## Appendix I: Cryogenic Reference Tables

## **Cryogenic Heat Flow Calculations**

The heat flow  $\dot{Q}$  conducted across small temperature differences can be calculated using the formula:

$$\dot{Q} = -KA \frac{dT}{dx} \approx -KA \frac{\Delta T}{L}$$
 Eqn. 1

where K is the thermal conductivity, A is the cross-sectional area,  $\Delta T$  is the temperature difference, and L is the length of the heat conduction path.

Thermal conduction across significant temperature differences should be calculated using thermal conductivity integrals.

Note that the thermal conductivity and the thermal conductivity integral of a material can depend strongly on composition and fabrication history. Without verification, the data in the accompanying figures should be used only for qualitative heat flow calculations.

Calculating the heat conduction through a body with its ends at greatly different temperatures is made difficult by the strong temperature dependence of the thermal conductivity between absolute zero and room temperature. The use of thermal conductivity integrals (called thermal boundary potentials by Garwin) allows the heat flow to be calculated as

$$\dot{Q} = -G(\Theta_2 - \Theta_1)$$
 Eqn. 2

where  $\Theta$  is the integral of the temperature-dependent thermal conductivity, K, calculated as

$$\Theta_1 = \int_0^{T_1} KdT \qquad Eqn.$$

and G is a geometry factor calculated as

$$\frac{1}{G} = \int_{x_1}^{x_2} \frac{dx}{A}$$
 Eqn. 4

where A(x) is the cross sectional area at position x along the path of heat flow. Note that G=A/L in the case of a body of length L and uniform cross-sectional area A.

Equation 1 is only applicable to bodies within which a common thermal conductivity integral function applies.

Reference: R. L. Garwin, Rev. Sci. Instrum. 27 (1956) 826.

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Figure 1 – Thermal Conductivity of Selected Materials

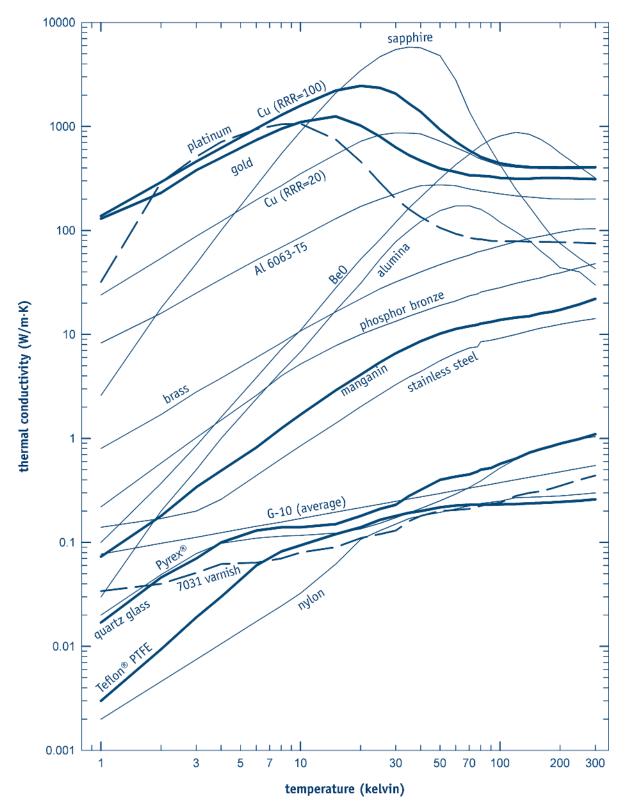
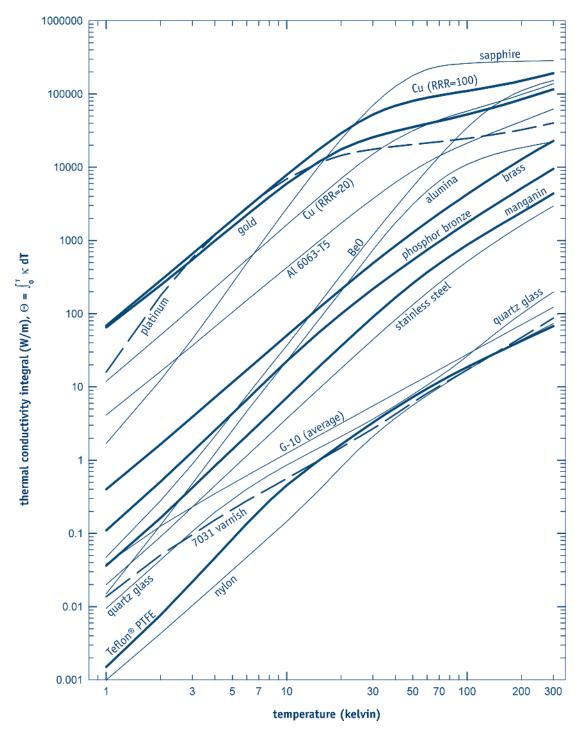


Figure 2 – Thermal Conductivity Integral of Selected Materials



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Table 1 - Thermodynamic Properties for Various Cryogenic Liquids

	Temperatu	Temperature (K)			ssure			Latent Heat of Vaporization	
	Triple point	Normal boiling point	Critical point	Triple point (kPa)	Critical point (kPa)	Critical density (kg/m³)	L (J/g)	Density (g/ml)	
Helium	2.1768ª	4.222	5.1953	5.048	227.46	69.64	20.6	0.13	
Hydrogen	13.8	20.28	32.94	7.042	1283.8	31.36	441	0.07	
Neon	24.5561	27.09	44.44	43.35	2703	483.23	86	1.20	
Nitrogen	63.15	77.36	126.26	12.46	3399	313.11	199	0.81	
Oxygen	54.36	90.19	154.58	0.148	5043	436.14	213	1.14	
Argon	83.8	87.28	150.86	68.9	4906	535.70	162	1.40	
Krypton	115.76	119.77	209.39	73.2	5496	910.75	108	2.40	
Xenon	161.36	165.04	289.74	81.6	5821	1100	96	3.10	
CO <sub>2</sub>	216.58	_	304.21	518.16	7384	466.51	571	1.56	
Methane	90.69	111.63	190.55	11.7	4599	162.65	510	0.42	
Ethane	90.35	184.55	305.33	0.0011	4871	206.73	489	0.55	
Propane	85.47	231.07	369.85	0.1 × 10 <sup>-6</sup>	4248	220.49	425	0.58	
Ammonia	195.49	239.81	406.65	0.0662	11627	237.57	1371	0.68	

<sup>&</sup>lt;sup>a</sup> Triple point values for helium are those of the lambda point

Table 2 - Gamma Radiation-Induced Calibration Offsets as a Function of Temperature for Several Types of Cryogenic Temperature Sensors

		Radiation-induced offset (mK) at temperature				
	Model	4.2 K	20 K	77 K	200 K	300 K
Platinum <sup>b</sup>	PT-103	NA	<b>–15</b>	-10 <sup>d</sup>	10 <sup>d</sup>	10 <sup>d</sup>
Rhodium-iron <sup>b</sup>	RF-100-AA	$2^d$	15 <sup>d</sup>	15 <sup>d</sup>	5 <sup>d</sup>	5 <sup>d</sup>
Cernox™b	CX-1050-SD	-10	-10 <sup>d</sup>	-5 <sup>d</sup>	25 <sup>d</sup>	25 <sup>d</sup>
Carbon-glass <sup>b</sup>	CGR-1-1000	-30	-140	-700	-1300	-3400
Germanium <sup>b</sup>	GR-1400-AA	-5	-20	-25	NA	NA
Ruthenium oxide <sup>b</sup>	R0600	20	150	d	d	NA
GaAlAs diode <sup>b</sup>	TG-120P	-15	-25	2200	2500	400
Silicon diode <sup>b</sup>	DT-470-SD	25	1000	1300	1000	2700
Silicon diode <sup>b</sup>	DT-500P-GR-M	350	50	20	250	300
Silicon diode <sup>b</sup>	SI-410-NN	600	2000	300	450	1400
Platinum <sup>c</sup>	PT-103	NA	<b>–</b> 50	5 <sup>d</sup>	50	75
Rhodium-iron <sup>c</sup>	RF-800-4	5 <sup>d</sup>	15 <sup>d</sup>	25	10 <sup>d</sup>	-15 <sup>d</sup>
Rhodium-iron <sup>c</sup>	RF-100-AA	-5 <sup>d</sup>	-5 <sup>d</sup>	5 <sup>d</sup>	-10 <sup>d</sup>	5 <sup>d</sup>
Carbon-glass <sup>c</sup>	CGR-1-1000	-25	-175	-1400	-4200	-6500
Germanium	GR-1400-AA	<b>2</b> <sup>d</sup>	2 <sup>d</sup>	5 <sup>d</sup>	NA	NA
GaAlAs diodec	TG-120P	-50	<b>-</b> 75	700	600	-250
Silicon diode <sup>c</sup>	DT-470-SD	+20	-200	1500	11000	18000
Silicon diodec	DT-500P-GR-M	10 <sup>d</sup>	10 <sup>d</sup>	-5 <sup>d</sup>	-5 <sup>d</sup>	-100

<sup>&</sup>lt;sup>b</sup> Sensors were irradiated in situ at 4.2 K with a cobalt-60 gamma source at a dose rate of 3,000 Gy/hr to a total dose of 10,000 Gy (1  $\times$  10 $^6$  rad)

<sup>&</sup>lt;sup>c</sup> Sensors were irradiated at room temperature with a cesium-137 gamma source at a dose of 30 Gy/hr to a total dose of 10,000 Gy (1  $\times$  10 $^6$  rad)

<sup>&</sup>lt;sup>d</sup> Deviations smaller than calibration uncertainty

Table 3 - Vapor Pressure of Some Gases at Selected Temperatures in Pascals (Torr)

	4 K	20 K	77 K	150 K	Triple <sup>e</sup> Point Temperature
Water	f	f	f	$1.33 \times 10^{-4}  (10^{-7})$	273 K
Carbon dioxide	f	f	$1.33 \times 10^{-5} (10^{-8})$	1333 (10)	217 K
Argon	f	$1.33 \times 10^{-10}  (10^{-13})$	21332 (160)	h	84 K
Oxygen	f	$1.33 \times 10^{-10}  (10^{-13})$	19998 (150)	h	54 K
Nitrogen	f	$1.33 \times 10^{-8}  (10^{-11})$	97325 (730)	g	63 K
Neon	f	4000 (30)	g	g	25 K
Hydrogen	$1.33 \times 10^{-4}  (10^{-7})$	101,325 (760)	g	g	14 K

Note: estimates – useful for comparison purposes only (1 Torr = 133.3 Pa)

Table 4 – Thermal Contraction of Selected Materials Between 293 K and 4 K

Material	Contraction (per 10 <sup>4</sup> )
Teflon®	214
Nylon	139
Stycast® 1266	115
SP22 Vespel®	63.3
Stycast® 2850FT	50.8
Stycast® 2850GT	45
Al	41.4
Brass (65% Cu/35% Zn)	38.4
Cu	32.6
Stainless steel	30
Quartz a-axis	25
Quartz c-axis	10
Quartz mean, for typical transducer	15
Titanium	15.1
Ge	9.3
Pyrex®	5.6
Si	2.2

Table 5 – Electrical Resistivity of Alloys (in  $\mu\Omega \cdot cm$ )

Material	Resistivity (295 K)	(4.2 K)
Brass	7.2	4.3
Constantan	52.5	44
CuNi (80% Cu/20% Ni)	26	23
Evanohm®	134	133
Manganin	48	43
Stainless steel	71 to 74	49 to 51

<sup>&</sup>lt;sup>e</sup> Solid and vapor only at equilibrium below this temperature; no liquid

f Less than 10<sup>-13</sup> Torr

<sup>&</sup>lt;sup>g</sup> Greater than 1 atm

<sup>&</sup>lt;sup>h</sup> Above the critical temperature, liquid does not exist

Table 6 - Defining Fixed Points of the ITS-90

Temperature (T <sub>90</sub> /K)	Substance <sup>i</sup>	State <sup>/</sup>		Defining l	Instrument	
0.65 to 3			He vapor pressure			
3 to 5	He	V	thermometer			
13.8033	e-He <sub>2</sub>	T		Constant volume gas thermometer		
~17	e-He <sub>2</sub> (or He)	V (or G)				
~20.3	e-He <sub>2</sub> (or He)	V (or G)				
24.5561	Ne	T				
54.3584	02	T				
83.8058	Ar	T			Platinum	
234.3156	Hg	T			resistance	
273.16	H <sub>2</sub> 0	T			thermometer	
302.9146	Ga	M				
429.7485	ln	F				
505.078	Sn	F				
692.677	Zn	F				
933.473	Al	F				
1234.93	Ag	F				
1337.33	Au	F				Radiation
1357.77	Cu	F				

<sup>&</sup>lt;sup>i</sup> All substances except 3He are of natural isotopic composition;

Table 7 - Saturated Vapor Pressure of Helium

T (K)	P (Pa)
5.1	211600
5	196000
4.9	181000
4.8	167000
4.7	154300
4.6	141900
4.5	130300
4.4	119300
4.3	108900
4.2	99230
4.1	90140
4	81620
3.9	73660
3.8	66250
3.7	59350
3.6	52960
3.5	47040

T (K)	P (Pa)
3.4	41590
3.3	36590
3.2	32010
3.1	27840
3	24050
2.9	20630
2.8	17550
2.7	14810
2.6	12370
2.5	10230
2.4	8354
2.3	6730
2.2	5335
2.1	4141
2	3129
1.9	2299
1.8	1638

28 6.4 1.5
1.5
2.0
7.9
0.7
7.3
.42
.58
.45
.68
.98
.07
.67
.57

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e-H<sub>2</sub> is hydrogen at the equilibrium concentration of the ortho- and para-molecular forms

For complete definitions and advice on the realization of these various states, see "Supplementary Information for the ITS-90"; the symbols have the following meanings: V - Vapor pressure point; T - Triple point; G - Gas thermometer point; M - Melting point; F - Freezing point