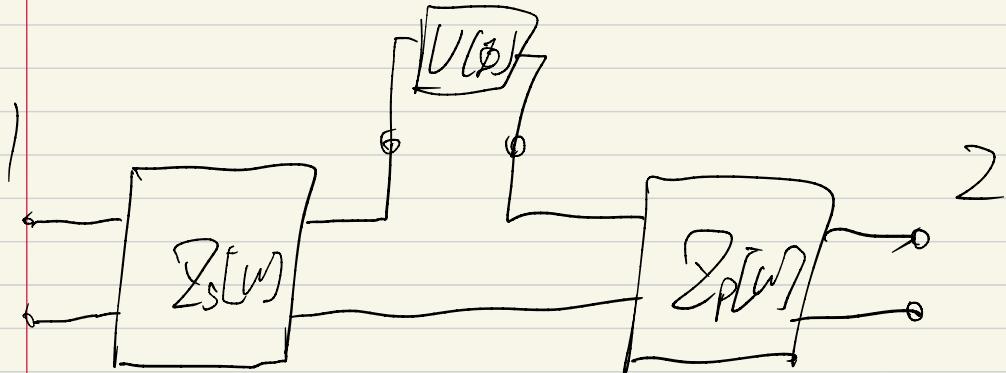
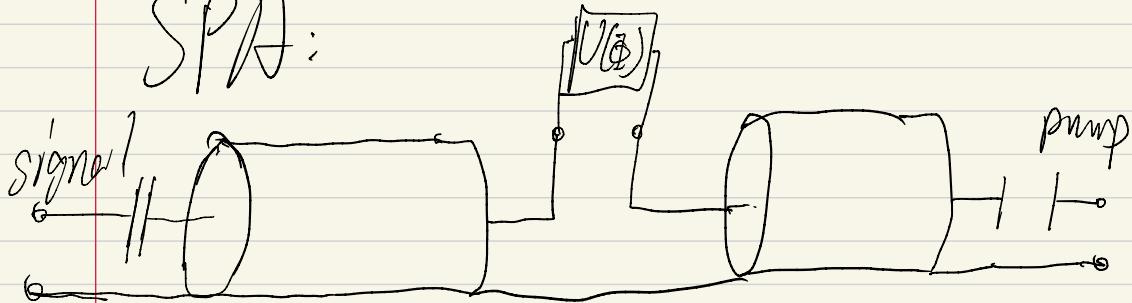


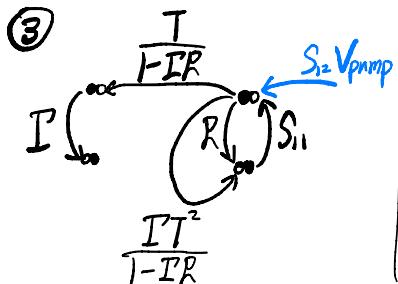
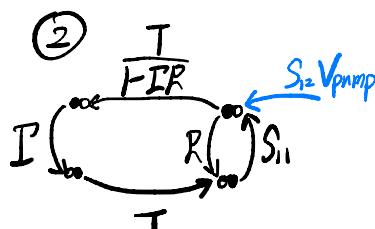
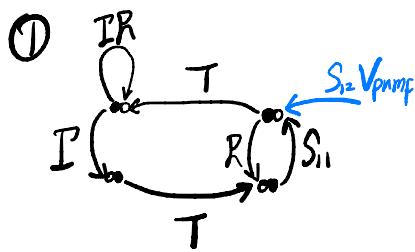
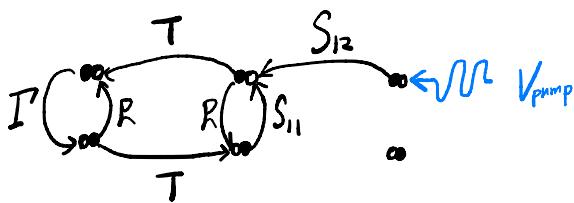
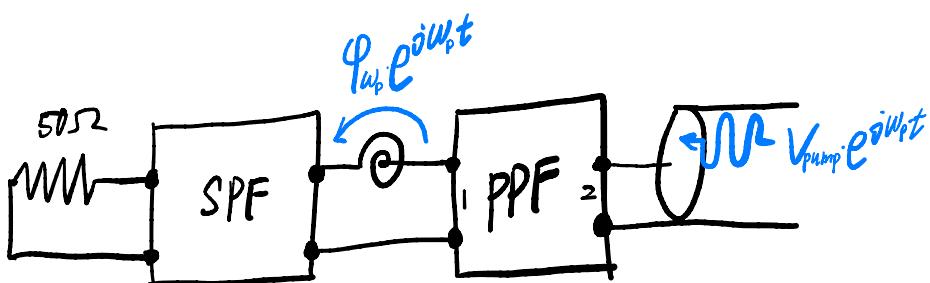
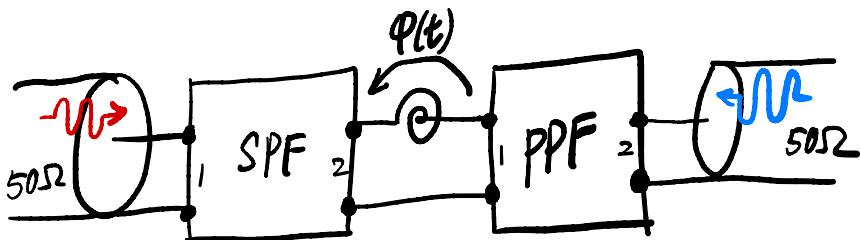

SPA:



1. $S11[W_s]$ gain

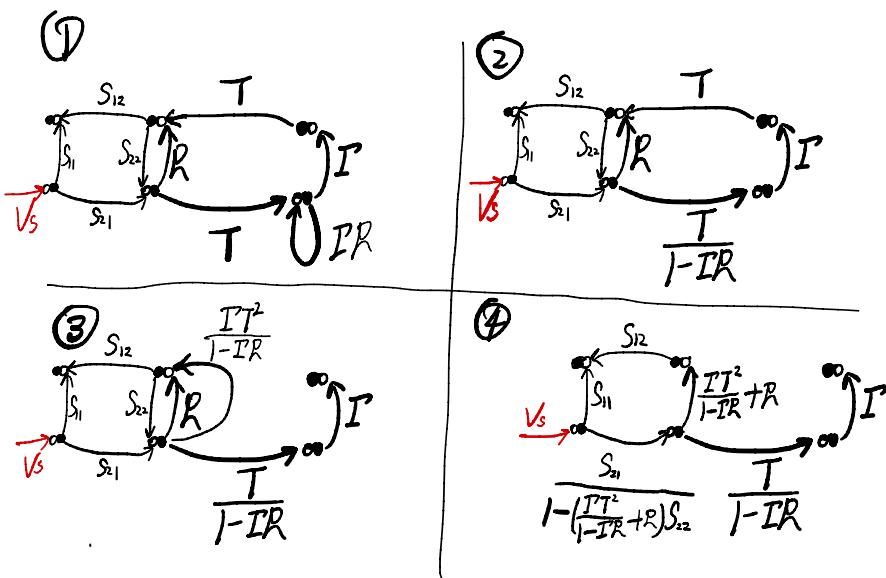
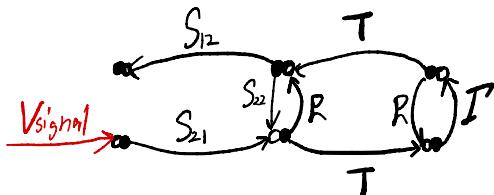
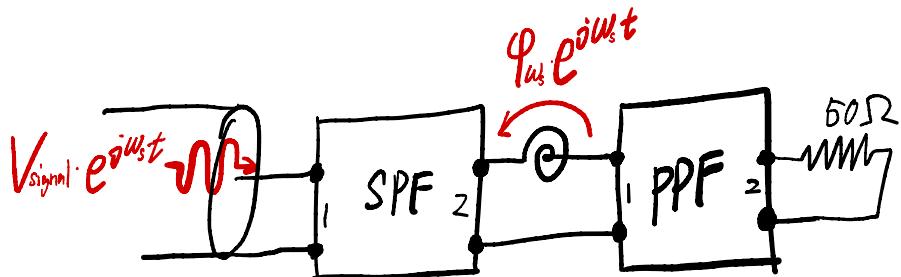
2. $S21[W_s]$ small (SNR , signal leakout)

3. $S12[W_p]$ small (protection)

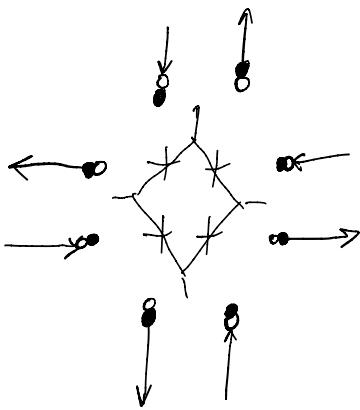


$$\frac{IT^2}{I-IR} \quad I - \frac{(IT^2)}{(I-IR)+R} S_{11}$$

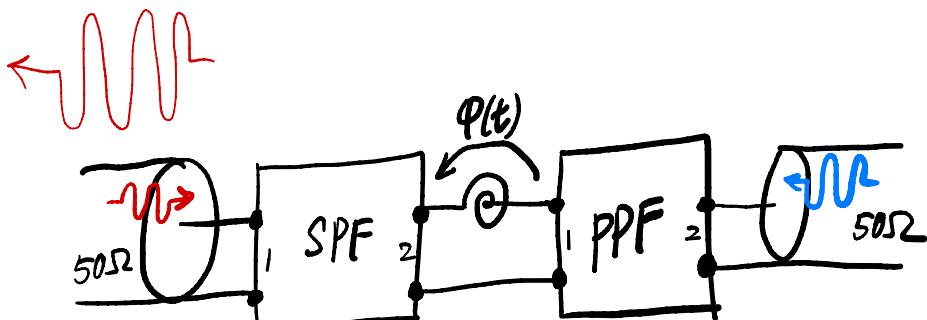
④ **T** network with two resistors R and two switches S_{11} and S_{12} . The output voltage is labeled $S_{12} V_{\text{pump}}$.

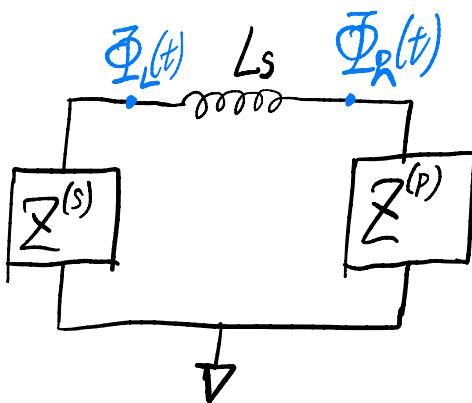
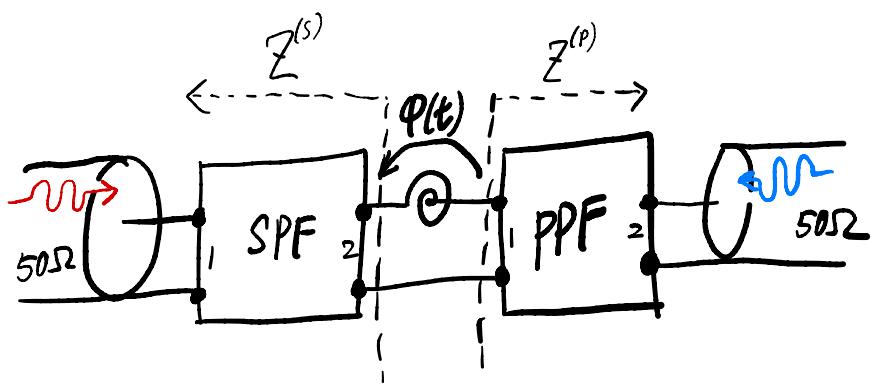


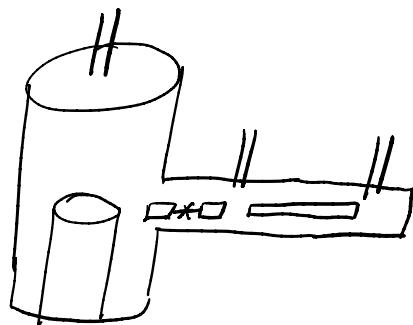
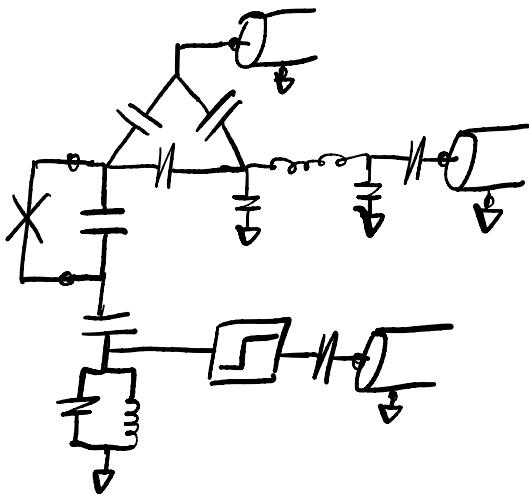
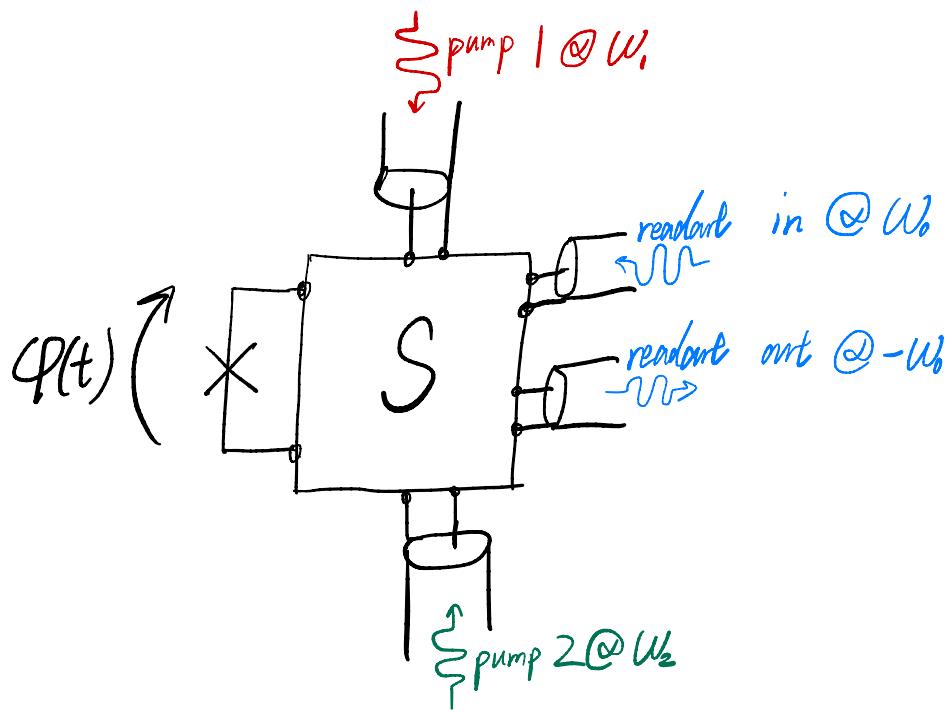
$$\frac{IT^2}{I - IR} + R = I \left(\frac{2Z_c}{Z + 2Z_c} \right)^2 + \frac{Z}{Z + 2Z_c}$$

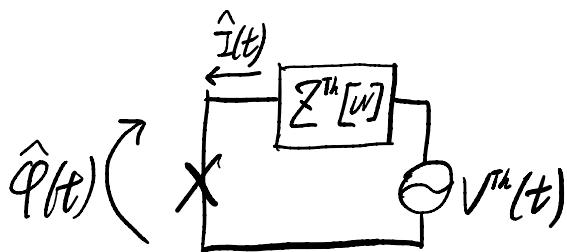


$$\begin{pmatrix} I_{W_s} \\ I_{W_i}^* \end{pmatrix} = \frac{1}{jL_s} \begin{pmatrix} 1 + \delta_s & -\varepsilon \\ -\varepsilon^* & 1 + \delta_i \end{pmatrix} \begin{pmatrix} V_{W_s} \\ V_{W_i}^* \end{pmatrix}$$









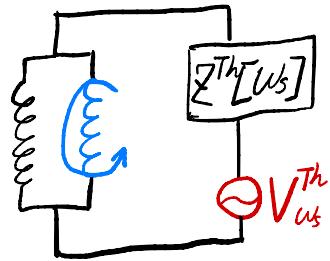
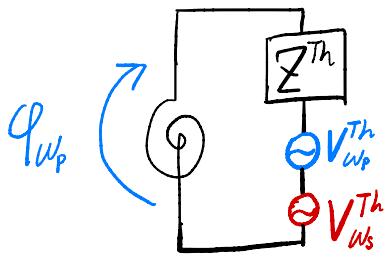
$$\operatorname{Re} (V_{w_1} e^{j\omega t} + V_{w_2} e^{j\omega t} + V_{w_3} e^{j\omega t})$$

$$\Sigma^{\text{Th}} \quad V^{\text{th}} \quad V^{\text{th}}$$

$$\hat{I} = \frac{E_J}{\phi_0} \left(C_2 \hat{\phi} + \frac{C_3}{2} \hat{\phi}^2 + \frac{C_4}{6} \hat{\phi}^3 + \dots \right)$$

$$I_{ws} = \frac{E_J}{\phi_0} \left[C_2 \varphi_{ws} + \frac{C_3}{2} \varphi_{ws} \varphi_{ws}^* + \frac{C_4}{8} \left(|\varphi_{ws}|^2 + 2|\varphi_{ws}|^2 + 2|\varphi_{ws}|^2 \right) \varphi_{ws} \right]$$

$$Y_J[w_s] = \frac{I_{ws}}{j w_s \phi_0 \varphi_{ws}} = \frac{1}{j w_s L_J} + \frac{1}{j w_s L_J} \cdot \frac{C_3 \varphi_{ws}}{2 C_2} \cdot \frac{\varphi_{ws}^*}{\varphi_{ws}}$$



$$\text{with } \begin{pmatrix} b_1 \\ b_2 \end{pmatrix} = S \begin{pmatrix} \alpha_1 \\ \alpha_2 \end{pmatrix}$$

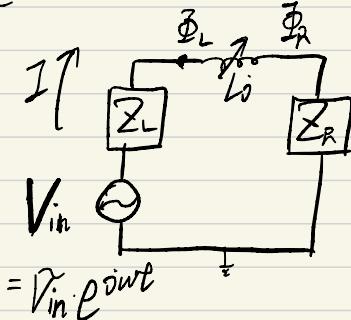
We can redefine "Transmission matrix" T_S :

$$\begin{pmatrix} b_1 \\ a_1 \end{pmatrix} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} \alpha_2 \\ b_2 \end{pmatrix}$$

$$T_S \left\{ \begin{array}{l} T_{11} = \frac{-\det(S)}{S_{21}} \\ T_{12} = \frac{S_{11}}{S_{21}} \\ T_{21} = \frac{-S_{22}}{S_{21}} \\ T_{22} = \frac{1}{S_{21}} \end{array} \right.$$



$$\textcircled{a} \quad W \approx W_S$$



$$\left. \begin{array}{l} j\omega \Phi_L = V_{in} - Z[W] \cdot I \\ j\omega (\Phi_L - \Phi_R) = j\omega L_0 \cdot I \\ j\omega \Phi_R = Z_R[W] \cdot I \end{array} \right\}$$

$$I = \tilde{I} \cdot e^{j\omega t}$$

$$(Z_R[W] + j\omega L_0 + Z_L[W]) \cdot \tilde{I} = \tilde{V}_{in}$$

$$\left[j(Im Z_R[W] + Im Z_L[W] + \omega L_0) + Re Z_L[W] \right] \cdot \tilde{I} = \tilde{V}_{in}$$