



Experiment to measure the Pockels effect from an HR AlGaAs coating (update)

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Pockels Effect (quick summary)

- Same physics used in electro-optic modulators (dn/dE)
- For AlGaAs HR coating (grown along [001] crystallographic direction):

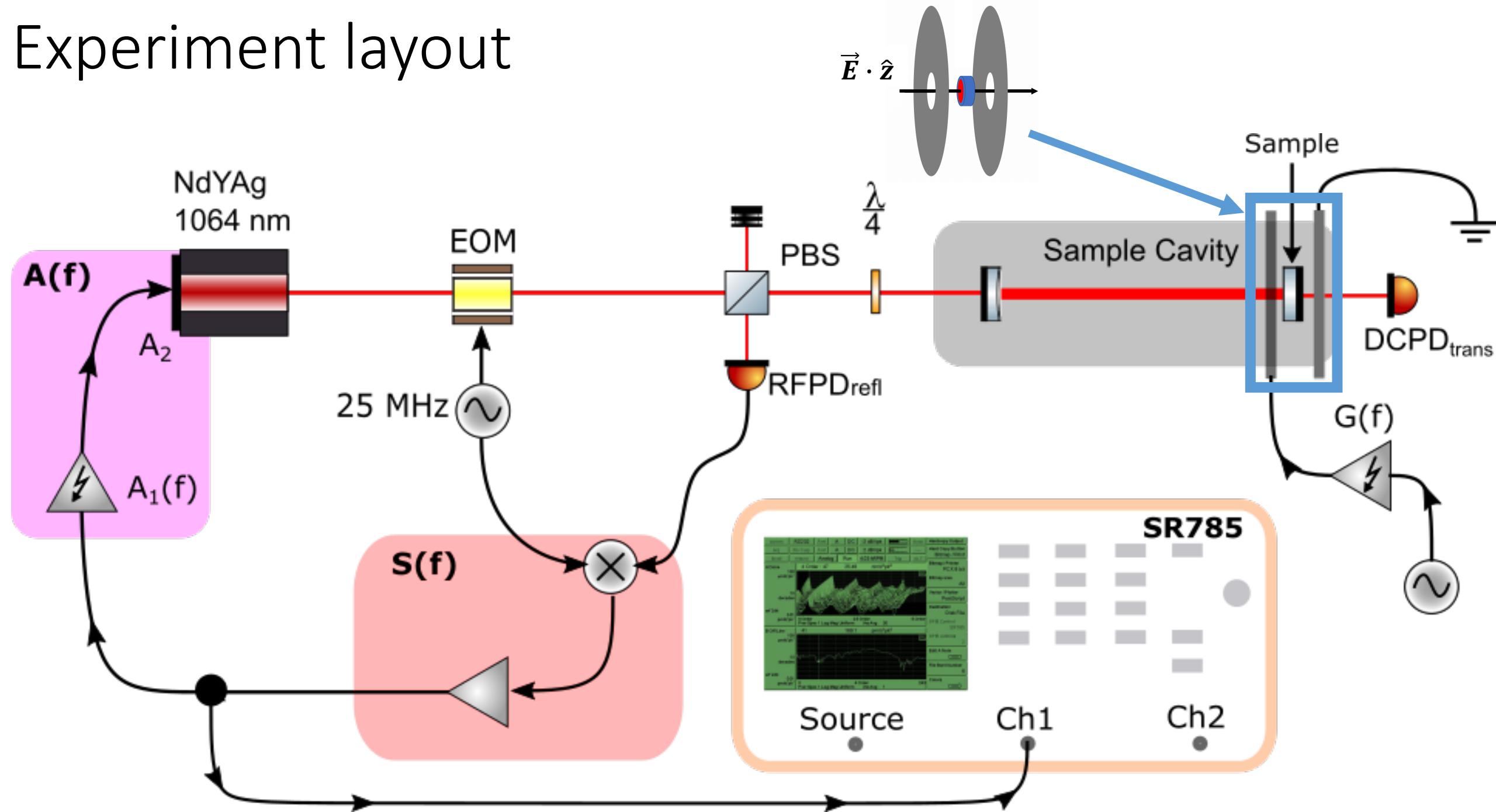
$$\left| \frac{\partial \phi}{\partial E_z} \right| = \pi \frac{r_{41}}{2} (n_2 n_3^2 + n_3 n_2^2) + \frac{n_2/n_3}{1 - \left(\frac{n_2}{n_3} \right)^2}$$

Where r_{41} (-1.2e-12 [m/V]) is the electro-optic coefficient and n_2 (3.0087) and n_3 (3.4426) are low and high index layers of the HR coating respectively

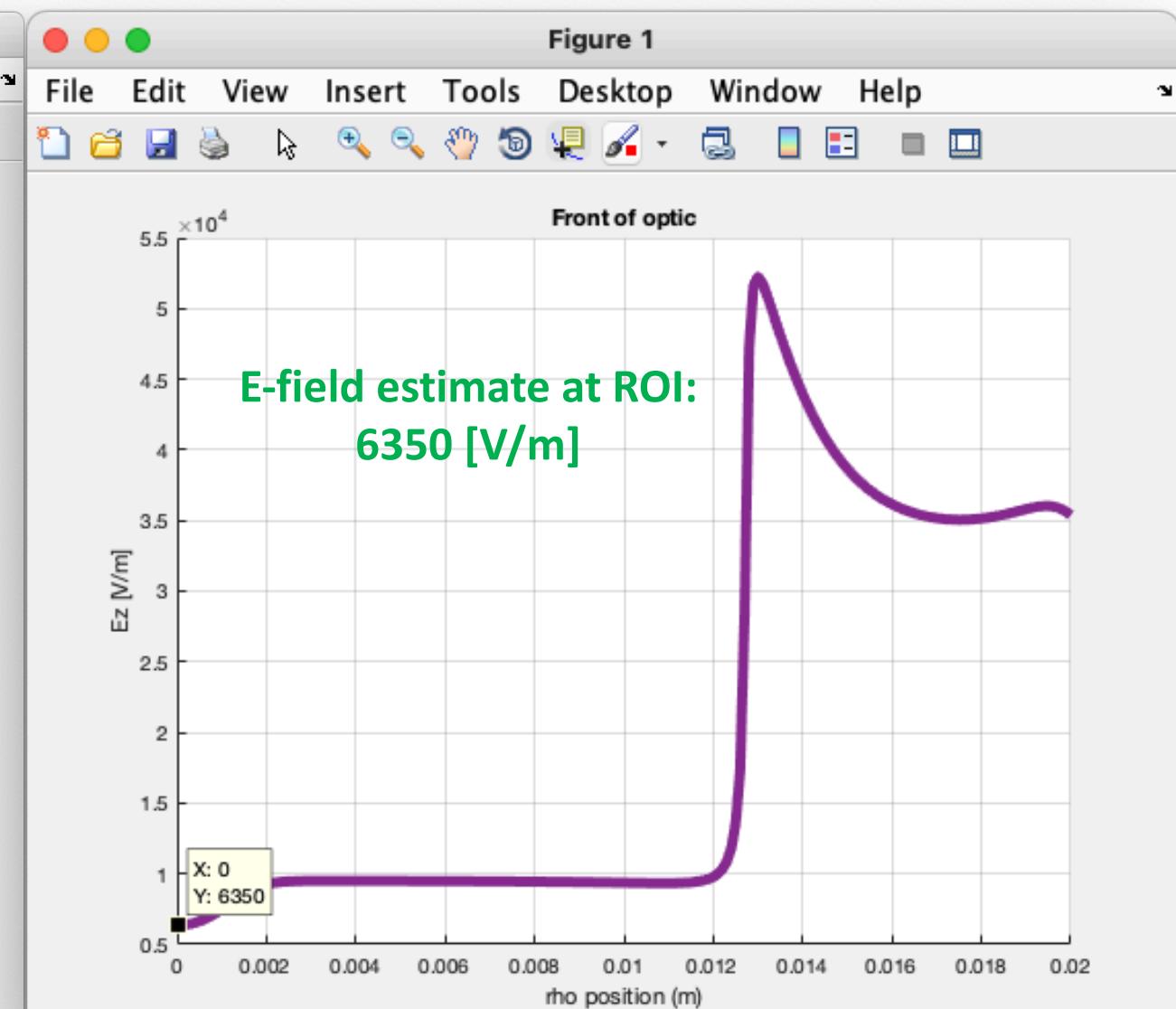
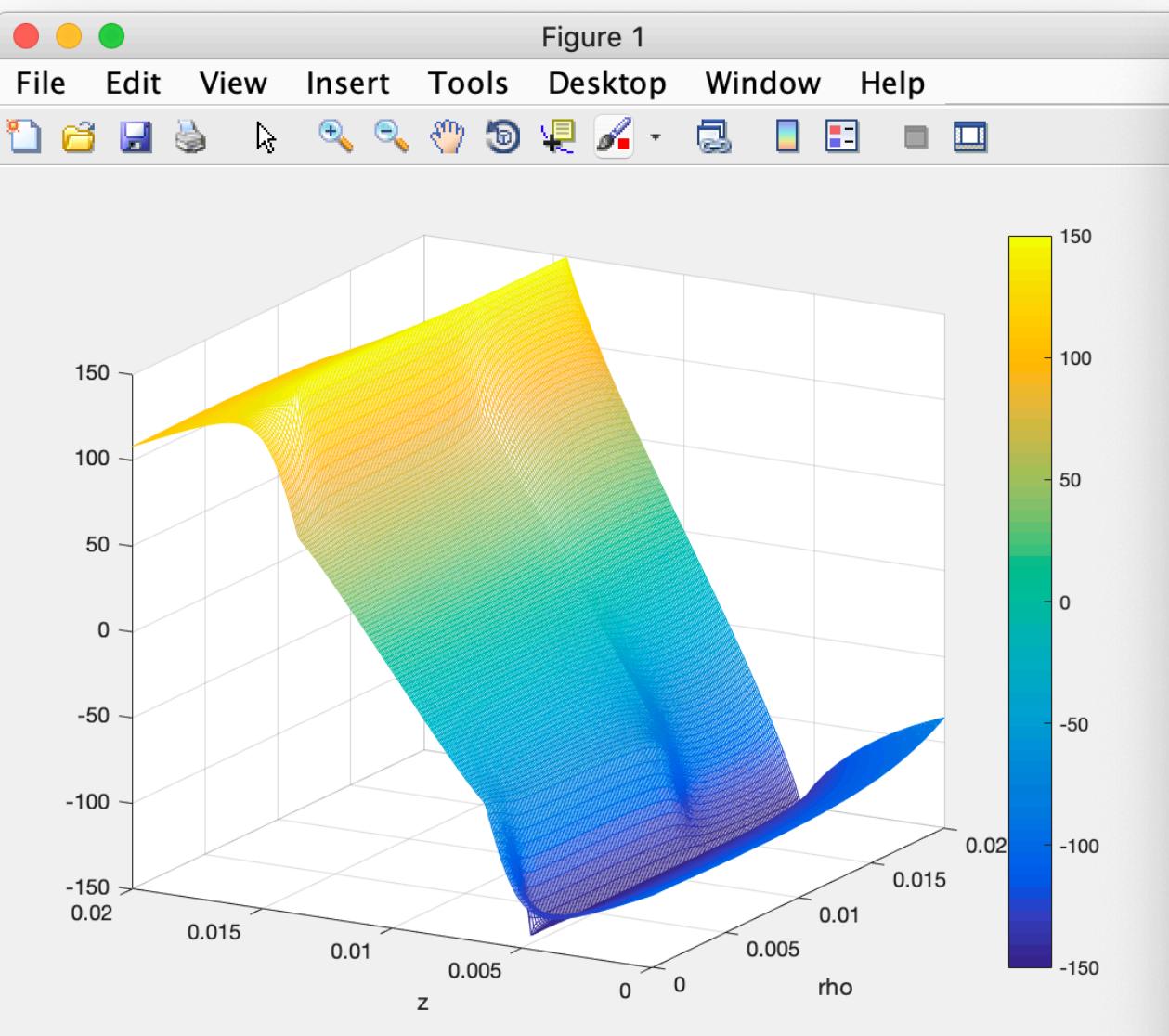
- And for $\lambda = 1064nm$ in reflection:

$$\left| \frac{\partial x}{\partial E_z} \right| = 3.8 * 10^{-17} [\text{m/V/m}]$$

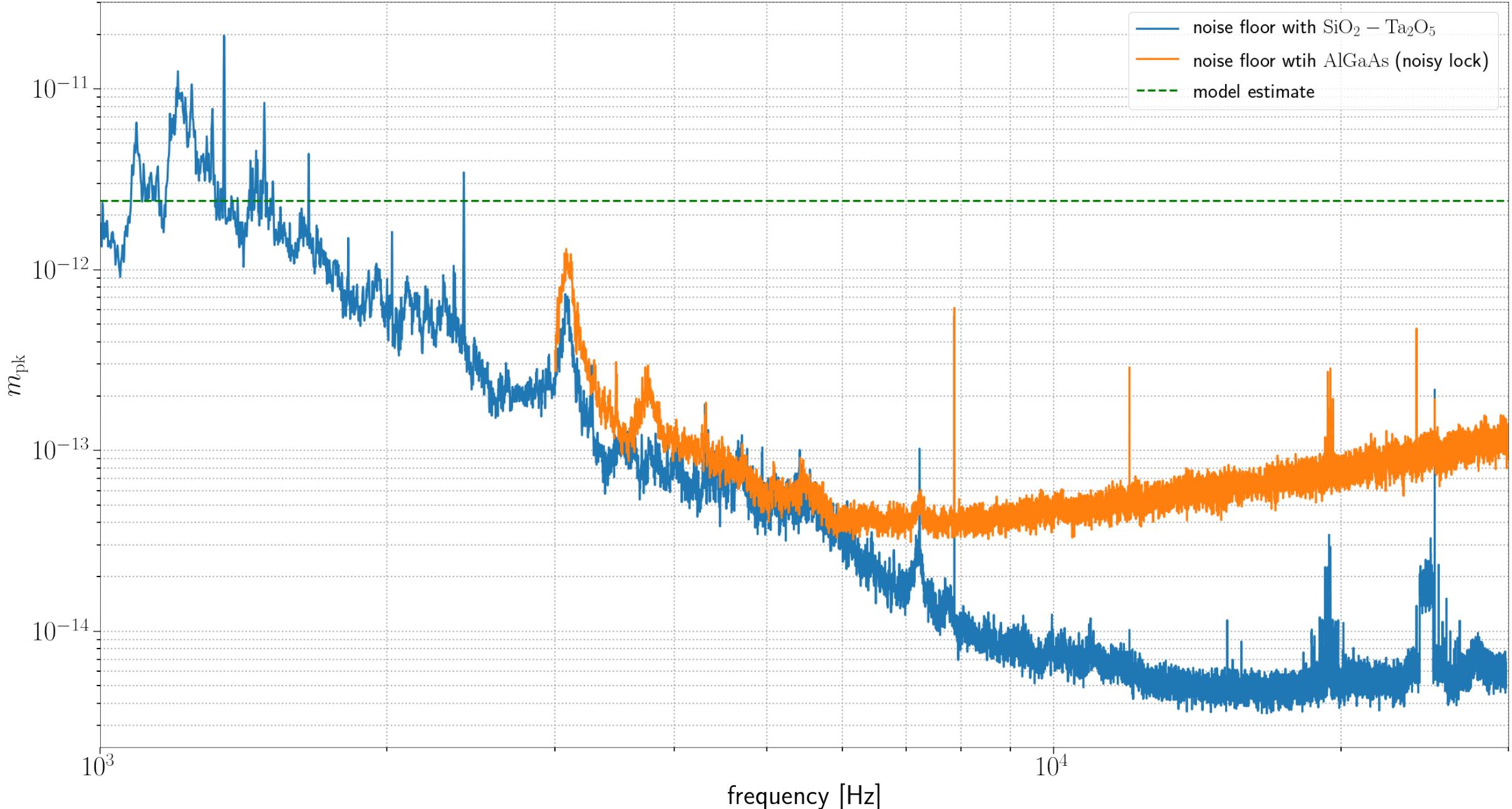
Experiment layout



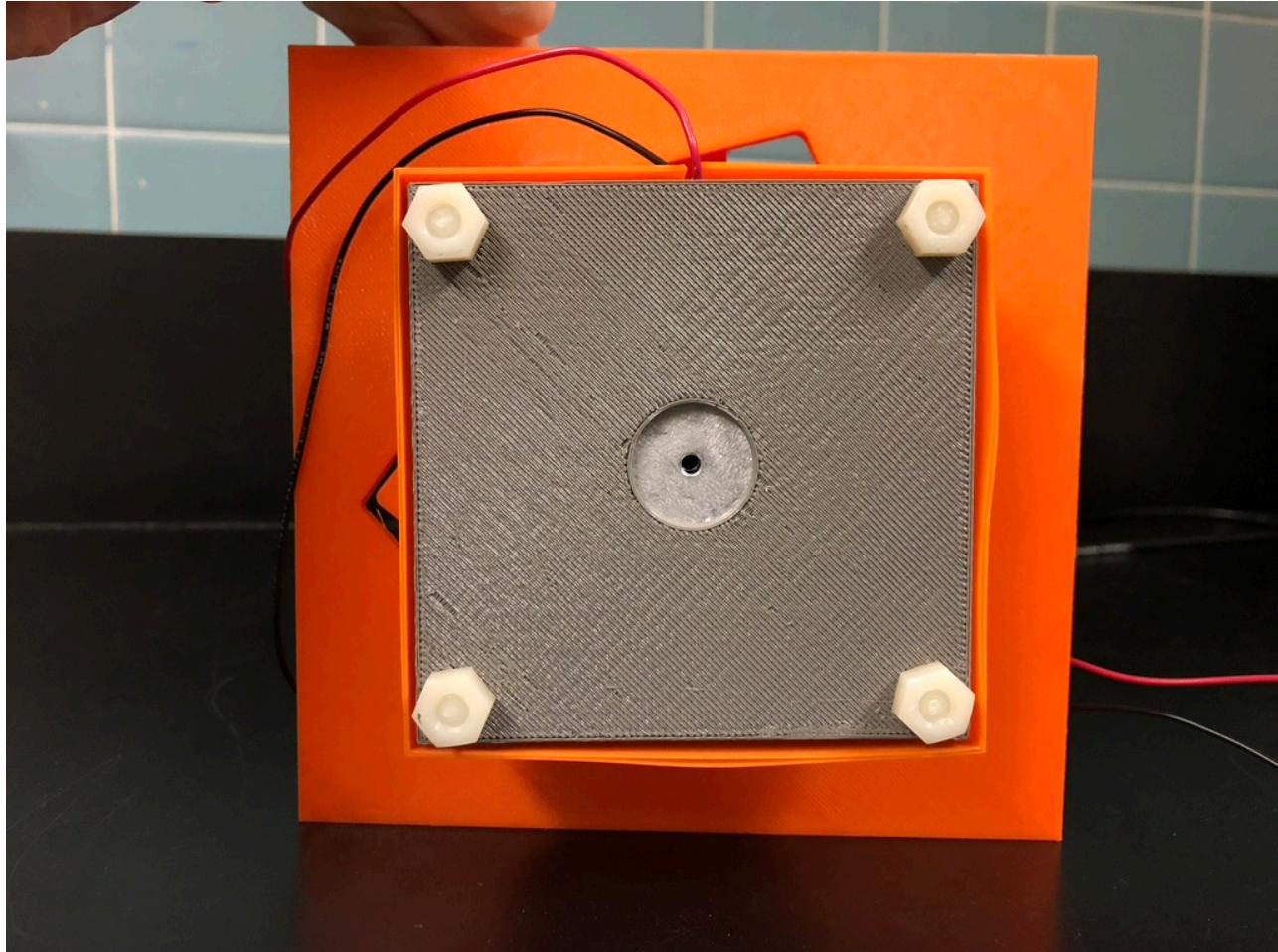
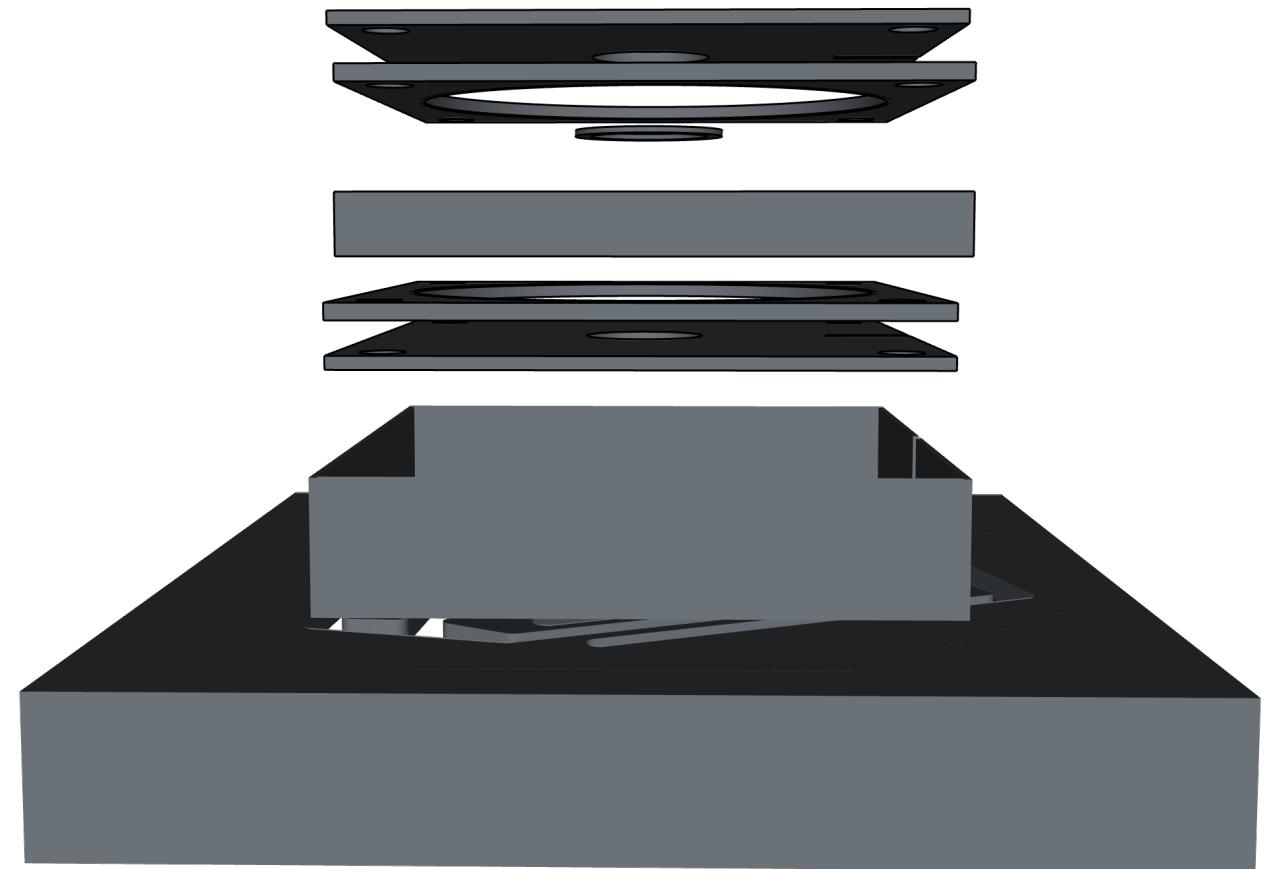
Electric field estimate within coating



Measurable using in-air cavity



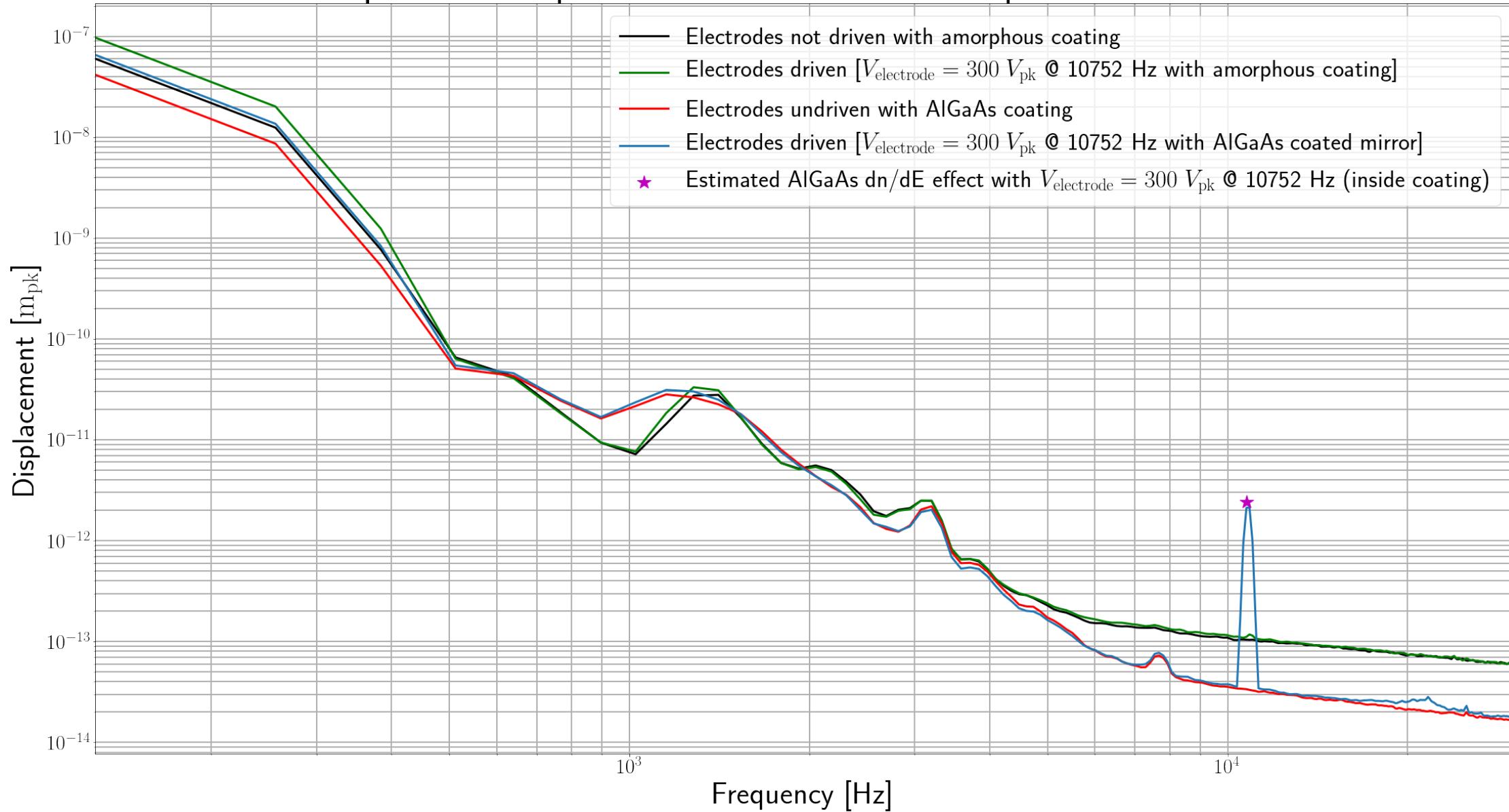
3D printed optical mount



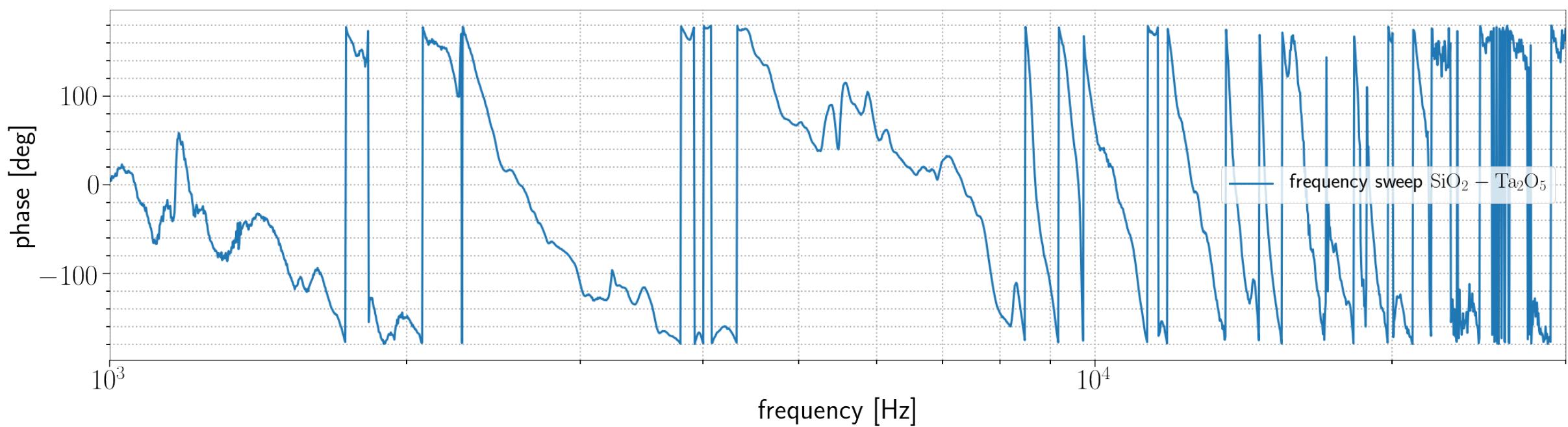
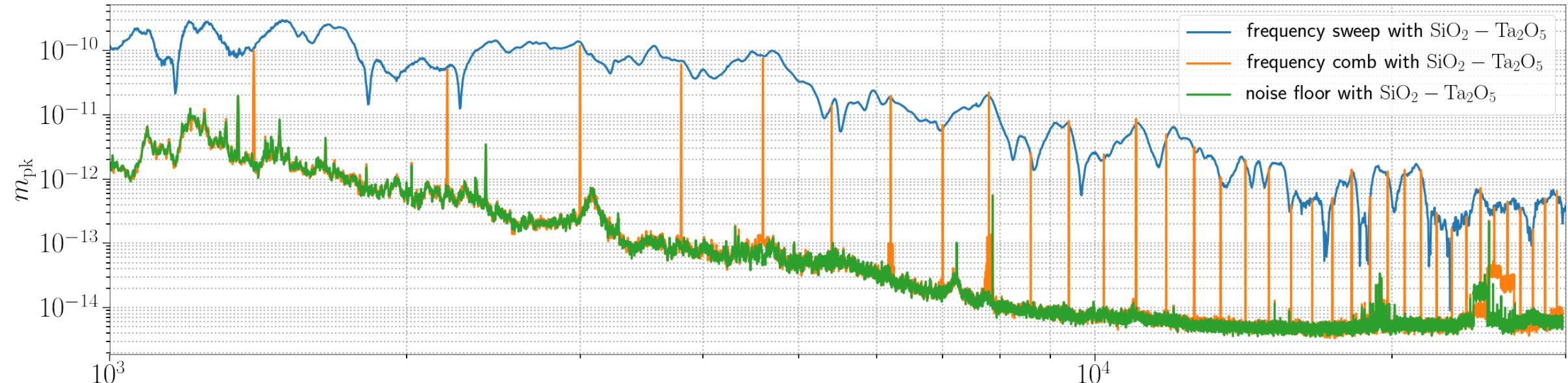
Ortho-planar spring design for pitch and yaw control

Previously reported single frequency drive results

Displacement spectra for AlGaAs Electro-optic measurement



Frequency sweep test ($\text{SiO}_2\text{-Ta}_2\text{O}_5$ sample mirror)



Next Steps

- Further investigation as to why we see the drive coupling into the PDH error signal for $\text{SiO}_2/\text{Ta}_2\text{O}_5$ sample
 - Potential mechanical instability of 3D printed mount
 - Electronics crosstalk
- Once aforementioned coupling is addressed, attempt to measure Pockels effect with AlGaAs sample
- Investment in calibration sample
- Measure effect with separate individual polarizations

Refrences

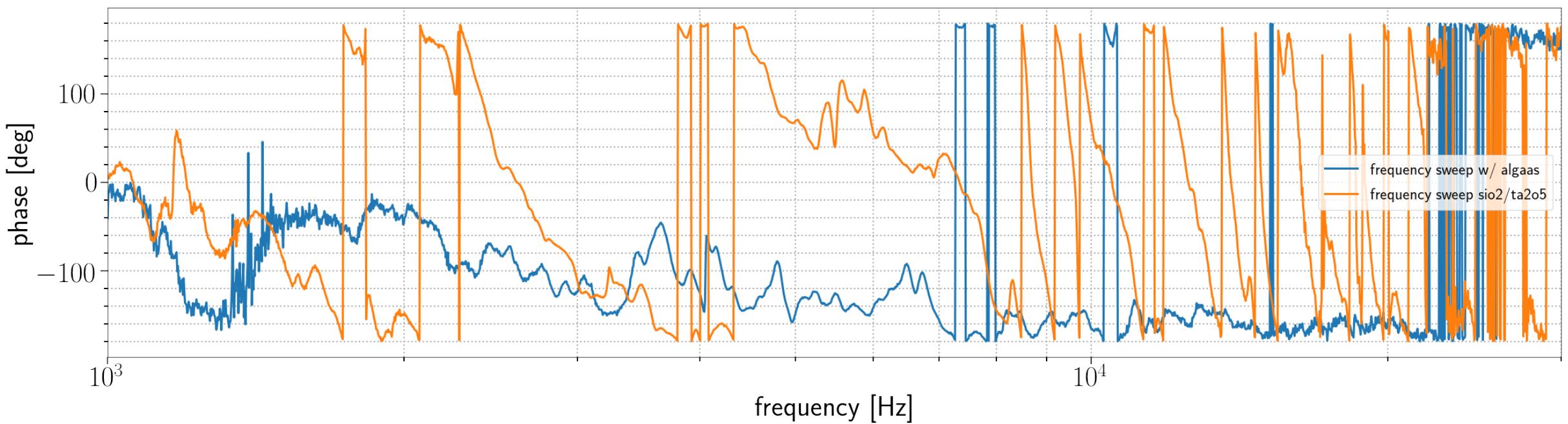
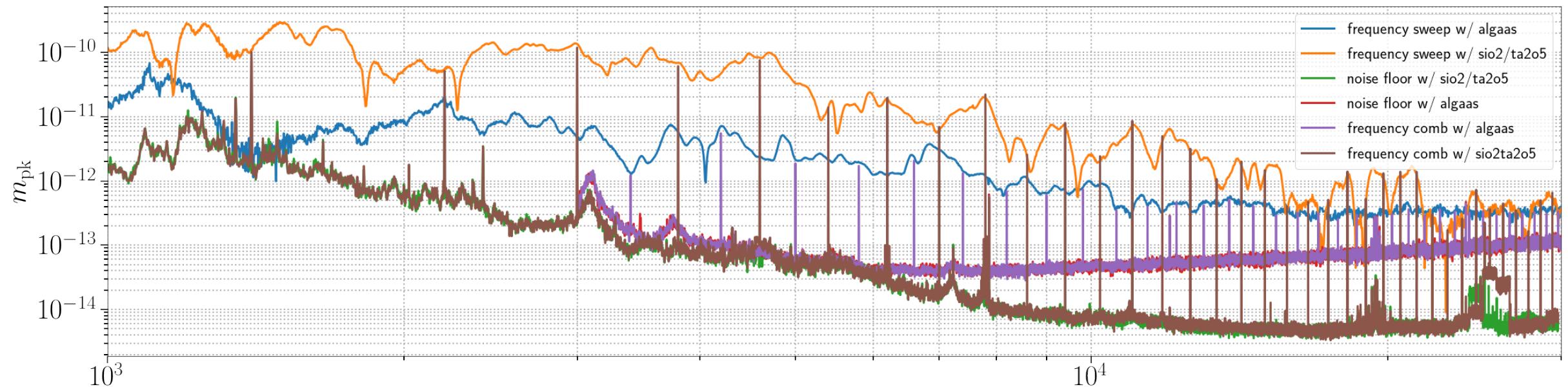
- Fejer, M.M. , *Electro-optic Effects in AlGaAs mirrors* , (2018)
- Yariv, A., 1988, *Quantum electronics*, 3rd edn, (John Wiley & Sons)
- BYU CMR, *Ortho-planar spring design* :
<https://www.thingiverse.com/thing:3007261>

Thank you!

Questions? Suggestions?

EXTRA SLIDES

Frequency sweep test (both sample mirrors)



Calibration

This frequency response measurement records the following ratio in dB of the following:

$$\alpha(f) = \frac{CH2(f)}{Source} \quad (1)$$

We also know that the error signal spectra of the loop is probed by $CH2(f)$:

$$CH2(f) = \frac{S(f) * (\text{signal } [V])}{(1 - OLG(f))} \quad (2)$$

Where (*signal* [V]) is the uncalibrated voltage output from the mixer, $S(f)$ is the FSS transfer function, and $OLG(f)$ is the open loop gain of the PDH system.

Calibration (cont.)

And we know $OLG(f) = S(f) * A_1(f) * A_2$ so :

$$(signal [m]) = CH2(f) * A_1(f) * A_2 * \frac{1 - OLG(f)}{OLG(f)} * \frac{L_{cav}}{f_{laser}} \quad (4)$$

Where $A_1(f), A_2$ are a high voltage amplifier response and measured response of the laser piezo respectively. L_{cav} is the sample cavity length, f_{laser} is the laser frequency.
 $(signal [m])$ is the effective cavity length change from the Pockels effect.

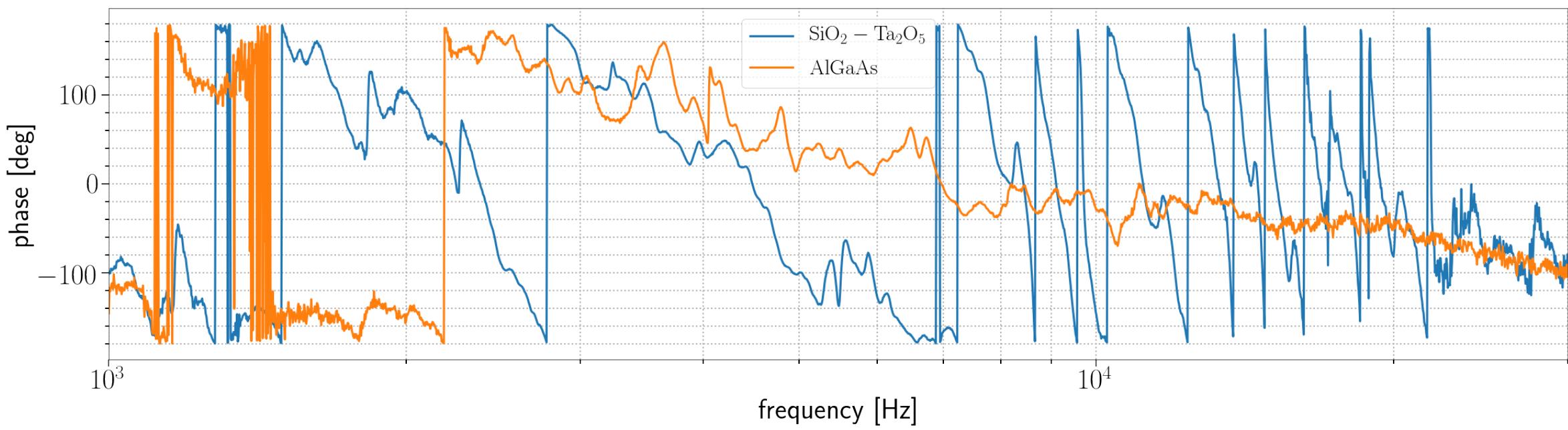
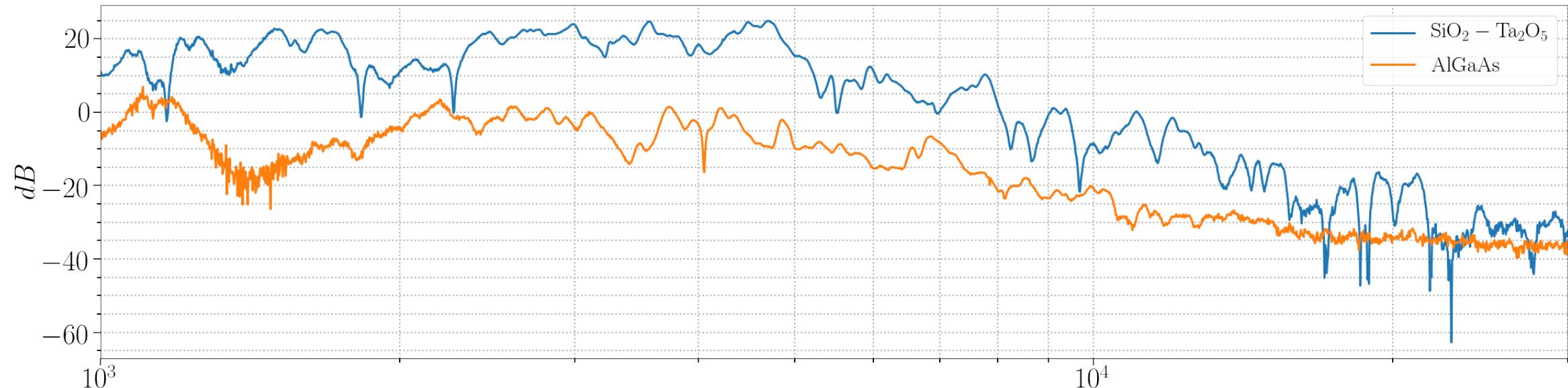
Substitute (1) into (4):

$$(signal [m]) = Source * \alpha(f) * A_1(f) * A_2 * \frac{1 - OLG(f)}{OLG(f)} * \frac{L_{cav}}{f_{laser}} \quad (5)$$

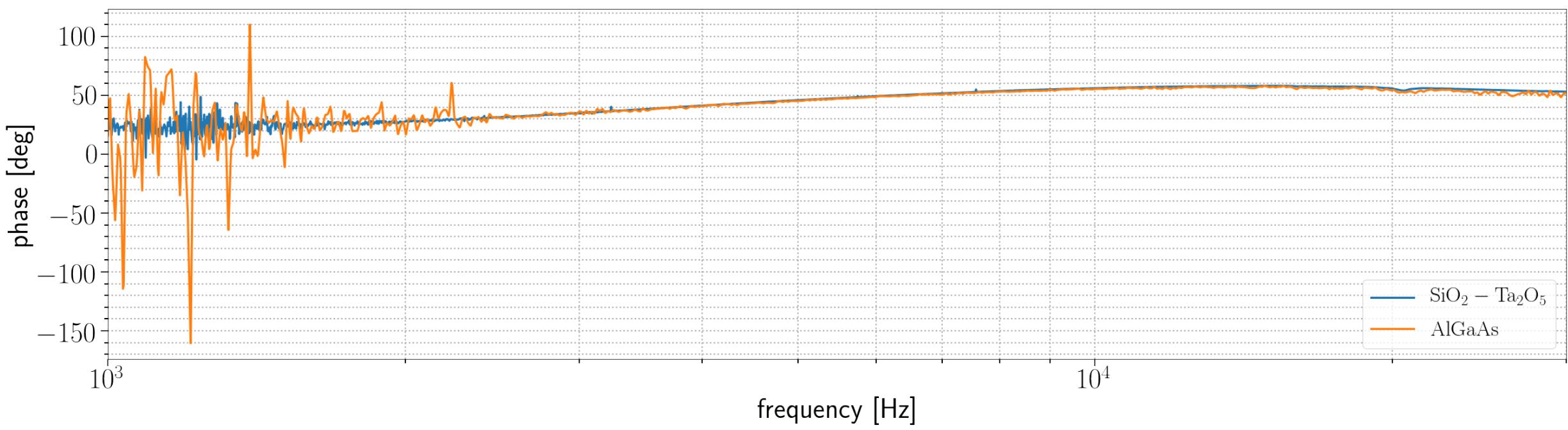
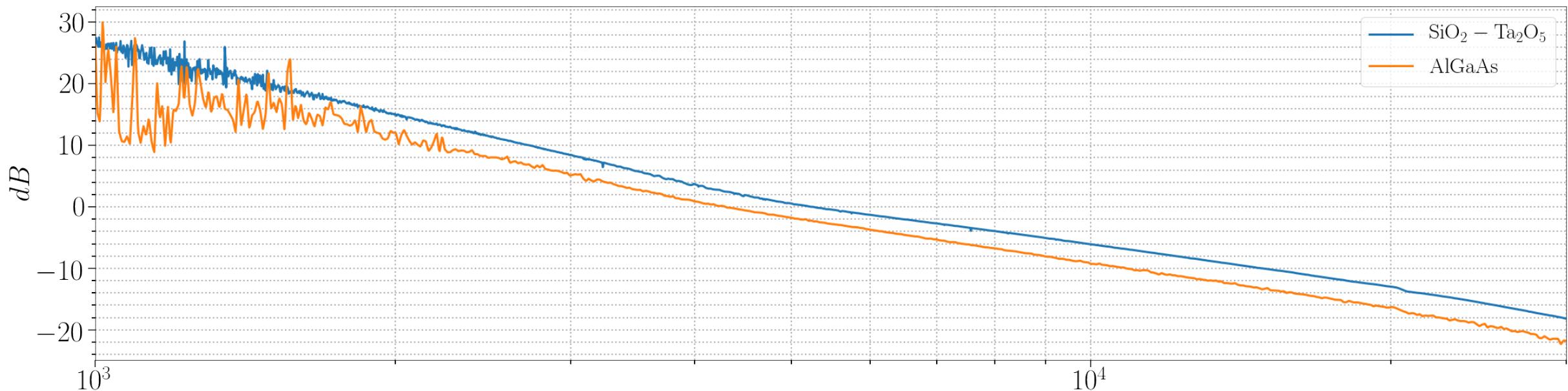
Measured : $Source, \alpha(f), OLG(f), A_1(f), A_2, \text{ and } L_{cav}$

$Source = 5 V_{pk}$ and $L_{cav} = .165 \text{ m}$, $f_{laser} = 2.8\text{e}14 \text{ Hz}$

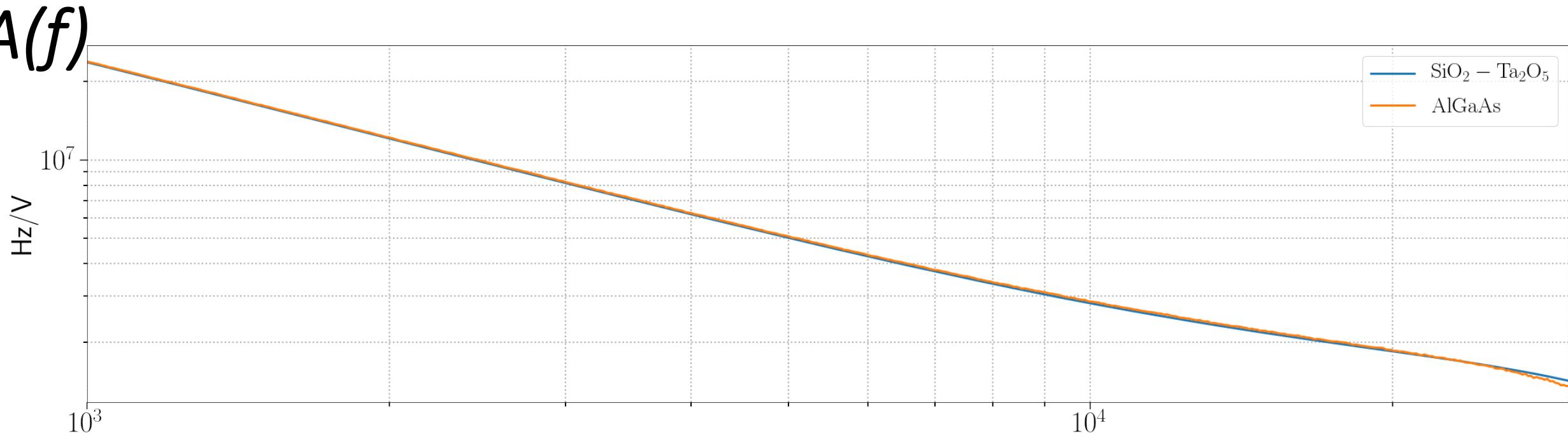
$\alpha(f)$



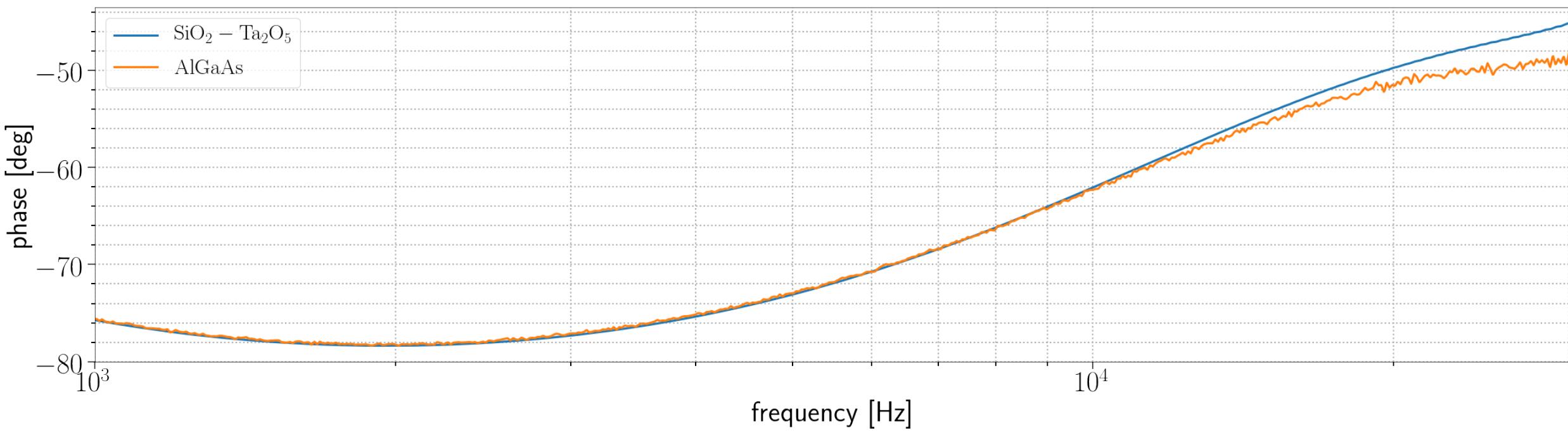
OLG



$A(f)$



phase [deg]



Voltage on front electrode plate (swept frequency measurement)

