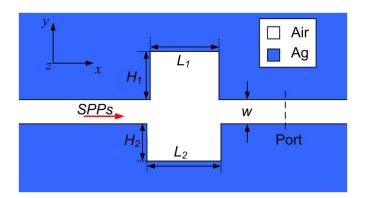




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Multiple Fano Resonances Based on Different Waveguide Modes in a Symmetry Breaking Plasmonic System

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Abstract: Multiple Fano resonances are numerically investigated based on different waveguide modes in a nanoscale plasmonic waveguide resonator system, which consists of two grooves coupled with a metal_insulator_metal (MIM) waveguide. Simulation results show that by introducing a small structural breaking in the plasmonic resonator, both symmetric and antisymmetric waveguide modes can be excited. Due to the interaction of the symmetric and antisymmetric waveguide modes, the transmission spectra possess a sharp asymmetrical profile. Because of different origins, these Fano resonances exhibit different dependence on the parameters of the structure and can be easily tuned. These characteristics offer flexibility to design the device. This nanosensor yields a sensitivity of ~820 nm/RIU and a figure-of-merit of ~3.2 × 10⁵. The utilization of the antisymmetric mode in the MIM waveguide provides a new possibility for designing high-performance plasmonic devices.

Index Terms: Surface plasmons, Fano resonance, resonator, sensor.

1. Introduction

Fano resonances have been studied extensively in quantum systems, and were realized well in plasmonic nanostructures in recent years. These resonances usually arise from the coupling and interference of a non-radiative mode and a continuum of radiative electromagnetic waves and are distinguished from the Lorentzian like profile by a distinctive asymmetric line shape [1], [2]. They have been observed in various plasmonic structures, such as nanoshells [3]–[5], rings [6]–[9], polymers [10]–[13] and metal–insulator–metal (MIM) waveguide [14]–[18]. Due to the advantage for enhanced bio-chemical sensing, spectroscopy, and multicolor nonlinear processes, the multiple Fano resonances become more important and have gained much attention [19]–[23]. Among all the nanostructures, the MIM waveguide structures have attracted many researchers attention because these structures exhibiting more suitable for the highly integrated optical circuits due to their deep-sub-wavelength confinement of light [24]–[27]. In the MIM waveguide, both of the symmetric and anti-symmetric waveguide modes could always be supported without modal cutoff in the visible and near-infrared wavelength ranges [28], [29]. The

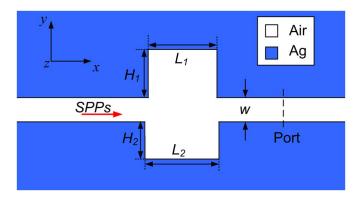


Fig. 1. Schematic configuration and geometric parameters of the plasmonic waveguide system.

symmetric waveguide mode in the MIM waveguide has long propagation lengths $(>10~\mu m)$ [28], and thus, it was widely used in the ultra-small plasmonic devices [14]–[27], while the anti-symmetric waveguide mode in the MIM waveguide was hardly used in the SPP devices, especially in the MIM-based resonators. This is mainly attributed to its large propagation loss (propagation length \sim 10 nm) [28] and its critical excitation condition [30]. In our previous work [31], we first introduced a metallic baffle in the wide gap resonator to excite the anti-symmetric mode, but the small baffle is difficult to fabricate due to the process technology, and only one Fano resonance profile was achieved.

In this paper, a MIM waveguide coupled with two different grooves is proposed to generate multiple Fano resonances. Simulation results show that by introducing a small structural breaking in the plasmonic resonator, both symmetric and anti-symmetric waveguide modes can be excited. Due to the interaction of the symmetric and anti-symmetric waveguide modes, the transmission spectra possess a sharp asymmetrical profile. Because of different origins, these Fano resonances exhibit different dependence on the parameters of the structure, and can be easily tuned. The proposed sub-structure can serve as an excellent plasmonic sensor with a sensitivity of \sim 820 nm/RIU and a figure of merit of \sim 3.2 × 10 5 . The utilization of the antisymmetric mode in the MIM waveguide provided a new possibility for designing high-performance plasmonic devices.

2. Structure and Simulations

The proposed plasmonic waveguide structure is schematically shown in Fig. 1, which is composed of a MIM structure with two different grooves. This system is a two-dimensional model, and the white and blue parts denote air $(\varepsilon_d=1.0)$ and Ag (ε_m) , respectively. The permittivity of Ag is characterized by the Drude model: $\varepsilon_m=\varepsilon_\infty-\omega_p^2/(\omega^2+i\omega\gamma)$ with $\varepsilon_\infty=3.7$, $\omega_p=9.1$ eV. $\gamma=0.018$ eV [32]. The length and height of the two grooves are L_1 , H_1 and L_2 , H_2 , respectively. The width of the MIM waveguide is w. The transmittance of SPPs is defined as the quotient between the SPP power flows (obtained by integrating the Poynting vector over the channel cross-section) of the observing port with structures (two grooves) and without structures [25], [27].

In order to investigate the optical responses of the proposed structure, its transmission spectra are numerically calculated using the finite element method (FEM) of COMSOL Multiphysics. In the simulations, first perform the boundary mode analysis on the input port of the structure and then solve the wave propagation problem using the mode shape obtained by the first step as a boundary condition. The width of the MIM waveguide is set to be w = 50 nm and is fixed throughout the paper. The lengths of the two grooves are set to be w = 50 nm, w = 100 nm, the height of the low groove is set to be w = 100 nm. In this case, the two grooves can be act as a plasmonic resonator, and the calculated transmission spectra are displayed in Fig. 2(a)–(e). Here, w = 100 here,

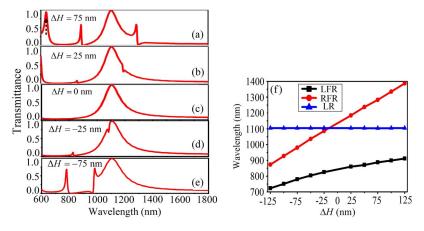


Fig. 2. Transmission spectra of the plasmonic waveguide system for different ΔH of (a) $\Delta H = 75$ nm, (b) $\Delta H = 25$ nm, (c) $\Delta H = 0$ nm, (d) $\Delta H = -25$ nm, and (e) $\Delta H = -75$ nm when $L_1 = 500$ nm, $L_2 = 500$ nm, and $L_2 = 225$ nm. (f) Dependence of the resonant wavelengths on the difference ΔH .

transmission spectra when $\Delta H \neq 0$. When $\Delta H = 0$ nm, only the broad Lorentzian-like profile is observed, as shown in Fig. 2(c), indicating that only the symmetry of the structure is broken, Fano resonances can be emerge. Specifically, when $\Delta H = 75$ nm, another Fano resonance peak appears in the transmission spectrum, as shown in Fig. 2(a) (denoted by the black arrow), and to facilitate the presentation, we call it the new Fano resonance or NFR.

As we know, in a rectangular cavity, the x- and y-directional resonances can be excited. We use mode (m, n) to denote different resonant modes in the rectangular cavity, m, n are integers and indicate the x- and y-directional resonant orders, respectively. In a plasmonic resonator, the accumulated phased shift per round trip for the SPPs is $\Phi = 4\pi n_{\rm eff} S/\lambda + 2\varphi$ [33], [34]. Constructive interference should occur when $\Phi = 2N\pi$, and thus the resonant wavelength is determined by

$$\lambda = \frac{2n_{\text{neff}}S}{(N - \varphi/\pi)} \tag{1}$$

where n_{eff} denotes the effective index of the SPPs, which can be obtained by solving the eigenfunction in the MIM waveguide [35]. φ is the phase shift brought by the SPP reflection off the metal wall in the resonator, S presents the L or H ($H_1 + H_2 + w$) of the rectangular cavity, and $N = 2^{m+n}$. Based on (1), we can obtain that the dependence of the variation of the resonant wavelength on the resonator length S is

$$\frac{d\lambda}{dS} = \frac{2n_{\text{eff}}}{N - \varphi/\pi}.$$
 (2)

In order to understand the underlying physics of the resonant peaks in the transmission spectra, the corresponding field distributions of $|H_z|^2$ at the transmission peaks in the proposed structure with $L_1=500$ nm, $L_2=500$ nm, $H_2=225$ nm, and $\Delta H=75$ nm are displayed in Fig. 3(a)–(d). Obviously, the four resonant modes can be named mode (1, 0), mode (0, 1), mode (1, 1), and mode (0, 2) for Fig. 3(a)–(d), respectively. First, we begin with the broad Lorentzian resonance or LR mode, which exhibits a nearly symmetric Lorentzian-like profile, as shown in Fig. 2. From Fig. 3(a), it is found that there is no node for the distribution along the y-axis direction for the broad transmission peak at $\lambda=1103$ nm, yielding a symmetric waveguide mode in the plasmonic resonator. Moreover, its resonant wavelength keeps almost unchanged $(\Delta \lambda/\Delta H\approx 0)$ with the difference ΔH increasing, as shown by the blue symbol line in Fig. 2(f). Because the resonant wavelength of LR is determined by the fixed values of L [33], we find that there is a large distribution proportion of the electromagnetic field at the connecting part between the

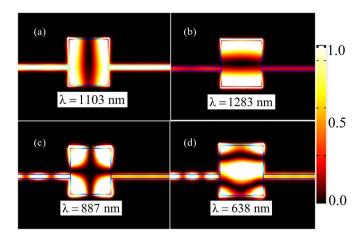


Fig. 3. Field distributions $(|H_z|^2)$ at (a) $\lambda=638$ nm, (b) $\lambda=1103$ nm, (c) $\lambda=887$ nm, and (d) $\lambda=1283$ nm for the proposed structure at $\Delta H=75$ nm.

plasmonic resonator and the MIM waveguide. Thus, the power flow of the symmetric waveguide mode in the plasmonic resonator can be easily leaked into the MIM waveguide, bringing a large leaky loss for the symmetric waveguide mode. As a result, the symmetric mode results in a broad Lorentzian-like response profile [see Fig. 2(c)], similar to the results in the previous reports [14], [18], [27], [32]–[34].

However, the situation for the left Fano resonance (LFR) or mode (1, 1) becomes different. Increasing ΔH , the resonant wavelengths of LFR has a redshift with a slope of $\Delta \lambda/\Delta H \approx 0.85$, as shown by the black symbol line in Fig. 2(f). Evidently, a standing wave pattern with strong intensities is excited in the plasmonic resonator because of the structural breaking [19]. Moreover, there exists each node for the distribution along the x- and y-axis direction, yielding an anti-symmetric waveguide mode in the plasmonic resonator [31]. In this case, the anti-node is nearly at the connecting part of the plasmonic resonator and the MIM waveguide, as shown in Fig. 3(c). Thus, the power flow of the anti-symmetric waveguide mode in the plasmonic resonator is difficult to leak into the MIM waveguide. That is, the power flow is trapped in the plasmonic resonator. This can result in a strongly trapped resonance in the plasmonic resonator, as shown in Fig. 3(c). Consequently, the interference of the narrow trapped resonance mode (1. 1) and the broad Lorentzian-like resonance mode (1, 0), which are based on different waveguide modes in the plasmonic resonator, gives rise to the Fano profile in the transmission spectra [1], [2], [14], [25], as shown in Fig. 2. For the mode (1, 1), the effective cavity length is L + H, and simulations show that φ equals about π . Thus, based on (2), it is easy to get that $d\lambda/dH \approx 2 \times 0.64/(4 - \pi/\pi) \times (1 + H/L) \approx 0.85$. These results agree well with the slope of the black symbol line in Fig. 2(f).

For the right Fano resonance (RFR) or mode (0, 1), it is also redshift with a slope $\Delta\lambda/\Delta H\approx 2$ when the height of the resonator increases, as shown in the red symbol line in Fig. 2(f). In this case, the antinodes of the standing wave pattern appear on both up and bottom edges of the resonator. Thus, the power flow of this waveguide mode in the plasmonic resonator is difficult to leak into the MIM waveguide. That is, the power flow is trapped in the plasmonic resonator. This can result in a strongly trapped resonance in the plasmonic resonator, as shown in Fig. 3(b). Consequently, the interference of the narrow trapped resonance mode (0, 1) and the broad Lorentzian-like resonance mode (1, 0), which are based on different waveguide modes in the plasmonic resonator, gives rise to the Fano profile in the transmission spectra [1], [2], [14], [25], as shown in Fig. 2. For the mode (0, 1), we have S = H, $N = 2^{0+1} = 2$. Thus, the (2) becomes $d\lambda/dH \approx 2 \times 1/(2 - \pi/\pi) \times (H/H) = 2$, agreeing well with the slope of the red symbol line in Fig. 2(f). According to above analysis, we know that the new Fano resonance (NFR) originates from the interference between the mode (1, 0) and the mode (0, 2).

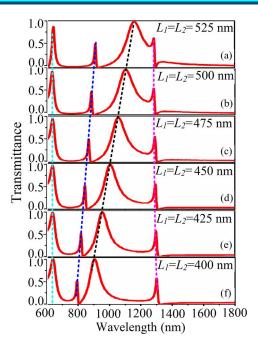


Fig. 4. Transmission spectra for different resonator length of (a) $L_1=L_2=525$ nm, (b) $L_1=L_2=500$ nm, (c) $L_1=L_2=475$ nm, (d) $L_1=L_2=450$ nm, (e) $L_1=L_2=425$ nm, and (f) $L_1=L_2=400$ nm when $H_1=300$ nm, and $H_2=225$ nm.

To further test our analysis, the transmission spectra of the broken plasmonic resonator are calculated by varying L_1 and L_2 , simultaneously, when $H_1=300$ nm, $H_2=225$ nm, and the results are displayed in Fig. 4. In this case, the height of the plasmonic resonator $H=H_1+H_2$ is fixed. It is observed the new Fano resonance and right Fano resonance are hardly carried because their resonant wavelengths are determined by the fixed values of H [33], as shown by the green and purple dotted lines in Fig. 4. For the left Fano resonance or mode (1, 1), we know that its resonant wavelength is determined by the values of H and L, and they have the same influence on it. Therefore, for a fixed L or H, the resonant wavelength of LFR has the similar change rule, as shown by the black symbol line in Fig. 2(f) and the blue dotted line in Fig. 4. For the Lorentzian resonance, it is observed that its resonant wavelength is linearly redshifted with increasing length L with a slope of $\Delta\lambda/\Delta L \approx 2$, as shown by the black dotted line in Fig. 4. This linear dependence between the resonant wavelength and the length of the resonator agrees well with the results in the literature [33], [34], as well as (2).

3. Sensing Applications Based on Fano Resonances

Because of the strongly trapped resonance, the Fano resonance exhibits sharp asymmetric profile, where the transmittance can drop or increase sharply from the peak (valley) to the valley (peak) of the spectra. Such a short wavelength change can provide a high sensitivity of spectrum response to the index variations of nearby or surrounding medium for the structure. Therefore, the insulator with different refractive index is employed to investigate the spectral response. The length of the two grooves are fixed to be $L_1 = 500$ nm, $L_2 = 500$ nm, $H_2 = 225$ nm. The transmission spectra are shown in Fig. 5(a) for $\Delta H = -75$ nm and Fig. 5(c) for $\Delta H = 75$ nm, respectively. The resonant wavelength has a red shift when increasing the refractive index. The sensitivity of a sensor (nm/RIU) is usually defined as the shift in the resonance wavelength per unit variations of the refractive index [36]. Thus, the sensitivity of the proposed structure is 680 nm/RIU, 820 nm/RIU and 840 nm/RIU, 1100 nm/RIU for the LFR and RFR at $\Delta H = -75$ nm and $\Delta H = 75$ nm, respectively. That is because the strong field confinement and low leaky loss in our structure [see Fig. 3(b) and (c)], making it more sensitive to the

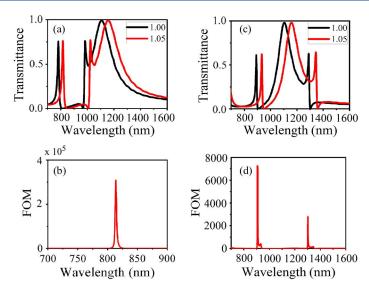


Fig. 5. Transmission spectra for different refractive index at (a) $\Delta H = -75$ nm, and (c) $\Delta H = 75$ nm. The calculated FOM at different wavelength for (b) $\Delta H = -75$ nm, and (d) $\Delta H = 75$ nm. The other parameters are fixed to be $L_1 = 500$ nm, $L_2 = 500$ nm, and $H_2 = 225$ nm.

refractive index of the material. These results are higher than those in the [18], [37]. To better evaluate the performance of the plasmonic sensor, the figure of merit (FOM) is studied, which defined as FOM = $\Delta T/(T\Delta n)$ [15], [38], [39], where T denotes the transmittance in the proposed structure. The calculated FOM for $\Delta H = -75$ nm and $\Delta H = 75$ nm are displayed in Fig. 5(b) and (d), respectively. The values of FOM is as high as 3.2×10^5 at $\lambda = 820$ nm when $\Delta H = -75$ nm (7400 at $\lambda = 900$ nm when $\Delta H = 75$ nm), which is due to the sharp asymmetric Fano line shape with ultra-low transmittance at this wavelength. These FOM values are significantly greater than that in the previous reports [18], [38].

Although, our structure is similar to that in [23], the parameters of our structure are very different with those in [23]. Many new phenomena emerge due to these differences. For example, the emerging of the anti-symmetric waveguide mode, which can be reflected back and forth off the right and left, up and bottom walls in the plasmonic resonator, constructing two Fabry–Perot resonators [14], [27], [40], makes our structure more functional in devices.

4. Conclusion

In summary, by utilizing the anti-symmetric waveguide mode in the MIM waveguide structure, an asymmetric plasmonic resonator was proposed to achieve multiple Fano resonances. The asymmetrical line shape and the resonant wavelength can be easily tuned by changing the geometrical parameters of the structure. Simulation results show that by introducing a small structural breaking in the plasmonic resonator, both symmetric and anti-symmetric waveguide modes can be excited. The interaction of the symmetric and anti-symmetric waveguide modes gives rise to the Fano resonances in the plasmonic system. These multiple Fano resonances resulted from different mechanisms and thus had different responses to the variations of the structural dimensions. A nano-sensor was designed based on the sharp asymmetrical profiles, which yielded a sensitivity of $\sim\!820$ nm/RIU and a figure of merit of $\sim\!3.2\times10^5$. The utilization of the anti-symmetric mode in the MIM waveguide provided a new possibility for designing high-performance plasmonic devices.

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