Obsvd. $t_g$	$v_1$ (i.e., $1/t_g$ )	Obsvd. $t_F$	$v_2$ (i.e., $1/t_F$ )	$(v_2'-v_2)$	$\sqrt{v_1}(v_2'-v_2)$
7.2 sec	0.1389	2.1 sec	0.4762	0.1984	0.0739
		3.6	0.2778	0.1978	0.0737
		12.5	0.0800		
$5.8  \sec$	0.1724	1.9	0.5263	0.3792	0.1575
		6.8	0.1471	0.8529	0.3541
		1.0	1.000	0.7059	0.2931
		3.4	0.2941		

## TABLE VII

n	$4.917 \times n$	Observed Charge	n	$4.917 \times n$	Observed Charge
1	4.917		10	49.17	49.41
2	9.834		11	54.09	53.91
3	14.75		12	59.00	59.12
4	19.66	19.66	13	63.92	63.68
5	24.59	24.60	14	68.84	68.65
6	29.50	29.62	15	73.75	• • • •
7	34.42	34.47	16	78.67	78.34
8	39.34	39.38	17	83.59	83.22
9	44.25	44.42	18	88.51	

	d = 0.5cm		d = 0.5cm	Charge on ion			Frictional charge		
$t_g$	$ \begin{array}{c c} v_1(=d/t_g) \\ \text{(cm/sec)} \end{array} $	$t_F$	$v_2(=d/t_F)$ (cm/sec)	$(v_2'\!-\!v_2)$	n'	$\frac{v_2' - v_2}{n'}$	$v_1 + v_2$	n	$\frac{v_1+v_2}{n}$
18.2	.00286	3.8	.01316				.01602	3	.00534
18.6	avr			.00470	1	.00470			
19.2		2.8	.01786						
18.0				.01561	3	.00520			
17.2		22.2	.00225						
15.4				.00544	1	.00544			
16.7		6.5	.00769						
18.0				.00541	1	.00541			
15.4		21.9	.00228						
17.3				.01123	2	.00562			
18.4		3.7	.01351						
17.5						.00527			.00534
avr						avr			

TABLE  $VI^a$ 

$ \begin{array}{ c c c c c c }\hline t_g\\ Sec. & & t_F\\ Sec. & t_F\\ $									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			$\frac{1}{t_F}$	$\frac{1}{t_F'} - \frac{1}{t_F}$	n'	$\frac{1}{n'} \big( \frac{1}{t_F'} - \frac{1}{t_F} \big)$	$\frac{1}{t_g} + \frac{1}{t_F}$	n	$\frac{1}{n}(\frac{1}{t_g} + \frac{1}{t_F})$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.848	80.708	.01236				.09655	18	.005366
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			}	.03234	6	.005390			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.908	22.390 }	.04470 {				.12887	24	.005371
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.904	22.368	}	.03751	7	.005358			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.882	140.565	.007192				.09138	17	.005375
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			}	.005348	1	.005348			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.906	79.600	.01254 {				.09673	18	.005374
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			}	.01616	3	.005387			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			.02870				.11289	21	.005376
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.840	29.286							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		}	.03414				.11833	22	.005379
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			}	.026872	5	.005375			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.870	137.308	.007268 {		ı				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			}	.021572					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		34.638	.02884 {	04.000	ı				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		22.10.1	}	.01623					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.846	22.104	0.4505						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.010	00.000	.04507 {	0.4007	ı				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			000000	.04307					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			.002000{	0.4070	ı				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.918	19.704	05070	.04879					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 070	10 669	.05079						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.870	19.008 /	\	03874	ı				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 888	77.630		.03014	I				
$ \begin{array}{c ccccc} 11.894 & 77.806 \\ 11.878 & 42.302 & .02364 \end{array} \right\} \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.000	11.050	01285						
11.878 42.302 .02364	11 894	77.806	.01200	01079	I				
			.02364	.01010	I				
LL XXII I	11.880	12.002	.02001	<u> </u>					

Duration of exp.	=45  min.	Pressure	= 75.62  cm.			
Plate distance	= 16  mm.	Oil density	= .9199			
Fall distance	= 10.21  mm.	Air viscosity	$=1,824 \times 10^{-7}$ [poise]			
Initial volts	= 5,088.8	Radius $(a)$	= .000276 cm.			
Final volts	= 5,081.2	$\frac{l}{a}$ [mean free path $\div a$ ]	= .034			
Temperature	= 22.82°C.	Speed of fall	= .08584 cm./sec.			
$e_i = 4.991 \times 10^{-10} \text{ [statcoulomb]}^b$						

 $<sup>^</sup>a[$  The bracketed numbers are our corrections of errors in the original paper.]  $^b[$  The value presently accepted is  $4.802\times10^{-10}$  stateoulombs.]

1	2 , 3	4
5	$6 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	8
9	10 11	12
1	2 3	4
5	6 > 7	8
9	10 / 11	12

- First line
- Second line
- Third line, which is quite long and seemingly tedious in the extreme
- Fourth line, which isn't as long as the third
- Fifth line

$$P(\boldsymbol{a}, \boldsymbol{b}) = \int d\lambda \, \rho(\lambda) A(\boldsymbol{a}, \lambda) B(\boldsymbol{b}, \lambda).^{1}$$
 (1)

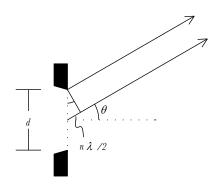
<sup>&</sup>lt;sup>1</sup>[According to the hypothesis Bell is investigating, the "more complete specification" of the particles' state, the extra information that would tell the observer who knew it which way the particle would respond to a given measurement, is given by  $\lambda$ . Equation (2) considers all the possible  $\lambda$ 's and weights them according to how likely each is. Mathematically, that means integrating over all the possible values of  $\lambda$  and weighting each by its likelihood, represented by the probability distribution  $\rho(\lambda)$ . It may be helpful to note that P was likely chosen to stand for "product," since the term we are integrating  $\rho$  against is the product of A and B. Because we've defined A and B such that the results of measurements yield the values +1and -1, the product for any given value of  $\lambda$  will always be either +1 (meaning that the two particles would both be measured to be pointing either in the selected directions  $\boldsymbol{a}$  and  $\boldsymbol{b}$  or in directions opposed to them) or -1 (meaning that the directions of  $\sigma_1$  and  $\sigma_2$  would be measured to be opposed, whether because  $\sigma_1$  would not be measured to point in direction aand  $\sigma_2$  would be measured to point in direction **b** or because  $\sigma_1$  would be measured to point in direction a and  $\sigma_2$  would not be measured to point in direction b. Since it is weighted sum of all the positive and negative terms,  $P(\boldsymbol{a},\boldsymbol{b})$  is thus a measure of the correlation between the spin-direction of the two particles relative to the angles  $\boldsymbol{a}$  and  $\boldsymbol{b}$ .

## Note

## Single-slit Diffraction and the Limit of Optical Resolution

1. Single-slit diffraction. Let there be a narrow slit of width d, illuminated uniformly along the axis perpendicular to the plane of the slit. As in Huygens' treatment, consider the plane of the slit to be populated by infinitely many centers of wavelets, expanding in all forward directions. Thus the light beam will spread out as it leaves the slit.

There will be some angle, say  $\theta$ , at which the wavelets that were emitted from *one edge* of the slit and from the *center* of the slit, respectively, will cover distances that differ by an integral num-

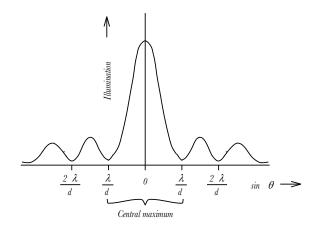


ber of half-wavelengths and arrive together at some distant point—where they will mutually cancel, being exactly out of phase with one another. The innumerable remaining wavelets may be similarly paired for mutual cancellation; so that the overall result will be a dark spot at angle  $\theta$  from the perpendicular axis.

In the right triangle thus formed with hypotenuse d/2 and one leg an integral multiple of  $\lambda/2$ , the marked angle will be equal to  $\theta$  and will have sine given by

$$\sin \theta = \frac{n\lambda/2}{d/2} = \frac{n\lambda}{d}.$$

Since n is any integer, there will be alternating bands of illumination and darkness for all angles up to  $90^{\circ}$  on either side of the perpendicular axis. But in practice the greatest illumination



is found within the "central maximum," that region bounded by the two minima for which n=1 (called "first-order" minima). Suppose these minima appear at angles  $\theta_1$  on either side of the axis. Then  $\theta_1$  will be the angular half-width of the central maximum, and will be given by

$$\sin \theta_1 = \frac{\lambda}{d}.$$

2. Optical resolution.<sup>2</sup> Consider points  $P_1$  and  $P_2$  on the surface of some object. Let their angular separation be  $\beta$ , and let it be supposed that both points emit or reflect light of wavelength  $\lambda$ . For the sake of simplicity, we will let the aperture through which light is admitted to the instrument be a slit of width a (a circular aperture can be analogously treated, but numerous complications arise for that case). Light from each point forms its own independent diffraction pattern with a central maximum flanked by pairs of minima. As shown in the previous section 1, each central maximum will have an angular half-width equal to  $\theta_1$  such that

$$\sin \theta_1 = \lambda/a$$
.

Now the central maxima of the two patterns lie in the focal plane of the instrument lens and (since rays passing through the center of a lens are not bent) must be separated from one another by the angle  $\beta$ . But as aperture a is made smaller, the angular half-width of each central maximum increases, until eventually  $\theta_1 = \beta$ —that is, the central maximum of each pattern coincides with a first-order minimum of the other pattern. The central bright maxima will then be immediately adjacent to one another. Inspection of the sum of the two intensity graphs under these conditions shows that instead of forming two distinct bands, the central maxima will merge into a *single band*.

Someone viewing such an image through the instrument would be quite unable to distinguish either of these maxima from the other; and thus the points P1 and P2 would become *indistinguishable*. No increase of magnifying power, so long as the same aperture width is retained, can remedy this limitation. However, if the aperture width a is increased even the slightest amount, so that the separation between the two patterns increases by any degree at all, there will be found a dip between the two maxima when the sum of the intensity graphs is plotted as before. Thus, that the central maximum of each pattern shall coincide with the first-order minimum of the other is a *limiting condition* for the resolution of the images of two points; it is called *Rayleigh's criterion*.

Heisenberg's equation (16) derives directly from Rayleigh's criterion. For suppose  $\theta_1 = \beta$  as described above; that is, let

$$\sin \beta = \lambda/a. \tag{2}$$

Let the object distance be R, and suppose also that angle  $\beta$  is very small. Then  $\Delta x$  is the chord of a circle with center at the vertex of  $\beta$ , and so it very nearly equals the arc which it subtends. This small arc equals  $R\beta$  (radians); while in its turn a very small angle  $\beta$  (in radians) nearly equals  $\sin \beta$ . This gives  $\Delta x \approx R \times \sin \beta$ , so that

$$\sin \beta \approx \Delta x/R. \tag{3}$$

From equations (1) and (2) it follows that

$$\frac{\Delta x}{R} = \frac{\lambda}{a}.\tag{4}$$

<sup>&</sup>lt;sup>2</sup>After Curtis Wilson, c. 1980.

Similarly, the aperture of width a located at distance R from a point will subtend an angle  $\varepsilon$  such that, if  $\varepsilon$  is very small,

$$\sin \varepsilon \approx a/R$$
,

from which

$$a \approx R \sin \varepsilon.$$
 (5)

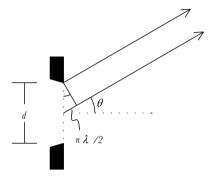
Substitution of equation (4) into equation (3) above yields

$$\frac{\Delta x}{R} \approx \frac{\lambda}{R \sin \varepsilon}$$

which becomes Heisenberg's equation (16), when R is canceled from both sides. Q.E.D.

## SINGLE-SLIT DIFFRACTION AND LIMIT OF OPTICAL RESOLUTION

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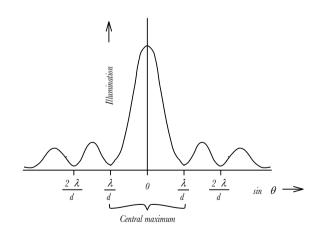


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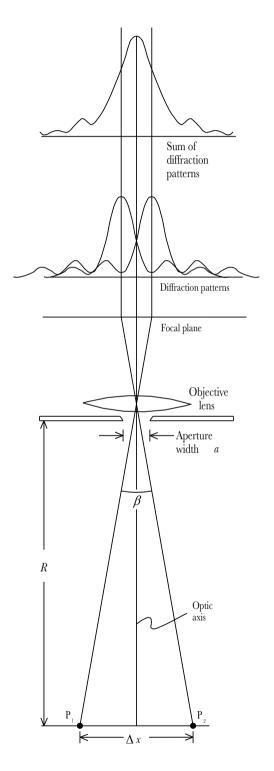
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