the complete measurement, registration and evaluation process.

The accuracy of laser distance measurements depends on the pulse length, the stability of the photomultiplier, and the time resolution. Atmospheric delay is corrected with standard atmospheric models, cf. [5.1.2]. A dual-color laser development aims at the improvement of the refraction correction by exploiting the dispersion of light. Depending on the satellite's altitude and the constraints of the observation program, some 100 to 1000 distances can be measured during one passage. Third generation lasers operate with pulse lengths of 0.1 to 0.2 ns which corresponds to an accuracy of 1 to 3 cm; and the single-shot precision is now 5 to 10 mm. The amount of photons per pulse reduces significantly on the way from the emission (about 10^{15} per pulse) to the receiver, by about 12 or more orders of magnitude, which led to the use of pulse trains (3 to 10 pulses) at a fixed interval, and the development of single photon detectors. By compressing the data to "normal points" (e.g., at Lageos as the average over 30 s to

120 s), sub-cm precision is achieved. Fourth generation lasers will be characterized by repetition rates of 10^2 to 10^3 Hz ("kHz-laser").

About 40 *laser-satellite systems* are nowadays operating worldwide, either in the stationary (and partly permanent) or in the mobile mode. As an example, the actual Wettzell laser ranging system employs a Nd:Yag laser (532 nm) and a 75 cm telescope. It operates with high-energy short pulses (pulse length 180 ps, pulse energy 100 mJ) at a pulse repetition rate of 1 to 10 Hz in the single-shot mode. Visible and/or infrared light is used, allowing a day-and-night operation to satellites at altitudes between a few 100 and 40 000 km, Fig. 5.26. Further developments are directed to reduce the pulse length to some 10 ps and to reduce the pulse energy.

Mobile systems have been developed in the U.S.A. and in Germany/Netherlands, among others (Silverberg, 1978). Operating with low energy and single-photon detection, these systems are employed mainly for the investigation of recent crustal movements, cf. [8.3.4]. The NASA SLR-network consists of a number of mobile laser ranging systems distributed worldwide. A transportable, integrated geodetic-observatory (TIGO) is operated by BKG (Bundesamt für Kartographie und Geodäsie, Germany). In addition to the laser unit, it includes a VLBI module and a GPS unit. TIGO is employed for strengthening fundamental reference networks, especially in the southern hemisphere, and is now operating near Concepcion/Chile.

Laser retroreflector arrays have been placed on the *moon* by the U.S. Apollo 11 (1969), 14, and 15 (1971) missions, and the French reflectors Luna 17 (return signals obtained only in 2010) and Luna 21 were deployed 1970/1973 by the Soviet automatic lunar



Fig. 5.26: 75 cm telescope, Wettzell Laser Ranging System (WLRS), Geodetic Observatory Wettzell, Germany, courtesy Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt a.M., Germany (<http://www.fs.wettzell.de>).

missions Lunokhod 1 and Lunokhod 2. These reflectors provide targets for *lunar laser ranging* (LLR), Shelus (2001) (Fig. 5.27). Pulsed lasers with a tightly bundled beam and a powerful telescope are necessary in order to recapture the weak returning signal. A single photon technique has to be applied as eventually only one photon out of an emitted amount of 10^{19} has to be detected. The tracking system must provide a $2''$ pointing accuracy. The accuracy of these measurements is about 1 cm, and will probably be improved to a few mm.

Observations to the moon have been carried out regularly since 1969 by the McDonald Observatory, University of Texas, and since the 1980s also at the Observatoire de la Côte d'Azur, Grasse/France. At the beginning of the twenty first century a new laser ranging station (APOLLO) with lunar capability was established at Apache Point Observatory, New Mexico, U.S.A. It is equipped with a 3.5 m-telescope, designed for mm-accuracy. Actual plans for joining the LLR tracking network include the laser ranging systems in Wettzell/Germany and Matera/Italy.

Due to the high accuracy and the long-term stability, LLR results especially contribute to investigations of the dynamics of the Earth-moon system including lunar ephemerides and lunar libration, testing of the theory of relativity, connection of celestial and terrestrial reference frames, and research on terrestrial geodynamic processes and the lunar interior (Müller, 1991; Müller et al., 2007, 2009; Williams et al., 2009).

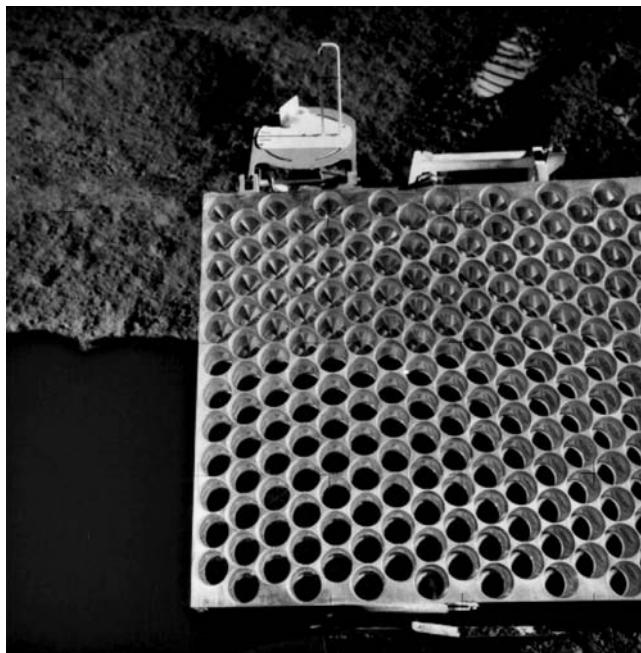


Fig. 5.27: Lunar Laser Reflector, courtesy Lunar and Planetary Institute, Houston, TX, U.S.A. (<http://www.lpi.usra.edu>).

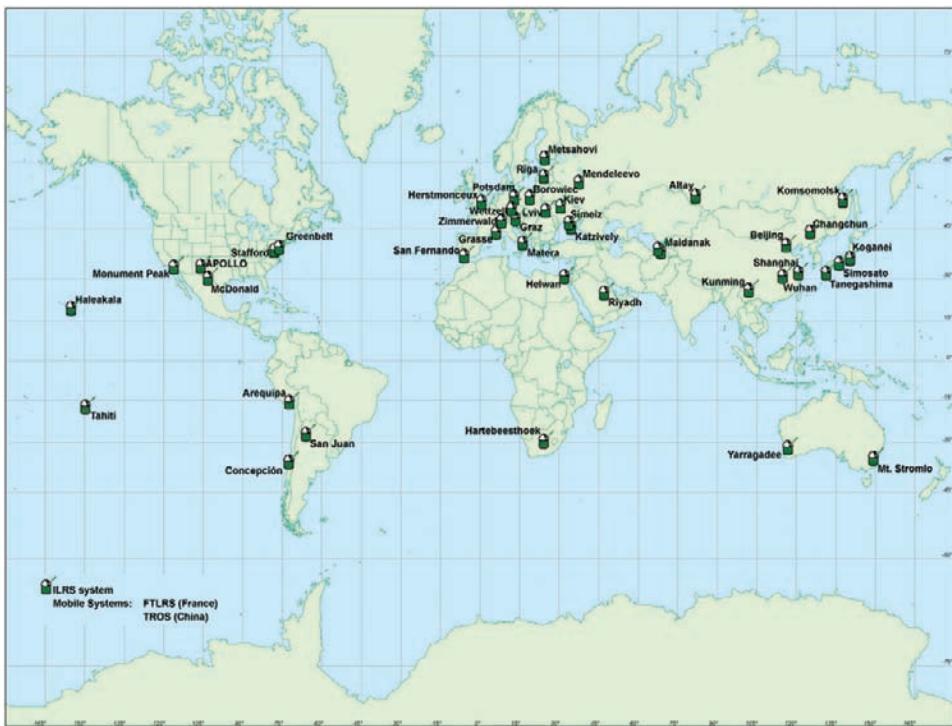


Fig. 5.28: Network stations of the International Laser Ranging Service ILRS (status 2011), courtesy ILRS (<http://ilrs.gsfc.nasa.gov/>).

The *International Laser Ranging Service* (ILRS) of IAG collects, analyzes and distributes the SLR and LLR data sets of presently about 40 stations, heterogeneously distributed over the globe (Fig. 5.28), Pearlman et al. (2007), Pavlis and Müller (2011). In addition to the ephemerides of the observed satellites (cm-accuracy), the service products include weekly solutions of the station coordinates and velocities with an accuracy of 6 mm and 2 mm/year, respectively; in contrast to other space methods the height accuracy is here better than the accuracy of the horizontal coordinates. The data also contribute to the determination of polar motion and length of day, and they are of special importance for the definition of the scale and the origin of the terrestrial reference frame (together with VLBI), and for monitoring the movement of the Earth's center of mass with respect to the ground stations. SLR observations finally are an important data set for the computation of gravity field coefficients, providing the long-wavelength part of the field including its variations with time.

5.2.7 Satellite altimetry

Satellite altimetry is based on a satellite-borne *radar altimeter* that transmits short pulses in the vertical direction to the Earth's surface (Chelton et al., 2001; Chambers, 2009). The ocean surface (and also ice and open water on land) partly reflects the pulses

perpendicularly, and the measurement of the travel time Δt furnishes the height of the satellite above the instantaneous sea surface (Fig. 5.29):

$$a = \frac{c}{2} \Delta t. \quad (5.49a)$$

(The denotation a should not be confused with the abbreviation for the semi-major axes of the satellite's orbit and of the Earth ellipsoid.)

In spherical approximation, the altimetric result can be expressed as

$$a = r_s - r_p - (N + SST), \quad (5.49b)$$

where r_s and r_p are the geocentric distances to the satellite and to the subsatellite point P on the ellipsoid, and $r_s - r_p$ is the satellite's height above the ellipsoid; N is the geoid height and SST the height of the sea surface topography. A proper reduction of atmospheric refraction effects and ocean tides is presupposed in (5.49b). Tracking provides the satellite's orbit and thus r_s , and geodetic positioning gives r_p . According to (5.49b), altimetry thus delivers information on the geoid and on sea surface topography. An ellipsoidal development of (5.49b) is given by Gopalapillai (1974).

Radar altimeters operate in the 14 GHz frequency range (corresponding to a wavelength of 2.2 cm) with short (a few ns) pulses and a high-pulse frequency (e.g., 100 pulses/s). The effects of beam divergence and finite pulse length result in measurements that refer to a "mean" sea surface within a circular "footprint" (few km diameter); short-wavelength features of the ocean (waves) are thereby smoothed out. For example, by averaging the measurements over one second, the along-track resolution is about 7 km.

Satellite altimetry missions are designed to provide either an exact repetition of ground tracks (days to weeks) or a dense pattern of profiles. The different modes are achieved by orbital maneuvers (Knudsen, 1993). The latter is for determination of the altimetric geoid according to (5.49b), and the former for investigation of ocean variability (Fig. 5.30).

The first global survey with a radar altimeter was accomplished by the GEOS-3 satellite (U.S.A., 1975–1978). The oceanographic satellites SEASAT (1978) and GEOSAT (U.S. Navy, 1985–1990) carried improved altimeter systems and operated in heights close to 800 km with 108° inclination and repetition rates of 3 and 17 days (McAdoo and Sandwell, 1988). The European Remote Sensing Satellites ERS-1 (1991–1996) and ERS-2 (1995–2007) operated at similar heights

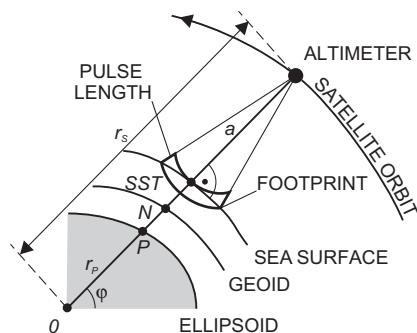


Fig. 5.29: Satellite altimetry principle.

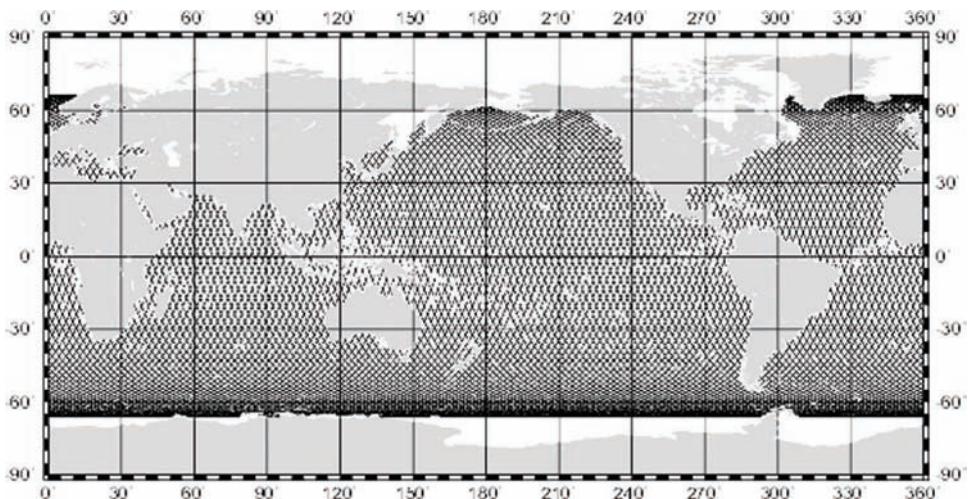


Fig. 5.30: TOPEX/Poseidon subsatellite tracks covered within the 9.9 days repeat cycle, Bosch (2001a).

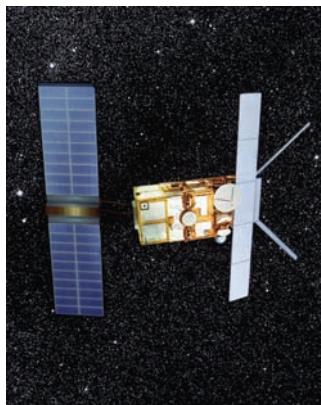


Fig. 5.31: European Remote Sensing (altimeter) Satellite ERS, courtesy ESA.

with 98° inclination (Fig. 5.31). Repetition rates were 35 and 168 days, respectively, and ground track distances at the equator 80 km and 8 km for geodetic missions (JGR, 1998). The NASA/CNES (French space agency) TOPEX/Poseidon satellite (1992–2005, 5.3 and 13.6 GHz) was placed in a circular orbit at an altitude of 1340 km and an inclination of 66°. Repetition time was 10 days, and the equatorial ground track interval 316 km (Fu et al., 1994; Cheney, 1995), see Fig. 5.32. GEOSAT follow-on (GFO, launch 1998), JASON-1 (2001–2008) and JASON-2 (since 2009), and the Environmental Satellite ENVISAT (since 2002) are successor missions of GEOSAT, TOPEX/Poseidon and ERS-1/-2, with similar orbital parameters. GPS and DORIS as well as laser retro-reflector arrays serve for orbit determination at these recent altimetry missions.



Fig. 5.32: TOPEX/Poseidon (altimeter) satellite, courtesy JPL/NASA, Pasadena, CA, U.S.A.

Dedicated altimetry missions deal with the repeated survey of the *polar ice caps* and the *sea ice*, in order to get more insight into the ice sheet mass balance. The NASA ICESat (Ice, Cloud, and land Elevation Satellite) operated from 2003 to 2009 in a near-polar orbit (altitude 600 km, $i = 94^\circ$). The satellite carried, among others, a laser altimeter (pulse length 5 ns, 40 Hz shot repetition rate) and a dual-frequency GPS receiver. The laser range precision (0.1 m) decreased with increasing ice slope, and the vertical orbit error was 0.05 m. An ICESat-2 mission is scheduled for 2015. Determination of ice topography and monitoring of ice height changes is also pursued by the ESA CryoSat-2 mission (altitude 720 km, $i = 92^\circ$) which was launched again in 2010, after the launch failure of CryoSat-1 in 2005. Height measurements are performed with a radar altimeter (few cm precision, horizontal resolution about 300 m), and for orbit determination the satellite is equipped with a DORIS receiver and laser retro-reflectors (Wingham et al., 2006).

The *error budget* of satellite altimetry is composed of orbit errors, instrumental errors, and signal propagation errors.

In order to achieve high radial-orbit accuracy, the satellites are equipped with laser retroreflectors for SLR, and additionally with microwave-based positioning systems such as Doppler, GPS, and DORIS (Andersen et al., 1998), cf. [5.2.3]. Further orbital improvements have been achieved by “tailored” gravitational field models developed for each dedicated altimeter mission (Tapley et al., 1996). The orbital error thus has been reduced from about 0.5 m for the GEOS-3 mission to a few cm for TOPEX/Poseidon and other more recent altimeter missions.

The precision (instrumental noise) of a one-second-mean altimeter observation is now better than 2 cm. Systematic instrumental effects (altimeter bias and drift) can be determined by calibration over ground-truth test areas, while the correction of sea state effects requires a careful signal analysis. The atmospheric propagation delay is taken into account by appropriate models, improved by simultaneous radiometer measurements of the water vapor for tropospheric refraction, and by the use of two frequencies for modeling the ionospheric refraction, cf. [5.1.3]. After reduction of the ocean tides and large-scale air pressure effects, the altimetric results refer to the quasi-stationary sea surface and yield its height with an accuracy of a few cm. For the evaluation of a region sampled multiple times with high spatial-resolution altimeter profiles, the track crossover discrepancies can be adjusted by minimum conditions modeling the errors

by time-dependent functions as low-degree polynomials (e.g., shift and inclination), splines or Fourier series (Van Gysen and Coleman, 1997). A multi-mission discrete crossover analysis of nearly simultaneous tracks has proved to be a powerful tool for cross calibration and detection of relative range biases (Bosch and Savcenko, 2007).

Monitoring of the sea surface by means of *reflected GPS signals* is still in the experimental stage. This method could possibly supplement satellite altimetry especially with respect to real-time determination of sea level and wave heights.

5.2.8 Satellite-to-satellite tracking, satellite gravity gradiometry

High-resolution gravity-field determination from space requires low-orbiting satellites and highly sensitive sensors, cf. [5.2.3]. This can be achieved by satellite-to-satellite tracking and satellite gravity gradiometry (Balmino et al., 1999; Rummel et al., 2002; Ilk et al., 2005a).

Satellite-to-satellite tracking (SST) employs microwave systems (laser distance measurements are under investigation) for measuring range and range rates between two satellites. High-low (several high and one low-flying satellite) and low-low (two low-flying satellites at the same altitude) configurations have been designed, a combination of both configurations is possible, Fig. 5.33. The basic observables are the range rates and the changes of the range rates along the line of sight between the satellites, these variations are due to gravitational and non-gravitational “disturbing” forces, cf. [5.2.2]. The gravitational field parameters (harmonic coefficients) can be derived after proper reduction of the effects of surface forces derived from dedicated accelerometer measurements, cf. (5.35). In order to achieve a gravity field resolution of 100 km, the orbital altitude of the lower satellite must not exceed a few 100 km (Jekeli, 2001b). The relative velocity between the satellites has to be determined with an accuracy of 1 to 10 $\mu\text{m/s}$, and precise orbit determination should be guaranteed by on-board satellite systems (GPS), supported by ground tracking stations.

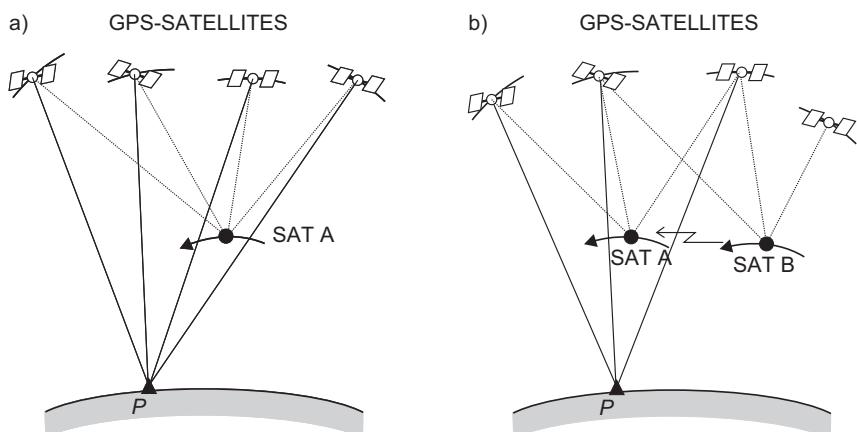


Fig. 5.33: Satellite-to-satellite tracking principle: a) high-low mode and b) low-low mode for the determination of range and range rate.

SST experiments started in the 1970s, e.g., between GEOS-3 and the geostationary satellite ATS-6 (nearly circular equatorial orbit, $h \approx 36000$ km). The CHAMP satellite (GFZ and DLR/Germany, 2000–2010) started a series of dedicated gravity field missions (Reigber et al., 2006; Flechtner, 2010). It was launched into a decaying orbit starting at an altitude of 450 km, which was raised several times in order to extend the satellite's lifetime. CHAMP (dimensions $4\text{ m} \times 1\text{ m} \times 1.6\text{ m}$) moved in a nearly circular polar-orbit ($i = 87^\circ$), Fig. 5.34. It carried a special (NASA) GPS receiver for continuous tracking (high-low mode) and a laser reflector array for ground support, cm-accuracy was thus achieved for the satellite's orbit. A three-axis accelerometer was used for measuring (precision 10^{-8} ms^{-2}) non-conservative forces as air drag and solar radiation, for later correction in post-processing. As this instrument was located in the satellite's center of mass, where gravity is compensated by the centrifugal force, it measured only the non-gravitational accelerations. A star imager provided attitude information and spatial orientation with respect to the inertial system. A magnetometer and a digital ion drift meter augmented the instrumentation. Gravity field recovery up to degree and order 120 was achieved, and the long-wavelength part of the geoid (until degree and order 30) could be derived with "cm-accuracy". Atmospheric sounding by GPS radio occultation was another result of the mission (Wickert et al., 2010).

The GRACE mission (NASA/German Aerospace Center DLR) started in 2002, and is now expected to continue until 2015. Primary mission objectives are the determination of the global high-resolution gravity field and especially its temporal variations. The mission employs two satellites of the CHAMP type orbiting at the same altitude (initially about 490 km) and in a nearly circular orbit ($i = 89.5^\circ$), with a varying (around 220 km) along-track separation (Fig. 5.35), Tapley et al. (2004). The intersatellite tracking (low-low mode) delivers range and range rate measurements (K-band microwave measurements with two frequencies (24 GHz, 32 GHz, μm -accuracy,

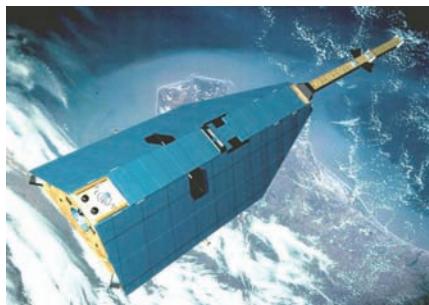


Fig. 5.34: CHAMP satellite, courtesy GFZ German Research Centre for Geosciences, Potsdam, Germany.

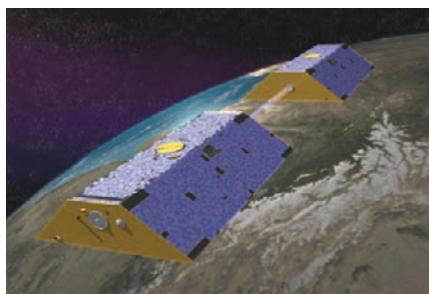


Fig. 5.35: GRACE satellites, courtesy NASA.

10 Hz sampling rate) between the satellites. Kinematic orbit determination is based on GPS-tracking (high-low mode) supported by laser distance measurement from ground stations to the satellites' nadir-directed laser retroreflector. Based on 5-minutes position series, an orbital accuracy of 1 to 2 cm is achieved. Attitude control is provided by star sensors, in connection with a GPS navigation solution. As at the CHAMP mission, a three-axis accelerometer is located in each satellite's center of mass and measures the non-conservative forces.

As a result from the GRACE mission, the static gravity field could be significantly improved in the long- and medium-part, and modeled up to spherical degree and order 150 to 180, with accuracies of 10 to 30 $\mu\text{m s}^{-2}$ for the gravity anomalies and 0.1 m for the geoid ("cm-accuracy" for the geoid part until degree 100), cf. [6.6.3]. Temporal variations of different origin have been found from monthly resp. weekly solutions, which are complete to degree and order 120, 120 and 30, 30 respectively, cf. [8.3.5].

In *satellite gravity gradiometry*, the second derivatives of the gravitational potential V are used for gravity field determination, and derived from the output of a gravity gradiometer (Fig. 5.36, Fig. 5.37), Rummel (1986), Esa (1999). The individual derivatives are generally combined in the gravitational gradient tensor (Marussi tensor)

$$\mathbf{V}'' = \begin{pmatrix} V_{xx} & V_{xy} & V_{xz} \\ V_{yx} & V_{yy} & V_{yz} \\ V_{zx} & V_{zy} & V_{zz} \end{pmatrix}, \quad (5.50)$$

with the x -axis pointing in flight direction, the y -axis in cross-track direction, and the z -axis in the outward radial direction, cf. [3.2.2]. From the nine elements in (5.50) only five are mutually independent, due to the tensor's symmetry and Laplace's equation, as demonstrated by (3.46) and (3.49) for the gravity field. By different orientation of the sensors, different components of the gravity gradient can be determined.

On the *Earth's surface*, gravity gradiometry has been employed since about 1900 with sensor pairs (accelerometers) sensitive to local changes of the gravity field in a certain direction, advanced gradiometric *airborne* techniques are used today in geophysics, cf. [5.4.5].

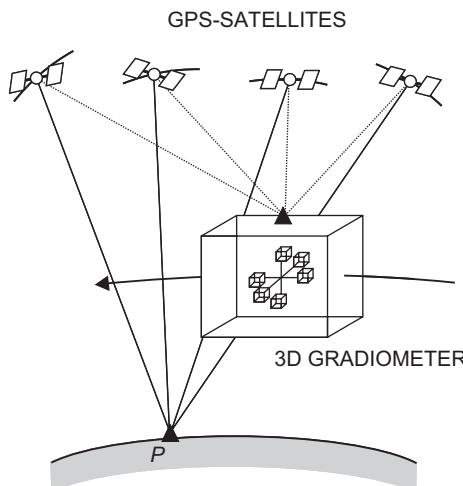


Fig. 5.36: Satellite gravity gradiometry principle, modified after Rummel et al. (2002).

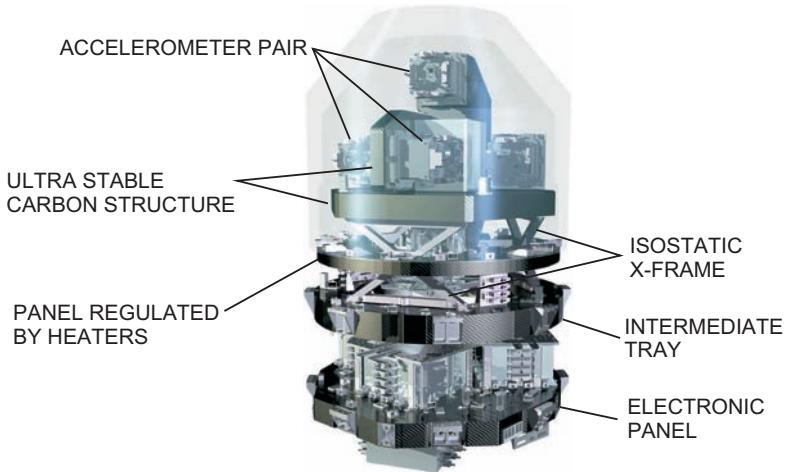


Fig. 5.37: GOCE Gravity gradiometer, courtesy ESA, modified after Rummel et al. (2009).

For *space-borne* applications, the attenuation of the gravity field with height (the second derivatives of the potential diminish with the third order of the radial distance!) requires a high measurement accuracy for the second derivatives. In the frequencies of interest (medium- and short-wavelengths' parts of the gravity field), the signals to be detected are of the order of $10^{-9} \text{ s}^2/\sqrt{\text{Hz}}$ only, at heights of a few 100 km. This requires a measurement accuracy at the order of 10^{-11} to 10^{-13} s^2 (Rummel, 1997). In addition to the gravity gradient tensor, the gradiometer output contains two terms which describe the orientation of the satellite with respect to an inertial system, and the effect of non-gravitational forces. The latter effects can be derived from the sum of the accelerometer pair outputs, and they cancel partly (linear parts) when differencing them (Moritz, 1968b). They can be compensated by a drag control system using thrusters ("drag-free" system). After proper compensation, the observation equation of satellite gravity gradiometry then reads as (Müller, 2001; Rummel et al., 2011)

$$\Gamma = \mathbf{V}'' + \boldsymbol{\Omega}\boldsymbol{\Omega} + \dot{\boldsymbol{\Omega}}. \quad (5.51)$$

The skew-symmetric matrices $\boldsymbol{\Omega}$ and $\dot{\boldsymbol{\Omega}}$ contain the components of the angular velocity around the x -, y - and z -axes and the corresponding angular acceleration, the tensor $\boldsymbol{\Omega}\boldsymbol{\Omega}$ is symmetric:

$$\boldsymbol{\Omega}\boldsymbol{\Omega} = \begin{pmatrix} -\Omega_y^2 - \Omega_z^2 & \Omega_x\Omega_y & \Omega_{xz} \\ \Omega_x\Omega_y & -\Omega_x^2 - \Omega_z^2 & \Omega_y\Omega_z \\ \Omega_{xz} & \Omega_y\Omega_z & -\Omega_x^2 - \Omega_y^2 \end{pmatrix},$$

$$\dot{\boldsymbol{\Omega}} = \begin{pmatrix} 0 & \dot{\Omega}_z & -\dot{\Omega}_y \\ -\dot{\Omega}_z & 0 & \dot{\Omega}_x \\ \dot{\Omega}_y & -\dot{\Omega}_x & 0 \end{pmatrix}. \quad (5.52)$$

This rotational part of the observation equations can be derived from combinations of the gradiometer observation equations, supported by orientation data from star



Fig. 5.38: GOCE satellite, courtesy ESA.

trackers. Special emphasis has to be laid on the accelerometers' calibration (scale, orientation, misalignments) realized in space and through comparison with ground truth. High requirements are posed on the satellite's orbit, which by orbital analysis also delivers the long-term parts of the gravitational field. Orbit determination is nowadays usually based on GNSS-tracking, with support through ground-based laser measurements (Jarecki and Müller, 2009).

ESA has started (launch 2009) the first dedicated gravity gradiometry mission called GOCE (*Gravity Field and Steady-State Ocean Circulation Explorer*, Fig. 5.38.), with a drag-free satellite in a sun-synchronous near circular orbit ($h = 265$ km, $i = 97^\circ$), Drinkwater and Haagmans (2007), Rummel et al. (2009), Rummel and Gruber (2010), also Rummel, 2011). Orbit determination is performed by satellite-to-satellite tracking, from the on-board dual-frequency GPS receiver (high-low mode positioning), and the satellite is also equipped with laser retroreflectors. Three accelerometer pairs (precision of a few $10^{-12} \text{ s}^{-2}/\sqrt{\text{Hz}}$, sampling rate 1 s) are arranged over three mutually orthogonal directions, with baselines of 50 cm, and Earth-pointing orientation (attitude control) is provided by star trackers and gradiometer data. While the diagonal element of the gradient tensor and the horizontal gravity gradient's component in flight direction (V_{xz}, V_{zx}) can be determined with high accuracy, the off-diagonal elements are less accurate due to specific constraints at ground-based pre-calibration. At modeling, the low-degree potential terms (up to about degree and order 50) will be determined primarily through orbital analysis from GPS tracking, while the higher degrees will be derived from the gradiometer measurements. Based on orbital data and gradiometer results, a first gravity model could be derived complete to degree and order 224, with an accuracy of better than 0.1 m (geoid) and $30 \mu\text{m s}^{-2}$ (gravity anomalies). Accuracies around 2 cm and $10 \mu\text{m s}^{-2}$, respectively, are expected for the full mission period originally planned for about 1.5 years (Pail et al., 2010a).

5.3 Geodetic astronomy

Classical geodetic astronomy is concerned with the determination of astronomic latitude, longitude, and azimuth from ground-based optical direction measurements to fixed stars, which also requires time determination (Mueller, 1969; Schödlbauer, 2000). Several types of observational instruments are available for this purpose [5.3.1], and different methods of observation have been developed [5.3.2]. A number of reductions are necessary in

order to refer the observations to the celestial reference frame [5.3.3]. Geodetic astronomy is based on astrometric methods and spherical astronomy (Eichhorn, 1974; Kovalevsky, 2002; Kovalevsky and Seidelmann, 2004).

The importance of *optical* astrometry has decreased since the development of efficient satellite positioning and gravity field determination methods, and is now restricted to more local applications of gravity field (plumb line direction, geoid) and azimuth determinations. On the other hand, *radio* waves emitted from extragalactic sources are used extensively in order to derive base-line vectors between fundamental terrestrial stations and to determine Earth orientation parameters: Very Long Base Line Interferometry [5.3.4].

5.3.1 Optical observation instruments

Optical observations to fixed stars are carried out in the local level (horizon) system. The direction to a star is determined by the astronomic azimuth A and the zenith angle z (sometimes the altitude or elevation angle $90^\circ - z$ is used), cf. [2.5]. Due to the relative movement of the observer with respect to the stars, simultaneous time measurements are required.

Time determination in optical geodetic astronomy requires an accuracy of 1 ms. This is provided by quartz clocks, which are based on quartz crystal oscillators (frequency stability 10^{-8} to 10^{-9} over a few hours) and synchronized by time signals. Nowadays a simple time measurement is possible with a GNSS receiver, cf. [5.2.5]. In order to record the time of a star transit through the horizontal or vertical thread of a telescope, a registration device has to be implemented in the measurement system.

Astronomic instruments are either permanently installed in observatories or constructed as transportable devices for field operation.

Until the 1980s, observations of highest precision with *stationary* instruments have been utilized by the former International Time Service and International Polar Motion Service. Among other instruments, the photographic zenith tube has been employed. In this case, stars near the zenith are photographed symmetrically with respect to the meridian, and the direction of the vertical was established by a mercury pool. By employing CCD-techniques, this method is still of significance for astronomy. Comparable precision ($0.05''$) was achieved by the Danjon prism astrolabe, measuring the transit time of stars crossing a defined almucantar (see also below under "prism astrolab"). These observatory measurements, in connection with satellite-based astrometry, still contribute to the realization of an optical celestial reference frame, cf. [2.4.1].

The *universal instrument* was employed for field measurements of first-order precision ($0.1''$ to $0.3''$). It consists of a high-precision theodolite, cf. [5.5.1], of very stable design with a few attachments for astronomic observations (Fig. 5.39).

An angled telescope permits observations near the zenith. The movable thread of the registering micrometer is driven to follow the star so that impulses are generated and recorded at uniform intervals. The suspension level serves to measure the tilt of the horizontal axis. The Horrebow level, mounted at right angles to the horizontal axis, registers any changes in the tilt of the telescope. The Kern DKM3-A and the Wild T4 universal theodolites were used widely.

The *prism astrolab* is used for the *simultaneous* observation of astronomic latitude and longitude. With this device, one measures the transit times of those stars that cross the



Fig. 5.39: Universal instrument Kern DKM3-A, Kern/Leica Geosystems AG, Heerbrugg, Switzerland.

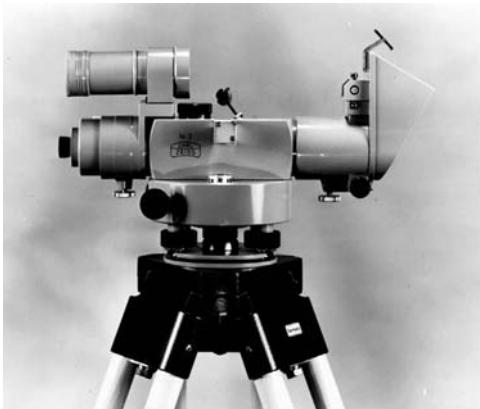


Fig. 5.40: ZEISS Ni2 level with prism astrolab, Carl Zeiss, Oberkochen, Germany.

same small-circle parallel to the horizon (almucantar). The constant zenith distance (usually $\approx 30^\circ$) is realized by a prism placed in front of the telescope, and the direction of the vertical is defined by the surface of a pool of mercury or by a compensator pendulum. Astrolabe attachments were particularly common. They have been mounted either on a theodolite (e.g., the Wild T3 astrolabe with a mercury pool) or on an automatic level (Zeiss Ni2 astrolabe, Fig. 5.40).

Transportable zenith cameras have been developed for the rapid determination of astronomic latitude and longitude, and have proved to be very efficient (Seeber and Torge, 1985; Kovalevsky, 2002). The development started with photographic instruments, consisting of a camera oriented in the direction of the plumb line (focal length 300 to 1000 mm, relative aperture $\approx 1:5$), which could be rotated around the plumb-line axis in any azimuth. The photography of the zenith-near field of stars with the subsequent (tedious) comparator measurement of the photographic plate coordinates has been substituted now by an electronic image procedure using CCD-technique, followed by the transformation into the astronomical system.

The principle of CCD (charge-coupled device) is based on the photoelectric effect produced on a semiconductor plate. The number of collected photoelectrons is proportional to the light received. A CCD-matrix is composed of a number of linear arrays and may contain several 1000×1000 pixels, of $10 \mu\text{m}$ or less size, with a resolution of 0.1 pixels.

In addition to the camera-system and a timing device, a digital zenith camera system contains two electronic tilt meters that are arranged at right angles to each other, and serve for the automatic alignment of the camera to the plumb line. A single observation comprises two images of zenithal stars, exposed in opposite camera directions, and the exposure epochs and tilt measurements. Using an image processing unit and a PC, an automatic on-line evaluation of the star observations is achieved, which includes the transformation of the CCD-coordinates into the α, δ -system, and results in the astronomic latitude and longitude of the observation site. Digital zenith camera systems have been developed over the past decades at a few institutions, and are now employed for the determination of vertical deflections along profiles or in areas of limited extension, cf. [6.7.4], Fig. 5.41. These systems include a GPS receiver which is used for time tagging of the exposure epochs and for determining geodetic latitude

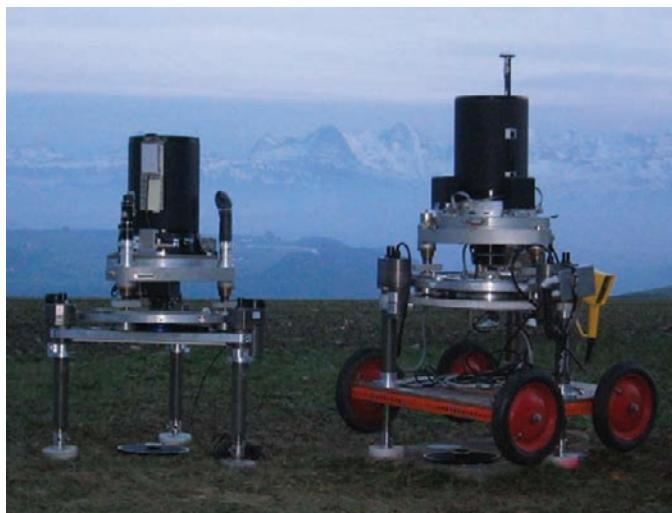


Fig. 5.41: Digital Astronomical Deflection Measuring System (DIADEM), Geodesy and Geodynamics Laboratory, ETH Zürich and Digital Transportable Zenith Camera, TZK2-D System, Institut für Erdmessung, Universität Hannover (Hirt and Bürki, 2006).

and longitude. Main error sources are of astrometric type (image centering, catalogue positions, scintillation), followed by tilt corrections, while errors of time tagging and geodetic coordinates play a minor role (Hirt and Bürgi, 2003; Hirt and Seeger, 2008).

With the Hannover Digital Zenith Camera System a single observation takes approximately 30s, and the image usually contains 20 to 50 stars. The evaluation results in an accuracy of about 0.2" to 0.3", which can be improved by multiple observations. With a one-hour observation time (100 observations) an accuracy of 0.05" to 0.1" is obtained.

5.3.2 Astronomic positioning and azimuth determination

The determination of astronomic latitude, longitude and azimuth is based on the relations given in [2.5], where the star positions (α, δ) are provided by star catalogues.

Star catalogues have been compiled since ancient times, cf. [2.4.1], and in a more regular manner since the nineteenth century. Derived from Earth-based astrometry, the number of stars observed and their positional accuracy had reached a certain limit in the second half of the twentieth century, examples are the AGK-catalogues (northern hemisphere) of the "Astronomische Gesellschaft" and the SAO (Smithsonian Astrophysical Observatory) Catalogue of 1966. These rather heterogeneous compilations finally included a few 100 000 stars, with accuracies not exceeding 0.1" ... 0.2". The HIPPARCOS space mission (since 1989) and the introduction of CCD-techniques significantly improved quantity and quality of star catalogues. The TYCHO catalogue (2000) is based on star-mapper data from the HIPPARCOS satellite, it contains about 2.5 million stars with an accuracy of 0.01" ... 0.02" (Høg et al., 2000). We further mention the UCAC Astrograph Catalogues of the U.S. Naval Observatory which provide positions with an accuracy between 0.02" and 0.1", for stars down to a magnitude of 16^m, and about 2000 stars per square degree (Zacharias et al., 2004). For future space missions as GAIA see [2.4.1].

As the relevance of astrometry in geodesy has decreased during the last decades, we mention here only a few of the many methods developed in geodetic astronomy.

In determining the *astronomic latitude* Φ , it is required, according to (2.20), to ascertain the zenith angle z and the hour angle h . The zenith angle can be directly observed, while the hour angle has to be derived from the rectascension α and the measured time, see (2.21).

By total differentiation of (2.20) we obtain differential formulas for estimating the effect of observational errors on the results and for finding optimum configurations for the observations, e.g., Schödlbauer (2000, pp. 34 and 505 ff.). For the latitude we obtain

$$d\Phi = -\frac{1}{\cos A} dz - \cos\Phi \tan A dh, \quad (5.53)$$

where we have neglected the (small) declination error. The accuracy of Φ hence strongly depends on the azimuth, with minimum effects of errors in z and h at $A = 0^\circ$ and $A = 180^\circ$, i. e., at meridian transits of the star.

For an upper culmination (the smaller zenith angle) of a northern star ($A = 0^\circ$) or a southern star ($A = 180^\circ$), the latitude is given by (see also Fig. 2.4)

$$\Phi = \delta_N - z_N \text{ and } \Phi = \delta_S + z_S, \quad (5.54)$$

respectively. Measuring the meridian zenith angle (e.g., to Polaris) is therefore most suitable for the determination of the latitude.

If one observes a pair of stars consisting of both a northern and a southern star having approximately the same zenith angle, averaging (5.54) significantly reduces the uncertainties in z due to refraction (*Sternbeck* method):

$$\Phi = \frac{1}{2}(\delta_N + \delta_S) + \frac{1}{2}(z_S - z_N). \quad (5.55)$$

In the *Horrebow-Talcott* method, the small difference between the meridian zenith angle of the northern and southern stars in a star pair is measured by a registering micrometer. The optical axis in each case is adjusted to the same zenith angle using the Horrebow level that is mounted on the horizontal axis. Since accurate circle and time readings are not required, this method provides precise results, with an accuracy of $0.1''$ when about 20 star pairs are observed.

The *astronomic longitude* Λ is given by the difference between the local sidereal time LAST and the Greenwich sidereal time GAST (2.22):

$$\Lambda = \text{LAST} - \text{GAST}, \quad (5.56)$$

where 1 s corresponds to $15''$. According to (2.21), LAST is related to the hour angle h :

$$\text{LAST} = h + \alpha. \quad (5.57)$$

If the latitude is known, h can be computed from the zenith angle according to (2.20):

$$\cos h = \frac{\cos z - \sin \Phi \sin \delta}{\cos \Phi \cos \delta}. \quad (5.58)$$

Converting measured universal time UT to GAST then allows the determination of Λ according to (5.56).

By differentiating (2.20), we get the differential relation for the hour angle:

$$dh = -\frac{dz}{\sin A \cos \Phi} - \frac{\cot A}{\cos \Phi} d\Phi. \quad (5.59)$$

The effect due to errors in z is minimum when observations are made on the prime vertical ($A = 90^\circ$), while the effect is zero for errors in Φ . The influence of refraction is largely eliminated when observing east and west stars of the same altitude that are symmetric with respect to the meridian. On the other hand, by observing the time of transit across the meridian ($h = 0$) we get $\text{LAST} = \alpha$. An accuracy of 0.01 to 0.02 s is obtained from approximately 30 transits.

The accuracy of the determination of longitude primarily depends on the systematic errors of the observer, the instrument, and the time comparison. If the determinations are made by the same observer, using the same instrument and the same time signal transmitting station as well as the same stars, then longitude differences are essentially free from these errors. Longitude determinations of high accuracy have thus been carried out as measurements of differences with respect to a reference station.

An economical method to determine the latitude and longitude simultaneously is known as the method of *position lines*.

The zenith angles z_1, z_2 of two stars $S_1(\alpha_1, \delta_1), S_2(\alpha_2, \delta_2)$ are observed at sidereal times $\text{LAST}_1, \text{LAST}_2$ and at azimuths A_1, A_2 . If S_1, S_2 are projected on the Earth's surface, then the intersections of the circles centered at the projections S'_1, S'_2 having radii z_1, z_2 represent two geometric positions P and (P) for the point of observation (Fig. 5.42). Near P , the circles can be replaced by their tangent lines (position lines), while the point (P) can be excluded from the solution if approximate coordinates are known. The intersection of the position lines then yields an approximation to P .

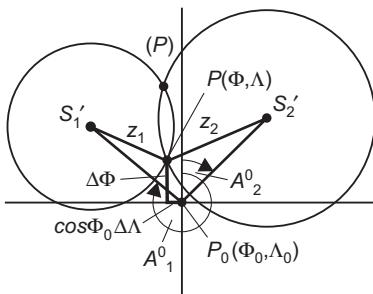


Fig. 5.42: Method of position lines.

Computationally, one obtains the corrections $\Delta\Phi = \Phi - \Phi_0$ and $\Delta\Lambda = \Lambda - \Lambda_0$ upon introducing an approximate position $P_0(\Phi_0, \Lambda_0)$. When observations are made with the prism astrolabe, cf. [5.3.1], the zenith angle predetermined by the prism is treated as an additional unknown. One obtains accuracies of a few $0.1''$ from about 20 stars evenly distributed above the horizon.

As explained in [5.3.1], a transportable *zenith camera* also permits the rapid and accurate simultaneous determination of latitude and longitude. From the coordinates α_z, δ_z of the zenith, derived from the observations, we obtain

$$\Phi = \delta_z, \quad \Lambda = \alpha_z - \text{GAST}, \quad (5.60)$$

see also Figs. 2.2, 2.4. Repeated observations with a digital camera system deliver an accuracy of better than $0.1''$, with further improvements at longer observation times.

If the latitude is known, then the *azimuth* A can be obtained, according to (2.20), from the hour angle h derived from the sidereal time and the rectascension (5.57):

$$\tan A = \frac{\sin h}{\sin \Phi \cos h - \cos \Phi \tan \delta}. \quad (5.61)$$

Differentiation of (2.20) yields

$$dA = \frac{\cos q \cos \delta}{\sin z} dh + \cot z \sin A \, d\Phi \quad (5.62)$$

where q is the parallactic angle, cf. [2.5]. An error in h has a minimum effect for $\delta \approx 90^\circ$ (stars near the pole). For some 10 observations, we get an accuracy of $0.3''$ to $0.5''$. The azimuth of a terrestrial station is obtained by additionally measuring the angle between the directions to the star and the target on the Earth's surface.

5.3.3 Reductions

In order to refer the “observed” positions (epoch t) of fixed stars to the system of the star catalogue (mean positions at the reference epoch t_0), several reductions have to be applied on the observed (topocentric) directions:

- *Astromic refraction* causes an apparent increase in the star’s altitude (Fig. 5.43). The true zenith angle z is obtained from the observed quantity z' by adding the astromic refraction angle Δz_∞ :

$$z = z' + \Delta z_\infty. \quad (5.63)$$

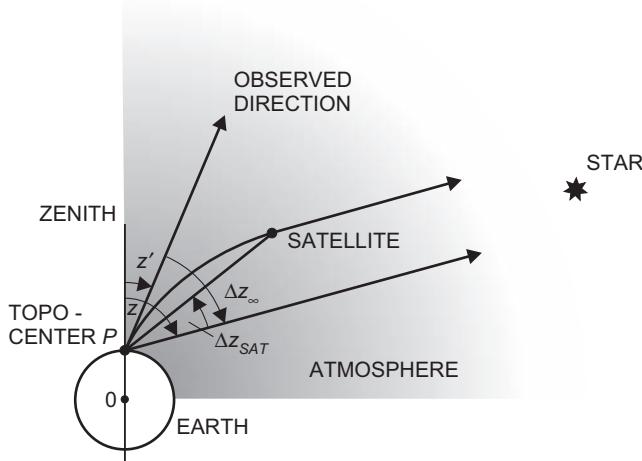


Fig. 5.43: Astronomic and satellite refraction.

According to (5.10) and (5.11), the refraction angle depends on the vertical gradient of the refractive index along the path of the ray. For a standard atmosphere (temperature 288.15 K, atmospheric pressure 1013.25 hPa), we obtain from Snell's law, and with a layered standard atmosphere for $z' < 70^\circ$:

$$\Delta z_0 = 57.08'' \tan z' - 0.067'' \tan^3 z'. \quad (5.64)$$

For actual conditions (temperature T , pressure p), we have the transformation

$$\Delta z_\infty = \Delta z_0 \frac{p}{1013} \frac{288}{T}, \quad (5.65)$$

(Kovalevsky, 2002). The uncertainty of Δz_∞ varies between a few 0.01" and a few 0.1" and depends strongly on systematic deviations from the atmospheric model (turbulences, slope of the atmospheric layers).

- The *diurnal aberration* is an apparent displacement in direction resulting from the finite velocity of light and the relative velocity of the observer with respect to the stars, due to the Earth's rotation. The corresponding latitude dependent reduction reaches a maximum of 0.3" at the equator.
- The *geocentric* (or diurnal) *parallax* represents the difference between the topocentric and the geocentric direction; it can be neglected for star observations.

Through these reductions, the "observed" position is transformed to the "apparent" position (apparent place) at epoch t . The reduction of the star *coordinates* from the "mean" position (epoch t_0) to the apparent position (epoch t) involves the following steps:

- Applying *precession* and *proper motion* (generally $<0.1''/\text{year}$, maximum $10''/\text{year}$) for the time interval $t - t_0$ transforms the mean position (t_0) to the mean position at epoch t , cf. [2.3.2], [2.4.3].
- Accounting for *nutation* transforms the mean position (t) to the true position (t). The origin of the system is still at the barycenter of the solar system.

According to the IAU2000 precession-nutation model, these two effects have been combined, but the separate treatment may continue for a certain time. The combined reduction now leads to the Intermediate Reference System, cf. [2.4.3], and the difference between “mean” and “true” coordinates disappears.

The transition to the (geocentric) apparent position (t) is performed by applying the following reductions:

- *Annual aberration*, resulting from the revolution of the Earth about the sun. It may reach values up to $20''$, and is calculated from the ephemerides of the sun and the Earth.
- *Annual parallax*, arising from the difference between the heliocentric and the geocentric directions. Its maximum value as obtained for a close star remains less than $0.8''$.
- The *relativistic light deflection* remains small and can be easily taken into account. For light rays passing the edge of the sun, it reaches the extreme value of $1.75''$.

Instead of reducing from the mean position (t_0) to the apparent position (t), the *apparent places* of fundamental stars for a particular year can be used. They can be drawn from astronomic almanacs, as the “Apparent Places of Fundamental Stars”, Astronomisches Recheninstitut Heidelberg.

Finally, we must consider that the results (astronomic latitude, longitude and azimuth) refer to the *instantaneous* spin-axis of the Earth. They are transformed into the IERS reference pole by applying reductions for polar motion, cf. [2.4.2]. Multiplying the polar motion rotation matrix (2.16b) with the unit vector of the local vertical (2.18) gives the corresponding *polar motion reductions* (Mueller, 1969, p. 86 ff.):

$$\begin{aligned}\Delta\Phi_p &= \Phi_{\text{ITRS}} - \Phi = -(x_p \cos\Lambda - y_p \sin\Lambda) \\ \Delta\Lambda_p &= \Lambda_{\text{ITRS}} - \Lambda = -(x_p \sin\Lambda + y_p \cos\Lambda) \tan\Phi, \\ \Delta A_p &= A_{\text{ITRS}} - A = -(x_p \sin\Lambda + y_p \cos\Lambda) \sec\Phi\end{aligned}\quad (5.66)$$

where x_p, y_p are the pole coordinates with respect to ITRS.

5.3.4 Very Long Baseline Interferometry

Extragalactic radio sources (quasars: quasi-stellar radio sources, radio galaxies) emit waves in the cm to dm range, which can be detected by large antennas (radio telescopes) used in radio astronomy. The approximate angular resolution of such a telescope is given by the wavelength/diameter ratio, and thus it is limited to a few arcmin for telescope diameters less than 100 m. By employing a receiving system of two widely (a few 1000 to 10 000 km) separated radio telescopes (baseline), the resolution can be increased to $0.001''$ and better: *Very Long Baseline Interferometry* VLBI (Moritz and Mueller, 1987, p. 381 ff.; Seeber, 2003, p. 485 ff.).

The wave train from an extragalactic radio source arrives at the telescope P_2 with a phase difference Φ with respect to the telescope P_1 . Φ is related to the time delay τ , the time the wave requires to travel the path difference $c\tau$ (c velocity of light in vacuum),

Fig. 5.44. Due to the Earth's rotation, Φ and τ depend on time t . The following relation is valid:

$$\Phi(t) = 2\pi \frac{c}{\lambda} \tau(t) = 2\pi v \tau(t), \quad (5.67)$$

where λ and v are the respective wavelength and the frequency of the received radio wave. We introduce the baseline vector

$$\mathbf{b}_{\text{ITRS}} = \mathbf{r}_2 - \mathbf{r}_1 = \begin{bmatrix} X_2 - X_1 \\ Y_2 - Y_1 \\ Z_2 - Z_1 \end{bmatrix}, \quad (5.68)$$

described in the terrestrial geocentric system ITRS (2.13) and the unit vector to the quasar:

$$\mathbf{s}_{\text{ICRS}} = \begin{bmatrix} \cos \alpha \cos \delta \\ \sin \alpha \cos \delta \\ \sin \delta \end{bmatrix}, \quad (5.69)$$

given in the celestial reference system ICRS (2.10). After transformation of \mathbf{s} to the terrestrial system, performed by means of the Earth orientation parameters according to (2.16), we obtain the time delay (see Fig. 5.44),

$$\tau(t) = -\frac{1}{c} \mathbf{b} \cdot \mathbf{s}(t). \quad (5.70)$$

The negative sign takes the direction of \mathbf{s} into account, which is opposite to the direction of wave propagation. By comparing the two wave trains received at P_1 and P_2 , interferences are obtained. The *frequency* of the interference *fringes* (maxima and minima) changes due to the Earth's rotation:

$$f(t) = \frac{1}{2\pi} \frac{d\Phi(t)}{dt}. \quad (5.71)$$

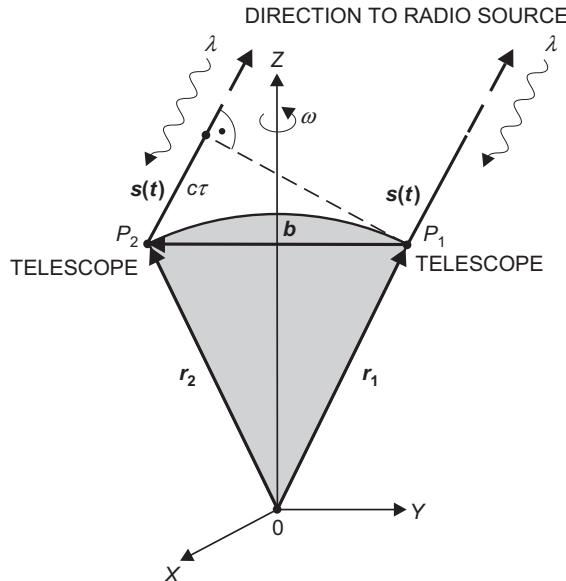


Fig. 5.44: Very long baseline interferometry.

With (5.67) and (5.70), the fringe frequency can be expressed as

$$f(t) = \nu \frac{d\tau(t)}{dt} = -\frac{\nu}{c} \mathbf{b} \cdot \dot{\mathbf{s}}(t), \quad (5.72)$$

$\dot{\mathbf{s}} = d\mathbf{s}/dt$. Equations (5.70) and (5.72) represent the VLBI *observation equations*. The complete observation equation will be found in the IERS Conventions 2010 (Petit and Luzum, 2010, p. 159 ff.).

The VLBI observables are the time delay τ (or the phase delay, respectively) which is regarded as the primary observation quantity, and the delay rate $d\tau/dt$. They are derived by a comparison of the digital signals received at each telescope. These signals are digitized, time-tagged and recorded on magnetic tapes or hard disks, the precise time being provided by hydrogen maser frequency standards. The transportation of the data to the few correlators available worldwide is mostly done still by courier service, but electronic data transfer is rapidly supporting and replacing this costly procedure. The correlation process consists of a relative shifting of the signals until a correlation maximum is found. The correlation function then furnishes the time delay and the delay rate for the two stations involved. The observable τ represents a group delay, while Φ is a phase delay, cf. [5.1.1], which involves the problem of ambiguity resolution, cf. [5.2.5]. The fringe frequency (delay rate) observation is free of this problem but of less importance due to its lower accuracy as compared to the delay observation, and since it allows only the determination of a reduced set of parameters. A VLBI observing session usually comprises between five to nine radio telescopes (Fig.5.45), which form geometrical networks between the baselines. Typically, about 50 radio sources are tracked several times over periods of 3–6 min, at the usual 24-h observation session.

Reductions are applied for the daily aberration, cf. [5.3.3], for systematic clock differences (clock synchronization), for the effects of the tropospheric refraction, cf. [5.1.2],



Fig. 5.45: 20m-radio telescope, Geodetic Observatory Wettzell, courtesy Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt a.M., Germany (<http://www.fs.wettzell.de>).

and for relativistic effects. The effect of the ionosphere is compensated for by observing in two frequency-bands, namely 2.3 GHz (S-band) and 8.4 GHz (X-band), cf. [5.1.3]. Main error sources result from timing (± 1 ps) and frequency instabilities ($\pm 10^{-15}$ over a few days) as well as from tropospheric models (MacMillan and Ma, 1997). The determination of the “wet” component plays a major part in this aspect. Attempts have been made to measure the water vapor content along the signal path by water vapor radiometers in order to estimate the wet component with cm-accuracy, cf. [5.1.2]. The vertical baseline component is mainly affected by the uncertainty of the wet component, and by atmospheric pressure loading. Special care is required with respect to the definition of the telescope’s reference point, its connection to a ground marker, and the control of the antenna’s thermal deformation (Nothnagel, 2008).

Among the *parameters* to be estimated from (5.70) and (5.72) are the components of the baseline vector in the terrestrial reference system (few mm-precision at a 24 h session). Global solutions for a given epoch deliver a corresponding accuracy for the station coordinates, and a mm/year and better accuracy for station velocities; they also contribute to the determination of the scale of the terrestrial system. Another VLBI product are the Earth orientation parameters, entering through the transformation between the terrestrial and the celestial system, cf. [2.4.3]. From a 24 h-session, the pole coordinates and Universal Time UT1 can be determined with an accuracy of better than 30 to 100 μ as and 5 to 10 μ s, respectively; corrections to the precession and nutation models can be derived with comparable accuracy (Vennebusch et al., 2007). Solutions derived from a few hours observation time are less accurate by a factor of two or three.

VLBI for geodetic and astrometric purposes started in the 1970s (Shapiro, 1978; Campbell and Witte, 1978). Today, about 40 radio telescopes (some of mobile type) with antenna diameters from 3 m to 100 m) cooperate within the framework of the International VLBI Service for Geodesy and Astrometry (IVS), and six correlators are available for processing the raw VLBI data (Schlüter and Behrend, 2007), Fig. 5.46. This network provides the celestial reference frame ICRF, and contributes to the maintenance of the terrestrial reference frame ITRF, including the determination of the Earth orientation parameters, cf. [2.4.1] to [2.4.3]. The stations are mainly located in North America, Europe, and Japan, but the global coverage has been strengthened in the last time (Fig. 5.46). As an example, the U.S. Very Long Baseline Array VLBA (National Radio Astronomy Observatory/National Science Foundation) consists of ten 25 m-antennas spread over the US territory, and is operating since 1994. The results obtained include seasonal signals at the mm-order and a number of co-seismic deformations, occurring at tectonic plate boundaries (Petrov et al., 2009).

Mobile radio telescopes have been developed for rapid surveying of regions with recent crustal movements, such as California or the Eastern Mediterranean, and to fill gaps of the terrestrial reference frame in the southern hemisphere. We mention the antenna, incorporated in the Transportable Integrated Geodetic Observatory (TIGO), Fig 5.47, operating since 2002 within a German-Chilean cooperation project at Conception/Chile (Nothnagel et al., 2004). Future VLBI development is directed towards increased accuracy (1 mm for baselines and 0.1 mm/year for station velocities) and more continuous measurements, with near real-time solutions for the Earth orientation parameters (Behrend et al., 2009). One strategy in this direction is the installation of a “twin”-telescope, e.g., at the Geodetic Observatory Wettzell, consisting of two identical telescopes (13 m diameter) with improved optics and fast moving capability (Hase et al., 2008).



Fig. 5.46: Radio telescopes participating in the International VLBI Service for Geodesy and Astrometry IVS (status 2010), <http://ivscc.gsfc.nasa.gov>.



Fig. 5.47: 6m-radio telescope as part of the Transportable Integrated Geodetic Observatory (TIGO), courtesy Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt a.M., Germany (<http://www.fs.wettzell.de>).

5.4 Gravimetry

Gravimetry deals with the measurement of the gravity intensity (gravity) and the gravity gradient by terrestrial methods on or close to the Earth's surface (Marson and Faller, 1986; Torge, 1989; Timmen, 2010). "Absolute" gravity measurements refer directly to the standards of length and time [5.4.1], while modern "relative" measurements use a counter-force for the determination of gravity differences [5.4.2]. A conventional gravity reference system is needed in order to provide a global standard of high metrological quality, serving as a basis for global, regional and local gravity measurements [5.4.3]. Gravity measurements on moving platforms permit the economic survey of areas difficult to access [5.4.4]. Local gravity-field information can be obtained by the measurement of the gravity gradient [5.4.5]. The continuous record of gravity provides temporal gravity variations at different time scales, especially the effects of solid Earth tides [5.4.6].

The *unit* of gravity in the SI-system is ms^{-2} . The units $\text{mGal} = 10^{-5} \text{ ms}^{-2}$ and $\mu\text{Gal} = 10^{-8} \text{ ms}^{-2} = 10 \text{ nms}^{-2}$ are still in widespread use in geodesy and geophysics. They are derived from the unit *Gal* (after Galilei) of the former cgs-system and serve for a simple description of gravity field differences resp. measurement accuracy. The unit of the *gravity gradient* components is s^{-2} . In view of the magnitude of the components and the obtainable accuracy, the components are generally expressed in $10^{-9} \text{ s}^{-2} = \text{ns}^{-2}$, traditionally called *Eötvös unit* (*E*).

5.4.1 Absolute gravity measurements

An "absolute" gravity measurement determines the gravity g from the fundamental acceleration quantities length and time. We distinguish between the pendulum and the free-fall method, both going back to *Galileo Galilei* (1564–1642), see Faller and Marson (1988), Niebauer (2009).

The *pendulum method* is no longer applied today but governed gravimetry for about 300 years. Because of its fundamental importance, and because more recent results are still part of some gravity networks, a short introduction is given here.

The pendulum method is based on the measurement of the period and the length of a freely swinging pendulum. For a *mathematical* pendulum (point mass m suspended on a weightless wire of length l) we have the equation of oscillation

$$ml\ddot{\varphi} + mgsin\varphi = 0, \quad (5.73)$$

with the phase angle $\varphi = \varphi(t)$, and the angular acceleration $\ddot{\varphi} = d^2\varphi/dt^2$ (Fig. 5.48). Integration over a full period leads to an elliptical integral. After expansion into a series, we obtain the period T of oscillation

$$T = 2\pi\sqrt{\frac{l}{g}} \left(1 + \frac{\varphi_0^2}{16} + \dots\right), \quad (5.74)$$

where the amplitude φ_0 is kept small. Thus, gravity is derived from the measurement of T and l .

The mathematical pendulum is difficult to realize. But equations (5.73) and (5.74) also hold for a *physical* pendulum if l is replaced by the reduced pendulum length

$$l_r = \frac{l}{ma}. \quad (5.75)$$

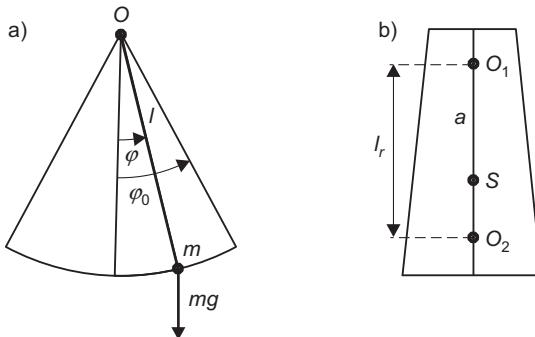


Fig. 5.48: Absolute pendulum method: a) mathematical pendulum, b) reversible pendulum.

Here, J is the moment of inertia with respect to the axis of rotation O , m the total mass, and a the distance between O and the center of mass S . The *reversible pendulum* is characterized by two axes of rotation, for which, after a corresponding adjustment, the same oscillation time is achieved. The distance between the two axes is then equal to the reduced pendulum length, thus avoiding the direct determination of J , m , and a (Fig. 5.48).

Early pendulum measurements using mathematical pendulums were carried out at the classical arc measurements of the eighteenth century, and also with respect to the introduction of a “natural” unit for length (*Borda* and *Cassini* in Paris, 1792; *Bessel* in Berlin, 1835), cf. [1.3.2]. The reversible pendulum was introduced by *Henry Kater* (1818), and a limited number of observations were carried out, primarily after the 1860s (transportable devices by *Repsold*, *Brunner*, and others). After the fundamental gravity determination in Potsdam, cf. [5.4.3], only a few more experiments were performed in the twentieth century. The accuracy achieved finally remained at a few μms^{-2} , which is mainly due to problems in determining the length of the swinging pendulum, and keeping the pendulum length constant over an observation set comprising a large number of oscillations (Schüler et al., 1971).

The *free-fall method* is based on the equation of motion

$$m\ddot{z} = mg(z) \quad (5.76a)$$

of a freely falling body. Here m is mass; z is along the local vertical axis, and $\ddot{z} = d^2z/dt^2$ (Fig. 5.49). Assuming a *homogeneous* gravity field along the falling distance, double integration of (5.76a) yields the free-fall equation

$$z = z_0 + \dot{z}_0 t + \frac{g}{2} t^2. \quad (5.76b)$$

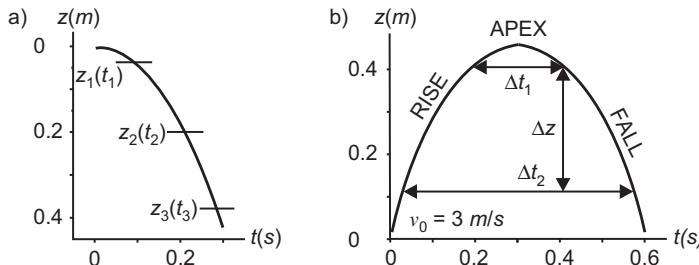


Fig. 5.49: Distance-time diagram: a) free-fall method, b) symmetrical rise and fall.

Equation (5.76b) relates the position z of the falling body at the time t to gravity. The integration constants z_0 and \dot{z}_0 represent z and $\dot{z} = dz/dt$ at the starting time of the experiment ($t = 0$). These quantities slightly deviate from zero, due to problems in accurately defining the starting position (resting position of the gravity center of the test mass at the start of the experiment) and small microseismic accelerations.

If at least three position/time pairs are measured, z_0 and \dot{z}_0 can be eliminated in (5.76b), and gravity is given by

$$g = 2 \frac{(z_3 - z_1)(t_2 - t_1) - (z_2 - z_1)(t_3 - t_1)}{(t_3 - t_1)(t_2 - t_1)(t_3 - t_2)}. \quad (5.77)$$

For the *symmetrical rise and fall*, the test mass is thrown vertically upward and falls back after having reached the apex (Fig. 5.49). Now, it is sufficient to measure time at the same two positions during rise and fall. Evaluation of (5.76a) then yields

$$g = \frac{8\Delta z}{\Delta t_2^2 - \Delta t_1^2}, \quad (5.78)$$

with $\Delta z = z_2 - z_1$, $\Delta t_1 = t_3 - t_2$, $\Delta t_2 = t_4 - t_1$.

With modern technology (see below), considerably more than the necessary number of position/time pairs is measured at one site. A least-squares adjustment of (5.76b) then provides the parabolic fitting curve, and also z_0 and \dot{z}_0 .

Present accuracy also requires that the gravity change along the falling distance has to be taken into account (*non-homogeneous* gravity field) by introducing $\partial g/\partial z = g_z$. Equation (5.76a) then reads as

$$m\ddot{z} = m(g_0 + g_z z), \quad (5.79a)$$

with $g_0 = g$ at the resting position $z = 0$. Double integration now leads to

$$z = \frac{g_0}{g_z} (\cosh \sqrt{g_z} t - 1), \quad (5.79b)$$

for $z_0 = \dot{z}_0 = 0$. A series development of z (up to order t^4) with inclusion of z_0 , \dot{z}_0 gives the observation equation (Cook, 1965)

$$z = z_0 \left(1 + \frac{1}{2} g_z t^2 \right) + \dot{z}_0 \left(t + \frac{1}{6} g_z t^3 \right) + \frac{1}{2} g_0 \left(t^2 + \frac{1}{12} g_z t^4 \right) + \dots \quad (5.79c)$$

The vertical gradient is generally determined independently by repeated relative gravity measurements along a vertical tripod, and the adjusted final gravity value is referred to a fixed reference height (with minimum effect of vertical gradient error!), e.g., 1.2 m at the FG5 gravimeter (Timmens, 2003).

Accuracy demands for absolute gravimetry are at the order of 10^{-9} g or 10^{-8} ms $^{-2}$. Hence, according to (5.76b), for a falling distance of 0.2 m (falling time 0.2 s), accuracies of 0.2 nm and 0.1 ns are required for position and time, respectively. This is achieved by interferometric distance measurements and simultaneous electronic timing.

For recent free-fall gravimeters, a polarization or iodine stabilized He-Ne gas laser ($\lambda = 633$ nm) serves as the length standard and an atomic (rubidium) frequency normal as the time standard. A Michelson interferometer is used for the distance measurement, with two corner-cube reflectors as the main components (Fig. 5.50). One of the reflectors is fixed and serves as a reference; the other one represents the falling body (test mass). By splitting the laser light into a measurement and a reference beam, and superimposing

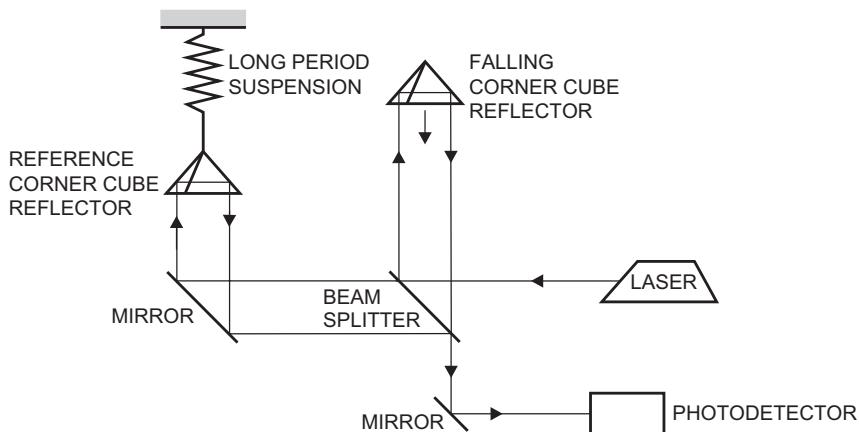


Fig. 5.50: Michelson interferometer principle.

them again after parallel reflection, light interferences occur. The zero crossings of this fringe signal have a distance of $\lambda/2$, and the fringe frequency increases with time due to the velocity increase of the test mass according to $\dot{z}(t) = gt$ (Fig. 5.51). The zero crossings are sensed by a photodiode, converted to an electronic signal, amplified, triggered, and counted. A time measurement (atomic clock and time interval counter) is carried out after a preset number n of zero crossings, which corresponds to a falling distance of

$$\Delta z = n \frac{\lambda}{2}. \quad (5.80)$$

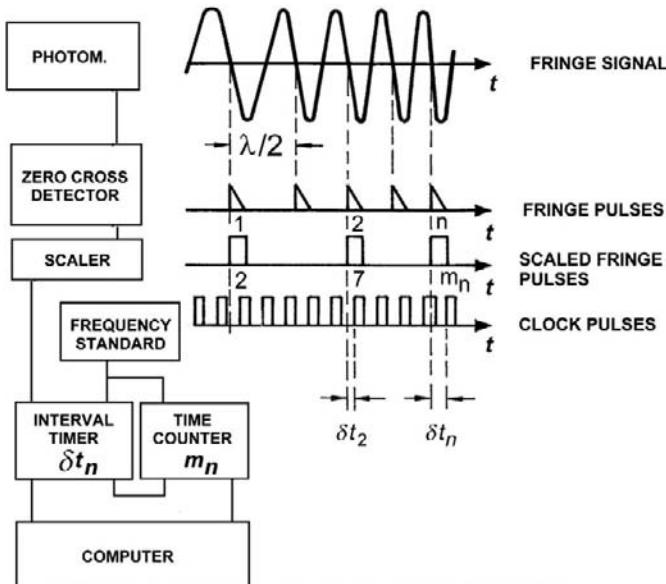


Fig. 5.51: Timing of scaled fringe pulses, after Zumberge et al. (1982).

The experiments are performed in vacuum (10^{-4} Pa) in order to eliminate air resistance. Microseismicity is to a large part absorbed by long-period ($T > 10$ s) compensation devices. A further reduction is achieved by randomization, performing a large number (several 100 to a few 1000) of drops per station. For the *rise and fall* method, systematic errors that are proportional to the falling body's velocity (residual air drag, timing errors) cancel to a large degree according to (5.78). On the other hand, the rise and fall method is handicapped by the problems which arise at the realization of a perfect vertical trajectory.

Several *reductions* have to be applied to the observed gravity values. The *gravimetric tides* being caused by the Earth's body and ocean tides, can be reduced with an accuracy of a few $0.01 \mu\text{ms}^{-2}$ or better in most parts of the world, cf. [8.3.6]. The *polar motion* reduction ("gravity pole tide"), according to (3.109) and (5.66), is given by

$$\delta g_{\text{pole}} = -\delta_{\text{pole}} \omega^2 R \sin 2\varphi (x_p \cos \lambda - y_p \sin \lambda), \quad (5.81\text{a})$$

where ω is the rotational velocity of the Earth, R the Earth's radius, and x_p and y_p the coordinates of the instantaneous pole with respect to the IERS reference pole. The geodetic coordinates φ, λ sufficiently approximate astronomic latitude and longitude. The factor $\varphi_{\text{pole}} = 1.16$ accounts for the Earth's elasticity, cf. [5.4.6].

The direct (gravitation) and indirect (deformation) effect of *air pressure* variations is taken into account by a reduction

$$\delta g_p = 3(p - p_n) \text{nms}^{-2}, \quad (5.81\text{b})$$

with p being the actual air pressure, and p_n the normal air pressure as given by a standard atmosphere, cf. [5.1.1], both in hPa (Nebauer, 1988). Current weather conditions may cause larger deviations from the global regression factor used in (5.81b). Improvements are possible by means of local/global weather data and deformation models (Gitlein and Timmen, 2007), cf. [8.3.1]. Finally, the *finite velocity of light* c must be taken into account by adding the term z/c to the observed time values. The reduction of the adjusted gravity value from the *reference height* to the *ground mark* is performed by relative gravity measurements, with an accuracy of 0.01 to $0.02 \mu\text{ms}^{-2}$, cf. [5.4.5].

The long-term *stability* of the length and time standards is controlled by calibration of the laser (10^{-9} to 10^{-10} frequency stability) and the atomic clock (10^{-10}). The *repeatability* of the gravimeter system (hard- and software) can be checked by regular measurements at a reference station, (Fig. 5.52), the data may be systematically biased by

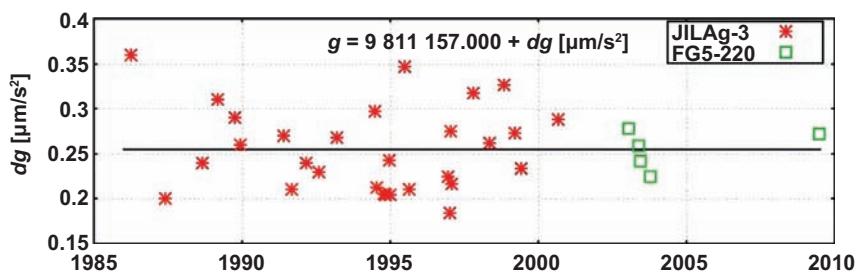


Fig. 5.52: Long-term stability control of JILAG-3 and FG5-220 absolute gravimeters at station Clausthal, Germany (hard bedrock). An instrumental offset of $-0.09 \mu\text{ms}^{-2}$ was applied to the JILAG-3 results, after Timmen (2010).

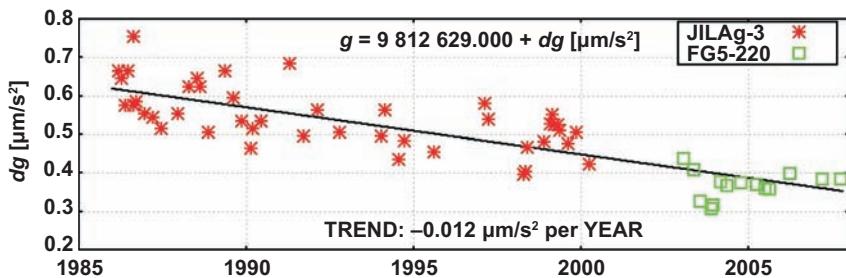


Fig. 5.53: Long-term repeatability of JILAg-3 (offset corrected) and FG5-220 absolute gravimeters at station Hannover/Germany (glacial sediments close to a river-bed), after Timmen (2010).

environmental effects (Fig. 5.53). The accuracy of the absolute gravimeter results, on the other hand, can be estimated only by comparisons with other instruments, with possibly different design and evaluation procedure, cf. [5.4.3].

The accuracy of absolute gravity measurements strongly depends on site conditions. Stable sites (hard bedrock, low man-made noise) provide better results than locations in sediments, close to the coast, or in urban environment. The drop-to-drop scatter (0.05 to a few $\mu\text{m/s}^2$) is reduced by a large number of measurements. The adjusted station gravity-value (generally several 1000 drops distributed over 1 to 3 days) is derived with a standard deviation of 0.01 to $0.03 \mu\text{m/s}^2$. The accuracy is at the order of a few $0.01 \mu\text{m/s}^2$, due to unmodeled instrumental effects (e.g., floor recoil, electronic phase shift, laser instabilities) or environmental “noise” (atmospheric loading, groundwater table variations etc.). Systematic discrepancies (“offsets”) between different instruments may reach $0.05 \mu\text{m/s}^2$ and more, cf. [5.4.3].

The free-fall method was developed in the 1950s (*Volet and Sakuma* at the BIPM Sèvres, *Cook* at the National Physical Laboratory, Teddington). A first transportable instrument was designed by *Faller* in 1968 and employed at the establishment of a worldwide gravity net, cf. [5.4.3], it was followed by a small series of operational JILA (Joint Institute for Laboratory Astrophysics, Boulder, CO, U.S.A.) gravimeters (Faller et al., 1983). A commercial absolute gravimeter version is available now with the FG5 (Micro-g LaCoste, Inc., U.S.A.) free-fall instrument (Nebauer et al., 1995). With these instruments, around 200 (JILA gravimeter) respectively 700 (FG5 gravimeter) position/time data pairs are collected over one drop, which are evenly distributed in distance over the drop length of 20 cm, and adjusted on-line to a fitting parabola. The time interval between two drops is between 10 and 30 s, which includes the reset of the falling corner-cube and the online adjustment. The falling object moves in a co-accelerated “drag-free” chamber. The chamber eliminates residual air drag and serves, by adequate acceleration, for dropping and catching the corner-cube as well as for transporting it back to the initial position. The reference corner-cube is isolated from ground motions by a “super-spring”, which by a feed-back system electronically generates effective free-oscillation periods between 30 and 60 s. While the JILA gravimeters have a horizontal interferometer basis, the FG5 instruments employ the Mach-Zender interferometer arrangement. Here, the falling and fixed corner-cube are arranged in the vertical, with corresponding laser beam splitting (Figs. 5.54, 5.55). The vertical basis strongly reduces the influence of floor recoil and tilt on the optical path length. The iodine-stabilized laser is separated from the instrumental vibrations induced by dropping, by routing the laser light through a fibre optic cable to the interferometer base. The instruments are

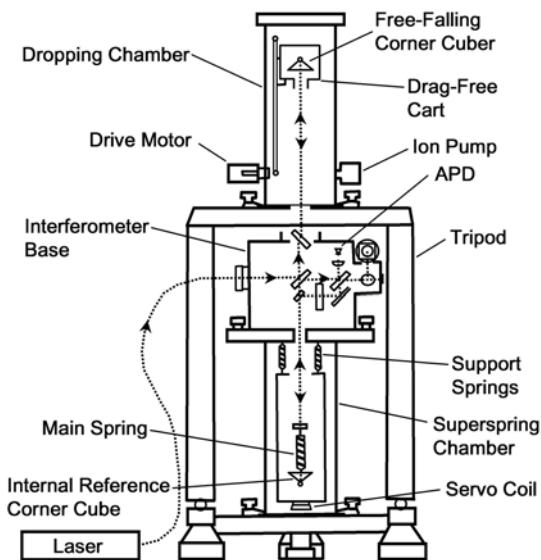


Fig. 5.54: Free-fall gravimeter FG5 principle, courtesy Micro-g – A, Division of LRS, Lafayette, CO, U.S.A.



Fig. 5.55: Free-fall gravimeter FG5 view, courtesy Micro-g Lacoste – A Division of LRS, Lafayette, CO, U.S.A.

disassembled for transportation (FG5: 240 kg in eight containers). Setting up at a station requires about 2 h, and observations (e.g., 1500-3000 computer-controlled drops, subdivided into sets of 50 drops each) are generally carried out over 1 to 3 days, depending on local noise (Torge et al., 1987; Timmen, 2010). A portable modification (drop length 0.15 m) of the FG5 gravimeter (A-10 absolute gravimeter) can be used in outdoor environment on quiet sites. It allows a sampling rate of 1 Hz, and provides a precision of $0.1 \mu\text{ms}^{-2}$ after 10 min of operation (Liard and Gagnon, 2002), Fig. 5.56. Other absolute gravimeter developments (e.g., in Russia, Japan, China) also date back to the 1970s, and partly also operated worldwide (e.g., the gravimeter of the Institute of Automation and Electrometry, Siberian Branch, Russian Academy of Sciences).

Based on the research work of Sakuma at BIPM, transportable *rise-and-fall* instruments have been developed at the Istituto Nazionale di Ricerca Metrologica (formerly Istituto di Metrologia "G. Colonnelli" IMGC), Torino, Italy (Alasia et al., 1982) and by Jaeger S.A., France (Sakuma, 1983). The recent IMGC-02 construction is highly operational and applied, among others, for the investigation of active volcanoes. The rise-and-fall range amounts to 20 cm, and the reference reflector is fixed to a 20 s-seismometer. With a launch carried out every 30 s, the result of a 12 h-observation session is better than $0.1 \mu\text{ms}^{-2}$ (D'Agostino et al., 2008).

Cold atom gravimeters represent a promising alternative to the corner cube free fall instruments (Kasevich and Chu, 1992). At this method, a source of cooled atoms is introduced into a free-fall chamber, and the free-fall acceleration of the atoms is measured by atomic interferometry. There are no moving parts which can wear off, and measurements can be performed with a high repetition rate (e.g., 3 Hz). A transportable device developed at LNE-SYRTE, Paris, already provides an accuracy of a few $0.01 \mu\text{ms}^{-2}$ from a 1-night observation series (Merlet et al., 2010).



Fig. 5.56: Portable absolute gravimeter A-10, courtesy Micro-g LaCoste – A Division of LRS, Lafayette, CO, U.S.A.

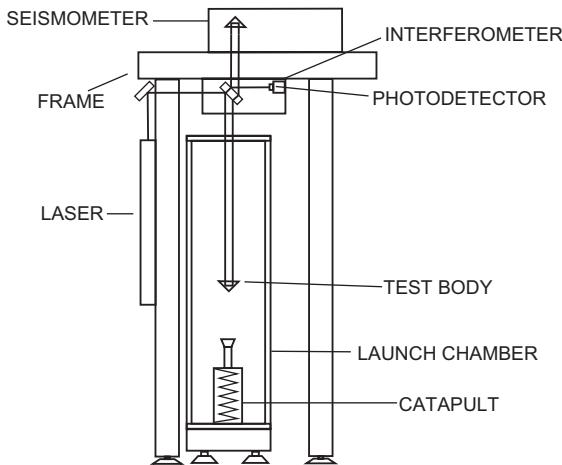


Fig. 5.57: Rise and fall transportable absolute gravimeter IMGC-02 principle, modified after D'Agostino et al. (2008).

5.4.2 Relative gravity measurements

“Relative” gravity measurements yield the gravity differences between different stations or – if carried out in the stationary mode – the variations of gravity with time, cf. [5.4.6]. Either time or length is measured, keeping the other quantity fixed. As a consequence, relative measurements can be performed more easily than absolute ones.

For the *pendulum method*, the oscillation periods T_1 and T_2 of the same pendulum are measured at two stations P_1 and P_2 . From (5.74) we obtain

$$\frac{g_2}{g_1} = \frac{T_1^2}{T_2^2} \quad (5.82)$$

or, after simple transformation, the gravity difference

$$\Delta g_{1,2} = g_2 - g_1 = -2g_1 \frac{T_2 - T_1}{T_2} + g_1 \frac{(T_2 - T_1)^2}{T_2^2}. \quad (5.83)$$

“Relative” pendulum measurements were carried out already at the first modern arc measurements (*Bouguer, Maupertuis* and others) and at the marine expeditions of the early nineteenth century (*Sabine, Biot* and others). At these surveys, the “mathematical” and the *Kater* reversible pendulum were used in the relative mode, in order to derive the gravity differences to “reference” stations as the Paris or Greenwich Observatory, cf. [5.4.1]. The method was employed extensively since *R.v. Sterneck* (1887) developed a transportable device (pendulum length 25 cm, two pendulums swinging on the same support in opposite phase in order to eliminate floor recoil effects). Although the systematic effects that are independent of time and position cancel with this differential method, the accuracy could not be increased over a few μms^{-2} due to problems in keeping the pendulum length constant during a field survey. The pendulum method was superseded in the 1930s by relative measurements employing elastic spring gravimeters (see below). Nevertheless, the method was still used until the 1960s for establishing gravimeter calibration lines, exploiting the fact that pendulum results are given in the unit of acceleration and do not need to be calibrated.

Relative *gravity meters* use a counterforce in order to keep a test mass in equilibrium with gravity. Gravity changes in space or time are monitored by corresponding changes of the counterforce, which are transformed to the gravity unit by a calibration function. An elastic counterforce is used at most constructions, but magnetic counterforces are also employed, mainly in instruments operating on moving platforms and in the stationary mode, cf. [5.4.4], [5.4.6].

The *elastic spring gravimeter* is based on the principle of a spring balance. If gravity changes, the spring length will also change in order to maintain static equilibrium between gravity and the elastic force. According to *Hooke's law*, the strain is proportional to the stress for small elongations. We distinguish between translational and rotational systems.

In a *translational system* (vertical spring balance), the condition of equilibrium is given by (Fig. 5.58a)

$$mg - k(l - l_0) = 0, \quad (5.84)$$

where k is the spring constant and l (resp. l_0) is the length of the spring with (resp. without) load. Applying (5.84) on a gravity difference Δg furnishes a linear relationship between Δg and the observed difference in length Δl :

$$\Delta g = \frac{k}{m} \Delta l = \frac{g}{l - l_0} \Delta l. \quad (5.85)$$

An undamped spring generates a harmonic oscillation with the proper frequency

$$\omega_0 = \sqrt{\frac{k}{m}} \quad (5.86)$$

and the oscillation time

$$T_0 = 2\pi \sqrt{\frac{m}{k}} = 2\pi \sqrt{\frac{l - l_0}{g}}. \quad (5.87)$$

By differentiation, we obtain the mechanical *sensitivity*

$$\frac{dl}{dg} = \frac{m}{k} = \frac{T_0^2}{4\pi^2}. \quad (5.88)$$

In order to assess gravity changes with a relative accuracy of 10^{-8} , length changes of a 0.1 m long spring would have to be determined to 1 nm.

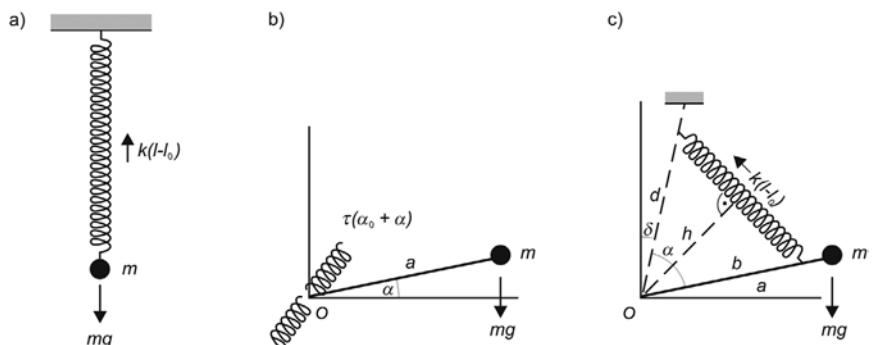


Fig. 5.58: Elastic spring gravimeter principle: a) vertical spring balance, b) lever torsion spring balance, c) general lever spring balance.

Rotational systems (lever spring balance) consist of a lever that supports a mass m and rotates about an axis O . Equilibrium can be obtained through a horizontal torsion spring or through a vertically or obliquely acting helical spring. The equilibrium of the torques for the *lever torsion spring balance* (Fig. 5.58b) yields

$$mg \cos \alpha - \tau(\alpha_0 + \alpha) = 0, \quad (5.89)$$

where a is the length of the lever, α the angle between the horizontal and the lever, τ the torsion constant, and α_0 the pretension angle of the spring. This non-linear system becomes a linear one for $\alpha = 0$, with

$$\Delta g = \frac{\tau}{ma} \Delta \alpha. \quad (5.90)$$

For the *general lever spring balance*, the spring counterforce acts under an arbitrary angle on the lever carrying the mass. The line connecting the rotation axis O with the upper point where the spring is mounted deviates by an angle δ from the vertical (Fig. 5.58c). With the vertical distance

$$h = \left(\frac{bd}{l} \right) \sin \alpha \quad (5.91a)$$

between the axis of rotation and the spring, the equilibrium condition for the torques reads

$$mga \sin(\alpha + \delta) - kbd \frac{l - l_0}{l} \sin \alpha = 0. \quad (5.91b)$$

The sensitivity of this non-linear system can be significantly increased by approximating the torques of gravity and of the elastic spring (astatization). With a zero-length spring ($l_0 = 0$), we have the sensitivity

$$\frac{d\alpha}{dg} = \frac{\sin(\alpha + \delta) \sin \alpha}{g \sin \delta}. \quad (5.92)$$

High sensitivity is achieved at a small angle δ and $\alpha \approx 90^\circ$. For $a = 0.1$ m, $\alpha + \delta = 90^\circ$, and $\delta = 100''$, displacements have to be measured with a precision of 2 μm in order to obtain a relative accuracy of 10^{-8} . Compared to the linear system, the sensitivity is thus increased by a factor of 2000.

The required accuracies of $0.1 \mu\text{ms}^{-2}$, or better, place high demands on the reading systems as well as on the stability of the counterforce with time.

Optical and/or electrical reading systems are used to observe the position of the test mass. A capacitive position-indicator is usually employed and is connected to a digital readout unit. The *zero-method* is preferred for the measurement of the displacement, with a compensation device for restoring the zero position. Mechanical compensation is performed by a measurement screw. Since the 1980s, electronic feedback systems are preferred as they are not affected by screw errors (Röder et al., 1988).

The *elasticity* of the spring should exhibit a time stability of 10^{-8} over several hours, which is the time interval required for transporting the gravimeter between the stations of a large-scale network, cf. [7.4]. Spring materials include NiFe alloys (small thermo-elastic coefficient) and fused quartz (large but linear thermoelastic coefficient, small coefficient of thermal expansion, less sensitivity to mechanical shocks). In addition, the measurement system has to be protected against changes in temperature (thermostat), air pressure (air-tight sealing), and magnetic field (shielding of metal alloy springs). The effects of mechanical shocks and vibrations can be reduced by a damping device, in addition to air-damping.

Spring gravimeters have been developed since the 1930s for use in geophysical exploration. From the 1950s, instruments were available which could be used for establishing large-scale gravity networks (Woollard, 1950). Most of these early gravimeters had a limited measuring range (e.g., $2000 \mu\text{ms}^{-2}$) and required a reset screw for changing to another gravity range (Askania gravimeter: torsion spring balance, metal alloy; Worden gravimeter: fused quartz system with horizontal beam and vertical counter spring). The LaCoste and Romberg astatized gravimeters employ a metal alloy zero-length spring, acting at 45° inclination on the horizontal beam (model G: $70000 \mu\text{ms}^{-2}$ range, measuring screw with $10 \mu\text{ms}^{-2}$ per one rotation), Krieg (1981), Kanngieser (1983). Recently developed instruments are microprocessor-controlled and are highly automated. They employ capacitive transducers and electronic feedback systems with worldwide range (Valliant et al., 1986). Self-leveling by electronic levels, a high data acquisition rate (e.g., 1 s-reading cycle and 30 s-sampling over 15 min) and on-line evaluation (automatic data compression and analysis, Earth tides reduction, drift control and correction) are further characteristics of these state-of-the-art instruments. We mention the Scintrex CG-3 and CG-5 Autograph gravimeters (non-astatized linear fused-silica system with vertical spring, pick-off resolution 0.2 nm, world-wide range, constant calibration factor and no periodic errors (Timmen and Gitlein, 2004) and the automated Burris Gravity Meter of ZLS Corporation based on the LaCoste and Romberg system, with a digital feedback range of $500 \mu\text{ms}^{-2}$ (Jentzsch, 2008), Figs. 5.59, 5.60.

Options of conventional land gravimeters include underwater and bore-hole instruments. After sealing in a pressure and water protected diving bell, an *underwater gravimeter* is



Fig. 5.59: ZLS Burris Gravity Meter, courtesy ZLS Corporation, Austin, TX, U.S.A.



Fig. 5.60: Scintrex Autograph CG-5 Gravity Meter, courtesy Scintrex, Concord, Ontario, Canada.

lowered to the sea bottom and remotely operated from on board a survey vessel. Underwater gravimeters have been used since several decades, mainly in the shelf areas at water depths less than 200 m (Beyer et al., 1966). A remotely operated deep ocean seafloor gravimeter has been developed recently using three gravity sensors (Scintrex CG-3M) in one watertight pressure case, with motorized gimbals for leveling and quartz pressure gauges for depth information. Repeated measurements atop seafloor benchmarks yielded a repeatability of better than $0.1 \mu\text{ms}^{-2}$ (Sasagawa et al., 2003). A bore-hole gravimeter (Micro-g LaCoste Inc.) is characterized by small dimensions and remote-controlled operation at high temperatures. It is used for the estimation of rock densities from vertical profiles, and corresponding modelling of geological layers (LaFehr, 1983).

Air/sea gravimeters will be described in [5.4.4], and recording (Earth tide) gravimeters in [5.4.6].

Despite all measures to protect the gravimeter's measuring system against environmental disturbances, the zero reading changes with time: drift and tares. The *drift* is caused by aging of the spring material (approximating zero after some years) and short-term changes which occur during a field survey. This "transportation" drift results from reactions of the spring to vibrations and small shocks, uncompensated temperature fluctuations, and elastic effects after unclamping the lever. It depends on the spring material and on measurement conditions and can reach a few $\mu\text{ms}^{-2}/\text{day}$. Larger mechanical shocks may produce sudden *tares* of the same order of magnitude or more. The drift is determined by repeated station occupations during one day and subsequent modeling. Different methods have been developed depending on the instrumental behavior and the network structure; among them are the profile, the star, and the step method (Fig. 5.61).

After reducing the gravimeter reading for the Earth tides, cf. [8.3.6], the drift function can be modeled by a low-order polynomial with time (Fig. 5.62):

$$D(t) = d_1(t - t_0) + d_2(t - t_0)^2 + \dots, \quad (5.93)$$

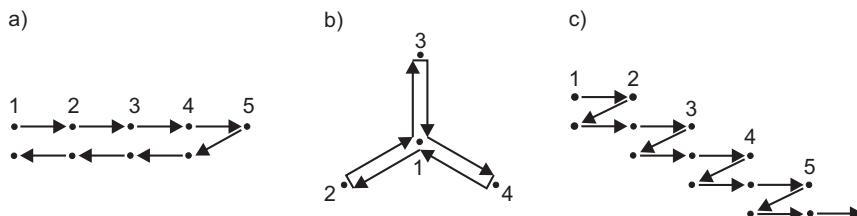


Fig. 5.61: Drift determination methods: a) profile method, b) star method, c) step method.

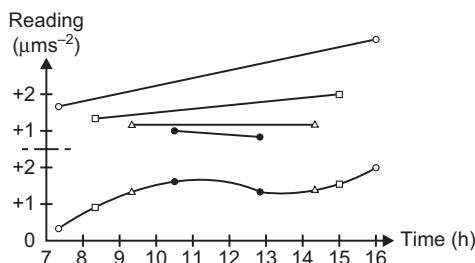


Fig. 5.62: Drift determination (profile method).

with t_0 being the starting time (e.g., beginning of the survey) and d_1, d_2, \dots the drift parameters. The network adjustment delivers the drift parameters, based on repeated observations, cf. [7.4].

The gravimeter reading z (in counter units) is converted to the gravity unit by means of the *calibration* function:

$$g = F(z). \quad (5.94a)$$

$F(z)$ depends on the physical and geometrical parameters of the measuring system, see (5.85), (5.90), (5.92), which cannot be determined individually with the desired accuracy.

Therefore, the calibration function is derived by comparing reading differences with known differences of gravity. Modeling is performed by a low degree polynomial (generally only a linear “scale factor”), periodic calibration terms may be added for taking cyclic errors of a measuring skrew into account. Restricting ourselves to the linear calibration coefficient, the transformation from the readings to the gravity reads

$$g_i = N_0 + Y_1 z_i = N_0 + (1 + y_1) z_i, \quad (5.94b)$$

where Y_1 is the scale factor and y_1 the (small) scale correction, N_0 represents the level unknown.

Laboratory and field methods are available for determining the coefficients of the calibration function. In the *laboratory*, gravity changes can be simulated and compared with the corresponding gravimeter readings. The tilt-table method uses the inclination by a known angle for producing an apparent gravity variation, and the mass method uses the defined change of the gravimeter mass. Special methods have been developed for recording gravimeters, cf. [5.4.6]. *Calibration lines* provide gravity differences, determined by absolute gravimeters, and eventually densified by relative gravimetry. They exploit the fact that gravity varies with latitude (horizontal calibration line) and height (vertical calibration line), Kanngieser et al. (1983), Timmen et al. (2006). The limited gravity range of these lines only allows determination of an approximate value for the linear calibration factor; an improved estimate of the linear and eventual non-linear parameters must be based on a global gravity reference system, cf. [5.4.3]

Gravity networks are generally *adjusted* by the method of parameter variation (Torge, 1993). Absolute gravity measurements and relative gravimeter readings are introduced as observations, and gravity values as well as (for relative gravimeters) drift and calibration coefficients are to be determined. The *observation equation* for an *absolute* gravity measurement on the station i reads

$$\bar{z}_i = g_i, \quad (5.95a)$$

where \bar{z}_i represents the observed mean value corrected for polar motion and Earth tides and reduced to ground level, cf. [5.4.1]. By combining (5.93) with (5.94b) we obtain the observation equation for *relative* gravimeter readings:

$$z_i = g_i - N_0 - Y_1 z_i + d_1 (t_i - t_0). \quad (5.95b)$$

In most applications, reading differences between the stations i and j are introduced as “observations”, hereby eliminating the level unknowns:

$$\Delta z_{ij} = z_j - z_i = g_j - g_i - Y_1 (z_j - z_i) + d_1 (t_j - t_i). \quad (5.95c)$$

The accuracy of gravity differences ($\Delta g < 1000$ to $2000 \mu\text{ms}^{-2}$) observed with well calibrated and drift-controlled instruments is 0.1 to $0.2 \mu\text{ms}^{-2}$. Repeated measurements and the use of several instruments increase the accuracy to $0.05 \mu\text{ms}^{-2}$ and better, and 0.01 to $0.02 \mu\text{ms}^{-2}$ for local ties (Becker et al., 2000; Timmen, 2010).

5.4.3 Gravity reference systems and gravity standard

Gravity reference systems provide homogeneity of gravimetric surveys by realizing a gravity standard through the gravity values of a selected number of stations.

The need to establish a global reference system arose at the end of the nineteenth century when larger sets of absolute and relative pendulum measurements had to be combined. *The Potsdam Gravity System* was introduced in 1909 by IAG. It was based on reversible pendulum measurements carried out in the Geodetic Institute Potsdam by Kühnen and Furtwängler (1898–1904). Relative pendulum ties to national base stations transferred the Potsdam absolute value to other parts of the world. Since the 1930s, new absolute and relative gravity measurements revealed that the Potsdam gravity value was $140 \mu\text{ms}^{-2}$ too high and that transfer errors of several $10 \mu\text{ms}^{-2}$ had occurred.

The Potsdam Gravity System was superseded by the *International Gravity Standardization Net 1971* (IGSN71), recommended by the IUGG (Morelli et al., 1974). This network contains 1854 gravity stations (among them about 500 primary stations) determined by 10 absolute and about 25 000 relative measurements, including 1 200 relative pendulum ties (Fig. 5.63).

The mean uncertainty of the adjusted gravity values is less than $1 \mu\text{ms}^{-2}$. High relative-accuracy is provided at gravimeter calibration lines, which extend in the north-south direction in America, Europe and Africa, and in the western Pacific. Meanwhile the IGSN71 has been extended to previously uncovered parts of the world. Regional networks have been connected to IGSN71, or transformed (shift and scale factor) to it, with the help of

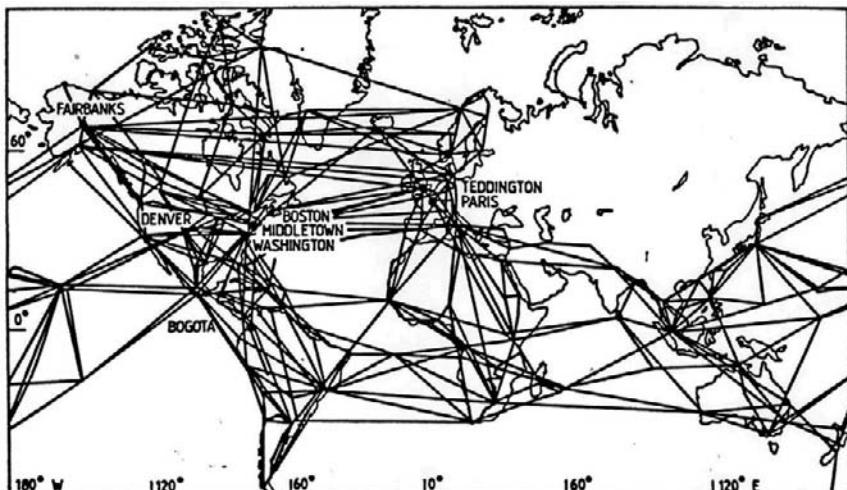


Fig. 5.63: International Gravity Standardization Net 1971 (IGSN71): absolute gravity stations and selected network ties, after Morelli et al. (1974).

identical stations. The IGSN71 gravity values can be used to derive the linear calibration factor of relative gravimeters with a relative accuracy of some 10^{-5} .

With the increasing availability of transportable *absolute gravimeters* with accuracy of $0.05 \mu\text{ms}^{-2}$ and better, the gravity standard can be established independently from a global system with any gravity survey, through the length and time standards inherent in the gravity meter (Torge, 1998). The linear calibration factors of relative gravimeters then are derived from the absolute values available in the survey area. The IGSN71 consequently does not need a readjustment but rather is improved continuously by networks based on absolute gravimetry. This strategy requires a regular quality control of the absolute gravimeter systems, cf. [5.4.1]. As a consequence, international comparisons of absolute gravimeters have been carried out since the 1980s at the BIPM, Sèvres (Vitushevkin et al., 2010), and since 2003 also at the European Centre of Geodynamics and Seismology in Walferdange, Luxembourg (Francis et al., 2010), see Fig. 5.64. For advanced absolute gravimeters, both the r.m.s. scatter around the reference station mean value and the long-term stability is a few $0.01 \mu\text{ms}^{-2}$, which characterizes the present state of the realization of the gravity standard.

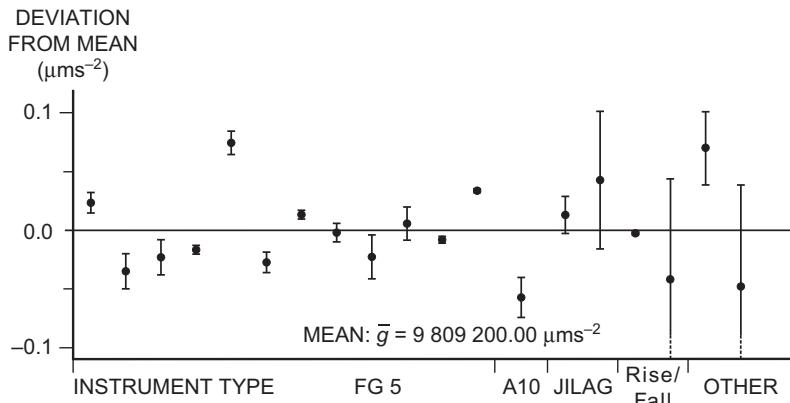


Fig. 5.64: Absolute gravimeter comparison, BIPM Sevres 2005: Deviations from mean value and standard deviations for different gravimeter types (FG5, A10, JILAG, rise and fall instruments, others), after Vitushkin et al. (2010), courtesy L. Vitushkin.

5.4.4 Gravity measurements on moving platforms

Kinematic methods have been developed for rapid and high-resolution gravimetric surveys in areas of having challenging environmental conditions, such as the oceans, the polar regions, high mountains, and tropical forests. Ships and airplanes are predominantly used as carriers, but helicopters and land vehicles also have been employed for local surveys. Sea gravimetry concentrates on regions of geological interest and geophysical exploration, especially at border seas and in shelf areas. Regional and local airborne surveys serve for covering areas lacking in terrestrial gravity data, and thus support high-resolution geoid calculations as well as geology, geophysics, and glaciology.

Compared to stationary gravimetry, additional difficulties arise in kinematic gravimetry, i.e., the continuous orientation of the gravity sensor with respect to the vertical, and the separation of gravity from non-gravitational accelerations, which occur at a broad frequency range (Brozena and Peters, 1995; Schwarz, 2001).

The principle of kinematic gravimetry is based on Newton's *law of motion* (e.g., Jekeli, 2001a). In an *inertial system* it reads as

$$\ddot{\mathbf{r}} = \mathbf{f} + \mathbf{g}, \quad (5.96a)$$

where $\ddot{\mathbf{r}} = d^2\mathbf{r}/dt^2$ is the kinematic acceleration of a body, \mathbf{f} the acceleration due to action forces (also called specific force, i.e., force per unit mass), and \mathbf{g} the *gravitational* vector. The specific force is measured by accelerometers (employing a mechanical spring, an electromagnetic force or a vibrating string as a sensor), with mechanical or computational orientation provided by gyros. The kinematic acceleration has to be determined independently by geometric methods of positioning and navigation, e.g., through GNSS (Fig. 5.65).

For an accelerometer *resting* on the surface of the rotating Earth and aligned with the local vertical, the kinematic acceleration in (5.96a) is zero. The accelerometer now measures *gravity* and is designated as gravity meter, see (5.84).

Based on (5.96a), modeling of kinematic gravimetry can be done in the local ellipsoidal system orientated in the system of global ellipsoidal coordinates, cf. [4.1.3], Timmen et al. (1998), Schwarz (2001). In kinematic gravimetry, this system is called *local level system* (subscript l), and generally defined as a north-east-down-system. We assume that the kinematic acceleration is given in this system (e.g., by GPS/GNSS positioning), and that the accelerometers are fixed to the vehicle, the specific force is then measured in the vehicle's body frame (subscript b). The transformation from the body frame to the local level system is carried out by the rotation matrix \mathbf{R} containing the orientation angles between the two frames which vary with time. The *gravity* vector (the measurement takes place on the rotating Earth, which introduces the centrifugal acceleration!) is now expressed by:

$$\mathbf{g}^l = \ddot{\mathbf{r}}^l - \mathbf{R}_b^l \mathbf{f}^b + (2\Omega_{ie}^l + \Omega_{el}^l) \times \dot{\mathbf{r}}^l, \quad (5.96b)$$

where again $\ddot{\mathbf{r}}$ is the platform kinematic acceleration and $\dot{\mathbf{r}}$ its velocity, \mathbf{r} is the position vector and \mathbf{f} is the measured acceleration vector. \mathbf{g} now represents *gravity* instead of gravitation as defined in (5.96a). As the platform moves with $\dot{\mathbf{r}}$ with respect to the rotating Earth, inertial accelerations arise. These accelerations are taken into account by the last term in (5.96b). Ω_{ie} and Ω_{el} are the skew-symmetric matrices of angular velocities due to the Earth's rotation rate and the vehicle's rate, referenced

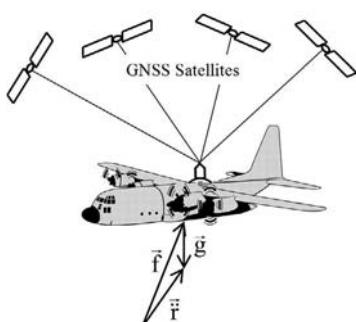


Fig. 5.65: Airborne gravity meter principle, modified after Timmen (2010).

to the ellipsoid (Earth-fixed frame e): Coriolis effect, see below (Jekeli, 2001a, p. 123 ff.).

The Earth's and the vehicle's rotational matrices depend on latitude and longitude rates (horizontal velocities), and on the Earth's angular velocity. Introducing the individual parameters into (5.96b) finally leads to a set of non-linear differential equations for position and velocity. Integration delivers the fundamental equations of inertial navigation/positioning. In *kinematic gravimetry*, they are solved for gravity, by introducing independently measured position and velocity. *Inertial positioning*, on the other hand, utilizes gravity field models, and solves for position, cf. [5.5.3].

At the practical evaluation of (5.96b) the normal gravity vector γ is subtracted from gravity, which introduces the *gravity disturbance* as the unknown parameter, in contrast to the gravity anomaly which is used traditionally at gravimetric geodesy, cf. [6.5.1].

Gravity sensors used in kinematic gravimetry are either land gravimeters (including special constructions) converted for use under dynamic conditions, or force-balanced accelerometers. They operate either on a stable platform or are (accelerometers) part of an inertial platform rigidly connected to the carrier (Glennie et al., 2000).

Operational sea and airborne gravimetry generally employs modified land *gravimeters* mounted on a damped two-axes *gyro-stabilized platform*. Stabilization occurs in the local-level frame by two gyroscope/accelerometer pairs operating in a feed-back mode. At this "scalar" gravimetry, only the *magnitude* of gravity is determined, and (5.96b) reduces to (Jekeli, 2001a, p. 334)

$$g = f_z - \ddot{z} + 2\omega \cos \varphi \sin \alpha v + \frac{v^2}{r}. \quad (5.97)$$

Here, f_z and \ddot{z} are the vertical (upward) components of the specific force and the platform acceleration, respectively. ω is the angular velocity of the Earth rotation, φ the geodetic latitude, α the geodetic azimuth, v the platform velocity with respect to the Earth, and r the distance to the Earth's center. Again, for the static case, (5.97) transforms into the equilibrium conditions of relative gravimetry, cf. [5.4.2].

The velocity dependent terms on the right-hand side of (5.97) represent the *Eötvös reduction* (Harlan, 1968). From Fig. 5.66, it can be identified as the Coriolis acceleration, which

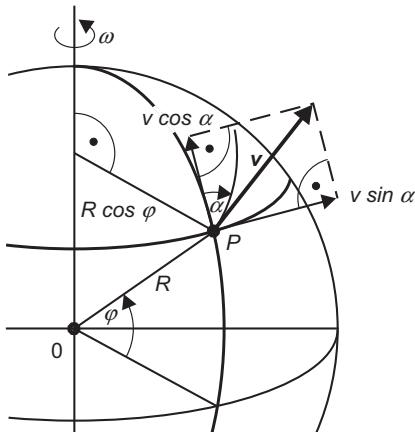


Fig. 5.66: Eötvös effect.

increases (for a west-east directed course) the angular velocity of the Earth rotation, and the centrifugal acceleration arising from the platform's angular velocity v/r around the center of the Earth. Close to the Earth ($r = R = 6371$ km) the Eötvös reduction amounts to

$$\delta g_{\text{Eot}} = 40v \cos \phi \sin \alpha + 0.012v^2 \mu\text{ms}^{-2}, \quad (5.98)$$

with v in km/h. The second term is small for sea gravimetry but attains large values with airborne applications. As velocities can be determined by GNSS navigation with an accuracy of 0.05 m/s and better, the uncertainty of the Eötvös reduction is now less than $10 \mu\text{ms}^{-2}$.

Instead of using a gravimeter on a stabilized platform, the gravity sensor can be rigidly connected to the vehicle. GNSS supported inertial navigation systems (INS) are employed with this *strapdown inertial gravimetry*, characterized by the use of force-rebalanced accelerometers with a high digital data rate (Jekeli, 2001a, p. 320 ff.). This vector gravimetry mode requires three orthogonally mounted accelerometers in order to determine the specific force *vector*. According to (5.96b), the orientation angles between the body-frame and the local level-frame are needed continuously, and are computed by integrating the output of the INS gyros and from GNSS multiantenna systems. One advantage of vector gravimetry would be the simultaneous determination of gravity disturbances *and* deflections of the vertical, with the possibility of a direct determination of geoid profiles, cf. [6.7.4]. Due to the high demands on attitude control (gyro drift!) vector gravimetry is still in the experimental stage (Jekeli and Kwon, 1999; Kreye et al., 2006), but it offers an inexpensive and robust tool for airborne gravimetry. In the *scalar* mode, only one approximately vertical accelerometer is used. Demands are now less stringent, especially if the output of an accelerometer triad is used for the determination of the magnitude of gravity (rotation invariant scalar gravimetry), Wei and Schwarz (1998).

The methods for separating *gravity* from *non-gravitational* accelerations depend on the frequency of the accelerations and differ for sea and airborne gravimetry, after strong reduction of high-frequency vibrations by damping of the measuring system.

At *sea gravimetry* (stabilized platform), "disturbing" accelerations occur with periods between 2 and 20 s, and they may reach amplitudes of 0.1 g. Due to low ship velocity (10 to 20 km/h) and the nearly constant reference surface (sea level), low-pass filtering sufficiently suppresses the *vertical* accelerations. By averaging the recorded data over time intervals of 1 to 5 minutes, mean gravity values over some 0.1 to 2 km are thus obtained. The effect of *horizontal* accelerations remains small because of the stabilization. Off-leveling effects generally can be neglected at an attitude accuracy of about $10''$. More critical are cross-coupling effects, which occur with horizontal lever spring gravimeters between the horizontal and the vertical component of the disturbing acceleration. They may reach $50 \mu\text{ms}^{-2}$ or more and must be corrected using the horizontal acceleration records. Straight line gravimeters (vertical sensitivity axis) are free from these errors. This is also valid for *vibrating string gravimeters* which are based on the fact that the resonant vibrational frequency of a string under tension is proportional to the square root of g . Other advantages of this design are the large dynamic measurement range and the little shock sensitivity.

For *airborne gravimetry*, accelerations vary with periods from 1 to 300 s (long-periodic eigenmotion of the airplane), and with amplitudes up to 0.01...1 g and more. Large airplane velocities (250 to 450 km/h) prevent an effective filtering, and thus with a long filter-length (one minute to several minutes) only *mean* gravity values over some km to 10 km and more are obtained. In addition, the attenuation of the gravity field with height,

cf. [3.3.3], prevents a high resolution at high flight altitudes of several km. These problems in principle require the employment of low-velocity and low-flying airborne vehicles. The vehicle's kinematic accelerations have to be determined independently by geodetic methods, nowadays practically performed through differential GNSS (carrier phase measurements), using the second derivative of height or the first derivative of velocity. As the measurement noise is amplified by these time differentiation, the first time derivative of velocity as obtained from Doppler shifts is preferred in this context. Over water and ice areas, radar and laser altimetry can also be employed for height determination. Heights are also needed in order to reduce the gravity data to a common reference level, by applying the free air reduction, cf. [6.5.3], this is achieved satisfactorily by GPS/GNSS heighting (Forsberg and Olesen, 2010).

Gravity observations on sea started at the beginning of the twentieth century, when *O. Hecker* obtained gravity data along several ocean-wide ship-tracks by exploiting the gravity correction to be applied to mercury thermometer readings, when compared with hypsometer (thermometer operating at the boiling point of water) results. In 1923, *F.A. Vening-Meinesz* constructed a three-pendulum instrument for gravity measurements in a submerged *submarine*; world-wide cruises followed until the 1960s. At that time, *sea gravimeters* (e.g., modified Askania and LaCoste and Romberg land gravimeters) mounted on gyro-stabilized platforms became operational on board of surface vessels (Dehlinger, 1978), Fig. 5.67. First attempts for *airborne* gravimetry were also made in the 1960s, using stable platform mounted sea gravimeters on board of high flying aircrafts (LaCoste, 1967). Conventional sea-air gravimeters on platforms are now employed operationally on board of helicopters and airplanes. A more recent development especially for use under rough conditions consists of a rotational double quartz filaments system embedded in a viscous fluid (Krasnov et al., 2008).

Since the 1970s, force-balanced *accelerometers*, as developed for inertial navigation, became another tool for sea-air gravimetry. These instruments are small and robust with respect to strong



Fig. 5.67: Gravimeter System KSS31M with Gravity sensor Gss30 and gyro-stabilized platform KT 31, Bodenseewerk Geosystem, Überlingen, Germany, courtesy Bundesanstalt für Geowissenschaften und Rohstoffe (BGR).

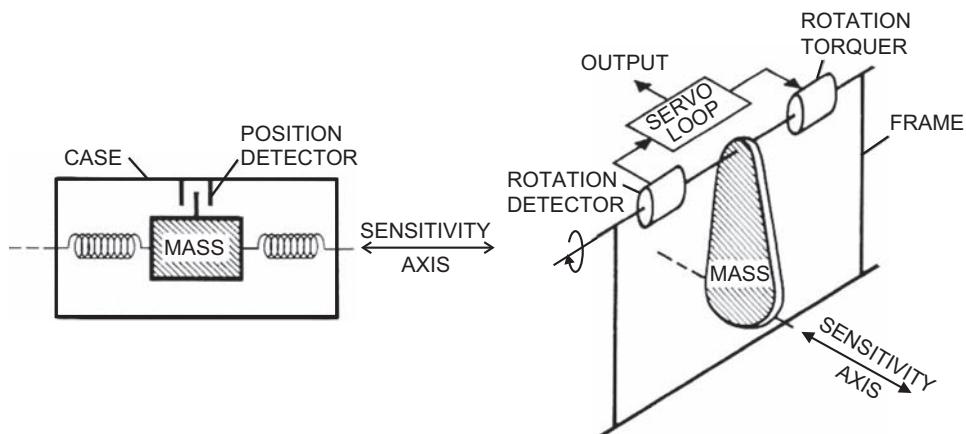


Fig. 5.68: Force-balanced accelerometer principle: translational (suspended mass) system (left) and rotational (pendulum) system (right).

dynamics but have less resolution and larger drift rates than conventional land gravimeters, linear and rotational systems are available (Fig. 5.68). For a linear system, the proof mass is constrained to move in only one direction and maintained at the zero position by an electromagnetic field, the electrical current needed to maintain zero is proportional to the acceleration. Depending on the direction of the sensitive axis, dedicated components of the specific force are measured. Force-balanced accelerometers are especially suited for use under rough conditions on sea and in air; they have also been employed on board of deep sea vessels (Bell and Watts, 1986; Cochran et al., 1999).

Sea and airborne gravimetric surveys generally are carried out along parallel tracks, with track distances ranging from a few km to 10 km and more. Orthogonal tracks serve for control and accuracy improvement by adjustment of the crossover discrepancies, (Denker and Roland, 2005), Fig. 5.69. The accuracy of sea and airborne gravity measurements (data recording generally with 1 s average) depends on the survey conditions (sea state, air turbulence, ship and aircraft properties, flight altitude and velocity), on attitude errors, and, for airborne gravimetry, on the separation between gravity and disturbing accelerations. Accuracies of 5 to 20 μms^{-2} are achieved with sea gravimetry with a resolution of about 1 km along track (track distances 1 to 5 km and more), Wessel and Watts (1988). Airborne gravimetry generally is carried out at flight heights of a few km, but low speed and elevation (several 100 m) surveys are also performed, especially with helicopters (Hammer, 1983; Segawa et al., 2002). A resolution of 5 to 10 km is routinely obtained now (helicopter 1 to 3 km), with accuracies of 20 to 50 μms^{-2} (helicopter 5 μms^{-2}). An increase in resolution and accuracy by a factor of two has been reached at surveys carried out at low altitudes and under favorable environmental conditions (e.g., Brozena and Peters, 1995; Skourop et al., 2009). It must be remembered that the attenuation of the gravity field with height prevents a high frequency resolution at high flight altitudes. Also high frequency disturbances through turbulence still pose severe problems, and may lead to corresponding changes at flight planning.

Among the areas covered by airborne gravity surveys since the 1990s are the Arctic (Fig. 5.70) including Greenland (Brozena et al., 1997; Kenyon et al., 2008), alpine Switzerland and France

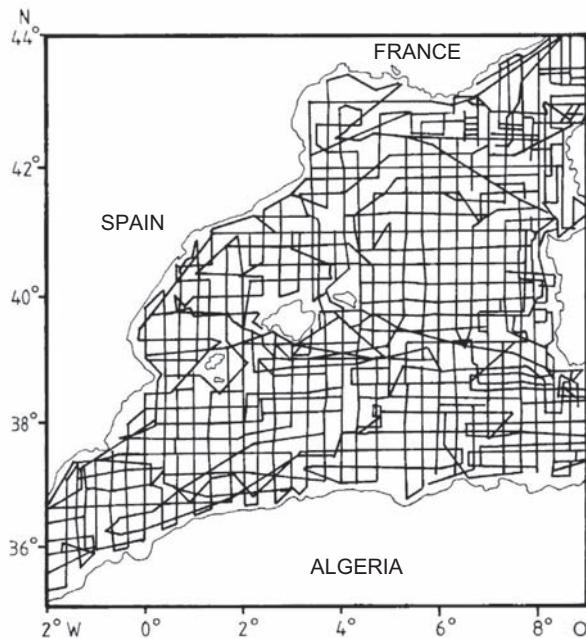


Fig. 5.69: Sea gravimetry profiles (1965–1972), Western Mediterranean Sea, Osservatorio Geofisico Sperimentale, Trieste, after Finetti and Morelli (1973).

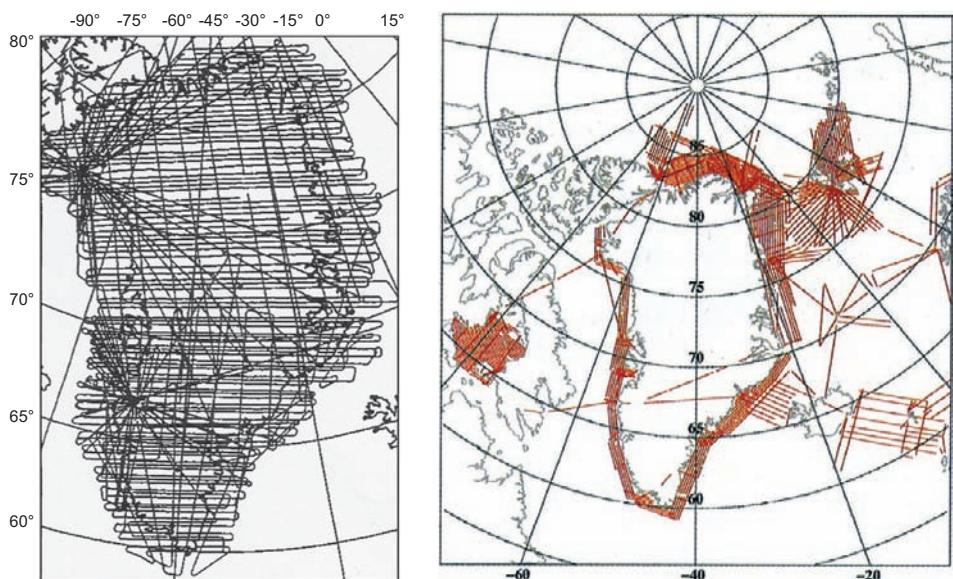


Fig. 5.70: Airborne gravity surveys over Greenland (1991/1992) and the Arctic (1998, 2003), Forsberg and Kenyon (1995) and Forsberg and Olesen (2010).

(Verdun et al., 2002), the Amazon region, and parts of central Asia and Africa. An international Antarctic project has started in order to obtain a homogeneous gravity field information over that continent which is only at small parts covered by terrestrial or airborne gravimetry (Scheinert, 2005).

5.4.5 Gravity gradiometry

The *gravity gradient tensor* (3.68) contains local gravity field information, and thus is of interest for high-resolution gravity field determination. It is generally expressed in the local astronomic (local level) system, cf. [3.2.2]. The unit of the components of grad \mathbf{g} is s^{-2} , with $10^{-9} s^{-2} = 1 \text{ ns}^{-2}$ traditionally called *Eötvös unit* (E).

A *gravity gradiometer* determines the components of grad \mathbf{g} , either all, several or linear combinations of them. This is achieved by exploiting the reaction of neighboring proof masses to the gravity field. A gradiometer unit consequently consists of two gravity sensors (mostly accelerometers) rigidly connected and generally orientated in the local level system. Taylor expansions of gravity in the two sensors 1 and 2, with respect to the center of mass C of the system, and differences in the output of the sensors (specific force \mathbf{f}) yields in the stationary mode

$$\mathbf{f}_2 - \mathbf{f}_1 = (\text{grad } \mathbf{g})_C (\mathbf{r}_2 - \mathbf{r}_1)^l \quad (5.99)$$

where $\mathbf{r}_1, \mathbf{r}_2$ are the position vectors of the sensors in the local level system. A gradiometer system is composed of several gradiometer units orientated in different directions in order to derive the corresponding components (Fig. 5.71). Rotation of the gradiometer units in the gravity field provides another means for the determination of different components (Torge, 1989, p. 300 ff.).

The *torsion balance*, developed by R.v. Eötvös around 1900, was the first dedicated gravity gradiometer. It consists of two equal masses situated at different heights and rigidly connected by a beam system. At the center of mass the system is suspended by a torsional thread. Equilibrium of the torques acting on the masses is achieved by horizontal rotation, which depends on the components $W_{yy} - W_{xx}, W_{xy}, W_{xz}, W_{yz}$. These quantities and the zero position of the beam are determined by observing the beam direction at five different azimuths. A precision of 1 to 3 ns^{-2} was obtained (Mueller et al., 1963). The torsion balance was widely employed in applied geophysics between 1920 and 1940, with great success at the early oil exploration, for example, at the reconnaissance of salt domes in Texas. The effect of rugged

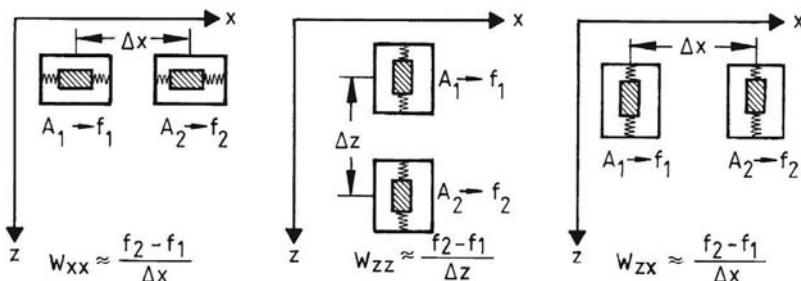


Fig. 5.71: Gravity gradiometer translational system principle with longitudinal (left and center) and transverse (right) constellation.

topography and close man-made constructions limited the application of the torsion balance to flat areas and reduced the accuracy of the results to about 10 ns^{-2} . A dedicated *borehole* gravity gradiometer has been developed in order to detect changes in oil/gas/water pore space (Nukut, 1989).

On the Earth's surface, *gravimeters* can also be used to approximate the components of grad g by measuring gravity differences between adjacent stations. The *horizontal* gradient (W_{zx}, W_{zy}) can be derived with a precision of 10 ns^{-2} from gravity profiles or area surveys, with station distances of 10 to 100 m (Hammer, 1979). The *vertical* component W_{zz} can be determined with the same precision by repeated relative gravity measurements on tripods, with heights up to 3 m (Timmen, 2010, p.26 ff.).

Terrestrial gravity gradiometry in the stationary mode is time consuming and strongly affected by local mass anomalies. Terrain reductions have to be taken into account even in the immediate surrounding (within 100 m), which limits the application to flat or moderate hilly areas.

Measurements on *moving platforms* allow rapid data collection (e.g., with a 1 s rate or more). Terrain effects are significantly reduced with height above ground, this favors airborne and satellite applications. With increasing height, on the other hand, the gradient signal decreases with the cube of the distance, which requires sophisticated data processing for the separation of signal and noise. We now concentrate on *airborne* gradiometry, satellite application have been presented in [5.2.8]. In this kinematic mode, the gradiometer unit consists of two accelerometer pairs, mounted orthogonally on a slowly rotating disk (Fig. 5.72), and set up on a gyro-stabilized platform. The disk's rotation (rotation rate, e.g., 0.5 Hz) minimizes systematic effects related to the instrument's orientation. By subtracting the readings of a pair of opposing accelerometers, non-gravitational accelerations of linear type mostly cancel. As in airborne gravimetry, effects of the platform's rotation about the Earth have to be taken into account, cf. [5.4.4].

Gravity gradiometry on moving platforms was adopted from military developments for U.S. Navy nuclear submarines (Bell Aerospace design), and further developed for geodetic and geophysical purposes (Jekeli, 1993). It reached commercial use at exploration geophysics (mineral deposits, cavities, groundwater) in the 1990s. Survey areas are limited in extension (few km to 10 km or more), and are surveyed by parallel profiles with line spacing ranging from

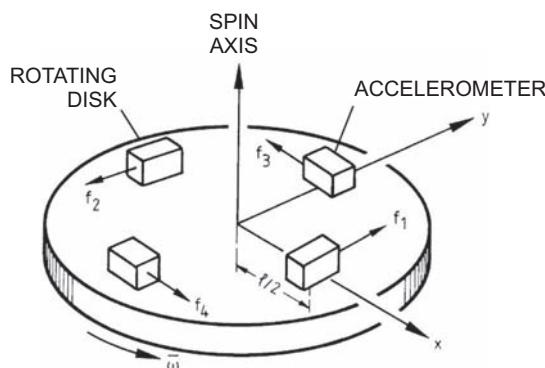


Fig. 5.72: Rotating gravity gradiometer principle, after Jekeli (1988a).

50 m to 2 km. Small fixed-wings aircrafts serve as gradiometer carrier, and flight height above ground may be less than 100 m. By combining three gradiometer units mounted on rotating disks under different orientation, the full tensor gravity gradient containing five independent elements can be derived. The additional hardware employed at a gravity gradiometry survey includes GPS for positioning and timing, and altimeter hardware for the construction of a high-resolution digital elevation model. With present-day technology, an accuracy of a few ns^{-2} and better can be obtained, with a gravity field resolution down to about 50 m (Murphy, 2004; Dransfield and Lee, 2004).

Gravity gradiometry in the *airborne* mode is primarily applied in exploration geophysics, while geodetic application concentrates on dedicated *satellite* missions, cf. [5.2.8].

5.4.6 Continuous gravity measurements

Continuous gravity records contain information especially on Earth and ocean tides, but also on a multitude of other geodynamic phenomena, ranging from seismic normal modes over atmospheric and ocean loading, free core nutation, polar motion and hydrologic effects to post-glacial rebound, tectonics, and volcanic and earthquake activity (Wilhelm et al., 1997). These effects occur at time scales between seconds and several years and have amplitudes of about 1 to 1000 (tides) nms^{-2} , cf. [8.3.6]. Hence, a *recording gravimeter* should provide a resolution of 0.01 to 1 nms^{-2} and a high stability with time (low drift rates). It should be time-controlled within 10 ms. In order to reduce environmental effects (temperature changes, microseismicity, local surface inclinations), recording gravimeters generally are installed at underground sites (basement, tunnel).

Recording gravimeters operate in an electronic feedback mode, cf. [5.4.2], over a limited measuring range, e.g., 10 μms^{-2} . The voltage output is proportional to gravity and first undergoes an analog filtering in order to reduce the high-frequency noise. It is then digitized by an A/D converter. Digital filtering delivers a data set (1 to 10 s samples), which is stored on a PC. Further numerical filtering and data reduction may be appropriate as well as the reduction of spikes due to earthquakes and the interpolation of data gaps. Corresponding procedures are part of data processing software for Earth tides analysis (Wenzel, 1996). An analogue output offers a convenient on-line control of the data acquisition.

Spring-type and superconducting (also cryogenic) gravimeters are used for gravity recording (Melchior, 1983).

Elastic spring gravimeters can be employed if supplemented with a low-pass filter, a recording unit, and a quartz clock. Special Earth tide gravimeters with small measuring range have also been developed and are characterized by long-term stability (e.g., by a double thermostat). Some recent land gravimeters also offer the option of an Earth tides mode through increased sensitivity, large memory, and computer-controlled remote operation. The long-term drift of these elastic-spring type instruments has to be removed by filtering. Consequently, only short-period effects (e.g., diurnal and higher-frequency tides) can be determined, at a noise level of a few 0.1 to 1 nms^{-2} (Fig. 5.73).

For the *superconducting* gravimeter (Goodkind, 1999) the gravity acting on the proof mass (hollow Niobium sphere of 2.5 cm diameter) is compensated by a magnetic counterforce (Fig. 5.74). The magnetic field is generated by superconducting coils and thus is extremely stable with time. The position of the mass levitating in the magnetic field is monitored by capacitive sensing plates, with the zero position restored by a feedback system. Cooling by liquid helium provides the superconducting state at a temperature

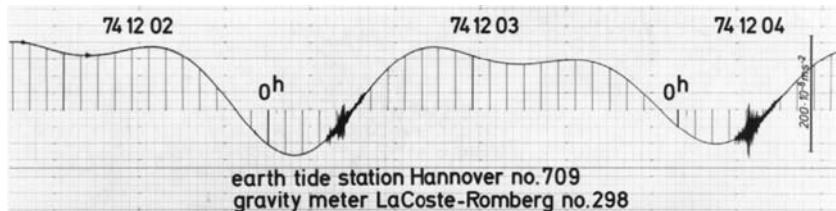


Fig. 5.73: Gravimetric Earth tide record, obtained with LaCoste and Romberg gravimeter G298, Institut für Erdmessung (IfE), University of Hannover.

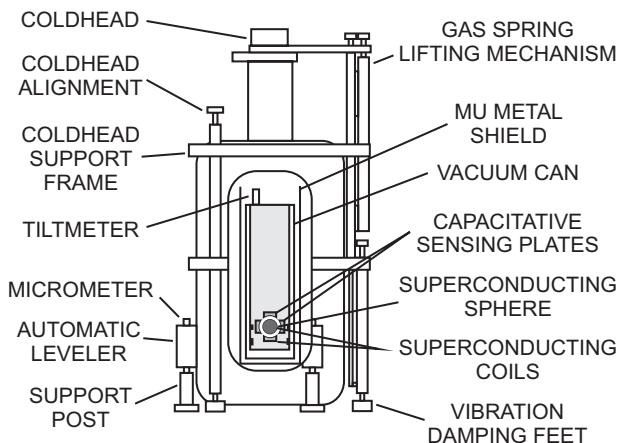


Fig. 5.74: Superconducting gravimeter principle, after GWR-Instruments information.



Fig. 5.75: OSG Observatory Superconducting Gravimeter view, courtesy of GWR-Instruments Inc., San Diego, CA, U.S.A.

of 4.2 K. The superconducting cylinder provides a primary shielding from the Earth's magnetic field, supported by an additional μ -metal shield on the outside of the vacuum case. The measuring system is kept in an insulating dewar vessel (Fig. 5.75). An automatic leveling system (two orthogonally mounted tiltmeters and two levelers under the dewar) provides an alignment better than 1 μrad .

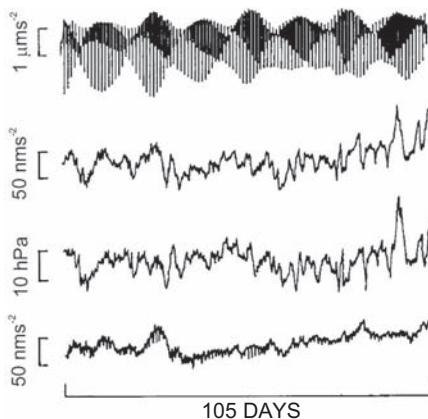


Fig. 5.76: GWR superconducting gravimeter drift, with (top to bottom) raw gravimeter signal, Earth tides reduced signal, atmospheric pressure and gravity residuals after removal of Earth tides and atmospheric pressure effects, courtesy GWR-Instruments, Inc., San Diego, CA, U.S.A.

The instrumental drift of a superconducting gravimeter is very small (on the order of $10 \text{ nms}^{-2}/\text{a}$), and may be modeled for the first months of observation by an exponential function, followed by a linear trend (Van Camp and Francis, 2007), Fig. 5.76. Absolute gravity measurements can be used to control the drift at longer time intervals. From tidal analysis, a noise level of $<0.01 \text{ nms}^{-2}$ (frequency domain) and $<1 \text{ nms}^{-2}$ (time domain) has been found for superconducting gravimeter results (Hinderer et al., 2009; Neumeyer, 2010).

The superconducting gravimeter was introduced by Prothero and Goodkind (1968) and commercially manufactured since the 1980s by GWR Instruments. Systematic investigations at several institutions, e.g., at the Observatoire Royal de Belgique, Brussels, and the Bundesamt für Kartographie und Geodäsie, Frankfurt a.M. (Richter, 1987) led to continuous improvements. This includes the reduction of the instrument's size, the increase of the time interval for helium refilling (a closed cycle cooling system will make the refilling practically superfluous), and the development of a dual-sphere instrument in order to detect instrumental offsets ("tares").

A global project of gravity recording with superconducting gravimeters (*Global Geodynamics Project GGP*) has been launched in 1991, and started operation in 1997. Today the net comprises about 20 stations, which continuously record gravity and provide the raw data decimated to 1 minute samples (Fig. 5.77). The results serve for improving Earth and ocean tidal models and for investigating a multitude of geodynamic phenomena, and are used as ground truth for gravimetric space missions, cf. [5.2.8], Crossley and Hinderer (2010). The GGP data are included in the data bank for tidal gravity measurements which is maintained at the International Centre for Earth Tides, it contains the tidal gravity data (hourly values) of about 360 stations (Melchior, 1994).

Calibration of a recording gravimeter is performed by relative and absolute methods. A *relative* calibration is realized by parallel registration with a "calibrated" gravimeter or by recording on a station with well-known tidal parameters. *Absolute* calibration procedures include the artificial periodic acceleration on a vertically moving platform, the controlled vertical displacement of large external masses, and the parallel registration

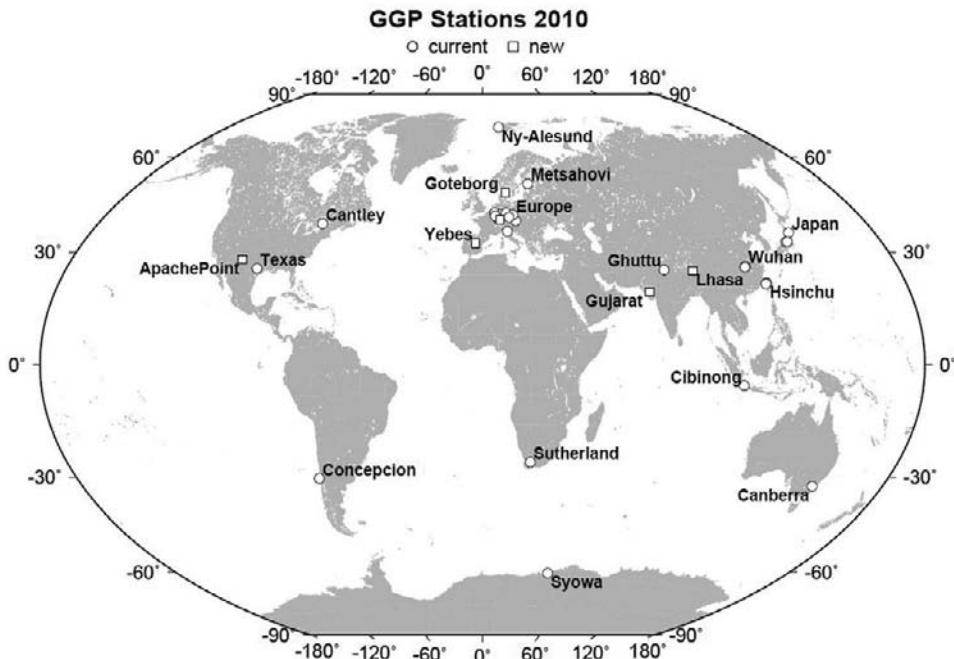


Fig. 5.77: Global Geodynamics Project: station distribution, status 2010 (Hinderer et al., 2009), courtesy GGP Website (<http://www.eas.slu.edu/GGP/ggphome.html>)

with an absolute gravimeter. Concentrating now on the superconducting gravimeter, the latter method is often used now, achieving a calibration precision of about 0.05% (Tamura et al., 2005). An even better precision has been obtained at the moving platform calibration, while the accuracy of the relative methods is limited to a few 0.1% (Richter et al., 1995; Francis, 1997). The instrumental phase shift is determined by recording the gravimeter's response to a defined impulse (step response method), Van Camp et al. (2000).

The gravity signal is strongly correlated with *atmospheric pressure*. A linear regression with local air pressure (between -2.5 and $-3.5 \text{ nms}^{-2}/\text{hPa}$) reduces the main part of this effect, see (5.81b), also Fig. 5.76. More refined models are available which also take the air pressure around the station and the elastic response of the Earth's crust into account (Merriam, 1992; Gitlein and Timmen, 2007; Kroner et al., 2007). Variations of *groundwater level* and *precipitation* also affect the gravity record and may reach the order of some 10 nms^{-2} , but they are difficult to model (Virtanen, 2000), cf. also [8.3.1].

Longer (several months and more) gravity records can be subjected to a *tidal analysis* (Wang, 1997; Agnew, 2009). This dedicated analysis is already introduced here, as the tidal frequencies for a rigid Earth are extremely well known, cf. [3.5.2], in contrast to the majority of other geodynamic phenomena, cf. [8.3.6]. The analysis is based on the spectral decomposition of the observed signal into a number of partial tides. By comparing the observations (hourly samples, atmospheric pressure effects reduced) with the gravimetric tides for a rigid Earth, deviations in amplitude and phase are found, which

depend on the Earth's elastic response to the tidal forces (Earth and ocean tides). For the partial tide i , this is expressed by the *amplitude factor* (also gravimetric factor)

$$\delta_i = A_i(\text{obs}) : A_i(\text{theor}) \quad (5.100)$$

and the *phase shift*

$$\Delta\Phi_i = \Phi_i(\text{obs}) - \Phi_i(\text{theor}), \quad (5.101)$$

where A_i is the observed resp. calculated (solid Earth) amplitude, and Φ_i the corresponding phase. The observation equation for a least-squares *spectral analysis* then reads

$$l(t) = \sum_{i=1}^n \delta_i A_i(\text{theor}) \cos(\omega_i t + \Phi_i(\text{theor}) + \Delta\Phi_i), \quad (5.102)$$

with $l(t)$ being the recorded gravity value at time t , and $\Phi_i = 2\pi T_i$ the circular frequency (T_i is the period) for the partial tide i (Wenzel, 1976, 1997a). As a first approximation, a gravimetric factor of $\delta = 1.16$ and a phase lag of zero may be introduced for the reduction of gravity data, but more sophisticated gravimetric tidal models are available. This will be discussed in [8.3.6], together with the relation of the gravimetric factor to the Love numbers describing the reaction of the elastic Earth to tidal forces and loads.

Elastic spring gravimeters allow the determination of 10 to 20 partial tides (mainly diurnal, semi-diurnal, ter-diurnal), with an observation time of 4 to 6 months. Superconducting gravimeters can resolve up to 40 tides (including semi-annual and annual) by registration over several years. The gravimetric factor for polar motion has also been derived from long-term series. As an example, a 158 days registration with a LaCoste and Romberg feedback gravimeter at Hannover ($\varphi = 52.387^\circ\text{N}$, $\lambda = 9.713^\circ\text{E}$, $H = 50$ m) yielded for the lunar diurnal tide O1 (Timmen and Wenzel, 1994a):

$$\delta(O1) = 1.151 \pm 0.001, \Delta\Phi(O1) = 0.16^\circ \pm 0.08^\circ$$

and for the semi-diurnal tide M2

$$\delta(M2) = 1.188 \pm 0.0005, \Delta\Phi(M2) = 1.70^\circ \pm 0.03^\circ.$$

The factor for O1 is close to the observed global value 1.155, while the M2 result differs due to ocean load and attraction, cf. [8.3.6].

5.5 Terrestrial geodetic measurements

Terrestrial geodetic measurements determine the relative position of points on the Earth's surface, and generally use electromagnetic waves for deriving geometric quantities between them. The majority of the observations refers to the local vertical, and thus delivers results orientated in local gravity related astronomic systems. The measurement of horizontal and zenith angles [5.5.1] and of distances [5.5.2] allows relative three-dimensional positioning. Combined instruments (total stations) are now generally used, and even integrated with absolute GNSS positioning. Inertial surveying applies acceleration measurements, and seafloor positioning uses acoustic waves, for positioning under special environmental conditions [5.5.3]. Precise height differences are provided by leveling, which again refers to the Earth's gravity field [5.5.4]. Strain and tilt measurements serve for detecting local changes of distances and inclination with time [5.5.5].

Due to the high accuracy and economy of satellite-based positioning techniques, terrestrial geodetic measurements are used primarily for interpolating satellite-derived results or in areas where satellite methods fail or need terrestrial support. This includes underground and underwater positioning, surveys in forests and in urban areas, engineering surveys, and monitoring of local geodynamic processes.

Terrestrial methods are treated in textbooks on surveying, e.g., Anderson and Mikhail (1998), Bannister et al. (1998), Johnson (2004), Kahmen (2006). Classical surveying instruments are described by Deumlich (1982), while a more recent state is dealt with in Deumlich and Staiger (2002) and Joeckel et al. (2008). Kahmen (1978) and Schlemmer (1996) concentrate on the fundamentals of electronics employed in geodetic instruments, and Brunner (1984b) deals with the effects of atmospheric refraction.

5.5.1 Horizontal and vertical angle measurements

The *horizontal angle* is defined as the angle measured in the horizontal plane of the local astronomic system between two vertical planes. It is formed by the difference in horizontal *directions* to the target points which define the vertical planes. The *vertical angle* is the angle measured in the vertical plane between the horizontal plane and the direction to the target point. The *zenith angle* (also zenith distance), being the complement to 90° , is often introduced instead of the vertical angle, cf. [2.5].

A *theodolite* is used for measuring horizontal and vertical angles. The principal components of this instrument are a horizontal and a vertical circle with graduation, a telescope capable of being rotated about the vertical and the horizontal axes, and a mechanism for reading the circles. In order to orientate the theodolite with respect to the plumb line direction, it is equipped with spirit or electronic levels.

Regarding the reading of the circle graduation, we distinguish between optical and electronic or digital theodolites.

Optical theodolites of highest precision were developed since the second half of the eighteenth century and were then used until the 1960s for first order triangulation (with the Kern DKM3 and the Wild T3 theodolites being the latest developments) at station distances of 30 to 60 km, cf. [7.1]. They were characterized by very stable construction and circle diameters of 100 to 250 mm. Circle graduation errors were less than $0.5''$, and reading accuracy reached $0.1''$ by using a coincidence microscope with micrometer screw. The lens aperture of the telescope was 60 to 70 mm, and the magnification 30 to 40 or more. Standard deviations of $0.2''$ to $0.4''$ have been achieved for an adjusted horizontal direction.

Today, horizontal and vertical angles are measured only over shorter distances reaching from a few meter to about one and eventually up to 10 km, at engineering projects, geodetic network densification, and local geodynamic control. *Electronic theodolites* (lens aperture 30 to 45 mm, magnification of 30 or more) are employed for this purpose, they have superseded the optical analogue instruments. Generally, the electronic theodolite is combined with a distance meter to produce a total station, cf. [5.5.2], but “pure” theodolites still find application at industrial surveys (Fig. 5.78).

The horizontal and vertical circles (circle diameter 60 to 70 mm) of an electronic theodolite are either coded (with code signals arranged on concentric circles) or carry an incremental graduation (bright/dark changes). Reading is microprocessor-controlled and performed by optical-electronic scanning and subsequent interpolation (electronic micrometer). Electronic levels are used as tilt sensors, they are based on



Fig. 5.78: Industrial Theodolite (Leica TM6100A), courtesy Leica Geosystems AG, Heerbrugg, Switzerland



Fig. 5.79: Gyrotheodolite (Gyromat 3000 with Leica TM5100 Theodolite), courtesy Deutsche Montan Technologie (DMT), Essen, Germany.

the reflexion of light at the surface of a fluid and measure the reflected light point's position by means of a CCD array. A dual-axes compensator serves for automatic leveling the instrument (measuring range about $5''$, precision $0.3\dots 0.5''$); a residual tilt correction may also be applied automatically. Collimation and horizontal axis errors are either eliminated by measurement at both positions of the telescope or corrected internally. For the measurement of *vertical angles*, the theodolite is equipped with a reading index for the vertical circle. By leveling the index either manually (spirit level) or automatically (electronic level) the readings are referred to the local vertical, with an accuracy of a few $0.1''$. With electronic theodolites an accuracy of $0.5''$ to $2''$ is obtained for observed angles.

Gyrotheodolites have been developed for the determination of astronomic azimuths by combining a theodolite with a gyroscope. The principle of the gyroscope is based on the fact that a rapidly rotating gyro with horizontal spin axis swings into the north direction due to the combined effects of the gyro's spin, the Earth's gravity, and the Earth's rotation. An accuracy of $3''$ can be obtained by an automatic measurement procedure (20 individual measurements), within a time span of 10 min. Gyrotheodolites are employed primarily for mining and tunnel surveys (Lienhart and Brunner, 2004), Fig. 5.79.

Ray bending by *terrestrial refraction* is an error source which may pose special problems, cf. [5.1]. The effect of *lateral refraction* on *horizontal* angles generally can be neglected, but may reach the arcsec order of magnitude under unfavorable circumstances, e.g., if the light ray is closely passing a hill. Extended classical triangulation networks partly suffer from this effect which is difficult to model. Further processing of *vertical* angles, on the other hand, always requires the consideration of errors due to *vertical refraction*.

The *refraction angle* depends on the coefficient of refraction and thereby on the meteorological conditions along the path of light, particularly the vertical gradient of temperature, cf. [5.1.2]. Generally, a traditional value for the refraction coefficient (e.g., $k = 0.13$) is introduced in order to reduce the effect of vertical refraction, more actual values for the refraction coefficient can be derived from meteorological data taken at the endpoints of the observation line. These strategies easily may lead to a vertical angle error of a few arcsec and more. The effect of this error on the height difference increases with the square of the distance and thus reaches the order of a few decimeters already over a few km. The error of the observed zenith angle, on the other hand, only propagates with distance and thus remains at the order of a few cm. An approximately symmetric behavior of refraction is to be expected for *simultaneous* observations at the endpoints, especially with cloudy weather and prior to the isothermal conditions of the evening and if the light ray is more than 15 to 20 m above the ground. The uncertainty of the refraction angle then remains less than $1''$ for distances below 10 to 25 km. This has led to the method of observing reciprocal-simultaneous zenith angles, cf. [6.4.2].

For the direct determination of the refraction angle, attempts have been made to utilize the *dispersion* of the light, cf. [5.1.1]. Here, two different wavelengths are used for observation which causes a difference between the two angles of refraction at the target point. The dispersion angle is proportional to the refraction angle but about two orders of magnitude smaller which requires a measuring accuracy of a few $0.01''$. Corresponding experiments at distances less than 20 km gave uncertainties of 1 to $2''$ for the refraction angle (Williams and Kahmen, 1984).

5.5.2 Distance measurements, total stations

Terrestrial distance measurements have played and still play an important role for positioning. They provide geometric relations between neighboring control points, and they have also established the scale of classical geodetic networks.

Until about 1960, the scale of triangulation networks, constructed from angle measurements, was derived from *baselines* having lengths of 5 to 10 km. Measuring rods and, since about 1900, wires or tapes served to measure the base line length. With the *Jäderin* (1880) method, freely hanging invar (NiFe alloy) wires 24 m in length were used, characterized by a small coefficient of thermal expansion. The relative accuracy of the more recent base lines amounts to 10^{-6} , which corresponds to 1 mm/km. For field calibrations of wires and tapes, several international *calibration lines* were established by interferometric methods. Starting from the length of a standard meter, the *Väisälä* light interference comparator provided an optical multiplication up to base line lengths of 864 m (relative accuracy 10^{-7}).

Electromagnetic distance measurements started at the end of the 1940s. They may either use light waves ($\lambda = 0.4$ to $0.8 \mu\text{m}$) and the near infrared (up to $\lambda = 1 \mu\text{m}$) or microwaves

($\lambda = 1$ to 10 cm) as carriers of the measuring signal (Rueger, 1997; Joeckel et al., 2008). Microwaves are hardly absorbed by the atmosphere and allow the measurement of large distances (50 km and more) even under unfavorable weather conditions. The effect of humidity on refraction, on the other hand, is big and may significantly deteriorate the results. Distances measured by *light waves* are about one order of magnitude more accurate, but the measurement range depends on visibility, and is eventually strongly limited by disturbances through clouds, haze, or fog, cf. [5.1.2].

The travel time Δt of the signal serves as a measure for the distance s , according to the relation

$$s = v\Delta t \text{ and } v = \frac{c}{n}, \quad (5.103a)$$

with v being the actual velocity of the electromagnetic waves, c the velocity in vacuum, and n the index of refraction, cf. [5.1.1]. Time measurement is performed by the *pulse* or the *phase comparison* method, where we have to distinguish between electro-optical and microwave distance meters.

For *electro-optical* distance measurements, the transmitting and the receiving unit are combined in one instrument, and a reflector (prism) is posted on the target station (reflectorless measurements are also possible over limited distances). At the *pulse method*, the transmitter emits a pulse which after reflection is observed at the receiver. An electronic timer measures the time Δt that the signal requires to travel forth and back along the distance s leading to

$$s = \frac{v}{2}\Delta t. \quad (5.103b)$$

If the uncertainty in distance is to remain less than 1 mm, the time of propagation must be obtained to an accuracy better than 0.01 ns. This high accuracy demand can be fulfilled by short (a few ns) laser pulses, electronic counting controlled by a reference oscillator, and averaging the results of a large amount of individual measurements.

A similar instrumental arrangement is used for the *phase comparison method*. A high-frequency carrier wave is produced by a laser diode, and modulated continuously (amplitude or frequency modulation), with modulation frequencies between about 10 and 100 MHz. The corresponding half wavelength (because of the double distance traveled by the signal) serves as a "yard stick" (about 1 to 10 m) in surveying the distance. After transmission and reflection, the phase shift $\Delta\varphi$ between the emitted and the received signal is measured by a phase meter (Fig. 5.80). It represents the residual part of the distance above an integral number N of complete wavelengths, which is determined automatically by applying several slightly different modulation frequencies generated by frequency division. With a digital phase detector and a microprocessor, the measuring process can be fully automatized; the resolution achievable is 10^{-3} to 10^{-4} , which corresponds to a "mm"-precision.

Travel time Δt and phase shift $\Delta\varphi$ are related through

$$\Delta t = \frac{N + \frac{\Delta\varphi}{2\pi}}{f}, \quad (5.104)$$

where N is the number of complete periods, and the modulation frequency

$$f = \frac{v}{\lambda} = \frac{c}{n\lambda}, \quad (5.105)$$

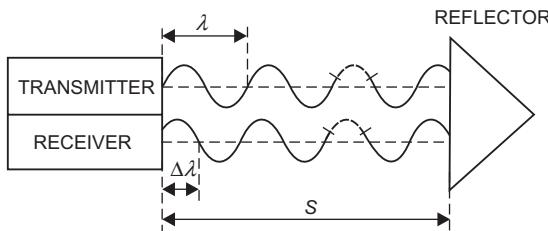


Fig. 5.80: Phase comparison method principle (electro-optical distance measurement).

with the group refractive index n (5.13) and the wavelength λ . Substituting (5.104) and (5.105) into (5.103b) delivers the distance

$$s = \frac{\lambda}{2} \left(N + \frac{\Delta\varphi}{2\pi} \right). \quad (5.106)$$

With the residual part of a wavelength

$$\Delta\lambda = \frac{\Delta\varphi}{2\pi} \lambda, \quad (5.107)$$

the distance can also be expressed by

$$s = N\frac{\lambda}{2} + \frac{\Delta\lambda}{2}. \quad (5.108)$$

Terrestrial *microwave* distance measurements differ from the *optical* method by the separate setting up of transmitter/receiver-units (combining master and remote function in one instrument) at the end points of the distance to be measured, both units are equipped with an antenna for sending and receiving the signals. The phase comparison method has been applied generally. Here, the emitted signal is received at the remote station, where it is demodulated and amplified. After superimposing on the remote station's carrier wave, the signal is sent back to the master station. Demodulation and comparison with a reference signal (phase measurement) delivers the phase shift, and again the use of different modulation frequencies allows a unique solution. At the pulse method the receiver has to include a correlator for measuring the travel time, while a one-way measurement would require precise clocks on both stations. The evaluation then would follow (5.103a), and apply modified formulas (5.106) and (5.108).

The *calibration* of electronic distance meters includes the control of the modulation frequency by a temperature-stabilized frequency meter and the determination of the instrumental constants (zero point correction and possible cyclic errors) on a comparator or on a short (about 1 km) calibration line. Calibration lines are usually partitioned into several sections and determined by laser interferometry or with a short-range distance meter of high precision.

Terrestrial *microwave* distance measurements started with the development of the tellurometer by *T. L. Wadley* (1956). Here, the master station emitted a modulated (modulation frequencies between 7.5 and 150 MHz) carrier wave ($\lambda = 8 \text{ mm to } 10 \text{ cm}$), which was retransmitted from an active transponder (receiver and transmitter). Measurement of ranges up to 100 km and more were obtained. The accuracy strongly depended on refraction uncertainties and could reach 10 ... 15 mm + 3 ppm (ppm is relative to distance). *Electro-optical* distance measurements trace back to the first geodimeter developed by *E. Bergstrand* (1948). Long-range distance meters used laser light

(He-Ne gas laser) with modulation frequencies between 15 and 50 MHz and were able to measure distances up to 60 km on clear days, with an accuracy of $1 \dots 5 \text{ mm} + 1 \dots 2 \text{ ppm}$. Long-range microwave and electro-optical distance measurements have been carried out extensively from the 1950s to the 1980s. The measurements were primarily for establishing first order control networks and for strengthening existing horizontal control, cf. [7.1].

Long-range distance measurements have become obsolete, as large-scale positioning is carried out nowadays almost exclusively by satellite methods; and terrestrial *microwave* distance measurements are no longer carried out at all. Microwave range and range rate measurements between satellites and ground stations, on the other hand, play an outstanding role for positioning and navigation on Earth and in space, cf. [5.2.5], [5.2.7].

Today, terrestrial distance measurements concentrate on distances less than one km, ranges of a few km are rarely exceeded. Visible light and near infrared are used, either in the pulse or in the phase comparison method. Separate distance meters have been available for special applications (partly suitable to be mounted on a theodolite), but generally electronic *total stations* are employed, providing distances, horizontal directions and zenith angles by combining a theodolite with a distance meter.

The measuring range of a distance measuring unit incorporated in a total station depends on the number of prisms posted on the target station. With one prism, distances up to 3 km can be observed, and the measurement range can be extended to about 6 km (three prisms) and 9 km (nine prisms), respectively. The error budget of the distance measurements contains a constant part that depends on uncertainties in timing or phase measurement and on the zero point stability. It is augmented by a distance dependent part which is determined by errors of the modulation frequency and by refraction effects. Generally, an accuracy of $3 \dots 5 \text{ mm} + 1 \text{ ppm}$ can be achieved with electro-optical distance meters, within a measuring time of a few seconds. The reflectorless mode allows ranging up to more than one km, with accuracies of $2 \dots 10 \text{ mm} + 2 \dots 10 \text{ ppm}$, depending on material and structure of the reflecting surface.

When integrated into a total station, the microprocessor-controlled operation in addition to distance measurement also provides automatic prism search, automatic leveling, and the measurement of horizontal directions and zenith angles. Further processing includes data storage in the internal memory, calibration, and application of refraction corrections with standard or actual meteorological data, as well as the transformation from local polar to Cartesian coordinates (Feist et al., 1998). High flexibility is given through the control unit in connection with a graphic display, and especially by the interchange of individual modules. Of special importance is the modular connection or the integration of GNSS units (antenna and receiver). The latter strategy allows precise absolute positioning through real time kinematic methods, cf. [5. 2.5], and consequently the transformation of the local results to a global reference. Examples for total stations are given in Figs. 5.81 to 5.83.

While refraction effects have played an important role at long-range distance measurements, they are of less importance at shorter distances usually observed today. Nevertheless, *refraction corrections* still have to be applied in order to achieve high accuracy at terrestrial distance measurements.

The *meteorological parameters* needed for modeling the corrections, cf. [5.1.2], generally are measured only at the instrument and at the target point, and the arithmetic mean is introduced with the refraction reduction. This value may not be representative for the entire distance, and thus a limiting factor for precise distance measurements is set (Iliffe and Dodson, 1987). It also must be noted that measurements conducted under



Fig. 5.81: Total station (Spectra Precision Focus 8), courtesy Spectra Precision, Westminster, CO, U.S.A.



Fig. 5.82: Total station (Trimble S8), courtesy Trimble Navigation Ltd., Sunnyvale, CA, U.S.A.



Fig. 5.83: Total station with integrated GNSS (Leica Smartstation TPS1200+), courtesy Leica Geosystems AG, Heerbrugg, Switzerland.

the same atmospheric conditions may be highly correlated, but this correlation can be significantly reduced if observations are carried out under different conditions.

The *refraction corrections* which have to be applied to the observed *distances* before further processing can be split up into three parts (Höpcke, 1966). The distance \bar{s}_0 read on the instrument is based on a standard value n_0 for the refractive index calculated from standard temperature and air pressure (5.17). If a more realistic value \bar{n} is available from local meteorological measurements, the relation

$$\bar{s}\bar{n} = \bar{s}_0 n_0 \quad (5.109)$$

provides a first *velocity correction*

$$k_n = \bar{s}(n_0 - \bar{n}). \quad (5.110)$$

As seen from (5.20a), the radius of the light curve differs from the Earth's radius ($r \approx 8 R$). Hence, the light passes through atmospheric layers with a larger refractive index than the mean value \bar{n} , calculated from the endpoint data only. With (5.10) and the coefficient of refraction $k = 0.13$, we obtain

$$\frac{dn}{dh} = -\frac{k}{R} = -20 \times 10^{-6}/\text{km}, \quad (5.111\text{a})$$

which can be used to derive a second velocity correction

$$k_{\Delta n} = -(k - k^2) \frac{\bar{s}^3}{12R^2}. \quad (5.111\text{b})$$

This correction is less than 1 mm over a distance of 15 km and can be neglected generally.

For three-dimensional computations, the *chord distance* s is required. By assuming a spherical arc with radius r we have

$$s = 2r \sin \frac{\bar{s}}{2r},$$

or after a series expansion

$$s = 2r \left(\frac{\bar{s}}{2r} - \frac{1}{6} \left(\frac{\bar{s}}{2r} \right)^3 + \dots \right).$$

Introducing (5.10) yields the curvature reduction

$$k_r = -k^2 \frac{\bar{s}^3}{24R^2}, \quad (5.112)$$

which is part of the reduction formula (5.6). This reduction is less than 0.1 mm for a distance of 15 km and can be neglected. By adding (5.110) to (5.112), we obtain the total reduction from the observed distance to the chord:

$$s - \bar{s}_0 = \bar{s}(n_0 - \bar{n}) - \frac{2k - k^2}{24R^2} \bar{s}^3. \quad (5.113)$$

The reduction from the chord distance to the length of the normal section and the geodesic on the ellipsoid will be given in [6.3.2].

Special distance meters have been developed in order to measure shorter distances with very *high precision*, as required for calibration lines and for geodetic surveying, and for monitoring related to engineering projects and to geodynamic control networks. These developments are based either on instrumental refinements and better determination of the refraction effects or on the use of two or three different wavelengths.

The Kern Mekometer ME 5000 uses a He-Ne laser as a light source, with a polarization modulated wavelength of 0.6 m (Meier and Löser, 1986), Fig. 5.84. The modulation frequency (500 MHz) is automatically adjusted by means of a cavity resonator compensated for temperature change, such that the distance becomes an integer number of wavelengths. Distances of a few km can be measured with instruments of this type, and an accuracy of 0.1...0.2 mm + 0.2 ppm may be obtained, where residual refraction effects still play an essential role (Rueger and Cidder, 1987).

If the distance is measured with different wavelengths, the *dispersive* effect of air for visible light can be exploited, cf. [5.1.1]. The difference in the distances obtained with "blue" and "red" light particularly depends on the influence of temperature and atmospheric pressure on the index of refraction. If an additional microwave measurement is performed, the effect of humidity is reflected in the difference between the microwave and the light results. From (5.14), (5.15), (5.17), and (5.18), a relation between the geometric length of the path and



Fig. 5.84: Distance meter Mekometer ME 5000, Leica Geosystems AG, Heerbrugg, Switzerland.
IfE, Leibniz Universität Hannover.

the light and microwave results can be established, where a resolution of a few 0.01 mm is required. We mention the Terrameter as an realization of this strategy, which has been developed as a two-wave laser-instrument to measure distances up to 10 km with a precision of better than 0.1 mm, and which has been applied to measure crustal strain rates in California (Huggett, 1981).

5.5.3 Inertial surveying, underwater acoustic positioning

In the following we shortly describe two measurement methods which are *not* based on electromagnetic waves but use different physical signals for positioning: Inertial surveying and underwater acoustic positioning. The application of these methods is limited to areas where GNSS or classical terrestrial instruments fail or face severe problems, but GNSS techniques are generally integrated in order to strengthen the results and to connect them with the global geodetic reference frame.

Inertial positioning is based on measurements with an inertial navigation system (INS, also inertial survey system) carried on a vehicle moving in space (car, helicopter, ship, submarine, airplane, spacecraft). INSs have been originally developed for autonomous navigation in aviation and missile guidance, and found wide application in space and marine (especially submarine) navigation (Salychev, 1998; Jekeli, 2001a). An INS consists of two sensor sets mounted on a common platform (body frame) and a computer. The platform may be gyro-stabilized or body-fixed (strap-down method). The sensors are the accelerometers measuring the (linear) velocity rates of the platform, and gyros providing the orientation of the accelerometers by monitoring the angular rates of the accelerometer frame with respect to the local level resp. inertial frame (cf. [4.1.3]); accelerometers and gyros are arranged at three mutually perpendicular axes.

The evaluation of the INS outputs is based on Newton's second law of motion, extended by the effect of gravity. The fundamental observation equations (5.96) thus can be solved either for gravity or for position. Solving for gravity leads to *kinematic gravimetry* and presupposes an independent determination of the moving vehicle's kinematic acceleration, e.g., by GNSS methods, cf. [5.4.4]. By introducing gravity values derived from a model (ellipsoidal normal gravity field, global gravity field model)

or from local gravity data, on the other hand, the observation equations can be solved for the platform's acceleration. Starting from an initial point with known position and velocity, the updated position and velocity is then continuously computed by single resp. double integration with time. This method of *inertial surveying* thus offers the possibility of a nearly continuous positioning, which, in principle, works independently of an external reference (Cross, 1985; Schwarz, 1986). The *simultaneous* evaluation of the INS/DGNSS data streams for the vehicle's trajectory *and* the gravity disturbance along its path may offer some advantage, but is generally avoided. This is due to the strongly different functional and stochastic (error) models to be applied for positioning and gravity determination (Schwarz, 2006), see below and [5.2.5].

Inertial surveying started in the 1970s, with a first commercial geodetic inertial survey system developed by Litton Guidance and Control Systems. Other local-level or space-stabilized systems followed, and Kalman filtering was developed for an optimal processing of the INS survey data (Schwarz, 1983). The method has been used until recently for the establishment of geodetic control and for station densification in existing networks, in order to accelerate mapping of vast undeveloped areas, e.g., in Canada and in Brazil.

A weakness of inertial positioning is the error propagation. INS errors are characterized by the time stability of the output's bias (drift) and of the scale factor (calibration). There exists a wide accuracy range at these quantities, ranging at the bias stability from $0.0001^{\circ}/\text{h}$ to $0.1^{\circ}/\text{h}$ for the gyro's and 10^{-6} to 10^{-2} for the accelerometers, and 1 to 100 ppm for the scale factors. These errors increase with the square of time, due to the double integration from acceleration to position. This error behavior led to the zero-velocity-updating (ZUPT) procedure, where the INS results are controlled and corrected every few minutes either by a stationary measurement (at land vehicles with the condition of zero velocity) or by external information (e.g., from GPS positioning). Today, INS surveys are generally combined with GNSS, which provide control of INS error propagation and system synchronization through updating and relate the INS results to a global reference system (Fig. 5.85). The INS results (output rate 10 to 100 Hz) on the other hand, supply high spatial resolution and serve for bridging gaps due to temporal loss of GNSS signals. Integrated positioning using INS and GNSS is usually done along a



Fig. 5.85: iMAR iNAV-RQH: Inertial Laser Gyro Navigation System, courtesy M. Becker, Institut für Physikalische Geodäsie (IPG), TU Darmstadt.

traverse connecting two points with known position, and traverses may be combined to an area network. Coordinates can be calculated already nearly real-time using Kalman filter techniques, but post-processing by least-squares adjustment delivers best results. With rapid updating, relative centimeter-accuracy can be achieved now, while INS networks with zero-velocity-updating every few minutes are characterized by an accuracy of 0.1 to 0.3 m over distances of 100 km and more.

At most geodetic applications, inertial positioning cannot compete nowadays with GNSS methods, with respect to economy and accuracy. Nevertheless, there are a number of useful applications, e.g., subterranean and submarine surveys. Continuous positioning and orientation based on integrated GNSS/INS instrumentation, on the other hand, is of high interest at kinematic applications using land, sea and air vehicles. The multitude of sensor results to be georeferenced especially includes photogrammetric, laser and radar mapping, and also gravity, magnetic and other geophysical surveys (Schwarz and El-Sheemy, 2004; Vennegeerts et al., 2008).

Acoustic waves are employed for positioning on, and mapping of the ocean floor and the bottom of rivers and lakes. This is due to the fact that sound waves propagate well in water, in contrast to electromagnetic waves which are attenuated rapidly with increasing frequency. The propagation of acoustic waves through water depends on the interdependent water properties temperature (main effect), salinity and density resp. pressure. Distances between points on the sea surface and on sea bottom are derived from acoustic signals emitted from a ship-borne transducer and either reflected by the sea bottom (mapping of the ocean, lake or river floor), or sent back by a transponder established at sea floor (positioning). Acoustic *sea floor mapping* is nowadays carried out efficiently and in a global scale by multibeam sonar systems, with GNSS positioning of the survey vessel Lurton (2002), it will not be discussed here further. Precise *positioning*, on the other hand, requires the installation of sea-bottom control points, with active transponders (acoustic beacons) transmitting the received signal to the transducer on board of the ship (Fig. 5.86), Chadwell et al. (1998).

The slant range between the transducer and the transponder is calculated from the propagation time of the signal traveling forth and back, according to the two-way pulse travel time relation (5.103b). Depending on the distance between the transponders ("baselines"), the frequency of the carrier waves varies between 5 to 20 kHz,

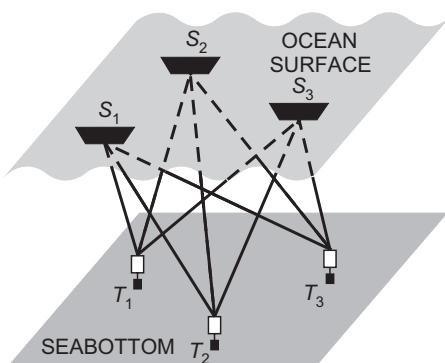


Fig. 5.86: Acoustic positioning on the sea bottom (transmitter S, transponder T).

for baseline lengths up to 10 km and more; pulse lengths are between 5 and 15 ms. Signal travel time is measured with μs -accuracy, and refraction (pulse delay and ray bending) is taken into account by empirical formulas for the effects of temperature, salinity and pressure changes. Velocity values vary between 1470 and 1540 m/s for sea water (mean value 1500 m/s), with large variations occurring within the uppermost 500 m. Baseline accuracy depends on the range and the network's configuration, and reaches the cm-order of magnitude. Relative positions of the sea floor control points are derived by spatial trilateration (Rinner, 1977), while the relation to the global reference system is established by GNSS-positioning on board of the surface vessel.

Geodetic underwater acoustic networks have been established locally for geodynamic investigations, e.g., for the observation of sea floor spreading at active ridge zones, and for monitoring crustal deformation at subduction zones (Spiess et al. (1998); Isshiki, 2000/2001/2004). Control points are usually arranged in arrays of three to four stations, with station separation of a few km to 10 km and more. The acoustic transponders are powered by batteries, with lifetime up to 5 years, or by nuclear energy sources. The connection to "stable" reference stations on land is realized through relay stations established at platforms on the sea surface (ship, buoy) or even inside the water.

5.5.4 Leveling

In *geometric leveling* (also spirit leveling or differential leveling), differences in height are determined using horizontal lines of sight between points in close proximity to each other. Leveling is conducted with a *leveling instrument* (level) and two vertically posted leveling rods (Fig. 5.87). The leveled height difference δn between the rods is given by the difference between the backsight (b) and the foresight (f) reading:

$$\delta n = b - f. \quad (5.114)$$

The *leveling instrument* consists primarily of a measuring telescope capable of rotation about the vertical axis. The line of sight is brought into the horizontal either by a coincidence bubble in conjunction with a tilting screw or, for most modern instruments, automatically by a compensator that is comprised mainly of a gravity

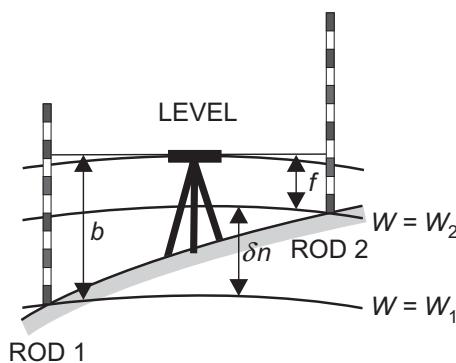


Fig. 5.87: Geometric leveling principle.



Fig. 5.88: Bubble precision level NABON, courtesy Breithaupt, Kassel/Germany.

pendulum (first introduced with the ZEISS Ni2 level in 1950). A setting accuracy of $0.2''$ to $0.5''$ is achieved by both methods. The use of a compensator increases the speed of leveling and reduces the sensitivity with respect to temperature variations. On the other hand, a spirit level is less sensitive with respect to high-frequency oscillations as produced by traffic, machinery or wind. Thus it may still offer advantages at high precision industrial and engineering surveys, Fig. 5.88.

High-precision levels employ telescopes with an aperture of 40 to 50 mm and a magnification of 30 to 40 or more. Lines of sight (distance between the level and the rods) depend on leveling purpose and topography, and are kept within 30 to 50 m at precise leveling. Setting-up the instrument in the middle of two subsequent rod positions is usual, as it eliminates errors due to non-parallelism of the collimation and the bubble axes as well as symmetric refraction effects (see below). In the *analog* mode, the leveling rods carry two graduation lines on invar tape, displaced against each other and numbered differently in order to detect reading errors. The line of sight is adjusted to the closest graduation mark by means of a parallel plate mounted in front of the objective's lens. The amount of the displacement is measured by a micrometer (Fig. 5.89).

Digital levels were introduced with the Wild NA 2000 (Ingensand, 1990). They are used in connection with invar staffs that carry a binary code (division e.g., 0.3 mm), Fig. 5.90. A code section around the horizontal sight is projected on a CCD sensor in the image plane of the telescope. A subsequent processing of the image by a microprocessor includes electronic scanning (A/D conversion) and correlation with a digital reference signal, whereby the automatically measured distance has to be taken into account. Special calibration procedures have been developed for digital levels and staffs (Rueger and Brunner, 2000).



Fig. 5.89: Automatic level (Wild/Leica NA2), courtesy Leica Geosystems AG, Heerbrugg, Switzerland.



Fig. 5.90: Digital level (Trimble DiNi Level), courtesy Trimble Navigation Ltd., Sunnyvale, CA, U.S.A.

In order to transfer heights over larger distances, the individual leveled differences are summed. For one set-up, the non-parallelism of the level surfaces may be neglected (quasi-differential method). The observed difference δn then corresponds to the height difference of the level surfaces passing through the rod sites. Summing the individual differences between two bench marks P_1 and P_2 yields the “raw” leveled height difference

$$\Delta n_{1,2} = \sum_1^2 \delta n. \quad (5.115)$$

At longer distances, the effect of the non-parallelism may reach the cm-order of magnitude and more, cf. [3.2.1]. Hence Δn depends on the path taken and does not provide a unique height. A unique height determination can only be achieved by considering gravity g , that is by referring to potential differences ΔW . According to (3.52) we have

$$\Delta W_{1,2} = W_2 - W_1 = - \int_1^2 g dn \approx - \sum_1^2 g \delta n. \quad (5.116)$$

Thus potential differences can be determined without any hypothesis from leveling and surface gravity. In order to obtain height differences in any specific height system from the raw leveling results, gravity reductions have to be applied, cf. [6.4.1].

The accuracy of precise leveling depends on many effects. Some of the leveling errors behave in a random manner and propagate with the square root of the number of individual setups. Other errors are of systematic type and may propagate with distance in a less favorable way. Hence, particular attention must be afforded to reduce them, by instrumental measures and modeling or by employing dedicated measurement methods. We mention the main *error sources* (Kukkämäki, 1980):

Misleveling of the instrument is of random type and results in an error of a few 0.01 mm for an individual height difference. Residual adjustment errors at a *bubble* instrument cancel at “leveling from the middle”. An imperfect operation of the *compensator* causes an “obliquity of

the horizon" which is eliminated by measuring in two opposite positions of the compensator. *Magnetic effects* on the compensator are kept small generally, but a regular control is advisable. *Rod graduation errors* include a "mean" scale error, errors of the individual graduation marks, and effects of thermal expansion. Routine calibrations deliver the corresponding corrections, with a remaining random part less than 5 to 10 μm (Rueger and Brunner, 2000). *Rod inclination* errors can be kept sufficiently small by properly adjusting the rod bubble and carefully holding the rod in the vertical position. Local *vertical movements* (0.01 to 0.1 mm per station) of the rods may occur during the measuring process, depending on the stability of the ground. If proportional to time, they cancel by forward and backward leveling runs.

Vertical refraction, cf. [5.1.2], contains an irregular (shimmer) and a systematic part. The first one acts as a random error, reaching 0.01 mm under cloudy skies. Systematic effects particularly affect observations made close to the ground or in terrain with steep slopes. These effects may reach 0.01 to 0.1 mm per 1 m height difference. They can be modeled in part by a refraction correction, with the vertical temperature gradient as a function of height, and eventually additional information about the environment (Angus-Leppan, 1984). The time-variable effect of the *Earth tides* plays a role at extended leveling networks, causing periodic inclinations of the line of sight. These can be modeled by the horizontal tidal component acting in the azimuth of the leveling line. Starting from (3.119) and taking the elasticity of the Earth into account, the tidal reduction for the moon reads

$$\delta_{t(m)} = 0.06 \sin 2 \psi_m \cos(\alpha_m - \alpha) s \text{ mm/km.} \quad (5.117)$$

Here, α_m and α are the azimuths of the moon and of the leveling line, and ψ_m is the geocentric central angle between the directions to the moon and the computation point; s is the length of the leveling line in km. The same equation is valid for the sun, with an effect of 46% of that for the moon (Kukkamaki, 1949).

In order to eliminate or reduce systematic errors, precise leveling is always carried out with equal back and foresights ("leveling from the middle") at less than 50 m distance. Observations should be performed during cloudy weather, preferably in the morning and in the evening hours. Line of sights very close to the ground (0.5 m or less) should be avoided. Leveling is generally conducted twice, in opposing directions and possibly under different meteorological conditions. For a 1 km double-run leveling, one can attain an accuracy of 0.2 to 1.0 mm.

The time needed for precise leveling can be significantly reduced by *motorized leveling*, whereby the instrument and the rods are carried in and operated from an automobile. This mode also reduces time dependent errors and partially eliminates asymmetric refraction effects, as the line of sight is more remote from the ground (Peschel, 1974; Becker, 2002).

For leveling across broad waterways and inlets of the sea, several methods have been developed. In *reciprocal leveling*, approximately horizontal sights to specially designed targets are taken simultaneously with precise levels from both sides of the waterway. For longer series of observations including a change of the instruments, height differences over 1 to 2 km can be determined with a precision of 1 to 2 mm (Kakkuri, 1966). Larger distances can be bridged by *hydrostatic leveling* based on the principle of communicating tubes. A hose filled with water (free of air bubbles, uniform temperature) is laid between the shores of the watercourse, and the water level at the vertical ends of the hose is observed, assuming that it represents the same level surface. In *hydrodynamic leveling* (geostrophic leveling), the height is transferred over the waterway utilizing water level records, which have to be reduced for the effects of sea surface topography, cf. [3.4.2]. This implies the use of a hydrodynamic model, which takes water velocity,

wind drag, water depth and bottom friction, atmospheric pressure and water density into account, as well as gravity and Coriolis force.

Hydrostatic leveling has been applied for ranges up to 20 km (e.g., Fehmarn-Belt/Baltic Sea) and delivers mm-precision (Andersen, 1992). In the Netherlands, it was used in an operational mode for measurements off-shore and through rivers and canals (Waalewijnen, 1964). Hydrodynamic leveling was employed, for instance, for a height transfer over the British channel (70 km), with a precision of about 1 cm (Cartwright and Crease, 1963).

5.5.5 Tilt and strain measurements

Tilt and strain observed on the surface of the Earth indicate the response of the Earth's crust (crustal deformations) to external and internal forces such as Earth tides, tectonic processes, and seismic and volcanic activities. Tilt and strain are dimensionless quantities and are given in radian or arcsec and (relative) extension (positive sign) or compression per distance, respectively.

Over time intervals of years to decades, long-term tilt and strain can be determined from repeated observations of geodetic control networks, delivering relative displacements between the observation sites. Classical terrestrial techniques as triangulation, trilateration and leveling could only detect the integral deformation effect over large time spans (years to decades), while satellite techniques as GPS are now able to continuous recording of absolute site displacements, in horizontal position and height, cf. [8.3.3]. Tiltmeters and strainmeters (also called extensometers), on the other hand, have been developed in order to monitor continuously *local* deformations (Agnew, 1986; Zadro and Braatenberg, 1999).

Short-term (up to 1 day) tilt and strain is dominated by tidal deformations and is at the order of 10^{-8} to 10^{-7} , which correspond to inclinations of $0.002''$ to $0.02''$ and lengths changes of 0.01 to 0.1 $\mu\text{m}/\text{m}$. *Long-term* effects of tectonic origin generally are only at the order of a few $10^{-7}/\text{year}$. Episodic effects related to seismic or volcanic events may reach the same order of magnitude and more over a few hours to a few weeks and months. Consequently, the instrumental *sensitivity* of tilt and strainmeters should be at least about 10^{-9} to 10^{-10} , and the stability with time should be better than $10^{-7}/\text{year}$. A variety of tiltmeters and strainmeters has been developed over the past 50 years and operated underground in order to reduce the strong disturbances of atmospheric and hydrological origin. Instrumental noise was remarkably reduced at the transition from analogue to digital recording.

Tiltmeters measure the inclination of the Earth's surface with respect to the local vertical. Two mutually perpendicular sensors are needed in order to completely determine the tilt, which are usually orientated in the NS and EW-directions. Tiltmeters have been designed as horizontal and vertical pendulums, electronic tiltmeters, and long water tubes (Zürn et al., 1986).

Horizontal pendulums consist of two nearly vertical threads that support an approximately horizontal beam with an attached mass (Zöllner suspension), Fig. 5.91. Because of the small inclination of the rotational axis with respect to the vertical, a tilt of the support (basis about 30 cm) or a plumb line variation cause a strongly amplified angular deflection (astatization), which may be further enlarged optically. Fused quartz (Verbaandert-Melchior pendulum) or metallic alloys are used as pendulum material in order to keep thermal effects small. Calibration is performed by controlled tilting of the instrument (Van Ruymbeke, 1976). Among the *vertical*

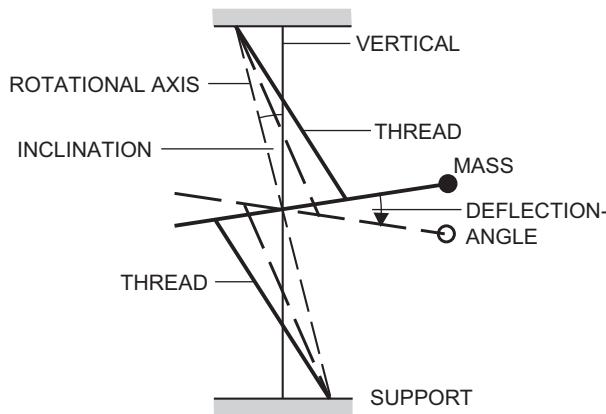


Fig. 5.91: Zöllner horizontal pendulum principle.

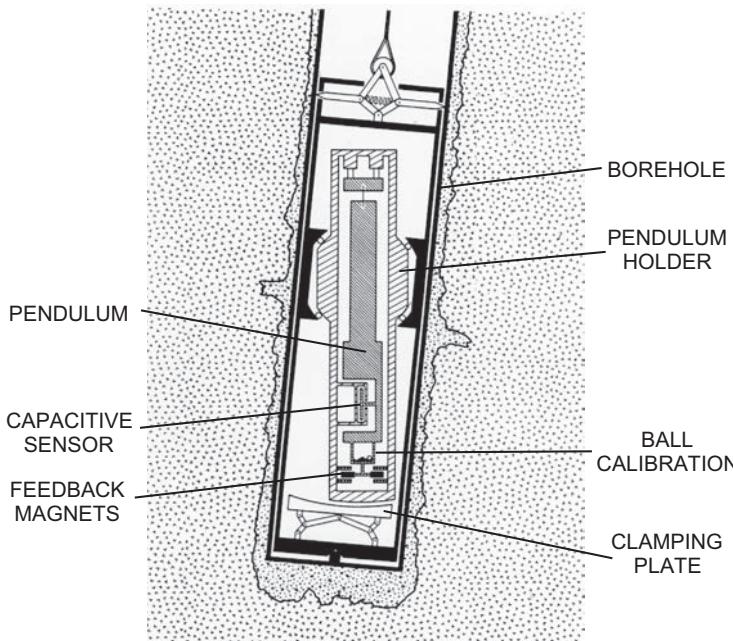


Fig. 5.92: Vertical pendulum “Askania borehole tiltmeter”, Bodenseewerk Geosystem, Überlingen, Germany, after Flach (1976) and Agnew (1986).

pendulums is the Askania borehole instrument (length 60 cm) which may operate in depths of 20 to 60 m (Fig. 5.92). The pendulum's suspension allows it to swing freely, and the deflections are sensed by two three-plate capacitive transducers installed at right angles to each other. The pendulum is calibrated by displacing a small mass over a known distance (Flach, 1976). Short-base electronic *tiltmeters* (e.g., the Hughes tiltmeter) use electrodes as sensors to measure

a bubble's position, or record the floating of the sensing mass in a magnetic field; these instruments are especially adapted for the installation in boreholes. *Water-tube tiltmeters* with lengths of several 100 m have also been developed, and installed in cavities. Tilt is derived from the water level variations at the endpoints of the tube which are measured by capacitive or interferometric methods (Kääriäinen, 1979).

Strainmeters measure relative displacements of the Earth's crust (King and Bilham, 1973). For a complete determination of the strain tensor, which contains six independent components, a strain meter array should be arranged with orientation in different spatial directions, although in most cases only horizontal strainmeters have been installed. Strainmeter constructions use mechanical or laser length standards, with baseline lengths from 0.1 m to 1 km.

Short-baseline strainmeters (baseline length 10 to 30 m and more) are represented by *invar wires* and fused *quartz tube* rods. One end of the instrument is fixed to the rock, and the crustal displacement is measured at the other end by inductive or capacitive transducers (King and Bilham, 1973), Fig. 5.93. Borehole strainmeters were developed since the 1960s, including a hydraulic dilatometer (Myren et al., 2006) and a 3-component rod strainmeter of 0.1 m-baselength (Gladwin et al., 1987). *Laser strainmeters* apply the Michelson interferometer principle. Operated in an evacuated tube, they can measure distances up to 1 km with nm resolution and better (Berger and Levine, 1974; Takemoto et al., 2006).

Among the *instrumental errors* of tiltmeters and strainmeters are the uncertainties of the calibration (about 0.1 to 1%) and the direct effects of temperature and air pressure variations, which are kept small by the selection of the material and appropriate shielding. Long-term drift effects are at the order of 10^{-6} to 10^{-7} /year and to a large part are due to problems inherent with the sensor-rock coupling. Effects induced by *atmospheric* and *hydrological* variations (air temperature, air pressure, solar radiation, rainfall, groundwater) pose severe problems in interpreting the results, especially for tiltmeters. These disturbances pronounce daily and seasonal periods but also happen at other time scales, they severely obscure tidal, tectonic and other geodynamic signals. Modeling of these effects, with frequency bands including those of the Earth tides and the seismotectonic deformations, is still in its infancy. Consequently, their influence is reduced by installing the instruments below the Earth's surface, in tunnels, mines, natural caves, and boreholes. Unfortunately, this strategy causes other problems to be discussed in the following.

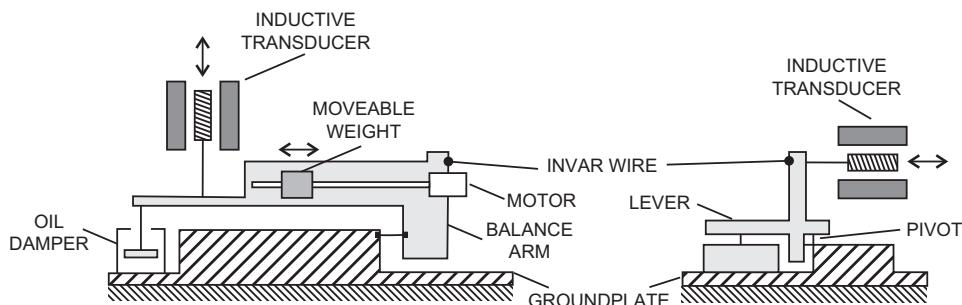


Fig. 5.93: Invar wire strainmeter, courtesy Black Forest Observatory Schiltach.

When installing tiltmeters and strainmeters below the Earth's surface, *geologic*, *topographic*, and *cavity* effects in most cases produce large local distortions of the tiltmeter and strainmeter data. This is due to variable rock properties including local fractures, rugged topography, and different cavity reactions to deformation. Local distortion may reach 10 to 15% and more, leading to non-representative results (Harrison, 1976). Attempts to model these effects have been only partly successful (Sato and Harrison, 1990; Kohl and Levine, 1995). Consequently, in addition to carefully selecting the observation site, preference now is given either to short-base tiltmeters and strainmeters operating in boreholes (if possible with depths of 100 m or more) or to long-baseline instruments installed in tunnels or cavities. In the latter case, local effects are reduced by integrating over the large distance of some 10 to some 100 m.

Tilt and strain is measured continuously at underground observatories and dedicated networks, frequently in connection with GNSS observations and gravity recording. Extensive observations started with the "International Geophysical Year" (1957), and concentrate now on regions of seismotectonic and volcanic activity, as the western United States, Japan, China, and Italy. A strong impetus also for tilt and strain techniques came from national earthquake prediction programs, as e.g., established in Japan and China. Among the participating observatories we have the Piñon Flat Observatory/California (Institute of Geophysics and Planetary Physics, University of California, Wyatt et al., 1990), the observatories of the Research Center for earthquake Prediction/Disaster Prevention (Kyoto University, Japan) and other Japanese institutions, the observation sites and observatories under the responsibility of the China Seismological Bureau, and the Black Forest Observatory Schiltach (Karlsruhe Institute of Technology KIT and University of Stuttgart, Germany). Extended geodetic networks for monitoring surface displacements due to plate tectonics have been installed, among others, in Japan (Takemoto, 1995) and in the western United States. Here, the Earth Scope Plate Boundary Observatory (PBO) started operation in 2008. This National Science Foundation funded project now coordinates the operation of more than 1000 permanent GPS stations (with partly one Hertz or higher frequency and one second and less latency) and a number of borehole and laser strainmeters, located along the Pacific/North-American plate boundary (Agnew, 2007). The strategy of obtaining "real-time" data for actual crustal movements is pursued also at the global differential GPS network (more than 100 stations) of JPL/NASA (Kechine et al., 2003). Tiltmeter networks have been established especially at active volcanoes, e.g., at the Kilauea/Hawaii and Mount Etna/Italy.

Tiltmeter and strainmeter results contribute to Earth tide research in the short-periodic part and to the detection of anomalous tilt and strain related to seismic and volcanic activity, cf. [8.3.4], [8.3.6].

6 Methods of Positioning and Gravity Field Modeling

Geodetic evaluation methods may be separated into positioning and gravity field determination (the determination of the Earth's rotation parameters is not pursued in the following, as it has been discussed in connection with global reference systems [2] and measuring techniques [5]). This separation is possible because positioning only requires an approximate knowledge of the gravity field, and gravity field modeling needs only approximate positions. The linearization of the gravity field is essential in both cases, and it permits a statistical field description [6.1]. Nowadays, positioning is based on three-dimensional models [6.2], while classical strategies distinguish between horizontal positioning [6.3] and height determination [6.4]. Gravity field modeling utilizes all kind of gravity field related observables, it can be formulated in the form of boundary-value problems of potential theory [6.5]. Global models are derived mainly from the results of space geodesy, with additional information from terrestrial observations [6.6]. Local gravity field estimation, on the other hand, is primarily based on terrestrial gravity field data, and generally supported by satellite results [6.7]. Least-squares collocation represents another efficient method for transformation and combination of gravity field quantities, and is now routinely applied for regional and local solutions [6.8].

The *simultaneous* determination of station coordinates *and* gravity field quantities, together with other parameters of different kind, in *one* mathematical model has been designated as *integrated* or *operational* geodesy (Eeg and Krarup, 1973; Hein, 1986). Employing all relevant data and taking the errors of the data into account, functional modeling finally leads to least-squares adjustment. The combination strategy allows to more completely exhaust the information content of the data, and to improve the accuracy and reliability of the results. On the other hand, the large amount of data and unknown parameters (at least at global and regional dimensions) raises serious problems with respect to proper weighting of the observations, modeling of systematic effects, and data processing. Hence, the application of deterministic combination methods is restricted to a limited number of observations and unknown geometric and physical parameters, recent examples being the "satellite-only" Earth models calculated since the early days of satellite geodesy, cf. [6.6.2]. An alternative (and extended) approach to combined modeling of geometric and physical quantities is least-squares collocation with parameters (Moritz, 1980, p. 111 ff.), where again for practical reasons the geometric part of the problem is treated separately from the gravimetric part. The *integration* of geodetic techniques and the consistent *combination* for geometry, gravity field and Earth rotation is a fundamental part of the Global Geodetic Observing System (GGOS) established by IAG, cf. [1.4.2], Plag and Pearlman (2009).

Geodetic evaluation methods are described in textbooks on geodesy, e.g., Bomford (1980), Moritz (1980), Vaniček and Krakiwsky (1986), Heck (2003a), Hofmann-Wellenhof and Moritz (2005). The theory of errors and adjustment methods applied to geodetic modeling are discussed in Koch (1999), Grafarend (2006), Niemeyer (2008) and Ghilani (2010), among others.

6.1 Residual gravity field

The actual gravity field can be sufficiently well approximated by the normal gravity field of the level ellipsoid, cf. [4.2.2], which results in linear relations between the residual observations and the unknown gravity field parameters. The fundamental quantity of the residual gravity field is the disturbing potential. It is closely related to the height anomaly and the geoid height [6.1.1]. The residual gravity vector generally is expressed by its scalar components, the gravity anomaly or the gravity disturbance and the deflection of the vertical [6.1.2]. On certain assumptions, the residual gravity field may be treated by statistical methods, which is of importance in gravity field interpolation and modeling [6.1.3].

6.1.1 Disturbing potential, height anomaly, geoid height

Approximation of the Earth's gravity potential W (3.42) by the normal gravity potential U (4.37) leads to the *disturbing potential* (also anomalous potential) T defined at the point P :

$$T_p = W_p - U_p. \quad (6.1)$$

W and U contain a gravitational and a centrifugal part. As the centrifugal acceleration of the Earth is known with high accuracy, cf. [3.1.4], we may assume that the centrifugal parts of W and U are identical. The disturbing potential then is formed by the difference of the gravitation of the Earth and of the level ellipsoid, and thus is a harmonic function outside the Earth's masses. Hence, it obeys Laplace's differential equation (3.29)

$$\Delta T = 0, \quad (6.2)$$

where Δ stands for the Laplace operator. T can be expanded into spherical harmonics, in analogy to the corresponding development for the gravitational potential (3.89) and (4.45). Expressed in spherical coordinates r, ϑ, λ , the disturbing potential as a spatial function reads, in abbreviated form, see (3.88):

$$T = T(r, \vartheta, \lambda) = \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^{l+1} T_l(\vartheta, \lambda). \quad (6.3)$$

In its full form this development reads as

$$T = \frac{GM}{r} \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta C_{lm} \cos m\lambda + \Delta S_{lm} \sin m\lambda) P_{lm}(\cos \vartheta), \quad (6.4)$$

where the ΔC_{lm} and ΔS_{lm} are the residual harmonic coefficients, being defined as differences between the coefficients of the actual and the normal gravity field. Comparing (6.3) and (6.4) yields the *surface spherical harmonics*

$$T_l = \frac{GM}{a} \sum_{m=0}^l (\Delta C_{lm} \cos m\lambda + \Delta S_{lm} \sin m\lambda) P_{lm}(\cos \vartheta). \quad (6.5)$$

Due to the properties of U , only the even zonal residual coefficients differ from the actual gravity field coefficients C_{lm} , while all the other ΔC_{lm} are identical with the actual gravity field parameters, cf. [4.2.2]. The development of (6.3) and (6.4) starts at $l = 2$ since equality of the masses of the Earth and the ellipsoid is assumed, as is coincidence of the center of the Earth's masses with the center of the ellipsoid, cf. [3.3.4].

The disturbing potential is closely related to the vertical distance between P and the point Q located on the spheroidal surface $U = U_Q$, cf. [6.5.1]. Q is associated with P by the condition

$$U_Q = W_P, \quad (6.6)$$

cf. [4.2.3], Fig. 6.1. This distance is called *height anomaly* ζ . Geometrically, it is the difference between the ellipsoidal height h and the normal height H^N (3.107), (4.66):

$$\zeta = h - H^N, \quad (6.7)$$

where we have neglected the slight curvature of the normal plumb line. The surface for which (6.6) holds at every point is called the *telluroid* (Hirvonen, 1960; Grafarend, 1978b). A corresponding relation holds at any point in the exterior space.

The telluroid represents an approximation to the physical surface of the Earth. By extending H^N downward from P we obtain the *quasigeoid*, which is often used as a zero height surface, cf. [3.4.3], [7.2]. The height anomaly ζ now becomes the distance between the level ellipsoid $U = U_0$ and the quasigeoid, and is also called quasigeoid height.

If P is located on the geoid, we obtain the *geoid height* N (also called geoid undulation) as the vertical distance between the ellipsoid and the geoid. In analogy to (6.7), a geometric definition follows by differencing the ellipsoidal height h and the orthometric height H (3.106):

$$N = h - H, \quad (6.8)$$

where again the effect of the plumb line curvature has been neglected.

The difference between the geoid height and the height anomaly is equal to the difference between the normal height and the orthometric height and follows from (3.106) and (3.107):

$$N - \zeta = H^N - H = \frac{\bar{g} - \bar{\gamma}}{\bar{\gamma}} H = \frac{\Delta g_B}{\bar{\gamma}} H. \quad (6.9)$$

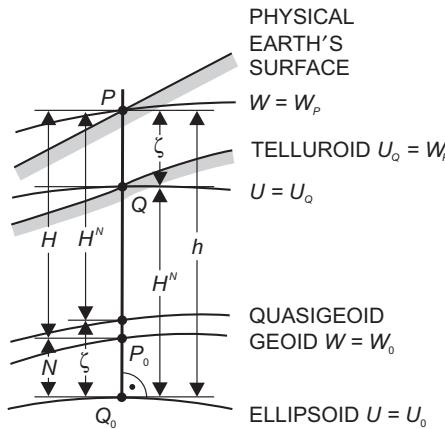


Fig. 6.1: Ellipsoidal, normal and orthometric height.

The difference depends on the height and thus is zero on the oceans, if we neglect the small effect of sea surface topography, cf. [3.4.2]. It also depends on a “mean” gravity anomaly $\bar{g} - \bar{\gamma}$, which (approximately) corresponds to the Bouguer anomaly $\Delta g_{B'}$ to be introduced in [6.5.3].

6.1.2 Gravity disturbance, gravity anomaly, deflection of the vertical

The gravity vector \mathbf{g} at P can be approximated by the vector of normal gravity $\boldsymbol{\gamma}$, which leads to the *gravity disturbance*

$$\delta\mathbf{g}_P = \mathbf{g}_P - \boldsymbol{\gamma}_P \quad (6.10)$$

see Fig. 6.2. Neglecting the small angle between the directions of \mathbf{g} and $\boldsymbol{\gamma}$ (deflection of the vertical), we obtain the magnitude of the gravity disturbance

$$\delta g_P = g_P - \gamma_P \quad (6.11)$$

g can be measured on the Earth’s surface and in the exterior space. The calculation of γ_P presupposes the knowledge of the geodetic coordinates (ellipsoidal latitude and height) of P . This is nowadays possible through geodetic space techniques (mainly GNSS methods), while classical geodesy had to consider the ellipsoidal coordinates as unknowns, cf. [6.3], [6.4]. This fact posed a serious problem with the height coordinate, as only normal or orthometric heights determined by leveling were available, cf. [3.4.3]. Consequently, gravity field modelling, instead of the gravity disturbance, employed (and generally still employs today) the *gravity anomaly*

$$\Delta\mathbf{g}_P = \mathbf{g}_P - \boldsymbol{\gamma}_{Q'} \quad (6.12)$$

with the magnitude

$$\Delta g_P = g_P - \gamma_{Q'} \quad (6.13)$$

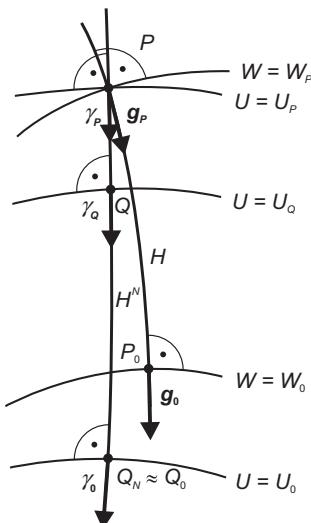


Fig. 6.2: Actual and normal gravity.

Again, Q is related to P by the condition (6.6). γ_Q can be calculated by (4.63), starting from normal gravity γ_0 on the ellipsoid (4.41) and replacing h by H^N (3.107). This free-air reduction is given by (4.61):

$$\delta g_F^N = -\frac{\partial \gamma}{\partial H^N} H^N. \quad (6.14)$$

The *free-air gravity anomaly*, defined on and outside the Earth's surface according to Molodensky, reads

$$\Delta g_F^N = g + \delta g_F^N - \gamma_0. \quad (6.15)$$

In many applications, $\frac{\partial \gamma}{\partial H^N}$ is approximated by a mean value of $-3.086 \text{ } \mu\text{ms}^{-2}/\text{m}$.

The determination of the *geoid* requires that the gravity anomalies are given everywhere on that level surface. Furthermore, in order to apply the Laplace equation, the masses outside the geoid have to be removed. Several types of gravity reductions are available for this purpose. The methods differ by the manner in which the topographical masses are displaced, and gravity is reduced onto the geoid. The gravity anomaly on the geoid then is defined as the difference between the gravity on the geoid g_0 and the normal gravity γ_0 on the ellipsoid (Fig. 6.2):

$$\Delta g = g_0 - \gamma_0. \quad (6.16)$$

Dependent on the kind of reduction, different types of geoid related *gravity anomalies* have been defined, serving not only for the determination of the geoid but also for gravity field interpolation and geophysical interpretation, cf. [6.5.3].

According to the previous definitions, gravity disturbance and gravity anomaly are vector quantities. Their directions are given through the difference between the direction of the actual plumb line and a reference direction defined in the normal gravity field. This difference is called *deflection of the vertical* (Fig. 6.3). With respect to the reference direction, we distinguish between three kinds of vertical deflection, which differ only slightly (Jekeli, 1999):

- The deflection of the vertical θ^N defined on the surface or the exterior of the Earth, with the direction of the normal plumb line at Q as a reference (Molodensky definition). The reference direction practically coincides with the surface normal to $U = U_p$ at P .

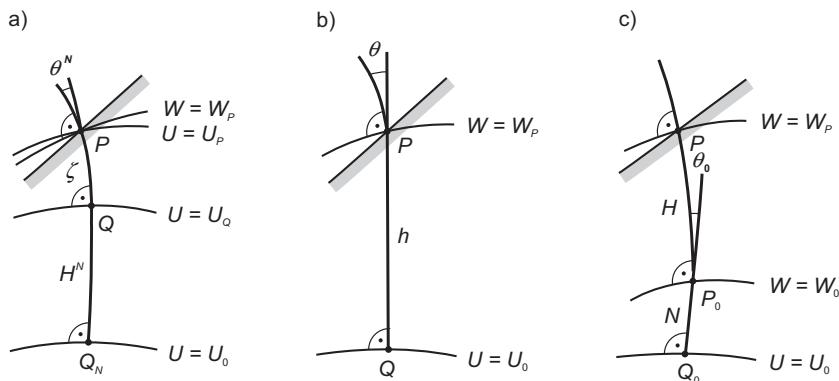


Fig. 6.3: Deflection of the vertical according to a) Molodensky, b) Helmert, c) Pizetti.

- The deflection of the vertical θ at the Earth's surface, referring to the ellipsoidal normal at P (*Helmer definition*). It differs from θ^N only by the slight curvature (effect of a few 0.1") of the normal plumb line, cf. [4.2.3]. This definition is preferred generally, as the ellipsoidal normal is provided by the geodetic coordinates.
- The deflection of the vertical θ_0 defined on the geoid (*Pizetti definition*). It is given by the difference between the actual plumb line on the geoid and the ellipsoidal normal. It differs from the previous definitions by the curvature of the actual plumb line and is of importance for the determination of the geoid.

The deflection of the vertical is expressed either by its magnitude θ and its azimuth α_θ or, more generally, by its components in the north-south and east-west directions. A geometric derivation follows from spherical trigonometry on the unit sphere around the calculation point (Fig. 6.4). Here, we assume that the minor axis of the reference ellipsoid is parallel to the Z -axis of the global reference system and that the ellipsoidal initial meridian is parallel to the X -axis. These conditions are practically fulfilled with modern reference systems and well approximated by classical geodetic systems, cf. [6.2.2]. After parallel displacement, we identify N as the point of intersection of the Z -axis with the unit sphere and Z_a and Z_g as the directions to the astronomic and the geodetic zenith, respectively. The deflection of the vertical represents the spherical distance between Z_a and Z_g , its azimuth is denoted by α_θ . The deflection is decomposed into the meridional component ξ (positive when Z_a is north of Z_g) and the component in the prime vertical η (positive when Z_a is east of Z_g). Along the azimuth α to a target point P_α we have the vertical deflection component ε .

From spherical trigonometry we get

$$\sin \varphi = \cos \eta \sin(\Phi - \xi), \quad \sin \eta = \cos \varphi \sin(\Lambda - \lambda),$$

and with

$$\cos \eta \approx 1, \quad \sin \eta \approx \eta, \quad \sin(\Lambda - \lambda) \approx \Lambda - \lambda,$$

the components are given by (linear approximation)

$$\xi = \Phi - \varphi, \quad \eta = (\Lambda - \lambda) \cos \varphi. \quad (6.17)$$

According to Fig. 6.4, the component ε in the azimuth α is composed by two parts:

$$\varepsilon = \xi \cos \alpha + \eta \sin \alpha. \quad (6.18)$$

These relations can also be derived by subtracting (4.36) from (3.45), after corresponding linearization, cf. [6.2.2].

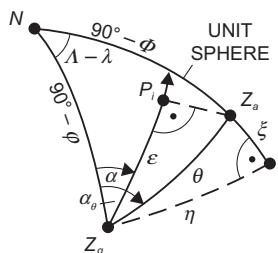


Fig. 6.4: Vertical deflection components.

Equations (6.17) and (6.18) are valid for *any definition* of the deflection of the vertical.

The residual gravity field quantities (disturbing potential, height anomaly/geoid height, gravity disturbance/gravity anomaly, deflection of the vertical and others) depend on the geodetic Earth model used for approximating the gravity field and on its orientation with respect to the Earth, cf. [6.2.2]. If referred to a *geocentric* mean Earth ellipsoid, they are designated as *absolute* quantities, otherwise they are *relative* only. The root mean square variation of absolute height anomalies and geoid heights is ± 30 m (maximum values about 100 m). The free-air gravity anomalies vary by about $\pm 400 \mu\text{ms}^{-2}$ (maximum values of a few $1000 \mu\text{ms}^{-2}$) and the deflections of the vertical by $\pm 7''$ (maximum $30''$ to $1''$ in the high mountains), cf. [6.1.3], [6.6.3].

6.1.3 Statistical description of the gravity field, interpolation

The residual gravity field can be viewed as a realization of a stochastic process and treated by statistical methods (Moritz, 1970; Tscherning, 1978). The gravity anomaly is used as a fundamental gravity field parameter in this aspect, as gravity data are available with high resolution on the continents and on the oceans. Other type gravity field observations are either restricted to the long-wave part of the gravity field (satellite derived spherical harmonic coefficients) or to the oceanic (satellite altimetry) respectively continental (deflections of the vertical) parts of the Earth's surface.

We assume that the *mean value* of the gravity anomalies Δg corresponding to the zero-degree term of the spherical harmonic expansion of Δg over the Earth (spherical approximation) is zero, cf. [6.5.4]:

$$M\{\Delta g\} = \frac{1}{4\pi} \iint_{\sigma} \Delta g \, d\sigma = 0, \quad (6.19)$$

where $M\{\cdot\}$ is the mean value operator, and σ represents the unit sphere with the area of 4π . The surface element can be expressed in spherical coordinates ϑ, λ by

$$d\sigma = \sin \vartheta \, d\vartheta \, d\lambda. \quad (6.20)$$

The further statistical behavior of Δg is described by the *covariance function*

$$C(\psi) = \text{cov}_{\psi} (\Delta g) = M\{\Delta g \Delta g'\}_{\psi}. \quad (6.21a)$$

It is defined as the mean value of all products of gravity anomalies at the points $P(\Delta g)$ and $P'(\Delta g')$ having constant spherical distance ψ on the unit sphere. $C(\psi)$ shall *only* depend on ψ and neither depend on the position (homogeneity of the anomalous gravity field) nor on the azimuth of the line PP' (isotropy), Grafarend (1976). The evaluation of (6.21a) leads to

$$C(\psi) = \frac{1}{2\pi} \cdot \frac{1}{4\pi} \int_{\lambda=0}^{2\pi} \int_{\vartheta=0}^{\pi} \int_{\alpha=0}^{2\pi} \Delta g \Delta g' \sin \vartheta \, d\vartheta \, d\lambda \, d\alpha = \frac{1}{4\pi} \iint_{\sigma} \{\Delta g \Delta g'\}_{\psi} \, d\sigma. \quad (6.21b)$$

$C(\psi)$ describes the distance dependent correlation of the gravity anomalies, which decreases with increasing distance. For $\psi = 0$, we have $\Delta g = \Delta g'$, and the covariance transforms into the *anomaly variance*

$$\sigma^2(\Delta g) = M\{\Delta g^2\} = \frac{1}{4\pi} \iint_{\sigma} \Delta g^2 \, d\sigma. \quad (6.22)$$

From the theory of stochastic processes, the statistical properties should be derived from an infinite number of process realizations. As only one realization of the gravity field is available,

the hypothesis of ergodicity is necessary, which states that the statistical quantities may also be calculated from mean values over one realization only (Moritz, 1980, p. 269).

As shown in [6.6.1], Δg as a functional of T can be expanded into spherical harmonics. On the Earth's surface ($r = R$) the abbreviated form of this expansion reads

$$\Delta g(\vartheta, \lambda) = \sum_{l=2}^{\infty} \Delta g_l(\vartheta, \lambda), \quad (6.23)$$

with Δg_l Laplace's surface harmonics, cf. [3.3.2]. With the conventions of mass equality between the Earth and the reference ellipsoid, and geocentric position of the ellipsoid, the terms of degree 0 and 1 are missing again, cf. [6.1.1]. As a consequence of (6.23), $C(\psi)$ can also be expanded into spherical harmonics in the definition range $0 \leq \psi \leq \pi$:

$$C(\psi) = \sum_{l=2}^{\infty} c_l P_l(\cos \psi), \quad (6.24a)$$

with $P_l(\cos \psi)$ Legendre polynomials. Because of isotropy, only zonal terms exist in (6.24a). As is well known from potential theory, the harmonic coefficients c_l can be derived by inversion, applying orthogonality relations:

$$\begin{aligned} c_l &= \frac{2l+1}{4\pi} \int_{\alpha=0}^{2\pi} \int_{\psi=0}^{\pi} C(\psi) P_l(\cos \psi) \sin \psi d\psi d\alpha \\ &= \frac{2l+1}{2} \int_{\psi=0}^{\pi} C(\psi) P_l(\cos \psi) \sin \psi d\psi. \end{aligned} \quad (6.24b)$$

Corresponding equations are valid for fully normalized spherical harmonics, cf. [3.3.2], with

$$C(\psi) = \sum_{l=2}^{\infty} \bar{c}_l \bar{P}_l(\cos \psi) \quad (6.25a)$$

and

$$\bar{c}_l = \frac{c_l}{\sqrt{2l+1}}. \quad (6.25b)$$

Equation (6.24b) can be solved for a known covariance function by numerical integration. By inserting (6.21) into (6.24b), and taking (6.23) into account, we finally obtain

$$c_l = M\{\Delta g_l^2\} = \sigma_l^2(\Delta g). \quad (6.26)$$

Hence, the coefficients are given by the *anomaly degree variances* defined as mean values over the squares of Δg_l , and related to the degree variances of the residual harmonic coefficients, cf. [6.6.1].

A good approximation to reality is provided by the Tscherning and Rapp (1974) – degree variance model and the related covariance function, both have been successfully applied to date. The Tscherning-Rapp-model is based on satellite-derived harmonic coefficients for the degrees 2 to 10 and a set of 1° equal area anomalies (approximately quadratic compartments with constant area $110 \text{ km} \times 110 \text{ km}$). The variance of the point anomalies is $\sigma^2(\Delta g) = (424 \mu \text{m s}^{-2})^2$ and that of the mean anomalies $\sigma^2(\overline{\Delta g})_{1^\circ} = (303 \mu \text{m s}^{-2})^2$. The transition from the variance/covariance of point to mean anomalies has been performed per degree by a smoothing factor, which depends on the cap radius of the mean anomaly block (here $1^\circ \times 1^\circ$). As seen from Fig. 6.5, the correlation of the $1^\circ \times 1^\circ$ -anomalies approaches zero at a spherical distance of about 30° to 40° .

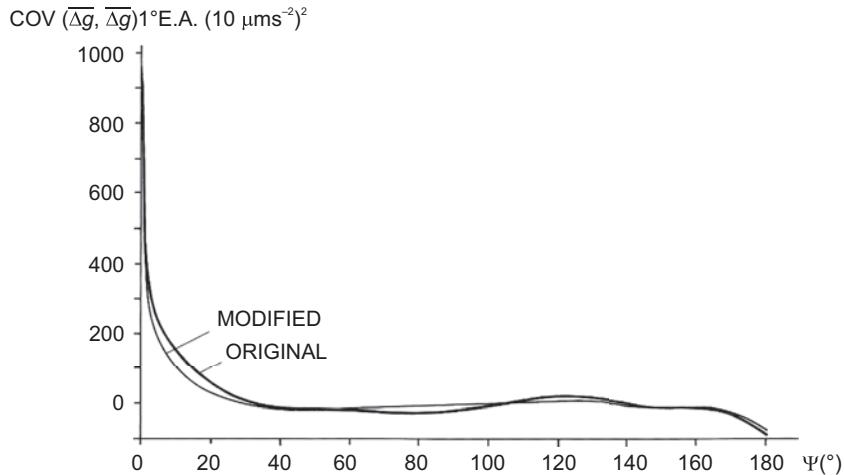


Fig. 6.5: Global covariance function of gravity anomalies, model Tscherning and Rapp (1974).

The anomaly degree variance model reads

$$\sigma_l^2(\Delta g) = \begin{cases} 0 & \text{for } l=0,1 \\ 754(\mu\text{ms}^{-2})^2 & \text{for } l=2 \\ \frac{A(l-1)}{(l-2)(l+B)}\sigma_0^{l+2} & \text{for } l \geq 3 \end{cases}, \quad (6.27)$$

with $A = 42\,528$ and $B = 24$. $\sigma_0 = (R_B/R)^2 = 0.999\,617$ is the ratio between the radius of the Bjerhammar sphere (internal boundary surface for the harmonic development, cf. [3.3.2]), and the Earth's radius, Fig. 6.6 shows the anomaly degree variances of the Tscherning-Rapp (1974) model and the more recent geopotential models EGM96 and EGM2008, cf. [6.6.2], where the latter one has been developed until degree and order 2159, see Arabelos and Tscherning (2010).

More details on the spherical harmonic development of *different* gravity field quantities and their relation with degree variances and covariance functions will be given in [6.6.1] and [6.8.2].

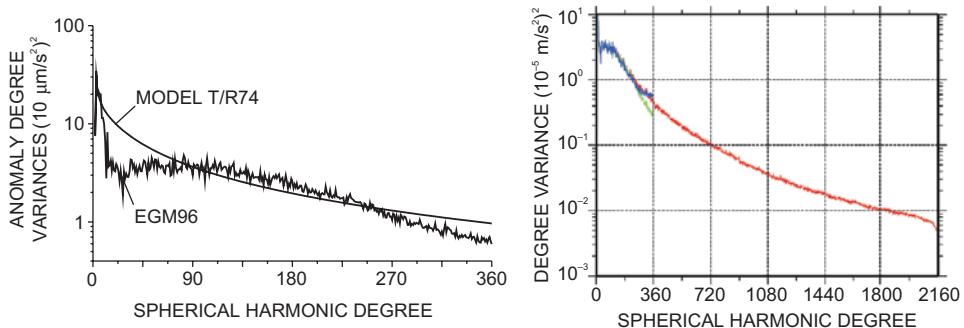


Fig. 6.6: Anomaly degree variances, left: model Tscherning and Rapp (1974) and geopotential model EGM96 (after Lemoine et al., 1998); right: EGM96 (green), EIGEN-GL04C (blue) and EGM2008 (red) (after Arabelos and Tscherning, 2010).

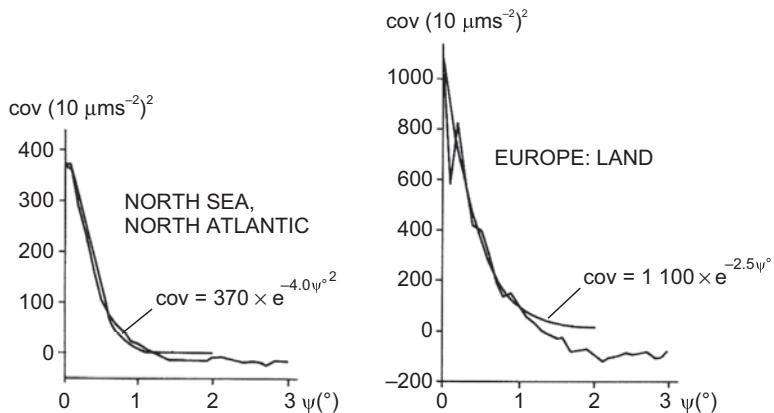


Fig. 6.7: Local covariance functions of trend-removed $6' \times 10'$ mean free air anomalies (Torge et al., 1984).

For *regional* applications, a covariance function may be derived by subtracting the long-wave part from the global function, which results in a decrease in the variance and a shortening of the correlation length. *Local* gravity field interpolation is even possible by a plane covariance function, e.g., the Gauss function

$$C(\psi) = C_0 e^{-A^2 \psi^2}, \quad (6.28)$$

see Fig. 6.7.

It should be noted that covariance functions have to be positive definite. This condition is fulfilled for (6.24), as all coefficients according to (6.26) are non-negative, as well as for (6.28).

An important application of the anomaly covariance function is the *interpolation* of gravity anomalies at points or areas not surveyed. Simple interpolation methods such as the manual construction of iso-anomaly maps or the geometric interpolation using adjacent data are not ideal and do not deliver optimum results. *Least-squares prediction*, on the other hand, utilizes the statistical information inherent in the covariance function and takes the errors of the observations into account.

In the usual *linear* prediction, the (unknown) gravity anomaly at the point P is estimated by a linear function of the anomalies observed at the points P_i ($i = 1, \dots, n$). We assume that, in addition to the covariance function of the anomalies, an *error covariance function* is also available, describing the statistical behavior of the data errors. It can be derived from a priori error and error correlation estimates, where the demands on homogeneity and isotropy have to be fulfilled again. Generally the *error covariances* are unknown, and the error model has to be restricted onto the *error variances*. Among the rare examples of error covariance functions are the analytical approximations, based on overlapping data of different sea gravimetry surveys carried out around Europe (Weber and Wenzel, 1983).

Based on the statistical information on the gravity anomalies and their errors, the following covariances, for any distance ψ , can be calculated:

$$C_{P_i} = M[\Delta g_p, \Delta g_i]: \text{cross-covariance of } \Delta g_p \text{ with the observation } \Delta g_i$$

$C_{ij} = M\{\Delta g_i \Delta g_j\}$: auto-covariance of the observations,
 $D_{ij} = M\{n_i n_j\}$: auto-covariance of the observational errors (noise n), and combined into

$$\mathbf{C}_p^T = (C_{p_1}, \dots, C_{p_l}, \dots, C_{p_n})$$

$$\mathbf{C} = \begin{pmatrix} C_{11} & \cdots & \cdots & \cdots & C_{1n} \\ \vdots & \ddots & & & \vdots \\ \vdots & & C_{ij} & & \vdots \\ \vdots & & & \ddots & \vdots \\ C_{n1} & \cdots & \cdots & \cdots & C_{nn} \end{pmatrix}, \quad \mathbf{D} = \begin{pmatrix} D_{11} & \cdots & \cdots & \cdots & D_{1n} \\ \vdots & \ddots & & & \vdots \\ \vdots & & D_{ij} & & \vdots \\ \vdots & & & \ddots & \vdots \\ D_{n1} & \cdots & \cdots & \cdots & D_{nn} \end{pmatrix}. \quad (6.29)$$

Now, the prediction error is introduced, being the difference between the true gravity anomaly and the predicted value $\Delta \hat{g}$. The requirement of a minimum prediction error variance, in analogy to least-squares adjustment, leads to the predicted anomaly, as the result of least-squares prediction

$$\Delta \hat{g}_p = \mathbf{C}_p^T \bar{\mathbf{C}}^{-1} \Delta \mathbf{g}, \quad (6.30)$$

where the observed anomalies have been collected in the vector

$$\Delta \mathbf{g}^T = (\Delta g_1, \dots, \Delta g_l, \dots, \Delta g_n). \quad (6.31)$$

Under the (plausible) assumption that the gravity anomalies and their errors are not correlated, the corresponding matrices \mathbf{C} and \mathbf{D} can be added element by element, leading to the combined matrix $\bar{\mathbf{C}}$ appearing in (6.30):

$$\bar{\mathbf{C}} = \mathbf{C} + \mathbf{D}. \quad (6.32)$$

The prediction of *point* free-air anomalies (based on a point anomaly covariance function) is successful only for very densely surveyed areas, as these anomalies strongly depend on height. A smoother gravity anomaly field with improved possibility of interpolation is obtained by calculating *mean* anomalies over larger surface elements (e.g., $5' \times 5'$, $30' \times 30'$). An effective smoothing is obtained by reducing the effect of the topographic masses, and eventually also geological mass anomalies, where Bouguer and isostatic anomalies are especially well suited for interpolation, cf. [6.5.3]. As well known from least-squares adjustment theory, the predicted values of the gravity anomalies are relatively independent from the choice of the covariance function, while the error estimates strongly depend on it. Realistic prediction results can be expected only within the correlation length defined by a covariance of $\frac{1}{2}\sigma^2(\Delta g)$.

6.2 Three-dimensional positioning

Three-dimensional positioning is generally carried out in a *Cartesian* coordinate system; the use of *ellipsoidal* coordinates results in more complicated models [6.2.1]. The Geodetic Datum provides the orientation of the three-dimensional model with respect to the global geocentric system [6.2.2]. Three-dimensional modeling has been early proposed by Bruns (1878), and taken up, expanded and carefully investigated since the

1950s by Hotine (1969), Wolf (1963a, b), Grafarend (1978a), also Hofmann-Wellenhof and Moritz (2005, p. 208 ff.).

6.2.1 Observation equations

As usual, the *observation equations* relate the observed quantities to the unknown station coordinates and other parameters (functional model). By “observations” we mean geometric quantities that result from preprocessing of the original measurements, such as signal travel time, phase and frequency, and readings on graduated circles or staffs, see the corresponding sections on geodetic measurement methods in [5]. We also assume that instrumental corrections have been applied (e.g., calibration) and that effects from the atmosphere (refraction) and the gravity field (Earth tides) have been taken into account. The observation equations are mostly non-linear. They have to be linearized for the subsequent least-squares adjustment, which also includes the treatment of the errors of the observations (stochastic model), see references given at the beginning of this chapter.

The “observations” used for three-dimensional positioning may be divided into space and terrestrial measurements.

Space observations include satellite related

- space directions, cf. [5.2.4],
- ranges derived from GNSS (GPS and other satellite systems) and laser distance measurements, cf. [5.2.5], [5.2.6],
- range rates from Doppler measurements, cf. [5.2.4].

We add

- baseline vectors obtained from VLBI, cf. [5.3.4].

Global and regional satellite and VLBI networks are nowadays adjusted separately, and independent from terrestrial geodetic data. The results (Cartesian coordinates or coordinate differences) can be introduced later as “observed” parameters into combined adjustments, together with other satellite networks or with terrestrial measurements. Naturally, the correlations produced by the previous adjustments (variance-covariance matrix) have to be taken into account in that case, cf. [2.5], [7.3].

Satellite observations provide the components of the *observation vector* \mathbf{s} directed from the station P to the satellite S (Fig. 6.8). The vector \mathbf{s} is related to the geocentric station vector \mathbf{r}_P and the radius vector \mathbf{r}_S of the satellite by

$$\mathbf{r}_P + \mathbf{s} - \mathbf{r}_S = \mathbf{0}, \quad (6.33a)$$

with

$$\mathbf{r}_P = \begin{pmatrix} X_P \\ Y_P \\ Z_P \end{pmatrix}, \quad \mathbf{r}_S = \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}, \quad \mathbf{r}_S - \mathbf{r}_P = \begin{pmatrix} \Delta X_P^S \\ \Delta Y_P^S \\ \Delta Z_P^S \end{pmatrix}. \quad (6.33b)$$

The “observation” vector is formed by the distance and the spatial direction (as obtained by optical direction measurements) to the satellite given in the hour angle system

$$\mathbf{s} = s \begin{pmatrix} \cos h_{Gr} \cos \delta \\ \sin h_{Gr} \cos \delta \\ \sin \delta \end{pmatrix}, \quad (6.34)$$

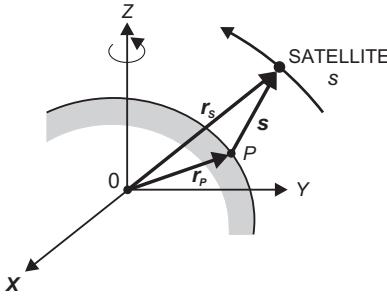


Fig. 6.8: Satellite tracking principle.

where δ is the declination and

$$h_{Gr} = \text{GAST} - \alpha \quad (6.35)$$

is the Greenwich hour angle, cf. [2.4.1]. For the reductions to be applied to the original topocentric observations in order to obtain declination and Greenwich hour angle see [5.3.3].

Inserting (6.34) into (6.33) and solving for the components of s yields the observation equations

$$\left. \begin{aligned} h_{Gr} &= \arctan \frac{\Delta Y_p^s}{\Delta X_p^s} \\ \delta &= \arctan \frac{\Delta Z_p^s}{\sqrt{\Delta X_p^s + \Delta Y_p^s}} \\ s &= \sqrt{\Delta X_p^s + \Delta Y_p^s + \Delta Z_p^s} \end{aligned} \right\}. \quad (6.36)$$

Range differences to the satellite positions (i, j) are given by

$$s_j - s_i = \sqrt{\Delta X_p^j + \Delta Y_p^j + \Delta Z_p^j} - \sqrt{\Delta X_p^i + \Delta Y_p^i + \Delta Z_p^i}, \quad (6.37a)$$

with

$$\Delta X_p^j = X_j - X_p \text{ etc., } \Delta X_p^i = X_i - X_p \text{ etc.} \quad (6.37b)$$

If the directions to the quasars are known, VLBI observations deliver the *baseline vector* between two terrestrial stations P_1 and P_2 :

$$\mathbf{b}_{1,2} = \mathbf{r}_2 - \mathbf{r}_1 = \begin{pmatrix} X_2 - X_1 \\ Y_2 - Y_1 \\ Z_2 - Z_1 \end{pmatrix}. \quad (6.38)$$

The relations of the original measurements to the “observations” introduced as geometrical quantities in (6.36) to (6.38) are given by (5.42) for Doppler counts, (5.43) and (5.45) for GNSS, (5.48) for satellite laser ranging, and (5.68) for VLBI.

The observation equations contain a large number of parameters in addition to the station coordinates, and the coordinates of the satellites (orbital parameters) and the quasars, respectively. Among them are the Earth orientation parameters, which relate the terrestrial to the celestial

reference frame, cf. [2.4.1], parameters describing temporal variations of the ground stations (e.g., Earth tides and crustal deformation effects), as well as the coefficients of the gravitational field and other “disturbing” forces entering through satellite orbit modeling. There are two strategies to handle the large amount of data and unknown parameters. The first one consists in estimating most of the unknowns in *one* adjustment process and to adopt only a few parameters (e.g., the Earth orientation parameters) from other sources. This leads to “satellite-only” Earth models, which provide a global set of station coordinates, the harmonic coefficients of the gravitational field, and other parameters. If only *positioning* is intended, the station coordinates are the most important adjustment unknowns. Numerical values for the other parameters are then taken from corresponding models (e.g. the high precision orbital parameters as provided by operational services for GNSS and laser satellites, geopotential models, tropospheric refraction models, and others, cf. [5.2], [5.3]). If necessary, small corrections to the model values can also be derived (corrections to the Keplerian elements for short arcs, introduction of a local tropospheric scale factor, clock corrections, etc.)

As already discussed for GNSS observations, cf. [5.2.5], we may distinguish between absolute and relative positioning when evaluating the observation equations. *Absolute positioning* utilizes the satellite’s orbit (coordinates of the satellite as a function of time) and delivers geocentric station coordinates, with an accuracy directly depending on the quality of the orbital data. *Relative positioning* is based on simultaneous observations on two or more stations. It leads to purely geometric solutions which contain datum deficiencies of a different kind. At least one station has to be known in order to fix the origin of the network. A pure triangulation network requires a minimum of one measured distance for defining the scale, and a trilateration net would need orientation through the spatial direction to stars or quasars.

By *differencing* simultaneous observations a number of errors are eliminated or greatly reduced which is due to the high error correlation between neighboring stations. This strategy has been developed especially for the parameter estimation in GPS/GNSS networks by introducing differences or linear combinations of the observables (code and carrier phases) into the adjustment (Teunissen and Kleusberg, 1998b). Since the absolute orientation is lost with this strategy, the absolute coordinates of at least one station have to be included into the adjustment model.

As a standard, “*single differences*” $s_1^A - s_2^A$ between the distances measured simultaneously from two receivers P_1, P_2 to the satellite A at epoch t_i are formed (Fig. 6.9). Thereby, the satellite clock errors are eliminated and refraction and orbital errors are reduced. “*Double differences*” are formed by differencing two single differences taken to different satellites A, B at the same epoch t_i : $(s_1^A - s_2^A) - (s_1^B - s_2^B)$. With double

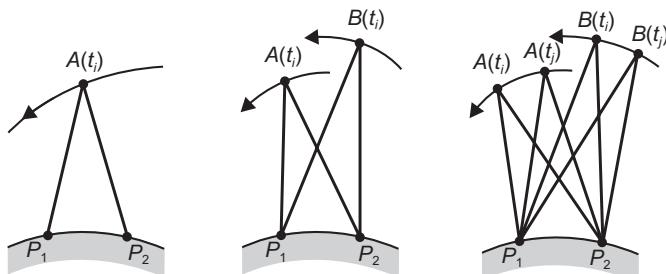


Fig. 6.9: GPS single, double and triple differences.

difference, the receiver clock errors vanish and refraction and orbital errors are further reduced. “*Triple differences*” are constructed by differencing two double differences taken at the epochs t_i and t_j . The ambiguity which enters into carrier phase measurements cancels in the observation equation. Due to the loss of information, triple differences allow reduced-accuracy positioning only but are useful for the detection and correction of cycle slips.

Sophisticated software packages are available for the *adjustment* of satellite networks; for GNSS networks we mention Wübbena (1989), Webb and Zumberge (1997), King and Bock 2005 and Dach et al. (2007). The adjustment delivers the Cartesian coordinates or coordinate differences of the ground stations and their full variance-covariance matrix, which has to be taken into account for further processing, e.g., for the combination with other space techniques and/or terrestrial data. If the orientation of the networks to be combined is not identical, a corresponding transformation (datum shift) has to be included in the adjustment, cf. [6.2.2].

Terrestrial measurements include (traditionally, astronomic observations to fixed stars are included here)

- Astronomic azimuths, latitudes, and longitudes, cf. [5.3.2],
- Horizontal directions (which can be regarded as azimuths without orientation) and horizontal angles (corresponding to differences of azimuths), cf. [5.5.1],
- Zenith angles, cf. [5.5.1],
- Distances, cf. [5.5.2],
- Leveled height differences, cf. [5.5.3].

Terrestrial measurements have been classically evaluated separately for horizontal position and for height, cf. [6.3], [6.4]. The resulting control networks are nowadays transformed to the global reference frame, provided by space methods. This is done by connection to the global network and (at least partial) remeasurement, with subsequent transformation. A joint evaluation of space and terrestrial observations is now restricted to local applications, with dimensions generally not exceeding a few kilometers. More details on the establishment and renewal of regional/local geodetic networks are given in [7.1] to [7.3].

By substituting (2.20) into (2.29) and taking (2.30) into account, we obtain the *observation equations* for *azimuths A*, *zenith angles z*, and *distances s*:

$$\left. \begin{aligned} A &= \arctan \frac{-\sin \Lambda \Delta X + \cos \Lambda \Delta Y}{-\sin \Phi \cos \Lambda \Delta X - \sin \Phi \sin \Lambda \Delta Y + \cos \Phi \Delta Z} \\ z &= \arccos \frac{\cos \Phi \cos \Lambda \Delta X + \cos \Phi \sin \Lambda \Delta Y + \sin \Phi \Delta Z}{(\Delta X^2 + \Delta Y^2 + \Delta Z^2)^{\frac{1}{2}}} \\ s &= (\Delta X^2 + \Delta Y^2 + \Delta Z^2)^{\frac{1}{2}} \end{aligned} \right\}, \quad (6.39)$$

with

$$\Delta X = X_2 - X_1, \quad \Delta Y = Y_2 - Y_1, \quad \Delta Z = Z_2 - Z_1.$$

Astronomic latitude Φ and astronomic longitude Λ enter as orientation parameters in (6.39). They relate the local astronomic systems to the global geocentric system and are treated here as additional unknown parameters. If *observed* latitudes and longitudes are available, they may be introduced as observed parameters in the adjustment.

As mentioned previously, least-squares adjustment requires linear relations between the observations and the unknowns. Corresponding *differential relations* are derived by numerical or analytical differentiation of (6.39). Analytical expressions for the partial derivatives $\partial A / \partial X$, etc. are found in Wolf (1963b) and Hofmann-Wellenhof and Moritz (2005, p. 211 ff.).

Geometric leveling can be incorporated into three-dimensional computations after transformation of the leveled height difference $\delta n \approx dn$ (5.114) into the geocentric coordinate system. This is achieved by introducing the ellipsoidal height difference dh , as obtained by reducing dn for the effect of the (surface) deflection of the vertical (Fig. 6.10). In the azimuth of the leveling line, the vertical deflection component ε (6.18) is effective, which gives

$$dh = dn - \varepsilon ds. \quad (6.40)$$

The negative sign prefixing εds is based on the sign definitions inherent in (6.17) and (6.7) resp. (6.8). A differential relationship between the ellipsoidal height and X, Y, Z is provided by (4.26a) and (4.27). With

$$d\bar{\mathbf{r}}_Q = \mathbf{0},$$

and replacing φ, λ with Φ, Λ , we obtain

$$dh = \bar{\mathbf{n}}^T \cdot d\mathbf{r} = \cos\Phi \cos\Lambda \, dX + \cos\Phi \sin\Lambda \, dY + \sin\Phi \, dZ. \quad (6.41)$$

Again, we have assumed that the axes of the ellipsoidal and the geocentric system are parallel:

$$d\bar{X} = dX, \quad d\bar{Y} = dY, \quad d\bar{Z} = dZ.$$

Integration of (6.40) yields the ellipsoidal height difference

$$\Delta h_{1,2} = h_2 - h_1 = \int_1^2 dn - \int_1^2 \varepsilon ds, \quad (6.42)$$

which can be included as an “observation” in three-dimensional computations: Geometric-astronomic leveling (Heitz, 1973). It is noted that both integrals in (6.42) have to be formed over the same path! The differential relation for (6.42) follows from differencing (6.41) for the points P_1 and P_2 :

$$d(\Delta h_{1,2}) = dh_2 - dh_1. \quad (6.43)$$

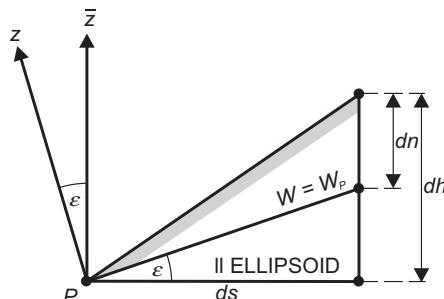


Fig. 6.10: Geometric-astronomic leveling.

The first integral in (6.42) can easily be computed by summing the leveled height differences. The evaluation of the second integral poses difficulties, as vertical deflections (derived from geodetic astronomy) are generally only available at larger station distances (several 10 km in classical networks). This introduces the problem of the interpolation of deflections of the vertical. In flat and hilly areas, with an average distance of the vertical deflection stations of 20 to 30 km, an accuracy of about 0.1 m/100 km can be achieved for the ellipsoidal height differences. If “cm”-accuracy is required, station distances of a few km and sophisticated interpolation methods are required (Torge, 1977; Hirt and Flury, 2008). By reducing the station distance to about 1 km and taking into account topography, even “mm”-accuracy can be achieved over distances of a few km, cf. [6.7.4].

The three-dimensional concept based on *terrestrial* observations was already introduced by Villarceau (1868) and Bruns (1878). Bruns suggested a point-wise determination of the Earth’s surface by a spatial polyhedron constructed from terrestrial measurements and orientated by astronomical observations. The feasibility of this concept was demonstrated in some test networks (e.g., Torge and Wenzel, 1978), but large-scale application was prevented due to the uncertainties of trigonometrical height transfer over larger distances and the problems with reducing geometric leveling to ellipsoidal height differences.

Ellipsoidal coordinates φ , λ , and sometimes also h are used for numerous applications in geodesy, geomatics and cartography, and navigation. They can easily be derived from the *Cartesian* coordinates by the transformation (4.28). However, network adjustments in the φ , λ , h -system are more complicated than in the X , Y , Z -system, and therefore restricted to special cases. Nevertheless, differential relations between the observations and the ellipsoidal coordinates are useful for solving dedicated problems, e.g., for deriving reductions onto the ellipsoid and for two-dimensional ellipsoidal calculations, cf. [6.3.2], [6.3.3].

Equations (4.27) provide the fundamental relations between the φ , λ , h - and the \bar{X} , \bar{Y} , \bar{Z} -systems. Differentiation yields

$$\begin{pmatrix} d\bar{X} \\ d\bar{Y} \\ d\bar{Z} \end{pmatrix} = \bar{\mathbf{A}} \begin{pmatrix} (M+h)d\varphi \\ (N+h)\cos\varphi d\lambda \\ dh \end{pmatrix} \quad (6.44)$$

where $\bar{\mathbf{A}}$ is given by (4.32). Again we assume parallelism of the ellipsoidal and the Cartesian coordinate systems. Equation (6.44) can immediately be used if satellite derived coordinates or coordinate differences are to be adjusted in the φ , λ , h -system. Differential formulas for the terrestrial observations A , z , s are obtained by inserting (6.44) into the differential relations for Cartesian coordinates and reordering (Wolf, 1963b; Heiskanen and Moritz, 1967, p. 220 ff.), cf. [6.3.2].

We finally mention the straightforward transformation from the “natural” coordinates Φ , Λ , and H (orthometric height) or H^N (normal height) to ellipsoidal coordinates φ , λ , h , where H and H^N are derived from the gravity potential W by (3.106) and (3.107), respectively. According to (6.17), the deflection of the vertical (ξ, η) transforms from the plumb line direction to the ellipsoidal normal:

$$\varphi = \Phi - \xi, \quad \lambda = \Lambda - \frac{\eta}{\cos\varphi}. \quad (6.45a)$$

If *normal* geodetic coordinates φ^N, λ^N (4.73) are required, the curvature of the normal plumb line has to be taken into account by $\delta\varphi^N$ (4.74):

$$\varphi^N = \Phi - (\xi + \delta\varphi^N) = \Phi - \xi^N, \quad \lambda^N = \lambda = \Lambda - \frac{\eta}{\cos\varphi}. \quad (6.45b)$$

The relation between h and H respectively H^N is given by, see Fig. 6.2:

$$h = H + N = H^N + \zeta, \quad (6.46)$$

where we have neglected the small (sub-mm order of magnitude) effect of the plumb line curvature.

As shown in [6.7], gravimetric evaluation techniques allow the calculation of the deflection of the vertical and the geoid height or the height anomaly from gravity field data. Equations (6.45) and (6.46) thus would permit to establish a geocentric system of ellipsoidal coordinates. This led to the idea of establishing a world geodetic system from "natural" coordinates and gravimetric corrections, which was pursued since the 1950s, exploiting the (at that time) sparse gravity data available especially on the northern hemisphere (Heiskanen 1951). This strategy had to be abandoned with the success of satellite geodesy, taking also into account the fact that astronomical latitude and longitude generally can be determined only with an accuracy of 0.1" (corresponding to 3 m in horizontal position) or less. The height transformation (6.46), on the other hand, has obtained high relevance, as it permits the connection of GNSS-derived ellipsoidal heights with heights determined by geometric leveling, cf. [6.4.3].

6.2.2 Geodetic datum

The *geodetic datum* describes the orientation of any geodetic coordinate system with respect to the Earth's body, cf. [2.3.3]. It can be expressed by a parameter set of three translations, three rotations and a scale factor (Drewes, 2009c). Generally, ellipsoidal coordinates are used at geodetic reference systems, in addition to or instead of spatial Cartesian coordinates. This requires the inclusion of two geometric ellipsoid parameters (semi-major axis and flattening) into the datum parameter set.

We distinguish between reference networks based on space methods (satellites, VLBI) and classical geodetic networks, established by terrestrial measurements and geodetic astronomy. The former networks are directly related to the geocenter and the Earth's spin axis, and thus are very close to a geocentric reference system as the ITRS, cf. [2.4.2]. Classical networks, on the other hand, could be orientated only by astronomical observations (position) and connection to mean sea level (height). This resulted in large deviations of the network's origin from the geocenter, while the axes could be made approximately parallel to the geocentric system. Another consequence was the separate treatment of horizontal and vertical control networks, with corresponding horizontal and vertical datum, see below and [6.3.3], [7.1], [7.2].

We start with the most general case, the transformation of a non-geocentric $\bar{X}, \bar{Y}, \bar{Z}$ -system into the geocentric X, Y, Z -system. This strategy can be directly applied to satellite-based networks, and after corresponding transformation, see [4.1.3] and below, also to classical ellipsoidal systems. The relation between the two systems is given by a *similarity transformation* in space, i.e., by three translations, three rotations, and a change in scale (Fig. 6.11):

$$\mathbf{r} = \mathbf{r}_0 + (1 + m)\mathbf{R}(\mathcal{E}_{\bar{X}'}, \mathcal{E}_{\bar{Y}'}, \mathcal{E}_{\bar{Z}'})\bar{\mathbf{r}}. \quad (6.47)$$

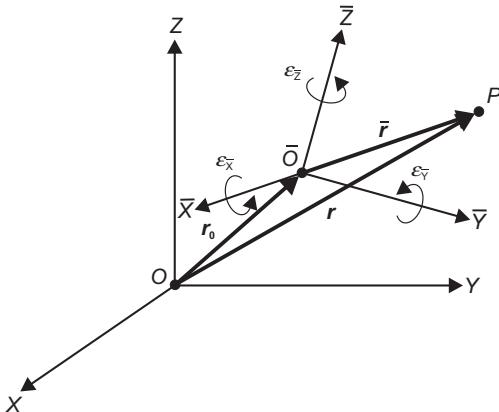


Fig. 6.11: Transformation between 3D-Cartesian coordinate systems.

Here, $\mathbf{r}^T = (X, Y, Z)$ and $\bar{\mathbf{r}}^T = (\bar{X}, \bar{Y}, \bar{Z})$ are the position vectors in the two systems, and $\mathbf{r}_0^T = (X_0, Y_0, Z_0)$ contains the coordinates of the origin \bar{O} of the $\bar{X}, \bar{Y}, \bar{Z}$ -system with respect to the geocenter O . We assume that the scale of the $\bar{X}, \bar{Y}, \bar{Z}$ -system differs only slightly from the scale of the global reference system, and that the axes of the two systems are approximately parallel. Consequently, m is a small scale correction, and the rotation matrix is composed of three *small* Eulerian angles; it takes the form

$$\mathbf{R}(\varepsilon_{\bar{X}}, \varepsilon_{\bar{Y}}, \varepsilon_{\bar{Z}}) = \begin{pmatrix} 1 & \varepsilon_{\bar{Z}} & -\varepsilon_{\bar{Y}} \\ -\varepsilon_{\bar{Z}} & 1 & \varepsilon_{\bar{X}} \\ \varepsilon_{\bar{Y}} & -\varepsilon_{\bar{X}} & 1 \end{pmatrix}. \quad (6.48)$$

In order to determine the seven parameters of the transformation (6.47), at least three points with seven coordinates given in both systems are required.

The parameters of a geodetic datum are provided indirectly by measurements carried out at control points located on the surface of the Earth. These data contain a multitude of *time-variable* effects, stemming from the gravity field and tides, from atmosphere, hydrosphere and cryosphere, as well as from crustal motion and deformation. With present-day accuracies, a large part of these effects significantly affects the results of geodetic networks, i.e. the coordinates of the reference frame's control points, where temporal variations should be corrected by appropriate models. In this connection, a clear distinction should be made between the reference frame with stations moving with time and the geodetic datum, which should be fixed over a longer time span (Drewes, 2009c). Here, the first and second degree spherical harmonic coefficients of the gravitational field play a special role, as they independently control shifts of the Earth's center of mass and the (time-variable) axis of rotation, cf. [3.3.4].

After converting the Cartesian coordinates into ellipsoidal ones (6.47) can be expressed in *ellipsoidal coordinates* φ, λ, h . The datum parameters in that case also have to include the geometric parameters of the ellipsoid, i.e., the semi-major axis a and the flattening f . Of practical interest are the *changes* of the ellipsoidal coordinates that result from a datum transformation, i.e., from translation, rotation, change in scale, and change of the parameters of the ellipsoid. We insert (4.27) into (6.47) and take the total differential. As the real position of P does not change, we have $d\mathbf{r} = \mathbf{0}$. Neglecting the linear scale factor (which can be easily introduced again at all metric quantities) and substituting the

differentials by (small) differences, a spherical approximation ($M + h = N + h = a$, $f = 0$) yields (Merry and Vaniček, 1974):

$$\begin{pmatrix} a \delta\varphi \\ a \cos\varphi \delta\lambda \\ \delta h \end{pmatrix} = -\bar{\mathbf{A}}^{-1} \delta \mathbf{r}_0 + \mathbf{C} \begin{pmatrix} \delta \varepsilon_{\bar{x}} \\ \delta \varepsilon_{\bar{y}} \\ \delta \varepsilon_{\bar{z}} \end{pmatrix} + \mathbf{F} \begin{pmatrix} \delta a \\ a \delta f \end{pmatrix}, \quad (6.49a)$$

where \mathbf{A}^{-1} is given by (4.34) and

$$\mathbf{C} = a \begin{pmatrix} \sin\lambda & -\cos\lambda & 0 \\ -\sin\varphi \cos\lambda & -\sin\varphi \sin\lambda & \cos\varphi \\ 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} 0 & \sin 2\varphi \\ 0 & 0 \\ -1 & \sin^2 \varphi \end{pmatrix}. \quad (6.49b)$$

Equations (6.49) can be used for estimating the changes of the coordinates if the changes of the parameters of the geodetic datum are known. All differences are formed in the sense geocentric minus non-geocentric, e.g., $\delta a = a(\text{geocentric}) - a(\text{non-geocentric})$. Formulas which take the flattening into account are given by Abd-Elmotaal and El-Tokhey (1995).

Classical geodetic networks, cf. [7.1], have been orientated by the ellipsoidal coordinates of an *initial* (or *fundamental*) point P_F and by condition equations for the parallelism of the axes with respect to the geocentric system: “*local geodetic datum*”, the distance to the geocenter remained unknown. If we apply (6.49) at a running point P and at the fundamental point P_F , the translation can be expressed in changes $\delta\varphi_F, \delta\lambda_F, \delta h_F$ of the fundamental point. An equivalent relation can be derived by substituting the ellipsoidal coordinates through the (small) residual quantities deflection of the vertical and geoid height, cf. [6.2.1]. By differentiating (6.45) and (6.46), and considering that because of $d\mathbf{r} = \mathbf{0}$ also $d\Phi = d\Lambda = dH = 0$, we obtain

$$\delta\xi = -\delta\varphi, \quad \delta\eta = -\cos\varphi \delta\lambda, \quad dN = dh. \quad (6.50)$$

Corresponding equations hold for the “normal” geodetic coordinates, cf. [4.2.3]. Hence, the coordinate changes at any point also can be expressed as *changes of the deflection of the vertical* and the *geoid height* (or height anomaly), depending on the corresponding changes in the fundamental point (Vening-Meinesz, 1950). Spherical approximation yields (Heiskanen and Moritz, 1967, p. 208)

$$\begin{aligned} d\xi &= (\cos\varphi_F \cos\varphi + \sin\varphi_F \sin\varphi \cos(\lambda - \lambda_F)) d\xi_F \\ &\quad - \sin\varphi \sin(\lambda - \lambda_F) d\eta_F \\ &\quad - (\sin\varphi_F \cos\varphi - \cos\varphi_F \sin\varphi \cos(\lambda - \lambda_F)) \\ &\quad \times \left(\frac{dN_F}{a} + \frac{da}{a} + \sin^2\varphi_F df \right) - 2\cos\varphi (\sin\varphi - \sin\varphi_F) df, \end{aligned} \quad (6.51a)$$

$$\begin{aligned} d\eta &= \sin\varphi_F \sin(\lambda - \lambda_F) d\xi_F + \cos(\lambda - \lambda_F) d\eta_F \\ &\quad + \cos\varphi_F \sin(\lambda - \lambda_F) \left(\frac{dN_F}{a} + \frac{da}{a} + \sin^2\varphi_F df \right), \end{aligned} \quad (6.51b)$$

$$\begin{aligned} dN &= -a (\cos\varphi_F \sin\varphi - \sin\varphi_F \cos\varphi \cos(\lambda - \lambda_F)) d\xi_F \\ &\quad - a \cos\varphi \sin(\lambda - \lambda_F) d\eta_F \\ &\quad + (\sin\varphi_F \sin\varphi + \cos\varphi_F \cos\varphi \cos(\lambda - \lambda_F)) \\ &\quad \times (dN_F + da + a \sin^2\varphi_F df) - da \\ &\quad + (\sin^2\varphi - 2\sin\varphi_F \sin\varphi) a df. \end{aligned} \quad (6.51c)$$

These relations have played a role in the optimum fitting of horizontal control networks to the geoid, cf. [7.1].

We now investigate how the (approximate) *parallelism of the axes* of classical geodetic networks with respect to the geocentric system has been achieved.

We describe the deviation between the local astronomic x, y, z -system (2.20) and the local ellipsoidal $\bar{x}, \bar{y}, \bar{z}$ -system (4.29) by three (small) Eulerian angles, after reflection of the y and \bar{y} -axes (generating right-handed systems), Fig. 6.12:

$$\mathbf{x} = \mathbf{R}(\xi, \eta, \psi) \bar{\mathbf{x}}, \quad (6.52a)$$

with the rotation matrix

$$\mathbf{R}(\xi, \eta, \psi) = \begin{pmatrix} 1 & \psi & -\xi \\ -\psi & 1 & \eta \\ \xi & -\eta & 1 \end{pmatrix}. \quad (6.52b)$$

The Eulerian angles are the components of the *deflection of the vertical*, cf. [6.1.2], in the meridian (ξ), in the prime vertical (η), and in the horizontal plane (ψ). If the axes of the global X, Y, Z - and $\bar{X}, \bar{Y}, \bar{Z}$ -systems are not parallel, the following relations hold, according to (2.26), (4.29), (6.47), and (6.52):

$$\Delta \mathbf{X} = \mathbf{A} \mathbf{x} = \mathbf{A} \mathbf{R}(\xi, \eta, \psi) \bar{\mathbf{x}} = \mathbf{R}(\varepsilon_{\bar{X}}, \varepsilon_{\bar{Y}}, \varepsilon_{\bar{Z}}) \bar{\mathbf{A}} \bar{\mathbf{x}} \quad (6.53)$$

or

$$\mathbf{R}(\varepsilon_{\bar{X}}, \varepsilon_{\bar{Y}}, \varepsilon_{\bar{Z}}) \bar{\mathbf{A}} = \mathbf{A} \mathbf{R}(\xi, \eta, \psi). \quad (6.54)$$

After inserting $\bar{\mathbf{A}}$ (4.32) and \mathbf{A} (2.28), the evaluation of (6.54) results in nine equations. Three of the nine equations are independent from each other (orthogonality relations). After Taylor expansion of the trigonometrical functions of Φ, Λ inherent in (2.28) at the point (φ, λ) , we obtain the components (linear approximation) of the *deflection of the vertical* if the axes of the global systems are *not parallel*:

$$\left. \begin{aligned} \xi &= \Phi - \varphi + \sin \lambda \varepsilon_{\bar{X}} - \cos \lambda \varepsilon_{\bar{Y}} \\ \eta &= (\Lambda - \lambda) \cos \varphi - \sin \varphi (\cos \lambda \varepsilon_{\bar{X}} + \sin \lambda \varepsilon_{\bar{Y}}) + \cos \varphi \varepsilon_{\bar{Z}} \\ \psi &= (\Lambda - \lambda) \sin \varphi + \cos \varphi (\cos \lambda \varepsilon_{\bar{X}} + \sin \lambda \varepsilon_{\bar{Y}}) + \sin \varphi \varepsilon_{\bar{Z}} \end{aligned} \right\}. \quad (6.55)$$

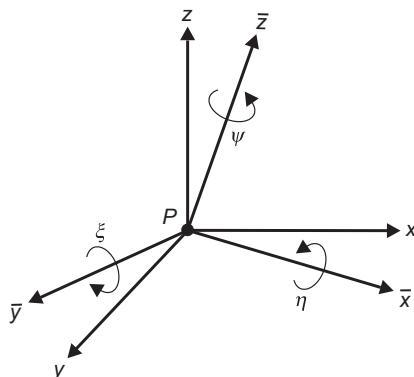


Fig. 6.12: Rotations between the local ellipsoidal and the local astronomic system.

We also generalize the equations for the *azimuth* and the *zenith angle* given in the local astronomic and the local ellipsoidal system. From (6.53) we have

$$\mathbf{Ax} = \mathbf{R}(\varepsilon_{\bar{x}}, \varepsilon_{\bar{y}}, \varepsilon_{\bar{z}}) \bar{\mathbf{A}}\bar{\mathbf{x}}.$$

Inserting (2.20) and (4.29) yields, after linearization of the trigonometrical functions of A, z at α, ζ :

$$\begin{aligned} A - \alpha &= (\Lambda - \lambda) \sin \varphi + ((\Phi - \varphi) \sin \alpha - \cos \varphi (\Lambda - \lambda) \cos \alpha) \cot \zeta \\ &\quad + \cos \varphi (\cos \lambda \varepsilon_{\bar{x}} + \sin \lambda \varepsilon_{\bar{y}}) + \sin \varphi \varepsilon_{\bar{z}}, \end{aligned} \quad (6.56a)$$

$$\begin{aligned} z - \zeta &= -((\Phi - \varphi) \cos \alpha + \cos \varphi (\Lambda - \lambda) \sin \alpha) \\ &\quad - (\cos \alpha \sin \lambda - \sin \alpha \sin \varphi \cos \lambda) \varepsilon_{\bar{x}} \\ &\quad + (\cos \alpha \cos \lambda + \sin \alpha \sin \varphi \sin \lambda) \varepsilon_{\bar{y}} \\ &\quad - \cos \varphi \sin \alpha \varepsilon_{\bar{z}}. \end{aligned} \quad (6.56b)$$

We now require parallelism of the axes, setting

$$\varepsilon_{\bar{x}} = \varepsilon_{\bar{y}} = \varepsilon_{\bar{z}} = 0.$$

(6.55) and (6.56) then transform into condition equations for the parallelism of the axes of the global and the local system. This was already presupposed when introducing the deflections of the vertical, in [6.1.2]. For the deflection of the vertical these equations obtain the form

$$\left. \begin{aligned} \xi &= \Phi - \varphi, & \eta &= (\Lambda - \lambda) \cos \varphi \\ \psi &= (\Lambda - \lambda) \sin \varphi \end{aligned} \right\}. \quad (6.57)$$

The condition equations for the azimuth and the zenith angle now read as

$$A - \alpha = \eta \tan \varphi + (\xi \sin \alpha - \eta \cos \alpha) \cot \zeta \quad (6.58)$$

and

$$z - \zeta = -(\xi \cos \alpha + \eta \sin \alpha). \quad (6.59)$$

Equation (6.58) is known as *Laplace's equation of orientation*, while (6.59) furnishes the component ε of the deflection of the vertical in the azimuth α (6.18), Vaniček and Wells (1974).

A geometric interpretation of the condition equations (6.58) and (6.59) reveals that they prevent rotations about the vertical and the horizontal axis of a theodolite. In addition, a rotation about the line of sight must be prevented in order to guarantee the parallelism of the global and the ellipsoidal system. This can be accomplished if, in addition to (6.58) and (6.59), another zenith angle equation is introduced at the fundamental point, possibly with an azimuth which differs by 90° . Due to the problems of vertical refraction, classical geodetic networks generally employed only the Laplace equation for orientation. A three-dimensional network then would need at least three *Laplace azimuths* at points well distributed over the network (Vincenty, 1985). In reality, only *horizontal* control networks were built up by reducing observed azimuths and horizontal directions onto the ellipsoid utilizing (6.58) for the reduction, cf. [6.3.2]. In order to achieve parallelism of the axes, at least one Laplace equation then had to be fulfilled at this two-dimensional positioning, cf. [7.1.2]. The reduction (6.59), on the other hand, plays an important role for trigonometric height determination, cf. [6.4.2].

6.3 Horizontal positioning

In classical geodetic networks, horizontal positioning (with an ellipsoid as reference surface) has been separated from height determination (referring to the geoid), although a three-dimensional concept for geodetic modeling was early available (Bruns, 1878), cf. [1.3.4] and [6.2]. This is due to the fact that *ellipsoidal* height differences to be derived from geometric leveling or zenith angles were affected by large uncertainties, which entered through the necessary reductions of gravity field related effects (geoid heights and deflections of the vertical, respectively) and of vertical refraction. The separate treatment of horizontal and vertical coordinates was readily accepted by the users of geodetic products, especially because gravity field related heights are generally required in practice. The possibility to directly compute ellipsoidal coordinates from GNSS-derived Cartesian coordinates, cf. [4.1.3], has strongly diminished the importance of horizontal positioning on the ellipsoid. In the following, we concentrate on some fundamentals of ellipsoidal geodesy, an extensive treatment is found in textbooks such as Grossmann (1976), Bomford (1980), and Heck (2003a).

With the ellipsoid as a reference surface, two-dimensional positioning requires ellipsoidal trigonometry [6.3.1] and reductions of the observed positional quantities onto the ellipsoid [6.3.2]. Ellipsoidal “observation” equations then allow the calculation of coordinates, after proper orientation of the ellipsoidal network with respect to the Earth’s body [6.3.3].

6.3.1 Ellipsoidal trigonometry

In order to carry out computations on the ellipsoidal surface, points on the ellipsoid are connected by surface curves. The arc of the normal section and the geodesic are primarily employed.

The *normal section* is defined by the curve of intersection of the vertical plane with the ellipsoid. Azimuths and distances, after being reduced to the ellipsoid, refer to normal sections. Since the surface normals of two points on the ellipsoid are in general skewed to each other, the reciprocal normal sections from P_1 to P_2 and from P_2 to P_1 do not coincide (Fig. 6.13). The differences in azimuth (less than $0.1''$ for $S = 100$ km) and in distance (less than 1 μm for $S = 100$ km) are small and can be taken into account easily (Bowring, 1971).

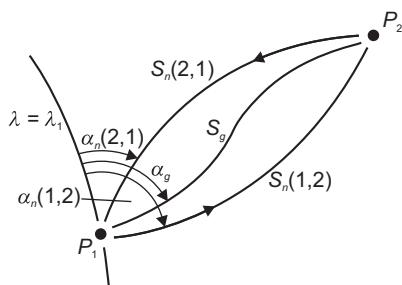


Fig. 6.13: Normal sections S_n and geodesic S_g .

Normally, because of its favorable properties, the *geodesic* is used for ellipsoidal calculations. It is uniquely defined as the shortest connection between two points and is generally bounded by the two normal sections. This definition is equal to the condition that the geodetic curvature (curvature of the normal projection of a surface curve onto the tangential plane) equals zero.

As known from differential geometry, the geodetic curvature k_g is represented by the triple scalar product

$$k_g = (\mathbf{r}' \times \mathbf{r}'') \cdot \mathbf{n}. \quad (6.60)$$

Here, $\mathbf{r}' = d\mathbf{r}/dS$ is the tangent vector and $\mathbf{r}'' = d^2\mathbf{r}/dS^2$ is the curvature vector. Also, S arc length of the geodesic, and \mathbf{n} designates the normal vector to the surface. With $k_g = 0$, we obtain a second-order vectorial *differential equation* for the *geodesic*:

$$(\mathbf{r}' \times \mathbf{r}'') \cdot \mathbf{n} = 0, \quad (6.61)$$

the local projection of the geodesic onto the tangential plane is a straight line. We now introduce the φ, λ -system of ellipsoidal coordinates (Fig. 6.14) and express the geodesic by the function $\lambda = \lambda(\varphi)$. Corresponding evaluation of (6.61) yields the *scalar* differential equations

$$\left. \begin{aligned} p^2 \frac{d^2\lambda}{d\varphi^2} + 2p \frac{dp}{d\varphi} \frac{d\lambda}{d\varphi} &= 0 \\ M \frac{dM}{d\varphi} - p \frac{dp}{d\varphi} \left(\frac{d\lambda}{d\varphi} \right)^2 &= 0 \end{aligned} \right\}, \quad (6.62)$$

with $p = N \cos \varphi$ radius of the circle of latitude (4.6) and the principal radii of curvature M and N (4.13), (4.15).

From Fig. 6.14, we take the relations

$$\frac{d\varphi}{dS} = \frac{\cos \alpha}{M}, \quad \frac{d\lambda}{dS} = \frac{\sin \alpha}{N \cos \varphi} \quad (6.63)$$

which are valid for any surface curve. We form $d\lambda/d\varphi$ and the second derivative and insert them into (6.62). Integration yields *Clairaut's equation*

$$N \cos \varphi \sin \alpha = \text{const.} \quad (6.64)$$

The constant corresponds to the radius of the parallel circle at which the geodesic has an azimuth of 90° . By differentiation with respect to S , and taking (6.63) into account, (6.64) is transformed into the equivalent relation

$$\frac{d\alpha}{dS} = \frac{\sin \alpha \tan \varphi}{N}. \quad (6.65)$$

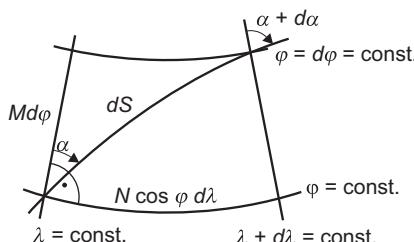


Fig. 6.14: Ellipsoidal (geodetic) surface coordinates.

Equations (6.63) and (6.64) resp. (6.65) form a system of *first-order* differential equations for the geodesic. The solution of this system leads to elliptic integrals which cannot be solved elementarily, cf. [6.3.3].

Two-dimensional positioning on the ellipsoid implies the solution of *ellipsoidal triangles*, bounded by geodesics. According to (4.18), the curvature of ellipsoidal surface curves depends on latitude and azimuth. As a consequence, the solution of a triangle not only requires three geometric elements (angles, distances) but also latitude and azimuth for orientation on the surface.

At point distances less than 100 km (classical terrestrial networks) the ellipsoid may be approximated by the Gaussian osculating sphere (4.23), with the latitude calculated as an arithmetic mean of the latitudes of the triangle vertices. Closed *spherical formulas* then can be used for the solution of triangles, e.g., the spherical law of sines

$$\frac{\sin \alpha}{\sin \beta} = \frac{\sin(a/R)}{\sin(b/R)}, \quad (6.66)$$

with the spherical angles α, β and sides a, b , R is the radius of the Gaussian sphere. Errors due to the spherical approximation remain less than $0.002''$ for the angles and less than 1 mm for the distances.

We finally mention the *spherical excess* which plays a role in spherical trigonometry. It is defined as the surplus over 180° of the angle sum of a spherical triangle. The excess is proportional to the area F of the triangle:

$$\varepsilon = \frac{F}{R^2}. \quad (6.67)$$

For an equilateral triangle with $S = 50$ km, the excess amounts to $5.48''$.

6.3.2 Reductions to the ellipsoid

In order to carry out a transfer of ellipsoidal coordinates on the ellipsoid, observed azimuths and distances have to be reduced to the ellipsoidal quantities α and S , which refer to the geodesic.

The reduction of the *astronomic azimuth* A is composed of three parts. Laplace's equation (6.58) takes the effect of the *deflection of the vertical* into account. The corresponding reduction to the normal section reads

$$\alpha - A = -(\eta \tan \phi + (\xi \sin \alpha - \eta \cos \alpha) \cot \zeta). \quad (6.68)$$

The first term in (6.68) is the azimuthal component of the deflection of the vertical. It does not depend on the azimuth and corresponds to a twist in the observed directions; horizontal angles are not affected by this change of orientation. The second term can be viewed as an "error" in setting up the theodolite, by orientating it along the plumb line direction instead of the ellipsoidal normal. While the first term reaches the order of magnitude of the vertical deflections and more, a strong reduction takes place in the second term due to $\cot \zeta$. Hence, this direction-dependent term is of the order of a few $0.1''$ in flat areas only but may reach some arcsec in the mountains.

If the target point is not located on the ellipsoid but at a height h_2 , a further reduction has to be applied. Namely, the vertical plane formed by the ellipsoidal normal at P_1 and the target point P_2 , in general, does not contain the ellipsoidal normal through P_2 (Fig. 6.15). Therefore, the ensuing normal section does not pass through the footpoint Q_2 , but through

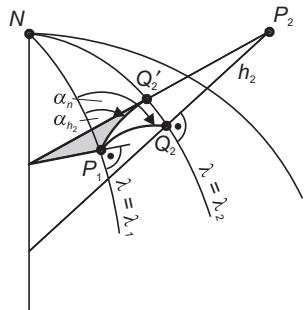


Fig. 6.15: Skew-normal reduction of the azimuth.

Q_2' , which requires a reduction by the angle $Q'_2 P_1 Q_2$. This *skew-normal* reduction can be derived from the partial derivative $\partial A / \partial h_2$, formed for the adjustment in the φ, λ, h -system, cf. [6.2.1]; it reads

$$\alpha_n - \alpha_{h_2} = \frac{e^2}{2b} \cos^2 \varphi \sin 2\alpha h_2, \quad (6.69)$$

where e is the first eccentricity and b the semi-minor axis of the ellipsoid, cf. [4.1.1]. For $\varphi = 0^\circ$ and $\alpha = 45^\circ$, the reduction attains only $0.11''$ at $h_2 = 1000$ m.

Finally, the azimuth has to be reduced from the *normal section* to the *geodesic*:

$$\alpha_g - \alpha_n = -\frac{e^2}{12a^2} \cos^2 \varphi \sin 2\alpha S^2. \quad (6.70)$$

At $\varphi = 0^\circ$ and $\alpha = 45^\circ$, this reduction reaches only $0.028''$ for $S = 100$ km.

The reduction of the chord *distance* s to the ellipsoid is a purely geometric problem, as distances do not depend on the gravity field (Höpcke, 1966). We assume that the effects of atmospheric refraction have been reduced beforehand, cf. [5.5.2]. From Fig. 6.16, we read

$$s^2 = (R + h_1)^2 + (R + h_2)^2 - 2(R + h_1)(R + h_2) \cos \psi,$$

$$s_0 = 2R \sin \frac{\psi}{2}, \quad S = R\psi,$$

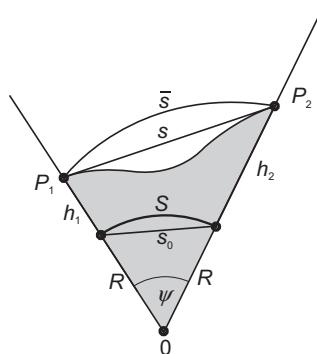


Fig. 6.16: Reduction of the spatial distance on the ellipsoid.

which gives closed formulas for the reduction to the normal section

$$s_0 = \sqrt{\frac{s^2 - (h_2 - h_1)^2}{(1 + h_1/R)(1 + h_2/R)}}, \quad S = 2R \arcsin \frac{s_0}{2R} \quad (6.71a)$$

where R is taken from Euler's formula (4.18). After series expansion, the different contributions to the reduction become apparent:

$$S - s = -\frac{h_1 + h_2}{2R}s - \frac{(h_2 - h_1)^2}{2s} + \frac{s_0^3}{24R^2}. \quad (6.71b)$$

The first term in (6.71b) corresponds to a reduction from the mean height to the ellipsoid. It reaches the meter-order of magnitude in the mountains at distances of several km. The second term takes the inclination of the distance into account. It generally remains below the meter-order of magnitude in the lowland but may attain large values in the high mountains. The magnitude of these reduction terms does not allow substitution of the ellipsoidal heights by orthometric or normal heights, otherwise relative errors of 10^{-5} have to be expected. The last term in (6.71b) provides the transition from the ellipsoidal chord to the normal section and reaches the cm-order only at larger distances.

The reduction from the *normal section* to the *geodesic* is given by

$$S_g - S_n = -\frac{e^4}{360a^4} \cos^4 \varphi \sin^2 2\alpha S^5. \quad (6.72)$$

The magnitude reaches the meter-order only at distances of several 1000 km and can be neglected in classical network computations.

6.3.3 Computations on the ellipsoid

As already mentioned, the relevance of ellipsoidal calculations has decreased, since the results of three-dimensional positioning in Cartesian coordinates can easily be transformed into ellipsoidal coordinates, see (4.28). Azimuths and distances derived from Cartesian coordinates, see (6.39), can be reduced to the ellipsoid according to [6.3.2]. Nevertheless, computations on the ellipsoid are still of significance in navigation, and they have been the basis for the calculation of classical horizontal control networks, which are still in use today.

The *geodetic datum* of the classical two-dimensional geodetic systems has been established by the deflection of the vertical and the geoid height at a fundamental point and the parameters of the reference ellipsoid, cf. [6.2.2]. Equation (6.57) then allows the transformation of observed astronomical latitude and longitude into the corresponding ellipsoidal quantities, and (6.46) provides the height relation between the geoid or quasigeoid and the ellipsoid. Having reduced the observed horizontal directions and the distances onto the ellipsoid, only one rotation about the ellipsoidal normal in the fundamental point is possible. This rotation is fixed by applying the Laplace equation on the astronomic azimuth observed at the fundamental point. Equations (6.57) and (6.58) thus provide the parallelism of the axes of the ellipsoidal system with respect to the global geocentric system.

The accuracy of the parallelism of axes depends on the accuracy of the (nineteenth or early twentieth century) astronomical observations which entered into (6.57) and (6.58), and hence

it is about 1 to 2 arcsec or even better. The origin of the classical systems, on the other hand, is far from being geocentric and may deviate by some 100 m and more from the geocenter. This results partly from the fact that 1 arcsec in astronomical positioning already corresponds to 30 m in horizontal position, but mainly from totally neglecting or only relative use of vertical deflections and geoid heights, cf. [7.1].

Having fixed the ellipsoidal coordinates and one geodetic azimuth at the fundamental point, ellipsoidal coordinate transfer can be carried out with the ellipsoidal "observations" referring to the geodesic. Here, it is assumed that the ellipsoidal network is error free; adjustment strategies are discussed in [7.1].

We distinguish between

- The *direct problem*, i.e., to compute the ellipsoidal coordinates φ_2, λ_2 of the point P_2 , as well as the azimuth α_2 , given the coordinates φ_1, λ_1 of point P_1 , the azimuth α_1 , and the distance S .
- The *inverse problem*, i.e., to compute the azimuths α_1, α_2 and the distance S , given the coordinates φ_1, λ_1 and φ_2, λ_2 of P_1 and P_2 .

The direct and the inverse problem correspond to the solution of the ellipsoidal polar triangle P_1NP_2 (Fig. 6.17), Ehlert (1993). With the geodesic introduced as a surface curve connecting P_1 and P_2 , elliptic integrals appear in the solutions, cf. [6.3.1]. Hence no closed solutions are available (Rösch and Kern, 2000). Dependent on the computing technique available, numerous solutions of the direct and the inverse problem have been developed over the past 200 years. They are based either on series expansions or on numerical integration, some examples follow.

A Taylor series expansion of latitude, longitude, and azimuth as a function of the arc length was given by Legendre already in 1806:

$$\left. \begin{aligned} \varphi_2 - \varphi_1 &= \left(\frac{d\varphi}{dS} \right)_1 S + \frac{1}{2} \left(\frac{d^2\varphi}{dS^2} \right)_1 S^2 + \dots \\ \lambda_2 - \lambda_1 &= \left(\frac{d\lambda}{dS} \right)_1 S + \frac{1}{2} \left(\frac{d^2\lambda}{dS^2} \right)_1 S^2 + \dots \\ \alpha_2 - \alpha_1 &= \left(\frac{d\alpha}{dS} \right)_1 S + \frac{1}{2} \left(\frac{d^2\alpha}{dS^2} \right)_1 S^2 + \dots \end{aligned} \right\} \quad (6.73)$$

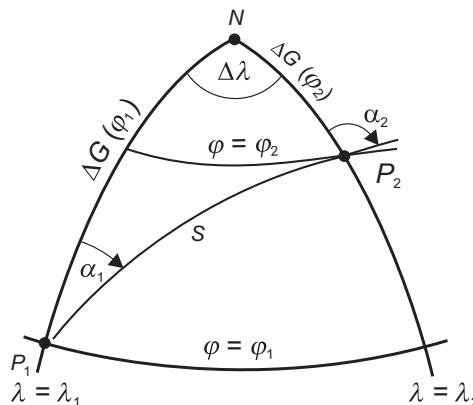


Fig. 6.17: Ellipsoidal polar triangle.

where the first-order derivatives are provided by (6.63) and (6.65), and the equation of the geodesic enters through $d\alpha/dS$. The higher-order derivatives are calculated according to

$$\frac{d^2\varphi}{dS^2} = \frac{\partial}{\partial\varphi} \left(\frac{d\varphi}{dS} \right) \frac{d\varphi}{dS} + \frac{\partial}{\partial\alpha} \left(\frac{d\varphi}{dS} \right) \frac{d\alpha}{dS}, \quad (6.74)$$

and so forth, with variable latitude and azimuth.

Since the Legendre series are expanded with respect to S , they converge slowly. An expansion to the fifth order (for φ, λ) and the fourth-order (for α) is necessary at mid-latitudes in order to provide an accuracy of $0.0001''$ and $0.001''$, respectively, at distances of 100 km. Developments up to the tenth order are available (Krack, 1982), and modifications of (6.73) improve the convergence and allow an efficient solution for lengths of several 100 km and more.

Series expansions suitable for very long geodesics have been developed by Bessel (1826) and improved by Helmert (1880). For this method, the ellipsoidal polar triangle is projected onto a concentric sphere with radius a (Fig. 6.18). The latitude φ is transformed to the reduced latitude β (4.10).

Due to Clairaut's equation (6.64), which now reads.

$$\cos\beta \sin\alpha = \text{const.}$$

the ellipsoidal azimuths are preserved, if the azimuth α_1 is transferred to the sphere. The relation between the ellipsoidal distance S and the spherical distance σ , as well as those between the ellipsoidal and the spherical longitude differences $\Delta\lambda$ and $\Delta\lambda'$, are given by differential formulas which correspond to (6.63):

$$\frac{d\beta}{d\sigma} = \cos\alpha, \quad \frac{d\lambda'}{d\sigma} = \frac{\sin\alpha}{\cos\beta}. \quad (6.75)$$

By combination with (6.63), the following relations are obtained:

$$dS = a\sqrt{1 - e^2 \cos^2\beta} d\sigma, \quad d\lambda = \sqrt{1 - e^2 \cos^2\beta} d\lambda'. \quad (6.76)$$

The elliptic integrals resulting from (6.76) are solved either by expanding the square roots in series and subsequent integration term by term or by numerical methods. As the series expansions are controlled by the (small) numerical eccentricity, they converge rapidly. After projection onto the sphere, the coordinate transfer is carried out by strict

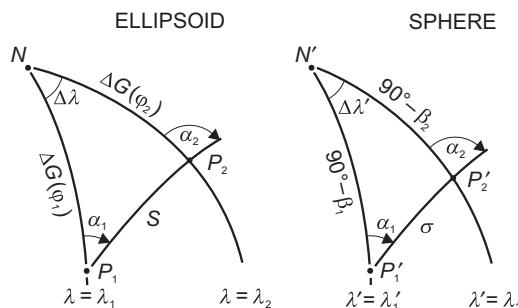


Fig. 6.18: Transfer of ellipsoidal coordinates: Bessel-Helmert solution.

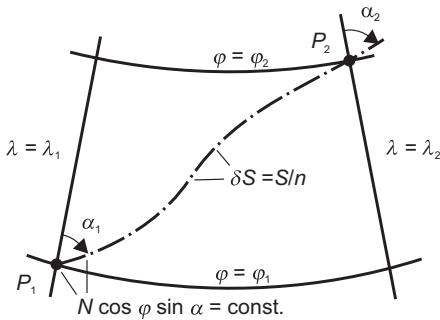


Fig. 6.19: Transfer of ellipsoidal coordinates: numerical solution.

formulas of spherical trigonometry, and the results are then transformed back to the ellipsoid by inverse relations. Computations around the globe are possible with mm accuracy (Klotz, 1993; Sjöberg, 2006).

Numerical methods are based either on a polynomial approximation of the integrals and subsequent integration (methods of Newton, Gauss, Simpson and others) or on numerical integration (Schmidt, 1999). In the latter case, the length of the geodesic is subdivided into small increments (number n), which are calculated using the differential formulas (6.63) and (6.64), Fig. 6.19. Clairaut's equation serves for keeping the increments on the direction of the geodesic. Summing the line elements provides a first approximation. By iteration with smaller increments and comparison of the results, a given error limit can be obtained. With increments of 100 m length, sub-cm accuracy can be achieved with geodesics of 10 000 km length.

By inversion, solutions of the *inverse problem* are available for all kind of methods. The adjustment of ellipsoidal networks would require *differential relations* $d\alpha/d\varphi$, $d\alpha/d\lambda$ and $dS/d\varphi$, $dS/d\lambda$. These relations can be derived from the corresponding differentials of a three-dimensional model reduced to the ellipsoid or by differentiating the solutions of the inverse problem (Wolf, 1963b).

6.4 Height determination

Precise height determination is possible either with the relative methods of geometric leveling and trigonometric height transfer using zenith angles, or with GNSS (today still mainly GPS) heighting which may be applied in the absolute or in the relative mode. The results of these methods refer to the geoid (quasigeoid) or the ellipsoid, which requires corresponding reductions. Geometric leveling after applying small reductions provides height differences defined in the gravity field [6.4.1]. Zenith angles also refer to the gravity field. Trigonometric heighting thus delivers corresponding height differences, which may be transformed into ellipsoidal ones by taking the effect of the gravity field (deflections of the vertical) into account [6.4.2]. GPS heighting, on the other hand, immediately results in geometrically defined ellipsoidal heights or height differences, which for practical use generally have to be reduced to heights above the geoid (quasigeoid) [6.4.3].

As precise heighting is based on observed *height differences*, the definition and realization of a vertical reference surface (geoid) is of fundamental importance. This *vertical datum* problem is extensively discussed in [3.4.3], for practical realization see also [7.2].

6.4.1 Heights from geometric leveling

The raw results of geometric leveling $\delta n \approx dn$ are transformed into potential differences by taking surface gravity g along the leveling line into account (5.116). If connected to the zero height surface (geoid or quasigeoid) geopotential numbers (3.104) are obtained:

$$C = W_0 - W_p = \int_0^P g dn. \quad (6.77)$$

In principle, the evaluation of (6.77) requires a *gravity* value at each leveling point, i.e., at distances of 100 m or less for precise leveling. This requirement can be diminished if we postulate the same relative accuracy for the effect of leveling and gravity on the geopotential differences:

$$\frac{dg}{g} = \frac{d(\Delta n)}{\Delta n}. \quad (6.78)$$

Assuming a leveling accuracy of 0.1 mm, gravity would only be needed with an accuracy of 100 μms^{-2} for $\Delta n = 10$ m, and 10 μms^{-2} for $\Delta n = 100$ m. Consequently, gravity values required in (6.77) can be interpolated from gravity measurements carried out at station distances of 5 to 20 km in flat areas, and at 1 to 2 km in the mountains. Preferably, gravity stations should be established at sites where the gravity changes depart from linearity (variations in slope or direction of the leveling line, gravity anomalies).

Precise leveling in fundamental networks is carried out in closed loops, cf. [7.2]. The calculation of heights is performed by adjusting *potential differences*, with the condition, cf. [3.2.3]:

$$\oint dW = 0. \quad (6.79)$$

Subsequent transformation yields metric heights, cf. [3.4.3].

An alternative approach, used classically, is to first convert the raw leveling results (with $\oint dn \neq 0$) into differences of the respective height system and then adjust *height differences*, where we distinguish again between dynamic, orthometric and normal heights.

Dynamic height differences are obtained by differencing (3.105):

$$\Delta H_{1,2}^{\text{dyn}} = H_2^{\text{dyn}} - H_1^{\text{dyn}} = \Delta n_{1,2} + E_{1,2}^{\text{dyn}}, \quad (6.80a)$$

with the dynamic height reduction

$$E_{1,2}^{\text{dyn}} = \int_1^2 \frac{g - \gamma_0^{45}}{\gamma_0^{45}} dn. \quad (6.80b)$$

For *orthometric heights*, we expand (3.106) by dynamic heights:

$$\Delta H_{1,2} = H_2 - H_1 = \Delta H_{1,2}^{\text{dyn}} + (H_2 - H_2^{\text{dyn}}) - (H_1 - H_1^{\text{dyn}}).$$

This leads to

$$\Delta H_{1,2} = \Delta n_{1,2} + E_{1,2}, \quad (6.81a)$$

with the *orthometric height reduction*

$$E_{1,2} = \int_1^2 \frac{g - \gamma_0^{45}}{\gamma_0^{45}} dn + \frac{\bar{g}_1 - \gamma_0^{45}}{\gamma_0^{45}} H_1 - \frac{\bar{g}_2 - \gamma_0^{45}}{\gamma_0^{45}} H_2. \quad (6.81b)$$

An analog equation is valid for the transformation of leveled height differences into *normal height* differences, where mean gravity along the plumb line \bar{g} is replaced by mean normal gravity $\bar{\gamma}$, and orthometric height H by normal height H^N (3.107). The *normal height reduction* then reads:

$$E_{1,2}^N = \int_1^2 \frac{g - \gamma_0^{45}}{\gamma_0^{45}} dn + \frac{\bar{\gamma}_1 - \gamma_0^{45}}{\gamma_0^{45}} H_1^N - \frac{\bar{\gamma}_2 - \gamma_0^{45}}{\gamma_0^{45}} H_2^N. \quad (6.81c)$$

The dynamic height reduction only depends on gravity and height differences along the path. It attains values between a few mm (flat terrain) and some cm to dm (mountains). Hence, it has to be taken into account even in local surveys if the vertical reference system is based on dynamic heights. The orthometric and the normal height reduction include the dynamic reduction, but, in addition, contain two terms with the mean gravity along the actual resp. normal plumb line at the end points of the leveling line. The different reduction terms substantially cancel each other, with the consequence that these reductions are below one mm in flat areas and only reach a few cm in the mountains.

Mean normal gravity $\bar{\gamma}$ can be calculated by (4.67) with the spherical approximation

$$\bar{\gamma} = \gamma_0 \left(1 - \frac{H^N}{R} \right). \quad (6.82)$$

Mean actual gravity \bar{g} , on the other hand, requires the knowledge of g along the plumb line between the geoid and the Earth's surface. At any point P' with height H' , we have

$$g' = g - \int_H^{H'} \frac{\partial g}{\partial H} dH, \quad (6.83a)$$

where g is the surface gravity at P . The actual vertical gravity gradient is given by (3.71), where we may introduce (4.60) for the free-air part and 2670 kg/m^3 as a mean crustal density; this yields the approximation

$$g' = g + 0.848 \times 10^{-6} (H - H') \text{ m s}^{-2}, \quad (6.83b)$$

also called *Poincaré-Prey reduction* (Hofmann-Wellenhof and Moritz, 2005, p. 138 ff.). After inserting into (3.106) and integration between $H' = 0$ and $H' = H/2$, we obtain the frequently used formula

$$\bar{g} = g + 0.424 \times 10^{-6} H \text{ m s}^{-2} \quad (6.84)$$

for the mean actual gravity between the Earth's surface and the geoid. Orthometric heights based on this estimate are called *Heimert heights*.

As shown in [6.5.3], the second term on the right side of (6.84) can be interpreted as a reduction of the surface gravity to actual gravity at $H/2$, with the Bouguer plate as a model of the topography. The effect of model errors remains small in flat terrain, but improved

models that take topography and density into account are needed in the mountains (Tenzer et al., 2005).

6.4.2 Trigonometrical heights

Zenith angles can be used for a trigonometrical height transfer if refraction effects have been reduced sufficiently, cf. [5.5.1], Fig. 6.20. The ellipsoidal zenith angle ζ is obtained from the observed quantity z' by

$$\zeta = z' + \delta + \varepsilon = z + \varepsilon, \quad (6.85)$$

where δ is the angle of refraction (5.11) and ε the vertical deflection component in the azimuth of the line of sight (6.18). Using spherical trigonometry, the *ellipsoidal height difference* is given by (Kneissl, 1956, p. 358):

$$\Delta h_{1,2} = h_2 - h_1 = S \left(1 + \frac{h_m}{R} \right) \cot \zeta_1 + \frac{S^2}{2R \sin^2 \zeta_1}. \quad (6.86)$$

S is the length of the ellipsoidal normal section, R the radius of curvature (4.18), and $h_m = (h_1 + h_2)/2$ represents a mean height.

The use of *reciprocal* zenith angles offers significant advantages. With the central angle ψ

$$\psi = \frac{S}{R} = \zeta_1 + \zeta_2 - \pi \quad (6.87)$$

taken from Fig. 6.20, we apply the law of tangents on the triangle P_1OP_2 . In connection with (6.85), the height difference is obtained:

$$\Delta h_{1,2} = S \left(1 + \frac{h_m}{R} + \frac{S^2}{12R^2} \right) \tan \frac{1}{2} ((z'_2 + \delta_2 + \varepsilon_2) - (z'_1 + \delta_1 + \varepsilon_1)). \quad (6.88)$$

Here, only differences in δ and ε appear. Symmetric refraction conditions may be expected with *simultaneous* observations, cf. [5.5.1], thus refraction effects will mostly

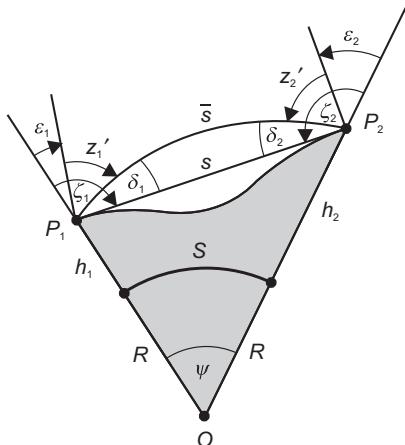


Fig. 6.20: Trigonometrical height transfer.

cancel with the use of simultaneous reciprocal-z zenith-angle measurements (Kuntz and Schmitt, 1995). They also offer a possibility to determine the *coefficient of refraction*. Combining (5.11), (6.85), and (6.87), and neglecting the deflections of the vertical, yields

$$k = 1 - \frac{R}{S} (z'_1 + z'_2 - \pi). \quad (6.89)$$

From (6.89), an average value of $k = 0.13 \pm 0.04$ was obtained by Gauss at his arc measurement in the kingdom of Hannover. This value was confirmed by other surveys for lines of sight with a large ground clearance, but close to the ground the coefficient of refraction may vary between -1 and $+1$. Network adjustment models may be extended by introducing individual refraction coefficients for each station or for each line (Hradilek, 1984), and observed meteorological parameters may also contribute to the determination of more realistic values for k , cf. [5.1.2], [5.5.1]. In spite of these refinements, refraction irregularities strongly limit the application of trigonometrical heighting. A cm-order of accuracy may be obtained over distances of a few km, but errors of the dm-order of magnitude and more have to be expected with larger distances.

Trigonometric leveling significantly diminishes the errors of a trigonometrical height transfer, by reducing the lines of sight to 100 to 300 m (Rüeger and Brunner, 1982). At this method, height differences are determined by measuring zenith angles and slope distances with a total station, cf. [5.5.2]. Either simultaneous-reciprocal observations are carried out using two reflector-equipped total stations or the method of leveling "from the middle" is applied, in analogy to geometric leveling, cf. [5.5.3]. Due to the short lines of sight running approximately parallel to the Earth's surface, refraction errors remain small and obey a favorable error propagation even over larger distances; accuracies of 1 to 2 mm per km can be achieved. The efficiency of the method can be increased by motorized procedures (Becker, 2002). Trigonometric leveling may be regarded as a special version of geometric leveling using inclined lines of sight. Hence, the results represent a good approximation to leveled height differences.

Trigonometric height determination with long lines played an important role in the establishment of classical horizontal networks by triangulation, as it simultaneously provided heights for reduction onto the ellipsoid and for the later construction of topographical maps. Today, it is restricted to special applications, e.g., to the height determination of inaccessible sites. Trigonometric leveling, on the other hand, has been employed successfully for surveying vertical control networks of large extension (Whalen, 1985).

6.4.3 Heights from GNSS (GPS)

GNSS and especially the Global Positioning System (GPS) provide global Cartesian coordinates with high accuracy, cf. [5.2.5], which can easily be transformed to ellipsoidal coordinates including the ellipsoidal height, see (4.28). While absolute heights above the reference ellipsoid can be derived with sub-cm accuracy only from global network observations, differential methods provide this accuracy already at observation times of a few hours or less, for distances of 100 km and more. Main error sources stem from the geometry of the satellites' constellation and the atmospheric refraction, cf. [5.2.5]. For distances of a few 10 km, even sub-cm accuracy can be obtained. Consequently,

GPS heighting may support or substitute time-consuming geometric leveling, at least for distances larger than about 10 km. This has led to the strategy of *GPS leveling* which requires that the reduction of ellipsoidal height differences to normal or orthometric height differences can be performed with corresponding accuracy (Dodson, 1995; Featherstone et al., 1998). According to (6.46), quasigeoid or geoid differences then provide the necessary reductions:

$$\Delta H^N = \Delta h - \Delta \zeta, \quad \Delta H = \Delta h - \Delta N. \quad (6.90)$$

We remark, that (6.90) may be evaluated for the determination of normal or orthometric height differences ("GPS leveling"), but also for deriving the quasigeoid or geoid, respectively. The latter problem presupposes the existence of a precise leveling network, well connected to the GPS derived heights, cf. [6.7]. Repeated GPS height determinations, on the other hand, may be directly evaluated with respect to temporal height changes, as correlated geoid variations only happen at large-scale mass shifts, and remain about one order of magnitude smaller. This fact can be exploited at the investigation of vertical crustal movements as well as for the detection of subsidence at tide gauges or at engineering projects, cf. [8.3.3], [8.3.4].

Today, global quasigeoid or geoid models have an accuracy of about 0.1 m, and regional models reach the cm accuracy, cf. [6.6], [6.7]. The use of these models for the reduction of GPS heights presupposes that the model contains the same reference surface as used as zero height surface for the height system, cf. [3.4.3]. This demand can be fulfilled by fitting the model to quasigeoid or geoid heights at control points where GPS and leveled heights are available. The fitting also reduces long- and medium-wave model errors. Following the method of least-squares collocation, cf. [6.8.2], the discrepancies found at the control points can be modeled (for normal heights) as follows (Denker et al., 2000):

$$h_{\text{gps}} - H^N - \zeta_{\text{mod}} = t + s + n, \quad (6.91\text{a})$$

where t describes a trend component, s is a stochastic signal part, and n represents the random noise of all types of observations involved (GPS, leveling, geopotential model). A simple trend function may consist of a three-parameter datum shift according to (6.41):

$$t = \cos \varphi \cos \lambda \Delta X + \cos \varphi \sin \lambda \Delta Y + \sin \varphi \Delta Z. \quad (6.91\text{b})$$

Equivalently, the trend function may consist of a change in the ellipsoidal coordinates of some initial point, which corresponds to a vertical shift and tilts in the NS- and the EW-direction. Presupposing a sufficient number of control points, the signal part can be derived from an empirical covariance function of the de-trended residuals and modeled, e.g., by an exponential function, cf. [6.1.3].

Using trend reduction only, the r.m.s. discrepancies between local geoid/quasigeoid models and GPS/leveling control points have been reduced to the dm-order of magnitude over a few 1000 km and to a few centimetre over several 100 km. By also including a signal part, cm-accuracy may be obtained over distances up to 1000 km, which corresponds to the accuracy of classical leveling networks (Denker, 1998). Large-scale GPS leveling is now an efficient tool for improving or completely renewing national and continental height systems, cf. [7.2]. Local applications include, among others, the height transfer to islands (e.g., Seeber and Torge, 1997) or to high mountains such as Mount Everest (Chen et al., 2010). For *local*

(several 10 km) applications, gravity field related heights may also be estimated by purely mathematical interpolation between GPS/leveling control points, employing, e.g., low-order surface polynomials or splines. If a dense net of control points is available, and if the gravity field is sufficiently smooth, cm-accuracy can be achieved (Collier and Croft, 1997). The interpolation accuracy rapidly decreases at rough topography, and a topographic reduction will be necessary then, cf. [6.5.3].

With the further improvement of global and regional quasigeoid/geoid models, GPS leveling will become even more important.

6.5 Fundamentals of gravity field modeling

Gravity field modeling is part of the geodetic boundary-value problem [6.5.1]. Topography plays an important role in the solution of this problem [6.5.2]. Gravity reductions serve for reducing observed gravity field data onto the geoid and subsequent geoid computation, and also provide different kinds of gravity anomalies for field interpolation and geophysical interpretation [6.5.3]. While the orientation of the gravimetrically derived geoid is uniquely defined, the scale remains unknown and has to be determined by distance measurements [6.5.4].

6.5.1 The geodetic boundary-value problem

The geodetic boundary-value problem comprises the determination of the surface of the Earth and of its external gravity field from observations on or close to the Earth's surface (Sansò and Rummel, 1997). The surface to be determined is either the geoid (*Stokes* problem) or the physical surface of the Earth and the quasigeoid (*Molodensky* problem), Sansò (1995).

We start from Green's third identity (e.g., Jekeli, 2009, p. 19), applied here for a function V , being continuous and finite outside and on the surface S , with continuous and finite partial derivatives of the first and second order there, and vanishing in infinity (Heiskanen and Moritz, 1967, p. 11ff.). With n being defined as the outer surface normal and l the distance between the point of evaluation and the source point, cf. [3.1.1], we have

$$\iiint_V \frac{1}{l} \Delta V dv = -pV - \iint_S \left(\frac{1}{l} \frac{\partial V}{\partial n} - V \frac{\partial}{\partial n} \left(\frac{1}{l} \right) \right) dS, \quad (6.92a)$$

with $p = 4\pi$ if P is outside S , and $p = 2\pi$ if P is on S . If we apply (6.92a) on the gravity potential W (3.42) and take the generalized Laplace equation (3.49) into account, the fundamental boundary problem of physical geodesy may be formulated by a non-linear integral equation of the second kind in the gravity potential (Molodenski et al., 1962). The above substitutions finally lead to (Heiskanen and Moritz, 1968, p. 15):

$$-2\pi W + \iint_S \left(W \frac{\partial}{\partial n_s} \left(\frac{1}{l} \right) - \frac{1}{l} \frac{\partial W}{\partial n_s} \right) dS + 2\pi \omega^2 (X^2 + Y^2) + 2\omega^2 \iiint_V \frac{dv}{l} = 0. \quad (6.92b)$$

Now n_s is the outer surface normal to the Earth's surface S , v is the volume of the Earth and ω its rotational velocity, and l denotes the distance between the source point (on the surface or the interior of the Earth) and the point of calculation. If W and $\partial W / \partial n_s$

(i.e., the gravity component normal to the surface) were known on S , then the geometry of the Earth's surface would remain as the only unknown quantity. After the determination of S , an upward continuation of W would deliver the external gravity field.

This boundary-value problem can be *linearized* by approximating the Earth's surface by the telluroid (with respect to the physical surface) or the ellipsoid (with respect to the geoid), and the actual gravity potential W by the normal potential U , cf. [6.1.1]. As the centrifugal part is well known, (6.92b) then transforms into an *integral equation* for T

$$-2\pi T + \iint_{\Sigma} \left(T \frac{\partial}{\partial n_{\Sigma}} \left(\frac{1}{I} \right) - \frac{1}{I} \frac{\partial T}{\partial n_{\Sigma}} \right) d\Sigma = 0. \quad (6.93)$$

For the *physical surface*, the integration is now performed over the *known* telluroid Σ . As the surface normal n_{Σ} deviates from the direction of the plumb line, $\partial T / \partial n_{\Sigma}$ not only depends on the gravity disturbance and gravity anomaly, respectively, but also on the deflection of the vertical and the slope of the terrain, cf. [6.7.2]. If (6.93), on the other hand, is applied on the *geoid* as boundary surface, this dependence reduces to the gravity disturbance respectively gravity anomaly.

Instead of the integral equation (6.93), the geodetic boundary-value problem can also be formulated by *Laplace's differential equation* (6.2):

$$\Delta T = 0. \quad (6.94)$$

The residual gravity field parameters observed on the Earth's surface, or reduced to the geoid, then enter into boundary conditions for the solution of (6.94). The primary "observables" are the height anomalies and the geoid heights, respectively, and the gravity disturbances or gravity anomalies. Deflections of the vertical and gravity gradient components play a role only in local calculations.

A Taylor development of U in the telluroid point Q gives

$$U_p = U_Q + \left(\frac{\partial U}{\partial \bar{n}} \right)_Q \zeta_p + \dots, \quad (6.95)$$

where \bar{n} is the normal to $U = U_Q$ and ζ_p the *height anomaly*. Solving for ζ_p and inserting into (6.1) yields

$$\zeta_p = \frac{T_p - (W_p - U_Q)}{\gamma_Q}, \quad (6.96a)$$

with the normal gravity

$$\gamma_Q = - \left(\frac{\partial U}{\partial \bar{n}} \right)_Q. \quad (6.96b)$$

The condition $U_Q = W_Q$ (6.6) finally delivers

$$\zeta_p = \frac{T_p}{\gamma_Q}. \quad (6.96c)$$

If (6.96a) is applied to the geoid, we obtain the corresponding relation between the *geoid height* and the disturbing potential on the geoid:

$$N = \frac{T - (W_0 - U_0)}{\gamma_0}, \quad (6.97a)$$

where γ_0 is normal gravity on the ellipsoid (4.41). Under the condition $U_0 = W_0$, (6.97a) reads

$$N = \frac{T}{\gamma_0}. \quad (6.97b)$$

This simple relation between the geoid height (a geometric quantity) and the disturbing potential (a physical quantity) has been known as *Brun's theorem*. As demonstrated above, it is also valid at the Earth's surface, and can be extended to the exterior space, cf. [6.7.3].

We now derive the relations between the disturbing potential and residual gravity (deflection of the vertical, gravity disturbance/anomaly, cf. [6.1.2]). The *deflection of the vertical* is the horizontal derivative of ζ resp. N (Fig. 6.21). Taking (6.96) and (6.97) into account, the components in the direction of the meridian and the prime vertical are then given by

$$\xi = -\frac{1}{\gamma(M+h)} \frac{\partial T}{\partial \varphi}, \quad \eta = -\frac{1}{\gamma(N+h) \cos \varphi} \frac{\partial T}{\partial \lambda}, \quad (6.98a)$$

where the ellipsoidal arc elements are provided by (4.20). The negative sign follows from the sign conventions for the quasigeoid (geoid) and the vertical deflection, see (6.40).

In spherical approximation we obtain

$$\xi = -\frac{1}{\gamma r} \frac{\partial T}{\partial \varphi}, \quad \eta = -\frac{1}{\gamma r \cos \varphi} \frac{\partial T}{\partial \lambda}. \quad (6.98b)$$

The *gravity disturbance* (6.11) is related to T by

$$\delta g_p = g_p - \gamma_p = -\left(\frac{\partial W}{\partial n}\right)_p - \left(-\frac{\partial U}{\partial n}\right)_p = -\left(\frac{\partial T}{\partial n}\right)_p, \quad (6.99a)$$

where we have neglected the deflection of the vertical. We now develop γ_p at the teluroid point Q , taking (6.96c) into account:

$$\gamma_p = \gamma_Q + \left(\frac{\partial \gamma}{\partial n}\right)_Q \xi_p + \dots. \quad (6.100a)$$

Inserting into (6.99) and taking (6.96c) into account yields the *gravity anomaly*:

$$\Delta g_p = g_p - \gamma_Q = -\left(\frac{\partial T}{\partial n}\right)_p + \frac{1}{\gamma_Q} \left(\frac{\partial \gamma}{\partial n}\right)_Q T_p. \quad (6.101a)$$

The important relation between gravity anomaly and gravity disturbance reads as

$$\Delta g_p = \delta g_p + \frac{1}{\gamma_Q} \left(\frac{\partial \gamma}{\partial n}\right)_Q T_p. \quad (6.102)$$

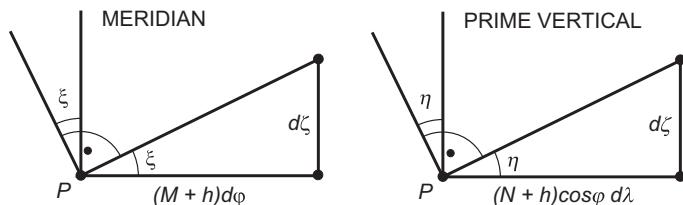


Fig. 6.21: Deflection of the vertical components and height anomaly.

With the spherical approximation cf. [4.2.2],

$$\frac{\partial}{\partial n} = \frac{\partial}{\partial \bar{n}} = \frac{\partial}{\partial r}, \text{ we have } \frac{\partial \gamma}{\partial \bar{n}} = \frac{\partial \gamma}{\partial r} = -2 \frac{\gamma}{r},$$

and (6.99a) to (6.101a) and (6.102) read as

$$\delta g_p = -\frac{\partial T}{\partial r}, \quad (6.99b)$$

$$\gamma_p = \gamma_Q - \frac{2}{r} T, \quad (6.100b)$$

$$\Delta g = -\frac{\partial T}{\partial r} - \frac{2}{r} T = \delta g - \frac{2}{r} T. \quad (6.101b)$$

Equations (6.99), (6.101) represent *boundary conditions* for the solution of the Laplace equation (6.94). Because of the importance of (6.101), this first-order partial differential equation in T is also known as the fundamental equation of physical geodesy.

High-resolution gravity-field modeling (e.g., geoid determination with cm-accuracy) requires some refinements in the formulation and solution of the geodetic boundary-value problem (Moritz, 1974; Heck, 1991). This includes the transition to an ellipsoidal approximation by developing the potential in ellipsoidal harmonics or by applying ellipsoidal corrections to the spherical approximation (Jekeli, 1988b; Wang, 1999). It should be remembered that the spherical approximation primarily stems from neglecting the ellipsoid's flattening, which is about 0.3%. This results in corresponding relative errors in the residual gravity field quantities derived from the solution of the boundary value problem. As an example, with an r.m.s. geoid variation of about 30 m, a geoid calculation would thus be erroneous by 0.1 m. Furthermore, the mass of the atmosphere has to be taken into account by a corresponding reduction, cf. [4.3], and the topography has to be smoothed by a terrain correction, cf. [6.5.3].

The geodetic boundary-value problem resembles the third boundary-value problem of potential theory, namely to determine a harmonic function given a linear combination of the function and its normal derivative on a bounding surface. It differs from the classical problem, as the bounding surface is supposed to be unknown: *free* boundary-value problem. In addition, observed gravity data do not represent potential derivatives with respect to the physical surface of the Earth, but rather refer to the plumb line: *free* and *oblique* boundary-value problem (Graffarend and Niemeier, 1971). Finally, the horizontal components of the position vector cannot be determined with sufficient accuracy from gravimetric data, cf. [6.2.1], consequently the geometric part of the problem is generally restricted to the determination of heights: *scalar* free gravimetric boundary-value problem (Heck, 1997).

With the rapid progress in satellite positioning and satellite altimetry, the geometry of the Earth's surface now can be assumed to be known with still increasing accuracy; the only remaining unknown at the boundary value problem then is the external gravity potential. Hence, a *fixed* boundary-value problem can be formulated according to (6.99) which employs gravity disturbances as boundary values (Koch and Pope, 1972; Bjerhammar and Svensson, 1983), cf. [6.7.1]. This corresponds to the second (*Neumann*) boundary-value problem of potential theory, which is to determine a harmonic function from its derivative given on the bounding surface. Finally, a mixed altimetric-gravimetric boundary-value problem may be set up, taking into account that – in addition to the harmonic coefficients derived from satellite orbit analysis or satellite gradiometry – altimetric geoid heights and gravity anomalies are the main data sets available on a global scale (Sansò and Rummel, 1997).

6.5.2 Gravitation of topography, digital elevation models

The short-wavelength part of the gravitational field is dominated by the effect of the *topographical masses*. By removing this effect, the gravity field is smoothed significantly, which simplifies gravity field interpolation and transformation procedures; a corresponding restoration of topography has to follow, cf. [6.7]. For the determination of the geoid, the topography has to be removed completely in order to establish this level surface as a boundary surface in the gravity field (Forsberg and Tscherning, 1997). In addition, the knowledge of the topography is of relevance at forward gravity modeling, i.e., for the calculation of synthetic gravity models from the Earth masses. These statements are also valid for the Earth's crust and upper mantle, where *isostasy* mainly governs the mass distribution and affects the gravity field in the medium-wavelength part, cf. [8.2.2]. In the following, we concentrate on the calculation of the gravitation of topographic (and isostatic) mass distributions and the present state of knowledge of topography (height and density).

The effect of the topographic masses on gravity field parameters is calculated by the law of gravitation. The evaluation of (3.10) and corresponding integrals for other parameters poses problems, as topography is rather irregular in geometry (heights) and, to a far lesser extent, also in density. Therefore, the topographic masses are subdivided into elementary bodies for which closed solutions of the mass integrals exist. Rectangular *prisms* of constant density are especially appropriate, as the heights of the topography nowadays are provided in gridded form by digital elevation models (see below), but spherical or ellipsoidal tesseroids and point masses may also be used (Heck and Seitz, 2007). Vertical *cylindrical* columns around the point of calculation, constructed from concentric circles and horizontal radii and with constant density and height, have been used extensively in the past, but require coordinate transformation.

Starting from a system of three-dimensional Cartesian coordinates, the gravitational potential of the topography is expressed by

$$V_{\text{top}} = G\rho \iiint_v \frac{dv}{l} = G\rho \int_{x_1}^{x_2} \int_{y_1}^{y_2} \int_{z_1}^{z_2} \frac{1}{l} dx dy dz, \quad (6.103)$$

with $l = \sqrt{x^2 + y^2 + z^2}$. The topographic effects on the deflection of the vertical, the gravity disturbance, and the gravity anomaly follow from the relations (6.97), (6.98), (6.99), and (6.101). The integration over a *rectangular prism* (Fig. 6.22) with density ρ delivers closed formulas for the potential and its derivatives (Nagy, 1966; Nagy et al., 2000, 2002; Denker, 2012, p. 57). As an example, for a point located at the origin of the local x, y, z -system, the potential is given by

$$\begin{aligned} V^{\text{prism}} = G\rho & \left| \left| \left| xy \ln(z+l) + xz \ln(y+l) + yz \ln(x+l) - \frac{x^2}{2} \arctan \frac{yz}{xl} \right. \right. \right. \\ & \left. \left. \left. - \frac{y^2}{2} \arctan \frac{xz}{yl} - \frac{z^2}{2} \arctan \frac{xy}{zl} \right|_{x_1}^{x_2} \right|_{y_1}^{y_2} \right|_{z_1}^{z_2}. \end{aligned} \quad (6.104a)$$

The *vertical* component of the *gravitation* reads as (Nagy, 1966)

$$b_z^{\text{prism}} = G\rho \left| \left| \left| x \ln(y+l) + y \ln(x+l) - z \arctan \frac{xy}{zl} \right|_{x_1}^{x_2} \right|_{y_1}^{y_2} \right|_{z_1}^{z_2}. \quad (6.104b)$$

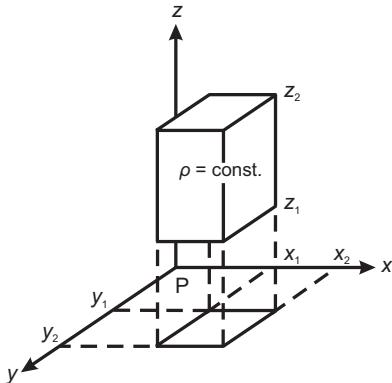


Fig. 6.22: Gravitation of topography: rectangular prism method.

The total effect of topography results from the sum over the gravitation of the individual elementary bodies:

$$\delta g_{\text{top}} = \sum b_z. \quad (6.105)$$

For heights given in a regular grid (e.g., formed by ellipsoidal or plane coordinates). Fast Fourier Transform (FFT) techniques provide a powerful tool for the efficient calculation of topographic effects (Schwarz et al., 1990).

Digital elevation models (DEM), also called digital terrain models, are nowadays available on a global and regional scale (Li et al., 2005). They provide gridded height values above the geoid, and depths below mean sea level (marine areas). The quality of a DEM depends on the sampling density and accuracy of the height measurement method, the grid resolution (ranging from about 1 arcsec to 5') and the data interpolation method as well as on the roughness of the terrain. Until recently, DEMs have been derived from digitized topographic and bathymetric maps, generally containing height/depths information in the form of contour lines. The underlying measurement methods included all kind of ground-based surveying methods as well as airborne stereo-photogrammetry and LIDAR (Light Detection And Ranging). Beginning in the 1980s, remote-sensing space techniques now dominate the development of DEMs. Among them is the space and airborne Interferometric Synthetic Aperture Radar (InSAR). This method uses a digital image correlation from two subsequent radar signals (intensity and phase) reflected from one point on the surface of the Earth. The phase differences obtained by two separate antenna positions are used for topographic mapping, where either two antennas are installed on the same platform (single-pass mode) or one antenna is operated on exactly repeated tracks (repeat-pass mode). The images from the same scene but different antenna positions then allow to determine topography and surface deformations, cf. [8.3.4], Hanssen (2001). Satellite laser and radar altimetry serve for the height determination of the Greenland and Antarctica ice sheets, cf. [5.2.7]. Radar altimetry also provides bathymetric information, due to the high correlation (at wavelengths of a few 10 to a few 100 km) between the ocean surface and the ocean bottom; ship depths soundings are efficiently supported and densified by this method (Sandwell and Smith, 2001).

With respect to the *density* of the topographic masses a special remark is necessary. In the uppermost layers of the Earth this quantity varies between 2000 and 3000 kg/m³, a global model with high spatial resolution is not available, cf. [8.2.1]. Therefore, a *mean* density value of 2670 kg/m³ (corresponding to the density of granite) generally is introduced in physical geodesy, for global and regional applications. More refined density models are used for local studies, where the density values are estimated from geological information, rock samples, and gravity profiles exploiting the density-dependent relation between gravity and height: *Nettleton* method (e.g., Torge, 1989).

Among the more recent global DEMs are the NOAA ETOPO5 (5' × 5' gridded land and seafloor elevations) and the GLOBE (GLObal land one-kilometer Base Elevation) model. GLOBE is given in a 30" × 30" grid; the accuracy depends on the data quality and varies between 20 m and a few 100 m (Hastings et al., 2000), the U.S. Geological Survey model GTOPO30 has similar properties. The NASA/NIMA Shuttle Radar Topography Mission (SRTM, February 2000) collected a global (between ±60° latitude) InSAR data set, with a resolution of 1 arcsec (for the area of the U.S.A.) and 3 arcsec, respectively, and an accuracy of 6 to 9 m (Farr et al., 2007). The results have been used, in connection with ICESat laser altimetry and ocean bathymetry, for the 30" × 30" DTM2006.0 (Digital Topographic Model) of the U.S. National Geospatial-Intelligence Agency (Becker et al., 2009). Fusing of SRTM data and satellite radar altimetry results (ERS, TOPEX, etc.) led to an improved global land digital elevation model (ACE2), Berry et al. (2010). Another high resolution (1"/0.3") and high accuracy (3 m/10 m) Global Digital Elevation Model (GDEM) is available from the ASTER (Advanced Spaceborne Thermal Emission and Reflection radiometer) instrument on-board the Terra satellite (1999, $i = 98^\circ$, $h \approx 670$ km), within the frame of an U.S./Japan cooperation. The German (DLR) TanDEM-X mission (fully operational since 2010) employs two active radar satellites (TerraSAR-X) in nearly identical orbit configuration (polar orbit, mutual distance of a few 100 m, $h \approx 514$ km). The absolute/relative accuracy of the resulting DEM amounts to 10 m/2 m, and the (latitude dependent) resolution is between 12 m and 5 m (Zheng et al., 2010). Regional DEMs have been developed in many countries with resolutions down to 1 arcsec (Smith and Roman, 2000).

Global height information also has been used early for developing *spherical harmonic models* of the topography (and later also for isostasy). While Prey (1922) could only carry out a development to the 16th degree, more recent models benefit from the rapid progress of DEMs. The degree of development orientates itself on the state of global gravity field modeling, cf. [6.6], resulting in developments (heights and depths) until degree and order 360 (Pavlis and Rapp, 1990) and 2190 (Pavlis et al., 2008), cf. [6.6.3]. These topographic-isostatic models not only serve for reduction purposes, but may also be used for the prediction of gravity anomalies in unsurveyed areas, cf. [6.5.3].

6.5.3 Gravity reductions to the geoid

The determination of the geoid requires some special considerations. As the solution of this problem is based on the assumption that the geoid represents a boundary surface in the gravity field, the topographic masses (masses above the geoid) have to be removed, and the observed gravity field data (here we restrict ourselves to gravity values, for the reduction of deflections of the vertical see [6.7.4]) have to be reduced to the geoid. This is done by *gravity reductions*, which provide gravity anomalies on the geoid.

Depending on how the topographic masses are displaced, different types of gravity anomalies are obtained. The topographic reduction is connected with a propagation of the topographic model errors (height and density errors) into the calculation of the geoid. This has to be taken into account, for example, in the calculation of orthometric heights (3.106), where the same topographic model has to be employed.

The displacement of the topographical masses changes the gravitational field of the Earth, including the potential of the geoid: *indirect effect* of the gravity reductions. The level surface which possesses the geoid potential after the displacement is called the *cogeoid*.

The terminus “compensated geoid” was introduced by J. de Graaff-Hunter and G. Bomford in the 1930s, after removal of topography and isostatic compensation at geoid calculations for India. The more general expression cogeoid results from the discussions at the IAG General Assembly in Oslo 1948.

The following steps may be distinguished in the calculation of the geoid (Fig. 6.23):

- Reduction of the *direct* effect of the topography on gravity and adding of the *direct* effect of the dislocated masses if necessary, both to be calculated by the law of gravitation, cf. [6.5.2],
- calculation of the *primary indirect* effect on the potential, caused by the removal of the topography and the dislocation of the topographic masses. The calculation is performed according to some rule of compensation:

$$\delta V = V_{\text{top}} - V_c, \quad (6.106)$$

with V_{top} potential of the topography and V_c potential of the compensating masses,

- calculation of the *vertical distance* between the geoid and the cogeoid according to Bruns' theorem (6.97b):

$$\delta N = \frac{\delta V}{\gamma}, \quad (6.107)$$

- reduction of the gravity values from the geoid to the cogeoid: *secondary indirect* effect. Here, a free-air reduction (6.101) is sufficient:

$$\delta g_c = 2 \frac{\gamma}{r} \delta N, \quad (6.108)$$

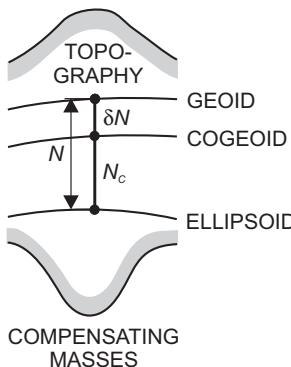


Fig. 6.23: Geoid and cogeoid.

- calculation of the heights N_c of the *cogeoid* above the ellipsoid, as the solution of a gravimetric boundary-value problem, cf. [6.6], [6.7],
- calculation of the *geoid* heights according to

$$N = N_c + \delta N. \quad (6.109)$$

In principle, every kind of gravity reduction could serve for the calculation of the geoid according to this scheme. Naturally, the indirect effect should be small in order to avoid laborious and error susceptible computations. Other criteria for the selection of gravity reductions include the smoothness of the resulting gravity anomalies, which facilitates interpolation, and their geophysical significance, which would allow a corresponding interpretation. Under these aspects, we may distinguish between the effects of a homogeneous topography, density anomalies within the topography and the Earth's crust, and isostatic compensation masses (Martinec, 1998), cf. [8.2.2].

The *free-air anomaly* is generally used for the calculation of the geoid, with the assumption that no masses exist above the geoid. The *free-air reduction*

$$\delta g_F = -\frac{\partial g}{\partial H} H, \quad (6.110)$$

with H being the orthometric height, provides the reduction of the surface gravity to the geoid, and the *simple free-air anomaly* on the geoid is then given by

$$\Delta g_F = g + \delta g_F - \gamma_0, \quad (6.111)$$

where γ_0 is normal gravity on the ellipsoid. The free-air anomaly on the *geoid* should be clearly distinguished from the free-air anomaly defined on the *surface* of the Earth (6.15) where the *normal* gravity gradient is used for reduction.

According to (6.110), the correct reduction to the geoid would require the knowledge of the real vertical gravity gradient. Splitting the gradient into a normal and an anomalous part gives

$$\frac{\partial g}{\partial H} = \frac{\partial \gamma}{\partial H} + \frac{\partial (\Delta g)}{\partial H}. \quad (6.112)$$

The real and the normal part may differ by 10% or more. The normal gravity gradient can be calculated by (4.61). The calculation of the anomalous part corresponds to the downward continuation of a harmonic function. It can be formulated by Poisson's integral, which is a solution of the first (Dirichlet) boundary-value problem of potential theory, and solved by an integration over the surface gravity anomalies, cf. [6.7.2]. If the gravity anomaly depends linearly on elevation, the anomalous gradient part of the free-air reduction corresponds to the terrain correction (Moritz, 1980, p. 421), see below. This is of importance at practical geoid calculations, cf. [6.7.1]. A discrete solution of this problem has been given by Bjerhammar (1985), which takes into account that gravity data are given only at discrete points. This solution satisfies all given data and generates missing data, and it is harmonic down to an internal sphere, located close to the Earth's surface (*Bjerhammar sphere*), cf. [3.3.2].

The *terrain correction* removes geometric irregularities of the topography. It creates a plate (spherical or planar) of constant thickness and (assumed to be) constant density by filling mass deficits below P and removing excess masses above the plate: *Bouguer plate* (Fig. 6.24). For planar approximation (Bouguer plate extending to infinity), both measures increase gravity at P ; the terrain correction then is always positive. It can be calculated from digital elevation models, cf. [6.5.2], and attains values of 1 to 10 $\mu\text{m s}^{-2}$

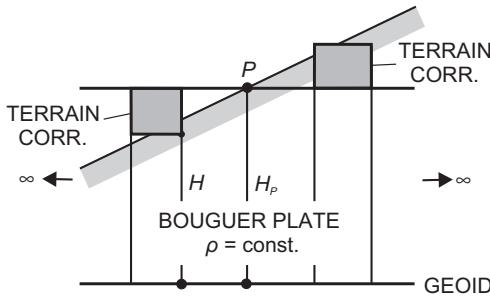


Fig. 6.24: Bouguer plate and terrain correction.

in flat areas, reaching several $100 \mu\text{ms}^{-2}$ in the mountains. From the evaluation of (6.103), we obtain for the terrain correction

$$\delta g_T = G\rho \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \int_{z=H_p}^{z=H} \frac{z - H_p}{l^3} dx dy dz. \quad (6.113a)$$

For small surface slopes, the distance

$$l = \sqrt{(x - x_p)^2 + (y - y_p)^2 + (z - z_p)^2}$$

may be approximated by

$$l_0 = \sqrt{(x - x_p)^2 + (y - y_p)^2}.$$

The linear approximation of the terrain correction then reads

$$\delta g_T = \frac{1}{2} G\rho \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \frac{(H - H_p)^2}{l_0^3} dx dy, \quad (6.113b)$$

where H and H_p are the orthometric heights of the (running) terrain point and the point of calculation (Forsberg and Tscherning, 1997).

By including the terrain correction into (6.111), we obtain the *terrain-corrected free-air anomaly*, also called *Faye anomaly*. The shift of the topographic masses now corresponds to a condensation of the Bouguer plate on the geoid (Helmert's *condensation method*), Heck (2003b). Here, the *surface density*

$$\mu = \frac{dm}{ds} = \rho \frac{dv}{ds} = \rho H \quad (6.114)$$

replaces the volume density ρ and takes the height of topography into account.

As the mass displacement is slight, the indirect effect of the free-air and the condensation reduction remains small. It reaches a few meters in the absolute sense at most, and is of the cm- to dm-order of magnitude for geoid differences. As the height-dependent effect of the topographic masses has not been removed, free-air anomalies are strongly correlated with height. Therefore, *point* free-air anomalies are not suited for interpolation and cannot be geophysically interpreted. For limited areas, the height-dependence generally can be described by linear regression, this smoothing of the anomaly field corresponds to the application of the Bouguer plate reduction (see below).

By removing the effect of topography explicitly through a *topographic reduction* δg_{top} , we obtain the *Bouguer gravity anomaly* Δg_B (we use this term under the assumption of a strict topographic mass reduction, although Bouguer for practical reasons originally applied an approximation, see below). After the removal of the masses the surface gravity again is reduced to the geoid by the free-air reduction and compared with the normal gravity γ_0 (Fig. 6.24):

$$\Delta g_B = g - \delta g_{\text{top}} + \delta g_F - \gamma_0. \quad (6.115)$$

The topographic reduction can be calculated from digital elevation models, applying the law of gravitation on standard mass elements, cf. [6.5.2].

Traditionally (in order to simplify calculation), the topographic reduction is decomposed into the Bouguer plate reduction δg_p and the terrain correction δg_T . The *Bouguer plate reduction* accounts for the gravitation of an infinitely extended horizontal plate with constant density. Its thickness is given by the height of the computation point. The gravitational effect of the Bouguer plate is derived from the attraction of a circular cylinder on a point located on the cylinder axis (e.g., Torge, 1989). By extending the cylinder radius to infinity, one obtains

$$\delta g_p = 2\pi G\rho H = 0.000\,419 \rho H \mu\text{ms}^{-2}, \quad (6.116)$$

where ρ is taken in kg/m^3 and H in m. Here we have assumed that the *terrain correction* has reduced the actual topography to the Bouguer plate (see above). After this decomposition of the topographic reduction the *Bouguer anomaly* reads

$$\Delta g_B = g - \delta g_p + \delta g_T + \delta g_F - \gamma_0. \quad (6.117)$$

Due to the removal of the height-dependent part of topography, Bouguer anomalies display smooth long-wave variations only. Hence, they are well suited for interpolation. Revealing density anomalies below the geoid, the Bouguer anomalies are also of considerable significance in geophysics and geology, cf. [8.2.4]. For regional and local applications (e.g., national gravimetric surveys), a *spherical* Bouguer plate and a corresponding terrain correction is used frequently, with a calculation extending 170 km from the computation point and conventional density being 2670 kg/m^3 . On the other hand, since the topographic masses are completely removed and not restored (i.e., they are shifted to infinity!), the indirect effect on the geoid is very large (up to several 100 m). Hence, Bouguer anomalies are not used for geoid computations.

The Bouguer plate model also allows a simple calculation of the *mean gravity* \bar{g} along the plumb line required for the computation of the orthometric height H (3.106), (6.81). If we assume a linear change of g along the vertical, \bar{g} will be found at the height $H/2$. Hence it can be derived from surface gravity by removing a Bouguer plate of thickness $H/2$, a free-air reduction from H to $H/2$, and a subsequent restoration of the Bouguer plate above $H/2$. Removing and restoring the Bouguer plate has the same (negative) effect on gravity; so we obtain

$$\bar{g} = g - \delta g_p(H) + \delta g_F\left(\frac{H}{2}\right). \quad (6.118)$$

Evaluation with (6.116) and (6.110), and introducing the density value 2670 kg/m^3 , leads to (6.84).

Equation (6.118) also provides an important interpretation of the difference between the heights of the geoid and the quasigeoid, and the normal and the orthometric height, respectively. We calculate the mean normal gravity

$$\bar{\gamma} = \gamma_0 - \delta g_F \left(\frac{H}{2} \right) \quad (6.119)$$

according to (6.118), and subtract it from \bar{g} . The *mean gravity anomaly* introduced in (6.9) is then identified as the “simple” Bouguer anomaly (terrain correction neglected)

$$\bar{g} - \bar{\gamma} = g - \delta g_p(H) + \delta g_F(H) - \gamma_0 = \Delta g_B. \quad (6.120)$$

This fact permits a simple transformation from the geoid to the quasigeoid and vice versa, e.g., Flury and Rummel (2009), cf. [6.7.2].

Isostatic anomalies are formed by not only removing the gravitational effect of topography but by also restoring compensation masses in the Earth’s crust below the geoid, according to some isostatic model (e.g., Martinec, 1993). In this way, the crust is regularized, obtaining constant thickness and density, cf. [8.2.2]. The gravitation of the compensating masses is taken into account by an *isostatic reduction* δg_I to be calculated from the isostatic model according to [6.5.2]. The isostatic anomaly then is given by

$$\Delta g_I = g - \delta g_{\text{top}} + \delta g_I + \delta g_F - \gamma_0. \quad (6.121)$$

The largest part of the Earth’s topography is isostatically compensated. Hence, isostatic anomalies are small and vary smoothly about zero, with the exception of uncompensated areas (tectonic plate boundaries, regions of postglacial land uplift, etc.). They may be successfully employed for gravity prediction, and they are of value for geophysical and geodynamic interpretation, cf. [8.2.4]. As the compensating masses are arranged more remote from topography than in the free-air reduction (see above), the indirect effect is larger and may reach the amount of 10 m. Therefore, isostatic anomalies have been rarely used for geoid calculations.

6.5.4 Orientation and scale of gravity field models

We now investigate the orientation and the scale of a gravimetrically derived geoid/quasigeoid, i.e., the “gravimetric datum”, see Hofmann-Wellenhof and Moritz (2005, p. 109 ff.).

The following *assumptions* were made for the spherical harmonic expansion of the disturbing potential and the quasigeoid/geoid, respectively, cf. [6.1.1], [6.5.1]:

- The level ellipsoid and the Earth have the same mass:

$$M_{\text{Ell}} = M. \quad (6.122)$$

- Hence, no zero-degree term T_0 appeared in the expansion (6.4).
- The center of the ellipsoid and the Earth’s center of mass (origin of the global coordinate system) coincide; no first-degree term entered into (6.4), cf. also [3.3.4].
- The normal potential U and the real potential W are related by

$$U_Q = W_p. \quad (6.123)$$

A first-degree term in the spherical harmonic expansion would not affect the gravity anomaly, as the corresponding expansion (6.136) contains the factor $(l - 1)$. Hence, the ellipsoid may be positioned in the geocenter without changing the gravity field: the gravimetric method yields “absolute” results.

Because of residual uncertainties in the determination of the mass and the potential, small differences between the values for the geoid and the ellipsoid may be admitted:

$$\delta M = M - M_{\text{Ell}}, \quad \delta W = W_0 - U_0. \quad (6.124)$$

The spherical harmonic expansion of T then must be extended by

$$T_0 = \frac{G\delta M}{R}, \quad (6.125)$$

and Bruns' formula must take T_0 and the potential difference into account:

$$N_0 = \frac{G\delta M}{\gamma R} - \frac{\delta W}{\gamma}. \quad (6.126)$$

For spherical approximation, the constant N_0 corresponds to a change in scale of the geoid.

The corresponding generalization of the spherical harmonic expansion of the gravity anomaly (6.137) provides another relation between the gravity field and the “gravimetric datum”. Taking (6.101) into account, we obtain for the zero-degree term (6.19):

$$\Delta g_0 = -\frac{T_0}{R} + \frac{2}{R} \delta W = -\frac{G\delta M}{R^2} + \frac{2}{R} \delta W, \quad (6.127)$$

see Hofmann-Wellenhof and Moritz (2005, p. 113 ff.). If N_0 and Δg_0 are determined by (geometric and gravimetric) measurements, (6.126) and (6.127) can be solved for δM and δW .

The *zero-degree undulation* N_0 can be derived from a comparison of gravimetric geoid heights with geoid values derived from the differences of geometric heights referring either to the geoid or to the ellipsoid. The primary data sets to be used for the latter purpose are from satellite altimetry (oceans) and GPS leveling (continents), see Fig. 6.25, Jekeli (1998). The geoid height is obtained from these satellite techniques by the relation

$$N_{\text{sat}} = h_{\text{sat}} - H, \quad (6.128)$$

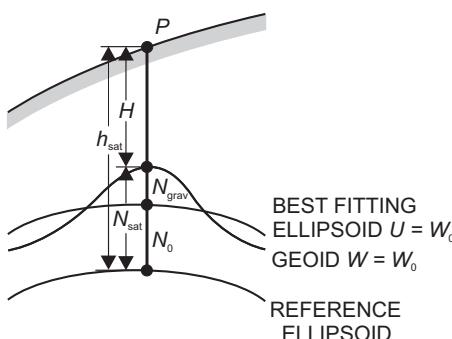


Fig. 6.25: Gravimetric geoid and geodetic reference ellipsoid.

where h_{sat} stands for the ellipsoidal height of the altimeter or the GPS height, and H is the height of the altimeter above the geoid (result of the altimeter measurements) or the orthometric height derived from leveling. The zero-degree term is then obtained by

$$N_0 = N_{\text{sat}} - N_{\text{grav}}, \quad (6.129)$$

where N_{grav} is the geoid height from the gravimetric solution. The determination of $\Delta g_0 = 0$, on the other hand, is still handicapped by deficiencies in the global gravity coverage. Another solution of this problem has been made possible by separating the determination of the geocentric gravitational constant GM . This quantity is known today with high accuracy from space probes and high-orbiting satellites, which allows the potential of the geoid to be determined from (6.126). Current values for the potential of the geoid and the semi-major axis of a best-fitting ellipsoid are given in [4.3].

As we have seen, with the usual assumption of *equality* of mass and potential the gravimetric solution of the boundary-value problem delivers results which refer to a best-fitting ellipsoid, where the equatorial radius ("scale") remains unknown by N_0 . After the determination of N_0 , it could be used to derive the semi-major axis of the best-fitting ellipsoid to which the gravimetric geoid heights refer (i.e. the ellipsoid is changed):

$$a_{\text{grav}} = a_{\text{sat}} + N_0. \quad (6.130)$$

In practice, the adopted ellipsoid parameters are generally part of an international geodetic reference system, cf. [4.3], and consequently kept *unchanged*. In that case, the gravimetrically determined geoid heights have to be corrected in order to refer to the international reference ellipsoid (e.g. the GRS80 ellipsoid):

$$N_{\text{ref}} = N_{\text{sat}} = N_{\text{grav}} + N_0. \quad (6.131)$$

6.6 Global gravity field modeling

Global gravity field modeling is required for large-scale problems including the determination of satellite orbits, inertial navigation, and development of geophysical and geodynamic models. Especially the geoid is required for establishing a global vertical reference system and for deriving sea surface topography. Finally, global models provide the long-wavelength part of the gravity field for local gravity field approximation, cf. [6.7].

Global gravity models are based on spherical harmonic expansions, applicable on all kinds of residual gravity field quantities [6.6.1]. The low and medium frequency part of these series expansions is derived from the analysis of satellite orbits, from satellite-to-satellite tracking and satellite gravity gradiometry [6.6.2]. High degree and order developments are achieved by combining these data with the results of terrestrial gravimetry and satellite altimetry [6.6.3].

6.6.1 Spherical harmonic expansion

Equations (6.3) to (6.5) provide the development of the disturbing potential T into spherical harmonics. A gravity field model thus is represented by the *spherical harmonic coefficients*. The functional relations between T and other relevant gravity field parameters, cf. [6.5.1],

also allow spherical harmonic expansions for the height anomaly, the geoid height, the gravity disturbance, the gravity anomaly, and other residual gravity field quantities. These expansions generally employ *fully normalized spherical harmonics*, cf. [3.3.2], and are valid in the Earth's exterior space and on its surface.

By inserting (6.4) into Bruns' theorem (6.96c), we obtain the spherical harmonic expansion for the *height anomaly*

$$\zeta(r, \vartheta, \lambda) = \frac{GM}{r\gamma} \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda + \Delta \bar{S}_{lm} \sin m\lambda) \bar{P}_{lm}(\cos \vartheta). \quad (6.132)$$

Here, we have introduced the *fully normalized spherical harmonics* indicated by bars, cf. [3.3.2]. From (6.97b), a corresponding expansion follows for the *geoid height*, with $r = R$ (spherical approximation) and $\gamma = \gamma_0$. By introducing (6.120) into (6.9), we may prove that simple (approximate) relation between the geoid height and the quasi-geoid height (height anomaly above the ellipsoid):

$$N(r, \vartheta, \lambda) = \zeta(r, \vartheta, \lambda) + \frac{\Delta g_B}{\bar{\gamma}} H. \quad (6.133)$$

The difference (which is also valid for the corresponding surfaces in outer space) depends on the Bouguer anomaly and on height. For the ocean surface ($H \approx 0$), this approximately leads to $N = \zeta$.

Differentiation of (6.3) with respect to r gives the spherical harmonic expansion (again in fully normalized harmonics) for the *gravity disturbance* (6.99):

$$\delta g(r, \vartheta, \lambda) = -\frac{\partial T}{\partial r} = \frac{1}{r} \sum_{l=2}^{\infty} (l+1) \left(\frac{a}{r}\right)^{l+1} T_l(\vartheta, \lambda). \quad (6.134a)$$

By introducing (6.5) we obtain the explicit formula

$$\begin{aligned} \delta g(r, \vartheta, \lambda) &= \frac{GM}{r^2} \sum_{l=2}^{\infty} (l+1) \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda \\ &\quad + \Delta \bar{S}_{lm} \sin m\lambda) \bar{P}_{lm}(\cos \vartheta). \end{aligned} \quad (6.134b)$$

Inserting (6.3) and (6.134a) into (6.101b) yields the expansion of the *gravity anomaly*

$$\Delta g(r, \vartheta, \lambda) = \frac{1}{r} \sum_{l=2}^{\infty} (l-1) \left(\frac{a}{r}\right)^{l+1} T_l(\vartheta, \lambda). \quad (6.135a)$$

Again substituting T_l from (6.5) gives the explicit solution

$$\begin{aligned} \Delta g(r, \vartheta, \lambda) &= \frac{GM}{r^2} \sum_{l=2}^{\infty} (l-1) \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda \\ &\quad + \Delta \bar{S}_{lm} \sin m\lambda) \bar{P}_{lm}(\cos \vartheta). \end{aligned} \quad (6.135b)$$

By comparing the abbreviated form

$$\Delta g(r, \vartheta, \lambda) = \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^{l+1} \Delta g_l(\vartheta, \lambda), \quad (6.135c)$$

with (6.135a), we obtain the relation between the surface spherical-harmonics of T and Δg :

$$\Delta g_l(\vartheta, \lambda) = \frac{l-1}{r} T_l(\vartheta, \lambda). \quad (6.136)$$

Corresponding developments for other residual gravity field quantities as deflections of the vertical or gravity gradient anomalies can be derived accordingly (e.g., Wenzel,

1985, p. 30 ff.; Wolf, 2007, p. 10 ff.). Due to the scarcity of terrestrial data of these types, these (global) expansions have been of limited relevance. This situation has changed with the availability of altimetry-derived vertical deflections on the oceans (Watts et al., 1984), and of second-order derivatives of T obtained from satellite gravity gradiometry (Rummel et al., 1993). These data sets now contribute significantly to the development of high-resolution geopotential models, cf. [6.6.3], and justify a corresponding representation. Subsequently, we give some examples (spherical approximation).

The spherical harmonic expansions for the *vertical deflection* components based on (6.98) read as follows:

$$\xi(r, \vartheta, \lambda) = \frac{GM}{r^2 \gamma} \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda + \Delta \bar{S}_{lm} \sin m\lambda) \frac{d\bar{P}_{lm}(\cos \vartheta)}{d\vartheta}, \quad (6.137a)$$

$$\eta(r, \vartheta, \lambda) = \frac{GM}{r^2 \gamma \sin \vartheta} \sum_{l=2}^{\infty} \left(\frac{a}{r}\right)^l \sum_{m=0}^l (-m \Delta \bar{C}_{lm} \sin m\lambda + m \Delta \bar{S}_{lm} \cos m\lambda) \bar{P}_{lm}(\cos \vartheta). \quad (6.137b)$$

The *second vertical derivative* $T_{zz} = T_{rr}$ (with z outwards directed coordinate in the local level system) of the disturbing potential, being the most important component of the corresponding Eötvös tensor (3.68), is given by

$$T_{rr}(r, \vartheta, \lambda) = \frac{GM}{r^3} \sum_{l=2}^{\infty} (l+1)(l+2) \left(\frac{a}{r}\right)^l \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda + \Delta \bar{S}_{lm} \sin m\lambda) \bar{P}_{lm}(\cos \vartheta). \quad (6.138)$$

Equations (6.132) to (6.138) permit the harmonic coefficients to be determined from "observations" (geoid heights, gravity anomalies, etc.), by *least-squares adjustment*, cf. [6.6.2].

The coefficients can also be determined by *quadrature* over the observations. Taking the orthogonality relations and the properties of the fully normalized harmonics into account, the inversion of (6.133) and (6.136) yields (Jekeli, 1998):

$$\begin{Bmatrix} \Delta \bar{C}_{lm} \\ \Delta \bar{S}_{lm} \end{Bmatrix} = \frac{1}{4\pi GM} \iint_{\sigma} r \gamma \left(\frac{r}{a}\right)^l N \bar{P}_{lm}(\cos \vartheta) \begin{Bmatrix} \cos m\lambda \\ \sin m\lambda \end{Bmatrix} d\sigma \quad (6.139a)$$

and

$$\begin{Bmatrix} \Delta \bar{C}_{lm} \\ \Delta \bar{S}_{lm} \end{Bmatrix} = \frac{1}{4\pi GM} \iint_{\sigma} \frac{r^2}{l-1} \left(\frac{r}{a}\right)^l \Delta g \bar{P}_{lm}(\cos \vartheta) \begin{Bmatrix} \cos m\lambda \\ \sin m\lambda \end{Bmatrix} d\sigma. \quad (6.139b)$$

The integration is extended over the unit sphere σ . In contrast to least-squares adjustment, the quadrature approach only allows exploitation of one type of data for the determination of the harmonic coefficients.

Terrestrial gravity field data sets (gravity anomalies, altimetric geoid heights) do not cover the Earth homogeneously, and they have a limited spatial resolution. Consequently, *mean* geoid heights and mean gravity anomalies over surface compartments are generally introduced in gravity field modeling, where the surface blocks are bounded by meridians and parallels. The mean values are calculated according to

$$\bar{N} = \frac{1}{\Delta \sigma_{\Delta \sigma}} \iint_{\Delta \sigma} N d\sigma, \quad \Delta \bar{g} = \frac{1}{\Delta \sigma_{\Delta \sigma}} \iint_{\Delta \sigma} \Delta g d\sigma. \quad (6.140)$$

The block size $\Delta\sigma$ depends on the data distribution, cf. [6.6.3]. The maximum gravity field resolution which can be achieved is $\sqrt{\Delta\sigma}$. This corresponds to a maximum degree of the spherical harmonic expansion $l_{\max} = 180^\circ/\text{resolution}^\circ$, cf. [3.3.3]. The introduction of mean values causes a local smoothing of the gravity field, which also leads to smoothed harmonic coefficients. This fact has to be taken into account by damping factors (≤ 1), which depend on the degree and the dimension of the compartment (Katsambalos, 1979).

The truncation of the spherical harmonic expansion at l_{\max} produces an *omission error* due to the neglected part of the gravity field. This “error” can be estimated from a degree variance model, as developed for gravity anomalies, see (6.27). Such models may be based on the covariance function of the gravity anomalies (6.25), but can also be calculated from Laplace’s surface harmonics Δg_l (6.26). In spherical approximation ($r = a = R$), (6.138) gives

$$\Delta g_l = \frac{GM}{R^2} (l-1) \sum_{m=0}^l (\Delta \bar{C}_{lm} \cos m\lambda + \Delta \bar{S}_{lm} \sin m\lambda) \bar{P}_{lm}(\cos \vartheta). \quad (6.141)$$

Inserting (6.141) into (6.26) and evaluating yields the anomaly degree variances as a function of the harmonic coefficients:

$$\sigma_l^2(\Delta g) = \left(\frac{GM}{R^2} \right)^2 (l-1)^2 \sum_{m=0}^l (\Delta \bar{C}_{lm}^2 + \Delta \bar{S}_{lm}^2). \quad (6.142)$$

The functional relations between the gravity field parameters, cf. [6.5.1], also permit the calculation of degree variances for geoid heights, deflections of the vertical, and higher-order derivatives (Tscherning and Rapp, 1974; Tscherning, 1976). As an example, with $\gamma = GM/r^2$, a comparison between (6.132) and (6.136) gives the geoid degree variance

$$\sigma_l^2(N) = \left(\frac{R}{\gamma(l-1)} \right)^2 \sigma_l^2(\Delta g). \quad (6.143)$$

Based on the anomaly degree variance model developed by Tscherning and Rapp (1974), the *omission error* for geoid heights, gravity anomalies, and deflections of the vertical can be estimated on a global scale, Fig. 6.26. For present-day satellite-only solutions (series truncation, e.g., at degree 200), this “error” amounts to about 0.4 m, $300 \mu\text{ms}^{-2}$, and $4''$. A recent development to degree 2160, cf. [6.6.2], is characterized by a geoid omission “error” of only 2 ... 3 cm, while the gravity anomalies and the vertical deflections still have omission parts of about $100 \mu\text{ms}^{-2}$ and $2''$. An expansion to $l = 10\,000$ (representing a spatial resolution of about 2 km) would reduce these errors to less than 1 mm, and $15 \mu\text{ms}^{-2}$ and $0.2''$, respectively.

An early and (at least for the lower spectral part) still useful estimate of the power spectrum of the Earth’s gravitational field based on a global set of gravity anomalies was given by Kaula

(1966), with $\sigma_l^2 = \sum_{m=0}^l (\Delta \bar{C}_{lm}^2 + \Delta \bar{S}_{lm}^2) \approx \frac{160 \times 10^{-12}}{l^3}$ and the average value per degree $\sigma(\Delta \bar{C}_{lm}, \Delta \bar{S}_{lm}) = \sigma_l / \sqrt{2l+1} \approx \pm 10^{-5}/l^2$. By summing up the geoid degree variances of the terms omitted at a spherical harmonic development until l_{\max} , Kaula obtained $\pm 64/l_{\max}$ m as a rough global estimate for the geoid omission error.

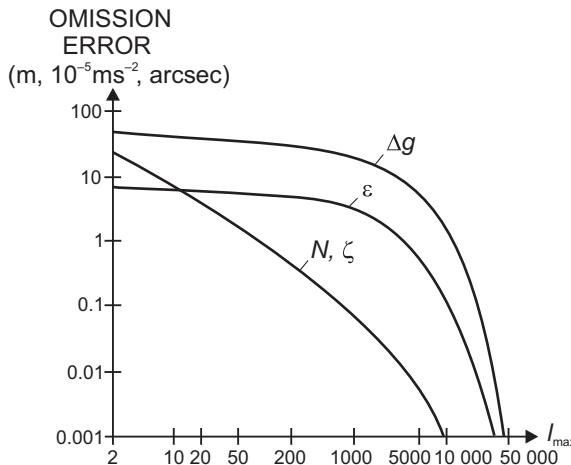


Fig. 6.26: Omission error for geoid heights (height anomalies), vertical deflections, and gravity anomalies (anomaly degree variance model Tscherning and Rapp, 1974).

6.6.2 “Satellite-only” gravity field models

Low-degree gravity field models are required for precise satellite orbit calculation, as needed for positioning, and for long-wave geoid representation necessary, e.g., for modeling sea surface topography, cf. [3.4.2]. Furthermore, these models provide an essential support for high-resolution geoid modeling, cf. [6.6.3], [6.7.1]. The models are based on satellite tracking from ground stations, on satellite-to-satellite tracking, and on satellite gravity gradiometry. These observations can be analyzed with respect to the deviations of the true orbit from a precalculated reference orbit, cf. [5.2.2], where the corresponding models include a spherical harmonic development of the gravitational potential: “*Satellite-only*” models. In some cases, these models have been utilized for the precise orbit determination of a specific satellite, by especially taking into account observations to that satellite (“tailored” models).

The basic equation for the estimation of gravity field parameters from satellite observations is given by (6.33a), which connects the positions of the ground station and the satellite through the observations. With known station coordinates, the satellite orbit remains the unknown quantity, where the Keplerian orbit elements are changed with time through the “perturbing” gravitational potential (5.35); here we neglect other “disturbing” forces. As the potential is modeled by a spherical harmonic expansion, the harmonic coefficients enter as unknowns into the observation equations of satellite geodesy, cf. [6.2.1].

Classical gravity field estimation is based on the influence of the *gravitational field* on the *satellite orbit*, where we may distinguish between secular (linear), long-periodic (few days to months), and short-periodic (periods less than one day or one satellite revolution) perturbations (Kaula, 1966; Schneider, 1992, 1993, 1996; Seeber, 2003). After transformation of the spherical coordinates of the harmonic expansion (3.89) into the Keplerian elements, we obtain the relationship between the orbital perturbations and

the harmonic coefficients by forming the derivatives of the perturbing potential with respect to the elements, and inserting them into (5.35).

Determination of the secular and long-periodic perturbations requires the integration over long arcs (several days). Here, short-periodic perturbations with periods of one or several revolutions are already eliminated. Furthermore, the influence of the tracking station coordinates becomes smaller with longer integration intervals. For the low-degree zonal coefficients, the integration over one satellite revolution yields the following variations for the orbital elements of main interest (Heiskanen and Moritz, 1967, p. 347 ff.):

$$\left. \begin{aligned} \Delta\Omega &= -3\pi \left(\frac{a_e}{\bar{p}} \right)^2 \cos i J_2 + \dots \\ \Delta\omega &= 6\pi \left(\frac{a_e}{\bar{p}} \right)^2 \left(1 - \frac{5}{4} \sin^2 i \right) J_2 + \dots \\ \Delta e &= -3\pi (1 - e^2) \left(\frac{a_e}{\bar{p}} \right)^3 \left(1 - \frac{5}{4} \sin^2 i \right) \sin i \cos \omega J_3 + \dots \\ \Delta i &= 3\pi e \left(\frac{a_e}{\bar{p}} \right)^3 \left(1 - \frac{5}{4} \sin^2 i \right) \cos i \cos \omega J_3 + \dots \end{aligned} \right\}, \quad (6.144)$$

with $\bar{p} = a(1 - e^2)$ and a_e semi-major axis of the Earth ellipsoid.

J_2 and higher even-zonal-coefficients cause *secular* perturbations in Ω and ω . For $i < 90^\circ$, Ω decreases in time (westward regression of the nodal line). The change in ω corresponds to a rotation of the orbital ellipse in the orbital plane (Fig. 5.5). This rotation produces *long-periodic* perturbations in the quantities e and i , as they depend on ω . The even zonals thus can be determined primarily from the perturbations in Ω and ω , while the odd zonals are obtained from i and e . If the perturbations are added to the orbital elements of the initial epoch, one obtains the orbital elements at a specific epoch as a function of the zonal harmonics. As mentioned earlier, the coefficients depend particularly on the inclination but also on the semi-major axis and the eccentricity.

The *tesseral* harmonics are responsible for small-amplitude (a few 100 m) short-periodic perturbations, especially in the elements i , Ω , ω . They can be determined from dense observation sequences over short arcs. Several tesseral terms of higher degree and order can be also determined by *resonance* effects, arising after days to weeks. These effects occur if the ratio of the mean angular velocity of the satellite to the rotational velocity of the Earth is an integer number, which produces an enhancement of perturbation in a repeat orbit.

In order to resolve the gravitational field to a certain degree, satellites in different altitudes and with different inclinations are required at this classical strategy, in addition to a good global distribution of the tracking stations and a sufficiently long observation time. The attenuation of the gravity field with height and the decrease of the harmonic coefficients at higher degrees, together with deficiencies in the geometry of the satellite orbits and the ground stations, limits the resolution of "satellite-only" models based only on *ground-based measurements*. Using several decades of tracking data, a certain limit at gravitational field modeling was reached around the year 2000, with spherical harmonic expansions until degree and order 70 to 90, where the relative uncertainty of the coefficients reached around 100% already at degree 30 to 40.

Dedicated *satellite gravity field missions* with low Earth orbiters (some 100 km altitude) and "in-situ" sensors (satellite-to-satellite tracking, gravity gradiometry) have led to

a significant change of this classical strategy, cf. [5.2.8], Rummel (1979), Reigber et al. (2005). Range, range rate and gradient measurements now enter into the corresponding observation equations for the determination of higher degree and order spherical harmonic coefficients, and tracking data from Earth or from other satellites mainly serve for improving the long-wave part of the gravitational field. Corresponding models have been calculated until degree and order 200 and higher, and agree well until degree and order 120 to 150 (Förste et al., 2009).

While limitations in computational facilities previously forced zonal, tesseral and resonant terms to be computed separately, the harmonic coefficients can now be rigorously determined from all available observations by a least-squares adjustment (for instance by adding the normal equations of different data sets evaluated separately). With present knowledge of the tracking station coordinates, the satellites' orbits, the Earth's rotation parameters, as well as the tidal effects, the corresponding parameters generally can be introduced as known quantities into the adjustment, and variations of the low-degree coefficients with time may be included (Reigber, 1989; Bouman, 1997). Weighting of different data sets and modeling of systematic effects still poses a special problem for these complex adjustments (this is also valid for the "combined" models to be discussed in [6.6.3]). As the accuracy estimates generally are too optimistic, the calculated standard deviations are often "scaled", i.e., enlarged (Lerch et al., 1991).

With respect to the *accuracy* of gravity models (this is valid for any kind of mathematical representation and also for the "combined" solutions!) we have to distinguish between the commission and the omission error. The *commission error* stems from the errors of the data which propagate through the modeling process (e.g., a least-squares adjustment) into the results. The limited spatial resolution of the data and the model derived from them, on the other hand, results in an *omission error* which can be estimated by corresponding models, cf. [6.6.1]. The accuracy (commission error) achieved at the most recent gravity field models (degree and order 200 and higher) is about 0.1 to 0.2 m (geoid) and 20 to 30 μms^{-2} (gravity anomalies), and an accuracy increase to 2 cm resp. 10 μms^{-2} or better is expected as result of the complete GOCE mission (e.g., Ihde et al., 2010).

The first gravity field information from space came from Sputnik I (1957), with the dynamic form factor J_2 (polar flattening); and from Vanguard I (1958), with the coefficient J_3 (unequal flattening at the north and south pole), O'Keefe et al. (1959). The Smithsonian Astrophysical Observatory (SAO) Standard Earth I provided a model complete to degree and order 8 (Lundquist and Veis, 1966). At the end of the twentieth century, *ground-based* "satellite-only" models employed several million records of tracking data. Laser distance and microwave range and range-rate measurements formed the bulk of the data, but optical directions also were included and assisted in stabilizing the solutions. Finally, observations to more than 30 satellites were generally used, with altitudes varying between 800 and 20 000 km and inclinations between 40° and 110°. Among the last solutions of this type we have the NASA Goddard Space Flight Center (GSFC) Earth model GEM T3 (Lerch et al., 1994), the joint (GSFC, University of Texas, Ohio State University, CNES France) gravity model JGM-2S, complete to degree and order 70 (Nerem et al., 1994), and the JGM-3 model (70,70, including DORIS and GPS tracking, Tapley et al., 1996), which was developed primarily for the TOPEX/POSEIDON mission, as well as the GRIM5-S1 (99,95) model (Geoforschungszentrum Potsdam and Groupe de Recherches de Géodésie Spatiale, Toulouse, Gruber et al., 2000).

Among the “satellite-only” gravity models derived during the past ten years from “in situ” (satellite-to-satellite tracking and gravity gradiometry) and tracking data, we have the GRACE-based solutions ITG-GRACE (180,180; Institut für Geodäsie und Geoinformation, Universität Bonn, Mayer-Gürr et al., 2010), GGM (180,180; Center for Space Research, University of Texas, Tapley et al., 2007), JEM01-RL03B (120,120; NASA/JPL, Pasadena), EIGEN – European Improved Gravity model of the Earth by New techniques – (150,150; GRACE and LAGEOS data, GRGS Toulouse and GFZ Potsdam, Reigber et al., 2005; Förste et al., 2008; Flechtner et al., 2010b). Large-scale gravity field variations with time have been found from monthly and weekly GRACE solutions, developed until degree 120 resp. 30 (Cheng and Tapley, 2004), cf. [8.3.5]. The evaluation of the first months of GOCE gravity gradiometry and tracking data led to GOCE-only models up to degree and order 240 (Pail et al., 2011), and to combined solutions with GRACE data, where GRACE dominates until degree and order 100, and GOCE significantly contributes from about 150,150 (Pail et al., 2010b), cf. [5.2.8].

6.6.3 Combined (high resolution) gravity field models

“Satellite-only” models can be improved (with respect to spatial resolution and accuracy) by *combining* them with satellite altimetry and surface gravity (Rapp, 1998). These data are generally available as mean values for compartments (blocks) formed by the grid of geographical coordinates, and ranging, e.g., from $5' \times 5'$ to $1^\circ \times 1^\circ$ dimensions. Again, the spherical harmonic expansion is employed for modeling, where degree and order of the development now depend on the spatial resolution of the altimetric and gravimetric data. A combination solution thus contains the following “observations”: the harmonic coefficients of a “satellite-only” model with the full error covariance matrix, mean free-air anomalies from terrestrial gravimetry on land and sea, and mean geoid heights derived from satellite altimetry, both with an appropriate error model. The corresponding observation equations (i.e., the relation of gravity anomalies and geoid heights to the spherical harmonic coefficients) are given by (6.136) and (6.133), where the reduction of sea surface topography from the altimeter measurements is presupposed. Some solutions also use gravity anomalies instead of altimetric geoid heights, with a transformation based either on an integral formula, cf. [6.7.1], or on least-squares collocation, cf. [6.8].

Point free-air gravity anomalies (or mean gravity anomalies for some countries) are collected and kept at a few global *gravity data bases* (U.S. National Geospatial-Intelligence Agency (NGA), Bureau Gravimetrique International, Toulouse, France), see Fig. 6.27. The accuracy of point anomalies derived from land, sea and airborne gravimetry varies between 5 and $50 \mu\text{ms}^{-2}$, cf. [5.4.4]. In order to avoid long-wave systematic errors in gravity field modeling, the anomalies have to refer to the same gravity (IGSN71), horizontal (ITRF, GRS80) and vertical reference systems, where the global vertical datum poses a special problem, cf. [3.4.3], Heck (1990). *Mean anomalies* can be derived, e.g., by least-squares prediction, where Bouguer anomalies may be used as intermediate gravity field quantities, cf. [6.5.3]. On the continents, mean gravity anomalies are now available for most regions, but with different spatial resolution (from $1' \times 1'$ to $30' \times 30'$) and accuracy (varying between about 20 and $200 \mu\text{ms}^{-2}$). Larger gaps still exist in parts of South America, Africa, Asia and especially in Antarctica, and will be filled by airborne gravimetry, cf. [5.4.4]. The oceans, on the other hand, are only sparsely covered by sea gravimetry tracks of rather heterogeneous accuracy, and this situation will in future change only slowly, see [4.4] and Fig. 6.27, Kenyon (1998). As a consequence, high-resolution gravity field

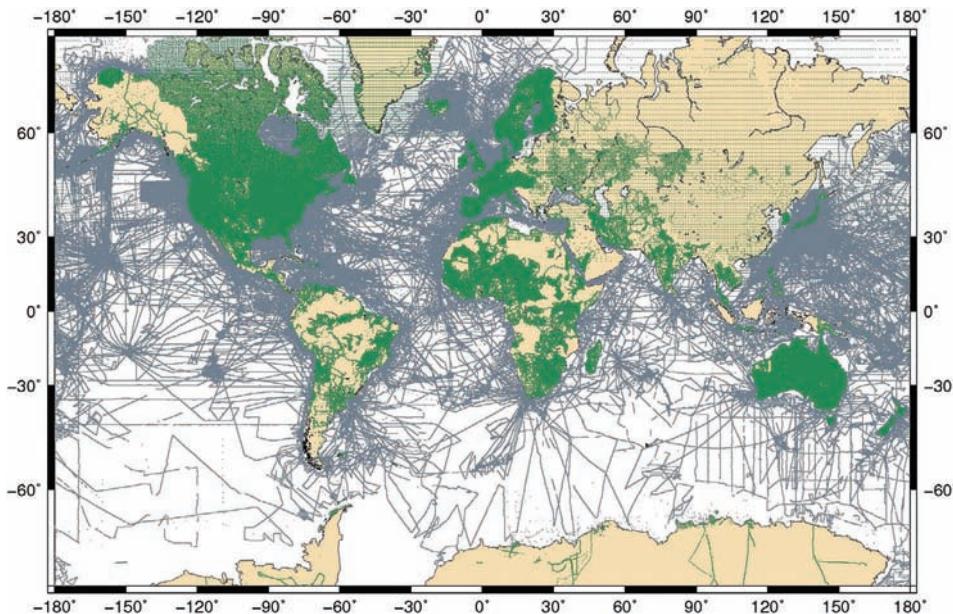


Fig. 6.27: Global distribution of terrestrial gravity data, courtesy S. Bonvalot, Bureau Gravimétrique International.

data for the oceans are now generally derived from satellite altimetry, which covers the oceans more homogeneously (see below).

More than three decades of satellite altimetry have provided a large amount of distance measurements between the altimeter satellites and the sea surface, cf. [5.2.7]. With proper reduction of sea surface topography (oceanographic model), accurate orbit determination (tracking), altimeter calibration and adjustment of the track crossover discrepancies, mean *altimetric geoid heights* have been derived for the ocean areas. Data sets of high accuracy and resolution (e.g. $2' \times 2'$ or $5' \times 5'$) are available especially from the GEOSAT and ERS-1 geodetic missions (Sandwell and Smith, 2009), which cover the oceans between $\pm 72^\circ$ and 82° latitude, respectively, with an equatorial track spacing of 4 and 8 km. After reducing the dynamic ocean topography from the altimetric ground data, along-track differentiation provides deflections of the vertical. Double differentiation delivers gravity gradients, which can be used for the evaluation of the GOCE mission results, cf. [5.2.8]. Mean altimetric *gravity anomalies* can be calculated by inversion from the mean geoid heights, cf. [6.7.1]. Recent solutions exploit retracked satellite altimetry and the results of more recent altimetry missions, and provides the global marine gravity field with $1' \times 1'$ spatial resolution and an average accuracy of 20 to 50 μms^{-2} (Andersen et al., 2010).

By combining the mean anomalies from surface gravimetry and altimetry, only a few percent of the Earth's surface remain uncovered. These gaps can be filled either by isostatic anomalies calculated from a topographic-isostatic model (Pavlis and Rapp, 1990), or just bridged by the satellite-only model.

High-degree geopotential models are calculated either by least-squares adjustment or by quadrature methods (Rapp, 1998).

A *least-squares adjustment*, in principle, would utilize all available data in order to determine the full set of potential coefficients (130 321 coefficients at $l,m = 360,360$; 3.67 million coefficients at 2160,2160), together with the error variance/covariance matrix. As computational limitations still prevent a rigorous adjustment of these quantities, alternative solutions have been developed. At these strategies, for instance, a complete data coverage on a grid and homogeneous and uncorrelated errors are presupposed for the high-resolution data sets. Special arrangements of the normal equation matrix (block-diagonal technique) then allow an efficient computation by iterative procedures (Wenzel, 1985; Pavlis et al., 1996). Subsequently, the normal equations of these data sets are added to the normal equations of the satellite-only model.

The *quadrature* approach employs the integration over the gravity anomalies according to (6.139b). As a global and homogeneous data set is required at this strategy, altimetric geoid heights have to be transformed into gravity anomalies (see above) and data gaps have to be filled by interpolation or model values. After the calculation of the harmonic coefficients from the gravity anomalies, they are again combined by adjustment with the coefficients of a satellite-only gravity model (e.g., Rapp and Pavlis, 1990).

Early spherical harmonic expansions based on terrestrial gravity data are due to Jeffreys (1941–1943), Zhongolovich (1952), and Uotila (1962). Sparse data coverage limited these expansions to the low-degree harmonics. Kaula (1959) introduced a constraint from satellite orbit analysis in order to develop a 8,8 geoid model. Among the geopotential models, developed before the advent of dedicated gravity field satellite missions are the Ohio State University (OSU) model OSU91 (combination of the satellite-only GEM-T2 (36,36) model with $1^\circ \times 1^\circ$ and $30^\circ \times 30^\circ$ gravity anomalies from surface gravimetry and altimetry, quadrature method, Rapp et al., 1991), and the Geoforschungszentrum Potsdam (GFZ) model GFZ96 (combination of the GRIM-4 (60,60/72,72) models with terrestrial anomalies and ERS-1 geoid heights, least-squares iteration, Gruber et al., 1997), both complete to degree and order 360. A 1800,1800 model GPM98 was developed by Wenzel (1999) by combining EGM96 with $5' \times 5'$ mean gravity anomalies available for about 75% of the Earth's surface. The inclusion of GRACE and also GOCE data significantly improves the quality of combined gravitational models. We mention the GGM02C (200, 200) model (Tapley et al., 2005) as a combination of a GRACE-only model with EGM96 (see below), and the EIGEN-5C (360, 360) model, as a combination of the satellite-only model EIGEN-5S with $0.5^\circ \times 0.5^\circ$ gravimetry and altimetry surface data (Förste et al., 2008). The EIGEN-6C (1420,1420) model combines LAGEOS-, GRACE- and GOCE-data (EIGEN-6S, 240,240) and gravity anomalies from altimetry (oceans) and the EGM2008 model (land), the solution includes time variable (drift, annual and semi-annual) spherical harmonic coefficients up to degree and order 50 (Förste et al., 2011).

Tab. 6.1 presents the low degree and order harmonic coefficients and a selection of higher degree values as derived from the recent combination solution EGM2008 (see below). The anomaly degree variances approximately follow Kaula's rule, with relative errors reaching about 50% around degree 700, and 100% around degree 1800 (Arabelos and Tscherning, 2010).

Extended sets of satellite tracking data, terrestrial gravity anomalies and ocean-wide satellite altimetry have been utilized in the NASA/GSFC and NIMA joint geopotential (360,360) model EGM96 (Lemoine et al., 1998). Up to degree and order 359, the model parameters

Tab. 6.1. Samples of fully normalized spherical harmonic coefficients ($\times 10^6$), EGM2008 Global Gravitational Model (Pavlis et al., 2008)

l	m	\bar{C}_{lm}	\bar{S}_{lm}
2	0	-484.169 317	—
2	1	-0.000 207	0.001 384
2	2	2.439 384	-1.400 274
3	0	0.957 161	—
3	1	2.030 462	0.248 200
3	2	0.904 788	-0.619 005
3	3	0.721 322	1.414 349
4	0	0.539 966	—
4	1	-0.536 157	-0.473 567
4	2	0.350 502	0.662 480
4	3	0.990 857	-0.200 957
4	4	-0.188 520	0.308 804
10	0	0.053 330	—
20	0	0.021 559	—
50	0	-0.004 844	—
100	0	0.002 355	—
200	0	-0.000 161	—
500	0	-0.000 029	—
1000	0	-0.000 007	—
1500	0	0.000 001	—
2000	0	0.000 001	—

have been derived from a block-diagonal least-squares adjustment, and the degree 360 coefficients were calculated by quadrature. Geoid accuracy estimates are between 0.5 m for the oceans and 1 m for land areas. The NGA (U.S.A. National Geospatial-Intelligence Agency) Earth Gravitational Model EGM2008 (Pavlis et al., 2008) is based upon the ITG-GRACE03S gravitational model (180,180) and a global gravity anomaly database of $5' \times 5'$ resolution. The anomalies have been derived from terrestrial gravity measurements on land (16% still not covered with high quality data) and satellite altimetry on the oceans, where a dynamic ocean topography model (degree and order 180) is also provided. EGM2008 is complete to degree and order 2159 (spherical harmonic coefficients given for the “zero-tide” and the “tide-free” system, cf. [3.4.1]), which corresponds to a $5'$ spatial resolution. The “scaling” parameters have the numerical values $GM = 398\,600.4415 \times 10^9 \text{ m}^3\text{s}^{-2}$ and $a = 6\,378\,136.3 \text{ m}$, and a version related to WGS84 is also available, cf. [5.2.5]. The quality of the $5' \times 5'$ geoid solution has been estimated by error propagation and by independent comparisons (GPS/leveling, astronomic deflections of the vertical), Förste et al. (2009). The accuracy obtained varies especially between land and ocean areas and amounts to about 0.1 m (geoid) resp. $1'' \dots 2''$ (deflection of the vertical) for the continents, and 0.06 m resp. $0.4''$ for the oceans. The omission error for the geoid is a few cm globally, but may reach up to 0.1 m in mountainous areas (Jekeli et al., 2009).

The long-wave structures of the *free-air anomalies* and the *geoid*, as derived from a recent geopotential model, are shown in Figs. 6.28 and 6.29. The free-air anomalies vary rather irregularly about zero, but a correlation with extended mountain chains

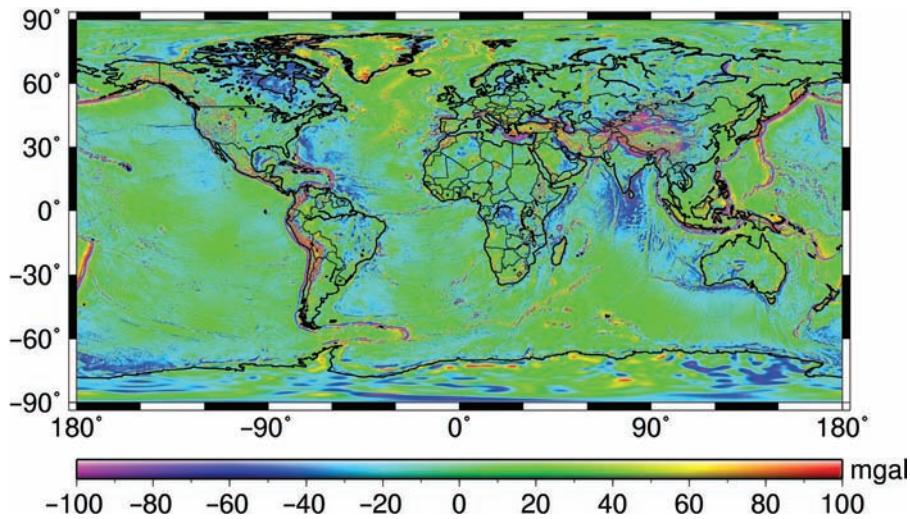


Fig. 6.28: EGM2008 gravity anomalies (Pavlis et al., 2008), (<http://Earth-info.nga.mil/GandG/wgs84/gravitymod/egm2008/>).

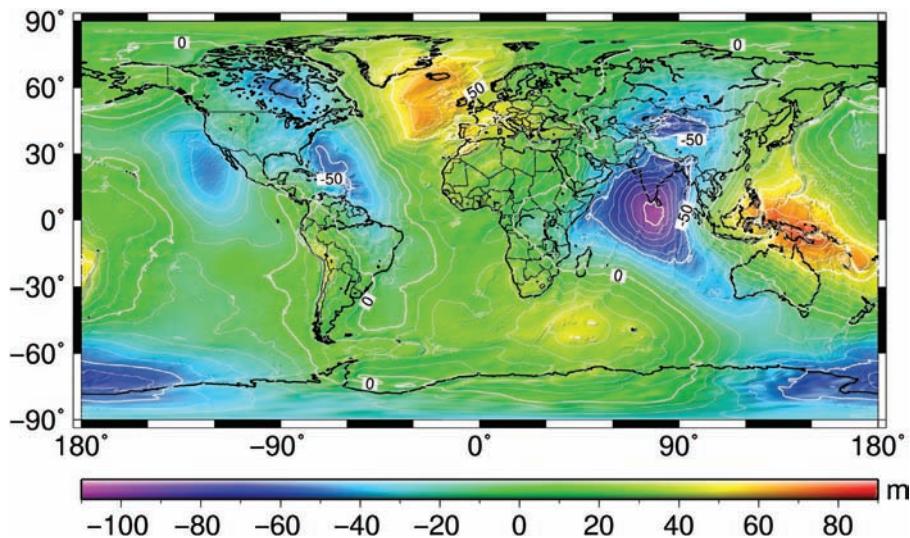


Fig. 6.29: EGM2008 geoid heights, contour line interval 10 m (Pavlis et al., 2008), (<http://Earth-info.nga.mil/GandG/wgs84/gravitymod/egm2008/>).

(Cordilleras, Himalaya) can be recognized. The principal features of the geoid include the maxima near New Guinea (+80 m), in the North Atlantic, the southwestern Indian Ocean, and in the Andes, as well as the minima at Sri Lanka (-105 m), in Antarctica, to the west of California, and near Puerto Rico.

6.7 Local gravity field modeling

Local gravity field modeling is especially useful for the determination of geoid/quasi-geoid heights or deflections of the vertical, with high accuracy and spatial resolution, as for instance needed for the reduction of GPS heights, cf. [6.4.3]. This strategy presupposes the availability of high resolution gravity field data in and around the area concerned. The spherical harmonic development of the gravity field, described in [6.6], was and is (not yet) capable of delivering such a local solution. Integral formulas, on the other hand, allow a pointwise calculation of gravity field quantities for the area under investigation, and thus provide the possibility of an arbitrarily high gravity field resolution which depends only on data coverage and quality (Sansò and Rummel, 1997).

Utilizing gravity anomalies as the primary data set, classical solutions aim at the determination of geoid heights and deflections of the vertical [6.7.1]. Reduction to the geoid is avoided in the calculation of the corresponding surface quantities, where the quasigeoid plays a special role [6.7.2]. Once the gravity field is known on the geoid or on the physical surface of the Earth, upward continuation provides gravity field quantities in space [6.7.3]. Astronomically determined deflections of the vertical furnish differences of geoid or quasigeoid heights and may locally support or substitute gravimetric solutions [6.7.4].

An alternative approach to the integral formulas is least-squares collocation which will be discussed in [6.8].

6.7.1 Gravimetric geoid heights and deflections of the vertical: integral formulas

The series expansion (6.4) for the disturbing potential T can also be represented by a surface integral. By inserting (6.138) into (6.3), this expansion reads

$$T(r, \vartheta, \lambda) = \sum_{l=2}^{\infty} \frac{r}{l-1} \left(\frac{a}{r}\right)^{l+1} \Delta g_l(\vartheta, \lambda). \quad (6.145)$$

As known from potential theory, the surface spherical harmonics Δg_l can be derived by inversion of (6.137), as a surface integral of the gravity anomalies over the unit sphere σ :

$$\Delta g_l = \frac{2l+1}{4\pi} \iint_{\sigma} \Delta g P_l(\cos \psi) d\sigma, \quad (6.146)$$

where $P_l(\cos \psi)$ are the Legendre polynomials. Inserting into (6.145) yields the *disturbing potential* on the *geoid* in spherical approximation ($r = R = a$)

$$T(\vartheta, \lambda) = \frac{R}{4\pi} \iint_{\sigma} S(\psi) \Delta g d\sigma, \quad (6.147)$$

where the integral kernel (Stokes' function)

$$S(\psi) = \sum_{l=2}^{\infty} \frac{2l+1}{l-1} P_l(\cos \psi) \quad (6.148a)$$

can be expressed in closed form:

$$S(\psi) = \frac{1}{\sin \frac{\psi}{2}} + 1 - 5 \cos \psi - 6 \sin \frac{\psi}{2} - 3 \cos \psi \ln \left(\sin \frac{\psi}{2} + \sin^2 \frac{\psi}{2} \right). \quad (6.148b)$$

This integral formula has been derived by Stokes (1849); it is called *Stokes' formula*.

By inserting (6.147) into Bruns' theorem (6.97b), we obtain the *geoid height*

$$N = \frac{R}{4\pi\gamma_m} \iint_{\sigma} S(\psi) \Delta g d\sigma, \quad (6.149)$$

where γ_m is a mean gravity value over the Earth. Stokes' formula can also be derived as a solution of the integral equation (6.93), if applied to the geoid. If a geoid accuracy of the cm-order of magnitude is required, *ellipsoidal* corrections have to be applied to (6.149), Sünkel (1997). We also remember the conditions of mass and potential equality between the geoid and the reference ellipsoid, inherent in Stokes' formula, cf. (6.126).

Stokes' function $S(\psi)$ acts as a weighting function on the gravity anomalies. It depends on the spherical distance ψ between the point of computation and the surface element $d\sigma$ with the gravity anomaly Δg . $S(\psi)$ decreases with ψ until a first zero value at $\psi = 39^\circ$, and then oscillates with large values and another zero value at 117° until $\psi = 180^\circ$ (Fig. 6.30). The *neighborhood* of the computation point requires particular attention, as $S(\psi)$ becomes infinite at $\psi = 0^\circ$. The contribution of the innermost zone around the point of computation can be estimated in planar approximation (e.g., with a radius $s_i = 5$ km), by expanding Δg in a Taylor series and performing integration term by term. To a first approximation, the effect of the *inner zone* on the geoid height depends on the gravity anomaly in the computation point:

$$N_i = \frac{s_i}{\gamma_m} \Delta g_p + \dots \quad (6.150)$$

The components of the *deflection of the vertical* are obtained by differentiating the disturbing potential T in north-south and east-west direction (6.98). This can be realized by expressing ψ in (6.147) in spherical coordinates of the computation point and the source point, the corresponding formulas of spherical trigonometry are taken from the spherical polar triangle, see Fig. 2.14. After differentiation with respect to latitude and longitude and subsequent resubstitution of ψ we obtain

$$\begin{Bmatrix} \xi \\ \eta \end{Bmatrix}_0 = \frac{1}{4\pi\gamma_m} \iint_{\sigma} \frac{dS(\psi)}{d\psi} \Delta g \begin{Bmatrix} \cos \alpha \\ \sin \alpha \end{Bmatrix} d\sigma, \quad (6.151)$$

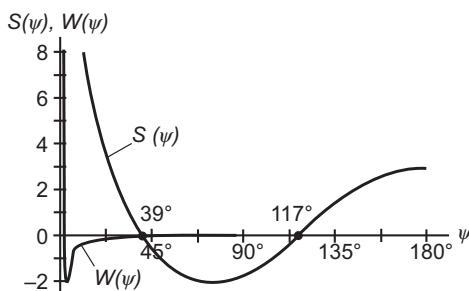


Fig. 6.30: Original and modified Stokes' function, modification according to (6.163).

where α is the azimuth of the great circle from the computation point to the source point. Equation (6.151) was derived by Vening-Meinesz (1928). The *Vening-Meinesz function*

$$\frac{dS}{d\psi} = -\frac{\cos(\frac{\psi}{2})}{2\sin^2(\frac{\psi}{2})} + 8\sin\psi - 6\cos(\frac{\psi}{2}) - 3\frac{1 - \sin(\frac{\psi}{2})}{\sin\psi} + 3\sin\psi \ln\left[\sin\left(\frac{\psi}{2}\right) + \sin^2\left(\frac{\psi}{2}\right)\right]. \quad (6.152)$$

is infinite at $\psi = 0^\circ$ and then decreases rapidly, attaining only small values after $\psi = 50^\circ$ to 60° (Fig. 6.31). The contribution of the *innermost zone* depends primarily on the horizontal gradient of the gravity anomalies:

$$\begin{Bmatrix} \xi \\ \eta \end{Bmatrix}_i = -\frac{s_i}{2\gamma_m} \begin{Bmatrix} \partial(\Delta g)/\partial x \\ \partial(\Delta g)/\partial y \end{Bmatrix}_p + \dots \quad (6.153)$$

Stokes' and Vening-Meinesz' formulas allow a *pointwise* calculation of the geoid height and the deflection of the vertical, by integrating the gravity anomalies given on the surface of the geoid, cf. [6.5.3]. The properties of Stokes' function require high resolution gravity data all over the Earth, while the effect of remote zones is small in the calculation of vertical deflections and can be estimated by low-degree global gravity field models. The inner zone may contribute some cm to the geoid height, this is well accounted for at gravity station distances of 1 to 5 km, depending mainly on the roughness of topography. The effect of the inner zone on the deflection of the vertical can reach several arcsec, especially in the mountains. A dense gravity survey and/or the calculation of the effect of topography is needed in order to achieve an accuracy better than 1 arcsec.

In practice, the integrals (6.149) and (6.151) are solved by a summation of finite surface elements. For this purpose, either a set of gridded point anomalies is formed from the observed data, using e.g., least-squares prediction or spline interpolation, or mean values over surface blocks delineated by meridians and parallels are calculated, cf. [6.6.3]. The latter case also requires the integration of the Stokes' or Vening-Meinesz' function over the block. After gridding, a very efficient solution is obtained in the spectral domain using Fast Fourier Transform (FFT) techniques. The convolution required in (6.149) and (6.151) then becomes a simple multiplication, and the results are easily retransformed to the space domain by the inverse FFT (Schwarz et al., 1990; Haagmans et al., 1993).

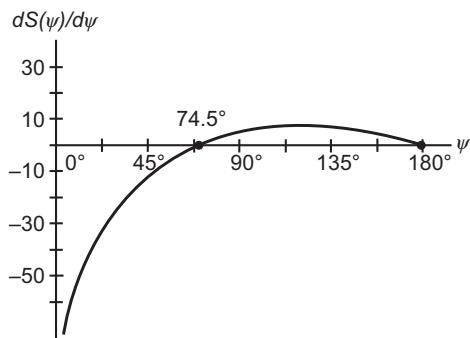


Fig. 6.31: Vening-Meinesz function.

As discussed in [6.6.3], *satellite altimetry* provides a high resolution data set of geoid heights for the oceans, which now significantly contributes to gravity field modeling. Computation strategies either directly use the altimetrically derived geoid heights or transform them into gravity anomalies. The transformation procedure is based on least-squares collocation, cf. [6.8.2], or on a surface integral over the geoid heights.

The surface integral for calculating gravity anomalies from geoid heights respectively from the disturbing potential is obtained by the inversion of Stokes' formula (6.149). Here we remember again that we restrict these developments to the boundary case of the Earth's surface, with a spherical approximation ($r = R$); the extension to space will be discussed in [6.7.3]. We start from the spherical harmonic expansion of (6.137) and the relation between the surface spherical harmonics of Δg and T (6.138), and take the surface integral for the calculation of surface spherical harmonics into account:

$$T_l = \frac{2l+1}{4\pi} \iint_{\sigma} T(\vartheta, \lambda) P_l(\cos \psi) d\sigma \quad (6.154)$$

(see the corresponding equation (6.146) for gravity anomalies). We thus obtain a first version of the *inverse Stokes' formula* (Molodenskii et al., 1962, p. 50):

$$\Delta g(\vartheta, \lambda) = \frac{1}{4\pi R} \iint_{\sigma} \hat{Z}(\psi) T(\vartheta', \lambda') d\sigma, \quad (6.155a)$$

with the (only distance dependent) kernel function:

$$\hat{Z}(\psi) = \sum_{l=0}^{\infty} (l-1)(2l+1) P_l(\cos \psi). \quad (6.155b)$$

For numerical calculations (6.155) generally is transformed into (Jekeli, 2009, p. 25 ff.):

$$\Delta g(\vartheta, \lambda) = -\frac{T(\vartheta, \lambda)}{R} + \frac{1}{4\pi R} \iint_{\sigma} (T(\vartheta', \lambda') - T(\vartheta, \lambda)) Z(\psi) d\sigma. \quad (6.156a)$$

The *inverse Stokes' function* now can be expressed also in a simple closed form:

$$Z(\psi) = \sum_{l=1}^{\infty} l(2l+1) P_l(\cos \psi) = -\frac{1}{4\sin^3 \frac{\psi}{2}}. \quad (6.156b)$$

The effect of the inner zone again has to be considered separately. It depends on the vertical gradient of the gravity anomaly (Lelgemann, 1976):

$$\Delta g_i = \frac{s_i}{4} \left(\frac{\partial (\Delta g)}{\partial r} \right)_P, \quad (6.157)$$

where s_i is the radius of the inner zone. Due to the properties of the integral kernel, the influence of the more remote zones on Δg decreases rapidly. Hence, in contrast to Stokes's integral, the integration of the inverse Stokes' integral can be restricted to a radius of a few degrees.

Satellite-based positioning (GNSS), provides ellipsoidal heights for points on the Earth's surface in a continuously increasing manner. This allows to calculate the gravity disturbance δg as an "observed" residual gravity field quantity, cf. [6.1.2], and to solve the gravimetric boundary value problem on a geometrically known boundary surface, cf. [6.5.1], (Hotine, 1969, p. 317 ff.; Koch and Pope, 1972). Exploiting the small difference between

Δg and δg , see (6.134), (6.135), we obtain *Hotine's formula* for the calculation of geoid heights from gravity disturbances (Hofmann-Wellenhof and Moritz, 2005, p. 115 ff.):

$$N = \frac{R}{4\pi\gamma_m} \iint_{\sigma} H(\psi) \delta g \, d\sigma \quad (6.158)$$

with the *Hotine function*

$$H(\psi) = \sum_{l=0}^{\infty} \frac{2l+1}{l+1} P_l(\cos \psi) = \frac{1}{\sin \frac{\psi}{2}} - \ln \left(1 + \frac{1}{\sin \frac{\psi}{2}} \right). \quad (6.159)$$

In the future, a corresponding strategy may obtain greater relevance for gravity field modeling.

Purely gravimetric or gravimetric/altimetric calculations of geoid heights and deflections of the vertical suffer from the data gaps at the polar caps, in some continental areas, and at coastal zones. They are also hampered by long-wave systematic data errors and by inhomogeneous spatial resolution and accuracy of the gravity data. As global geopotential models today provide the long-wave part of the gravity field with high accuracy, cf. [6.6.3], and gravity anomalies with station distances down to 1 to 5 km are available in many regions, *combined solutions* based on integral formulas have been developed for local solutions covering the area well surveyed by terrestrial gravimetry. In addition, data smoothing techniques are employed on the gravity anomalies, considering the gravimetric terrain effect which can be calculated from digital terrain models, cf. [6.5.2].

Combination solutions apply the *remove-restore technique* (Forsberg and Tscherning, 1981; Denker et al., 1986), which includes the following steps:

- Reduction of the gravity anomalies Δg by the anomaly part of the global model Δg_M (long wavelengths).
- Smoothing of the anomalies by some kind of terrain reduction Δg_T (short wavelengths), see below.
- Gridding of the residual gravity anomalies

$$\Delta g_{\text{res}} = \Delta g - \Delta g_M - \Delta g_T \quad (6.160)$$

- Application of Stokes' formula (6.149) on the residual gravity anomalies, resulting in residual geoid heights N_{res} .
- Restoration of the effects of the global model and the terrain to the residual geoid heights:

$$N = N_{\text{res}} + N_M + N_T \quad (6.161)$$

The remove-restore technique can also be applied on the deflections of the vertical or any other gravity field quantity. It is used successfully also with least-squares collocation.

Since the residual gravity anomalies neither contain the long nor the short-wave parts of the gravity field, they are considerably smaller and smoother than the original data, and they possess (approximately) homogeneity and isotropy properties, cf. [6.1.3]. With global spherical harmonic models of high degree and order, the integration area can be restricted to the region with dense data coverage and a narrow edge zone (spherical distance of a few degrees) around it. As only a small radius of integration is required at

this remove-restore technique, a *planar approximation of Stokes'* formula is permitted. Stokes' function then reduces to

$$S(\psi) \approx \frac{1}{\sin\left(\frac{\psi}{2}\right)} \approx \frac{2}{\psi} \approx 2 \frac{R}{l_0}, \quad (6.162a)$$

with $l_0 = \sqrt{(x - x_p)^2 + (y - y_p)^2}$ and x_p, y_p plane coordinates of the computation point. The spherical surface element is replaced by the planar element

$$dS = R^2 d\sigma. \quad (6.162b)$$

Inserting (6.162a) and (6.162b) into (6.149) yields *Stokes' formula in planar approximation*

$$N = \frac{1}{2\pi\gamma_m} \iint_S \frac{\Delta g}{l_0} dS, \quad (6.162c)$$

which is very convenient to evaluate by FFT techniques.

Different strategies can be pursued for the application of *terrain reductions* (Forsberg and Tscherning, 1997).

When *Helmers' condensation method* is employed, terrain-corrected Bouguer anomalies may be first used for gridding, cf. [6.5.3]. After restoring the Bouguer plate term ("condensation"), Faye anomalies reduced by the effect of the global model serve for the calculation of residual geoid heights.

With the *residual terrain correction*, only the high-frequency part of topography is taken into account in the remove-restore process, as the long-wave part has been subtracted already with the global model (Forsberg and Tscherning, 1981). It is calculated from a residual terrain model (RTM) which refers to a reference topography, as provided by a global topographic model (spherical harmonic expansion of the same degree and order as the geopotential model), or the moving average over mean heights of, e.g., $15' \times 15'$ or $30' \times 30'$ blocks, Fig. 6.32. The result of this procedure is a balanced set of positive and negative anomalies, where the prism method is used generally for the calculation, cf. [6.5.2].

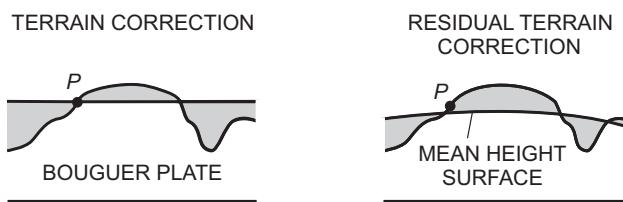


Fig. 6.32: Bouguer plate with terrain correction and residual terrain correction.

If applied to Stokes' formula, the remove-restore technique implies that the complete spectrum of the geoid heights is computed from the gravity anomalies in the integration area, substituted by the values of the global model only outside this region. In the case of long-wave discrepancies between the terrestrial gravity data and the global model, this leads to a distortion of the long wavelengths of the geoid. This problem is avoided by *least-squares spectral combination* (Sjöberg, 1979; Wenzel, 1982). Here, the long-wavelengths spectral components of the global model and of the gravity anomalies are combined within the area of integration, using least-squares adjustment with spectral weights

$$w_i = \frac{\sigma_i^2(\varepsilon_M)}{\sigma_i^2(\varepsilon_M) + \sigma_i^2(\varepsilon\Delta g)}. \quad (6.163a)$$

The error degree variances $\sigma_i^2(\mathcal{E}_M)$ of the potential coefficients of the global model are estimated in analogy to (6.143), and the error degree variances of the terrestrial anomalies $\sigma_i^2(\mathcal{E}_{\Delta g})$ are derived from an error covariance function, in analogy to (6.25). Stokes' function (6.148a) is extended now by the spectral weights to form an optimum integral kernel

$$W(\psi) = \sum_{l=2}^{\infty} \frac{2l+1}{l-1} w_l P_l(\cos \psi). \quad (6.163b)$$

This function is no longer infinite at $\psi = 0^\circ$, and it converges to zero more rapidly than the original Stokes' function, see Fig. 6.30.

Early gravimetric geoid calculations with Stokes' formula are due to *Hirvonen* (1934) and *Tanni* (1948). Based on isostatic anomalies, the "Columbus Geoid" was calculated at the Ohio State University (Heiskanen, 1957). A combination of a low-degree satellite model (Goddard GEM-6, degree and order 16) with $1^\circ \times 1^\circ$ free-air anomalies (integration radius 10°) was presented by Marsh and Vincent (1974). Among the recent regional solutions is the $1' \times 1'$ -gravimetric geoid model USGG2009 for the *United States of America* and its territories (Fig. 6.33), following the previous $2' \times 2'$ -geoid, which utilized the EGM96 model and Faye anomalies (Smith and Roman, 2001). USGG2009 is based on a $1' \times 1'$ -grid of free-anomalies, altimetry-derived anomalies, the SRTM 3' digital elevation model for topographic reductions, and the global geopotential model EGM2008 as a reference model, cf. [6.6.3]. The surface gravity data have been reduced by the long-wavelength part (global model) and the effect of topography (residual terrain model), and then transferred to the ellipsoid by harmonic downward continuation. A modified Stokes' kernel was applied for the integration of the residual anomalies, which retained all signal below degree 120 from EGM2008. USGG2009 refers to the NAD83 ellipsoid, cf. [7.1], and is centered in the ITRF reference frame. Presently it is the best approximation of mean sea level, with an accuracy of about 5 cm (Roman et al., 2009). Least-squares spectral combination has been also applied in the calculation of a European *quasigeoid*, which will be discussed in [6.7.2].

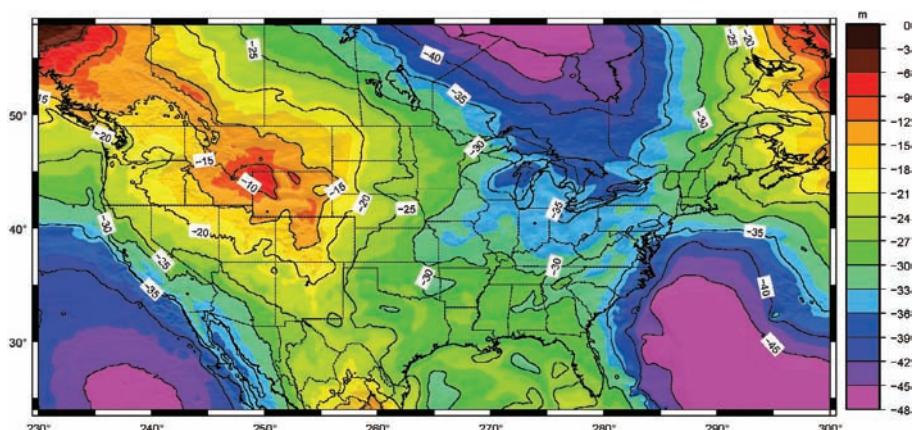


Fig. 6.33: Gravimetric Geoid USGG2009 of the U.S.A., contour line interval 5 m, courtesy National Geodetic Survey/NOAA (<http://www.ngs.noaa.gov/GEOID/USGG2009/>).

6.7.2 Gravimetric height anomalies and surface deflections of the vertical

The geodetic boundary-value problem for the *physical* surface of the Earth has been formulated by *M.S Molodensky*, through the integral equation (6.92), Molodenskii et al. (1962). By introducing the telluroid Σ as an approximation to the Earth's surface, an integral equation for the disturbing potential was obtained (6.93). In contrast to the derivative $\partial T/\partial n$ [n is the normal to the level surface, which entered into the fundamental relation (6.101)], the derivative $\partial T/\partial n_\Sigma$ (n_Σ normal to the telluroid) is now required. It not only depends on the gravity anomaly but also on the deflection of the vertical and the inclination of the terrain. Evaluating $\partial T/\partial n_\Sigma$ from (6.101) and inserting into (6.93) yields a linear integral equation of the second kind for T (Heiskanen and Moritz, 1967, p. 299 ff.)

$$\left. \begin{aligned} & T - \frac{1}{2\pi} \iint_{\Sigma} \left(\frac{\partial}{\partial n_\Sigma} \left(\frac{1}{l} \right) - \frac{1}{l} \frac{\partial \gamma}{\partial h} \frac{\cos \beta}{l} \right) T d\Sigma \\ & = \frac{1}{2\pi} \iint_{\Sigma} \frac{1}{l} \left(\Delta g - \gamma (\xi \tan \beta_x + \eta \tan \beta_y) \cos \beta \right) d\Sigma \end{aligned} \right\}, \quad (6.164)$$

with β_x, β_y being the angles of terrain inclination in NS and EW-direction, β the angle of maximum inclination, and ξ, η the vertical deflection components; l is the distance between the source point and the computation point. We remember that Δg represents the free-air anomaly defined on the Earth's surface according to Molodensky (6.15).

A simpler integral equation can be derived by expressing T as the potential of an infinitely thin *surface layer* condensed on the telluroid. With the surface density μ (6.114), the law of gravitation (3.10) yields

$$T = G \iint_{\Sigma} \frac{\mu}{l} d\Sigma. \quad (6.165)$$

As the potential of a surface layer is harmonic outside the surface, Laplace's equation is fulfilled, and we may introduce (6.165) and its normal derivative into the boundary condition (6.101). This strategy again results in a linear integral equation which now only depends on Δg and on the terrain inclination. It can be solved by successive approximation, leading to a series expansion for T . In spherical approximation (σ unit sphere, R Earth's radius), and limiting the series to its first two terms, the *disturbing potential* then is given by (Moritz, 1971):

$$T = \frac{R}{4\pi} \iint_{\sigma} S(\psi) (\Delta g + G_1 + \dots) d\sigma = T_0 + T_1 + \dots \quad (6.166a)$$

With Bruns' formula (6.96), the corresponding development for the *height anomaly* ζ is obtained:

$$\zeta = \frac{R}{4\pi\gamma} \iint_{\sigma} S(\psi) (\Delta g + G_1 + \dots) d\sigma = \zeta_0 + \zeta_1 + \dots \quad (6.166b)$$

With $S(\psi)$ being Stokes' function (6.148), the main term in (6.166a,b) corresponds to Stokes' formula now applied to the surface gravity anomalies (6.14). The first correction term, in close approximation, is given by

$$G_1 = \frac{R^2}{2\pi} \iint_{\sigma} \frac{H^N - H_p^N}{l_0^3} \Delta g d\sigma, \quad l_0 = 2R \sin \frac{\psi}{2}. \quad (6.166c)$$

It depends on the terrain inclination (H^N normal height) and on the gravity anomalies. Assuming a linear correlation of the gravity anomalies with height, G_1 can be approximated by the gravimetric terrain correction (6.113), Sideris (1990). Hence, Faye anomalies, cf. [6.5.3], are well suited for the computation of height anomalies.

Since the integral kernel in (6.166c) decreases rapidly with increasing spherical distance ψ , the integration can be restricted to a limited area. Higher-order terms in (6.166a/b) contain the tangent of the terrain inclination and can be neglected generally. In order to ensure convergence of Molodensky's series expansion, extreme inclinations and singularities (steep slopes) need to be removed by some smoothing procedure. The Molodensky correction terms reach the dm-order of magnitude in the high mountains and remain at the cm-order in the lowlands. If the remove-restore technique, cf. [6.7.1], is applied, the corrections reduce by about one-order of magnitude and the series convergence is significantly improved (Denker and Tziavos, 1999). Molodensky's problem has been thoroughly investigated by Moritz (1971) and others, and the existence and uniqueness of the solution was proved by Hörmander (1976) and Sansò (1988).

A very efficient method for calculating the height anomaly is provided by the "gradient solution", which is particularly well suited for FFT techniques (Moritz, 1980; Forsberg and Tscherning, 1997).

Here, the surface gravity anomalies are first reduced to sea level (geoid or quasigeoid), by analytical downward continuation. Then Stokes' integral is applied, leading to height anomalies on sea level. Subsequent upward continuation of the sea level height anomaly finally gives the *surface height anomaly*:

$$\zeta = \frac{R}{4\pi\gamma} \iint_{\sigma} \left(\Delta g - \frac{\partial(\Delta g)}{\partial H^N} H^N \right) S(\psi) d\sigma + \frac{\partial \zeta}{\partial H^N} H^N. \quad (6.167a)$$

Poisson's integral provides the radial derivative of Δg (Hofmann-Wellenhof and Moritz, 2005, p. 32 ff.):

$$\frac{\partial(\Delta g)}{\partial H^N} = \frac{R^2}{2\pi} \iint_{\sigma} \frac{\Delta g - \Delta g_p}{l_0^3} d\sigma, \quad (6.167b)$$

and the vertical gradient of ζ results from (6.96) and (6.101):

$$\frac{\partial \zeta}{\partial H^N} = \frac{\partial}{\partial H^N} \left(\frac{T}{\gamma} \right) = \frac{1}{\gamma} \left(\frac{\partial T}{\partial H^N} - \frac{1}{\gamma} \frac{\partial \gamma}{\partial H^N} T \right) = -\frac{\Delta g}{\gamma}. \quad (6.167c)$$

If the surface anomalies are reduced to the level of the *computation point* P , H^N in (6.167a) has to be substituted by $H^N - H_{p'}^N$. The last term in (6.167a) then vanishes, as H outside the integral means $H_{p'}^N$, and (6.167a) simplifies to

$$\zeta = \frac{R}{4\pi\gamma} \iint_{\sigma} \left(\Delta g - \frac{\partial(\Delta g)}{\partial H^N} (H^N - H_{p'}^N) \right) S(\psi) d\sigma. \quad (6.167d)$$

The anomalies are now reduced from ground level to the level of the calculation point, which means that reference levels are changing with the points of calculation.

The *surface deflection of the vertical* (see Molodensky's definition in [6.1.2]) is derived from (6.166b) by differentiation according to (6.98):

$$\begin{Bmatrix} \xi^N \\ \eta^N \end{Bmatrix} = \frac{1}{4\pi\gamma} \iint_{\sigma} (\Delta g + G_1 + \dots) \frac{dS(\psi)}{d\psi} \begin{Bmatrix} \cos \alpha \\ \sin \alpha \end{Bmatrix} d\sigma - \frac{\Delta g}{\gamma} \begin{Bmatrix} \tan \beta_x \\ \tan \beta_y \end{Bmatrix}. \quad (6.168)$$

The principal term in (6.168) is Vening-Meinesz' formula (6.151), and the Molodensky correction terms again take the effect of the terrain into account. Another version of (6.168) is obtained by differentiation of (6.167d), Hofmann-Wellenhof and Moritz (2005, p. 314 ff.).

Molodensky's problem is characterized by the fact that no assumptions on the density distribution within the Earth are necessary, in contrast to the geoid determination using Stokes' formula. By the relation (6.9) between the geoid and the quasigeoid, a simple method is available to derive geoid heights from height anomalies by adding a correction term which depends on the Bouguer anomaly and the height. Data reductions onto the geoid and calculations of indirect effects are avoided by this strategy, and density hypotheses enter only through the Bouguer anomaly (Flury and Rummel, 2009). On a large scale, the Bouguer anomalies are negative on the continents, cf. [8.2.4], hence the quasigeoid generally is above the geoid. The differences between the geoid and the quasigeoid are of the cm- to dm-order of magnitude in flat and hilly regions but may reach one meter and more in the mountains. Deflections of the vertical defined on the ground and on the geoid may differ by a few arcsec in mountainous areas.

One example for a regional quasigeoid determination is the European Gravimetric Quasigeoid EGG07 (Denker et al. 2009). It is based on a high-resolution data set of point and mean gravity anomalies derived from land, sea and airborne gravimetry, and on satellite altimetry in the marine areas (Fig. 6.34). The remove-restore technique was applied using the EIGEN-GL04C (360,360) model from GFZ geopotential model (based on CHAMP, GRACE and terrestrial data), and terrain reductions according to the residual terrain model technique. A $3'' \times 3''$ (partly $1'' \times 1''$) digital elevation model delivered the terrain information, and a moving average filter over $30' \times 45'$ blocks provided the reference topography. Gridded $1' \times 1'$ residual gravity anomalies were transformed to height anomalies by least-squares spectral combination, cf. [6.7.1]. The main part of EGG07 (Fig. 6.35) stems from the global model, but the contributions from terrestrial gravity data and topography still amount to ± 0.4 m (maximum 4 m) and ± 0.03 m

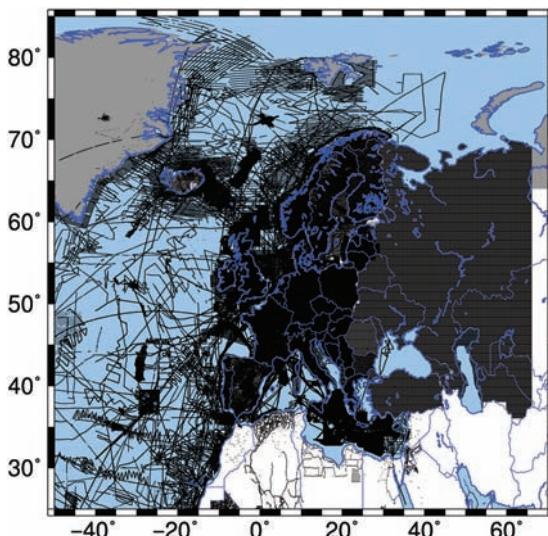


Fig. 6.34: Distribution of land, marine and airborne gravity data used for the European quasigeoid EGG07 (Denker et al., 2009).

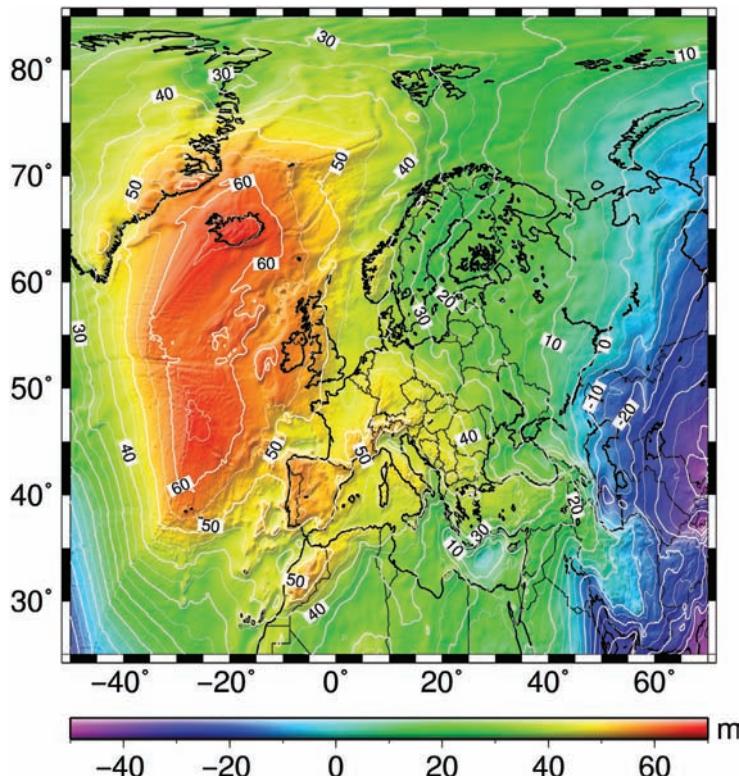


Fig. 6.35: European gravimetric quasigeoid EGG07, contour line interval 5 m (Denker et al., 2009).

(maximum 0.8 m), respectively. The accuracy of the $1' \times 1'$ EGG07 quasigeoid model has been evaluated by comparisons with GPS/leveling control points, which indicate an accuracy potential in the order of 0.03 to 0.05 m at continental scales and 0.01 to 0.02 m over distances up to a few 100 km, if high quality and high resolution input data are available in the area of interest. The EGG2008 solution follows the same philosophy, by combining an improved gravity anomaly data set with the global EGM2008 model, cf. [6.6.3]. This reduces the contribution from terrestrial gravity data to about ± 0.2 m (maximum 2.4 m), and further approaches the “cm” accuracy at local geoid/quasigeoid modeling (Denker, 2012).

Quasigeoid modeling for other parts of the world follow similar strategies, and partly also include GPS/leveling control points.

6.7.3 The external gravity field

The gravity field outside the Earth is of interest for the orbit determination of satellites, and for the evaluation and exploitation of gravity field related data obtained by satellite and airborne methods. Corresponding modeling is based on the fact that the gravitational potential is a harmonic function in the exterior space, cf. [3.1.3]. This includes the

upward or downward continuation of gravity field quantities from or towards the Earth's surface, either globally or locally.

Global modeling employs the *spherical harmonic expansion* of the disturbing potential (spherical approximation), see (6.3) to (6.4)

$$T(r, \vartheta, \psi) = \sum_{l=2}^{\infty} \left(\frac{R}{r}\right)^{l+1} T_l(\vartheta, \lambda) \quad (6.169)$$

and the corresponding expansions for the height anomaly (6.132), the gravity disturbance (6.134) and the gravity anomaly (6.135), the deflection of the vertical (6.137), the vertical gradient (6.138), and other residual gravity field quantities, where the $T_l(\vartheta, \lambda)$ represent the surface spherical harmonics of T . These expansions converge outside a sphere enclosing the Earth, cf. [3.3.2]. The spherical harmonic expansions clearly reveal the attenuation of the gravity field with altitude, being proportional to $1/r$ for the disturbing potential, to $1/r^2$ for the gravity anomaly (gravity disturbance) and deflection of the vertical, and to $1/r^3$ for the gravity gradient.

Some examples for gravity field attenuation with height are given in Fig. 6.36. Calculated from the Earth Gravitational Model EGM2008, cf. [6.6.3], the structures of the

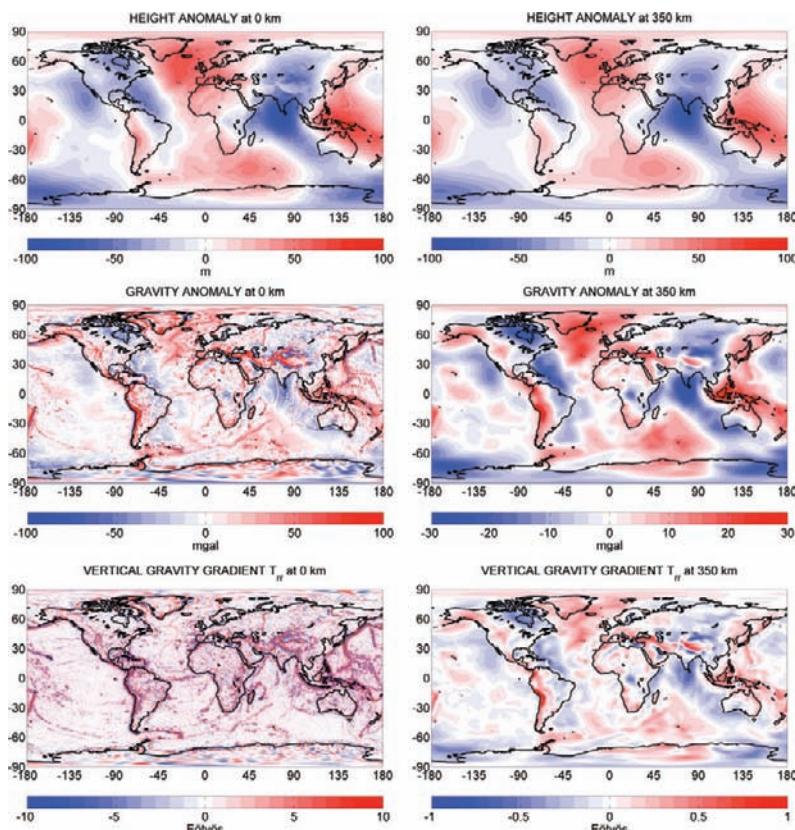


Fig. 6.36: Height anomaly, gravity anomaly and vertical gravity gradient at height $h = 0$ km and $h = 350$ km, from the Earth Gravitational Model EGM2008 (Pavlis et al., 2008); IfE, Leibniz Universität Hannover.

height anomaly (equal to the quasigeoid at height zero), the gravity anomaly, and the vertical gravity gradient are shown for the height $h = 0$ and $h = 350$ km, the different behavior of the residual gravity field quantities can be easily recognized.

Another example for the small gravity field signal at satellite altitude is given in Fig. 6.37. It shows the near radial component of the gravitational gradient tensor, as measured over two months by the GOCE satellite above the central Andes.

With continuously improving *global* gravity field data sets, cf. [6.6.3], spherical harmonic developments are of relevance for the majority of gravity field computations in space. More *local* problems as occurring for instance at airborne gravimetry, on the other hand, requires gravity field modeling which additionally utilizes local gravity data of high resolution and accuracy. The corresponding solutions are provided again by *integral formulas*.

Dealing with functions harmonic in space and given on the sphere as boundary surface (spherical approximation), the problem of upward continuation corresponds to the first boundary-value problem (*Dirichlet problem*) of potential theory. The solution is given by *Poisson's integral* which for the *disturbing potential* reads as (Hofmann-Wellenhof and Moritz, 2005, p. 247 ff.)

$$T_p = \frac{R(r^2 - R^2)}{4\pi} \iint_{\sigma} \frac{T}{l^3} d\sigma. \quad (6.170)$$

With respect to the *free-air anomaly* Δg , according to (6.135) the function

$$r\Delta g = \sum_{l=2}^{\infty} (l-1) \left(\frac{a}{r}\right)^{l+1} T_l(\vartheta, \lambda) \quad (6.171a)$$

is harmonic in space. This leads to the integral

$$\Delta g_p = \frac{R^2 (r^2 - R^2)}{4\pi r} \iint_{\sigma} \frac{\Delta g}{l^3} d\sigma \quad (6.171b)$$

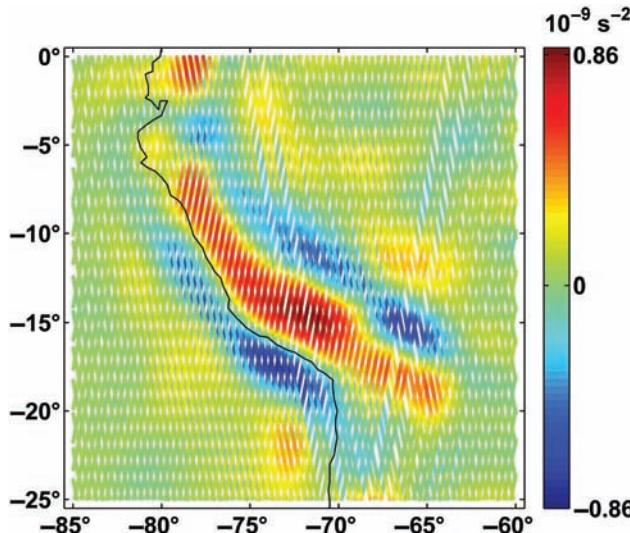


Fig. 6.37: Measured GOCE gravitational gradients T_{zz} (gradiometer reference frame) over the central Andes (October to December 2010), band-pass filtered to the gradiometer measurement bandwidth (0.005–0.1 Hz) corresponding to a spatial resolution of about 750 to 40 km, level 1b data provided by ESA; IfE, Leibniz Universität Hannover.

for the calculation of gravity anomalies in space from boundary values, where Δg_p refers to the point P in space and Δg are the surface anomalies on the spherical boundary surface. The integral kernel decreases rapidly with distance, which allows restriction of the integration area on a limited zone around the computation point.

We now insert (6.171b) into (6.101b) which now represents a differential equation in space, and remove the spherical harmonics of degree zero and one. This leads to a spatial extension of the geoid related Stokes' formula (6.147) for the *disturbing potential*, which was derived by Pizetti:

$$T(r, \vartheta, \lambda) = \frac{R}{4\pi} \iint_{\sigma} S(r, \psi) \Delta g d\sigma, \quad (6.172a)$$

where

$$S(r, \psi) = \frac{2R}{l} + \frac{R}{r} - \frac{3Rl}{r^2} - \frac{R^2}{r^2} \cos \psi \left(5 + 3 \ln \frac{r - R \cos \psi + l}{2r} \right), \quad (6.172b)$$

with

$$l = \sqrt{r^2 + R^2 - 2Rr \cos \psi}, \quad (6.172c)$$

is the extended Stokes' function.

Brun's theorem finally gives the separation between the geopotential surface $W = W_p$ and the spheropotential surface $U = U_Q = W_p$ (*height anomaly* in space):

$$\zeta(r, \vartheta, \lambda) = \frac{R}{4\pi} \iint_{\sigma} S(r, \psi) \Delta g d\sigma. \quad (6.173)$$

Corresponding spatial extensions can be derived for all other integral formulas such as the inverse Stokes' integral, Hotine's formula for gravity disturbance, and Vening-Meinesz formulae for the deflection of the vertical.

6.7.4 Astrogeodetic geoid and quasigeoid determination

Geoid and quasigeoid height *differences* can be obtained from deflections of the vertical, determined according to (6.57), (6.58) from astronomic and geodetic latitudes and longitudes resp. azimuths.

In *astronomic leveling*, the deflections of the vertical are integrated along the path, either on the geoid or on the Earth's surface (Fig. 6.38). On the *geoid*, we have

$$dN = -\varepsilon_0 ds, \quad (6.174a)$$

where ε_0 is the vertical deflection component in the azimuth direction of the path (6.18), reduced to the geoid according to Pizetti's definition, cf. [6.1.2]. Integration between P_1 and P_2 yields the geoid height difference

$$\Delta N_{1,2} = N_2 - N_1 = - \int_1^2 \varepsilon_0 ds. \quad (6.174b)$$

The negative sign follows from the sign conventions for the geoid height (6.8) and the deflection of the vertical (6.17).

The *geoid* deflection of the vertical, required in (6.174), is obtained by *reducing* the observed astronomic latitude and longitude onto the geoid:

$$\Phi_0 = \Phi + \delta\Phi, \quad \Lambda_0 = \Lambda + \delta\Lambda, \quad (6.175)$$

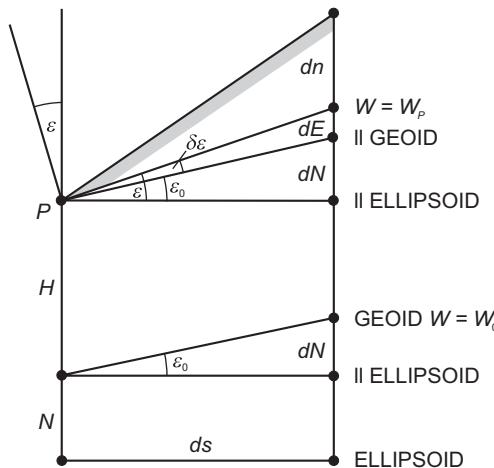


Fig. 6.38: Astronomic leveling.

where Φ_0 and Λ_0 are the astronomic coordinates on the geoid (Fig. 6.39). The reductions follow from the integration of the plumb line curvature κ_x, κ_y (3.74) between the Earth's surface and the geoid:

$$\delta\Phi = - \int_0^H \kappa_x dH, \quad \delta\Lambda \cos\Phi = - \int_0^H \kappa_y dH, \quad (6.176a)$$

with H being the orthometric height. Inserting (3.67) and (3.70) yields

$$\delta\Phi = - \int_0^H \frac{1}{g} \frac{\partial g}{\partial x} dH, \quad \delta\Lambda \cos\Phi = - \int_0^H \frac{1}{g} \frac{\partial g}{\partial y} dH, \quad (6.176b)$$

R mean radius of the Earth. With (6.17), the NS and EW components of the vertical deflection are given by

$$\xi_0 = \xi + \delta\Phi, \quad \eta_0 = \eta + \cos\Phi \delta\Lambda, \quad (6.177a)$$

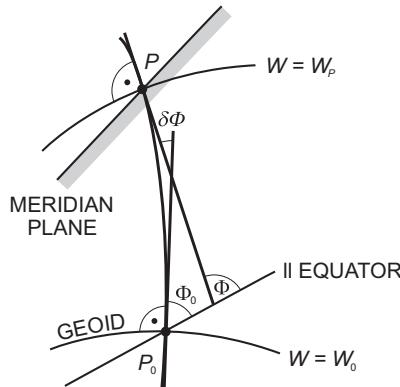


Fig. 6.39: Plumb line curvature in the meridian plane.

and the azimuthal component reads

$$\varepsilon_0 = \xi_0 \cos \alpha + \eta_0 \sin \alpha. \quad (6.177b)$$

In order to evaluate (6.176), the gravity and the horizontal gravity gradient along the plumb line are required. Digital terrain models allow estimation of these quantities with an accuracy between $0.1''$ and $1''$, but errors may be larger in high mountains. The angle of plumb line curvature itself attains values of a few $0.1''$ in the lowlands and may reach $10''$ and more at high mountain stations.

Instead of integrating the deflections of the vertical on the geoid, the *surface* vertical deflections (definitions from Helmert or from Molodensky) may be used. The azimuthal component of *Helmert's* deflections of the vertical is given by

$$\varepsilon = \varepsilon_0 - \delta\varepsilon, \quad (6.178)$$

where the components of $\delta\varepsilon$ are obtained from (6.176b). Inserting into (6.174b) yields the geoid height difference

$$\Delta N_{1,2} = N_2 - N_1 = - \int_1^2 \varepsilon ds - \int_1^2 \delta\varepsilon ds. \quad (6.179a)$$

As seen from Fig. 6.38, the second term on the righthand side equals the orthometric height reduction E which is well known from geometric leveling (6.81b): the angle of plumb line curvature is the horizontal derivative of E . We thus have

$$\Delta N_{1,2} = - \int_1^2 \varepsilon ds - E_{1,2}. \quad (6.179b)$$

For *height anomalies*, the difference follows from the differential (Moritz, 1983)

$$d\zeta = \frac{d\zeta}{ds} ds + \frac{d\zeta}{dh} dh. \quad (6.180)$$

The first term describes the effect of *Molodensky's* vertical deflection. The second term enters because the physical surface of the Earth is not a level surface. Using (6.167c) and integration along the path yields *Molodensky's* astronomic leveling of height anomalies

$$\Delta \zeta_{1,2} = \zeta_2 - \zeta_1 = - \int_1^2 \varepsilon^N ds - \int_1^2 \frac{\Delta g}{\gamma} dh, \quad (6.181)$$

where Δg refers to the Earth's surface.

The relation between geoid and quasigeoid height differences follows from (6.9) and (6.81):

$$\Delta \zeta_{1,2} = \Delta N_{1,2} + E_{1,2} - E_{1,2}^N \quad (6.182a)$$

or when taking (6.179b) into account

$$\Delta \zeta_{1,2} = - \int_1^2 \varepsilon ds - E_{1,2}^N, \quad (6.182b)$$

where $E_{1,2}^N$ is the normal height reduction (6.81c).

The small correction terms in (6.179), (6.181), and (6.182) can be calculated easily from surface gravity and a digital terrain model. Therefore, the integration of surface vertical deflections is of advantage even for geoid computations, as the tedious reductions onto the geoid required in (6.174) are not necessary.

The line integrals of astronomic leveling presuppose that the deflections of the vertical are given continuously along the path. In reality, vertical deflections generally are available only at larger distances (several 10 km or more), which is due to the time-consuming astronomic observations. Station distances of a few km or even less are restricted to special engineering or research surveys (see below). This poses the problem of *interpolation* between the vertical deflection points (in the following, we do not distinguish between the vertical deflections on the geoid and on the Earth's surface!). Interpolation can be carried out by purely mathematical methods or supported by additional information on the gravity field behavior.

In the simplest case of *mathematical interpolation*, a linear change of the deflections of the vertical between the stations P_1 and P_2 is assumed. The integration then yields

$$\Delta N_{1,2} = -\frac{\varepsilon_1 + \varepsilon_2}{2} s, \quad (6.183)$$

where s is the distance between P_1 and P_2 .

The linear interpolation model is adequate in flat areas and where the distances between the vertical deflection points are not too large (a few km). An area with sufficient control point coverage then can be evaluated either by forming triangles and adjusting the geoid height misclosures or by a surface polynomial approximation to the geoid (Vaniček and Merry, 1973). The polynomial coefficients are determined from the corresponding series expansions of the vertical deflection components, which result from (6.98) and Bruns' formula

$$\xi = -\frac{1}{R} \frac{\partial N}{\partial \varphi}, \quad \eta = -\frac{1}{R \cos \varphi} \frac{\partial N}{\partial \lambda}, \quad (6.184)$$

where the condition of integrability of a potential field, cf. [3.1.5], must be fulfilled:

$$\frac{\partial \xi}{\cos \varphi \partial \lambda} = \frac{\partial \eta}{\partial \varphi}. \quad (6.185)$$

Least-squares prediction, cf. [6.1.3], offers another efficient interpolation method (Heitz, 1969), while least-squares collocation, cf. [6.8.2], even allows direct estimation of geoid heights from the vertical deflections, thus providing an alternative to the integral formulas.

Additional *gravity field information* between the vertical deflection points can be supplied by terrain models, gravity anomalies, and zenith angles, and used for interpolation.

A digital *terrain model* (possibly also taking density variations into account) can be used to calculate the effect of topography on the deflections of the vertical. For more extended calculation areas, the effect of isostatically compensating masses should also be considered, cf. [6.5.2]. By subtracting the corresponding contribution from the observations, the vertical deflection field is smoothed, and mathematical interpolation methods are made easier. The interpolated *residual* deflections of the vertical are then augmented by the effects of topography and isostasy, leading to a densified network of vertical deflection points. This remove-restore method has proved to be efficient especially in mountainous areas (Hirt and Flury, 2008).

If a dense field of gravity stations around the vertical deflection points is available, it can be utilized for a *gravimetric* interpolation. Here, gravimetric deflections of the vertical are computed according to (6.151) by integrating the gravity anomalies over a limited area (e.g., three times the distance between the vertical deflection points). This gravimetric part is then removed from the observations, in addition a systematic difference between the astrogeodetic and the gravimetric

vertical deflections has to be taken into account (different reference systems, effect of the zones neglected in the calculation of the gravimetric vertical deflections). The residual deflections of the vertical thus obtained are smooth and easy to interpolate. This method has been extended to *astrogravimetric leveling*, with a gravimetric “correction” to quasigeoid differences obtained from linear interpolation of surface deflections of the vertical (Molodenski et al., 1962). This gravimetric interpolation allows calculation of geoid or quasigeoid height differences with cm to dm accuracy, even at larger spacing of the vertical deflection points.

Reciprocal zenith angles deliver differences of the vertical deflection components ε in the line of sight. According to (6.85), the observed zenith angles z and the ellipsoidal quantities ζ are related by (Fig. 6.20)

$$\zeta_1 = z_1 + \varepsilon_1, \quad \zeta_2 = z_2 + \varepsilon_2. \quad (6.186a)$$

Inserting into (6.87), and taking sign conventions into account, yields

$$\varepsilon_2 - \varepsilon_1 = z_1 + z_2 - \frac{S}{R} - \pi, \quad (6.186b)$$

where S is the spherical distance between P_1 and P_2 . Starting at a vertical deflection point, these differences can be used for the interpolation of deflections of the vertical. The method has found some application in mountainous areas, where an interpolation accuracy of about 1 arcsec has been achieved.

The advantage of the astrogeodetic method of geoid or quasigeoid determination consists in its independence from data outside the area of calculation, in contrast to the gravimetric method where a global coverage with gravity data is needed. In addition, the demands on the accuracy of the point heights are less stringent as with the formation of gravity anomalies. On the other hand, the establishment of a vertical deflection point requires substantially more time than a gravity measurement. A station spacing of 10 to 20 km is available only in few regions, and even distances of up to 30 to 50 km are limited to well-surveyed countries. Large parts of the continents are covered only sparsely, with concentration on profiles along first-order triangulation chains, cf. [7.1.1]. Under these conditions, the accuracy of astronomic leveling mainly depends on the quality of interpolation, where an accuracy of a few cm to 0.1 m over some 100 km can be achieved in densely surveyed areas. With station distances of a few km, and by applying remove-restore techniques with respect to topographic-isostatic effects (see above), the accuracy can be increased to 0.01 to 0.02 m over several 100 km. Sub-millimeter/km precision can be obtained at dedicated geoid profiles with station distances of 50 to 100 m, employing transportable zenith cameras (Hirt and Seeber, 2007), cf. [5.3.1].

The superior efficiency of gravimetric methods has greatly reduced the application of astronomic leveling. It is now only occasionally applied at areas or profiles which are not well covered by gravity measurements as in the mountains where gravity stations are typically concentrated along the roads. More important is the method’s capability to independently control gravimetric geoid/quasigeoid solutions, and to high-resolution local gravity field determination as required at sophisticated engineering projects.

Astronomic leveling was introduced by Helmert (1884) and first applied in the Harz mountains, Germany. From the 1950s to the 1970s, astrogeodetic geoid determinations were carried out in a number of countries, using astronomic observations on the first-order triangulation points (Heitz, 1969). Deflections of the vertical, and the resulting geoid, referred to the national geodetic datum and served for the reduction of horizontal angles and chord distances onto the national reference

ellipsoid, cf. [6.3.2], [7.1]. Large-scale solutions included the “*Bomford*” geoid for Europe (Levallois and Monge, 1978) and the continent-wide geoid determination by Fischer et al. (1968), with an average accuracy of a few meters. High precision astrogeodetic geoid models have been developed in Switzerland and Austria, based on a densified net of vertical deflection points and high-resolution digital terrain models, and employing remove-restore techniques (e.g., Marti, 1997). Profiles of 500 km length and with station distances of a few km have been established in Germany for the control of gravimetric geoid models. Based on astrogeodetic measurements with a transportable zenith camera system and a digital terrain model for applying the remove-restore technique, an agreement of a few cm was generally obtained between the astrogeodetic and the gravimetric solutions (Voigt et al., 2009). For parts of continental Europe, a corresponding comparison between astrogeodetic data and gravimetric deflections of the vertical derived from EGM2008 showed an agreement of about 3”, which reduced to about 1” after taking the omission error of the global model into account (Hirt et al., 2010).

6.8 Least-squares collocation

The strategy of combining observation equations for all relevant data and using least-squares adjustment for the determination of geometric and gravimetric parameters has been already shortly discussed at the beginning of this chapter. Through least-squares collocation, a stochastic model for gravity field estimation is added, which leads to a very general method of combination.

In the most general form of *least-squares collocation with parameters* (Moritz, 1980, p. 111 ff.), this method combines the calculation of station coordinates and other deterministic unknowns (harmonic coefficients, Earth ellipsoid and Earth orientation parameters, calibration and drift coefficients, etc.) with the estimation of residual gravity field quantities at unsurveyed points, utilizing all kind of (geometric and physical) observables (Krarup, 1969; Moritz, 1973). By extending the (linear) observation equation for least-squares (parameter) adjustment by a gravity field signal part, the general form of the *observation equation* reads

$$\mathbf{I} = \mathbf{Ax} + \mathbf{s} + \mathbf{n}, \quad (6.187)$$

where \mathbf{I} is the linearized vector of observations. It is composed of the deterministic part \mathbf{Ax} and two stochastic parts \mathbf{s} and \mathbf{n} . \mathbf{x} represents the parameter vector and \mathbf{A} the design matrix containing the differential relations between observations and parameters. The signal vector \mathbf{s} contains the residual gravity field quantities at any point, either observed or to be predicted; it is more formally handled as a random quantity. The signal vector may include, in contrast to least-squares prediction, cf. [6.1.3], any kind of gravity field quantities such as residual harmonic coefficients, geoid or quasigeoid heights, gravity anomalies, deflections of the vertical, gravity gradient components, etc. The noise vector \mathbf{n} represents the errors of the measurements, and is random originally. Each of the stochastic quantities is supposed to have a mean value of zero. The statistical behavior of these two parts is described by the covariance matrix \mathbf{C} of the gravity field signals, on the one hand, and the covariance matrix \mathbf{D} of the observational noise, on the other, where mutual independence of signal and noise is assumed.

As easily recognized, least-squares collocation with parameters is an overdetermined problem with respect to the parameters (the number of observations exceeds the number

of parameters) and an underdetermined problem with respect to the gravity field signal (more signals have to be predicted than have been observed). It is solved by applying a least-squares minimum condition on the weighted quadratic sum of the signal and the noise part, thus combining least-squares adjustment with least-squares prediction already discussed in [6.1.3], Moritz (1980). Following well-known rules of adjustment theory, the solution for the *parameter vector* is given by

$$\mathbf{x} = (\mathbf{A}^\top \bar{\mathbf{C}}^{-1} \mathbf{A})^{-1} \mathbf{A}^\top \bar{\mathbf{C}}^{-1} \mathbf{l}, \quad (6.188)$$

with $\bar{\mathbf{C}} = \mathbf{C} + \mathbf{D}$. The component of the *signal vector* predicted in an unsurveyed point P results in

$$\hat{s}_P = \mathbf{C}_P^\top \bar{\mathbf{C}}^{-1} (\mathbf{l} - \mathbf{Ax}), \quad (6.189)$$

where the covariance vectors and matrices are explained in [6.1.3], but may now include heterogeneous signals. Following the arguments given in [6.2.1] for the combined adjustment, the least-squares parameter adjustment generally is separated from detailed gravity field estimation. This leads to "pure" least-squares collocation, as an extension of least-squares prediction, cf. [6.1.3].

At *least-squares collocation*, applied to gravity field estimation, the elements of the signal covariance matrix \mathbf{C} are required, describing the correlation between *heterogeneous* residual gravity field quantities. Since all these quantities belong to the same gravity field, the covariances have to be derived from a (harmonic) basic covariance function through covariance propagation. The *covariance function* of the *disturbing potential* T is selected for this purpose, as all residual gravity field quantities are related to T in a simple manner. This covariance function is defined in analogy to the covariance function of the gravity anomalies (6.21). It is considered to be the mean value of the products of T in the points P and P' for a constant spherical distance ψ , where again we assume homogeneity and isotropy. The function is then given by:

$$K(\psi) = \text{cov}_\psi(T) = M\{TT'\}_\psi. \quad (6.190)$$

Covariance propagation is well known from the theory of errors and is applied here to gravity field signals. As demonstrated by (6.96) to (6.101), all residual gravity field quantities (either observed or to be predicted) can be expressed as a linear functional of T . For an *observation* I_i we thus have

$$I_i = L_i^P T(P'), \quad (6.191)$$

where L_i is the functional to be applied to the disturbing potential T in order to transform it into the gravity field quantity wanted. The covariance between T and I_i is obtained by applying L_i on the covariance function $K(\psi) = K(P, P')$, which can be expressed as a function of the spatial coordinates of P and P' :

$$C_{Pi} = M\{TI_i\} = L_i^P K(\psi). \quad (6.192)$$

For different types of observations at P and P' , the covariance results from a subsequent application of the functionals L valid for the transformation of T into the respective observation:

$$C_{ij} = M\{I_i I_j\} = L_i^P L_j^{P'} K(\psi). \quad (6.193)$$

The same rules have to be followed if heterogeneous signals shall be estimated.

The statistical description of the Earth's gravity field required for least squares collocation is available by anomaly degree variance models, cf. [6.1.3]. The relation of these models to the basic covariance function introduced above can be derived by applying the mean value operator (6.190) on the spherical harmonic expansion of the disturbing potential (6.4). This yields the spatial covariance function of T :

$$K(\psi) = \sum_{l=2}^{\infty} \sigma_l^2(T) \left(\frac{R^2}{rr'} \right)^{l+1} P_l(\cos \psi), \quad (6.194a)$$

where the potential degree variances are defined in analogy to (6.26):

$$\sigma_l^2(T) = M\{T_l^2\}. \quad (6.194b)$$

Taking Bruns' formula $N = T/\gamma$ into account, equation (6.143) provides the relation between the degree variances of the disturbing potential and the gravity anomalies:

$$\sigma_l^2(T) = \left(\frac{R}{l-1} \right)^2 \sigma_l^2(\Delta g). \quad (6.195)$$

Inserting (6.195) into (6.194a) finally yields

$$K(\psi) = R^2 \sum_{l=2}^{\infty} \frac{1}{(l-1)^2} \sigma_l^2(\Delta g) \left(\frac{R^2}{rr'} \right)^{l+1} P_l(\cos \psi), \quad (6.196)$$

which enables the calculation of the basic covariance function from an anomaly degree variance model. For *local* applications, the covariance function has to be fit to the gravity field structure in the area of calculation, cf. [6.1.3].

The advantage of least-squares collocation is the flexibility in estimating any kind of gravity field quantity from different types of gravity field observations, at surveyed and unsurveyed points. The data can be processed as discrete values and need not be continuous, as required for the application of integral formulas, cf. [6.7]. Neither gridding of the data nor reduction to some reference level is required. For homogeneous and continuously distributed data, least-squares collocation transforms into the integral formulas of physical geodesy (Moritz, 1976). On the other hand, the amount of data that can be handled remains limited by computing facilities, as equation systems have to be solved for the inversion of $\bar{\mathbf{C}}$ having a dimension equal to the number of observations. Applications have therefore been restricted to limited areas and data sets. By introducing some restrictions on the data, computing time can be reduced and larger data sets evaluated (Sünkel, 1986a; Bottoni and Barzaghi, 1993; Sansò and Tscherning, 2003).

Least-squares collocation is applied especially for local and regional geoid determination (Tscherning and Forsberg, 1986; Denker, 1988), but also for the estimation of gravity anomalies from altimetric geoid heights and for downward continuation problems. Remove-restore techniques are used generally, cf. [6.7.1], which reduces the data collection area. One example for the application of least-squares collocation is the geoid of Austria, determined from vertical deflections and gravity anomalies after reducing a global and a topographic-isostatic gravity model (accuracy of a few cm), Kühtreiber (2002). The upward continuation of second derivatives of the disturbing potential from the ground, for GOCE data calibration and validation represents another example of least-squares application (Wolf and Denker, 2005).

7 Geodetic and Gravimetric Networks

Geodetic and gravimetric networks consist of monumented control points that provide the reference frames for positioning and gravity-field determination. In the sequel, we concentrate on *regional* networks which are established nation- or continent-wide. They serve as the basis for all kind of surveying and navigation, as well as for geo-information systems including topographic and thematic map series, and for the investigation of recent geodynamics. Regional networks are increasingly derived from or integrated into *global* reference frames established and maintained by international conventions, cf. [2.4], [5.4.3]. *Local* networks are established, e.g., for engineering and exploration projects, real estate surveys and crustal movement investigations. They generally follow similar rules as regional networks at design, measurement, and evaluation, adapted to the specific demands and peculiarities of the respective problem.

Until recently, horizontal and vertical control networks have been established separately, following the classical treatment of (horizontal) positioning and heighting. These networks still are the basis of national geodetic reference systems, and they even have been partly combined to continent-wide systems [7.1], [7.2]. Since some decades, geodetic space methods allow the establishment of three-dimensional (3D) networks orientated with respect to a geocentric reference system. Today, these methods are characterized by very efficient procedures and homogeneous results of high accuracy, and consequently they are superseding the classical control networks. Strong endeavors are made now to integrate these networks into the 3D frame which also requires the inclusion of a geoid model [7.3]. Gravity networks serve the different needs of geodesy and geophysics, with the reference provided either by a global gravity standardization net or by absolute gravimetry; they are now also tied to the 3D geodetic reference frame [7.4].

If *reobserved* after a certain time span, geodetic and gravimetric networks can be utilized for the detection and investigation of medium- and long-term temporal variations of position and gravity. With progress in data acquisition and evaluation, continuously operating networks are established increasingly, which also allow the measurement of short-term variations. World-wide networks meanwhile monitor global changes and the variations of the Earth rotation routinely, cf. [2.4.2], while regional and local networks concentrate on the investigation of areas affected by recent geodynamic activities, cf. [8.3.4], [8.3.5].

The establishment of geodetic networks is treated in textbooks on geodesy and geodetic surveying, e.g., Bomford (1980); Moffitt and Bossler (1997); Anderson and Mikhail (1998); Kahmen (2006), and Hofmann-Wellenhof et al. (2008) with respect to GNSS; for gravity networks see, e.g., Torge (1989).

7.1 Horizontal control networks

National horizontal control networks were established from the eighteenth century until the 1980s, where the networks' design, observation, and computation methods changed with the available techniques. Computations were carried out on a conventional

reference ellipsoid fitted to the survey area. Since the 1960s, spatial geodetic methods have allowed orientation of the classical networks with respect to the global geocentric reference system, and control of scale and systematic distortions. In the following, we describe the design of these networks, the measurement and computation techniques applied, the accuracy achieved, and the orientation with respect to the Earth's body (geodetic datum). Having served (and serving) as a basis for many applications in surveying and mapping, they are still of relevance and now in a state of transition to the global 3D reference frame, cf. [7.3].

Horizontal control networks have been realized by *trigonometric (triangulation) points*, which in principle should be distributed evenly over the country. One distinguishes between different *orders* of trigonometric points, from first-order or primary (station separation 30 to 60 km) to second-order (about 10 km) to fourth- or even fifth-order (down to 1 to 2 km) stations, where the state of the networks' coverage strongly depends on the development of the respective region or country. The maximum distance between first-order points was determined by terrestrial measurement methods, which required intervisibility between the network stations. Consequently, first- and partly also second-order stations were established on the top of hills and mountains; observation towers (wooden or steel constructions with heights of 30 m and more) were erected especially in flat areas. The stations have been permanently marked by underground and surface monuments (stone plates, stone or concrete pillars, bolts in hard bedrock). Eccentric marks have been set up in order to aid in the recovery and verification of the center mark.

Classical horizontal control networks have been observed by the methods of triangulation, trilateration, and traversing.

In *triangulation*, all angles of the triangles formed by the trigonometric points are observed with a theodolite (Fig. 7.1). The instrument is set up on the observation pillar or tower; at large distances the targets are made visible by light signals. Either directions (successive observation of all target points) or angles (separate measurement of the two directions comprising one angle) are observed in several sets (i.e., in both positions of the telescope), distributed over the horizontal circle of the theodolite. The scale of a triangulation network is obtained from the length of at least one triangulation side, either derived from a short *baseline* through a baseline extension net or measured directly by a distance meter. Astronomic observations provide the orientation of the network, where an astronomic azimuth (Laplace azimuth) is needed for the horizontal orientation, see below.

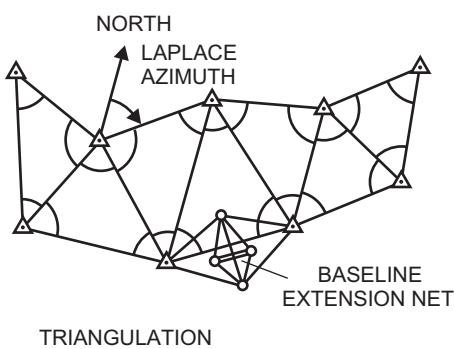


Fig. 7.1: Triangulation with baseline extension net and Laplace azimuth (principle).

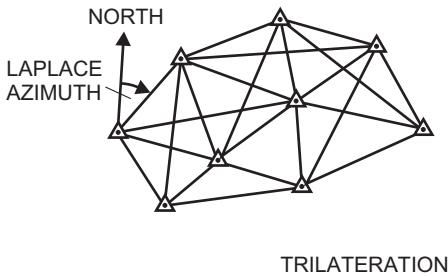


Fig. 7.2: Trilateration with Laplace azimuth (principle).

Trilateration employs electromagnetic distance meters in order to measure the lengths of all triangle sides of a network, including diagonals (Fig. 7.2). Again, at least one Laplace azimuth is needed for the orientation of the net. Electromagnetic distance measurements put less demands on the stability of observation towers as compared to angular measurements, and the use of microwaves makes the method more independent from weather conditions.

Traverses combine distance and angular measurements, where the traverse stations are arranged along a profile between already existing control points. The traverse stations may be either transformed into the national reference system by means of the control points, or immediately calculated in that system if astronomic (Laplace azimuth) or terrestrial orientation is available, Fig. 7.3 gives some examples. Traversing represents a very effective and flexible method for establishing horizontal control, with no more need to establish stations on hilltops. It has been employed primarily for the densification of higher-order networks.

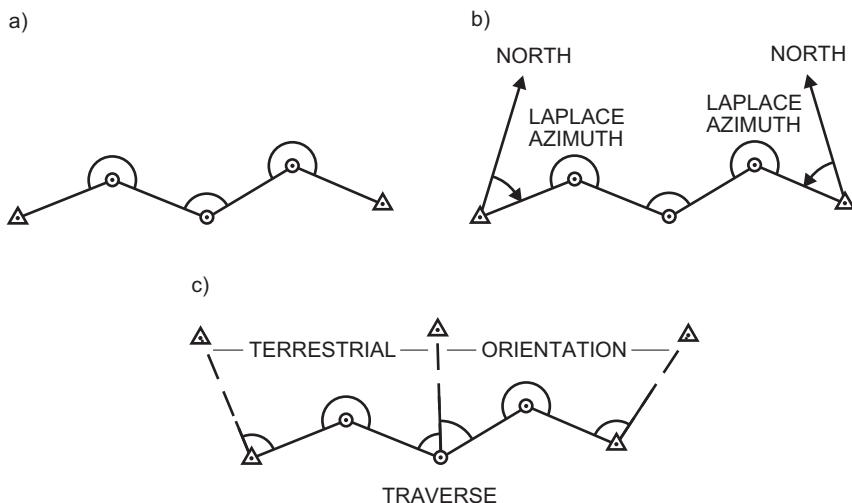


Fig. 7.3: Traverse connecting two control points (principle): a) without additional orientation, b) with orientation by Laplace azimuths, c) with orientation by directions to control points.

Horizontal control networks have also been formed by *combining* the methods of triangulation, trilateration, and traversing. Such networks are very stable in design, and allow establishment of first- and second-order control simultaneously. *Optimization* methods have been developed for the design and survey of trigonometric networks. Starting from the demands on accuracy and reliability, these methods provide information on the optimum point configuration and the distribution of the measurements in the network given the limitations of available equipment and the maximum allowable cost of the survey (Graffarend and Sansò, 1985).

Triangulation as part of a national geodetic survey started in France (1733–1750: *Carte géométrique de la France*, under the direction of *Cassini de Thury*) and in Great Britain (since about 1780 triangulation by the Ordnance Survey, under *W. Roy* and others). It continued to be the method for establishing horizontal control networks in the nineteenth and twentieth century until the introduction of electromagnetic distance measurements. Triangulation often started with chains (in many cases established along meridians and parallels) composed of triangles or quadrilaterals with diagonals tied together every few 100 km. The meshes of this framework then were filled by first- or second-order areal triangulation. The triangulations of Bavaria (1808–1828, *J.G. Soldner*) and of Prussia (since 1875, *O. Schreiber*) brought significant improvements in measurement and calculation techniques, which also influenced other national geodetic surveys. Large-scale networks (chains and filling nets) were developed in the U.S.A. (starting in the 1830s and connected with the names of *F. R. Hassler* and (later) *J.F. Hayford*, *W. Bowie* and many others) and in the former Soviet Union (since the 1930s, *T.N. Krassovski*). *Trilateration* was applied from the 1950s to the 1970s for strengthening, extending, and densifying triangulation networks. Airborne microwave methods were employed for the rapid survey of regions with difficult access and for bridging water areas (a few meters to 10 m accuracy over some 100 km). *Traversing* has been used mainly for network densification since the 1960s, but first-order geodimeter traverses also strengthened continental networks (U.S.A.) or even established them (Australia). From the 1960s to the 1980s, *satellite methods* were utilized to control the quality of horizontal control networks and especially to determine the orientation and the scale of the ellipsoidal systems with respect to the global geocentric system, see below.

First- and some second-order horizontal control networks have been calculated on a reference ellipsoid within the system of ellipsoidal coordinates, cf. [4.1]. Lower-order networks are primarily calculated in planar Cartesian coordinates, after conformal mapping of the ellipsoid onto the plane (Maling, 1973; Kuntz, 1990; Graffarend and Krumm, 2006). The *network calculation* started with the *reduction* of the observed horizontal angles/directions and spatial distances to the ellipsoid, where the gravity-field-related reductions (deflections of the vertical, geoid height) were not considered during earlier surveys, cf. [6.3.2]. The *adjustment* was carried out either by the method of conditions or by variation of the coordinates, with redundancy resulting from triangle misclosures, diagonals in trilateration quadrilaterals, and additional baselines and Laplace azimuths. The *coordinates' transfer* from an initial point (see below) was based on the solutions of the direct resp. inverse problem on the ellipsoid, cf. [6.3.3]. Among the deficiencies of this classical "*development method*" are the neglecting of the deflections of the vertical, the inadequate reduction of distances on the ellipsoid, and especially the step by step calculation of larger networks, with junction constraints when connecting a new network section to an existing one. This led to long-wavelength network distortions of different type, with regionally varying errors in scale (10^{-5} and more) and orientation

(a few arcsec). Coordinate errors with respect to the initial point increased from a few decimeters over about 100 km to about 1 m over several 100 km and reached 10 m and more at the edges of extended continent-wide networks.

The *geodetic datum* of a horizontal control network comprises the parameters of the reference ellipsoid and of the network's orientation with respect to the Earth's body, cf. [6.3.3]. *Conventional ellipsoids*, as computed by the adjustment of several arc measurements, were introduced during earlier geodetic surveys, cf. [1.3.3]. Some horizontal networks refer to locally *best-fitting ellipsoids*, as derived from a minimum condition on the observed vertical deflections, using the equations (6.51):

$$\sum(\xi^2 + \eta^2) = \min. \quad (7.1)$$

Tab. 7.1 gives the parameters of some reference ellipsoids that have been used for national geodetic surveys (Strasser, 1957; NIMA, 2000).

The ellipsoids of Airy (applied in Great Britain), Everest (India, etc.), Bessel (Germany, Austria, Japan, etc.), Clarke 1866 (U.S.A., Canada, etc.), and Clarke 1880 (France, etc.) are based on the adjustment of arc measurements distributed over the continents. The Hayford ellipsoid fits best to the vertical deflection (topographic-isostatically reduced) field in the U.S.A., it has been introduced in a number of countries. The Krassovski ellipsoid resulted from a fit to the Russian triangulations, with additional data from western Europe and the U.S.A. The ellipsoids of the Geodetic Reference Systems GRS67 (Australia, etc.) and GRS80 represent recent global approximations to the geoid, cf. [4.3].

The *orientation* of the ellipsoid was realized by defining the ellipsoidal coordinates of a fundamental (initial) point, also called network origin, and by conditions for the parallelism of the axes of the ellipsoidal and the global geocentric system, cf. [6.3.3].

In earlier surveys, the coordinates of the *fundamental point* were fixed by postulating equality between observed astronomic latitude, longitude, and orthometric height and the corresponding ellipsoidal quantities. This is identical to setting the deflection of the vertical and the geoid height of the fundamental point to zero:

$$\xi_F = 0, \quad \eta_F = 0, \quad N_F = 0. \quad (7.2)$$

Tab. 7.1. Parameters of reference ellipsoids (rounded values), NIMA (2000)

Name, Year	Semi-major axis a (m)	Reciprocal flattening $1/f$
Airy, 1830	6 377 563	299.3
Everest, 1830	6 377 276	300.8
Bessel, 1841	6 377 397	299.15
Clarke, 1866	6 378 206	294.98
Clarke, 1880	6 378 249	293.47
Hayford, 1909	6 378 388	297.0
= Int.Ell.1924		
Krassovski, 1940	6 378 245	298.3
GRS67	6 378 160	298.247
GRS80	6 378 137	298.257

This strategy provides a good approximation of the ellipsoid to the geoid close to the origin, but may lead to larger deviations at more remote areas (Fig. 7.4). If a sufficient number of vertical deflection points were available and well distributed over the area of calculation, the minimum condition (7.1) was used. It permits the determination of the deflection of the vertical in the fundamental point and at extended networks also the parameters of a best-fitting ellipsoid. This procedure led to an *optimum fitting* over the whole area, and kept the deflections of the vertical small. In many cases, the geoid height of the origin point was defined indirectly by reducing the baselines onto the geoid and treating them as ellipsoidal quantities (Fig. 7.5). The minimum condition for the geoid heights

$$\sum N^2 = \min. \quad (7.3)$$

was seldom applied using relative geoid heights calculated from astronomic leveling, cf. [6.7.4], and utilizing the last equation of (6.51).

The *parallelism* of the axes of the ellipsoidal and the geocentric system was achieved by the condition equations (6.57) and (6.58) for the deflection of the vertical and the azimuth (Laplace equation). In extended networks, several base lines and Laplace

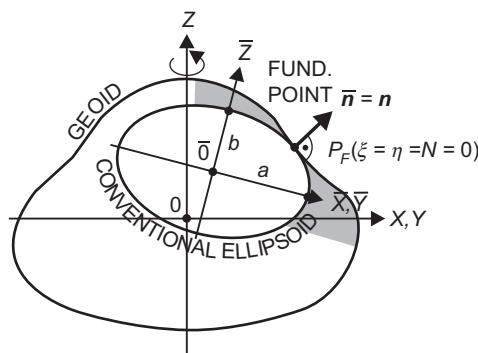


Fig. 7.4: Locally best fitting “conventional” ellipsoid.

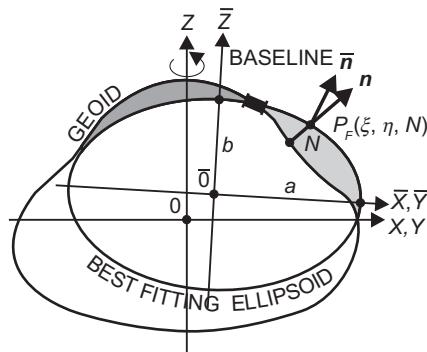


Fig. 7.5: Regionally best fitting ellipsoid.

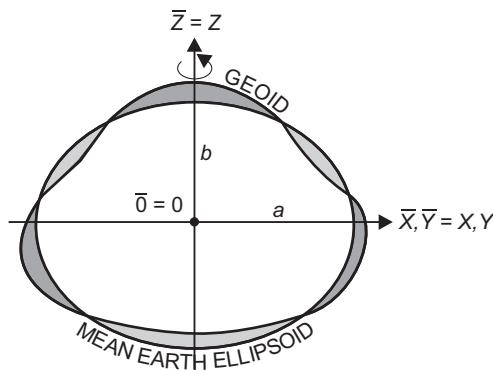


Fig. 7.6: Mean Earth ellipsoid.

stations often were established at distances of a few 100 km in order to control the error propagation through the network with respect to scale and orientation (effects of lateral refraction). More recently, the ellipsoid parameters of a geodetic reference system have been introduced, cf. [4.3], and the ellipsoid has been optimally fitted to the geoid, Fig. 7.6. Tab. 7.2 lists the ellipsoids and the origin points used for some geodetic datums (NIMA, 2000).

Tab. 7.2. Reference ellipsoids and origin points of some geodetic datums

Geodetic datum	Reference ellipsoid	Name of origin	Origin	
			Latit.	Longit.
Australian Geodetic 1984 (AGD84)	GRS67	Johnston	-25°57'	133°13'
Deutsches Hauptdreiecksnetz (DHDN), Germany	Bessel 1841	Rauenberg/Berlin	52°27'	13°22'
European Datum 1950 (ED50)	Intern. Ellipsoid 1924	Potsdam, Helmerturm	52°23'	13°04'
Indian	Everest 1830	Kalianpur	24°07'	77°39'
North American 1927 (NAD27)	Clarke 1866	Meades Ranch, Kansas	39°13'	261°27'
North American 1983 (NAD83)	GRS80	Geocentric		
Ordnance Survey of Great Britain 1936 (OSGB36)	Airy 1830	Herstmonceux	50°52'	0°21'
Pulkovo 1942, former Soviet Union	Krassovski 1940	Pulkovo	59°46'	30°20'
South American 1969 (SAD69)	GRS67	Chua, Brazil	-19°46'	311°54'

The following description of the triangulation networks established in *North America* and *Europe* illustrates the development of regional horizontal control systems, and the primary triangulation of *Germany* serves as an example for a local solution.

The horizontal control network of the U.S.A. was constructed by triangulation chains with mesh sizes of about 500 km. Nodal nets with baselines and Laplace azimuths were established at the junctions of the chains and treated as constraints in the adjustment, and areal networks later filled the meshes. A conventional ellipsoid (Clarke, 1866) was introduced, with the orientation obtained from the minimum condition for vertical deflections (7.1): *North American Datum 1927* (NAD27), see Tab. 7.2. This system has been replaced by the *North American Datum of 1983* (NAD83), implemented as legal datum in 1986. NAD83(1986) combines the horizontal control networks of the U.S.A., Canada, Greenland, Mexico, and Central America by a rigorous adjustment (Schwarz and Wade, 1990), Fig. 7.7. The observations include terrestrial data (horizontal directions, azimuths, distances), Doppler stations (for large-scale control and reference to the geocenter), and VLBI baselines (for scale and orientation). The adjustment (about 1.8 million observations and 300 000 points) was performed by Helmert-blocking (Wolf, 1978) and utilized a height-constrained 3D procedure, cf. [6.2] (Vincenty, 1982). The two-dimensional results refer to the Geodetic Reference System 1980, with a geocentric position accurate to about 2 m. The relative station uncertainty is a few cm to a few dm for distances between 10 and 300 km (Snay, 1990). NAD83 (1986) has been superimposed by GPS positioning since the end of the 1980s, and local readjustments of GPS and terrestrial data led to numerous state and regional High Precision Geodetic Networks (HPGNs), in addition to a continuously operating GPS network. This led to a recomputation as a 3D network, and a new realization of the horizontal datum within the National Spatial Reference System: NAD83 (NSRS2007), cf. [7.3].

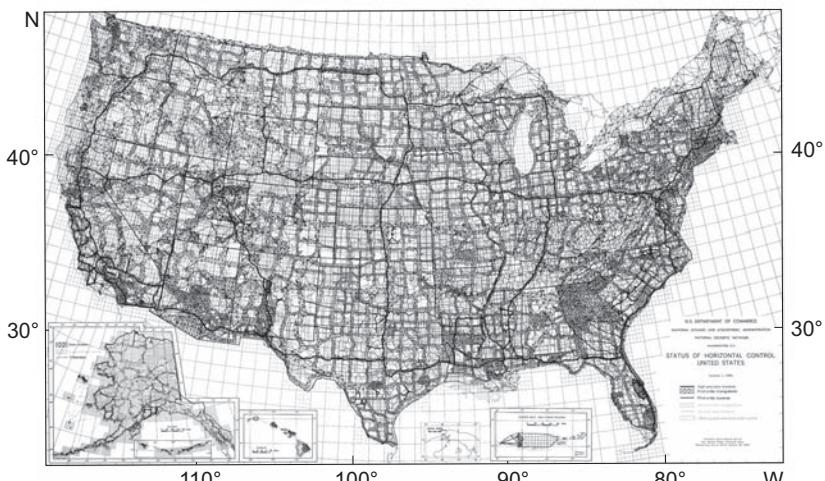


Fig. 7.7: Horizontal control network of the U.S.A. (NAD83), with first- and second-order triangulation, and traverses, courtesy National Geodetic Survey, National Ocean Service, NOAA.

Since the 1950s, attempts have been made in Europe to unify the national triangulation networks, where the political separation forced to separate solutions for western and eastern European countries. In *western Europe*, a unified *European triangulation network* (RETrig) was developed, which started from a central European network formed by selected triangulation chains and later was augmented by blocks in the southwest, southeast, and north (Whitten, 1952): *European Datum 1950* (ED50), see Tab. 7.2. The International Ellipsoid 1924 served as the reference surface and was orientated by the minimum condition (7.1), which provided vertical deflection components ($\xi = 3.36''$, $\eta = 1.78''$) for the origin Potsdam, Helmert-Turm. The baselines, reduced to the geoid, indirectly provided the geoid height ($N = 0.4$ m) at the origin. A rigorous readjustment of all first-order triangulation nets was carried out later, including electromagnetic distance measurements, VLBI, satellite laser ranging, and Doppler observations: *European datum 1987* (ED87), Poder and Hornik (1989). Orientation was adopted from ED50, but parallelism of the axes and scale could be improved. While ED50 was introduced in several countries, and served as the NATO military system until the 1990s, no practical application was found for ED87. Extensive retriangulations took place in *eastern Europe* since the 1950s. They were connected to the horizontal control network of the former Soviet Union, which was based on extended triangulation chains. Calculations were performed on the Krassovski (1940) ellipsoid, with parameters and orientation derived from the minimum condition for vertical deflections (7.1), and the geoid height set to zero at the origin Pulkovo: *Pulkovo Datum 1942* (Izotov, 1959). Reductions to the ellipsoid became possible by observed and gravimetrically interpolated deflections of the vertical and quasigeoid heights from astrogravimetric leveling, cf. [6.7.4]. A readjustment of the Russian triangulation chains together with the first- and second-order networks of the eastern European countries delivered the last realization of this unified astrogeodetic "System 42" in 1983. Since the end of the 1980s, a new European Terrestrial Reference System (ETRS) has been defined, and realized through geodetic space techniques, cf. [7.3].

The primary triangulation net of *Germany*, developed since the 1870s, is an example of a local horizontal control network. The northwestern part, between the rivers Elbe and Main, was covered by triangulation chains and densification nets between 1870 and 1895 as part of the geodetic survey of Prussia. A conventional ellipsoid (Bessel, 1841) was introduced for the calculation and orientated by the condition (7.2) at the origin Rauenberg/Berlin, whereby the geoid height was fixed indirectly through the reduction of five baselines, one of them located near Berlin. The Laplace azimuth from Rauenberg to Berlin, Marienkirche provided the network's orientation on the ellipsoid. After the network adjustment, the ellipsoidal coordinates were calculated according to the development method. The eastern parts of Prussia and the triangulations of the southern German states were later tied to this "*Schreiber's block*" utilizing common points at the networks' margins: *Deutsches Hauptdreiecksnetz* (DHDN), see Tab. 7.2. In western Germany, the DHDN has been locally improved since the 1950s by additional horizontal directions and electromagnetic distance measurements, without changing the original datum. While the relative accuracy over some 10 to 100 km is at the dm order of magnitude, distortions up to 1 m have been found between different parts of the network. In eastern Germany, a complete retriangulation was carried out after 1950 and calculated within the common adjustment of the eastern European triangulations (see above): *Staatliches Trigonometrisches Netz 1942/1983* (STN42/83), Ihde und Lindstrom (1995). The DHDN90 thus consists of three blocks observed over a time span of more than 100 years with different orientation (Schmidt, 1995), Fig. 7.8. The sites of this classical first-order triangulation generally are included into the national geodetic base net being established by means of GNSS methods. The densification networks, on the other hand, probably will be maintained only partially within the frame of state-wide horizontal control, cf. [7.3].

Satellite positioning was employed early to control the quality of horizontal-control networks given in a local or regional datum, and to determine the *datum transformation* parameters with respect to the geocentric system, Ashkenazi et al. (1988). Equations (6.47) were used to calculate translation, rotation, and scale factor, using identical stations coordinated in the global system (especially in the WGS84) and in the local or regional geodetic datum (after proper transformation from geodetic to Cartesian coordinates). Tab. 7.3 provides mean values for translation, rotation, and scale factor for some geodetic datums, with reference to a geocentric system.

Translations are at the order of magnitude of the deflections of the vertical. They are larger when conventional ellipsoids have been used and decrease with best-fitting ellipsoids. The rotation angles mirror the accuracy of the astronomic observations and are usually not significant. While the scale errors for older networks reach 10^{-5} and more, they attain only 10^{-6} and less in recent systems, characterizing the progress in length determination. The results strongly depend on the number and distribution of the identical points. Due to network distortions, datum-shift values for a limited area may differ significantly from the mean values of a national reference system given above, e.g., by 10 to 20 m and more for the translation parameters, and 10^{-6} and more for

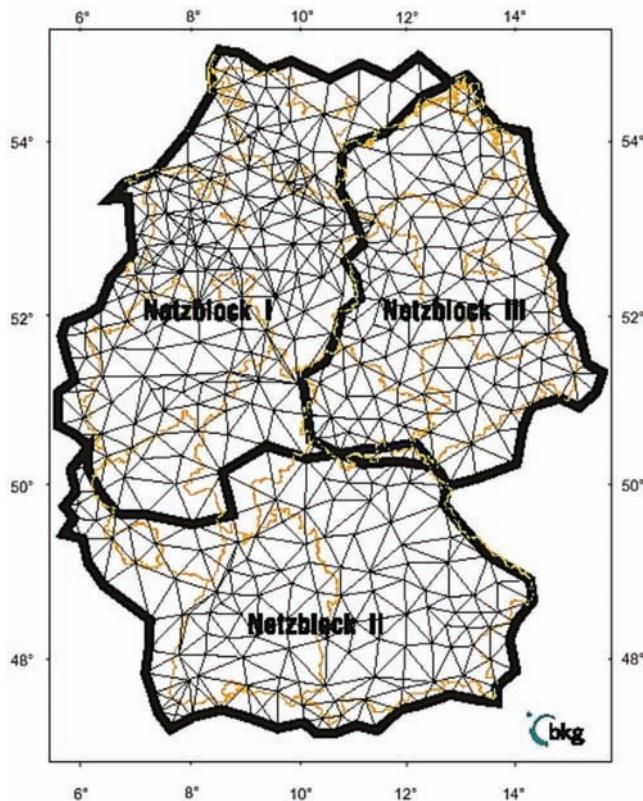


Fig. 7.8: Primary triangulation net of Germany (DHDN90), courtesy Bundesamt für Kartographie und Geodäsie (BKG), Frankfurt a.M., Germany.

Tab. 7.3. Translation, rotation, and scale factors (mean values) for some geodetic datums with reference to the geocentric system (DMA, 1987; NIMA, 2000), for DHDN and Pulkovo 1942 from Ihde and Lindstrom (1995)

Geodetic Datum (see Tab. 7.2)	7-Parameter-Transformation						3-Parameter-Transf.			
	Translation (m)			Rotation (arcsec)			Scale factor	Translation (m) only		
	X_0	Y_0	Z_0	$\varepsilon_{\bar{X}}$	$\varepsilon_{\bar{Y}}$	$\varepsilon_{\bar{Z}}$	$m \times 10^6$	X_0	Y_0	Z_0
AGD84	-127	-50	153	0.0	0.0	-0.1	1.2	-134	-48	149
DHDN	582	105	414	-1.0	-0.4	3.1	8.3			
ED50	-102	-102	-129	0.4	-0.2	0.4	2.5	-87	-98	-121
Indian	227	803	274	-0.4	-0.6	-0.4	6.6	295	736	257
NAD27	-4	166	183	-0.3	0.3	-0.1	0.4	-8	160	176
OSG36	446	-99	544	-0.9	-0.3	-0.4	-20.9	375	-111	431
Pulkovo 42	24	-123	-94	0.0	0.2	0.1	1.1	28	-130	-95
SAD69	-56	-3	-38	0.1	-0.6	-0.2	-0.6	-57	1	-41

Remark: Pulkovo42 7-Parameter-Transformation values are valid for eastern Germany, while 3-Parameter-Transformation values are valid for Russia.

the scale factor. As an example, a scale difference of nearly 3×10^{-6} has been found between the central and the southern part of DHDN/Germany. If a 3-parameter solution (translation only) is carried out, the translation values of older networks may experience considerable changes.

The *transformation* from a local/regional geodetic datum to the geocentric system can be done either by a complete readjustment including spatial observations (example: NAD83) or by transformation, the latter method being less laborious. Again, the transformation equations (6.47) are used, introducing either mean datum-shift parameters or (better) parameter values modeled as a function of position, e.g., as low-order polynomials. Corresponding parameter values or models are provided by the responsible agencies (e.g., by BKG Frankfurt a.M. for the transformation from the European national systems to ETRS89: <http://www.crs-geo.eu>), or they can be calculated together with the changes of coordinates. Residual differences between the two sets of coordinates may be determined also by refined transformation methods, e.g., by least-squares prediction, cf. also [7.3].

Of special interest is the datum transformation of *ellipsoidal (geodetic) coordinates*, which includes the transition from a conventional or best-fitting ellipsoid to a geocentric one. From (6.49) we obtain the corresponding changes which occur in the ellipsoidal latitude, longitude, and height. Restricting ourselves to a spherical approximation and neglecting the (small) rotations and change of scale, we get (ellipsoidal formulas are given by DMA, 1987 and Ehlert, 1991):

$$\left. \begin{aligned} a\Delta\varphi &= -\sin\varphi \cos\lambda X_0 - \sin\varphi \sin\lambda Y_0 + \cos\varphi Z_0 + a\sin^2\varphi\Delta f \\ a\cos\varphi \Delta\lambda &= -\sin\lambda X_0 + \cos\lambda Y_0 \\ \Delta h &= \cos\varphi \cos\lambda X_0 + \cos\varphi \sin\lambda Y_0 + \sin\varphi Z_0 - \Delta a + a\sin^2\varphi\Delta f \end{aligned} \right\}. \quad (7.4a)$$

Here, the sign of the translation vector

$$\mathbf{X}_0 = \begin{vmatrix} X_0 \\ Y_0 \\ Z_0 \end{vmatrix} = \begin{vmatrix} X - \bar{X} \\ Y - \bar{Y} \\ Z - \bar{Z} \end{vmatrix} \quad (7.4b)$$

has been changed (reduction!). All differences are formed in the sense “geocentric – local system”, resulting in the transformation

$$\begin{aligned} \varphi &= \bar{\varphi} + \Delta\varphi, & \lambda &= \bar{\lambda} + \Delta\lambda, & h &= \bar{h} + \Delta h \text{ and} \\ a &= \bar{a} + \Delta a, & f &= \bar{f} + \Delta f. \end{aligned} \quad (7.4c)$$

Again, the changes in φ , λ , h can be modeled and demonstrated in contour charts, provided a sufficiently large number of identical points have been used. The accuracy of these transformations depends on the area under investigation and the number of points available in both systems. A few m accuracy has been achieved for continent-wide geodetic systems, and residuals of a few cm may be obtained at well surveyed local networks.

7.2 Vertical control networks

Traditionally, national vertical control networks have been established separately from horizontal control nets. This is due to the demand that heights have to be defined with respect to the gravity field and a corresponding reference surface (e.g., geoid, quasi-geoid) rather than to the ellipsoidal system used for horizontal positioning.

Vertical control networks are surveyed by *geometric* (also spirit or differential) *leveling* and occasionally also by hydrostatic leveling, cf. [5.5.4], the control points being designated as *bench marks*. According to the leveling procedure and the accuracy achieved, national geodetic surveys distinguish between different orders of leveling. First-order leveling is carried out in closed loops (loop circumferences of some 100 km) following the rules for precise leveling. An accuracy of $0.5 \dots 1 \text{ mm}\sqrt{s}$ (km) is achieved at double-run leveling (s is the length of the leveled line), but systematic effects may lead to error accumulation over long distances. The loops are composed of leveling lines connecting the nodal points of the network (Fig. 7.9). The lines, in turn, are formed by

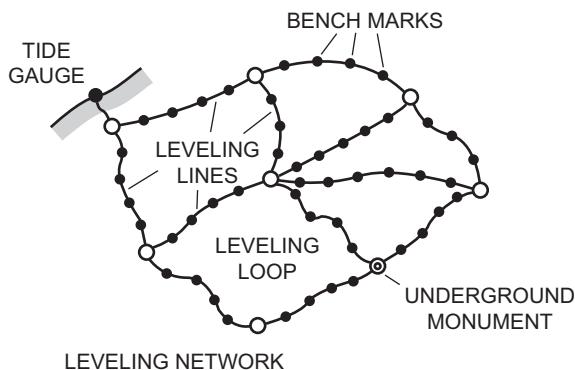


Fig. 7.9: Leveling network (principle).

leveling runs that connect neighboring benchmarks (average spacing 0.5 to 2 km and more). The first-order leveling network generally is densified by second to fourth-order leveling, with diminishing demands on accuracy.

Leveling lines generally follow main roads, railway lines, and waterways. The benchmarks consist of bolts in buildings, bedrock, or on concrete posts. Long pipes have been set up in alluvial regions. Underground monuments are established in geologically stable areas in order to control the network stability with respect to variations with time. First-order networks should be reobserved at time intervals of some 10 years, as regional and local height changes can reach one mm/year and more, especially in areas which experience vertical crustal movements of tectonic, isostatic or man-made origin, cf. [8.3.4].

Prior to the adjustment of a leveling network, the observed raw height differences have to be transformed either to geopotential differences or to differences of normal or orthometric heights by taking *surface gravity* into account, cf. [6.4.1]. The adjustment then utilizes the loop misclosure condition of zero and is carried out either by the method of condition equations or, preferably, by the method of parameter variation.

First-order leveling networks were established in many countries between the 1860s and the 1950s when surface gravity along the leveling lines was not known. Hence, gravity reductions were either neglected completely or actual gravity was approximated by normal gravity, leading to *normal* or *spheroidal* orthometric heights. These path-dependent heights may differ from normal or orthometric heights by some mm (flat terrain) to some dm (mountains). Today, surface gravity along the leveling lines is generally available by measurement or prediction, and can be taken into account.

The *vertical datum* of a national height system generally is defined by mean sea level (MSL) as derived from tide gauge records. The *zero height surface* running through the defining MSL depends on the choice of the height system, and is either a level surface close to the geoid (orthometric heights) or the quasigeoid (normal heights). In future, high-resolution geoid or quasigeoid models may also serve for the definition of the vertical datum, again being realized through the heights of fundamental bench marks. If based on MSL from *different* tide gauges, national height systems may differ by some dm to one m and more, between each other and from the geoid as a global reference surface. This is due to the effect of sea surface topography, which additionally causes network distortions if the vertical datum is constrained to MSL of more than one tide gauge, cf. [3.4.3].

Estimates of the differences between the vertical datum of different height systems are available from satellite positioning and global geoid models and from continent-wide leveling connected to tide gauges (Rapp, 1995b). For instance, the zero height surface of the North American Vertical Datum of 1988 is about 0.5 m below MSL at Amsterdam. In Europe, the national vertical datums have been derived from MSL records in the Mediterranean Sea, the North Sea, and the Baltic Sea. Taking the mean sea level in Amsterdam (used, e.g., in the Netherlands, in Germany, and in the European leveling net) as reference, MSL in Kronstadt (near St. Petersburg, Russia) is about 15 cm higher, and zero-height surfaces derived from tide gauge records along the Mediterranean Sea are about 0.4 to 0.5 m lower (Sacher et al., 1999).

We now shortly describe the development of the *North American* and the *European* leveling networks, as well as the *German* height system, being examples for classical regional and local vertical control nets.

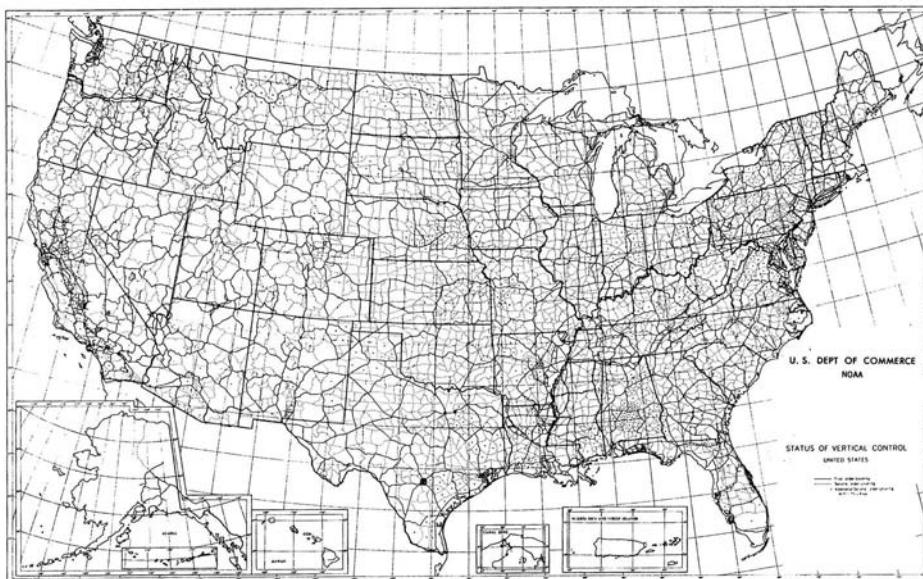


Fig. 7.10: NAVD 88 leveling network, from Zilkoski et al. (1995).

Geodetic leveling in the *United States* began in the middle of the nineteenth century, and a first network adjustment was performed in 1900. The adjustment of more than 100 000 kilometers of geometric leveling from the U.S.A. and from Canada provided the *National Geodetic Vertical Datum of 1929* (NGVD29). Being constrained to the MSL of 26 tide gauges, network distortions of 50 cm and more thus have been introduced into the results. After replacing destroyed bench marks and extensive re-leveling, a new adjustment of the leveling data of the U.S.A., Canada and Mexico was started in the 1970s, and resulted in the *North American Vertical Datum of 1988* (NAVD88). The adjustment included more than 700 000 bench marks and was carried out in geopotential numbers, employing the Helmert-blocking technique. Heights are given as orthometric heights according to Helmert, see (6.84), and refer to MSL of now only *one* primary bench mark (Father Point, Rimouski, Quebec, Canada), Zilkoski et al. (1995). A national height modernization program is underway which will utilize an up-to-date regional gravitational geoid model, on the one hand, and a geoid model fitted to GNSS/NAVD88 control points, on the other, for defining a vertical datum suitable for GNSS techniques.

The *United European Leveling Net* (UELN) has been formed by first-order leveling lines of the European countries. Several re-adjustments have been carried out since 1954, with continuous quality improvement and network extension, the latest one being UELN95/98 (Fig. 7.11). The adjustments are performed in geopotential numbers, and normal heights are derived. The average accuracy of the leveling is about $1.1 \text{ mm } \sqrt{s} (\text{km})$, and the standard deviations related to the datum point Amsterdam remain less than 0.1 m. The vertical datum is taken from MSL of the North Sea as determined in the period 1940 to 1958 at Amsterdam (Normal Amsterdamsch Peil NAP of 1950). The UELN is connected to a large number of tide gauges, which permits determination of sea surface topography around Europe, in addition to the datum differences between national vertical reference systems (see above). UELN represents the basis of the European Vertical Reference System (EVRS), which by combination with GNSS heights is embedded in the spatial reference system ETRS, cf. [7.3], Ihde et al.

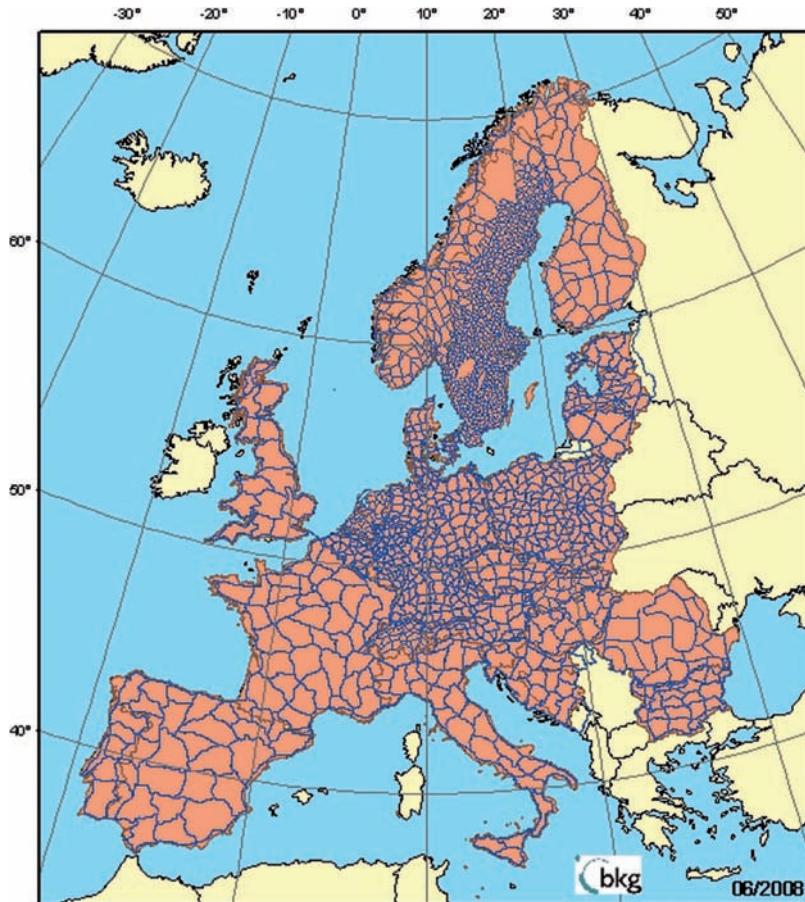


Fig. 7.11: United European Levelling Net (status 2008), courtesy BKG, Frankfurt a.M., Germany.

(2002). The latest realization of this integrated system is the reference frame EVRF2007, calculated in the zero-tide system. The datum of the UELN has been kept as good as possible by introducing the previous heights of 13 "datum points", assumed to be not affected by temporal variations. Leveling data from the northern European land uplift area have been reduced to epoch 2000. In future, UELN will be extended to a kinematic height system by including vertical point velocities (Sacher et al., 2008).

First-order leveling in *Germany* started state-wide around 1865 and finally led to a national height system calculated from the raw leveling data, with the leveling of Prussia as the core network. The vertical datum was derived by connection to the Amsterdam normal tide gauge, representing mean high tide for the period 1683/1684 (Waalewijn, 1986). The zero height surface (*Normal-Null*, N.N.) was fixed by a standard bench mark, established 37.000 m above N.N. at the former Berlin observatory and since 1912 by a set of underground marks. Complete re-surveys were carried out from 1912 to 1960 and from 1980 to 1985 (only western Germany). These networks were adjusted as normal-orthometric heights: *Deutsches Haupthöhenetz* (DHHN). In eastern Germany, re-leveling was performed in the 1970s and adjusted as normal heights within the frame of the eastern European height system, where the vertical datum was

taken from MSL at the tide gauge in Kronstadt near St. Petersburg: *Höhennull* (HN). Due to the different definitions of the vertical datum and the height system, systematic height differences between 8 and 16 cm were later found at the former boundary between western and eastern Germany. After 1990, a re-adjustment of the complete national network (loop diameter 30 to 80 km, more than 50 000 bench marks with mutual distance between 0.5 and 1.5 km) was carried out in geopotential numbers. The vertical datum is defined now by the geopotential number of the UELN86 nodal point Wallenhorst and thus refers to MSL at Amsterdam (see above): DHHN92, Fig. 7.12. Normal heights have been introduced as official heights, referring to the quasigeoid as reference surface: *Normalhöhennull* (NHN), Weber (1995). Recent modernization includes re-survey of most leveling lines and connection to existing GNSS-networks and absolute gravity stations, a dedicated DHHN-GNSS network comprising about 250 stations was established at the beginning of the twenty-first century.

Leveling networks are characterized by high accuracy, but systematic errors may accumulate over large distances. A severe handicap of classical leveling networks is the significant loss of benchmarks with time due to human activities, and the manifold height changes occurring at local and regional scales. Due to the time-consuming measurement procedure, repetition or restoration surveys are feasible only after longer time intervals, which leads to a rapid network decay. A more rapid establishment of vertical control networks has been achieved occasionally by trigonometric leveling, cf. [6.4.2], and a drastic change is now taking place by GNSS heighting in connection with high-resolution geoid or quasigeoid models, cf. [6.4.3]. In this way, vertical control networks are integrated in, and gradually substituted by 3D reference systems, cf. [7.3]. The time-consuming spirit leveling required for the establishment and maintenance of the classical vertical control networks may become mostly superfluous. On the other hand, geometric leveling will maintain

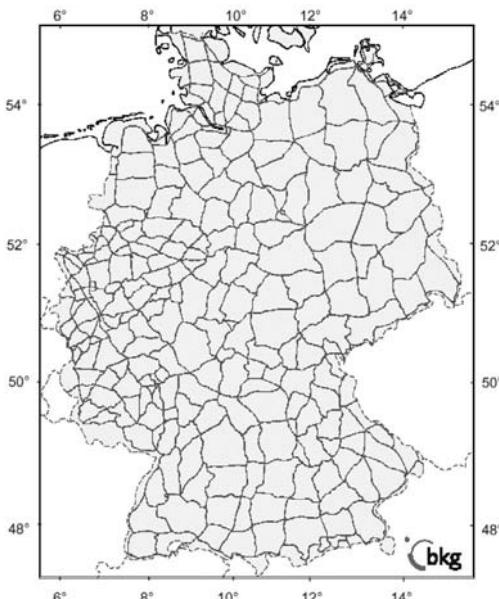


Fig. 7.12: Primary leveling network of Germany (DHHN92), courtesy BKG, Frankfurt a.M., Germany.

its importance over shorter distances, and especially in areas of recent crustal movements, such as regions of land subsidence and zones of Earthquake or volcanic activity, cf. [8.3.4].

7.3 Three-dimensional networks

Starting in the end of the 1980s, GNSS techniques have more and more entered into geodesy and are now primarily used at all scales for positioning and navigation, cf. [5.2.5]. This has led to a drastic change at the establishment and maintenance of geodetic control networks which are now definitely *3D* and based on satellites as system carriers.

Nowadays, the *global* geodetic reference is well established and provided by the *International Terrestrial Reference Frame* (ITRF) being the realization of the International Terrestrial Reference System. The ITRF stations are given with their 3D geocentric coordinates (cm-accuracy) for a certain reference epoch, and with corresponding horizontal velocities, cf. [2.4.2]. The *International GNSS Service* (IGS) provides a powerful contribution to the ITRF and serves for densifying this global reference frame, cf. [5.2.5]. A multitude of GNSS surveys has already densified or will in future densify this global reference frame, superseding the classical control networks. This process happens at local, regional or continent-wide dimensions, and has triggered a new definition and realization of national and supra-national geodetic reference systems, and strategies for integrating the existing control nets.

Immediately following the development of geodetic GPS and other GNSS methods, *continent-wide* (supra-national) and *national* 3D networks were established. Although a more or less homogeneous station-coverage is generally the goal, the distances between the observation sites in reality vary considerably. The station distribution depends, among others, on topography and on the state of economic development, and station distances consequently range from a few ten to some 100 km and more. At least three stations per country have been often selected as a reference for further densification and for the transformation of existing control networks, cf. [7.1]. The *station sites* are selected according to the requirements of GNSS observations (no visibility obstructions between 5° to 15° and 90° elevation, absence of multipath effects, no radio wave interference), cf. [5.2.5]. Generally the stations are monumented by concrete pillars, providing a forced centering for the GNSS antenna and a height reference mark. Eccentric marks are established in order to locally control horizontal position and height, and underground monuments are beneficial for the long-term preservation of the network. Existing first- and second-order control points may be used if they fulfill the GNSS requirements, otherwise the GNSS stations should be connected to the existing control networks by local surveys.

Although the strategies for establishing and maintaining these GNSS based reference networks differ, the following directions clearly can be identified:

- establishment of a large-scale (continent-wide, national) fundamental three-dimensional network by GNSS campaigns, with proper system definition and connection to the International Terrestrial Reference Frame,
- installation of a network of permanent GNSS stations,

- densification of the fundamental network by GNSS methods,
- transformation of existing classical horizontal control network into the three-dimensional system,
- connection of the 3D-reference system to the vertical control and gravity reference systems.

Dedicated *GNSS campaigns* are carried out for the determination of the 3D-coordinates of the network stations, employing relative positioning, cf. [5.2.5]. This strategy requires the inclusion of at least one reference station with coordinates given in the ITRF, but generally all ITRF and IGS stations (or control stations of a continent-wide reference system) in the survey region are introduced as reference (“fiducial”) stations. Depending on the number of stations and available GNSS receivers (two-frequency geodetic type), either all stations are observed simultaneously or the network is divided into blocks that are observed sequentially (Fig. 7.13). All observations made simultaneously during a given time interval are called a “session” (Snay, 1986). The duration of one session is between 8 and 24 h, which permits determination of the ambiguity unknowns and a simultaneous solution for the station coordinates and tropospheric correction parameters (“multi-station” adjustment). The results of *one* session are highly correlated. Consequently, two or more sessions are generally carried out, leading to a total observation time of some days to one week. A “multi-session” adjustment then combines the results of several sessions. Optimization methods have been developed and may be employed for network planning and survey (Dare and Saleh, 2000).

By referencing the network to IGS stations and applying the IGS precise orbital data, the effect of reference station and orbital errors on the station coordinates is only at the few mm level. When different type GNSS receivers are employed in one campaign, corrections have to be applied for antenna phase-center differences. In addition, phase-center variations have to be taken into account by calibration (Seeber et al., 1998). Longer observation periods increase the accuracy of the results, due to the changing satellite geometry and the reduction of residual tropospheric, multipath, and antenna effects. This is especially valid for the height component, where small satellite elevations improve the geometry of the solution but introduce larger tropospheric errors. *Accuracies* of 1 cm and better are achieved now for the adjusted horizontal coordinates of fundamental network stations, and heights can be determined with an accuracy of 1 to 2 cm.

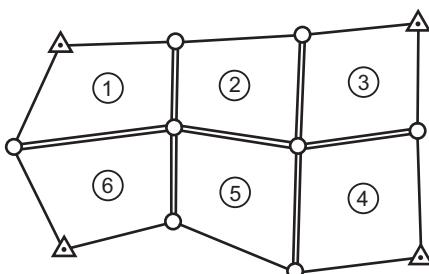


Fig. 7.13: GNSS network constructed from individual blocks (principle).

Following the ITRF strategy, *reference epochs* are defined for the final station coordinates of the fundamental networks, which may differ from the epoch of the ITRF stations introduced and from the time of the observation campaign. Consequently, reductions have to be applied which take the station velocities between the different epochs into account.

Permanent GNSS networks have increasingly been established since the 1990s at regional and local scales. They consist of “active” GNSS stations, equipped with geodetic GNSS receivers that continuously track all visible GNSS satellites with a high data rate (e.g., 1 s). Station distances vary considerably, ranging from about 100 km to a few 100 km at continent-wide networks, and 30 to 100 km and more at national systems. Undisturbed visibility to the satellites is achieved by installing the antennas several m to 10 m above the ground on concrete pillars, steel grid masts, etc., or on the top of buildings. Permanent networks represent a continuous realization of the underlying supra-national or national geodetic reference system, thus serving for maintenance and for control of variations with time due to recent crustal movements. They represent a reference for all types of GNSS surveys carried out within the permanent network area, by making available the raw GNSS tracking data (code and carrier phase measurements) for the “reference” station of a “baseline”, Fig. 7.14. More sophisticated “Satellite Positioning Services” exploit the known geometry of the stations’ array to determine the ambiguities and to calculate baseline corrections for ionospheric, tropospheric, and orbit effects. Together with the station coordinates this allows the application of differential GNSS methods with a single receiver (Wanninger, 2000). Real-time positioning with “baselines” is possible with cm-accuracy, and post-processing with long observation series may achieve a few mm precision, see below and [5.2.5], [6.2.1].

After the establishment of a national 3D geodetic reference frame, relative GNSS-positioning can be employed also for *network densification*. While the fundamental network may be constructed with station distances of several 10 km (corresponding to the first-order trigonometric points), densification nets with distances down to 10 km (former second-order triangulation) may be useful for larger countries. The relative mode again requires two or more receivers and the connection to reference stations. If a network of permanent GNSS stations as realization of the national reference frame is available (telemetry data transfer to the users), differential GNSS methods can be applied. For short (few to 10 km) baselines, a relative cm-accuracy can be achieved

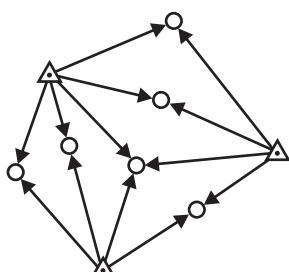


Fig. 7.14: GNSS network constructed from baselines to permanent GNSS stations (principle).

in quasi real-time after proper ambiguity solution. For longer baselines, the results are degraded by the distance-dependent errors of GNSS, and have to be improved by the corrections provided by the permanent network's positioning service.

With *Precise Point Positioning* (PPP), an alternative to the relative method of DGNSS has been developed and could also be used for the establishment of geodetic 3D control networks (Zumberge et al., 1997; Ebner and Featherstone, 2008). This absolute method evaluates undifferenced dual-frequency pseudorange and carrier phase observations obtained with only one receiver, along with IGS precise orbits and satellite clock corrections in one mathematical model, for estimating station coordinates, tropospheric zenith path delays, receiver clock corrections, and ambiguities (Kouba and Héroux, 2001). Network adjustments (post-processing) of extended observation series (up to 24 h) deliver cm-accuracy for position, and clock corrections at the 0.1 ns level. The method can be extended by taking current corrections into account derived from a regional or local RTK (real-time kinematic) network. This strategy allows an immediate determination of carrier phase ambiguities, and delivers quasi-real-time cm-accuracy (Wübbena et al., 2005).

By connecting the 3D GNSS network to first- and second-order trigonometric points, the existing classical horizontal control networks can be *transformed* into the three-dimensional reference frame. A minimum of three identical points with coordinates given in both systems is required for a 7-parameter transformation, which may suffice for homogeneous networks of high precision, cf. [7.1]. Additional GNSS control points are needed if the classical networks contain larger distortions; the selection of these points depends on the network peculiarities, and usually more sophisticated transformation models will be necessary, including polynomial, least-squares, or spline approximation (Moritz, 1978). In this way, the local cm-accuracy of classical networks can be kept, and the effect of the network distortions can be reduced to the order of a few cm to dm over distances of some 10 to 100 km. After the completion of the transformation to a 3D reference frame, the classical horizontal networks of lower order generally will no longer be maintained.

Space-geodetic and especially GNSS methods also give reason for a change with respect to the definition and realization of *vertical reference systems*. This is due to the fact that space-based techniques allow the determination of ellipsoidal heights with an accuracy comparable with the accuracy of spirit leveling, at least at distances larger than a few ten kilometers, cf. [6.4.3]. By combining with high-resolution global or local geoid/quasigeoid models, cf. [6.6], [6.7], another method for determining gravity-field related heights thus is available. This forces the incorporation of the classical vertical control networks into the 3D reference frame. By including first-order leveling benchmarks and tide gauges in the 3D network, the differences between the ellipsoidal heights and the heights of the national height system can be determined at selected points, i.e., the geoid or quasigeoid heights. These GNSS/leveling control points allow the national height system to be fitted to a regional geoid or quasigeoid model, and they can be used to derive gravity-field related heights (orthometric heights, normal heights) for all three-dimensional reference stations. The vertical datum may be even defined by a global or regional geoid/quasigeoid model, with corresponding reductions of the heights given in the classical height system. The *vertical control points* now are an integrated part of the 3D reference frame, evenly distributed over the respective continent or nation and not

restricted to the leveling lines. With increasing accuracy of the geoid resp. quasigeoid-“reduction” of GNSS heights, the application of geometric leveling will be reduced to more local problems where mm-accuracy is required, cf. [7.2].

Finally, there is a tendency to also measure absolute gravity on the primary stations of a 3D reference frame. This will lead to fundamental geodetic control networks, providing 3D geodetic coordinates, gravity potential (and related height) and gravity for a certain epoch, and (as far as possible) corresponding long-term variations with time.

Some examples for the transition from the classical geodetic control networks to reference frames embedded in the global 3D system are given in the following, with the continent-wide reference systems introduced in the U.S.A., in South and Central America, and in Europe, and with the spatial reference frame established in Germany.

Since the 1980s, GPS-based methods rapidly entered into surveying and navigation in the U.S.A. Numerous adjustments of new GPS and existing terrestrial data led to a number of state High Precision Geodetic Networks (HPGN's), with a local accuracy of around 5 cm, but consistency problems across state lines. In addition, a Continuously Operating Reference Station (CORS) network was established in the mid-1990s by NGS, which is now operating with about 1600 stations in the U.S.A., its territories and a few foreign countries, Fig. 7.15. Based on the contributions of over 200 different institutions, CORS provides GNSS data consisting of carrier phase and code range measurements in support of 3D positioning, and allows a few cm-accuracy. These drastic changes triggered the establishment of a *National Spatial Reference System* (NSRS), superimposing or integrating the previous horizontal and vertical survey control. Consequently, a re-adjustment of horizontal positions and ellipsoidal heights for GPS stations in the contiguous United States was carried out, holding the CORS coordinates fixed (ITRF geocentric datum!) and including only GPS measurements. ITRF- and NAD83-related



Fig. 7.15: CORS station equipped with a Trimble Zephyr Geodetic Antenna, El Paso, TX, U.S.A., courtesy NGS (<http://www.ngs.noaa.gov/CORS>).

coordinates NAD83(NSRS) have been produced, where the latter experienced changes of 0.2 to 1 m relative to NAD83(1986), Pearson (2011).

In South America, a continent-wide densification of the ITRF started in 1995, and was later extended to Central and North America: *Sistema de Referencia Geocéntrico para las Américas* (SIRGAS). The system has been first realized through two measuring campaigns (1995, 2000), where simultaneous GPS observations over 10 days were carried out on some 60 resp. 200 stations well distributed over the sub-continent and the whole hemisphere, respectively; positions were calculated in ITRF2000 (Drewes et al., 2005). Since 2000, the continuously operating network (SIRGAS-CON) represents a third realization of this system, which is well connected to the global IGS net (Fig. 7.16.). It provides weekly solutions for the station positions and multi-annual solutions which contain linear station velocities, cf. [8.3.4]. SIRGAS also serves as a basis for the national reference frames recently established through GPS measurements, and for the transformation of the classical horizontal control networks in South America (generally given in the South American Datum 1969) into the global reference system (Sanchez and Brunini, 2009). A dedicated SIRGAS GPS campaign was carried out in 2000 which included leveling benchmarks and tide gauges, in order to

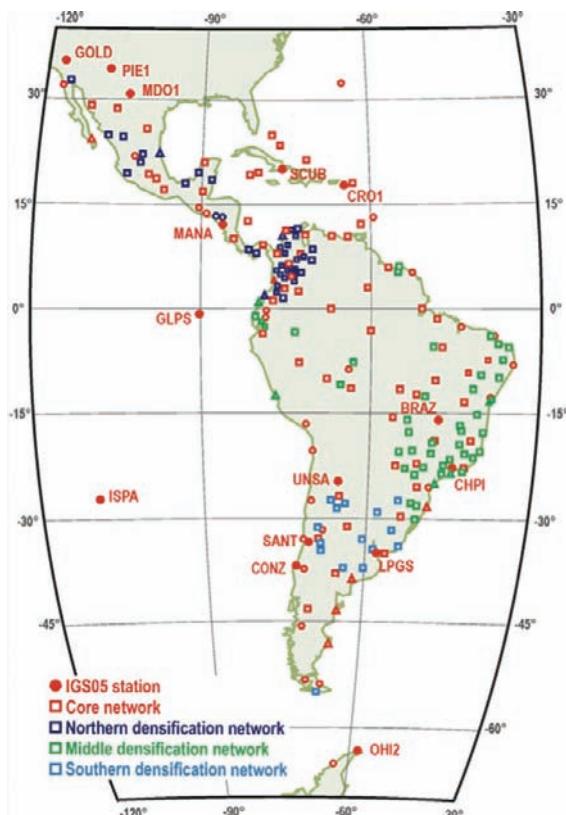


Fig. 7.16: Reference frame SIRGAS-CON, station distribution (status 2010), courtesy DGFI München.

derive a unified height system for South America. This system shall be defined by a geoid potential value (national vertical datums now deviate by 0.5 m and more from a common MSL) and realized by the geopotential numbers of the control points, based on SIRGAS ellipsoidal heights and a geoid model, as well as on readjustments of the existing national height networks (Sanchez, 2007).

A *European Reference Frame* (EUREF) has been built up since the end of the 1980s, as realization of the European Terrestrial Reference System 1989 (ETRS89). This system is defined through the coordinates (1989.0) of the ITRF89 stations located on the “stable” (i.e., moving with the same plate velocity) part of the European tectonic plate, which allows the frame to remain unchanged over a longer time interval. ETRS was first realized through the European Terrestrial Reference Frame 1989 (ETRF89), and continuously extended over the continent. The station positions were determined by successive GPS campaigns that included ITRF and IGS stations and generally included several countries. With ETRF2000 the network now covers nearly all of Europe, with station distances between 100 and 500 km or more. Of special relevance is the EUREF Permanent Network (EPN) comprising more than 200 stations with continuously observing dual-frequency GPS and GPS/GLONASS receivers (Fig. 7.17). Providing hourly data, EPN contributes to IGS and densifies it (Torres et al., 2009).

A *European Unified Vertical Network* (EUVN) is under construction, and integrated into EUREF. The network now comprises about 200 stations determined since 1997 by dedicated GPS campaigns using one-week observation time. It includes EUREF sites, nodal points of the European leveling net UELN, tide gauges, and a number of permanent GNSS stations, with 3D coordinates, geopotential numbers and normal heights. EUVN thus will serve (at a few-cm accuracy level) to unify the different European height systems, and provide fiducial points



Fig. 7.17: EUREF Permanent Network tracking stations (status 2012), courtesy C. Bruyninx EPN Central Bureau, Observatoire Royal de Belgique (http://www.epnrb.oma.be/_trackingnetwork/).

in order to fit the European quasigeoid, cf. [6.4.3], to a unified European height system. By extension to a kinematic height system, EUVN shall be used for monitoring large-scale vertical crustal movements and sea level changes (Kenyon et al., 2000).

In Germany, a 3D network related to ITRF and EUREF stations was established in 1991: Deutsches Referenznetz 1991 (DREF91). The network stations are mostly co-located with first- or second-order trigonometric points. The integration of DREF into the European reference frame is realized through the German Geodetic Reference Net (GREF), being part of the European GNSS Permanent Net and of IGS. Operated by BKG, it contains about 30 permanent stations, with an accuracy of 5 mm in position and 10 mm in height, Fig. 7.18. The Satellite Positioning Service (SAPOS) of the State Survey Agencies breaks this DREF/GREF reference frame down to the state level. SAPOS is based on about 260 GPS reference stations (average distance 50 km, accuracy 1 cm), well distributed over the German states (Hankemeier et al., 1998), Fig. 7.19, Fig. 7.20. It serves for differential GNSS positioning by providing range corrections for real-time code or carrier phase measurements (meter- resp. cm-accuracy), and raw observation data for post-processing (sub-cm accuracy).

With respect to further network densification and connection to existing control nets, the German state survey agencies went different ways. This led to a strategy for the development of a unified geodetic spatial reference in Germany (AdV, 2006). According to this planning, the spatial reference shall consist of the geodetic base net and the SAPOS reference stations both defined in ETRS89, the first-order vertical control points given in DHHN92, cf. [7.2], and the gravity control points given in DHSN96, cf. [7.4]. The base net stations shall have a maximum distance of 30 km which corresponds to the average distance of the classical first-



Fig. 7.18: German Geodetic Reference Net GREF (status 2009), courtesy BKG, Frankfurt a.M., Germany.



Fig. 7.19: Satellite Positioning Service (SAPOS) of the German State Survey Administration (status 2011), courtesy Landesbetrieb Geoinformation und Vermessung Hamburg (<http://www.hamburg.de/sapos>).



Fig. 7.20: SAPOS permanent GNSS station, courtesy Landesbetrieb Geoinformation und Vermessung Hamburg (<http://www.hamburg.de/sapos>).

order triangulation points, and well marked with respect to horizontal position and height. They shall be determined by geodetic satellite methods, precise leveling, and gravity measurements, with accuracy demands corresponding to the requirements for GREF, DHHN92, and DHSN96. Lower-order trigonometric control networks will be under the responsibility of the state survey administrations, and generally maintained only at a reduced level.

7.4 Gravity networks

Gravity networks provide the frame for gravimetric surveys on global, regional, or local scales. They consist of gravity stations where gravity has been determined by absolute or relative methods. On a global scale, the gravity standard has been realized by the *International Gravity Standardization Net 1971* (IGSN71), but *absolute gravimeters* now allow an independent realization, cf. [5.4.3].

National gravimetric surveys are based on a primary or *base network*, which in most cases is densified by lower-order nets. The gravity base network stations should be evenly distributed over the area, with station distances varying between a few 10 km to a few 100 km depending on the size of the country. The station sites should be (as far as possible) stable with respect to geological, hydrological, and microseismic conditions. They should be permanently marked, and co-location with geodetic base-stations is advisable. Eccenter sites may serve for securing the center station and for controlling local height and mass changes. Horizontal position and height of the gravity stations should be determined with m- and mm- to cm-accuracy, respectively. Subsequent gravimetric densification networks generally are co-located with horizontal and vertical control nets.

Absolute gravimeters generally are employed nowadays for the establishment of gravity base networks, partly in combination with relative gravity meters. Densification networks are observed primarily with relative instruments, cf. [5.4.1], [5.4.2]. *Relative* gravimeters need to be calibrated, and repeated measurements are necessary in order to determine the instrumental drift. The use of several instruments reduces residual systematic effects. Relative gravimetry requires at least one absolute station in order to derive the gravity "datum", and a calibration line for the control and improvement of the calibration factor. The establishment of gravity networks for *geophysical* and *geodynamic* investigations follows the same rules, but the distribution of the gravity stations is then determined by the geological structures or the geodynamic processes to be investigated, cf. [8.3.5]. The *accuracy* of primary gravity networks, established by absolute gravimeters or by a combination of absolute and relative gravimetry, is about $0.05 \mu\text{m s}^{-2}$ to $0.1 \mu\text{m s}^{-2}$; densification networks may be accurate to $0.1 \dots 0.5 \mu\text{m s}^{-2}$.

Gravity measurements on national scale started in the second half of the nineteenth century, triggered by growing demands from geodesy and geophysics. In the twentieth century, exploration geophysics and physical geodesy (geoid determination) became strong drivers for denser gravity field surveying, based on accurate and reliable gravity reference networks. These demands led in many countries to the establishment of gravity base networks, which continuously improved through progress in technology.

In the U.S.A., the Coast and Geodetic Survey and its successor, the National Geodetic Survey (NGS), carried out numerous gravity surveys during the second half of the twentieth century, generally within the frame of dedicated programs (statewide surveys, surveys along leveling lines, gravimeter calibration lines, etc.). A country-wide gravity network was established in 1976/1979 by LaCoste and Romberg gravimeters and constrained to the absolute standard. A running NGS absolute gravity program (jointly with NIMA Geospatial Sciences Division) is covering the country with a multitude of absolute gravity measurements (comprising now several hundred absolute gravity sites), serving as national gravity reference network and for the studies of vertical crustal movements, among others (Peter et al., 1989). In Canada, the primary control points of the Canadian Gravity Standardization Net will be replaced by the Canadian Absolute Gravity Array sites, co-located with GNSS reference sites (Fig. 7.21). Following previous

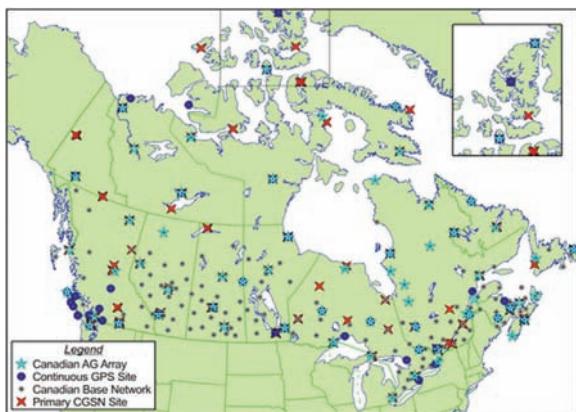


Fig. 7.21: Canadian Absolute Gravity Array and Base Network (status 2010), courtesy National Resources Canada Geodetic Survey Division (http://www.geod.nrcan.gc.ca/edu/gravi_e.php).



Fig. 7.22: Primary gravity net (red circles) of Germany (DHSN96), with German gravity base net (DSGN94) stations (blue circles), courtesy BKG, Frankfurt a.M., Germany.

repeated absolute gravity observations, regular resurveys of the array stations will contribute to the investigation of sea-level rise, post-glacial rebound, and tectonic deformation, cf. [8.3.5].

In *Germany*, gravity base networks and densifying networks were established since the 1930s, employing relative pendulum instruments and gravity meters, and tied to the Potsdam absolute gravity value. Absolute gravimetry was introduced in 1976/1977 in order to establish a combined absolute/relative base network in *western Germany* which was extended to *eastern Germany* and completely re-measured in 1994/1995: Deutsches Schwerergrundnetz 1994 (DSGN94). The network consists of 30 stations (one center and at least two eccentric points) that were observed with an absolute gravimeter FG5. Repeated observations and relative ties (several gravimeters of type LaCoste and Romberg and Scintrex) served for investigations of accuracy ($0.05 \mu\text{m s}^{-2}$) and reliability (Torge et al., 1999). A first-order densification net (average station distance 30 km) was observed with several relative gravimeters (1978–1982, 1994), Fig. 7.22. Further densification down to a few km has been realized or is in progress.

8 Structure and Dynamics of the Earth

As discussed in the previous chapters, geodesy covers the determination of the Earth's figure, its external gravity field, and its orientation in space, which results in time-dependent models for the geometry, the gravity field and the orientation of the Earth, see also [1]. As a part of the geosciences (geophysics including oceanography, hydrology and meteorology, geology, petrology, mineralogy, geochemistry and others), geodesy thus provides direct information or boundary conditions for the development of static and dynamic geophysical Earth models. These models, in turn, deliver significant information for the planning of geodetic networks and space missions, and for proper reduction of observations.

Global geophysical Earth models are mainly based on a radial structure of physical properties, and presuppose hydrostatic equilibrium [8.1]. These assumptions are not valid for the upper (and partly also for deeper) layers of the Earth, where geodynamic processes play an important role [8.2]. The contributions of geodesy to research in geodynamics are demonstrated by examples from Earth rotation variations, sea level changes, recent crustal movements, and temporal gravity changes [8.3].

From the extensive geophysical literature, we mention the classical work of Jeffreys (1970) and the textbooks by Fowler (2005) and Lowrie (2007). The interrelations between geodesy and geophysics have been treated early in Heiskanen and Vening-Meinesz (1958), see also Lambeck (1988) and Moritz (1990). For the state of geophysical data collection and parameter estimation, we refer to Ahrens (1995) and Grotens (2004).

8.1 The geophysical Earth model

Various observations show that the Earth does not posses a *homogeneous* structure:

- The *mass* M of the Earth as derived from the geocentric gravitational constant GM , cf. [4.3], and the constant of gravitation G , cf. [2.1], amounts to $M = 5.973 \times 10^{24}$ kg. With the volume of the Earth ellipsoid $1083 \times 10^{18} \text{ m}^3$, we obtain the *mean density*

$$\rho_m = 5.515 \times 10^3 \text{ kg m}^{-3}.$$

As the density of the Earth's crust only amounts to $2.7 \dots 2.9 \times 10^3 \text{ kg m}^{-3}$, density must increase toward the interior of the Earth.

- Astronomic and geodetic observations of the lunisolar precession, cf. [2.3.2], deliver the *dynamic* (mechanical) *ellipticity* (Fukushima, 2003):

$$H = \frac{C - \bar{A}}{C} = 3.2738 \times 10^{-3}, \quad \bar{A} = \frac{1}{2}(A + B). \quad (8.1)$$

A , B , and C are the equatorial and polar moments of inertia of the Earth, cf. [3.3.4]. With the *dynamical form factor* provided by satellite geodesy, cf. [4.3],

$$J_2 = \frac{C - \bar{A}}{a^2 M} = 1082.63 \times 10^{-6}, \quad (8.2)$$

we obtain the *moment of inertia* with respect to the *rotational axis*

$$C = 0.330\,701\,a^2 M.$$

If the Earth were a homogeneous sphere, we would have $C = 0.4\,a^2 M$. This again indicates a density increase with depth.

- Seismology shows that the Earth has a *shell-like* structure, with the shell boundaries being defined by discontinuities of the seismic waves velocities.

With the velocities of the seismic waves being known, and under the assumption of hydrostatic equilibrium, density, gravity, and pressure inside a spherically layered Earth model can be calculated as a function of the radial distance from the Earth's center of mass. Here, the assumption of hydrostatic pressure in the Earth's interior is justified by the fact that the Earth originally existed in a liquid state. In that case, the pressure depends only on the weight of the masses lying above, and it increases toward the center of the Earth.

Seismology determines the *velocities* of the primary (compression) and the secondary (shear) seismic waves, v_p and v_s . From these velocities the *seismic parameter*

$$\Phi = \frac{K}{\rho} = v_p^2 - \frac{4}{3} v_s^2 \quad (8.3)$$

is derived, where K is the bulk modulus (compressibility) and ρ is density. K is defined as the ratio between the hydrostatic pressure and the dilation experienced by a body under this pressure. The relationship between changes of *pressure* p and *density* is given by

$$d\rho = \frac{1}{\Phi} dp. \quad (8.4)$$

Under hydrostatic equilibrium, the increase of *pressure* with *depth* depends on the weight of the additional vertical mass column. With the radial distance r , the fundamental hydrostatic equation reads

$$dp = -g(r)\rho(r) dr, \quad (8.5)$$

where the minus indicates that pressure decreases with increasing radius. Finally, from (8.4) and (8.5) we obtain the relation between *height* and *density* changes (*Adams-Williamson equation*):

$$\frac{d\rho}{dr} = -\frac{g(r)\rho(r)}{\Phi(r)}. \quad (8.6)$$

According to (3.52), the radial change of the gravity potential W is given by

$$dW = -g(r)dr. \quad (8.7)$$

Inserting (8.7) into (8.5) yields

$$d\rho = \rho(r) dW. \quad (8.8)$$

Hence, the surfaces of equal pressure (isobaric surfaces) coincide with equipotential surfaces and, after (8.4), also with surfaces of equal density.

Starting from density and gravity values on the Earth's surface, density, pressure and gravity inside the Earth can be calculated iteratively, using (8.3), (8.4) and (3.22), (3.23). Here, we use the total mass and the polar moment of inertia as boundary conditions. Corresponding spherically symmetric *Earth models* based on seismic data consist of several layers characterized by chemical and physical properties (composition, pressure, temperature), and are based primarily on the results of seismology (seismic travel times from body waves and surface waves, free oscillation frequencies). The velocities, or the velocity gradients, of the seismic waves change abruptly at the boundaries of the layers (discontinuity surfaces or zones), as does density (Fig. 8.1). Inside one layer, density increases smoothly and reaches about $13\ 000\ \text{kg m}^{-3}$ at the Earth's center. Gravity remains nearly constant within the Earth's mantle and decreases almost linearly to zero in the core. Pressure increases continuously with depth. The Earth models developed by Bullen (1975) and the Preliminary Earth Model (PREM) from Dziewonski and Anderson (1981) have gained special importance.

The layered structure of the Earth is shown in (Fig. 8.2). The Earth's *crust* (average thickness over the continents and the oceans is about 24 km) is the uppermost layer and is characterized by a complex structure. It is separated from the *upper mantle* by the *Mohorovičić discontinuity*. Lateral density variations are pronounced in the crust, but are found also in the upper mantle, cf. [8.2.1]. The crust and the uppermost part of the mantle (also called the *lid* of the low-velocity layer beneath it) behave approximately rigidly, they are part of plate tectonic motions, cf. [8.2.3]. The *lower mantle* starts at a depth of 650 to 670 km and is separated from the core at 2890 km depth, through the *Wiechert-Gutenberg discontinuity*. The liquid *outer core* extends to 5150 km, followed by the solid *inner core*.

The density distribution of these Earth models can also be tested by comparing its *elasticity* parameters with the results obtained from the observation of natural oscillations and (to a limited extent) Earth tides, cf. [8.3.6]. The free oscillations especially provide an important constraint on the models.

More refined models have to take the *deviations* from *spherical symmetry* into account, as well as departures from hydrostatic equilibrium. These deviations are clearly

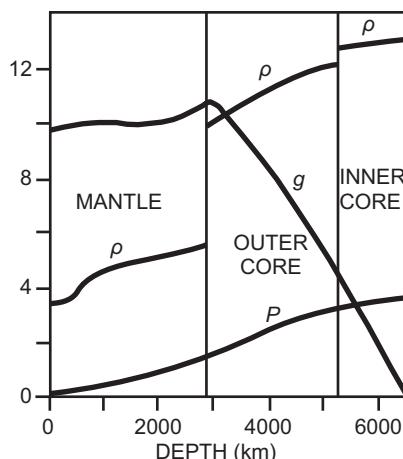


Fig. 8.1: Density ρ ($10^3\ \text{kg/m}^3$), gravity g (m/s^2), and pressure P with ($10^{11}\ \text{Pa}$) inside a spherically symmetric Earth model (PREM), after Dziewonski and Anderson (1981).

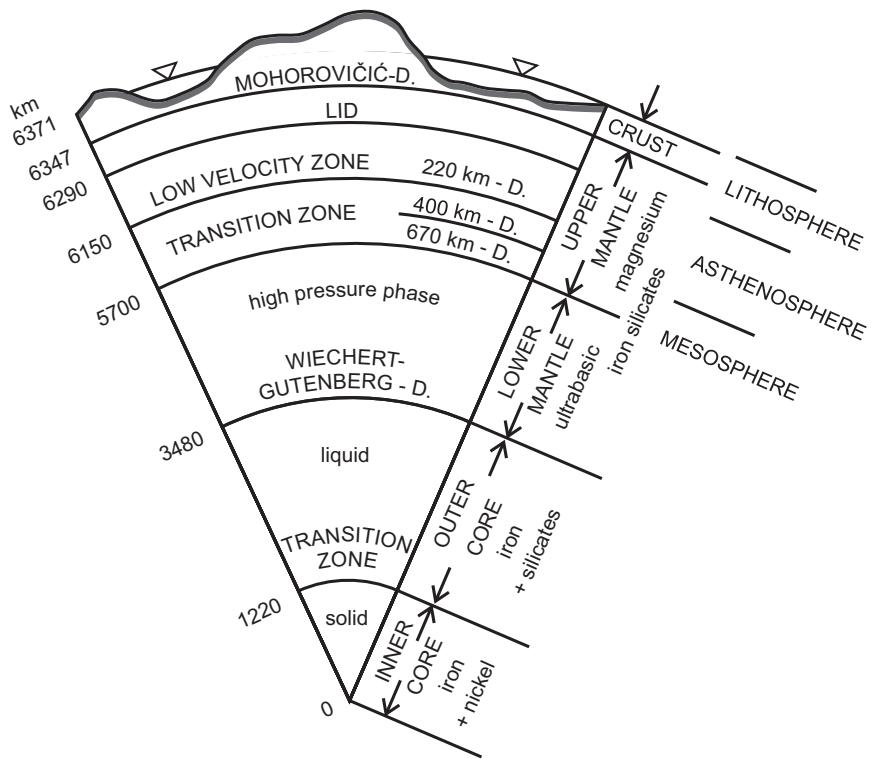


Fig. 8.2: Spherical Earth model (PREM), with homogeneous shells separated by discontinuity zones (D.), not to scale, after Dziewonski and Anderson (1981).

indicated by the odd zonal and the tesseral harmonic coefficients of the gravity potential, cf. [3.3.4], and by other geophysical observations. We remember that the second-degree harmonic coefficients in the gravity field reveal the main deviations of the Earth's figure from a sphere, i.e., the polar and the equatorial *ellipticity*, cf. [3.3.4]. The latter one is significantly smaller than the flattening at the poles, as demonstrated by the two nearly equal equatorial moments of inertia $A = 0.329\,615\,a^2\,M$ and $B = 0.329\,622\,a^2\,M$, where the larger principal axis of inertia is directed to about 15°W longitude. Refined geophysical Earth models that take the ellipsoidal form and the rotation of the Earth into account may use the level ellipsoid as a good approximation for the *external* boundary surface, cf. [4.2.1].

A global deviation from *hydrostatic equilibrium* is indicated by the flattening of a rotating spheroidal body in equilibrium, composed of density layers that are approximately ellipsoidal. A differential equation derived by Clairaut (1743) provides the flattening of a corresponding layer as a function of its radius. The solution relates the dynamic ellipticity $H = 1/305.45$ with the hydrostatic flattening f_h and the geodetic parameter m (4.50):

$$H = \frac{f_h - \frac{1}{2}m}{1 - \frac{2}{5}\sqrt{\frac{5m}{2f_h} - 1}}. \quad (8.9)$$

Inserting the observed values for H and m results in *hydrostatic flattening* values around 1/299.8, which differ significantly from the value 1/298.25 derived directly from satellite orbit analyses, cf. [4.3], Denis et al. (1997).

The deviation of the observed from the hydrostatic value may be attributed to a “fossil” flattening of the lower mantle, which developed when the Earth’s rotational velocity was larger and which is not compensated yet. The still incomplete recovery of the ancient ice loads at the polar caps may be another explanation.

8.2 The upper layers of the Earth

Large deviations from the spherically symmetric Earth model are found in the Earth’s crust and upper mantle [8.2.1]. Topographic mass excesses (mountains) and deficiencies (oceans) are, to a large part, compensated by the underlying masses, which leads to isostatic equilibrium [8.2.2]. The theory of plate tectonics introduces (nearly) rigid lithospheric plates that move against each other, causing crustal deformations, especially at the plate boundaries [8.2.3]. Since the gravity field reflects the distribution of the terrestrial masses, it provides an essential constraint in the development of crust and mantle models [8.2.4].

8.2.1 Structure of the Earth’s crust and upper mantle

The heterogeneous structure of the uppermost layers of the Earth is recognized by the distribution and composition of the *topographic* masses. There is a pronounced difference between the mean elevation of the continents (about 0.5 km) and the mean depth of the oceans (about 4.5 km). Ocean depths increase with growing distance from the ocean ridges (mean depth around 2.5 km) due to thermal cooling and contraction of the oceanic lithosphere with sea-floor spreading, cf. [8.2.3]. Consequently, the age of the oceanic crust is 200 million years, at most, while the continental crust dates back about 4 billion years (Cazenave, 1995).

The *crust* is composed of a variety of sedimentary, igneous (effusive and intrusive), and metamorphic rocks. Density changes occur primarily between different types of rock, but larger density variations are also found within the same rock material, especially in sediments. Density estimates are based on surface rock samples, borehole probes, and the relationship between density and seismic wave velocities (Mueller, 1974). The *mantle* has been investigated mainly by seismic methods, and three-dimensional models are now available from seismic tomography. Large-scale lateral variations of the P- and S-wave velocities are found here, correlated with zones of density and temperature anomalies (Dziewonski and Woodhouse, 1987).

The *structure* of the Earth’s *crust* and *upper mantle* may be briefly described as follows (Fig. 8.3):

Sediment layers with highly varying thickness are found in the uppermost stratum in large parts of the *crust*. Seismic wave velocities and rock densities (average value 2400 kg m^{-3} for consolidated sandstone) vary considerably in this zone. In *continental* areas, the next lower layer of the upper crust consists mainly of acidic rocks such as granite (mean density 2700 kg m^{-3}); primary wave velocities vary between 5.9 and 6.3 km s^{-1} . The lower crust is composed of basic rocks such as basalt and gabbro (mean density 2900 kg m^{-3}).

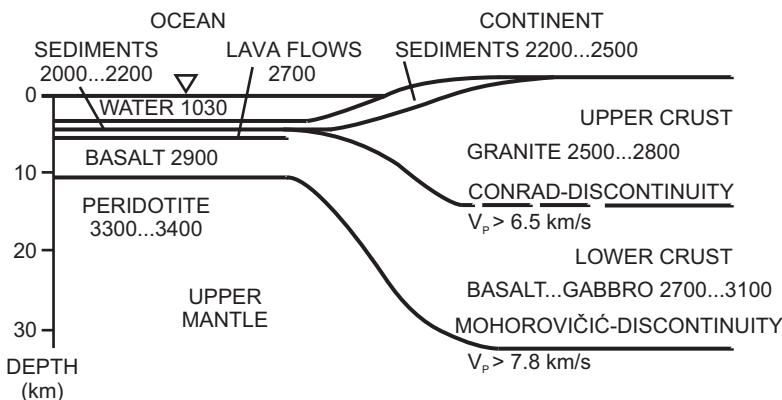


Fig. 8.3: Structure of the Earth's crust with rock densities (kg m^{-3}) and velocities of seismic primary waves.

Wave velocities exceed 6.5 km s^{-1} and gradually increase to more than 7 km s^{-1} . The boundary between the upper and the lower crust (*Conrad discontinuity*) is marked only in some parts of the continents, at depths of 10 to 20 km. Beneath the oceans, consolidated sediments and basalt lava flows are found in the upper part of the crust above a basaltic layer of 6 to 7 km thickness (Tanimoto, 1995).

A sharp (over a few km) change in seismic velocity ($v_p > 7.8 \text{ km s}^{-1}$) is found at an average depth of 35 km on the continents and 10 km on the oceans. This *Mohorovičić discontinuity* (Moho) defines the boundary between crust and mantle. Ultrabasic rocks (peridotite, with olivine as the main mineral constituent) are assumed to be located below the Moho, with a density of 3300 to 3400 kg m^{-3} . The depth of the Moho is closely related to topography. On the continents, it may be less than 20 km (e.g., at the Afar hotspot), reaching about 30 to 40 km at old shields and platforms. Cenozoic mountain belts (Alps, Rocky Mountains, Himalaya) are characterized by a crustal thickness of 60 to 80 km. Beneath the oceans, the crustal thickness is more constant. An extremely thin crust of a few kilometers is found at slow spreading and fracture zones, while a thick crust of about 20 km may appear where hotspots (mantle plumes) are located under ridge axes, as in southern Iceland. These variations of crustal thickness are mainly due to isostasy and plate tectonics, cf. [8.2.2], [8.2.3].

Three-dimensional models of the crust are based on seismic and non-seismic data. They contain information on the subsurface spatial distribution and density of ice and water, soft and hard sediments, and the upper, middle and lower crust. The global CRUST 2.0 model (U.S. Geological Survey) provides a horizontal resolution of $2^\circ \times 2^\circ$; the accuracy of the sediment and crustal thickness is estimated to 1 km and 5 km, respectively (Mooney et al., 1998; Tenzer et al., 2009). More detailed crustal models are available for several parts of the world, e.g., for Europe (EuCRUST-07: $15' \times 15'$ grid, sediments and two layers of the crystalline crust), Tesauro et al. (2008).

8.2.2 Isostasy

When considering the topographic masses and ocean waters as deviations from hydrostatic equilibrium, the removal of topography and the filling of the oceans should create an equilibrium figure, with a gravity field approximately coinciding with the normal

gravity field, cf. [4.2.2]. However, from the systematic behavior of the residual gravity field quantities, it follows that the visible mass excesses and deficiencies are, to a large part, compensated by a corresponding mass distribution in the interior of the Earth (Heiskanen and Vening-Meinesz, 1958; Watts, 2001).

Already during the arc measurement in Peru, cf. [1.3.2], *Bouguer* discovered that the *deflections of the vertical* as computed from the masses of the mountains were larger than the observed values. In the nineteenth century, the Survey of India (*G. Everest*) revealed significant differences between observed and calculated deflections of the vertical caused by the Himalaya Mountains, the computed values being several times larger than the observed ones. This observation was the basis for the theory of isostasy and the isostatic models developed by *Airy* and *Pratt* (see below).

The large-scale behavior of the *Bouguer anomalies*, cf. [6.5.3], is another indication for the compensation of the visible mass anomalies. In mountainous areas, the Bouguer anomalies are generally negative, reaching values as low as $-2000 \mu\text{m s}^{-2}$, while positive values (up to $4000 \mu\text{m s}^{-2}$) are common over the oceans. A correlation with the mean height or depth (mean value calculated over a dimension of several 100 km) can be demonstrated and in many parts of the world approximated by a regression of $-1000 \mu\text{m s}^{-2}/1000 \text{ m height}$, and $+1000 \mu\text{m s}^{-2}/1000 \text{ m depth}$. Finally, the *geoid heights* produced alone by the topographic masses would reach values of up to about $\pm 500 \text{ m}$ (Helmert, 1884), whereas the observed values hardly exceed 100 m.

The model of *isostasy* is used to explain these observations. It postulates that the topographic masses (excess masses on the continents, deficit masses on the oceans) are compensated in such a way that hydrostatic pressure equilibrium is achieved at a certain depth of compensation. The compensation depends on the quantity of the topographic load and may be achieved by different mechanisms. Loads of several 10 km to about 100 km horizontal dimensions are supported by the strength of the lithosphere and not isostatically compensated, while larger loads generally lead to an elastic flexure of the lithosphere and corresponding compensation. Therefore, large-scale topographic features of several 100 km dimension and more are generally in isostatic equilibrium.

Incomplete isostatic compensation is found in the areas of strong pleistocene glaciation (North America and Fennoscandia), at structures of plate tectonics, and in some mountain areas. In the first case, the melting of the ice masses (between about 20 000 and 10 000 years B.C.) after the Pleistocene has caused an isostatic imbalance, which is still compensated by *postglacial rebound* (glacial isostatic adjustment). The resulting sea level changes, land uplift rates and gravity variations are observed using different terrestrial and space techniques, and provide information on the viscosity of the Earth's mantle, cf. [8.3.3]–[8.3.5]. Isostatic mass transports also happen at *tectonic plate boundaries* as characterized by ocean ridges, deep-sea trenches, and continental collision zones (mountain building), which consequently are not in a perfect state of equilibrium, cf. [8.2.3]. *Mountains* may also become overcompensated by large erosion, and as a consequence a vertical uplift will occur.

The classical isostasy models of *Airy* and *Pratt* are based on the assumption that isostatic compensation takes place locally in vertical columns only. Utilizing the hydrostatic equation (8.5), the condition of isostasy then reads (with $g = \text{const.}$)

$$\int_{H+T}^H \rho dz = \text{const.}, \quad (8.10)$$

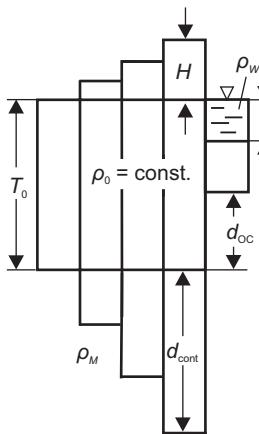


Fig. 8.4: Isostatic model of Airy.

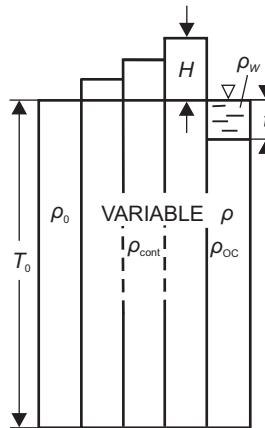


Fig. 8.5: Isostatic model of Pratt.

with z depth, H height of topography, T depth of compensation. The model developed by G.B. Airy in 1855 (also designated Airy-Heiskanen model) is based on a crust of constant density ρ_0 and varying thickness, where the “normal” column of height $H = 0$ has the thickness T_0 (Fig. 8.4). The continental topography ($H > 0$) forms mountain “roots” (thickness d_{cont}), while “antiroots” (thickness d_{oc}) are found beneath the oceanic columns. The ocean depth is denoted as t . In this way, the crust penetrates with varying depths into the upper mantle, realizing a floating equilibrium. Neglecting the Earth’s curvature, the following equilibrium conditions hold for the continental and the oceanic columns:

$$\begin{aligned} (\rho_M - \rho_0) d_{\text{cont}} &= \rho_0 H \\ (\rho_M - \rho_0) d_{\text{oc}} &= (\rho_0 - \rho_w) t, \end{aligned} \quad (8.11)$$

with ρ_0 density of the crust, ρ_M density of the upper mantle, ρ_w sea water density. With the conventional values $\rho_0 = 2670 \text{ kg m}^{-3}$, $\rho_M = 3270 \text{ kg m}^{-3}$, $\rho_w = 1030 \text{ kg m}^{-3}$, the thickness of the root and the antiroot is given by

$$d_{\text{cont}} = 4.45 H, \quad d_{\text{oc}} = 2.73 t. \quad (8.12)$$

The thickness T_0 of the normal column can be estimated from isostatic gravity anomalies calculated on the basis of a certain depth of compensation, cf. [6.5.3]. For $T_0 = 30$ to 40 km, these anomalies generally do not depend on the height of the topography. Hence, the depth of compensation is in good agreement with the depth of the Moho as obtained from seismology, cf. [8.2.1].

The isostatic model of J.H. Pratt (1855, also called Pratt-Hayford model) assumes a crustal layer of constant thickness T_0 and allows lateral changes in density in order to obtain isostatic equilibrium (Fig. 8.5). With the density ρ_0 for the normal column ($H = 0$), continental columns generate densities smaller than ρ_0 , while oceanic columns are denser. The equilibrium conditions for the continents and the oceans are:

$$\begin{aligned} \rho_{\text{cont}}(T_0 + H) &= \rho_0 T_0 \\ \rho_w t + \rho_{\text{oc}}(T_0 - t) &= \rho_0 T_0, \end{aligned} \quad (8.13)$$

with $\rho_0 = 2670 \text{ kg m}^{-3}$ and $\rho_w = 1030 \text{ kg m}^{-3}$ the densities of the continental and the oceanic columns are given by

$$\rho_{\text{cont}} = 2670 \frac{T_0}{T_0 + H'} \quad \rho_{\text{oc}} = \frac{2670}{T_0 - t} \frac{T_0 - 1030}{T_0 - t}. \quad (8.14)$$

The depth of compensation can be estimated from the behavior of residual gravity field quantities calculated with different depths. By utilizing topographic-isostatically reduced deflections of the vertical in the U.S.A., Hayford (1909) obtained minimum values for a compensation depth of 113.7 km. This value is close to the thickness of the continental lithosphere, cf. [8.2.3].

A refined isostatic model was proposed by Vening-Meinesz (1931). It admits *regional isostatic compensation* by assuming that the upper layer behaves like an elastic plate overlying a low-viscosity layer. A surface load then causes a flexure of the plate, with subsidence in the vicinity of the load and regional bending with slight uplift, over a horizontal distance wider than the load dimension (Fig. 8.6). The deformation continues visco-elastically until the isostatic compensation has been reached. The amount of flexure depends on the distance from the load and can be calculated from the load, the density contrast between the plate and the substratum, and the elastic parameters (Young's modulus, Poisson's ratio) of the plate (crust or even lithosphere), Abd-Elmotaal (1995).

Globally, the models of Airy-Heiskanen and Vening-Meinesz, respectively, describe the dominating isostatic features in many areas (e.g., at major mountain ranges), but lateral density variations (Pratt-Hayford model) also contribute significantly to isostasy, e.g., at deep ocean trenches, Göttl and Rummel (2009). In the compensated parts of the Earth, isostatic anomalies vary irregularly about zero (maximum values of about $500 \mu\text{ms}^{-2}$), and they clearly indicate areas which are not in isostatic equilibrium. On the other hand, they are not very sensitive with respect to a change of the model or variations of the model parameters, which makes discerning of different models and estimating the absolute depth of the compensation level difficult. Utilizing global models of the topography, cf. [6.5.2], spherical harmonic expansions of the topographic-isostatic potential have been developed (Sünkel, 1986b). More refined isostatic models are based on recent crustal models, and take the lithospheric density structure into account, with a density jump of 300 to 400 kg m^{-3} at the Moho (Martinec, 1993; Kaban et al., 2004). Residual isostatic gravity anomalies or geoid heights derived from these models can be analyzed with respect to mantle convection and deep seated density inhomogeneities.

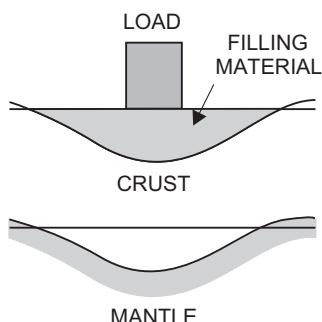


Fig. 8.6: Regional isostatic model of Vening-Meinesz.

8.2.3 Plate tectonics

The theory of plate tectonics synthesizes a multitude of individual observations of geological and geophysical nature. The theory integrates the concepts of *continental drift* (Wegener, 1915) and *sea-floor spreading* (Dietz, 1961; Hess, 1962). According to this model, new oceanic crust is formed by uprising basaltic magma at the axes of the mid-oceanic ridges, and it spreads out to both sides of the rift system. The spreading sea-floor is characterized by stripes of interchanging positive and negative magnetic anomalies aligned parallel to the ridges, which indicate the reversal of the Earth's magnetic field occurring irregularly at intervals of tens of thousands to tens of million years (Vine and Matthews, 1963). Radiometric age determinations of the oceanic rocks show that the age of the ocean floor increases with the distance from the ridge axes and does not exceed 200 million years.

Before that time (Permian and Triassic), the supercontinent Pangaea, postulated by Wegener, united all present land masses. Break up started during the Jurassic period, when Pangaea rifted into Laurasia (today North America and Eurasia) and Gondwana (today South America, Africa, India, Antarctica and Australia), with the Tethys Sea between them. This rifting process finally led to the present distribution of the continents and oceans.

The spreading rates of the ocean floor (referring to geological time spans) can be derived from the spacing of the magnetic anomalies and the rock age. They vary between 2 cm/year (e.g., at the Reykjanes Ridge south of Iceland) and 15 cm/year at the East Pacific Rise, Minster and Jordan (1978).

Plate tectonics (McKenzie and Parker, 1967; Morgan, 1968) originally postulated seven larger (Pacific, North and South American, Eurasian, African, Indian-Australian, Antarctic) and more than 20 smaller, nearly rigid lithospheric plates which move against each other on the asthenosphere; the number of plates – well established or presumed – since then has increased continuously (see below). The *lithosphere* includes the Earth's crust and the uppermost part of the mantle; it possesses a thickness of 70 to 100 km under the deep oceans and 100 to 150 km under the continents. The *asthenosphere* is characterized by low viscosity (resistance to flow within a fluid), which allows a viscous flow on geological time scales. The plate boundaries can be identified by an accumulation of seismic (earthquakes) and volcanic activity, where the boundary zones vary in width between some 10 to some 100 km and more (Fig. 8.7).

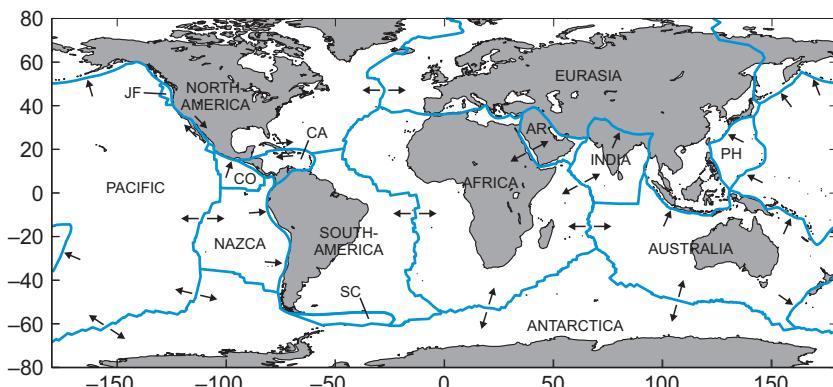


Fig. 8.7: Major lithospheric plates and direction of plate movements, according to the model NUVEL-1. AR Arabian, CA Caribbean, CO Cocos, JF Juan de Fuca, PH Philippines, SC Scotia plate, after De Mets et al. (1990).

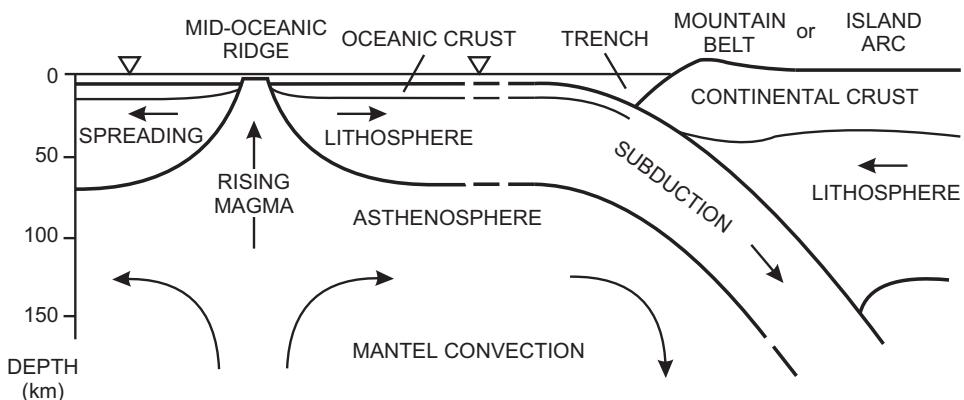


Fig. 8.8: Motion of lithospheric plates at diverging and converging plate boundaries, vertical scale exaggerated.

The movement of the tectonic plates can be described as follows (Le Pichon et al., 1973; Lowrie, 2007), Fig. 8.8.

The mid-ocean ridges represent *diverging* (constructive) plate boundaries where new lithospheric material is formed from magma uprising from the asthenosphere and pressed apart. When colliding with another plate, the cooled, heavier oceanic plate is forced to sink into the upper mantle (subduction) where it is consumed at depths of around 700 km: *converging* (destructive) plate boundary. This process creates deep-sea trenches and island arcs (e.g., at the western and northern Pacific, subduction rate of about 9 cm/year at the Japan trench) or mountain ranges (e.g., the Andes). The collision of two continental plates leads to the formation of mountain chains (e.g., the Himalaya and the Alps). *Transform faults* with relative motion parallel to the strike of the fault are found between ridge segments, but also occur where two plates meet with shear movements (e.g., San Andreas Fault, California, shear movements of several cm/year): *conservative* plate boundary. About 85% of the Earth's surface is covered by the (nearly) rigid plates, while deformations are concentrated on the plate boundary zones. Thermic *convection* (heat transfer by movement of molecules) in the mantle with extension of some 100 to 1000 km is assumed to be the driving mechanism for the plate movements (Runcorn, 1962). Different theories exist on the size and the location of the convection cells (whole-mantle or layered-mantle convection).

The *motions* of the lithospheric plates on the spherical Earth can be described as a rotation of a spherical cap about an axis through a fixed point (pole of rotation) with a certain angular velocity (Gordon, 1995). From these parameters, the *relative* plate motion (direction and magnitude) can be calculated for any location. Geological (average over the last few million years) plate velocities have been estimated from the spacing of the magnetic anomalies across the mid-ocean ridges and from the azimuths of submarine transform faults and slips from large earthquakes.

Geological models such as NUVEL-1 (De Mets et al., 1990) and NUVEL-1A (De Mets et al., 1994) include 14 major plates (Africa, Antarctica, Arabia, Australia, Caribbean, Cocos, Eurasia, India, Juan de Fuca, Nazca, North America, Pacific, Philippine Sea, South America).

Plate motion is described by keeping either one plate fixed (NUVEL-1: Pacific plate), or referencing the motions to a rotation-free system coupled with the Earth: no-net rotation (NUVEL-1A). The refined interpretation of topography, volcanism, and seismicity led to an additional number of 38 smaller tectonic plates and a corresponding digital model (PB2002) of plate boundaries (Bird, 2003). The model includes several deformation zones ("orogens" like the Alps-Persia-Tibet mountain belt) which are not expected to follow the plate tectonic movements. Recent plate motion models (MORVEL) provide velocity estimates for 25 larger plates, under the no-net rotation condition (De Mets et al., 2010). Best-fitting angular velocities for the plates bordered by mid-ocean ridges have been determined from seafloor spreading and fault azimuths, and some minor plates were linked by GPS data. An *absolute* plate motion can be derived by reference to the hotspots (Solomon and Sleep, 1974). Here, hot material is rising from deep mantle plumes that (probably) do not participate in the plate tectonic motions. Hotspots are characterized by surface volcanism and high heat flow; examples are Hawaii, Iceland, and Afar (Ethiopia).

It has to be stressed again that the plate velocities derived from these models represent the average over *geological* time spans. The results depend on the choice of the plates used and also from the choice of the hotspots introduced for reference. Deformations occurring especially at the converging plate boundaries are not taken into account, and intra-plate deformation is also neglected. *Geodetic* measurements allow the determination of *present-day* plate motion, and identification of local and regional deformation at the plate boundaries and inside the plates, cf. [2.4.2], [8.3.4].

8.2.4 Interpretation of the gravity field

The observed gravity field reflects the integrated effect of the mass distribution inside the Earth and reveals deviations from spherical symmetry and hydrostatic equilibrium, cf. [8.1]. Static and dynamic geophysical Earth models must fulfill the constraints imposed by the gravity field. The *inverse problem*, i.e., the determination of the density distribution from the external gravity field, on the other hand, suffers from an inherent ambiguity, which means that it cannot be solved uniquely (e.g., Martinec, 1994; Lowrie, 2007). This fact is seen, for instance, in the formula for the gravitation of a spherical Earth composed of homogeneous shells, cf. [3.1.2], and in Stokes' theorem, where the external gravity field of an equipotential surface is completely determined without knowing the distribution of the internal masses, cf. [4.2.1]. Consequently, gravity field interpretation requires additional information through geophysical and geological data, where seismically derived depths of bounding surfaces and the composition and density of the masses play a major role (Chao, 2005).

Synthetic Earth gravity models have been derived through forward modeling, applying Newton's law of gravitation on refined geophysical models. These models are based upon a global spherical model, cf. [8.1], and supplemented by models of topography, bathymetry, crust and mantle, now available, cf. [8.2.1]. Given by a spherical harmonic representation, these models allow the independent evaluation of methods used at gravity field modeling from terrestrial and space data (Kuhn and Featherstone, 2005).

Gravity field interpretation is based on *residual* gravity field quantities obtained by reducing the effect of the normal gravity field, cf. [6.1], and also partly the gravitation of the uppermost layers of the Earth. The primary gravity field parameters used for interpretation are gravity anomalies and geoid heights, and to a limited extent also deflections of the vertical and second derivatives of the gravity potential (gravity gradient). The effect of the masses on gravity anomalies and vertical deflections is inversely proportional to the square of the distance, while geoid heights depend on the reciprocal distance to the masses. Consequently, *gravity anomalies* and *deflections of the vertical* are more suited for investigating the density distribution in the *upper* layers of the Earth. Gravity anomalies react primarily to vertically extended masses, while vertical deflections reflect the effect of horizontal layers, hence they especially support local investigations. *Geoid heights* reveal deeper seated mass anomalies, which generally have large dimensions (Vaniček and Christou, 1994).

The spectral decomposition of the gravity field as provided by the *spherical harmonic expansion* is especially appropriate for global and regional interpretation, cf. [6.6.1], where the geoid and the gravity anomalies play an outstanding role. Degree variance models for the gravity anomalies (6.27) and the geoid heights (6.142) show that globally about 95% of the geoid variance is concentrated in degrees 2 to 10 (corresponding to wavelengths of 20 000 to 4000 km), while this long-wave spectral part attains only 9% of the gravity anomalies. Medium (degree 11 to 180) and short (degree 181 to 2000) wavelengths, on the other hand, each contribute more than 40% to the anomaly variance. Nearly 10% of the anomaly variance still stem from wavelengths less than 20 km (degrees >2000), reflecting small structures in the upper crust (e.g., salt domes). Deflections of the vertical show a spectral distribution similar to that of the gravity anomalies. With the GOCE gravity field mission, cf. [5.2.8], second-order derivatives of the gravitational potential became available measured in the satellite's height and on global scale. Although the signal is weak, it contains high-resolution gravity field information, cf. [6.7.3].

Modeling of the long-wave geoid structures can also be based on equivalent point masses arranged primarily around the bounding surfaces as determined by seismology, cf. [8.1], Bowin (1994). These solutions strongly depend on the choice of the spectral part to be modeled, the distribution of the masses, and the introduced density differences.

Hence, the interpretation of the *geoid* concentrates on the long and medium-wave part of the spectrum. Density and/or temperature anomalies are thought to produce the low degrees of the spherical harmonic expansion, while mantle convection and lithospheric structures are seen in wavelengths of thousands of kilometers (Bowin, 2000). Shorter wavelengths of a few 100 to 1000 km can be correlated with diverging and converging plate boundaries and with hotspots (Cazenave, 1994). Areas of postglacial rebound or significant crustal thinning are also reflected in this spectral part.

Slow-spreading oceanic ridges and hotspots may exhibit relative geoid maxima of several meters. Deep-sea trenches are characterized by narrow zones of geoid depression up to 5 to 20 m, followed by a geoid rise along the island arcs (Fig. 8.9). Postglacial land uplift areas show a geoid depression (up to 10 m in Fennoscandia), which is correlated with present

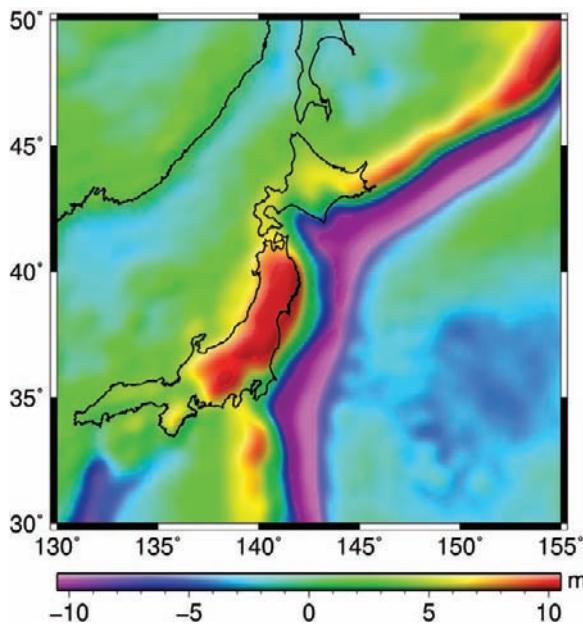


Fig. 8.9: Geoid structure at the Japan subduction zone, EGM2008 geoid model, spectral part degree 11 to 360, after Pavlis et al. (2008).

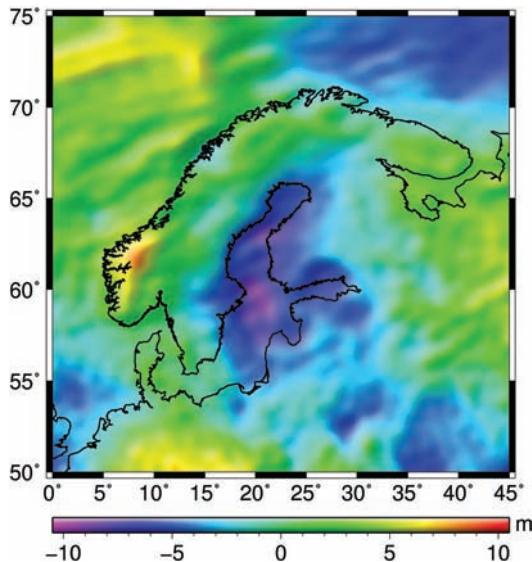


Fig. 8.10: Geoid structure at the Fennoscandian land uplift area, spectral part degree 11 to 360, after Pavlis et al. (2008).

uplift rates (Bjerhammar, 1981), Fig. 8.10. The Ivrea body (western Alps) is an example of a local geoid rise (up to 9 m) due to the ascending of lower crustal/upper mantle material to a shallow level (Bürki, 1989).

The interpretation of *gravity anomalies* uses either the spherical harmonic expansion (global and large-scale investigations) or local models based on gridded data. Different types of gravity anomalies can be used for regional and local investigations, cf. [6.5.3].

Point *free-air anomalies* strongly depend on height and are not suited for interpretation. The long- and medium-wave part provided by global models, or corresponding *mean anomalies*, on the other hand, can be exploited, due to the smoothing of the high frequencies. The free-air anomalies then may be interpreted as isostatic anomalies with a compensation depth of zero. Structures of plate tectonics (e.g., subduction zones) and postglacial rebound can be identified, where proper filtering again may be necessary.

Bouguer anomalies are employed for regional and local investigations, as they are free from the effect of topography. They mainly reflect density anomalies in the crust and upper mantle and can be correlated with tectonic structures such as ocean ridges, deep-sea trenches, continental grabens, young-folded mountains, and with upper mantle structures (Kogan and McNutt, 1993). Isostatic compensation is indicated by the large-scale systematic behavior of the Bouguer anomalies, with negative values in the mountains and positive values in the oceans, cf. [8.2.2], Fig. 8.11. Bouguer anomalies play an important role in geophysical prospecting (Dobrin and Savit, 1988; Kearey et al., 2002).

More detailed investigations of the deeper regions of the crust are made possible by further reducing the effects of known or assumed mass distributions. *Isostatic anomalies* take the effect of the compensating masses into account; deviations from zero indicate areas of isostatic imbalance and are often correlated with geological features (Simpson et al., 1986). The reduction of geologically known structures ("crustal stripping") allows, among others, the estimation of the depth of sedimentary basins and of the crust-mantle boundary (Hammer, 1963). Large-scale crustal stripping down to the Moho is possible through the use of crustal models, cf. [8.2.1]. After eliminating the gravitational effect of the topography and the crust from a

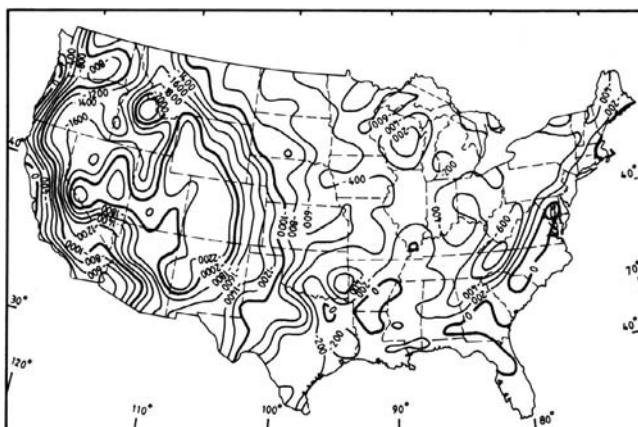


Fig. 8.11: Regional Bouguer gravity anomaly map of the United States, composed of wavelengths longer than 250 km, referred to IGSN71 and GRS67, rock density 2670 kg/m^3 , contour line interval $200 \mu\text{m/s}^2$, after Kane and Godson (1985).

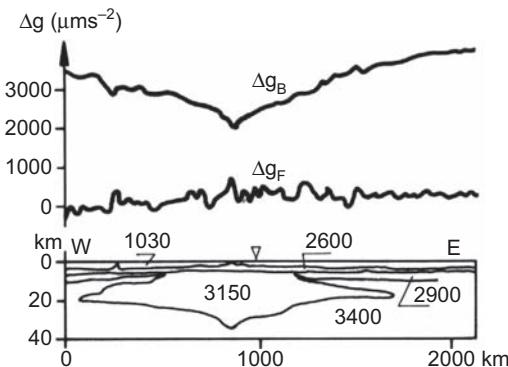


Fig. 8.12: Bouguer and free-air anomalies across the Mid-Atlantic ridge and crustal density model, with oceanic layers (2600 kg/m^3), low-density zone (3150 kg/m^3), and upper mantle (3400 kg/m^3), after Talwani et al. (1965).

global gravity model, the residual gravity field can be interpreted with respect to the morphology and density of the mantle lithosphere (upper mantle), and partially also reveals sub-lithospheric density heterogeneities due to mantle convection (Tenzer et al., 2009).

Gravity anomalies have proved to be an efficient tool for modeling a variety of crust and mantle structures of local and regional extent. Here, a starting model is iteratively improved by varying the geometry and densities of the masses, taking the constraints from seismic data and geology into account. Summarizing we mention the following large-scale relationships found between the gravity field and crustal structures (e.g., Nerem et al., 1997; Lowrie, 2007):

- Bouguer anomalies over the *continents* are generally negative, and strongly positive over the *ocean*. This observation can well be explained by the approximate isostatic equilibrium of the Earth's crust, cf. [8.2.2].
- *Oceanic ridges* show negative Bouguer anomalies (up to $-2000 \mu\text{ms}^{-2}$) due to high anomalous mantle material, while free-air anomalies deviate only slightly from zero, Fig. 8.12.
- *Deep-sea trenches* are characterized by strong, negative free-air anomalies (up to $-4000 \mu\text{ms}^{-2}$), which are explained in part by thick sedimentary layers and sea floor topography. Further inland, large positive anomalies occur due to the subtraction of the cool descending slab into the hot mantle material, Fig. 8.13.
- *Continental grabens* are correlated with strong negative Bouguer anomalies due to sedimentary layers and/or anomalous mantle material; local highs may occur through crustal thinning.
- Young folded *mountain chains* arising at continental collision zones exhibit strong negative Bouguer anomalies, indicating isostatic compensation. Nevertheless, isostatic anomalies may differ from zero due to recent tectonic processes and incomplete compensation.
- *Postglacial rebound* areas are characterized by negative free-air anomalies.

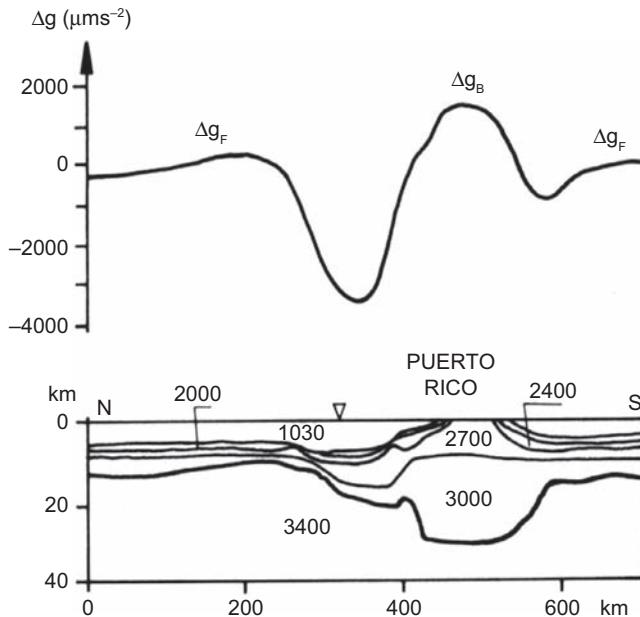


Fig. 8.13: Generalized free-air anomalies (Bouguer anomalies on land) across the Puerto Rico trench and crustal density model, with unconsolidated (2000 kg/m^3) and consolidated (2400 kg/m^3) sediments, upper (2700 kg/m^3) and lower (3000 kg/m^3) crust, and upper mantle (3400 kg/m^3), after Talwani et al. (1959).

8.3 Geodesy and recent geodynamics

Geodetic measurement methods are characterized today by repeated geometric and gravimetric data acquisition of high accuracy, and with high spatial and temporal resolution. Geodesy thus is able to determine *temporal variations* of the Earth's orientation, the Earth's surface geometry, and the external gravity field. The observed changes, after proper modeling, are used for reducing the data and referring them to common standard epochs. The observations contain, on the other hand, the effects of a multitude of geodynamic processes of extraterrestrial and terrestrial origin, the latter ones being located in the solid Earth as well as in the hydrosphere and the atmosphere. Geodesy thus significantly contributes to research in *geodynamics*, in collaboration with astronomy, oceanography, meteorology, hydrology, glaciology, solid Earth geophysics, and geology.

Previous chapters already dealt with individual geodynamic processes and their effects on geodetic measurements and products, as Earth rotation [2.3.4], crustal deformation [2.4.2], geoid [3.4], gravity and gravimetric tides [3.5]. In the following, we concentrate on *recent results* obtained by geodetic space and terrestrial methods, with selected examples from the different branches of geodesy. A review on the manifold effects acting on the rotation, surface and gravity field of the Earth is given in [8.3.1]. Changes in the Earth's rate of rotation result from a variety of geodynamic phenomena, which are partly well-known, but partly still under investigation [8.3.2]. Sea level changes, among others, reveal the effects of global warming and melting

of the ice sheets [8.3.3]. Recent crustal movements (horizontal and vertical) serve as constraints for modeling of geodynamic processes at all scales, and as earthquake and volcanism precursor phenomena [8.3.4]. Gravity field variations contain a wide range of information on mass redistribution on the Earth's surface and inside the Earth, and support and supplement geometric information [8.3.5]. Continuous geometric and gravimetric observations are especially useful for tidal research, but also contain additional information on geodynamics [8.3.6].

Geodynamics is treated in monographs and textbooks on physics of the Earth (e.g., Turcotte and Schubert, 2002; Lowrie, 2007). For the contribution of geodesy to geodynamics research see Lambeck (1988) and Mueller and Zerbini (1989), among others, also Ilk et al. (2005b) and Rummel et al. (2009).

8.3.1 Geophysical processes and effects on geodetic products

In the following, we shortly describe the manifold geophysical processes which occur within the system Earth (solid Earth with inner and outer core, mantle and crust, hydrosphere, atmosphere), and which, by different mechanism, affect the three fundamental types of geodetic products: Earth rotation, surface geometry, and external gravity field (e.g., Ilk et al., 2005b; Rummel, 2005; Rummel et al., 2009). The observable effects cover a broad time scale, ranging from minutes and hours (e.g., co-seismic deformation or tsunamis) to decades (e.g., sea level change) and secular processes (e.g., postglacial rebound, changes in ice cover, tectonic plate movements), and they enter in different way into the geodetic observations and parameters, see Fig. 8.14.

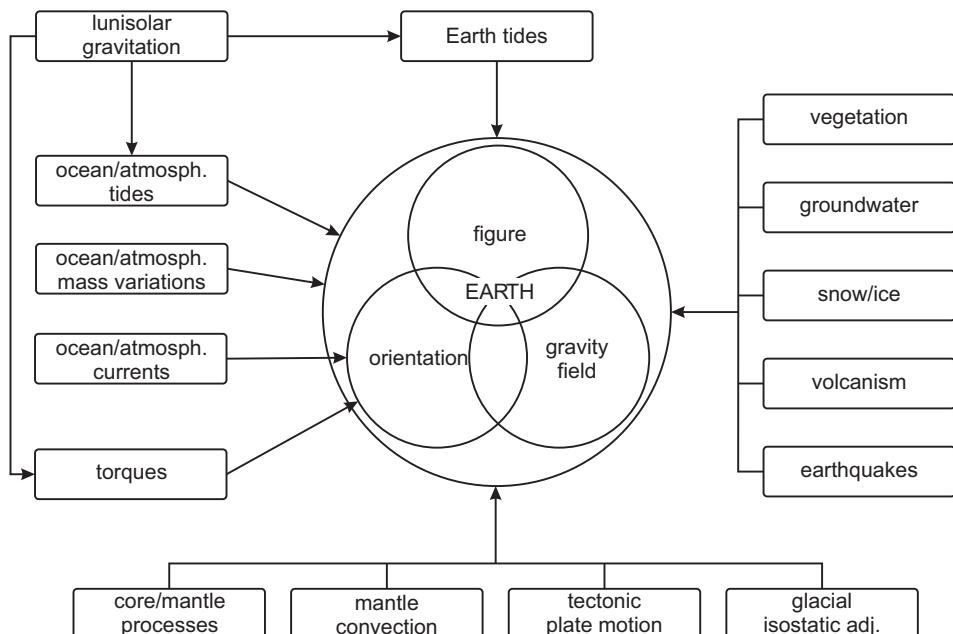


Fig. 8.14: Astronomical and geophysical processes and effects on the Earth's figure, gravity field and orientation.

Starting with the *rotation* of the *Earth*, the dynamic Euler equation describes the balance between the Earth's angular momentum $\mathbf{H}(t)$ and the external torques $\mathbf{L}(t)$ due to the lunisolar and planetary gravitational forces (e.g., Moritz and Mueller, 1987; Seitz and Schuh, 2010):

$$\frac{d}{dt}\mathbf{H}(t) + \boldsymbol{\omega}(t) \times \mathbf{H}(t) = \mathbf{L}(t) \quad (8.15a)$$

with $\boldsymbol{\omega}(t)$ rotation vector of the Earth. For a deformable body, the angular momentum is composed of two terms:

$$\mathbf{H}(t) = \mathbf{I}(t) \cdot \boldsymbol{\omega}(t) + \mathbf{h}(t). \quad (8.15b)$$

The first term $\mathbf{I}(t) \cdot \boldsymbol{\omega}(t)$ describes the angular momentum of a rigid body, where the tensor of inertia $\mathbf{I}(t)$ contains the time variable mass elements ("mass term"). The second term $\mathbf{h}(t)$ represents the angular momentum relative to the body rotation, and contains the mass elements' velocities with respect to the reference system ("motion term"). The equation (8.15a), (8.15b) is known as Euler-Liouville equation. It relates the – well-known – gravitational forces of moon, sun and planets, cf. [3.5.2], to mass redistributions and mass motions within the Earth's body. After linearization, the solution of (8.15) provides polar motion and length of day (LOD) variations as functions of their excitations, and allows the study of Earth's rotation variations.

Going more into detail, the torques from luni-solar and planetary gravitational acceleration directly determine the orientation of the Earth in space: precession, nutation, cf. [2.3.2]. Atmospheric and oceanic tides, together with other atmospheric (winds) and oceanic (ocean currents) transport processes, change the inertia tensor and exert corresponding angular momenta. These effects become visible in polar motion and LOD variations. In addition to these direct effects, there is a variety of further contributions to Earth's rotation, resulting from mass redistribution and movements in the fluid and solid parts of the system Earth.

Starting with the *Earth's interior*, we have the effects of the (still not very well known) core-mantle dynamics and of motions in the fluid outer core (Greiner-Mai and Barthelmes, 2001). *Mantle convection* is another deep-seated source for rotation changes. With the involvement of the mantle and lithosphere, we proceed to the numerous processes which produce *deformations* and – generally – also *gravity changes*. The close connection between deformation and gravity change is of special interest, as it provides a deeper insight into the mass transfer inside the Earth, and allows the discrimination from surface effects. Plate tectonics and glacial isostatic adjustment are the dominant global processes.

While modeling of the relations between *mantle convection*, mantle plumes/hotspots and *plate tectonics* is still in its infancy, geophysical/geological plate motion models generally agree with recent geodetic observations, cf. [8.2.3], [8.3.4]. *Seismic* events (earthquakes) and *volcanic* activities are also related to plate tectonic structures, but pose severe problems at modeling and "prediction".

Glacial isostatic adjustment or *postglacial rebound*, on the other hand, is far better understood, and provides an outstanding opportunity to get insight into the rheology of lithosphere and upper mantle. This adjustment process is the response of the Earth to the changing surface ice load at the recent deglaciation cycle which started about 21 000 years ago, it tends to restore the hydrostatic equilibrium. Postglacial

rebound becomes visible in a multitude of geological, geophysical, hydrographic and geodetic observations, including sea level trends, surface displacements (especially uplift), gravity field variations, and it also enters into Earth rotation, cf. [8.3.3]–[8.3.5]. The related data contain valuable constraints on mantle viscosity and thickness of the lithosphere (Lambeck et al., 1998; Mitrovica et al., 2009), and they serve as boundary conditions for modeling the isostatic adjustment process. Corresponding models provide the history of sea-level change relative to the deforming Earth through a time-dependent convolution integral over the surface mass load weighted by a visco-elastic Green's function, for separating geoid and solid Earth surface (equivalent to the elastic surface load Love numbers), Peltier (2004), cf. [8.3.6]. Models for the time-dependent displacements (vertical and horizontal) and gravity changes follow from the evaluation of corresponding convolution integrals, based on the elastic properties of a reference Earth model.

In addition to glacial isostatic adjustment, there are several other large-scale *loading effects* which produce deformations and gravity variations. These effects have either tidal origin, or result from mass displacements in the atmosphere, the oceans, and the continental water/ice budget.

The *Earth body tides* directly affect the solid Earth, with well known deformations and gravity changes, cf. [8.3.6]. This is also valid for the solid Earth and the ocean *pole tide* which are caused by the centrifugal effect of polar motion. *Atmospheric* and *ocean loading* are composed of the effects of atmospheric tides and atmospheric currents, and ocean tides and ocean currents, respectively. Again, the tidal contribution can be modeled rather well, based on corresponding models, cf. [8.3.6].

Non-tidal loading effects due to mass redistribution in the atmosphere, the oceans, the cryosphere (snow and ice coverage), the continental hydrosphere (groundwater, soil moisture, surface water) and, to a lesser extent, the vegetation are more difficult to model; more sophisticated models especially exist for the coupled atmosphere and ocean circulation (Williams and Penna, 2011). In contrast to the slowly (from decades to several thousands of years and more) progressing variations due to processes in the Earth's interior, to isostatic rebound and to climatologic changes in land water and ice, recent loading-induced effects run on time scales of minutes to years.

Based on the theory of continuum mechanics, the *loading effects* are modeled by calculating the (vertical and horizontal) deformation and gravity change caused by an additional thin surface layer of limited extension, spread on a conventional geophysical Earth model. Calculation either employs an empirical admittance function or global models of the time-variable physical parameters (Neumeyer, 2010). The empirical approach is based on measured local data (atmospheric pressure, ocean height, groundwater level depth, etc.) exploiting their correlation with the observed changes, e.g., by linear regression. The physical model approach evaluates global models with assimilated observations. The calculation of these gravitational and loading effects follows the procedure developed by Farrell (1972), for estimating the deformation of the Earth by surface loads, cf. [8.3.6].

Atmosphere and ocean general circulation models (now generally coupled models) are developed extensively for weather forecast and for simulation of climate changes, they

often include land surface and sea ice information. The models deliver relevant information (for instance air pressure, ocean height) with spatial resolution of 0.5° to 1° and daily or even sub-daily basis, e.g., Jungclaus et al. (2006), Pozzer et al. (2011). *Hydrological* models provide the continental water storage expressed as equivalent water columns in mm of water height, e.g., the NASA Global Land Data Assimilation System (GLDAS), Rodell et al. (2004). For further examples of circulation models including continental hydrology see, e.g., Hense et al. (2009), and for hydrology also Döll et al. (2003) and Fan and van den Dool (2004).

8.3.2 Changes in Earth rotation

Temporal changes of the Earth's rotation vector with respect to the Earth's body are described by the Earth's *rotation parameters* polar motion and Earth rotation angle or length of the day (LOD), respectively. Space geodetic techniques provide these quantities with high temporal resolution and accuracy, and coordinated results are published regularly through the IERS, cf. [2.4.3], [2.4.4]. The integral effect of the redistribution of masses can be recovered by repeated gravity field observations, employing dedicated satellite missions like GRACE and terrestrial gravimetry, cf. also [8.3.5], Schuh et al. (2003), Ilk et al. (2005b).

The observed changes of the Earth rotation parameters mirror the combined effects of terrestrial *mass redistribution*, which affect the inertia tensor of the Earth, and of the related *motions*, which act on the angular momentum of the respective layer (e.g., atmosphere, ocean, continental water, mantle, core), cf. [8.3.1]. The law of the conservation of the Earth's *total* angular momentum then requires corresponding changes of the rotational vector. Mass redistribution mainly affects polar motion, while LOD variations are dominated by motion of the masses.

Polar motion and LOD contain a variety of components, which result from different processes and proceed at time scales from hours to decades and millenia, at the $0.1''$ resp. 1 ms and more order of magnitude, cf. [2.3.4]. From the many possible sources of these variations, only a limited number has been clearly identified in the observation series, and most of them cannot be modeled at all or with sufficient accuracy. We summarize some results (Gross, 2009; Dehant and Mathews, 2009; Seitz and Schuh, 2010).

Long-term observations of *polar motion* (about 150 years) and LOD (about 2500 years) reveal *secular variations*. While tidal friction in the oceans is responsible for the main part of the secular change of LOD, a multitude of slow mass redistributions affects polar motion. On time scales of a few thousand years, glacial isostatic adjustment and sea level change, among others, contribute to polar motion and LOD change. The Chandler oscillation and the annual wobble represent the main constituents of polar motion, driven by a number of gravitational and internal geophysical excitations (Gross, 2000; Schuh et al., 2011). The individual contributions cannot be sufficiently modeled yet, but signal decomposition allows for a corresponding splitting of the polar motion signal (Seitz and Schuh, 2010). Fig. 8.15 shows the x-component of polar motion after linear trend removal, as observed over the past 150 years. The Chandler oscillation is characterized by stronger variations, while the annual period is rather uniform. The course of the residuals

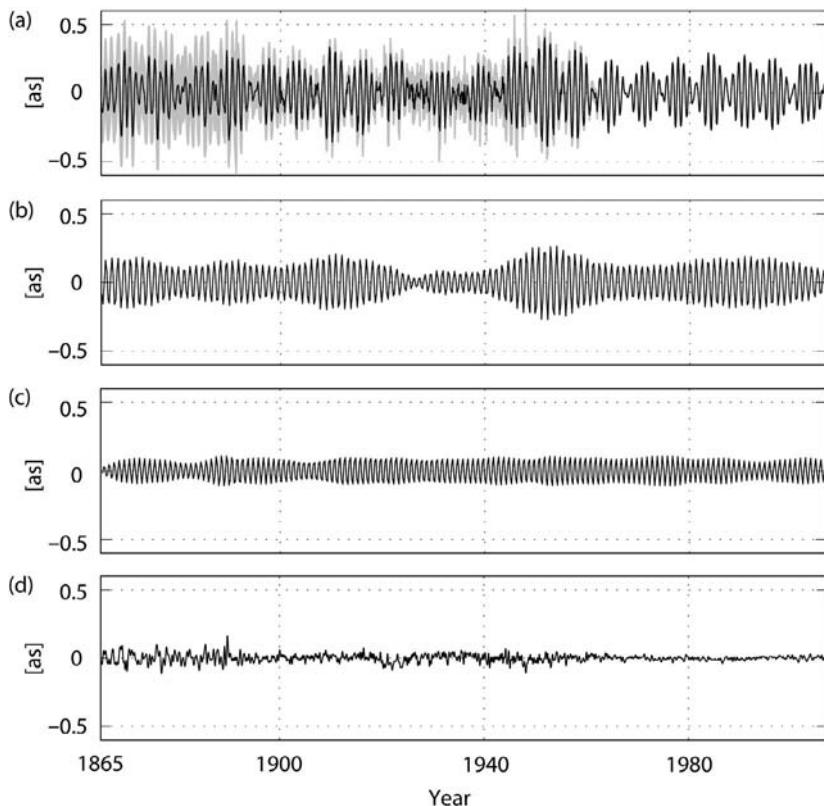


Fig. 8.15: Long-term observation of polar motion (x-component, linear trend removed) between 1860 and 2009 (a), Chandler (b) and annual (c) signal component determined by wavelength filtering, and residuals (d), after Seitz and Schuh (2010), courtesy F. Seitz.

demonstrates the increasing accuracy of the observations, and the small amplitudes of remaining contributions ranging from decadal to instantaneous, including strong earthquakes (Gross, 1986; Chao et al., 1996) and El Niño effects (Kosek et al., 2001), cf. [2.4.3].

The interpretation of *length-of-day* variations can be partly based on models of the exciting processes, but partly again on filtering. This is demonstrated in Fig. 8.16, with the LOD variations between 1962 and 2009 (Seitz and Schuh, 2010). The secular change due to tidal friction is superposed by decadal variations, mainly resulting from the exchange of angular momentum between the Earth's core and mantle. The effect of solid Earth and (far less) of ocean tides can be calculated from tidal models, while the annual and semi-annual signal component is more difficult to model (Herring and Dong, 1994). The residual time series again mirrors the observational accuracy, and indicates episodic effects like the El Niño event.

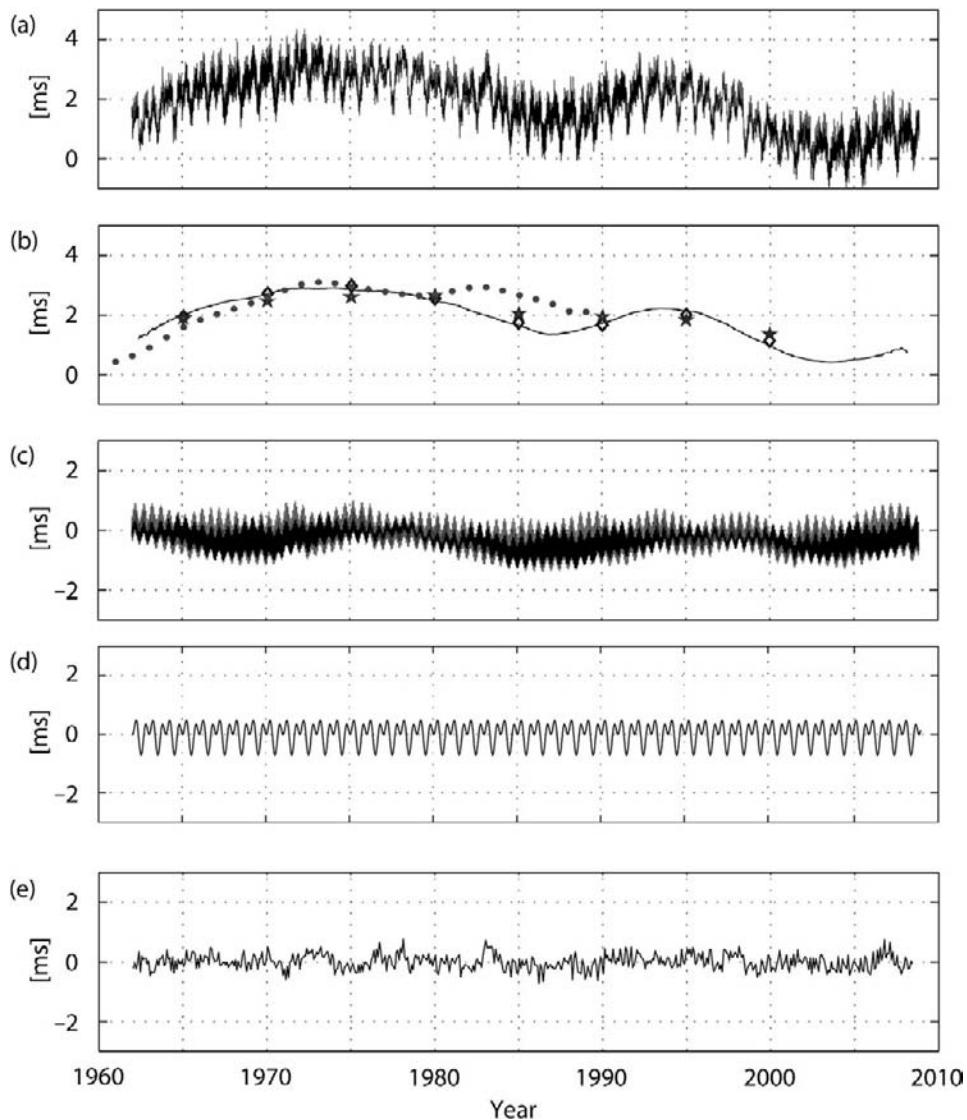


Fig. 8.16: Variations of length-of-day (ΔLOD) between 1962 and 2009 with (a) observation time series EOP 05 C04, (b) moving average over 5 years compared with the JGB model (Jackson, 1997) for the influence of core-mantle interaction, (c) effect of solid Earth tides, (d) annual and semi-annual signal component, (e) residual time series, after Seitz and Schuh (2010), courtesy F. Seitz.

8.3.3 Sea level variations

Variations of sea level with time are relevant in geodesy for the definition and realization of height reference surfaces, especially the geoid, cf. [3.4.3], [8.3.5]. Atmospheric and oceanic excitation also contribute to polar motion and to length of day changes,

i.e., to Earth's rotation variations (Gross et al., 2003; Gross et al., 2004), cf. [8.3.2]. Finally, the variable mass distribution – tidal and non-tidal – in the oceans leads to crustal loading effects, which produce surface deformation and gravity variations (Boy and Llovel, 2008). The determination and interpretation of sea level changes, on the other hand, contributes to a better understanding of the coupled *atmosphere-ocean circulation* and of *climate change* processes, and thus is of high interest for oceanography, meteorology and other geophysical disciplines.

Sea level changes occur at a wide range of temporal and spatial scales, with amplitudes at the 0.1 to 1 m order of magnitude (Lisitzin, 1974; Cazenave and Llovel, 2010). Many different sources contribute to these changes of the dynamic ocean sea surface. This includes tidal effects and density variations due to changes in temperature and salinity, ocean currents and eddies, and atmosphere/ocean coupling (wind and pressure), as well as exchange with continental waters and the effect of melting ice sheets and glaciers, cf. [3.4.2].

Special attention is focussed today on the global *sea level rise*, cf. [3.4.2], Cazenave and Llovel (2010). Fig. 8.17 shows the observed (since 1800) and projected (after 2000) change of the global mean sea level. Satellite altimetry has measured the recent acceleration of sea level rise which indicates global warming (Solomon et al., 2007), (Fig. 8.18).

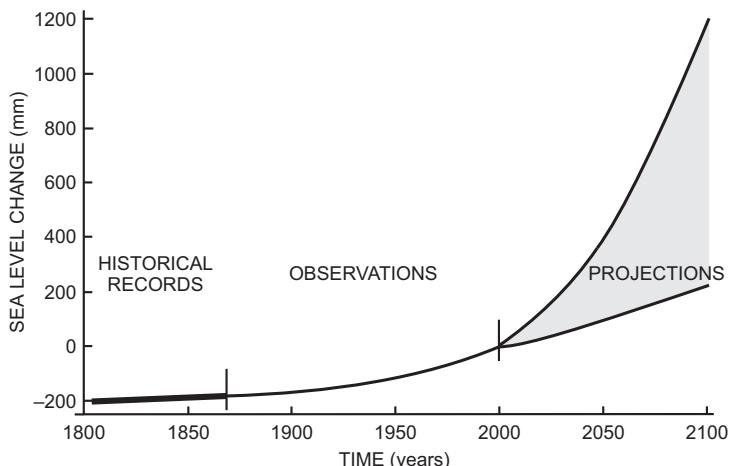


Fig. 8.17: Global mean sea level between 1800 and 2100 from observations (until 2000) and future projections. Modified after Cazenave and Llovel (2010, p. 166).

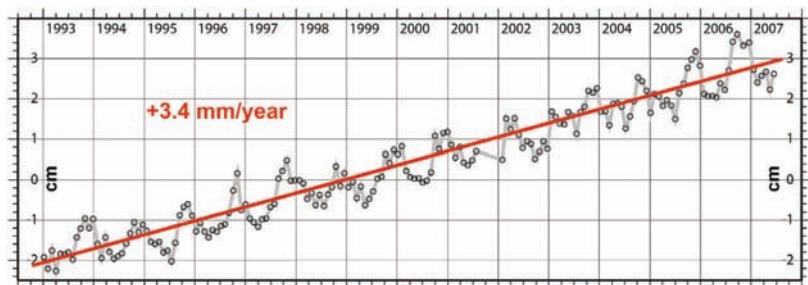


Fig. 8.18: Sea level rise between 1993 and 2007 (monthly mean Values), derived from TOPEX and Jason1 satellite altimetry, after Bosch et al. (2010).

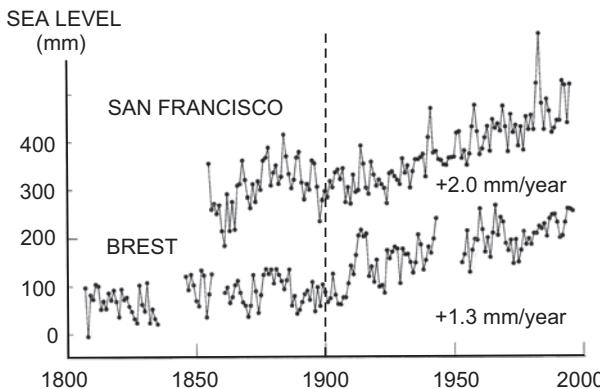


Fig. 8.19: Sea level records for San Francisco and Brest, after Woodworth (1997).

Sea level changes can directly be measured by tide gauges and by repeated satellite altimetry, cf. [3.4.2]. In situ ocean temperature data allow to estimate the contribution of ocean warming to sea level rise, and repeated gravity field determinations from the GRACE satellite mission provide information on the redistribution of the oceanic water masses, as, for instance, due to the melting of ice sheets, cf. [8.3.5].

Tide gauge records can be evaluated for the determination of the oceanic tides and other short- and medium-term phenomena, including the effects of atmospheric pressure changes, storm surges, and meltwater inflow. Averaging over long time intervals reveals long-term water level variations. For the twentieth century, an average global rise of 0.1 to 0.2 m/100 years has been found, with large regional and local scatter and decadal variations (Woodworth, 1997), Fig. 8.19.

It must be emphasized that tide gauge data only provide *relative* water level changes, by a superposition of absolute water level changes and local or regional vertical crustal movements affecting the mareograph (Tamisiea and Mitrovica, 2011). These movements are at the one mm/year order of magnitude and may reach several mm/year and more in areas of postglacial land uplift, cf. [8.3.4]. Hence, long-term height control with mm-accuracy is required for tide gauges (e.g., Carter et al., 1989). This is achieved locally by leveling connections to neighboring bench marks, and globally by repeated GNSS/GPS height-determination. Continuous GNSS monitoring is now usual at many sites, with networks well tied to the International Terrestrial Reference Frame (ITRF). Repeated absolute gravimetry provides an independent method for the detection of vertical displacements and delivers additional information about internal mass redistribution. One example for a regional tide gauge control is given by the dedicated continuous GPS stations established at U.K. mareographs, which are regularly surveyed by absolute gravimetry (Teferle et al., 2007).

Satellite altimetry provides a nearly global and quasi-continuous monitoring of the sea level with cm-accuracy. Recent ocean tide models allow reduction of the tidal effects with cm-accuracy (Shum et al., 1997). The analysis of long-term (several years) altimetry observation series improved the ocean tide models and revealed a number of other phenomena, with variations of 0.1 to 0.3 m (Nerem et al., 1997). This includes ocean basin-wide decadal and interannual fluctuations, probably due to the shift of water masses (Bosch et al., 2010), see Fig. 8.20. An annual cycle includes a 180° phase shift between the northern and the southern hemisphere caused by thermal expansion and contraction.

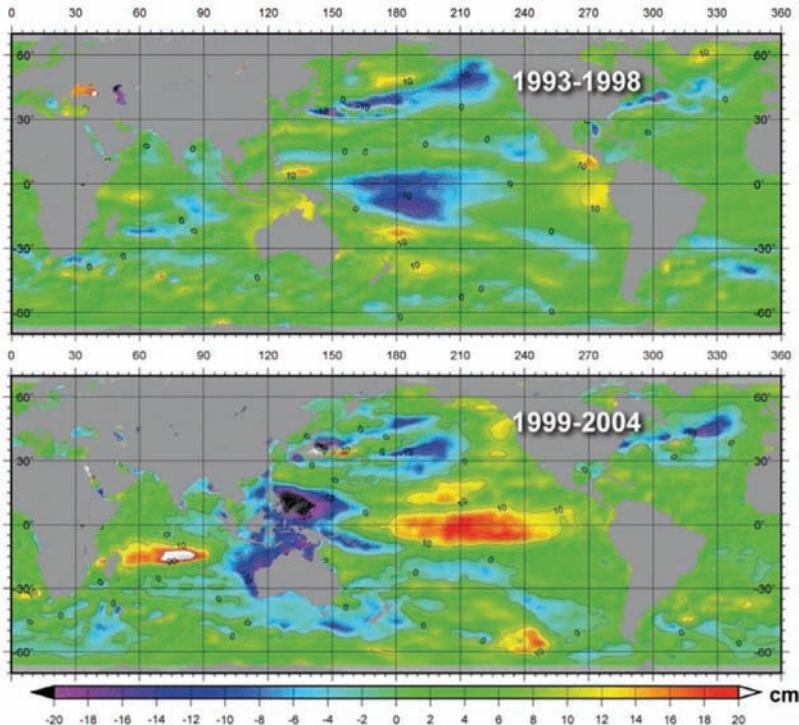


Fig. 8.20: Regional sea level changes (cm) for the periods 1993–1998 and 1999–2004, after Bosch et al. (2010).

Interannual and seasonal variations can be correlated with the variability of ocean currents such as the Gulf Stream meandering and eddies and the El Niño phenomenon.

The El Niño Southern Oscillation (ENSO) is an outstanding example of a large-scale interannual process. It comprises variable warm water currents in the eastern and central tropical Pacific, caused by strong oscillations of the sea surface temperature and pressure. ENSO occurs with varying intensity at irregular intervals of 2 to 7 years, the until now largest event happening in 1997/1998. El Niño effects have been clearly identified in LOD (increase of several 0.1 to 1 ms) and in irregular perturbations of polar motion (Salstein et al., 1999), and are clearly visible by variable sea level inclination in west-east direction.

The combination of *tide gauge* data and *satellite altimetry* has led to significant improvements in sea level monitoring (Cazenave et al., 1999). Here, the tide gauge data serve for ground control and can be used to remove biases in the altimetric results, which may be affected by altimeter drift, systematic orbit errors, and differences between the tracking station's reference systems. By combining the results of different altimetry missions the spatial resolution can be improved. Oceanographic and meteorological data such as sea surface temperature, salinity, current velocities, and air pressure may also be integrated.

A significant contribution to the investigations on sea level change is delivered through the time-variable gravity field obtained monthly with 1° spatial resolution by the GRACE satellite mission, cf. [5.2.8]. Although the inherent ocean mass gravity change signal is significantly less (a few cm only) than the corresponding signal from land, cf. [8.3.5], it

is extremely useful as it quantifies the amount of mass changes in the oceans and thus monitors the non-steric contribution to sea-surface variability. Combination with satellite altimetry allows to distinguish between steric and non-steric contributions to sea level rise (Chambers, 2006; Lombard et al., 2007). The presently available GRACE results show that, since the beginning of the twenty-first century, the sea level rise can be explained to a large part by an ocean mass increase, with contributions from the melting of polar ice sheets and mountain glaciers, and – to less extent – from continental waters. The previously dominant steric sea level contribution due to ocean thermal expansion and salinity effects is since then reducing (Cazenave et al., 2008). The acceleration of ice mass loss observed at the Greenland and Antarctic ice sheets leads to the conclusion that melting of ice sheets could be the main part of sea level rise in the twenty-first century (Rignot et al., 2011), cf. [8.3.5].

8.3.4 Crustal deformation

Recent crustal deformation (horizontal and vertical displacements) can be determined by geodetic measurements, carried out on the Earth's surface at certain repetition rates or continuously. Geometric positioning employs satellite (three-dimensional) and terrestrial (horizontal position and height separately) methods, frequently supported by repeated gravity measurements which deliver additional information on inherent mass redistributions, cf. [8.3.5]. Remote sensing space techniques like InSAR offer the additional possibility for mapping of surface deformations, without requiring monuments on the ground.

Radar interferometry from space-borne platforms is extensively employed for topographic mapping, cf. [6.5.2]. *Interferometric Synthetic Aperture Radar* (InSAR) has also proved as an efficient technique for three-dimensional mapping of surface *displacements*. The evaluation is based on the radar phase change obtained through measuring the surface two times from an exactly repeated pass. The phase difference obtained can be transformed into the three-dimensional deformation of the image point. Repetition rates and spatial resolution of mapping vary considerably, amounting, e.g., to 35 days and 30 m at ERS satellites, and 11 days and a few meters at TerraSAR-X, cf. [6.5.2]. Among the first successful applications were the detection of deformations associated with an ice stream in Antarctica (Goldstein et al., 1993), and with the 1992 Landers earthquake in southern California (Massonnet et al., 1993). Meanwhile, InSAR mapping surveys have been carried out successfully at numerous different type deformation areas, related to seismic (earthquakes) and volcanic activities, glacier flows and ice sheet coverage, as well as to landslides and subsidence due to oil or water withdrawal (Massonnet and Feigl, 1998; Simons and Rosen, 2009; Xia, 2010). The evaluation of InSAR requires a digital elevation model, monitoring of areas of limited extension can be supported by ground-based GNSS/GPS and corner reflector arrays. The accuracy achieved at InSAR deformation monitoring is at the cm- to mm-order of magnitude.

The *observation sites* for surface-based observations have to be carefully monumented, possibly by anchoring the pillar or antenna to the Earth's crust at depths of some meters or more. In addition, the monument's (i.e., the local reference marker's) local behavior with time must be controlled and reduced for displacements not under investigation (Petit and Luzum, 2010, p. 99 ff.). Present-day sub-centimeter to millimeter accuracies put high demands on the corresponding reductions, to be derived from models and supported by local measurements. The major reductions include the effects of solid Earth and ocean tides, of loads from atmosphere, oceans and hydrology, and of Earth's rotation changes (pole tide and ocean pole tide loading), e.g., Ducarme and Janssen (1990), Van Dam et al. (1994), Van Dam et al. (2001), Gipson and Ma (1998), see also [8.3.1].

On *global* scale, space-geodetic networks (VLBI, SLR, GNSS/GPS, DORIS) provide geocentric coordinates for certain epochs and station velocities with mm/year to cm/year accuracy, with GNSS/GPS playing a dominant role (Larson et al., 1997; Blewitt, 2009). The individual network solutions are combined by the IERS, and the annual station velocities are then part of the International Terrestrial Reference Frame ITRF, cf. [2.4.2]. The horizontal velocities derived from these global networks are primarily due to the motion of the *tectonic plates* (Robbins et al., 1993). The detection of correlated vertical motion is still problematic (Soudarin et al., 1999), in contrast to height changes of *regional* and *local* character (see below). For stations located in the interior of the tectonic plates, the recently observed horizontal motions (relative velocities) range between 2 and 3 cm/year (Mid-Atlantic Ridge) and 16 cm/year (East Pacific Rise) at diverging plate boundaries, and attain values of up to 10 cm/year at subduction zones as the Peru-Chile or the Japan trench zones. These values generally agree well with the velocities given by geological/geophysical models as mean values over the past 3 to 10 million years, cf. [8.2.3]. Larger discrepancies are found at the plate boundaries, as the recent local deformations are not taken into account in those models.

Geodetic Actual Plate Kinematic Models (APKIM) have been developed by combining global geodetic data sets (Drewes, 2009a). These models assume the plates' interior as being rigid and rotating on the Earth's surface. They admit deformation zones at the plate boundaries that result from the forces exerted by the adjacent plates. By interpolation, the velocity field is provided in a $1^\circ \times 1^\circ$ grid, with the condition that the integrated velocities over the whole Earth's surface are zero. Fig. 8.21 provides a comparison between a geodetic and a geophysical plate motion model.

Regional crustal deformation is derived from the repeated survey of national or continental control networks and from dedicated networks set up in areas of geodynamic activity.

Triangulation and leveling networks established in most parts of the world between the end of the nineteenth and the second half of the twentieth century are only partially valuable for the detection of long-term crustal movements. Systematically repeated surveys of these classical

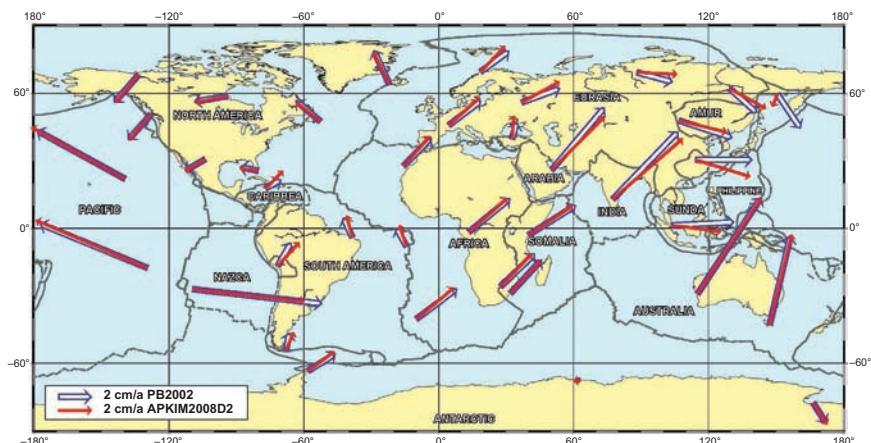


Fig. 8.21: Plate motions from geodetic observations (APKIM2008 model) and from the geophysical model PB2002 (Bird, 2003), DGFI Annual Report 2009, courtesy Deutsches Geodätisches Forschungsinstitut (DGFI), München.

networks have been carried out in high earthquake risk areas such as California and Japan. Higher repetition rates and accuracies became possible since the 1970s, with Laser distance measurements and mobile VLBI and SLR systems. Deformation measurements with GPS started in the 1980s, followed by other GNSS systems.

GNSS/GPS measurements are now the primary tool for investigations of recent crustal deformation, related to all kind of natural or man-made processes. Data are acquired either at measurement campaigns carried out at different epochs, or by permanently operating stations. Real-time GNSS/GPS measurements obtained from continuously operating regional or local networks are going to play an important role in this connection. By providing a data rate of 1 Hz or higher with a latency of seconds or less, the corresponding data series do not only serve for a better understanding of geodynamic processes, but also for the improvement of natural disaster warning systems (Hammond et al., 2011). Naturally, the GNSS/GPS results contribute to the maintenance of national or supranational geodetic reference systems, by revealing the development of the reference frame with time, cf. [7.3].

By inverting GPS station velocities and taking constraints from seismics and geological fault slip data into account, a global map of strain-rate has been derived (Kreemer et al., 2003). This contributes to the development of a global tectonic stress map (Heidbach et al., 2010).

We mention some examples of large-scale monitoring of plate-boundary and intra-plate deformation.

Iceland offers a unique opportunity to observe crustal deformations occurring at a diverging plate boundary. Triangulation (and gravity measurements) for monitoring these movements started in 1938, and GPS measurements have been carried out since 1986 (Völksen, 2000). Country-wide GPS campaigns in 1993 and 2004 revealed an average overall spreading rate of 20 mm/year. Recent deglaciation processes explain the uplift (a few mm/year) observed in central and southeastern Iceland, although the overall pattern of vertical motion is rather heterogeneous (Árnadóttir et al., 2010). The *Krafla* (northern Iceland) *rifting episode* (1975–1984) represents an active event within the rifting process, it has been extensively monitored by terrestrial measurements, GPS and gravimetry, among others (Björnsson, 1989). The rifting process was triggered by the in- and out-flow of magma in a shallow magma chamber, which caused repeated inflation and deflation of the Krafla volcano (Tryggvasson, 1994). During the rifting episode, large horizontal (several m) and vertical (up to 1 m and more) crustal movements have been observed. These displacements decreased to a few cm/year during the following stress relaxation phase, along a narrow zone around the Krafla fissure swarm, and finally approached the average plate-spreading rate (Jahn et al., 1994), Fig. 8.22. Satellite radar interferometry identified a post-rifting subsidence (several mm/year to 2 cm/year) above the magma chamber and along the spreading segment, due to cooling induced contraction and ductile flow of material away from the spreading axis (Sigmundsson et al., 1997).

The Mediterranean collision zone between the Eurasian and African plates has been early surveyed by repeated GPS campaigns, including several permanent GPS networks. The *eastern Mediterranean* is characterized by complicated movements of some cm/year, involving the Arabian and the Anatolian plates (Kahle et al., 2000). The *western Mediterranean and Western Europe*, on the other hand, are deforming only at slow rates (<5 mm/year over more than 1000 km). It follows that most of Europe behaves rigidly at a 0.5 mm/year level, but that the convergence process between the African and the

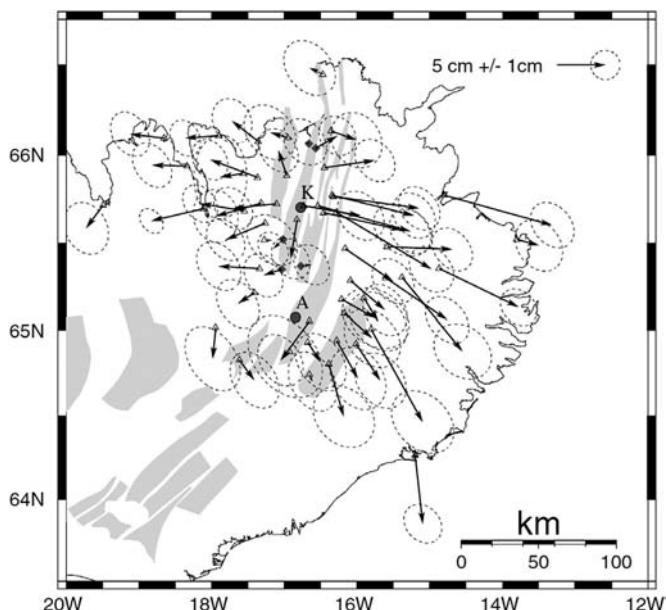


Fig. 8.22: Horizontal crustal deformations 1987–1990 in northeastern Iceland, as determined from repeated GPS measurements, with (assumed) non-movable stations in the Krafla fissure swarm, A Askja volcano, K Krafla volcano, after Völksen (2000).

Eurasian plate may differ significantly from the geological models (Nocquet and Calais, 2004). Another example for crustal deformations related to a collision zone (*Indian* and *Eurasian tectonic plates*) is given by repeated GPS surveys in southern Tibet and Nepal. Slip rates of 1 to 2 cm/year of the Indian plate beneath southern Tibet have been found here between 1991 and 2000 (Chen et al., 2004). A combination of gravity and GPS measurements carried out over two decades reveals an uplift of the Tibetan plateau at a mm/year level, with crustal thickening and mass loss beneath (Sun et al., 2009).

In Japan, a countrywide continuously operating GPS network (GEONET) has been established by the Geospatial Information Authority of Japan, containing about 1200 stations with an average station distance of 25 km (Miyazaki et al., 1997). Monitoring the three-dimensional displacement field at the subduction zone along the Japan trench is among the main objectives of this network (Tsuji et al., 1995), which delivered important information on crustal deformation related to strong earthquakes (see below).

Large-scale vertical crustal movements are found in areas of postglacial rebound, mountain building at plate collision zones, continental erosion, and sedimentary subsidence. While geometric leveling only allows repetition rates of several years to decades, GPS heighting (epoch measurements or permanent stations) offers the possibility to determine elevation changes with high temporal resolution. Repeated gravity measurements often support and extend these investigations, cf. [8.3.5].

It must be stressed that leveling and GPS heighting refer to different reference surfaces, i.e., the geoid and the ellipsoid, respectively. As the geoid is affected by mass redistributions, the leveling results should be reduced accordingly. For that purpose, the formulas developed for gravity field

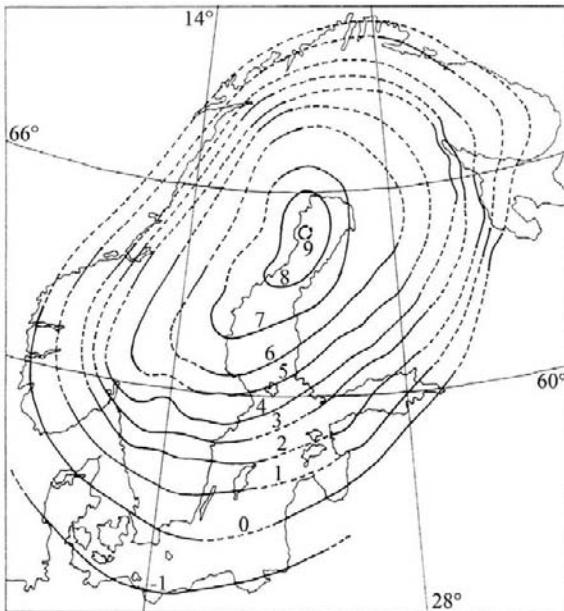


Fig. 8.23: Land uplift rates (relative to sea level) in mm/year, determined from tide gauge measurements and repeated geodetic leveling since 1892, after Ekman and Mäkinen (1996).

modeling can be used, now applied on gravity variations with time, cf. [6.6.1], [6.7.1]. Even with large mass shifts, as in the Fennoscandian land uplift area, this reduction remains significantly below 10% of the height changes and can often be neglected (Ekman, 1993).

Postglacial land uplift as occurring in Fennoscandia and Canada is due to isostatic adjustment, which involves the complete lithosphere, cf. [8.2.2]. The uplift is a function of the ice load time history and the Earth's mantle viscosity (Peltier, 2004). Present-day changes in ice cover as occurring in Antarctica and Greenland also result in vertical displacements, with, e.g., rates of several mm/year around Antarctica, and up to 10 mm/year and more around Greenland. The rapid melting of the Patagonia icefield even resulted in a crustal uplift rate of up to 39 mm/year, measured between 2003 and 2006 using GPS (Dietrich et al., 2010). Here we have an overlapping of elastic and viscoelastic response, the latter one due to past changes in ice coverage, and eventually several times larger than the elastic response (Wahr et al., 1995). Postglacial rebound effects can be also found in Earth rotation and sea level changes, [2.3.4] and [3.4.2], as well as in gravity field variations [8.3.5].

Fennoscandia is among the best-surveyed areas of recent vertical movements, with the postglacial land uplift being investigated by leveling, sea level data, GPS, and gravimetry, cf. [8.3.5]. The apparent land uplift (referring to mean sea level) as determined from leveling reaches a maximum of 9 mm/year (Fig. 8.23), and is associated with a viscous inflow of mass in the upper mantle (Ekman and Mäkinen, 1996; Vestøl, 2006), cf. [8.2.5]. Repeated GPS measurements confirm this uplift, where the vertical movement now is absolute (Fig. 8.24). In addition, the *horizontal strain* related to the isostatic adjustment process has also been derived from GPS data, with extreme values of 1 mm/year and more (Lidberg et al., 2007). From nearly 9 years of continuous GPS

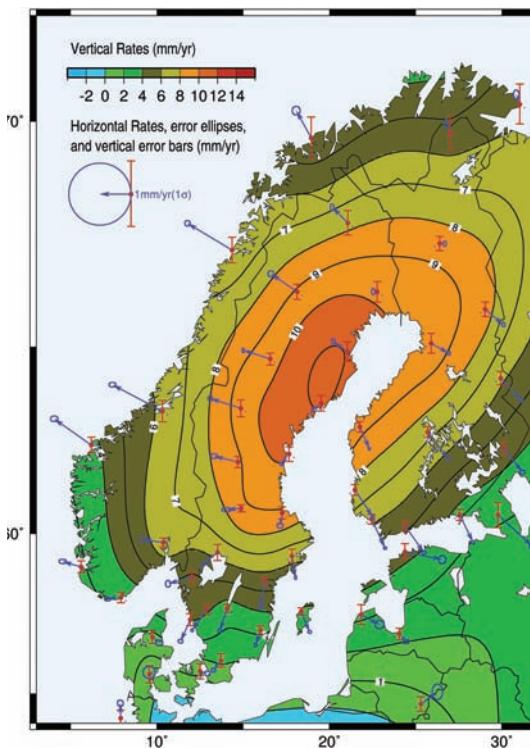


Fig. 8.24: Absolute land uplift rates in mm/year, determined from continuous GPS measurements from 1993 to 2007 (BIFROST Project) after Lidberg (2007).

observations, recent vertical and horizontal station velocities have been estimated with accuracies of about 0.5 mm/year (vertical) and 0.2 mm/year (horizontal).

Land uplift in Fennoscandia naturally also affects the definition of the vertical reference system, cf. [8.2]. For that reason, the precise leveling from the countries around the Baltic Sea were reduced to the epoch 2000.0. The geophysical land uplift model (lithosphere, mantle, ice sheet) used for the reduction was tuned to tide gauge observations and to uplift rates determined from leveling and permanent GPS stations. The adjusted normal heights refer to the zero level (epoch 2000) of the United European Leveling Network (Ågren and Svensson, 2006).

Large-scale vertical displacements of non- (or only partly) isostatic origin have been also found in other regions. The uplift generally remains less than 1 to 2 mm/year, and is difficult to interpret. For example, repeated leveling and continuous GPS measurements in the *western and central Alps* revealed a mountain uplift pattern with rates of 1 mm/year and more. These recent movements are probably caused by isostatic rebound after erosional unloading, but may also reflect tectonic processes at the convergent European/African plate boundary, with the Adriatic microplate rotating relative to stable Europe (Champagnac et al., 2009). From repeated leveling and GPS data collected at the German North Sea coastal region, areas of land subsidence reaching 1 to 1.5 mm/year have been found (Wanninger et al., 2009). While

more local effects are caused by the exploitation of natural gas and by sedimentary effects at the river estuaries, a large-scale edge effect of the Fennoscandian land uplift cannot be excluded.

Local investigations in earthquake and volcanic risk areas generally employ a multitude of geodetic techniques (terrestrial distance measurements, leveling, GNSS/GPS, strain and tilt measurements, gravimetry) and also InSAR, in order to detect precursor phenomena and to monitor surface deformations during and after activity phases (Rikitake, 1982; Rummel et al., 2009).

In *seismotectonically* active zones, geodetic data provide information on the accumulation of strain energy, its release during an earthquake, and the relaxation that follows the quake (Hudnut, 1995), where continuous GNSS/GPS measurements offer special advantage (Blewitt et al., 2006; Larson, 2009). Significant deformations have been found in connection with large earthquakes. Horizontal and vertical co-seismic displacements may easily reach the order of a few cm in an area of some 100 km to 1000 km (depending on the earthquake's magnitude) around the epicenter, and several meters close to it.

The *San Andreas Fault*, California, governed by the shear movements between the North American and the Pacific plates and affected by several large earthquakes in historical time, is among the areas where co- and inter-seismic slip rates are determined by geodetic methods since long time (Whitten, 1948; Gan et al., 2000). With a strong impetus from the 1992 Landers M7.3 earthquake (Wyatt et al., 1994), continuous GPS measurements now play an outstanding role (Larsen and Reilinger, 1992; Bock et al., 1997). More recently, co- and post-seismic displacements have been observed by GNSS in several seismically active regions, e.g., in Chile and Japan, among others. The 2010 Chile M8.8 earthquake occurred at the subduction zone between the Nazca and the South American plate. Based on GPS data from the SIRGAS network stations, cf. [7.3], co- and post-seismic horizontal and vertical displacements at the cm- to dm-order of magnitude have been found, occurring up to a distance of 1500 km from the epicenter, and reaching about 3 m close to it (Drewes and Heidbach, 2012). The 2011 Tohoku (Sendai) M9.0 earthquake was related to the plate collision process at the *Japan* trench subduction zone. From the continuously operating Japanese GPS network (see above) slip rates of several meters have been observed over large areas before, during and after the earthquake (Fig. 8.25.), with a maximum co-seismic displacement of about 30 m close to the epicenter (Miyazaki et al., 2011).

Geodetic monitoring of *volcanoes* allows, in addition to classical repeated surveys, the extensive employment of data recording systems. This is due to the well-known location of the investigation object. Volcano monitoring methods especially include GPS measurements, supported by leveling and gravimetry, cf. [8.3.5]. Strain and tilt measurements also serve for observing the phases of volcanic activity, but suffer not only from atmospheric and hydrological effects, but also from disturbances through local topography and geology (cavity effects), cf. [5.5.5], Takemoto (1995), Zadro and Braitenberg (1999).

In addition, InSAR mapping has proved to be an efficient tool for the investigation of crustal deformation related to volcanic activity. This is demonstrated by Fig. 8.26, with samples of the deformation (in the sensor's line of sight) of the Alcedo caldera (Galapagos Islands) between October 1997 and November 2000. The deformation is estimated from a stack of 14 descending track SAR images acquired by the ERS satellite, and refers to the north-western corner of the image which is assumed to be stable. The Stanford method for persistent scatterer radar interferometry was used for the analysis (Hooper,

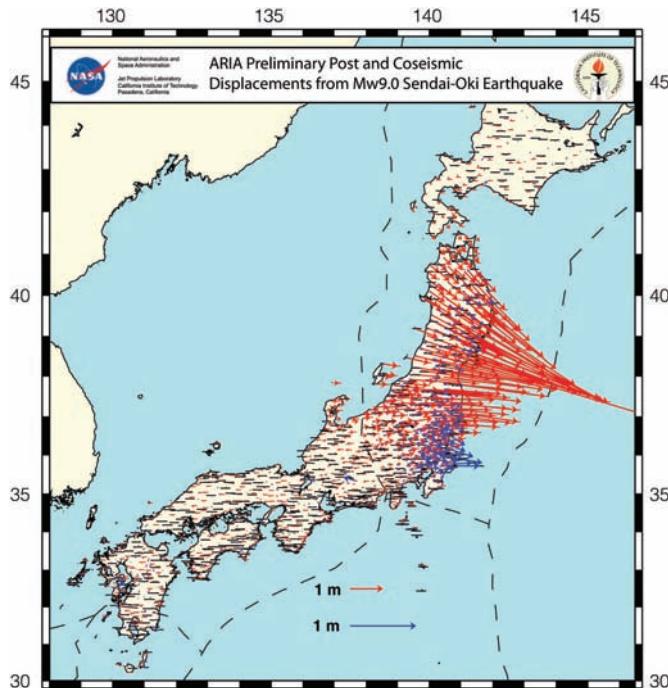


Fig. 8.25: GPS-derived rates of horizontal shifts caused by the big Sendai earthquake. Co-seismic displacement is shown in red, and first hour of post-seismic motion is shown in blue, including motion caused by aftershocks. Preliminary GPS time series provided by the ARIA team at JPL and Caltech. All original GEONET RINEX data provided to Caltech by the Geospatial Information Authority (GSI) of Japan.

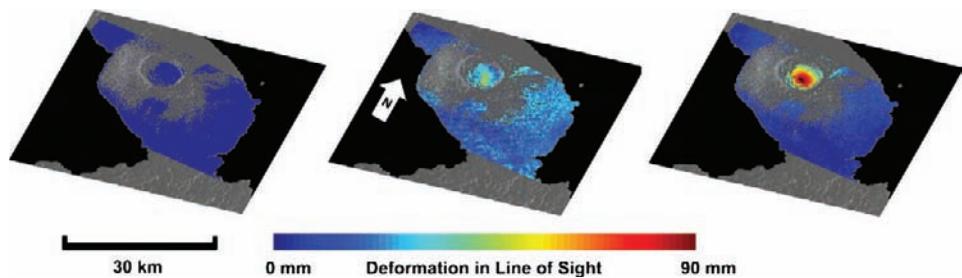


Fig. 8.26: Displacements in line of sight, Alcedo caldera (Galapagos islands). Samples from a SAR series (ERS satellite, 10.1997/03.1999/11.2000); Institut für Photogrammetrie und GeoInformation, Leibniz Universität Hannover.

2006). The uplift within the caldera (up to several 10 mm/year) is clearly visible and probably driven by crystallization processes in the magma chamber.

Geodetic methods thus contribute in different ways to the modeling of volcanic processes and the forecasting of volcanic eruptions (Dvorak, 1995; Dzurisin, 2003). Large deformations occurring at major eruptions and connected with magma injection and

outflow can be easily observed. A prediction of active volcanic phases, on the other hand, is still difficult as volcanoes are inherently unstable, with surface movements ranging from slow spreading to sudden collapses. In addition, recorded precursor signals may be strongly deteriorated by environmental disturbances.

Among the routinely surveyed active volcanoes are the Kilauea and Mauna Loa, Hawaii (Owen et al., 2000), Long Valley, California (Rundle and Whitcomb, 1986), and Mount Etna, Italy (Bonaccorso et al., 1995). At the Mount Etna flank project, GPS and InSAR results detected slip rates between 1993 and 2006 which varied between several mm/year and meters/week, with the largest instability events associated with major eruptions (Neri et al., 2009).

Man-made vertical crustal movements are related to the exploitation of natural gas, oil, and geothermal fields, the withdrawal of groundwater, mining, and load changes in water reservoirs, among others. They are of more local character and generally result in surface subsidence. Monitoring is carried out by repeated leveling, GPS heighting, gravimetry, and InSAR, cf. also [8.3.5].

8.3.5 Gravity field variations with time

Gravity variations with time result from a multitude of sources, cf. [3.5]. Here we consider the variations that are caused by the redistribution of terrestrial masses, while tidal effects are discussed in [8.3.6]. All these variations are of importance for geodesy, as they affect Earth rotation and reference systems, and are closely related to Earth surface deformations. The geophysical information inherent in the time-variable gravity field is, on the other hand, of extreme value for modeling geodynamic processes.

Gravity field changes with time can be derived from the long-term analysis of satellite orbits, from dedicated gravity satellite missions like GRACE, and from repeated terrestrial gravity measurements. While gravity field data derived from satellites are independent from vertical displacements of the Earth's surface, terrestrial gravity measurements depend on them and always contain the effect of mass redistribution and vertical shift of the observer.

Global gravity field variations were determined early from the *harmonic coefficients* of the gravitational field obtained from satellite observations (satellite laser ranging to LAGEOS, cf. [5.2.6]) over about three decades (Cheng and Tapley, 2004). Secular changes of the low degree zonal harmonics (up to degree 5) have been clearly analyzed using SLR data, with a change of $\dot{J}_2 = dJ_2/dt = -2.6 \times 10^{-11}$ /year for the dynamical form factor. It mainly results from postglacial rebound in the polar regions, but other geophysical processes may also contribute (Mitrovica et al. 2009). Annual and seasonal variations of the second degree harmonics are related to mass redistribution in the atmosphere, the oceans, the ice shields, and the continental groundwater (Cheng and Tapley, 1999). If the harmonics of degree one are included in the evaluation, variations indicate the movement (a few mm to cm) of the geocenter with respect to the terrestrial reference frame, as realized by the coordinates of the tracking stations (Swenson et al., 2008), cf. [2.4.2], [3.3.4].

A significantly higher resolution in space and time is achieved by dedicated *satellite gravimetry missions*, the GRACE mission (Tapley et al., 2004; Chen and Wilson, 2008) being the first experiment of this type, cf. [5.2.8], Wahr (2009). Providing regularly monthly and partly also weekly solutions, a spatial resolution of about 300 km (corresponding to a

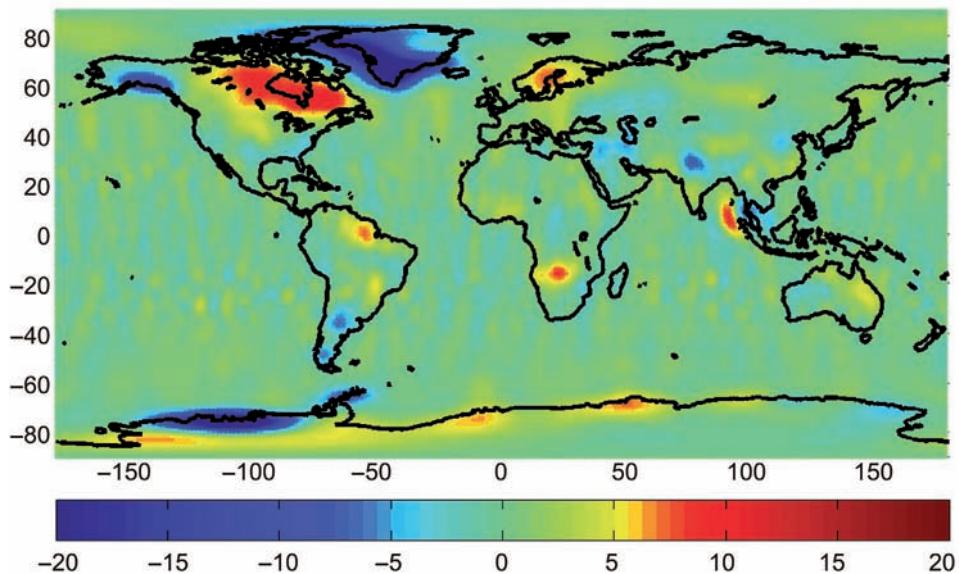


Fig. 8.27: Global linear gravity changes in $\text{nms}^{-2}/\text{year}$ calculated from monthly GRACE gravity models (01.2003–07.2011) of the GFZ analysis center, Gaussian filtering with 400 km radius; data provided by <ftp://podaac-ftp.jpl.nasa.gov/allData/grace/L2/GFZ/RL04/>; IfE, Leibniz Universität Hannover.

spherical harmonic development up to degree and order 60) is achieved. This allows the investigation of a multitude of mass redistribution phenomena, on temporal scales ranging from secular via decadal and seasonal down to monthly and even sub-monthly. The underlying mass transports are strongly associated with the global water cycle, with a complex interaction of hydrosphere (oceans and land hydrology), cryosphere, and atmosphere, and with geodynamic processes on the surface and in the interior of the Earth (e.g., Van Dam et al., 2007). The results obtained include effects due to ocean mass changes (non-steric sea level change) and melting of ice-sheets and glaciers, to variations of the continental water storage (e.g., at tropical river systems like the Amazon, Congo or Ganges), to post-glacial rebound (Canada, Fennoscandia, etc.), and to large earthquakes, cf. also [8.3.3], [8.3.4], among others. Man-made contributions have been also found, for example through considerable mass loss resulting from the irrigation of large areas in India, and subsequent groundwater subsidence (Chen, 2007; Chen et al., 2007b; Rodell et al., 2009).

The interpretation of monthly GRACE-derived gravity field solutions is based primarily on the temporal variation of gravity and of the geoid. The following examples demonstrate some *global* results.

A linear trend in *gravity changes* between 2003 and 2011, as derived from monthly gravity models of degree and order 120 (GFZ analysis center) is shown in Fig. 8.27. The high-frequency gravity field part has been Gaussian-filtered (Jekeli, 1981) with radius 400 km, in order to suppress noise. The gravity changes reach ± 10 to $15 \text{ nms}^{-2}/\text{year}$ and more. Gravity increase is clearly correlated with isostatic rebound processes in Northern America and Europe (see below), and with water storage change, e.g., in the Amazon region. Gravity decrease becomes visible through ice melting in Greenland, Alaska, and the Antarctic (Chen et al., 2006; Schrama and Wouters, 2011). Co-seismic mass redistribution related

to the Sumatra-Andaman earthquake is visible in southeast Asia, with negative gravity change at the subduction zone and positive change at the uplift zone (Chen et al., 2007a).

Temporal variations of the *geoid* have been discussed since a long time, where we have to distinguish between a shift in the geoid potential value, cf. [3.4.], and the geometrical change due to the geoid height variations (Ekman, 1989). Mean sea level variations affect the oceanic, but also the continental geoid (Kuhn, 2002). These changes are superposed by the effect of the manifold large-scale mass shifts in the Earth's interior and on the surface of the solid Earth (see above). The resulting geoid variations may reach annual variations of about 10 mm amplitude, with regionally very different behavior, while the long-term trend remains at the order of 0.1 mm/year.

Geoid height variations estimated from monthly GRACE data between 2003 and 2011 are shown in Figs. 8.28 and 8.29, where data were smoothed using a 600 km Gaussian-filter, and atmospheric and ocean effects reduced. Larger annual cycle amplitudes of hydrological origin can be recognized in the river basin of Amazon, Niger, Zambesi and Ganges. The geoid height trend is correlated with postglacial land uplift and polar ice reduction, among others.

The potential of GRACE results for estimating more *regional mass changes* is demonstrated by examples referring to the accelerated ice mass loss in Greenland, and to hydrology-induced variations in central Siberia.

In *Greenland*, significant ice mass loss has been observed by GRACE for the time span 2003–2010 (Sørensen and Forsberg, 2010; Schrama and Wouters, 2011). Expressed, e.g., as surface density trend, a different spatial distribution of the mass loss becomes visible, which amounts to about 200 Gt/year averaged over whole Greenland during the observation epoch (Fig. 8.30). These results are supported by ICESat altimetry (Ewert et al., 2011). Mass losses of the Antarctic iceshield also reach 100 Gigatons/year, as derived from GRACE monthly solutions between 2002 and 2008 (Horwath and Dietrich, 2009).

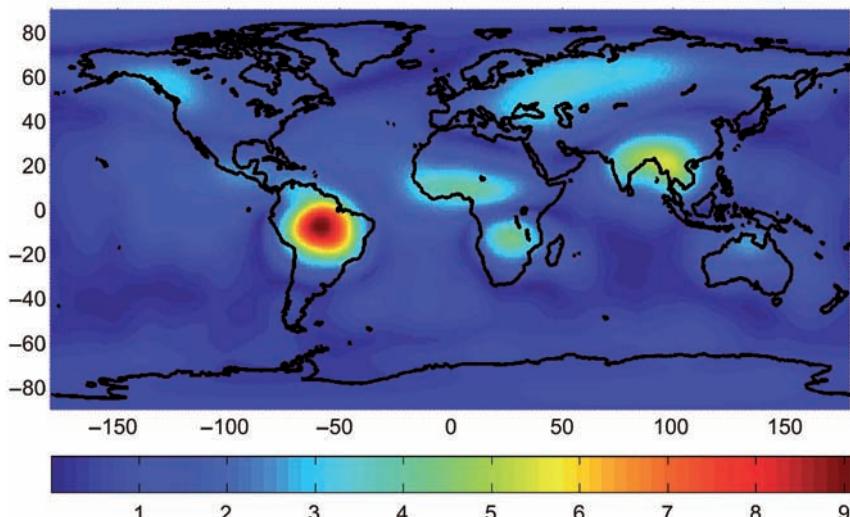


Fig. 8.28: Annual amplitude (mm) of geoid height variation estimated from monthly GRACE gravity field solutions (01.2003–07.2011) provided by GFZ, Gaussian-filtering with 600 km radius; IfE, Leibniz Universität Hannover.

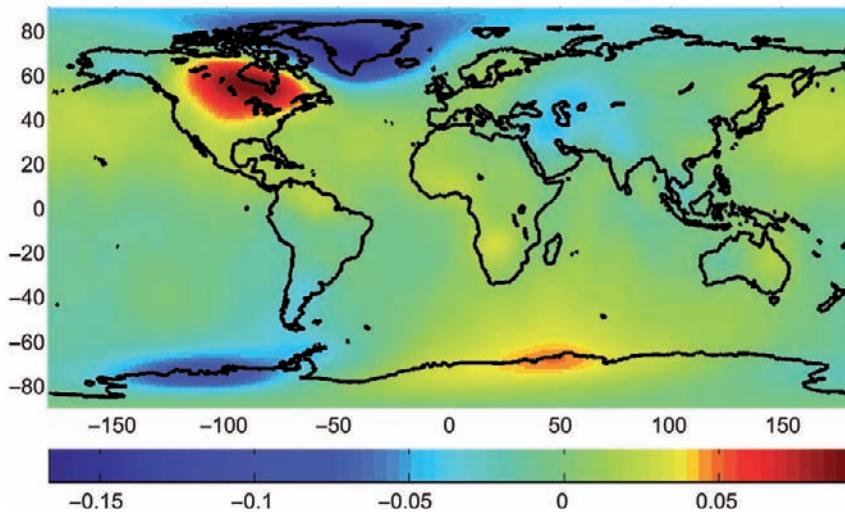


Fig. 8.29: Trend in geoid height variation (mm/year) estimated from monthly GRACE data (01.2003–07.2011) provided by GFZ, Gaussian-filtering with 600 km radius, IfE, Leibniz Universität Hannover.

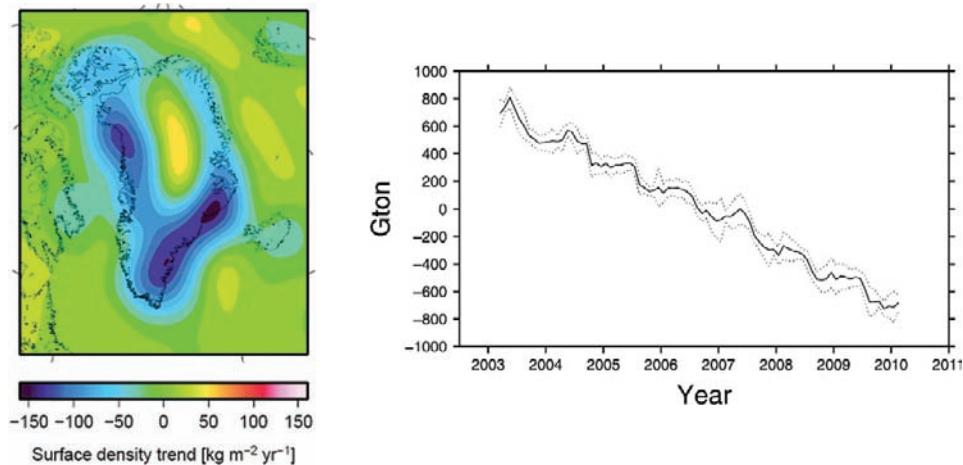


Fig. 8.30: Ice mass changes in Greenland, expressed as surface density trend ($\text{kgm}^{-2}/\text{year}$, left part, Ewert et al., 2011), and averaged mass loss (Gigatons) for epoch 2003–2010, after Schrama and Wouters (2011).

The effect of hydrological variations in a *Siberian permafrost location* is demonstrated by the monthly variations in equivalent water column (EWC) from GRACE for the station Yakutsk, central Siberia (Fig. 8.31). In addition to the annual cycle there is an increase in water mass until 2007 related to strong rain and subsequent snow fall, but there is no significant trend over the whole period (Müller et al., 2011b).

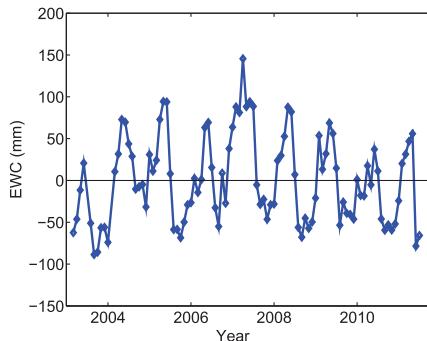


Fig. 8.31: Monthly variations in equivalent water column (EWC) from GRACE for the station Yakutsk, Siberia. Data provided by GFZ, Gaussian-filtering with 340 km radius; IfE, Leibniz Universität Hannover.

A limiting factor of satellite-derived gravity field (static as well as time varying) solutions is the *omission error*, due to the un-modeled part of the field, cf. [6.6.1]. Recent GRACE and GOCE geoid solutions, e.g., are still affected by omission errors of 0.3 to 0.4 m, while the accuracy of the modeled part (commission error) is reaching an order of magnitude of 1 nms^{-2} and 1 cm (static gravity field), and $1 \text{ nms}^{-2}/\text{year}$ and 0.1 mm/year (time-variable field), respectively, cf. [6.6.2].

This has led to discussing the needs for *future satellite gravity field missions*, under the aspects and demands of Earth sciences (Flury and Rummel, 2005a). Requirements for future gravity field missions include a spatial resolution down to 50 km, which is very likely the limit for measurements from space. A higher resolution, as for instance necessary for the "cm-geoid", will still require the use of terrestrial measurements and high resolution terrain models (Flury and Rummel, 2005b). A synopsis of future science requirements on geoid and gravity field is given in Sneeuw et al. (2005), together with a scenario of possible space missions (combination of results obtained from very high altitude satellites, satellite-borne gradiometry, and low-low satellite-to-satellite tracking, extended to configuration flights with inter-satellite tracking in several spatial directions). A follow-on gravity mission to GRACE is discussed by Loomis et al. (2011).

Repeated *terrestrial* absolute and relative gravity measurements are required in order to detect *regional* and *local* gravity changes with time. The surface-based gravity data can provide a higher spatial and temporal resolution than the gravity field determinations from space. Corresponding investigations concentrate on areas where recent mass changes occur, caused by mass redistributions due to, e.g., postglacial uplift, mountain building, earthquake and volcanic activity, and man-made land subsidence, cf. [8.3.4]. Moreover, absolute gravity measurements may support the vertical control of tide gauges, and serve as ground truth for the variable gravity field derived from satellite missions like GRACE (Timmen, 2010).

In order to detect and analyze the small gravity changes associated with global or large-scale geodynamic phenomena, a high measurement accuracy and the adequate *reduction* of tidal and loading effects is required. Present-day models of the *solid Earth* and the *ocean tides* allow the reduction of the gravimetric tidal effects (including tidal loading) for most parts of the continents, with an accuracy of a few nms^{-2} , larger deviations may occur close to the coast. Reductions due to non-tidal ocean mass redistribution (Kroner et al., 2009) and ocean pole tide are small and can be reduced sufficiently, this is also valid for the polar motion effect on gravity ("gravity pole tide"), cf. [5.4.1], [8.3.6].

The effects of *atmospheric pressure* changes may cause gravity changes of 100 nms^{-2} and more, due to the direct attraction and the indirect loading effect. They can be modeled approximately by a Bouguer plate, where an empirical coefficient of regression also takes the loading effect into account, cf. [5.4.1]. A refined reduction is based on atmospheric Green's functions calculated for a model atmosphere on a spherical elastic Earth (Merriam, 1992; Guo et al., 2004). The main contribution to the reduction results from the gravitational part of a local zone (radius 0.5° around the gravity station), meteorological data as supplied from Weather Forecast Agencies data significantly improve the reduction accuracy (Gitlein and Timmen, 2007; Abe et al., 2010). Atmospheric pressure effects have to be taken into account at absolute gravity measurements and at continuous gravity recording, whereas they cancel at relative gravity measurements.

Temporal variations of the *groundwater level* and *soil moisture* mainly occur seasonally, with superimposed short-term fluctuations of a few hours to a few days. They may produce maximum gravity changes of 50 to 100 nms^{-2} (seasonal), and several 100 nms^{-2} at strong rainfall. For simple hydrological structures, a reduction is possible again by applying the Bouguer plate model

$$\delta g_{\text{groundwater}} = 4.2 P \delta H \text{nms}^{-2}, \quad (8.16)$$

with P pore volume (%), and δH change of groundwater level in m. A corresponding relation holds for the soil moisture reduction (Mäkinen and Tattari, 1988). A more refined reduction is generally handicapped by missing data on local and regional/global hydrology. Station specific topography and geology may contribute a few 10 nms^{-2} , and large-scale hydrological effects may reach 10 nms^{-2} and more, for time scales of days to years (Kroner et al., 2007). This requires sophisticated local modeling eventually supported by global hydrological models, as provided, e.g., by the WaterGap Hydrological Model WGHM (Döll et al., 2003).

Postglacial rebound in Fennoscandia and in Canada has been monitored early also by terrestrial gravimetry, supporting tide gauge observations, geometric leveling, and GPS measurements, cf. [8.3.4], while GRACE results contribute to large-scale information (see above).

In *Fennoscandia*, relative gravimetry profiles delivered an average value of $-2 \text{ nm s}^{-2}/\text{mm}$ for the ratio of gravity change and absolute land-uplift rate, where a geoid change of 0.6 mm/year had to be applied to the leveling results (Ekman and Mäkinen, 1996). Since 2003, repeated absolute gravity measurements have been carried out by different institutions, in order to independently monitor the land uplift and to validate the temporal variations obtained from GRACE (Gitlein, 2009; Müller et al., 2011a). Gravity variations of -10 to $-20 \text{ nms}^{-2}/\text{year}$ have been found from annual repetitions over 4 to 5 years, with a gravity to height variation ratio of $-1.6 \text{ \mu ms}^{-2}/\text{m}$. This agrees well with the assumption of a Bouguer plate effect with mass increase in the upper mantle (Timmen, et al., 2011), see below. For comparison with the GRACE temporal gravity field, the absolute measurements have been reduced by the free-air gravity gradient, thus taking the effect of height changes into account, Fig. 8.32. Absolute gravimetry and GRACE results agree well, especially near the uplift center, and differ more at the supposed zero-uplift line; combining the data improves the data-based model of the present-day secular mass variation.

In *Canada*, relative gravity measurements carried out over 40 years have been combined with repeated absolute gravity observations which started in the 1980s. Although the resulting map of secular variations of gravity is rather inhomogeneous with respect

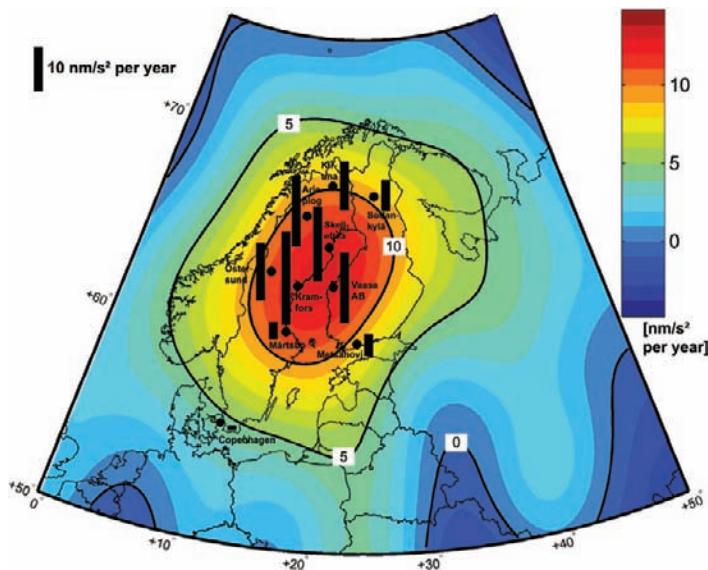


Fig. 8.32: Linear gravity changes for Fennoscandia derived from GRACE GFZ monthly solutions (08.2002–09.2008, Gaussian filter radius 400 km) and from terrestrial measurements at 10 stations (absolute gravimetry with FG5-220 and GPS shown as black bars, after Gitlein (2009)).

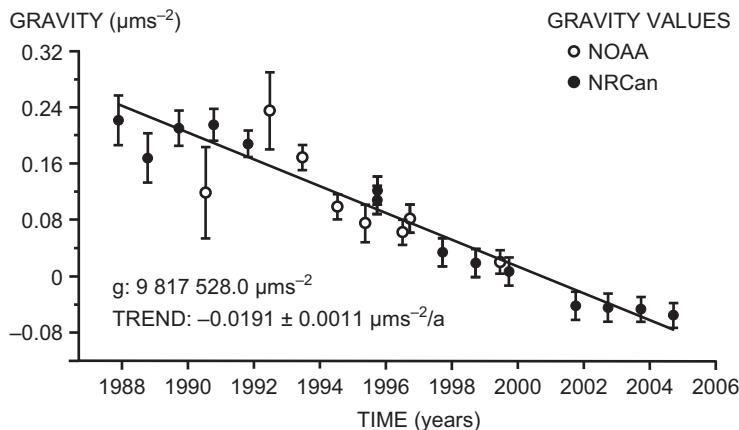


Fig. 8.33: Absolute gravity variations (95% error bound) and linear gravity trend (1987–2005) at Churchill, Manitoba, Canada, observed by NRCan and NOAA, employing JILA (until 1993) and FG5-model instruments, after Lambert et al. (2006).

to accuracy (a few nms^{-2} on the average), it provides constraints for the evaluation and refinement of post-glacial rebound models (Pagiatakis and Salib, 2003). Absolute gravity monitoring over nearly two decades at 10 field sites yields gravity changes of -10 to $-20 \text{nms}^{-2}/\text{year}$, after reduction of gravity changes due to ocean tide loading, and soil moisture and water table variations. The residual long-term trend is clearly associated with postglacial rebound (Lambert et al., 2006), Fig. 8.33.

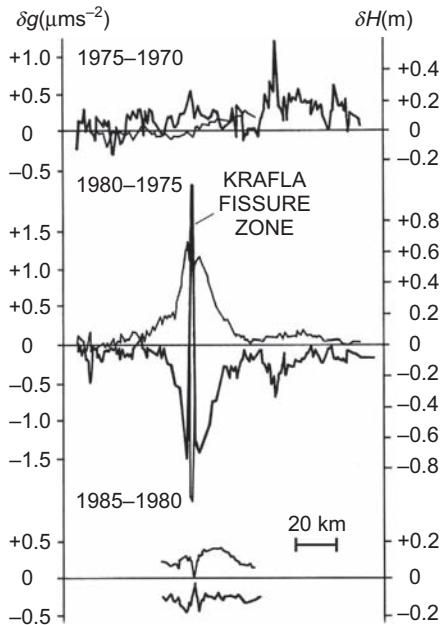


Fig. 8.34: Long-term gravity and height changes along an EW-profile ($\varphi = 65^{\circ}40'$) in northern Iceland, related to the Krafla rifting episode, after Torge et al. (1992).

Gravimetry is also extensively applied at *tectonic plate boundaries* and especially in areas of *seismotectonic* activity, adding valuable information to geometric deformation monitoring. While gravity changes caused by slow plate tectonic processes are still difficult to identify, local effects due to subsidence of sedimentary basins and seasonal hydrology could be extracted from observations over several years, e.g., in the Venezuelan Andes (Drewes et al., 1991). Seismically induced gravity changes have been found from terrestrial gravity data for the Alaska 1964 earthquake (Barnes, 1966), and since then at several tectonically active zones as, e.g., California (Jachens et al., 1983) and Japan (Satomura et al., 1986). The Krafla rifting process, cf. [8.3.4], in northern Iceland mirrored itself in gravity and height variations with significant correlation (Torge et al., 1992), Fig. 8.34. Co- and post-seismic gravity changes observed around the Krafla volcano have been evaluated together with other geodetic data, for describing the mass transport and vertical displacements at the evolution of the magma chamber and the associated rifting (De Zeeuw-van Dalfsen et al., 2006). Occasionally, gravity changes of a few μms^{-2} have been observed before strong *earthquakes*, one example being the 1976 Tangshan/China (M7.8) earthquake (Li et al., 1989). The GRACE results offer the possibility to recognize the large-scale temporal gravity variations related to strong (partly reaching M9 magnitude) earthquakes, examples being the Sumatra (2004), Chile (2010), and Japan (2011) events, with gravity changes reaching 50 nms^{-2} and more (Chen et al., 2007a; Heki and Matsuo, 2010; Matsuo and Heki, 2011).

Volcano monitoring, in most cases, also includes gravimetry, which has proved to be an efficient tool for detecting magma inflation and deflation, and to contribute to eruption

forecasting and observation of the phase of activity (Rymer and Williams-Jones, 2000; Battaglia et al., 2008). Extensive gravity measurements based on dedicated control networks are – since several decades – carried out on and around volcanoes in Italy, Japan, and the U.S.A., among others, where gravity changes up to $1 \mu\text{ms}^{-2}$ have been observed related to magma rising and withdrawal (Jachens and Roberts, 1985; Berrino and Corrado, 2008; Greco et al., 2010). Continuous gravity measurements offer additional opportunities at volcano monitoring and prediction of eruptions (Williams-Jones et al., 2008).

Repeated gravity measurements also contribute to the investigation of land subsidence caused by *man-made* activities, including predictions on the subsurface mass redistributions. This includes the exploitation of geothermal fields (Hunt and Kissling, 1994) and of natural gas and oil (Van Gelderen et al., 1999), the withdrawal of groundwater (Chapman et al., 2008), and the effects of mining (Lyness, 1985).

As discussed above, repeated gravity measurements are often combined with height determination, by leveling or by GNSS/GPS. The latter method delivers “absolute” height changes, while leveling results refer to the geoid, which is also affected by (small) temporal variations. As the observed gravity change contains the combined effect of internal mass redistribution and a vertical shift of the observer, the ratio between gravity change and vertical displacement contains information on the mass redistribution process (i.e., the rheology of crust and mantle). Corresponding investigations have been carried out especially with respect to postglacial rebound (see above), tectonic motions, co-seismic deformation, volcanic activity, and atmosphere/hydrosphere surface loading. Generally, the *gravity-to-height variation ratio* for tectonic motions may vary between -1.5 and $-3.5 \mu\text{m s}^{-2}/\text{m}$ (Jachens, 1978). The free-air relation of $-3 \mu\text{m s}^{-2}/\text{m}$ is often found locally and corresponds to a vertical shift without mass changes (e.g., dilating sphere). For larger areas, the Bouguer plate relation of $-2 \mu\text{m s}^{-2}/\text{m}$ is more typical, indicating internal mass displacements, cf. [6.5.3]. More sophisticated models have been developed for the gravity-to-height variation ratio due to surface loads (continental hydrology, atmospheric pressure, ocean tides), taking the extension of and the distance to the load into account (De Linage et al., 2009).

8.3.6 Earth tides and tidal loading

The reaction of the solid Earth’s surface to the tidal forces results in deformations and gravity changes. These effects are visible in geodetic measurements, and have to be reduced for time-independent geodetic modeling. As the observed tidal signal contains different kind of information on the Earth’s interior, it is of high interest for geophysics. Corresponding modeling and interpretation requires the reduction of “disturbing” effects which especially result from atmospheric, oceanic, and hydrological loading, cf. [8.3.1]. In the following, we discuss the fundamentals of solid Earth tides including tidal loading, and some results obtained.

Tidal effects on a *rigid* Earth can be calculated from the ephemerides of the moon, the sun, and the planets, through a spherical harmonics development of the tidal gravitational potential, cf. [3.5.2]. In reality, the *solid* Earth reacts to the tidal forces primarily like an elastic body with deformation: Solid *Earth tides* (also *Earth body tides*). Tidal variations are also generated in the oceans and – to far less extent – in the atmosphere: *Ocean tides*, cf. [3.4.2], and *atmospheric tides*. The tidal deformation and potential change at the solid Earth surface is superimposed by the corresponding loading effects:

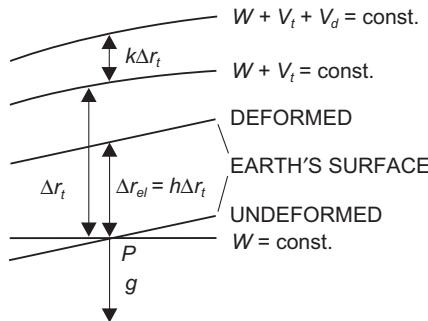


Fig. 8.35: Tidal-induced vertical shift of a level surface and the physical surface of the Earth.

tidal loading. Tidal theory and measurements are described in the classical work by Melchior (1983), and with a more recent status in Wilhelm et al. (1997). For Earth tides see, e.g., Wang (1997) and Agnew (2009).

The fundamental theory on the tidal response of an *elastic*, spherically symmetric, non-rotating, oceanless Earth goes back to Love (1911). Deformations and potential change caused by the *Earth tides* can be represented by applying coefficients of proportionality called *Love numbers* on the tidal potential V_t (3.116) of a rigid Earth. The dimensionless *Love numbers* h , k , l (l also called *Shida number*) are functions of density and the Lamé parameters (compressibility and rigidity), and they depend on the degree of the spherical harmonic expansion of the tidal potential (3.117). Again restricting ourselves to the dominant term of degree two, the following relations hold between the tidal potential V_t and the tidal effects on an elastic Earth.

The *vertical deformation* of the Earth's surface is modeled by the Love number h (Fig. 8.35)

$$\Delta r_{el} = h \Delta r_t, \quad (8.17a)$$

where the shift of the level surface follows from the fundamental relation (3.52) between the changes of potential and height:

$$\Delta r_t = \frac{V_t}{g}. \quad (8.17b)$$

The *horizontal* displacement in NS- and EW-direction is obtained correspondingly, and controlled by the Shida number l :

$$\Delta x_{el} = \frac{l}{g} \frac{\partial V_t}{\partial \bar{\varphi}}, \quad \Delta y_{el} = \frac{l}{g} \frac{\partial V_t}{\cos \bar{\varphi} \partial \lambda}, \quad (8.18)$$

with $\bar{\varphi}$, λ geocentric latitude and longitude.

The tidal-induced mass shift causes an additional *deformation potential* which is proportional to the tidal potential, according to the Love number k :

$$V_d = k V_t. \quad (8.19)$$

For the surface of a stratified spherical Earth model like PREM, cf. [8.1], the Love numbers of degree 2 amount to

$$h = 0.60, \quad l = 0.08, \quad k = 0.30.$$

The *gravitational potential* on the Earth's surface experiences a tidal-induced change V_{el} which is composed of the direct attraction and the deformation part V_t and V_d , and the potential change due to the vertical shift of the surface. By introducing (8.19) and (8.17) we obtain:

$$V_{el} = V_t + V_d - g\Delta r_{el} = V_t(1 + k - h). \quad (8.20)$$

Differentiating with respect to the radial distance r delivers the *vertical* component of the tidal *acceleration*. According to (3.117), (3.118), we have for the rigid Earth

$$b_r = \frac{\partial V_t}{\partial r} = 2\frac{V_t}{r}. \quad (8.21a)$$

Expressing the deformation potential by a spherical harmonic expansion of degree two, and taking (8.19) into account, results in

$$\frac{\partial V_d}{\partial r} = -\frac{3}{r}V_d = -\frac{3}{r}kV_t. \quad (8.21b)$$

Inserting (8.21a, b) into the vertical derivative of (8.20), and taking (3.118) and (8.17) into account yields the vertical tidal acceleration

$$b_{r(el)} = \left(1 - \frac{3}{2}k + h\right)b_r, \quad (8.22a)$$

with the *gravimetric* (amplitude) *factor*

$$\delta = 1 - \frac{3}{2}k + h \quad (8.22b)$$

already introduced in (5.97).

The *horizontal* component of the tidal acceleration and its relation to the corresponding component on a rigid Earth (3.119) follows from

$$b_{\psi(el)} = -\frac{\partial V_{el}}{r\partial\psi} = (1 + k - h)b_\psi, \quad (8.23a)$$

with the *tilt* (amplitude) *factor*

$$\gamma = 1 + k - h. \quad (8.23b)$$

With the above model values for the love numbers h and k we obtain

$$\delta = 1.16, \gamma = 0.69.$$

By applying Love numbers on the tidal effects for a rigid Earth, cf. [3.5.2], we estimate the tidal "perturbations" on the elastic Earth at the order of magnitude of a few decimeter in height, 1 to 2 $\mu\text{m s}^{-2}$ in gravity, 0.01" to 0.02" in tilt, and 10^{-7} to 10^{-8} in strain. Hence, they are clearly visible in geodetic data series. It should be noted that the gravity change observed on an elastic Earth is larger than on a rigid one, which is due to the vertical shift of the observer. The tilt factor mirrors the flexibility of the Earth's surface with respect to the tidal force.

Refined *Earth tide models* use the density and elastic parameters of a geophysical Earth model like PREM, with slight surface layer modification, cf. [8.1]. They solve for an ellipsoidal, rotating Earth in hydrostatic equilibrium, where rotation and ellipticity result in a slight latitude dependence of the tidal parameters (Wahr, 1981b; Dehant, 1987). An inelastic non-hydrostatic equilibrium Earth model also takes mantle visco-elasticity into account,

and includes a small frequency-dependent increase of amplitude and phase delay, Dehant et al. (1999). The discrepancies between these models are of the order of 0.1% only, but measured tidal parameters may deviate significantly from the model values due to loading effects, to local inhomogeneities in the crust, and to recent geodynamic processes.

The “disturbing” geophysical signals entering into time series of Earth’s rotation, geometry and gravity field observations have been discussed before. Here, we concentrate on *tidal loading* and its effect on the solid Earth’s surface. Although formally treated as loading effects of atmospheric and oceanic origin, it is distinguished from them by its well-known driving force.

Ocean tidal loading is caused by the tides of the oceans, and composed of the direct attraction of the water masses and their loading effect on the Earth’s surface (Jentzsch, 1997). Superposing the tides of the solid Earth, loading effects are especially pronounced in the semi-diurnal waves, where they may reach several percent of the Earth tides at stations located in the continent’s interior. Close to the coast, the loading effect may assume up to 10% of the gravimetric tidal signal, several 10% in strain, and 100% and more in tilt, with corresponding deviations in phase shift; the vertical displacement may reach 10 cm.

Modeling of ocean tidal loading is based on ocean tide models as derived from the hydrodynamic equations, and assimilated by different types of observations, cf. [3.4.2]. It follows the theory developed by Farrell (1972), which describes the response of an elastic Earth model to a point load on its surface. The loading effects (for displacement, gravity/tilt, strain) are computed by a convolution integral of the relevant Green’s function and the tidal model (amplitude/phase), over the loaded region. Where, according to [8.3.1], Green’s functions are formed by the weighted sums of the load Love numbers and the spherical harmonics, depending on the spherical distance to the load. The degree-dependent *load Love numbers* h'_l , l'_l , k'_l are computed for a reference Earth model like PREM, and – in analogy to the development for the Earth’s tides – refer to the vertical and horizontal displacement, and to the potential of the deformed Earth. But, depending on the location and the dimensions of the load, it is now necessary to extend the series expansion to rather high degrees, e.g., to $l = 10\,000$.

The solar heating of the atmosphere causes surface pressure oscillations, at periods of diurnal and semi-diurnal solar days. The *loading* effects induced by these “*atmospheric tides*” manifest themselves, e.g., in vertical surface deformations of 1 to 2 cm, while horizontal deformations are one order of magnitude smaller. Modeling is possible by a corresponding tidal model based on global surface pressure data collected for weather forecast (Boy et al., 2006). Contrary to this “thermic” effect, the direct (gravitational) effect of the lunisolar tides can be neglected, as it remains at least one order of magnitude below.

Continuous gravity recording has reached a high level of accuracy, and contains not only tidal effects but also gravity variations induced by a variety of geophysical processes (Agnew, 2009; Neumeyer, 2010). Here, elastic-spring type gravimeters provide the short-periodic partial tides, while superconducting instruments, characterized by high sensitivity and low drift rate, also deliver long-periodic tides, the pole tide, cf. [5.4.6], and a multitude of other geophysical information. *Strain-* and *tilt-meter* measurements are of less importance at this aspect, as they are disturbed frequently by local crustal heterogeneities. Consequently, they fail at solving global problems, but are useful, e.g., for monitoring seismic and volcanic activities, cf. [5.5.5]. Data series obtained from continuous (or repeated) monitoring of *space geodetic stations* (VLBI, SLR, LLR, GNSS) can be evaluated with respect to the tidal deformation of

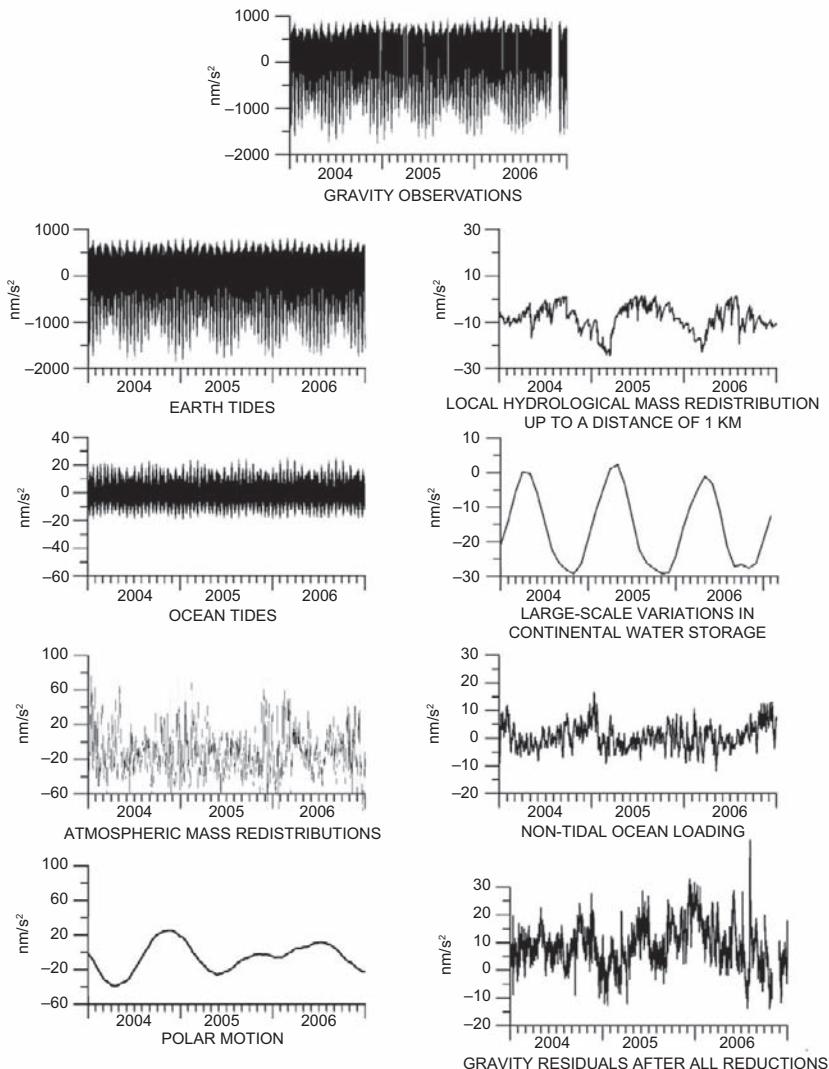


Fig. 8.36: Recorded gravity signal (linear instrumental drift removed) 2004–2006, Earth tide station Moxa, Institute of Geosciences, Applied Geophysics, Friedrich-Schiller-University, Germany ($\varphi = 50.64^\circ\text{N}$, $\lambda = 11.62^\circ\text{E}$, $H = 455\text{ m}$), superconducting gravimeter CD034, with reductions and residual gravity, courtesy C. Kröner.

the observation site (Mathews et al., 1997). This delivers, among others, the Love numbers h and k , and the ocean loading effects (Schuh and Haas, 1998).

An example for long-term gravimetric recording and reductions for Earth tides, ocean tides, atmospheric mass redistributions, polar motion, local hydrological mass redistributions, large-scale variations in continental water storage, and non-tidal ocean loading is given in Fig. 8.36, where reductions are based on global or local modeling (Weise et al., 2009).

Tab. 8.1. Adjusted gravimetric Earth tide parameters (selection, rounded values), Earth tide station no.765, GFZ/Potsdam ($\varphi = 52.38^\circ \text{N}$, $\lambda = 13.07^\circ \text{E}$, $H = 81 \text{ m}$), superconducting gravimeter GWR TT70 No. 018, recording time June 1992 to October 1998 (2250 days). Standard deviation (short- and long-periodic tides adjusted): $\pm 9 \text{ nms}^{-2}$, only short-periodic tides: $\pm 0.8 \text{ nms}^{-2}$; air pressure regression coefficient $-2.776 \text{ nms}^{-2}/\text{hPa}$, pole-tide δ -factor 1.13. after Dittfeld (2000)

Tide Symbol	Period	Amplitude (nms^{-2})	Ampl. factor δ	Phase lead $\Delta\Phi(^{\circ})$
Long-periodic (d)				
Sa	365.26	18.4	4.4	-40
Ssa	182.62	29.7	1.13	-2
Mm	27.55	34.0	1.14	0.6
Mf	13.66	64.4	1.14	-3
Diurnal (h)				
Q1	26.87	66.0	1.146	-0.22
O1	25.82	345.6	1.150	-0.13
P1	24.07	160.9	1.150	0.12
S1	24.00	4.2	1.28	2.0
K1	23.93	480.6	1.137	0.2
ψ_1	23.87	4.2	1.26	0.6
φ_1	23.80	7.1	1.18	-0.1
Semi-diurnal (h)				
N2	12.66	63.2	1.179	1.99
M2	12.42	332.3	1.186	1.36
S2	12.00	154.6	1.186	0.21
K2	11.97	42.0	1.186	0.45
Ter-diurnal (h)				
M3	8.28	3.6	1.073	0.3

We summarize some results of the *gravimetric* Earth tide analysis (Wenzel, 1997b; Neumeyer, 2010):

- The high precision obtained at gravity recording allows the evaluation of *gravimetric amplitude factors* and *phase shifts* for a large range of periods. As an example, Tab. 8.1 contains the gravimetric tidal parameters for a selected number of partial tides (out of a total number of 57 analyzed wave groups) from long-term observations with a superconducting gravimeter (Dittfeld, 2000), cf. [3.5.2].
- The separation of the small S1 wave mirrors the *quality* of the analysis, as the diurnal tides are strongly contaminated by meteorological effects.
- The standard deviations of the adjusted *tidal parameters* are approximately inversely proportional to the amplitude of the waves. The amplitude factor of the principal waves (O1, P1, K1, M2, S2) can be obtained with a relative accuracy of about 0.01% and the phase shift with 0.01°, and better. The long-periodic tides (Mm, Mf) are accurate to a few % and a few degrees.
- *Loading effects* from mass redistributions in the atmosphere, the oceans and the continental water storage can be partly reduced by global or local modeling, but

local irregularities in hydrology may cause larger errors (Harnisch and Harnisch, 2006). This is also valid for the effect of *ocean tidal loading*, which is clearly visible in the semi-diurnal tides. After corresponding reduction, the observed tidal parameters are in close agreement (within 0.1%) with advanced elastic and inelastic body tide models. They may also provide useful constraints for oceanic tidal models (Jentzsch, 1997).

Calibration accuracy of gravity meters still is a major problem at validating Earth and ocean tide models using tidal gravity measurements (Baker and Bos, 2003). Tidal gravity observations at several western European sites, e.g., delivered mean gravimetric factors and phases of $\delta(O1) = 1.149$ (0.10°) and $\delta(M2) = 1.184$ (1.64°). After correction for ocean loading, these values reduced to 1.153 (0.00°) and 1.161 (0.02°), respectively, which does not allow to distinguish between different models.

- World-wide *synthetic gravity tide parameters* have been calculated for a $1^\circ \times 1^\circ$ grid, based on the Wahr (1981b)/Dehant (1987) body tide and the Schwiderski (1980) ocean tide models. The parameter values agree well with the gravimetric Earth tide observations, they provide the gravimetric *tidal reductions* with the desired accuracy with the exception of strongly disturbed coastal zones and polar regions, Timmen and Wenzel (1994b).
- A dependence on large-scale mantle lateral heterogeneities or heat flow has not yet been detected (Zürn, 1997).
- *Co-seismic* gravity changes of some 10 nms^{-2} have been recorded at several earthquakes, but tidal triggering of earthquakes and volcanic eruptions is still under controversial discussion (Emter, 1997).
- The *resonance effect* of the liquid outer core (free core nutation), cf. [2.3.4], has been clearly identified in the diurnal tides ($K1, \psi_1, \varphi_1$), Ducarme et al. (2009).
- *Free oscillations* (vertical component) of the Earth as excited by strong earthquakes, with periods between 10 s and 54 mins, have been analyzed from high resolution records and can be used for the support of global seismic networks (e.g., Rosat et al., 2005).

This list of the results of gravity recording is by far not complete, but leads to the following conclusions:

With presently available *models* of solid Earth, ocean and atmospheric tides, geodetic measurements in most cases can be reduced satisfactorily. Data series and tidal parameters obtained from continuous (or repeated) monitoring of geodetic sites (VLBI, SLR, LLR, GNSS, and gravity) are also useful for the validation of satellite-derived results. Verifying global Earth models, and validating and improving global and regional ocean tide and hydrological models plays an important role at the analysis of continuous gravity records, and is of high relevance. Among the challenges of data interpretation are the relations to seismicity and tectonic processes, volcanism, and recent hydrological variations (Neumeyer, 2010).

References

Abbreviations used:

- Adv. Space Res. = Advances in Space Research. Official Journal of COSPAR, Elsevier.
- Allg. Verm. Nachr. = Allgemeine Vermessungsnachrichten, Wichmann-Hüthig, Heidelberg.
- Ann. Geophys. = Annales Geophysicae, European Geosciences Union.
- Astron. Astrophys. = Astronomy & Astrophysics, EDP Sciences, Les Ulis, France (until 2000: Springer, Berlin-Heidelberg)
- Astron. J. = The Astronomical Journal, American Astronomical Society.
- Boll. Geof. Teor. Appl. = Bollettino di Geofisica Teorica ed Applicata. Osservatorio Geofisico Sperimentale, Trieste.
- Bull. Géod. = Bulletin Géodesique. Springer, Berlin-Heidelberg-New York.
- Bur. Gravim. Int. = Bulletin d'Information, Bureau Gravimétrique Internationale, Toulouse.
- DGK = Veröffentlichungen der Deutschen Geodätischen Kommission bei der Bayerischen Akademie der Wissenschaften, München und Frankfurt a.M.
- Earth Planet. Sci. Lett. = Earth and Planetary Science Letters, Elsevier.
- EOS = Transactions American Geophysical Union, Washington, D.C.
- Geophys. J. Int. = Geophysical Journal International, on behalf of the Royal Astronomical Society, publ. by Wiley-Blackwell.
- Geophys. J. R. Astr. Soc. = Geophysical Journal of the Royal Astronomical Society.
- Geophys. Res. Lett. = Geophysical Research Letters, American Geophysical Union.
- IAG Symp. Proc. = International Association of Geodesy, Symposia Proceedings, Springer, Berlin- Heidelberg-New York.
- J. Geod. = Journal of Geodesy, Springer, Berlin-Heidelberg-New York.
- J. Geodyn. = Journal of Geodynamics, Elsevier.
- J. Geophys. = Journal of Geophysics (Zeitschrift für Geophysik).
- JGR = Journal of Geophysical Research. American Geophysical Union, Washington, D.C.
- Man. Geod. = Manuscripta Geodaetica. Springer, Berlin-Heidelberg-New York.
- Mar. Geod. = Marine Geodesy. Taylor and Francis Group, London.
- Marées Terr. = Bulletin d'Information, Marées Terrestres, Observatoire Royal de Belgique, Bruxelles
- Mitt. BKG = Mitteilungen des Bundesamtes für Kartographie und Geodäsie, Frankfurt a.M.
- OSU Rep. = Reports of the Department of Civil and Environment Engineering and Geodetic Science, Geodetic Science and Surveying, The Ohio State University, Columbus, Ohio.
- Phys. Chem. Earth = Physics and Chemistry of the Earth, Elsevier.
- Phys. Earth Planet. Int. = Physics of the Earth and Planetary Interiors, Elsevier.
- Pure Appl. Geophys. (Pageoph) = Pure and Applied Geophysics, Birkhäuser, Basel.
- Rev. Geophys. = Review of Geophysics, American Geophysical Union.
- Rev. Geophys. Space Phys. = Review of Geophysics and Space Physics, American Geophysical Union.
- Studia geophys. geod. = Studia Geophysica et Geodaetica, Springer.
- Surv. Geophys. = Surveys in Geophysics, Springer.
- Surv. Rev. = Survey Review. Maney Publishing, Leeds-London-Boston.
- Unisurv G = Univ. of New South Wales, Geodesy Reports, Kensington, N.S.W.
- Wiss. Arb. Univ. Hannover = Wissenschaftliche Arbeiten der Fachrichtung Geodäsie und Geoinformatik der Leibniz Universität Hannover.
- ZfV (zfv) = Zeitschrift für Geodäsie, Geoinformation und Landmanagement (formerly Zeitschrift für Vermessungswesen). Wißner-Verlag, Augsburg (formerly K. Wittwer, Stuttgart).

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