## Code for ikinelbow:

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% ikinelbow computes the inverse kinematics for the 7 DoF Baxter robot
% constrained to be 6 DoF with theta3=0
      theta (joint angle) values given specification of the robot geometry
      and a desired end position and orientation
      i.e. (a1, a2)
    i.e. (d1, d4, d6)
    Tw_tool = Homogeneous transformation matrix which specifies a desired
    location and orientation of the end effector from the tool frame with
    respect to the world frame
    LR = 1 if specifying the "lefty" solution and 0 if specifying the
    UD = 1 if specifying the "elbow up" solution and 0 if specifying the
    "elbow down" solution
    NF = 1 if specifying the "flip" solution and 0 if specifying the
      Ryan Dalby
      ME EN 6220
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function [theta] = ikinelbow(a,d,Tw_tool,LR,UD,NF)
theta = zeros(1,6);
R_w_tool = Tw_tool(1:3,1:3);
d_w_wtool = Tw_tool(1:3,4);
a1 = a(1);
a2 = a(2);
d1 = d(1);
d4 = d(2);
d6 = d(3);
R_w_0 = [sqrt(2)/2 \ sqrt(2)/2 \ 0;...
         -sqrt(2)/2 sqrt(2)/2 0;...
         0 0 1];
L = 221; \% mm
h = 22; \% mm
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H = 1104; % mm
d_{w_w} = [L; h; H];
% Information for transformation between frame 6 and tool frame
R_6_tool = [1 0 0;...
         0 1 0;...
         0 0 1];
d 6 4tool = [0; 0; d6];
% Extract necessary information to use solution used in ikinebaxter
R_0_6 = transpose(R_w_0)*R_w_tool*transpose(R_6_tool);
d 0 0tool = transpose(R_w_0)*(d_w_wtool-d_w_w0);
d 0 4tool = R 0 6 * d 6 4tool;
d 0 04 = d 0 0tool - d 0 4tool;
% Workspace determination
% Assume that d4=374.29mm, a2=370.82mm, and a1=69mm
d_{00} = d_{00} = d_{00}
d_{00} = mag = norm(d_{00} = 06);
inner_primary_workspace_diameter = a1+a2-d4;
outer primary workspace diameter = a2+d4-a1;
if (d_0_06_mag < inner_primary_workspace_diameter) || (d_0_06_mag >
outer_primary_workspace diameter)
    disp('Outside of primary workspace');
    return;
end
% Regional structure inverse kinematics
% theta 1 determination
theta(1) = atan2(d_0_04(2), d_0_04(1));
if (~LR)
    theta(1) = theta(1) + pi;
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end
% theta 3 and theta 2 determination
d_0_01 = [a1*cos(theta(1)); a1*sin(theta(1)); d1];
R_1_0 = [\cos(\text{theta}(1)) \sin(\text{theta}(1)) 0;...
         0 0 -1;...
          -sin(theta(1)) cos(theta(1)) 0];
d_1_14 = R_1_0 * (d_0_04-d_0_01);
r2 = d_1_14(1)^2 + d_1_14(2)^2;
alpha = 2*atan2(sqrt((a2+d4)^2 - (r2)), sqrt((r2) - (a2-d4)^2));
if(~UD)
    alpha = alpha * -1;
end
theta(3) = alpha - pi/2;
psi = atan2((d4*sin(alpha)),(a2+d4*cos(alpha)));
phi = atan2(d_1_14(2),d_1_14(1));
theta(2) = phi - psi;
% Orientation structure inverse kinematics
R_0_1 = transpose(R_1_0);
R_1_2 = [\cos(\text{theta}(2)) - \sin(\text{theta}(2)) \ 0;...
          sin(theta(2)) cos(theta(2)) 0;...
          0 0 1];
R_2_3 = [\cos(\text{theta}(3)) \circ -\sin(\text{theta}(3));...
          sin(theta(3)) @ cos(theta(3));...
          0 -1 0];
R 0 3 = R 0 1*R 1 2*R 2 3;
R_{3_6} = transpose(R_{0_3}) * R_{0_6};
% theta 4 determination
theta(4) = atan2(-R_3_6(2,3),-R_3_6(1,3));
if(NF)
    theta(4) = theta(4) + pi;
end
% theta 5 and theta 6 determination
R_3_4 = [\cos(\text{theta}(4)) \circ \sin(\text{theta}(4));...
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sin(theta(4)) 0 -cos(theta(4));...
0 1 0];

R_4_6 = transpose(R_3_4) * R_3_6;

theta(5) = atan2(-R_4_6(1,3),R_4_6(2,3));

theta(6) = atan2(-R_4_6(3,1),-R_4_6(3,2));
end
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