

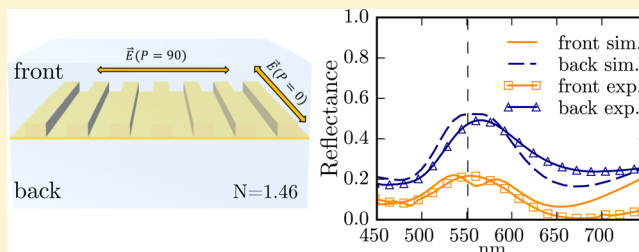
Bianisotropy and Magnetism in Plasmonic Gratings

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S Supporting Information

ABSTRACT: We present a simple design to achieve bianisotropy at visible wavelengths: an ultrathin plasmonic grating made of a gold grating covered by a thin flat layer of gold. We show experimentally and through simulations that the grating exhibits magnetoelectric coupling and features asymmetric reflection and absorption, all that with a device thickness of a tenth of the operating wavelength. We compared the spectral results and retrieved the effective material parameters of different polarizations and devices. We show that both asymmetry and strong coupling between the incoming light and the optically interacting surfaces are required for obtaining asymmetric optical behavior in metasurfaces.

KEYWORDS: bianisotropy, magnetism, plasmonics, grating, metamaterial



In their seminal book,¹ Landau and Lifshitz commented on the insignificance of magnetism at optical frequencies. Yet, several recent studies have shown that magnetic effects are present in optical systems,^{2–4} particularly those containing metals that have been structured in some way. The mechanism is familiar from the concept of metamaterials, whereby novel electrical and magnetic properties can be found by engineering the microstructure.^{5–8} Here we present an experimental study of a structured system, in our case a grating, and interpret the data in terms of effective parameters of an equivalent ultrathin layer of metamaterial. Features such as asymmetric reflection will emerge from the interplay of magnetic and electric fields.

Lately, a lot of attention has been given to the development of metasurfaces: textured surfaces at a subwavelength scale with tailored electromagnetic properties.^{9–14} These devices are the two-dimensional counterpart of metamaterials and benefit from the advantages of reduced profile, reduced ohmic and magnetic losses, and simpler fabrication processes, thus enabling a range of applications from analogue computing¹⁵ to “flat optics”¹⁶ and light-harvesting applications,^{17,18} to name a few.

A special class of metasurfaces comprises bianisotropic ones, that is, materials exhibiting coupling between the electric and magnetic fields,^{19–22} which are described by the constitutive relations¹⁹ $D = \epsilon E + \xi H$ and $B = \mu H + \zeta E$ (see **Methods**), with the coupling parameters ξ and ζ relating the displacement current (D) with the magnetic field (H), and the magnetic flux density (B) with the electrical field (E), respectively. A typical characteristic of bianisotropic structures is their asymmetric response depending on which side of the structure they are being probed from.²³

There is a large body of literature discussing bianisotropy in the THz^{21,24} and GHz regimes,^{25–28} with applications in polarization changers,^{27,29} asymmetric absorbers/reflectors,^{25,28} and perfect absorbers.³⁰ However, in the spectral optical

regime, very few experimental studies exist.^{29,31,32} Recently, an asymmetric absorber operating in the visible frequency range has been designed,³² where the asymmetry originates from a dielectric–metal stack of thin Ag nanohole arrays patterned over a silicon nitride membrane.

In this paper we show experimentally that asymmetric reflection based on bianisotropy and magnetoelectric coupling can be achieved at visible wavelengths simply using all-metal plasmonic gratings with reduced thickness of the active region, in a design that requires simple and commonly used fabrication methods. Electrodynamical simulations are compared with experimental results and are interpreted in terms of the effective material parameters of the system, which clearly indicate magnetoelectric coupling.

RESULTS AND DISCUSSION

Our bianisotropic metamaterial structure is made of metallic grating lines of width 100 nm and a thin conducting layer covering the grating lines and the spacing (also 100 nm) between them. These dimensions provide a good trade-off between entering the subwavelength regime, which is necessary for a subsequent metamaterial description, and a good uniformity across the grating in the fabrication process. **Figure 1** illustrates the bianisotropic structure—80 $\mu\text{m} \times 80 \mu\text{m}$ arrays of a 50 nm thick gold grating covered by 10 nm layer of gold—next to a “control” structure with a similar grating array (with slightly larger grating lines due to fabrication imperfections), but lacking the thin gold layer. The two types of gold structures were fabricated by means of electron beam lithography and thermal evaporation on the same quartz substrate. Finally, in

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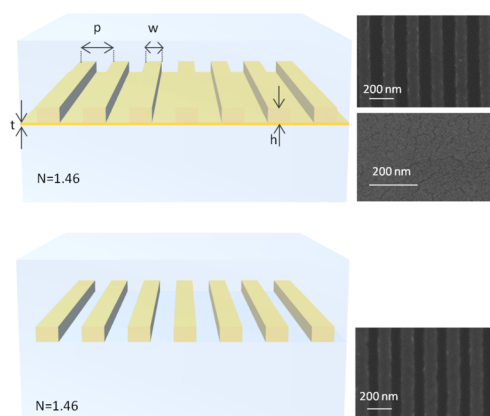


Figure 1. Grating structures. (Top) Bianisotropic structure. The letters and arrows indicate the physical dimensions of the structure: $w = 100$ nm is the width of grating lines; $p = 200$ nm is the grating pitch; $t = 10$ nm is the thickness of the gold layer; and $h = 55$ nm is the thickness of the grating lines (including the 10 nm gold layer that covers both the grating lines and the spacing between them). (Bottom) Control structure with $w = 110$ nm, $p = 200$ nm, and $h = 45$ nm. Both structures are embedded within a medium with $n = 1.46$ at $\lambda = 560$ nm. Placed to the right of the illustrations are close-up SEM images of the two grating structures (taken before the deposition of the thin film of gold), and the thin gold layer; all SEM images were taken before the attachment of the covering quartz slide.

order to limit asymmetries in the device only to the active metallic gratings (and not to the substrate, for example), the device was completed by the bonding of another quartz slab on top of the structures (see [Methods](#) for fabrication details).

Reflection and Transmission Spectra. The reflection and transmission spectra of the two types of structures were obtained using a setup of an optical microscope coupled to a grating spectrometer for two linear polarizations: one for which the electric field is aligned with the grating lines ($P = 0$) and one where the polarization is orthogonal to the gratings lines ($P = 90$). For both simulations and measurements the plane wave is normally incident (note that in our experiments, though centered around the normal to the plane of the gratings, the plane wave is distributed throughout the numerical aperture of the objective ($N = 0.5$)). The recording of the transmitted and reflected light was completed via Si photodiodes coupled to a lock-in amplifier ([Figure 2](#); see [Methods](#) for detailed information about the measurement setup).

[Figure 3](#) shows the experimental and simulated reflectance spectra for the bianisotropic and the control structures. For polarized light with its electric field *orthogonal* to the grating lines it shows a remarkable difference between the control sample with the metal gratings only and the bianisotropic sample with the additional thin layer of gold: while the reflection spectra of the control structure ([Figure 3c](#)) are inherently indifferent to the direction of incoming light, as expected from an optically symmetric structure, the reflection signal of the gold grating with the additional thin gold layer ([Figure 3a](#)) is up to ~ 3 times stronger when the device is probed from the side of the thin film (aka, “back exposure”), compared to probing from the corrugated side (“front exposure”). For this polarization of the electrical field the bianisotropic and the control devices show a plasmon resonance with maximal reflection at ~ 550 and ~ 595 nm, respectively, indicating strong coupling to the incident light. The difference in the resonance position partly arises because of

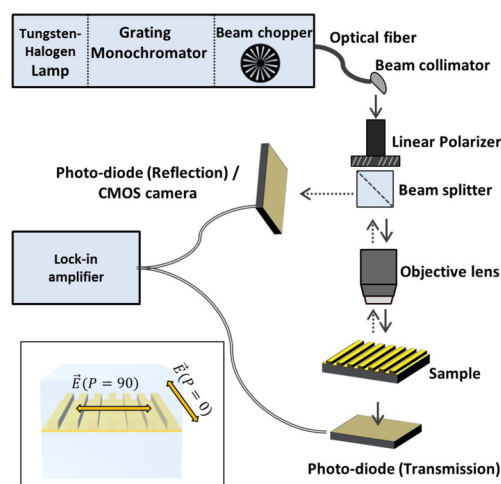


Figure 2. Experimental setup for transmission and reflection measurements. White light is being diffracted, chopped, and coupled to an optical microscope via an optical fiber and beam collimator. The collimated monochromatic light was linearly polarized (along or transversely to the gratings lines — indicated in the inset as “ $P = 0$ ” and “ $P = 90$ ”, respectively) and focused on the structures. A beam splitter was used to direct the reflected light toward the reflection photodiode (the path of the reflected light is indicated by dashed arrows) or toward a camera used to assist in locating the structures on the sample. The transmitted/reflected light was recorded on Si photodiodes connected to a lock-in amplifier.

the difference in the width of the grating lines, *but* is mostly due to the addition of the thin conducting layer, which alters the physical response of the system. Also note that the coupling to the plasmon can increase both the reflectance and absorption (not shown here), hence the peak in reflection at the plasmonic resonance in [Figure 3](#); energy conservation then demands a reduction in transmission at the resonance, as observed in [Figure 4](#).

When probing the metal grating with the electrical field polarized *along* the grating lines ([Figure 3b](#) and [d](#)), both the plasmon resonance and the asymmetric reflection diminish, and we are left with a reflection curve akin to that of a planar Au layer. Unlike the reflection spectra, the transmission curve ([Figure 4](#)) is independent of the illumination direction, regardless of structure and polarization, as it must be due to reciprocity. For all structures and polarizations we see a qualitative agreement between experimental and numerical results, with quantitative differences arising most likely from fabrication imperfections and uncertainties in the value of the permittivity.

It appears that an asymmetric reflection from our low-profile structures is evident when the following two conditions are satisfied simultaneously: (a) the device has to bear some optical asymmetry and (b) the incoming light has to be strongly coupled to, and absorbed by, the active part of the device, here, achieved by means of plasmonic coupling between the incident light and the grating, when probed with the appropriate polarization. It is worth noting that, in *bulk* materials and structures, an optical asymmetry—and therefore asymmetric reflection—is abundant in nature and our daily life. Take for example a single side polished silicon wafer or a common bathroom mirror; both meet the former condition above and demonstrate asymmetric reflection with one side reflecting more than the other. However, while the asymmetric reflection in the case of the two macroscopic examples given above is due

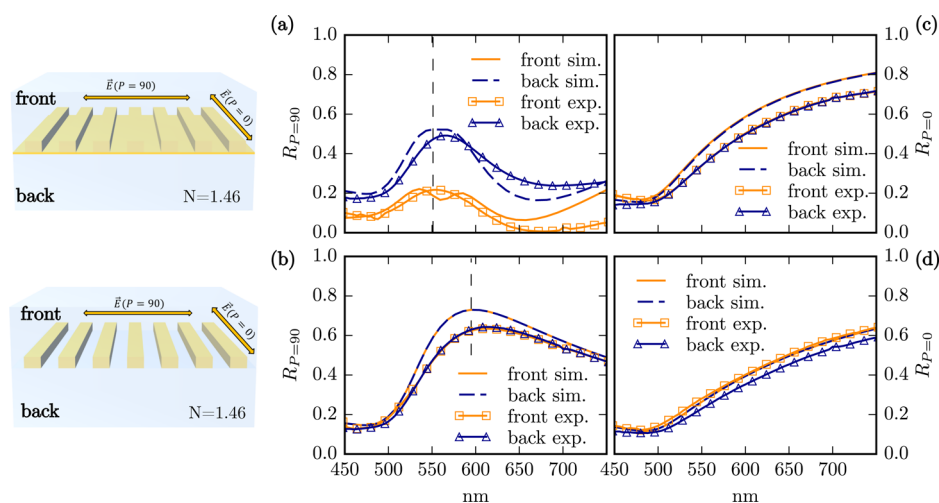


Figure 3. Reflectance spectra. Open triangles and squares are the experimental results for “back” and “front” exposure, as defined in the illustration on the left to the plots; blue dashed and orange solid lines correspond to numerical simulations of “back” and “front” exposures. (a) Bianisotropic structure probed with orthogonal polarization of the electric field ($P = 90^\circ$). (c) Bianisotropic structure excited with polarization of the electric field along the grating lines ($P = 0^\circ$). (b and d) Control structure with metal grating only for electrical-field polarizations $P = 90^\circ$ and $P = 0^\circ$, respectively. The vertical dashed lines indicate the spectral positions of the resonant peaks.

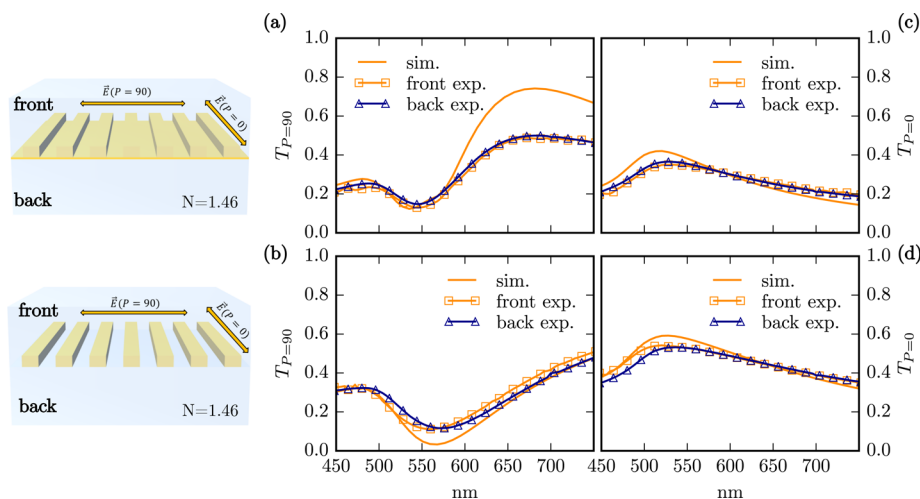


Figure 4. Transmission spectra. Open triangles and squares are the experimental results for “back” and “front” exposure, as defined in the illustration on the left to the plots; blue dashed and orange solid lines correspond to numerical simulations of “back” and “front” exposures. (a) Bianisotropic structure probed with orthogonal polarization of the electric field ($P = 90^\circ$). (c) Bianisotropic structure excited with polarization of the electric field along the grating lines ($P = 0^\circ$). (b and d) Reflection spectra of the control structure with metal grating only for electrical field polarizations $P = 90^\circ$ and $P = 0^\circ$, respectively.

to their two dissimilar noninteracting surfaces, achieving asymmetric reflection while maintaining a low structure profile on the order of $\lambda/10$, as demonstrated here, requires a design that meets also the second condition of strong coupling between the incoming light and the optically interacting surfaces.

As asymmetric reflection could be observed only for the grating with the 10 nm connecting layer of gold, it is clear that understanding the role of the thin conducting layer is crucial for the understanding of the origin of the asymmetric reflection: the conductive layer electrically connects neighboring grating lines, therefore enabling a flow of electrical current in the direction normal to the grating lines ($P = 90^\circ$). The induced current, in turn, generates a magnetic field³³ radiating energy into the far field and interfering with the incident wave. This effect is enhanced via a plasmon resonance, as more energy is coupled into the grating. However, the structural asymmetry

leads to different coupling strengths for front or back illumination. If the light is incident on the flat side, the surface does not immediately provide the missing momentum to couple to plasmons, so that a large fraction of the light is reflected. On the corrugated side, the surface immediately provides the missing momentum and coupling into plasmons is more efficient, leading to higher absorption and thus reduced reflection properties. This behavior is well known from bianisotropic bulk materials exhibiting magnetoelectric coupling.^{19,23} In order to further investigate the magnetoelectric coupling and quantify its strength, we continue by modeling our metasurface as a bianisotropic metamaterial.^{19,23}

Effective Material Parameters and Bianisotropy. An asymmetric reflection/absorption spectrum cannot be described by a *homogeneous* slab model using effective permittivity and permeability alone; instead, magnetoelectric coupling has to be introduced to the physical model by modifying the

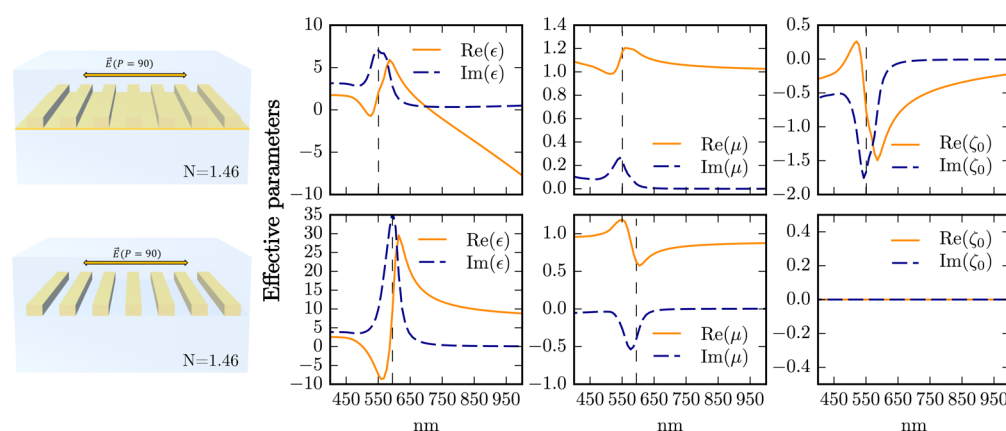


Figure 5. Effective material parameters retrieved from numerical simulations of the gold gratings described in Figure 1. Results are for $P = 90$. The left column shows the effective permittivity, the middle column the effective permeability, and the right column the bianisotropic coupling parameter. We used standard retrieval methods^{21,23,34} and assumed a symmetric metamaterial slab with thickness d_{eff} equal to the maximum thickness of the gold gratings, i.e., $d_{\text{eff}} = 55$ nm for the connected (top) and $d_{\text{eff}} = 45$ nm for the unconnected grating (bottom). The vertical dashed lines indicate the positions of the respective reflection maxima.

constitutive relations.^{19,21,23} The magnetoelectric coupling is quantified by new material parameters, ζ and ξ (see the introduction), which make the electric and magnetic fields interact in a way such that even a symmetric slab exhibits asymmetric reflection.^{19,21,23}

We model our connected grating as a homogeneous bianisotropic slab and compare against the control grating. Note that the magnetoelectric coupling parameters ξ and ζ are determined by a single parameter ζ_0 , on which we focus hereafter. For a determination of the effective material parameters, both the phase and magnitude of the reflection/transmission coefficient are needed. Since our experimental setup gives access to the magnitude, but not the phase, we subsequently focus on the simulations. Figure 5 shows the material parameters retrieved from simulations of the types of gold grating structures for $P = 90$. Clearly, the interplay of plasmon resonance and structural asymmetry in the connected gold grating leads to an induced magnetoelectric effect, as demonstrated by the strong resonance in the coupling parameter ζ_0 . The control grating, however, shows no such coupling, highlighting the importance of that thin connecting Au layer for the design. Figure 5 exhibits two additional differences between the bianisotropic and control gratings. First, although both samples feature optical magnetic effects (resonant permeability) at the plasmon resonance, the permeability of the control grating does not return to unity in the long-wavelength limit, but remains weakly diamagnetic. This seemingly counterintuitive result is explained as follows. In the long-wavelength limit, gold approaches a perfect conductor, thus expelling part of the magnetic field from its interior. This results in “squeezing” of the magnetic field lines through the gaps of the grating, leading to the diamagnetic effect observed.³⁵ The smaller the gap, the stronger this effect (see Figure S4 in the Supporting Information).

The case of the bianisotropic sample with the connected grating is understood by analogy with a superconductor where the permeability is unity, but the permittivity diverges inversely as the frequency squared. In this case magnetic fields are expelled entirely through the action of the permittivity, contrary to some misinformed statements to the effect that superconductors are perfect diamagnets. In Figure 5 top left we see

that for the continuously connected sample the effective permittivity diverges at long wavelengths.

For the other polarization, $P = 0$, none of the effects above are featured, as the electric field is polarized along the grating lines and current can flow freely in both the control and bianisotropic gratings, similar to the current flow in thin gold films. The effective material parameters for this case are shown in the Supporting Information (Figure S5) for completeness.

CONCLUSION

We demonstrated experimentally and through simulations that plasmonic gratings provide a simple design for asymmetric reflectors/absorbers at visible wavelengths. We found that the asymmetry in the spectra is a direct consequence of magnetoelectric coupling in the grating, i.e., bianisotropy, and should be interpreted as such. The strength of the bianisotropy provides a good measure for the expected asymmetry in the spectra and may be used for the optimization of this effect, as has been done at much lower frequencies previously.²⁵ Finally, the bianisotropy of our grating is inherent to it, rather than induced by a substrate,³² which leads to an extremely small footprint of the structure (~ 55 nm thickness). Further optimizations in the grating design and fabrication are certain to enhance the strength of the asymmetry.

METHODS

Experimental Setup and Fabrication. *Fabrication of Grating Structures.* First, quartz substrates were cleaned by ultrasonic agitation in an acetone bath, followed up by IPA and DIW rinse. A poly(methyl methacrylate) (PMMA 950, A4) positive resist was spun on the cleaned substrates at 3500 rpm for 60 s and soft-baked on a hot plate at 180 °C for 60 s, forming a 250 nm lift-off mask. Multiple arrays of grating lines were defined using a Raith Elne electron beam lithography tool at 10 kV accelerating voltage and 10 μm aperture and developed for 30 s in 1:3 methyl isobutyl ketone/isopropyl alcohol developer. Prior to the deposition of gold grating lines, the surface was modified to improve the adhesion of gold to the SiO_2 substrate: a drop of (3-aminopropyl)triethoxysilane diluted in ethanol at a volumetric ratio of 1:25 was dropped and was left on the sample for 30 s before being washed in ethanol and dried on a hot plate at 90 °C for 15 min. Au (45

nm) was thermally evaporated (Angstrom AMOD) at a rate of 2 Å/s. The fabrication of the grating pattern was completed by lift-off of the gold layer in an acetone bath for 24 h at room temperature. After lift-off, the surface was functionalized again (as discussed above), and an additional layer of 10 nm of Au was deposited on the sample (at a higher deposition rate of 5 Å/s to improve surface uniformity) through a mechanical mask that shaded half of the sample, completing the control, and bianisotropic structures on a single substrate. The device was finished by bonding an additional quartz substrate on top, using a UV-cured, indexed-matched, low-viscosity optical glue (Norland Optical Adhesive 85).

Reflection Transmission Measurements. These were carried out using a custom-made microscope setup: The output of a halogen lamp connected to a Bentham Instruments monochromator was coupled to a multimode optical fiber with a reflective collimator at its end. The collimated beam passed through a Glan-Thompson polarizer (Thorlabs) and a nonpolarizing beamsplitter cube (coated with antireflective coating optimized to 400–700 nm; Thorlabs) before entering a custom-built microscope system and focused to a spot of diameter 50 μm via a 50× long-working distance objective lens with NA = 0.5 (see Figure 2). The reflected and transmitted spectra were recorded using a Si photodiode connected to a lock-in amplifier. Absolute transmission values were calculated by dividing the measured transmission photocurrent by the measured current without the sample. Absolute reflection values were calculated by first subtracting background reflections (originated mainly from the beam splitter for wavelengths below ~450 nm or above ~680 nm; measured for the same optical path without the sample) from the reflection photocurrent and from the reflectance measured from a calibrated silver-coated mirror and then dividing the background-free reflectance current of the sample by that of the calibrated mirror.

Numerical Modeling. The numerical simulations were carried out using the frequency domain solver of the commercial software package COMSOL Multiphysics (version 4.3a). We used the port boundary conditions to set up the exciting plane wave and periodic boundary conditions for the other two boundaries. The length of the simulation domain has been set to 1500 nm, and convergence with respect to it had been ensured. We used an adaptive triangular mesh with a maximum element size of 2 nm inside the gold gratings and 10 nm in the surrounding medium; again convergence had been ensured. The exact dimensions of the gratings were chosen in accordance with the experimental structures; detailed sketches can be found in the Supporting Information. We used experimental values for the permittivity of an evaporated gold film from reference 36. The port boundary conditions allow computing the scattering, i.e., S-parameters of the system, from which reflectance and transmittance can be deduced, as well as the effective material parameters.^{21,23,34}

In this Letter we modeled the two gratings as a bianisotropic metamaterial. That is, we replaced the whole system with a symmetric metamaterial slab of thickness d_{eff} and effective material parameters determined by the scattering parameters of the gratings. Bianisotropy means that the electric and magnetic fields inside such a material are coupled via^{19,23}

$$D = \epsilon E + \xi H$$

$$B = \mu H + \zeta E$$

with permittivity and permeability tensor^{19,23}

$$\epsilon = \begin{pmatrix} \epsilon_x & 0 & 0 \\ 0 & \epsilon_y & 0 \\ 0 & 0 & \epsilon_z \end{pmatrix}, \quad \mu = \begin{pmatrix} \mu_x & 0 & 0 \\ 0 & \mu_y & 0 \\ 0 & 0 & \mu_z \end{pmatrix} \quad (1)$$

and magnetoelectric coupling matrices,^{19,23}

$$\xi = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & -i\xi_0 & 0 \end{pmatrix}, \quad \zeta = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & i\xi_0 \\ 0 & 0 & 0 \end{pmatrix} \quad (2)$$

The magnetoelectric coupling parameter that has been retrieved in this Letter corresponds to the effective ξ_0 . In our system we assumed the grating to lie in the y - z -plane, with the grating lines pointing along the z -direction and the periodic modulation along the y -direction. This means that for a wave traveling along the x -direction and polarized along y ($P = 90$ here) the effective permittivity and permeability component that are probed are ϵ_y and μ_z , respectively, whereas the $P = 0$ case probes ϵ_z and μ_y .

In our simulations we can access the S-parameters of the system by using “Port boundary conditions”. However, the effective material parameters cannot be accessed directly in COMSOL. For this some postprocessing is needed. Fortunately, standard methods have been developed to retrieve material parameters for a symmetric metamaterial slab from the S-parameters.^{21,23,34} In our case, the thickness, d_{eff} of this metamaterial slab was chosen to be the maximum thickness of the gold gratings.

■ ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsphotonics.6b00206.

It includes enlarged SEM images of the bianisotropic and control gratings, detailed profiles of the gratings used in the simulations, a figure showing the mode profile at the plasmon resonance, a figure comparing the retrieved effective permeability for control gratings with different gap sizes between the grating lines for $P = 90$ and a figure for the effective parameters for $P = 0$ polarization. (PDF)

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Notes

The authors declare no competing financial interest.

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