

NENG 685, Fall 17
Boltzmann Transport Equation
October 23, 2017

For more information, reference Lewis and Miller Chp. 1 [3] and Duderstadt and Hamilton Chp. 4 [1]. Note: Duderstadt and Martin [2] is a very good general reference. It goes through all of this same stuff, but from a slightly more generic point of view (since this applies to any collection of neutral particles).

A primary goal of nuclear reactor analysis and design is the reliable prediction of neutron population production and loss rates. Similarly, for nuclear weapon design, we want to be able to predict neutron populations, minimize loss rates, and model the time-dependent change in those properties. Although these notes are often phrased in context of a nuclear reactor, they are applicable to nuclear weapons or any other neutral particle transport. A very gross simplification is to think of nuclear weapons as one-time use reactors that output a lifetime of energy almost instantaneously.

In order to fully describe neutron transport through media, we need to describe neutron motion and neutron interactions with matter. To begin determining probabilities of neutron-nuclear reactions, we will first review the aspects of nuclear physics that are relevant for fission chain reactions.

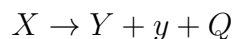
Nuclear Physics of Chain Reactions

Notation reminder: A_ZX indicates that chemical element X has Z protons (atomic number) and A total nucleons (protons + neutrons = mass number).

Excited states are written as ${}^A_ZX^*$, and metastable/isomeric as ${}^A_ZX^m$.

There are two types of **basic nuclear transformations**:

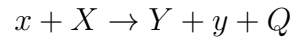
1. Spontaneous disintegration: The spontaneous decay of unstable nuclei, with emission of particles or radiation



These are probabilistic events that depend only on the type of nucleus.

2. Induced by collision: An event in which, because of interaction with a particle or radiation (a projectile), a nucleus (target) is changed in mass, charge or energy state, and particles or

radiation is emitted.



here y is typically n , p , α , β , or γ and Q is energy. x can be any of the same particles as y , but it can also be other nuclei. At higher energies of collision induced reactions, the available decay options for y greatly expand beyond the indicated list.

Examples of common reactions:

- Potential elastic scattering (n, n) : ${}_0^1\text{n} + {}_Z^AX \rightarrow {}_0^1\text{n} + {}_Z^AX$
- Resonance elastic scattering (n, n) : ${}_0^1\text{n} + {}_Z^AX \rightarrow ({}_Z^AX^*) \rightarrow {}_0^1\text{n} + {}_Z^AX$
- Inelastic scattering (n, n') : ${}_0^1\text{n} + {}_Z^AX \rightarrow ({}_Z^AX^*) \rightarrow {}_0^1\text{n} + {}_Z^AX + \gamma$
- Radiative capture (absorption) (n, γ) : ${}_0^1\text{n} + {}_Z^AX \rightarrow ({}_Z^AX^*) \rightarrow {}_Z^{A+1}X + \gamma$
- Fission (absorption) (n, f) : ${}_0^1\text{n} + {}_Z^AX \rightarrow {}_{Z_1}^{A_1}X + {}_{Z_2}^{A_2}X + (\text{a few}){}_0^1\text{n}$
- Charged-Particle Reactions (absorption): (n, α) ${}_0^1\text{n} + {}_Z^AX \rightarrow {}_{Z-2}^{A-3}Y + {}_2^4\text{He}$;
 (n, p) ${}_0^1\text{n} + {}_Z^AX \rightarrow {}_{Z-1}^AY + {}_1^1\text{p}$
- Neutron-Producing Reactions (absorption): $(n, 2n)$ ${}_0^1\text{n} + {}_Z^AX \rightarrow {}_Z^{A-1}X + 2{}_0^1\text{n}$

Which reaction happens depends on the type of nucleus, the energy of the incoming neutron, and statistics. We can, fortunately, draw general categories for many types of reactions:

Nuclear Reactions have to obey a set of **Conservation Laws**, which govern what actually happens in the transformations.

- Conservation of Mass/Energy: The total energy of the system before nuclear transformation must be equal to the total energy of the system after the transformation.
- Conservation of Linear Momentum: Total linear momentum of the system (a vector) before nuclear transformation must be equal to the total linear momentum of the system (a vector) after the transformation.
- Conservation of Charge: Total charge of the system before nuclear transformation must be equal to the total charge of the system after the transformation.
- Conservation of Nucleons: Total number of nucleons (protons and neutrons) of the system before nuclear transformation must be equal to the total number of nucleons (protons and neutrons) of the system after the transformation.

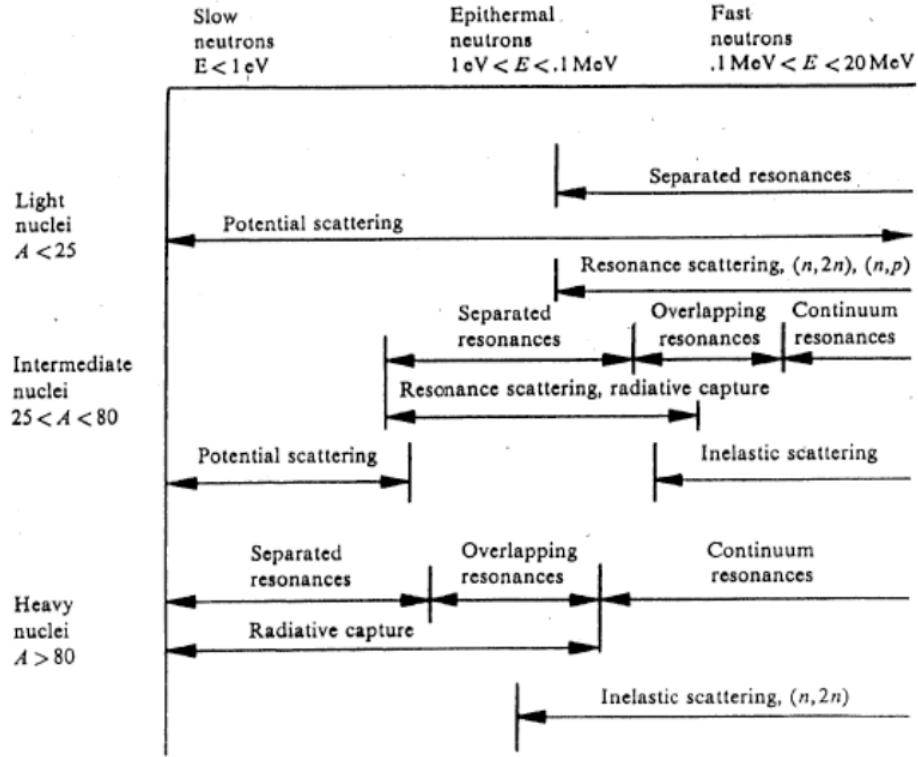


Figure 1: Neutron Interactions by Energy and Atomic Number

The conservation laws govern what reactions can happen. What reactions actually happen govern the neutron population in a reactor.

What we'll cover next are the definitions and terms we will use to describe neutrons in six-dimensional phase space: $(x, y, z, \hat{\Omega}, E)$.

Definitions

Spatial logistics

- $d\vec{r} = d^3r$ = ordinary volume = $r^2 \sin(\theta) d\theta d\phi dr$
- v = speed (scaler)
- $\vec{v} = v\hat{\Omega}$ = velocity (vector)
- $d\vec{v} = d^3v$ = velocity volume = $v^2 \sin(\theta) d\theta d\phi dv$
- $v = \sqrt{(2E)/m}$ where m is the rest mass of the particle. Thus, we can relate energy and speed.

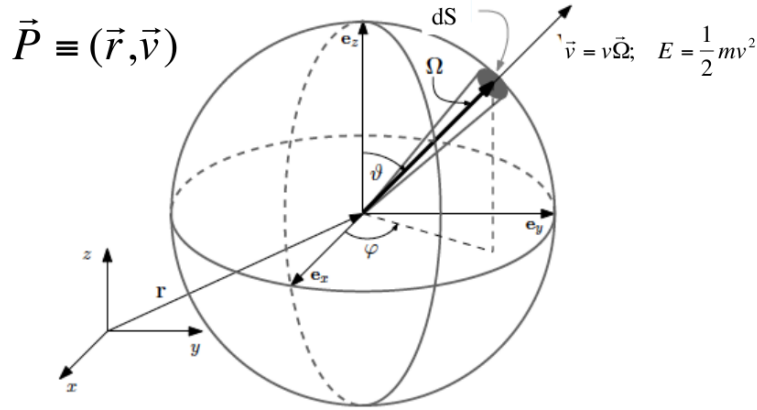


Figure 2: Schematic of Phase Space

- $\hat{\Omega}$: unit directional vector in velocity space, $\vec{v} = v\hat{\Omega}$
- $d\hat{\Omega} = \sin(\theta)d\theta d\varphi = d^2\Omega$

These are the possible reactions we're generally going to worry about in this course for solving the BTE:

total (t): all interactions. We can break total into:

- scattering (s): a neutron interacts with an atom and bounces off either elastically or inelastically.
- absorption (a): a neutron is absorbed by a nucleus. If this happens it might
- fission (f): cause the nucleus to split into two pieces, releasing more neutrons.

Physics terms we will use:

1. **microscopic x-sec** ($\sigma, [cm^2]$): measure of the probability that an incident neutron will collide with a specific nucleus; σ_j indicates a specific reaction, e.g. $j = f$ is fission.
2. **macroscopic x-sec** ($\Sigma [cm^{-1}]$): measure of the probability per unit path length that an incident neutron will collide with a target

$$\Sigma_j = \sigma_j N ,$$

where N is the atomic density of the target. The total cross section is simply the sum of all possible reaction types, j .

If a material is made of multiple isotopes, the material macroscopic cross section is also the sum over all materials, i :

$$\Sigma_i(\vec{r}, E, t) = \sum_{j=1}^J N_j(\vec{r}, t) \sigma_{i,j}(E) \quad \Sigma_t(\vec{r}, E, t) = \sum_{j=1}^J \sum_{i=1}^I N_j(\vec{r}, t) \sigma_{i,j}(E)$$

3. **double-differential scattering x-sec** ($\sigma_s(E, \hat{\Omega} \rightarrow E', \hat{\Omega}') dE' d\hat{\Omega}'$): measure of the probability that a neutron of energy E and moving in direction $\hat{\Omega}$ scatters off of a specific nucleus into energy range $[E', E' + dE']$ and direction range $[\hat{\Omega}', \hat{\Omega}' + d\hat{\Omega}']$.

We can think of this as the fractional probability multiplied by the total scattering cross section

$$\begin{aligned} \sigma_s(E, \hat{\Omega} \rightarrow E', \hat{\Omega}') &= \sigma_s(E) f_s(E, \hat{\Omega} \rightarrow E', \hat{\Omega}') \\ \text{where } \int_0^{E_0} dE' \int_{4\pi} d\hat{\Omega}' f_s(E, \hat{\Omega} \rightarrow E', \hat{\Omega}') &= 1 \\ \sigma_s(E) &= \int_0^{E_0} dE' \int_{4\pi} d\hat{\Omega}' \sigma_s(E, \hat{\Omega} \rightarrow E', \hat{\Omega}') \end{aligned}$$

4. **fission yield** ($\nu(E)$): average # of neutrons released by a fission induced by a neutron of energy E .
5. **fission spectrum** ($\chi(E) dE$): average # of neutrons produced from fission that are born with energy in $[E, E + dE]$. This is normalized such that

$$\int_0^\infty \chi(E) dE = 1 .$$

- U-235: $\chi(E) = 0.453e^{-1.036E} \sinh(\sqrt{2.29E})$
- Pu-239: $\chi(E) = 0.6739\sqrt{E}e^{-E/1.41}$

6. **particle angular density** ($n(\vec{r}, E, \hat{\Omega}, t) d\vec{r} d\hat{\Omega} dE$): expected number of particles in volume element d^3r at \vec{r} whose energies are in $[E, E + dE]$ and direction of motion is in $[\hat{\Omega}, \hat{\Omega} + d\hat{\Omega}]$ at time t .

Note:

$$n(\vec{r}, E, \hat{\Omega}, t) = \frac{1}{mv} n(\vec{r}, v, \hat{\Omega}, t)$$

$$n(\vec{r}, v, \hat{\Omega}, t) = v^2 n(\vec{r}, \vec{v}, t)$$

$$n(\vec{r}, \vec{v}, t) = \frac{m}{v} n(\vec{r}, E, \hat{\Omega}, t)$$

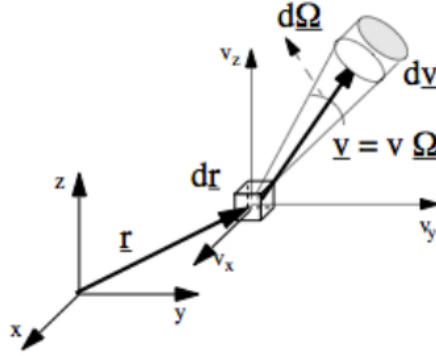


Figure 3: Differential volume, velocity (energy), and angle

7. **particle density:** $(N(\vec{r}, E, t)d^3r dE)$: expected number of particles in d^3r at \vec{r} whose energies are in $[E, E + dE]$ at time t .

$$N(\vec{r}, E, t)d^3r dE = \int_{4\pi} d\hat{\Omega} n(\vec{r}, E, \hat{\Omega}, t)d^3r dE$$

8. **angular flux:** $\psi(\vec{r}, E, \hat{\Omega}, t) \equiv vn(\vec{r}, E, \hat{\Omega}, t)$ [neutrons / (cm² s MeV steradian)] can be thought of as path length per unit volume about \vec{r} passed by neutrons with energies...

9. **scalar flux:** $\phi(\vec{r}, E, t) \equiv vN(\vec{r}, E, t)$ [neutrons / (cm² s MeV)] can be thought of as the number of neutrons that penetrate a sphere of 1 cm² cross sectional area at \vec{r} with energies in dE about E at time t .

$$= \int_{4\pi} d\hat{\Omega} \psi(\vec{r}, E, \hat{\Omega}, t)$$

10. **interaction rate density:** expected number of j reactions per volume per energy at time t .

$$\int_{4\pi} d\hat{\Omega} \Sigma_j vn(\vec{r}, E, \hat{\Omega}, t) = \Sigma_j \phi(\vec{r}, E, t)$$

11. **angular current density** or partial current: $\vec{j}(\vec{r}, E, \hat{\Omega}, t) = \vec{v}n(\vec{r}, E, \hat{\Omega}, t)$;

$\vec{j}(\vec{r}, E, \hat{\Omega}, t) \cdot \hat{e} dA dE d\hat{\Omega}$ is the expected number of particles crossing dA per second along unit direction \hat{e} with energy in $[E, E + dE]$ and direction in $[\hat{\Omega}, \hat{\Omega} + d\hat{\Omega}]$ at time t .

12. **net current**: $\vec{J}(\vec{r}, E, t)$ is the net # of particles crossing a unit area per second along a direction normal to that area with energies in $[E, E + dE]$ at time t .

$$\vec{J}(\vec{r}, E, t) = \int_{4\pi} d\hat{\Omega} \hat{\Omega} \psi(\vec{r}, E, \hat{\Omega}, t)$$

Assumptions

1. Particles are point objects ($\lambda = h/(mv)$) is small compared to the atomic diameter): its state is fully described by its location, velocity vector, and a given time. This ignores rotation and quantum effects.
2. Neutral particles travel in straight lines between collisions.
3. Particle-particle collisions are negligible (makes TE linear).
4. Material properties are isotropic (generally valid unless velocities are very low).
5. Material composition is time-independent (generally valid over short time scales).
6. Quantities are expected values: fluctuations about the mean for very low densities are not accounted for.
7. Neglect potential energy (i.e. neglect gravity).
8. Ignore neutron decay.

The Boltzmann Transport Equation (BTE)

We consider a six-dimensional volume (as a six-dimensional cube) fixed in space, of dimensions $\Delta x, \Delta y, \Delta z, \Delta E, \Delta \theta, \Delta \varphi$. Then, the number of particles within this volume at time t is

$$n(\vec{r}, E, \hat{\Omega}, t) \Delta x \Delta y \Delta z \Delta E \Delta \theta \Delta \varphi = n(\vec{r}, E, \hat{\Omega}, t) \Delta \beta,$$

where all arguments of N are “average” arguments in the increment of six-dimensional phase space $\Delta\beta$. The number of particles in this cube changes with time:

$$\Delta\beta \frac{\partial}{\partial t} n(\vec{r}, E, \hat{\Omega}, t) = \text{time rate of change of the number of particles in the six-dimensional cube } \Delta\beta.$$

This time rate of change is due to five separate processes:

1. The rate of streaming of particles out of the volume through the boundaries
2. The rate of absorption in the “cube”
3. The rate of scattering from $E, \hat{\Omega}$ to all other energies and directions, known as outscattering
4. The rate of scattering into $E, \hat{\Omega}$ from all other energies and directions, known as inscattering
5. The rate of production of particles due to an internal source

Now, let us consider each of these in detail.

#1) Let us first consider the surfaces of the cube perpendicular to the x -axis. For the net rate of particles leaving the cube through these two surfaces, we have

$$(\text{Streaming})_x = \dot{x} n(\vec{r}, E, \hat{\Omega}, t) \Big|_x^{x+\Delta x} \Delta y \Delta z \Delta E \Delta \theta \Delta \varphi,$$

where \dot{x} is the x component of the particle velocity, and $\Delta y \Delta z \Delta E \Delta \theta \Delta \varphi$ is the surface area. Letting Δx go to the differential dx , we rewrite

$$(\text{Streaming})_x = \Delta\beta \frac{\partial}{\partial x} [\dot{x} n(\vec{r}, E, \hat{\Omega}, t)].$$

Using the same procedure for the flow from the cube in the other five “directions”, we obtain

$$\begin{aligned} \text{Streaming} = & \left[\frac{\partial}{\partial x} (\dot{x} n) + \frac{\partial}{\partial y} (\dot{y} n) + \frac{\partial}{\partial z} (\dot{z} n) \right. \\ & \left. + \frac{\partial}{\partial E} (\dot{E} n) + \frac{\partial}{\partial \theta} (\dot{\theta} n) + \frac{\partial}{\partial \varphi} (\dot{\varphi} n) \right] \Delta\beta, \end{aligned}$$

where $n = n(\vec{r}, E, \hat{\Omega}, t)$.

#2) The rate of absorption within the cube is the product of the number of particles in the cube and the probability of absorption per particle per unit of time. This probability is given by the product

of the absorption cross section and the particle speed v . That is,

$$\text{Absorption} = v \Sigma_a(\vec{r}, E) n(\vec{r}, E, \hat{\Omega}, t) \Delta\beta.$$

#3-4) Using similar arguments and the fact that we need to sum the scattering from (to) $E, \hat{\Omega}$ to (from) all other energies and directions $E', \hat{\Omega}'$, we find

$$\begin{aligned} \text{Outscattering} &= \Delta\beta \int_0^\infty \int_{4\pi} v \Sigma_s(\vec{r}, E \rightarrow E', \hat{\Omega} \rightarrow \hat{\Omega}') n(\vec{r}, E, \hat{\Omega}, t) d\hat{\Omega}' dE', \\ \text{Inscattering} &= \Delta\beta \int_0^\infty \int_{4\pi} v' \Sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \rightarrow \hat{\Omega}) n(\vec{r}, E', \hat{\Omega}', t) d\hat{\Omega}' dE', \end{aligned}$$

where $\Sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \rightarrow \hat{\Omega})$ is the macroscopic differential scattering cross section. Since the distribution function in the integrand of the outscattering term is independent of the integration variables, we can rewrite Outscattering as $\Delta\beta v \Sigma_s(\vec{r}, E) n(\vec{r}, E, \hat{\Omega}, t)$.

#5) Finally, we need to consider the internal source of particles. We quantify this source by introducing the function $S(\vec{r}, E, \hat{\Omega}, t)$ such that the rate of introduction of particles into the cube is given by

$$\text{Source} = S(\vec{r}, E, \hat{\Omega}, t) \Delta\beta.$$

In order to build the transport equation, we sum these equations with appropriate signs for loss and gain, to the overall rate of change. Letting $\Delta\beta$ approach a differential element and canceling it, we obtain

$$\begin{aligned} \frac{\partial n}{\partial t} = & - \left[\frac{\partial(\dot{x}n)}{\partial x} + \frac{\partial(\dot{y}n)}{\partial y} + \frac{\partial(\dot{z}n)}{\partial z} + \frac{\partial(\dot{E}n)}{\partial E} + \frac{\partial(\dot{\theta}n)}{\partial \theta} + \frac{\partial(\dot{\varphi}n)}{\partial \varphi} \right] \\ & - v \Sigma_a(\vec{r}, E) n \\ & + \int_0^\infty \int_{4\pi} v' \Sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \rightarrow \hat{\Omega}) n(\vec{r}, E', \hat{\Omega}', t) d\hat{\Omega}' dE' \\ & - \int_0^\infty \int_{4\pi} v \Sigma_s(\vec{r}, E \rightarrow E', \hat{\Omega} \rightarrow \hat{\Omega}') n(\vec{r}, E, \hat{\Omega}, t) d\hat{\Omega}' dE' \\ & + S(\vec{r}, E, \hat{\Omega}, t), \end{aligned} \tag{1}$$

where $n = n(\vec{r}, E, \hat{\Omega}, t)$. Since particles travel in a straight line between collisions, $\dot{\theta} = \dot{\varphi} = 0$. Furthermore, $\dot{E} = 0$ because particles stream with no change in energy. Finally,

performing the outscattering integral:

$$\begin{aligned} & \frac{1}{v} \frac{\partial \psi}{\partial t}(\vec{r}, E, \hat{\Omega}, t) + \hat{\Omega} \cdot \nabla \psi(\vec{r}, E, \hat{\Omega}, t) + \Sigma_t(\vec{r}, E) \psi(\vec{r}, E, \hat{\Omega}, t) \\ &= \int_0^\infty \int_{4\pi} \Sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, E', \hat{\Omega}', t) d\hat{\Omega}' dE' + S(\vec{r}, E, \hat{\Omega}, t). \end{aligned} \quad (2)$$

We can easily generalize this equation to include nuclear fission. To do that, we must revisit our treatment of Σ_a ; there are two main processes responsible for the absorption of particles in the system: *radiative capture* and *nuclear fission* (note that we're ignoring (n,xn) reactions for the time being). Now, we define

$$\Sigma_\gamma(\vec{r}, E) ds = \text{probability of capture}$$

and

$$\Sigma_f(\vec{r}, E) ds = \text{probability of a fission event},$$

such that

$$\Sigma_a(\vec{r}, E) = \Sigma_\gamma(\vec{r}, E) + \Sigma_f(\vec{r}, E).$$

While a captured neutron is simply removed from the system, a neutron with energy E that induces a fission event causes the target nucleus to split into two smaller daughter nuclei, and

$$\nu(E) = \text{the mean number of fission neutrons that are released}.$$

Of this number, $\nu(E)[1 - M(E)]$ are *prompt* fission neutrons (being emitted within 10^{-15} seconds of the fission event). These fission neutrons are emitted isotropically, with an energy distribution given by the fission spectrum $\chi_p(E)$. Also, $\nu(E)M(E)$ *delayed* fission neutrons (being released roughly 0.1 to 60 seconds after the fission event) are created; a delayed neutron is produced when a radioactive daughter nucleus undergoes a radioactive decay process in which a neutron is emitted.

Assuming (for simplicity) that the number of delayed neutrons emitted by fission is very small [$M(E) \ll 1$], we can neglect the delayed neutron terms and rewrite the transport equation

as

$$\begin{aligned}
& \underbrace{\frac{1}{v} \frac{\partial \psi}{\partial t}(\vec{r}, E, \hat{\Omega}, t)}_{\text{time rate of change}} + \underbrace{\hat{\Omega} \cdot \nabla \psi(\vec{r}, E, \hat{\Omega}, t)}_{\text{streaming loss rate}} + \underbrace{\Sigma_t(\vec{r}, E) \psi(\vec{r}, E, \hat{\Omega}, t)}_{\text{total interaction loss rate}} \\
&= \underbrace{\int_0^\infty \int_{4\pi} \Sigma_s(\vec{r}, E' \rightarrow E, \hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, E', \hat{\Omega}', t) d\hat{\Omega}' dE'}_{\text{in scattering source rate}} \\
&\quad + \underbrace{\frac{\chi_p(E)}{4\pi} \int_0^\infty \int_{4\pi} \nu(E') \Sigma_f(\vec{r}, E') \psi(\vec{r}, E', \hat{\Omega}', t) d\hat{\Omega}' dE'}_{\text{fission source rate}} \\
&\quad + \underbrace{S(\vec{r}, E, \hat{\Omega}, t)}_{\text{external source rate}}.
\end{aligned} \tag{3}$$

Boundary and Initial Conditions

These equations require both spatial and temporal boundary conditions. *Assuming that the physical system of interest is nonreentrant* (convex) and characterized by a volume V , it is sufficient to specify the flux of particles at all points of the bounding surface of the system in the incoming directions. This implies

$$\psi(\vec{r}_s, E, \hat{\Omega}, t) = \psi_b(\vec{r}_s, E, \hat{\Omega}, t), \quad \mathbf{n} \cdot \hat{\Omega} < 0,$$

where ψ_b is a specified function at the boundary, \vec{r}_s is a point on the surface, and \mathbf{n} is the unit outward normal vector at this point. In the time variable, we assume the range of interest $0 \leq t < \infty$ and specify the initial condition at $t = 0$, such that

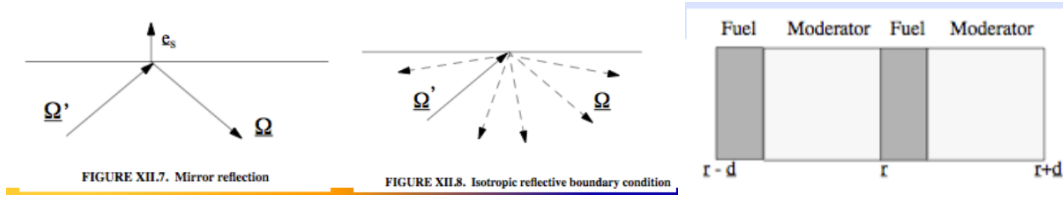
$$\psi(\vec{r}, E, \hat{\Omega}, 0) = \psi_0(\vec{r}, E, \hat{\Omega}),$$

where ψ_0 is a specified function.

A few other boundary conditions that we frequently use in nuclear engineering

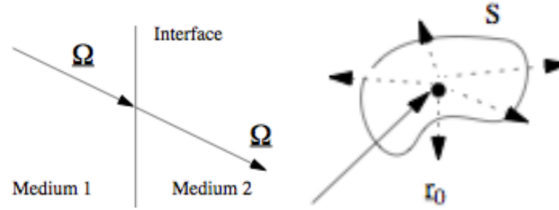
- mirror reflecting: $\psi(\vec{r}, E, \hat{\Omega}, t) = \psi(\vec{r}, E, \hat{\Omega}', t) \quad \forall \vec{r} \in S$, where S is a surface, and $(\hat{e}) \cdot \hat{\Omega} < 0$
- isotropic reflecting: $\psi(\vec{r}, E, \hat{\Omega}, t) = \frac{\phi(\vec{r}, E, t)}{4\pi}$
- vacuum: $\psi(\vec{r}, E, \hat{\Omega}, t) = 0 \quad \forall \vec{r} \in S$, where S is a surface, and $(\hat{e}) \cdot \hat{\Omega} < 0$
 $J^-(\vec{r}, E, t) = \int_{(\hat{e}) \cdot \hat{\Omega} < 0} d\hat{\Omega} |(\hat{e}) \cdot \hat{\Omega}| \psi(\vec{r}, E, \hat{\Omega}, t) = 0$

- periodic: $\psi(\vec{r}, E, \hat{\Omega}, t) = \psi(\vec{r} + d, E, \hat{\Omega}, t)$



Additional Conditions

- Finiteness condition: $0 \leq \psi(\vec{r}, E, \hat{\Omega}, t) \leq \infty$
- Interface condition: $\psi_1(\vec{r}, E, \hat{\Omega}, t) = \psi_2(\vec{r}, E, \hat{\Omega}, t) \quad \forall \vec{r} \in S_i, \text{ all energies, and all } \hat{\Omega}$
- Source condition: $Q(\vec{r}_0, E, \hat{\Omega}, t) = Q_0(E, \hat{\Omega}, t)\delta(\vec{r} - \vec{r}_0)$



Simplifications

One Speed

It is common to make extra assumptions in order to obtain a simpler version of these equations. For instance, assume all particles are at the same speed, so we no longer need energy dependence.

$$\frac{1}{v} \frac{\partial \psi(\vec{r}, \hat{\Omega}, t)}{\partial t} + \hat{\Omega} \cdot \nabla \psi(\vec{r}, \hat{\Omega}, t) + \Sigma_t \psi(\vec{r}, \hat{\Omega}, t) = \int_{4\pi} d\hat{\Omega}' \Sigma_s(\hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, \hat{\Omega}', t) + \frac{\nu \Sigma_f}{4\pi} \int_{4\pi} d\hat{\Omega}' \psi(\vec{r}, \hat{\Omega}', t) + s(\vec{r}, \hat{\Omega}, t)$$

One Speed, Time-independent

In the case of time-independent, monoenergetic particle transport in a homogeneous medium with a known interior isotropic source:

$$\hat{\Omega} \cdot \nabla \psi(\vec{r}, \hat{\Omega}) + \Sigma_t \psi(\vec{r}, \hat{\Omega}) = \int_{4\pi} \Sigma_s(\hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, \hat{\Omega}') d\hat{\Omega}' + \frac{S(\vec{r})}{4\pi},$$

and

$$\begin{aligned} \hat{\Omega} \cdot \nabla \psi(\vec{r}, \hat{\Omega}) + \Sigma_t \psi(\vec{r}, \hat{\Omega}) &= \int_{4\pi} \Sigma_s(\hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, \hat{\Omega}') d\hat{\Omega}' \\ &+ \frac{\nu \Sigma_f}{4\pi} \int_{4\pi} \psi(\vec{r}, \hat{\Omega}') d\hat{\Omega}' + \frac{S(\vec{r})}{4\pi}. \end{aligned}$$

Both the equations above need a spatial boundary condition, which is given by

$$\psi(\vec{r}_s, \hat{\Omega}) = \psi_b(\vec{r}_s, \hat{\Omega}), \quad \mathbf{n} \cdot \hat{\Omega} < 0.$$

In steady-state reactor calculations, one often sees a version of these equations in which the inhomogeneous source $S(\vec{r})$ and the boundary source $\psi_b(\vec{r}_s, \hat{\Omega})$ are set to zero, and the fission source is modified by a constant factor $1/k$:

$$\begin{aligned} \hat{\Omega} \cdot \nabla \psi(\vec{r}, \hat{\Omega}) + \Sigma_t \psi(\vec{r}, \hat{\Omega}) &= \int_{4\pi} \Sigma_s(\hat{\Omega}' \rightarrow \hat{\Omega}) \psi(\vec{r}, \hat{\Omega}') d\hat{\Omega}' \\ &+ \frac{\nu \Sigma_f}{4\pi k} \int_{4\pi} \psi(\vec{r}, \hat{\Omega}') d\hat{\Omega}', \\ \psi(\vec{r}_s, \hat{\Omega}) &= 0, \quad \mathbf{n} \cdot \hat{\Omega} < 0. \end{aligned}$$

These equations always have the zero solution $\psi = 0$; the goal is to find the largest value of k such that a nonzero solution ψ exists. The resulting k is called the *criticality* (or *criticality eigenvalue*) of the system. If a system has a fissionable region, it can be shown that k always exists, and the corresponding (eigenfunction) ψ is unique and positive.

One Speed, One Dimensional

We'd like to simplify even farther by only worrying about one dimension, so we'll get rid of y and z .

$$\vec{r} = (x, y, z)$$

$$d\hat{\Omega} = \sin(\theta)d\theta d\varphi = d\mu d\varphi$$

$$\text{Note } \mu = \cos(\theta) \text{ so } d\mu = \sin(\theta)$$

$$\Omega_x = \cos(\theta) = \mu$$

$$\begin{aligned} \frac{1}{v} \frac{\partial \psi(x, \hat{\Omega}, t)}{\partial t} + \left(\Omega_x \frac{\partial}{\partial x} + \cancel{\Omega_y \frac{\partial}{\partial y}} + \cancel{\Omega_z \frac{\partial}{\partial z}} \right) \psi(x, \hat{\Omega}, t) + \Sigma_t \psi(x, \hat{\Omega}, t) = \\ \int_{4\pi} d\hat{\Omega}' \Sigma_s(\hat{\Omega}' \rightarrow \hat{\Omega}) \psi(x, \hat{\Omega}', t) + \frac{\nu \Sigma_f}{4\pi} \int_{4\pi} d\hat{\Omega}' \psi(x, \hat{\Omega}', t) + s(x, \hat{\Omega}, t) \end{aligned}$$