

5XTC0, Components in wireless technologies

Lab 1: Computer-aided circuit simulation tool QUCS

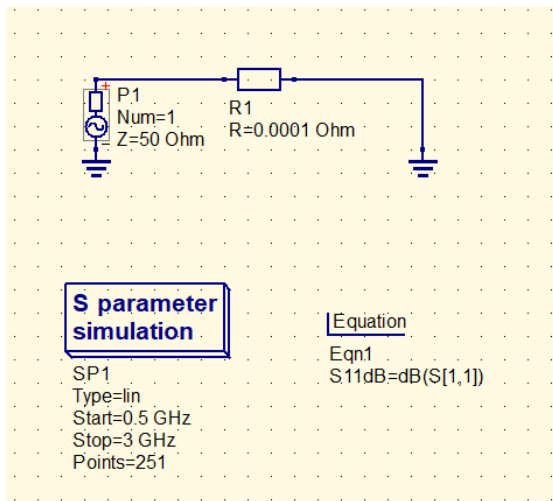


Student number
1819283

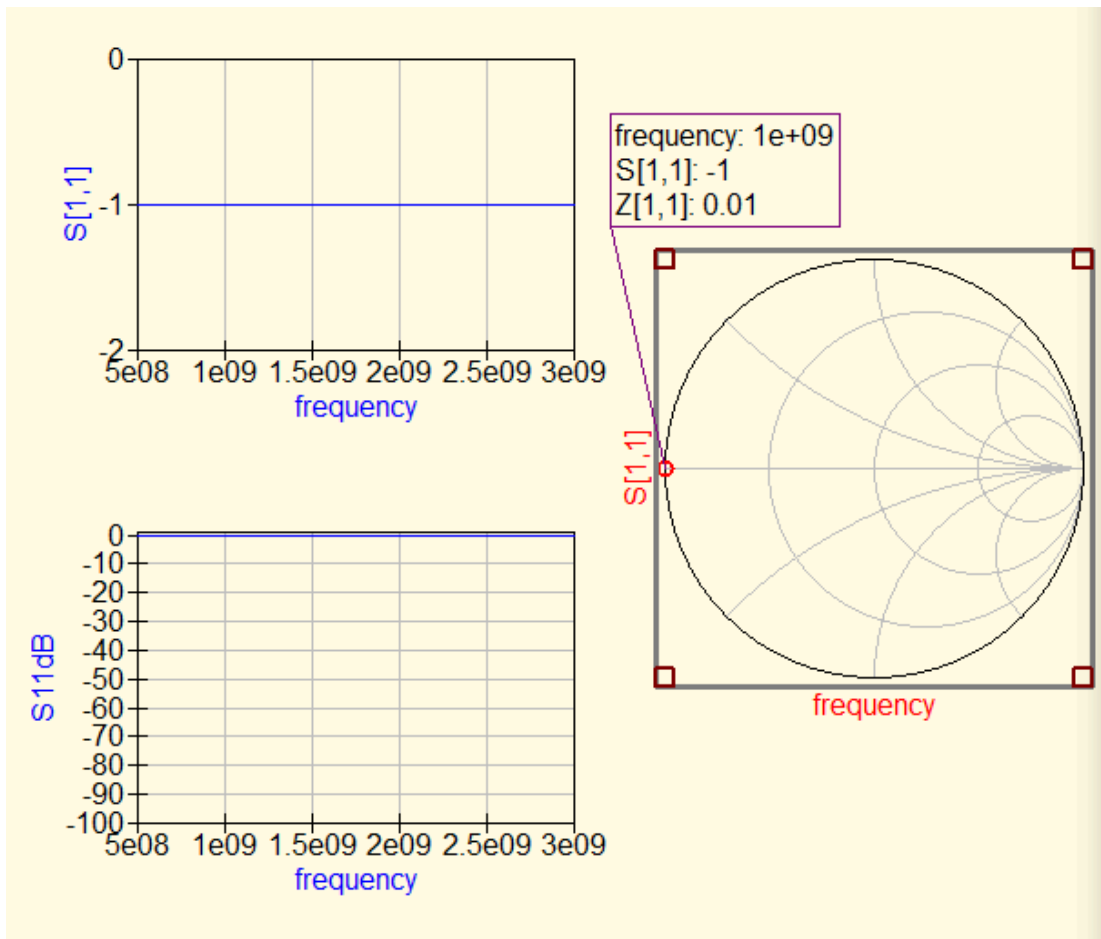
Daniel Tyukov
A. Example

Exercise 1a - Short-circuit load ($Z_0 = 50\Omega$)

Circuit diagram:



Simulation results:

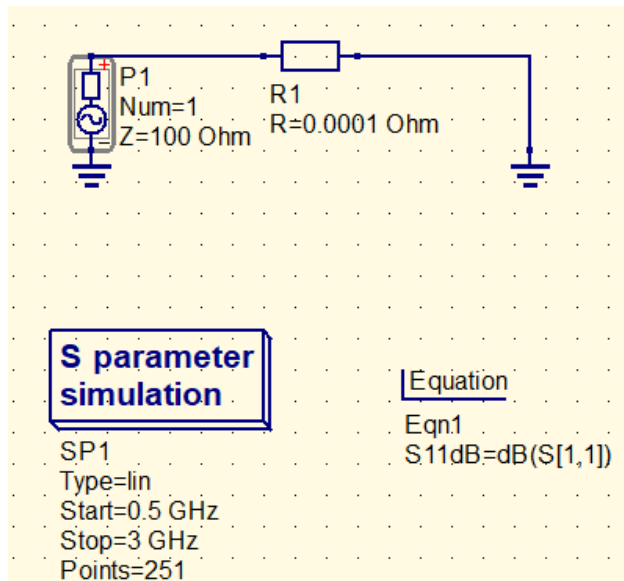


Explanation:

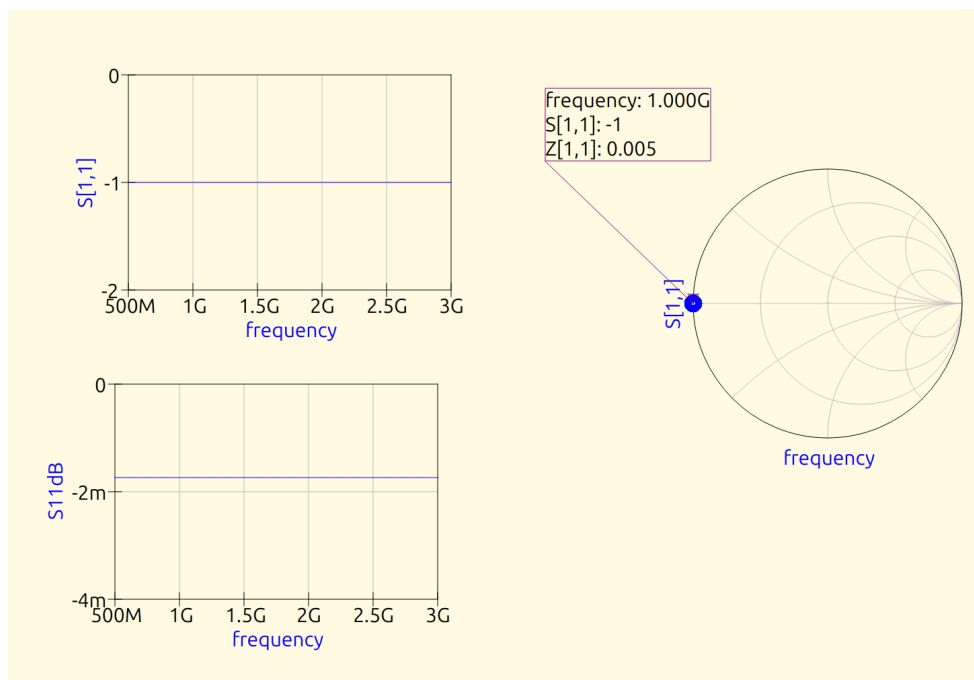
All power from the power source is reflected back but opposite phase. $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(0-50)}{(0+50)} = -50/50 = -1$.

Exercise 1b - Short-circuit load ($Z_0 = 100\Omega$)

Circuit diagram:



Simulation results:

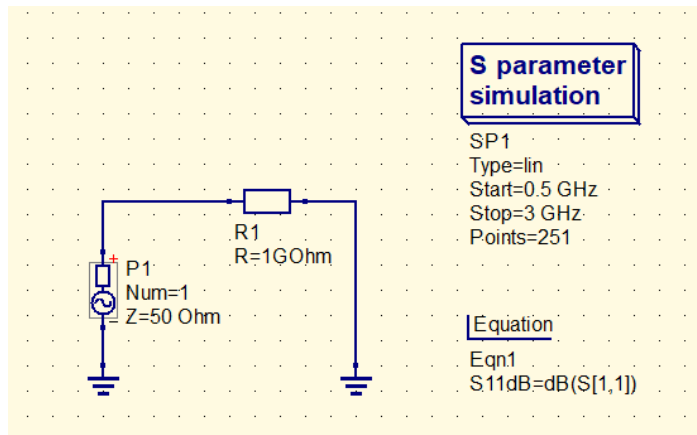


Explanation:

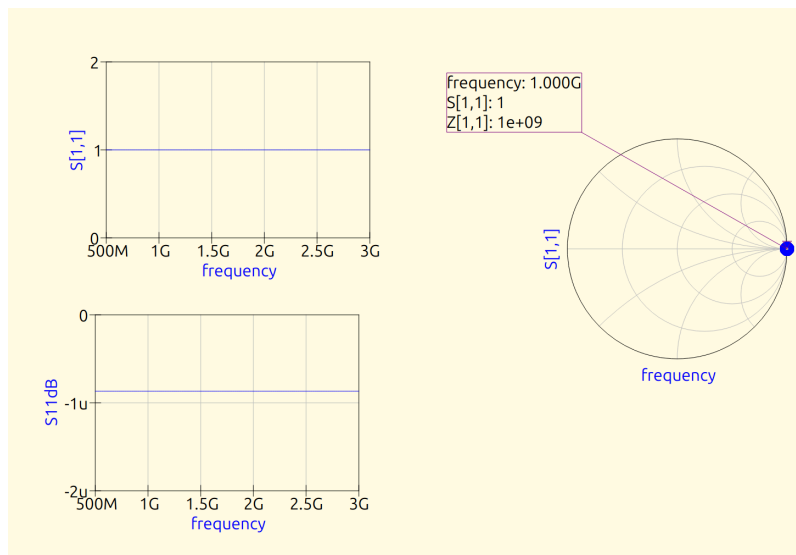
All power from the power source is reflected back but opposite phase. $\Gamma = Z_L - Z_0 / Z_L + Z_0 = (0 - 100) / (0 + 100) = -100/100 = -1$.

Exercise 1c - Open-circuit load ($Z_0 = 50\Omega$)

Circuit diagram:



Simulation results:

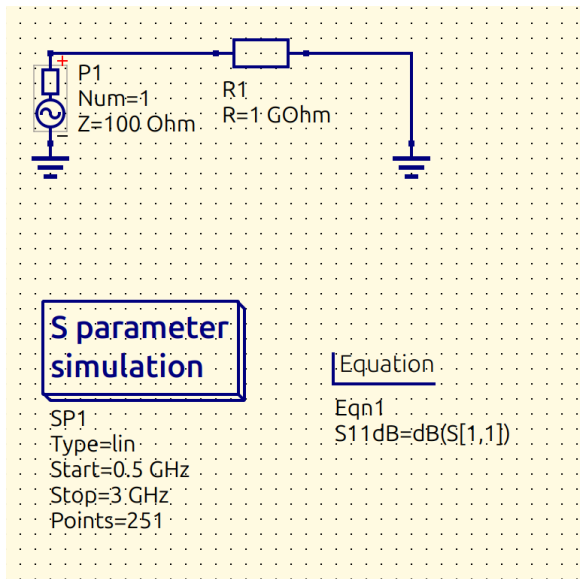


Explanation:

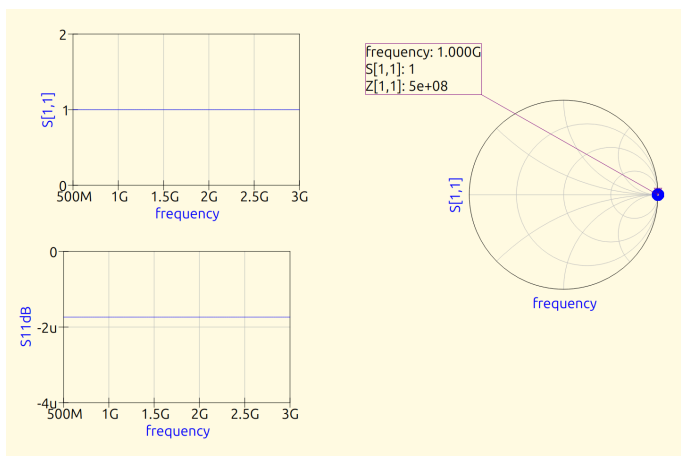
All power from the power source is reflected back with same phase and amplitude, $Z_L = \infty$. $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{0 - 50}{0 + 50} = \frac{\infty}{\infty} = 1$.

Exercise 1d - Open-circuit load ($Z_0 = 100\Omega$)

Circuit diagram:



Simulation results:

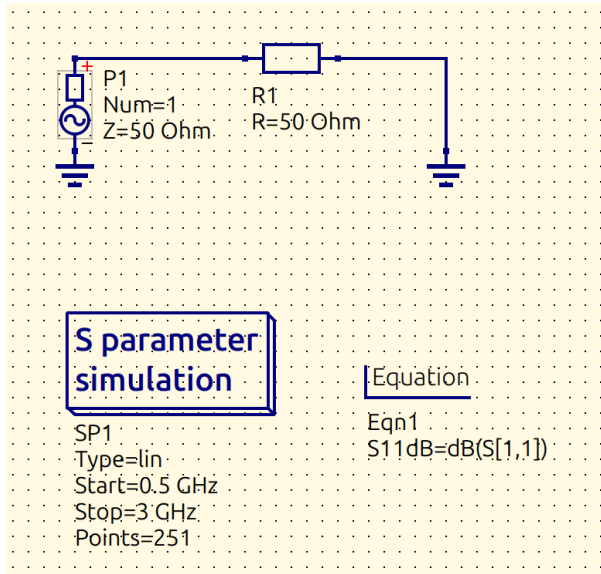


Explanation:

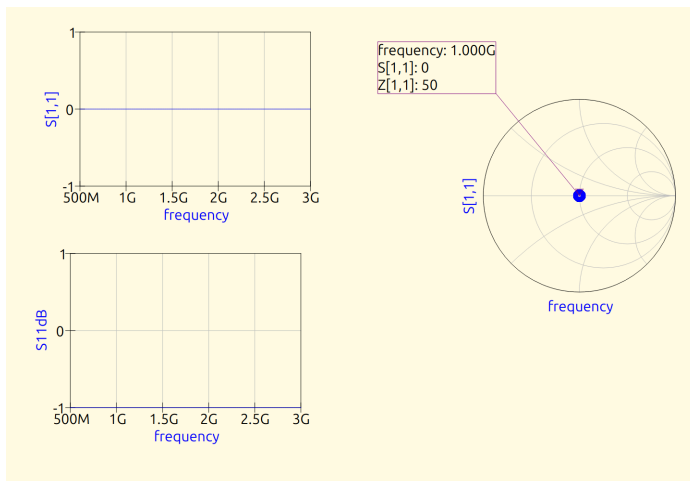
All power from the power source is reflected back with same phase and amplitude, $Z_L = \infty$. $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(0 - 100)}{(0 + 100)} = \frac{\infty}{\infty} = 1$.

Exercise 1e - Matched load ($Z_0 = 50\Omega$)

Circuit diagram:



Simulation results:

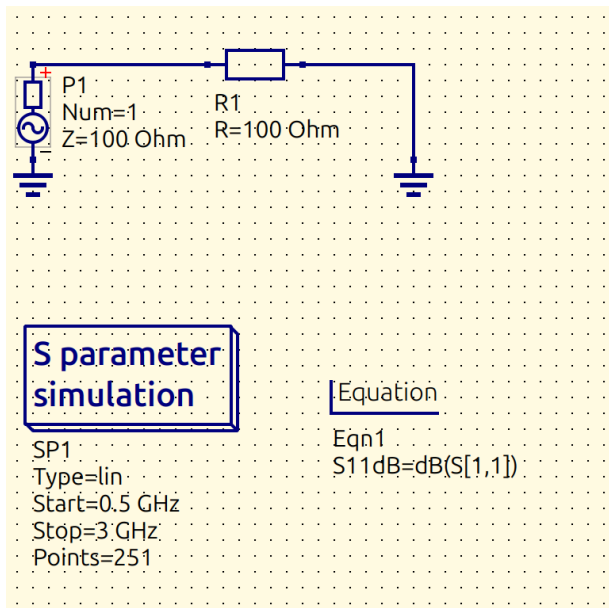


Explanation:

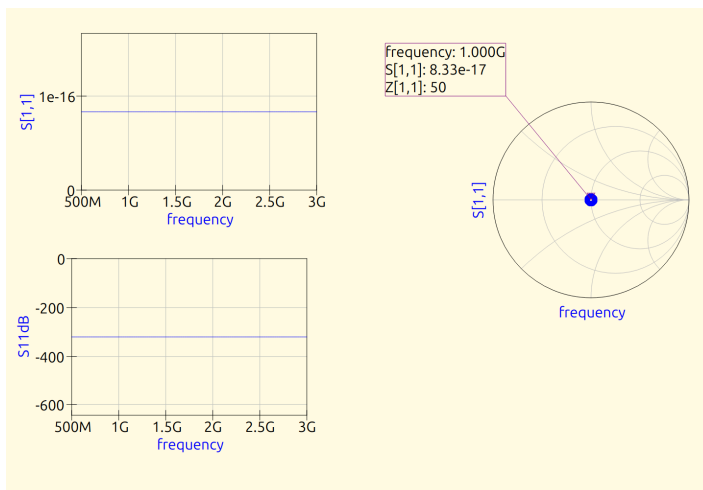
$Z_L = Z_0$ $\Gamma = 0$, with a matched filter there is 0 reflection coefficient perfect matching, no reflections.

Exercise 1f - Matched load ($Z_0 = 100\Omega$)

Circuit diagram:



Simulation results:

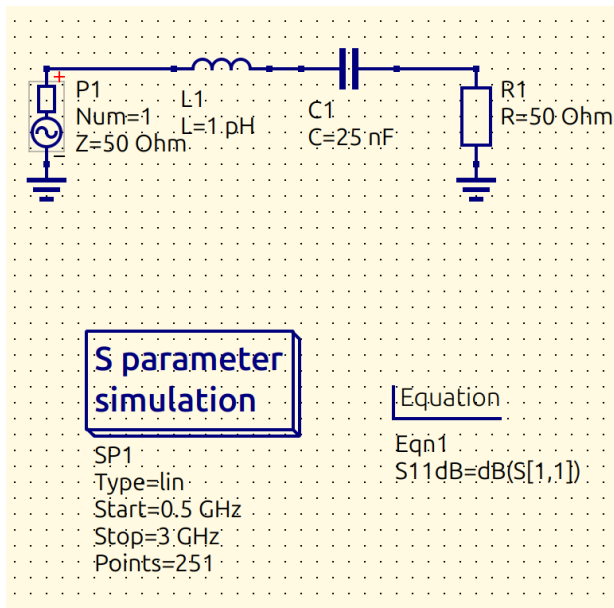


Explanation:

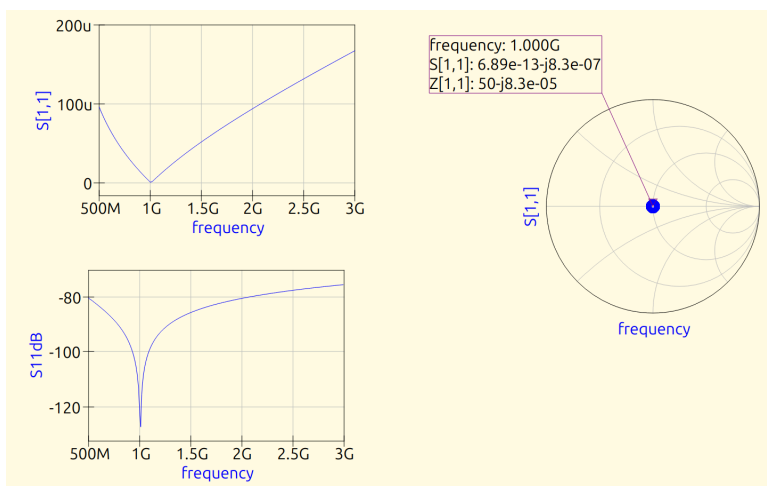
$Z_L = Z_0$ $\Gamma = 0$, with a matched filter there is 0 reflection coefficient perfect matching, no reflections. (In this case very minimal insignificant reflection).

Exercise 1g - LC lumped element (resonator) as load ($Z_0 = 50\Omega$)

Circuit diagram:



Simulation results:



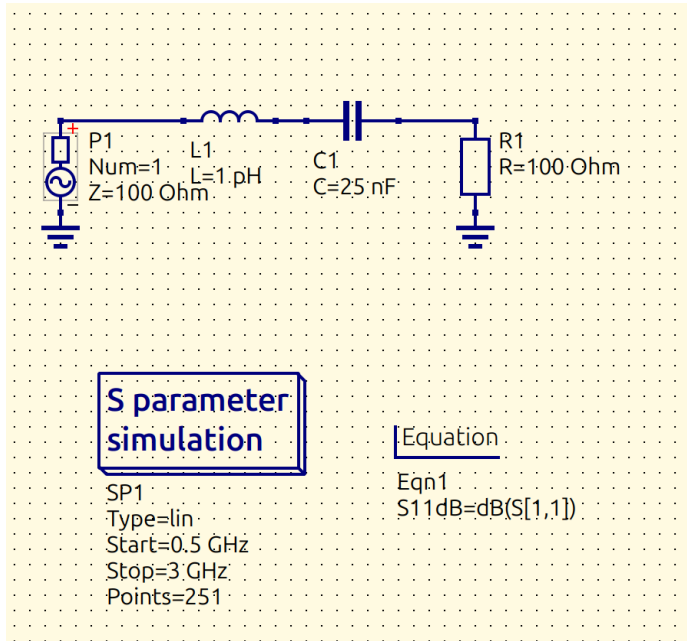
Explanation:

$f = 1/2\pi\sqrt{LC} \Rightarrow LC = 2.5 \cdot 10^{-20} = 25 \cdot 10^{-21}$ so we can use $L = 1 \cdot 10^{-12} = 1$ pico and $C = 25 \cdot 10^{-9} = 25$ nano

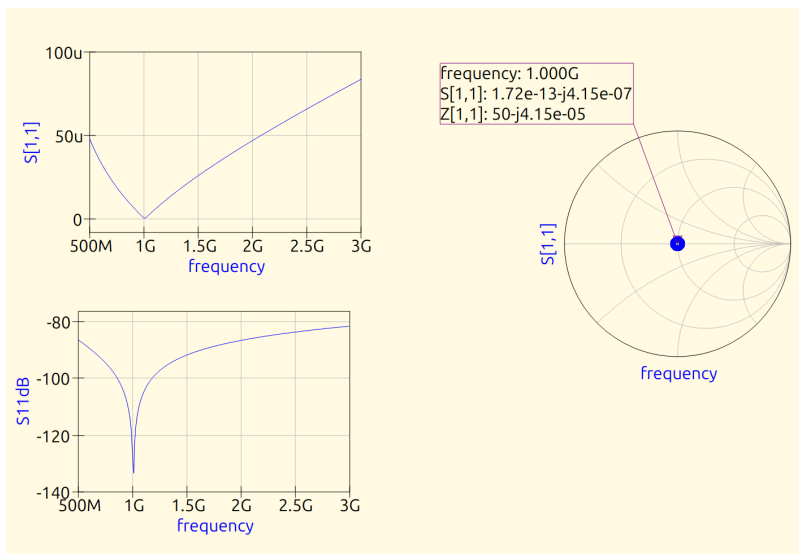
$Z_{LC} = j\omega L + 1/j\omega C = j6.27$, $Z_{total} = Z_{LC} \parallel 50$, $\Gamma = (Z_{total} - Z_0) / (Z_{total} + Z_0) = 6.89 \cdot 10^{-13} - j8.3 \cdot 10^{-7}$ is the obtained reflection coefficient.

Exercise 1g - LC lumped element (resonator) as load ($Z_0 = 100\Omega$)

Circuit diagram:



Simulation results:

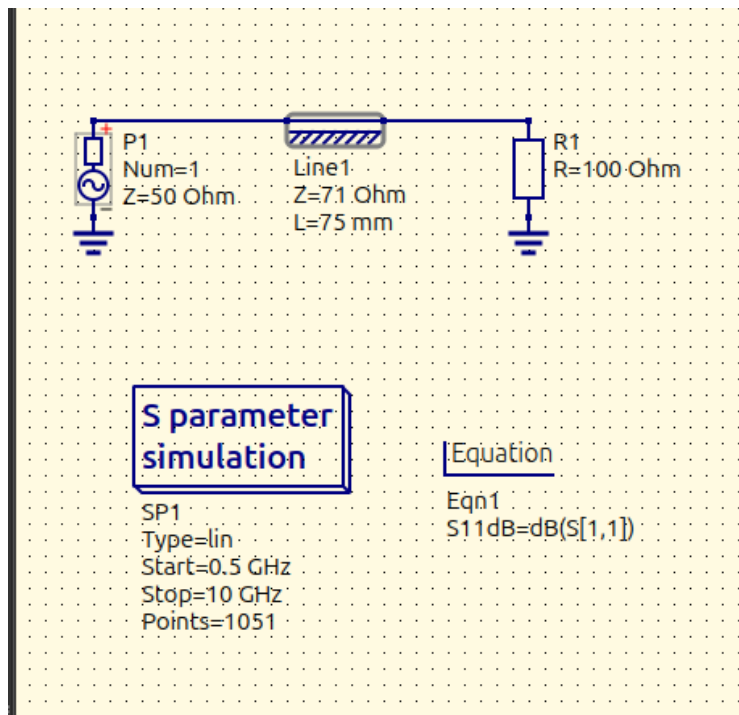


Explanation:

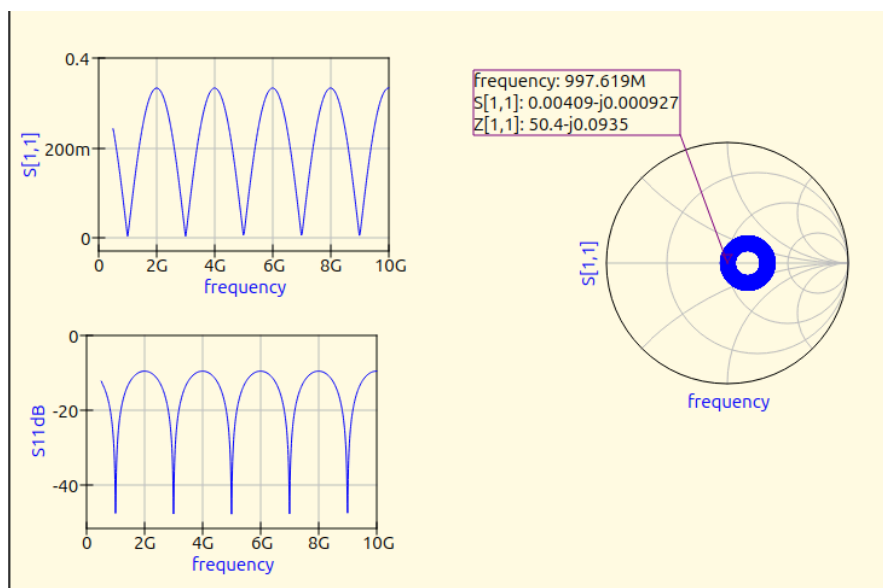
The exact same steps as in 1g just for $Z_0 = 100$

Exercise 2 - Quarter-wave transformer

Circuit diagram:



Simulation results:



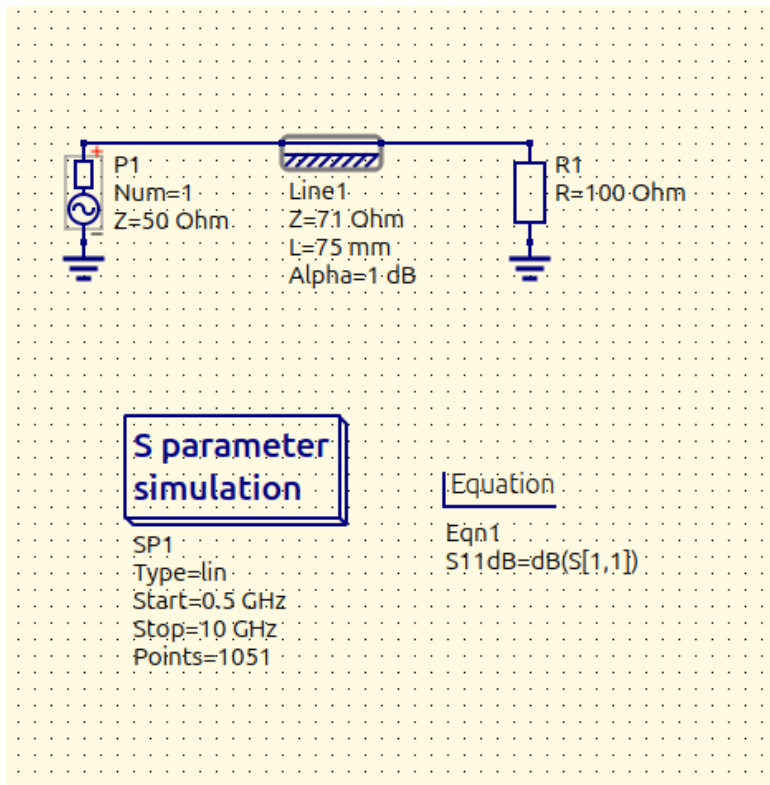
Explanation:

$Z_1 = \sqrt{Z_0 \cdot R_L} = \sqrt{50 \cdot 100} = 71 \text{ Ohm}$, $\lambda = c/f = 3 \cdot 10^8 / 1 \cdot 10^9 = 0.3 \text{ m}$ and then $L = \lambda/4 = 75 \text{ mm}$.

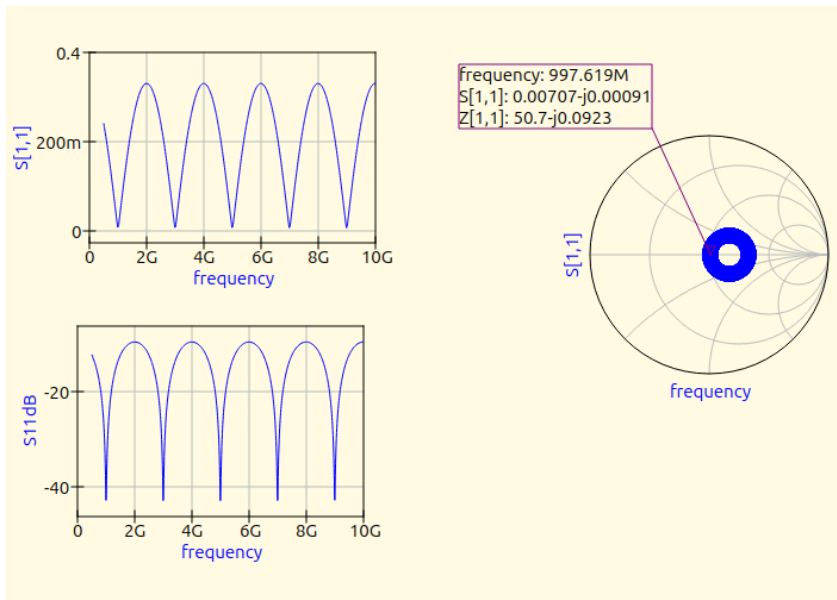
$\Gamma = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \rightarrow Z_{in} = \frac{Z_1^2}{R_L}$ where $Z_1 = \sqrt{Z_0 \cdot R_L}$ so $Z_{in} = Z_0$ so $\Gamma = 0$ in our case it is close to 0 so no reflection.

Exercise 3a – Lossy Quarter-wave transformer (1 dB/m)

Circuit diagram:



Simulation results:

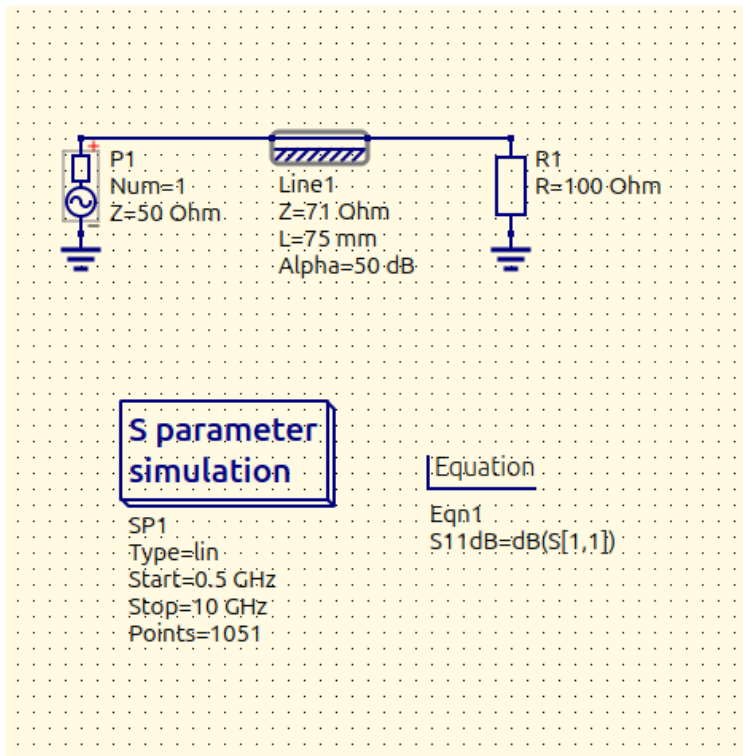


Explanation:

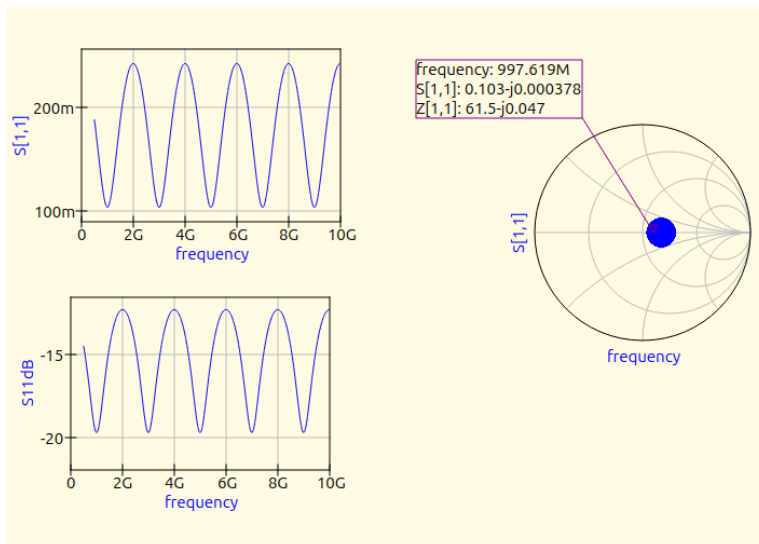
attenuation for 75mm = $aL = 1\text{dB/m} \times 0.075 = 0.075 \text{ dB}$, exponential loss factor = $e^{-2aL} = 0.983$, $Z_{\text{in}} \neq Z_0$ since we have real world attenuation, $Z_{\text{in}} = Z_0^2 / R_L \times e^{-2aL} = 50 \times 0.983 = 49.15$ so the $\Gamma \neq 0$ so reflects more.

Exercise 3b – Lossy Quarter-wave transformer (50 dB/m)

Circuit diagram:



Simulation results:

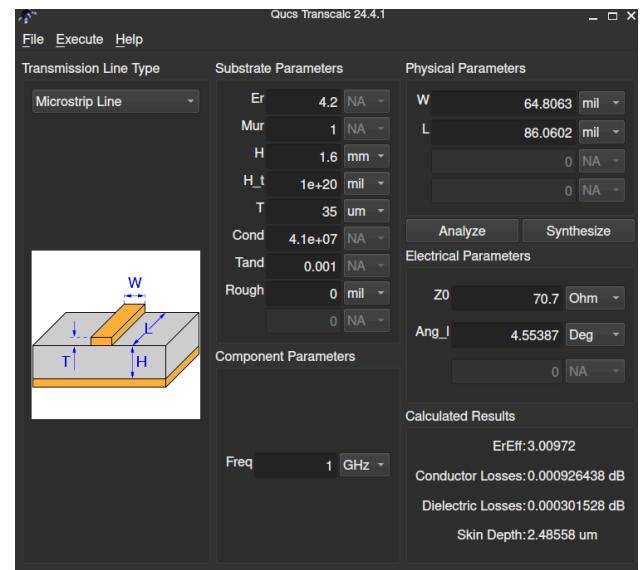
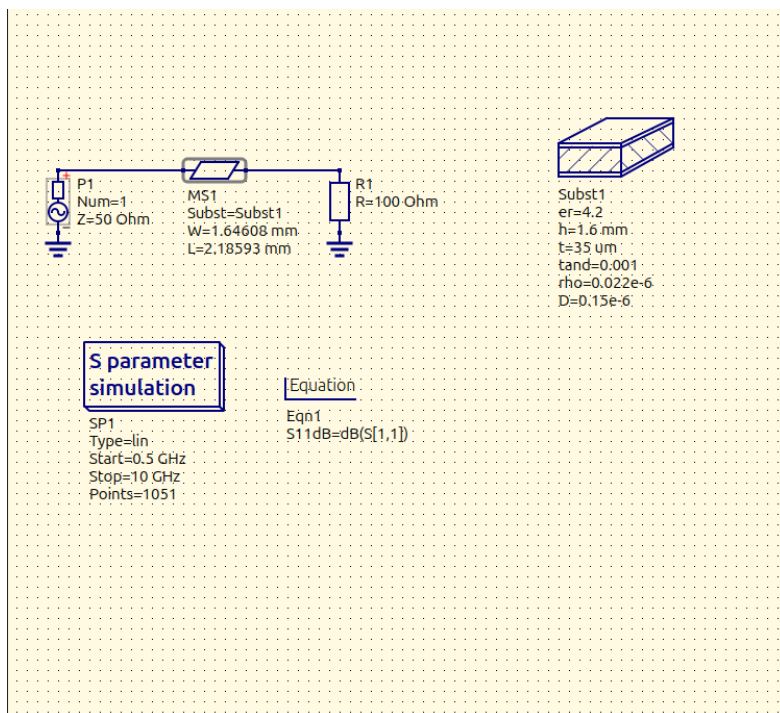


Explanation:

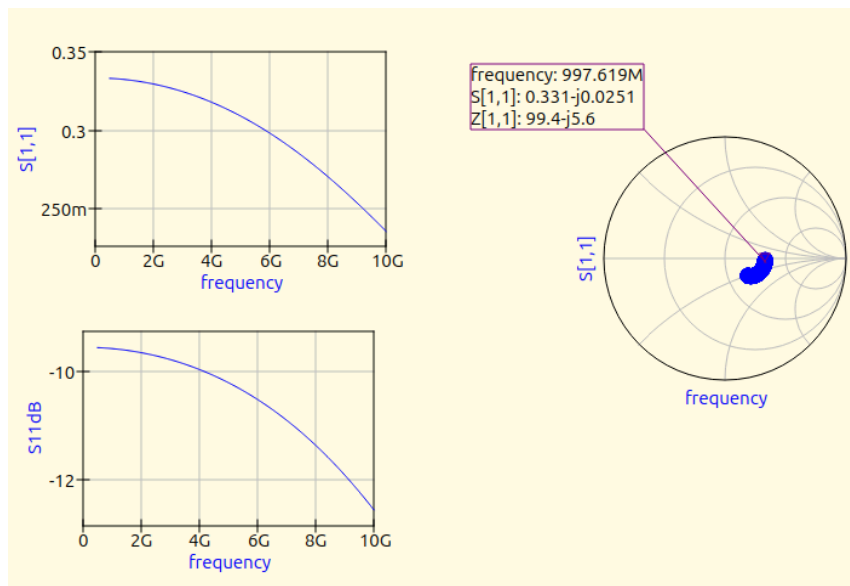
Same operation as last question but due to higher attenuation more reflection as a higher reflection coefficient in the range of 0.1.

Exercise 4 – microstrip Quarter-wave transformer

Circuit diagram:



Simulation results:

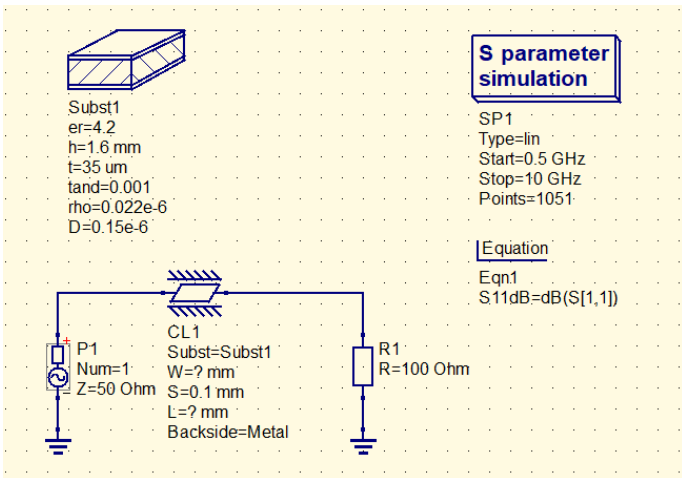


Why is L shorter as compared to the ideal Transmission line case?

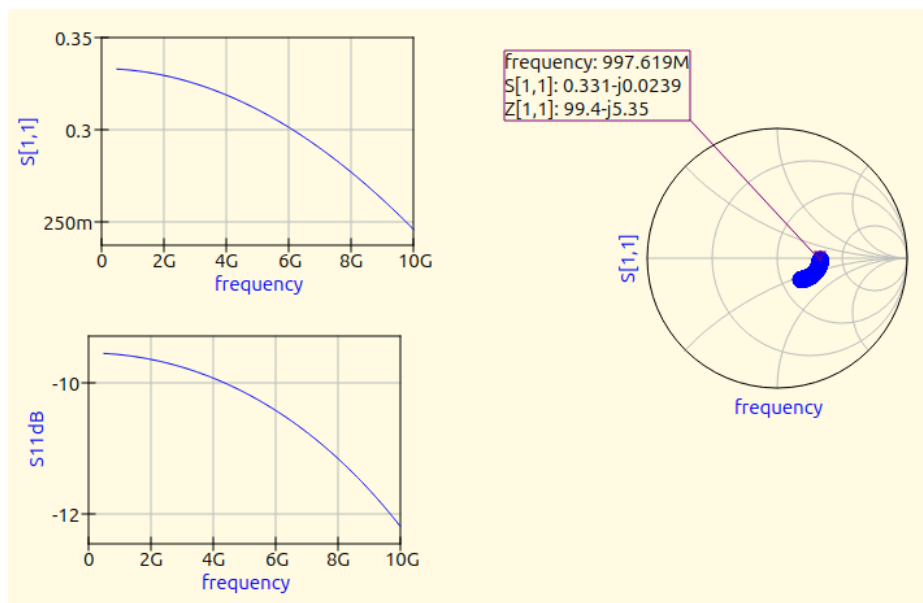
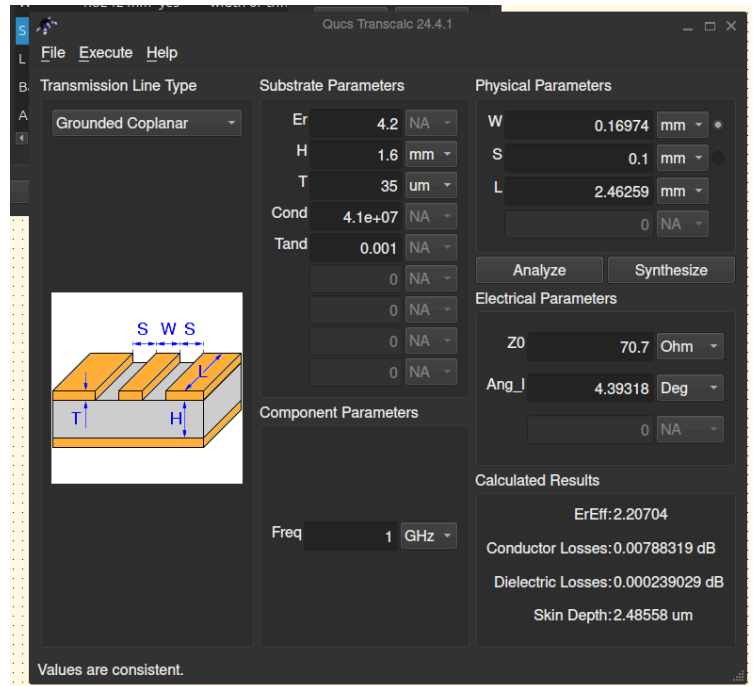
The length L is shorter in the microstrip case compared to an ideal transmission line because the effective permittivity ($\epsilon_{\text{eff}}=2.49$) of the microstrip is lower than the substrate permittivity ($\epsilon_r=4.2$), causing the guided wavelength (λ_g) to be shorter than the free-space wavelength (λ_0).

Exercise 5 – Grounded co-planar line Quarter-wave transformer

Circuit diagram:



Simulation results:



Which line is less lossy? The microstrip line of exercise 4, or this grounded coplanar line?

Microstrip Line (Exercise 4) Losses:

- **Conductor Losses = 0.0058358 dB**
- **Dielectric Losses = 0 dB**

Grounded Coplanar Line (Exercise 5) Losses:

- **Conductor Losses = 0.00788319 dB**
- **Dielectric Losses = 0.000239029 dB** (small but nonzero)

Comparison:

- The **Grounded Coplanar Line** has slightly **higher conductor losses** (0.00788 dB vs. 0.00583 dB).
- The **Dielectric Losses** in the grounded coplanar line are **slightly nonzero**, while they were effectively **0 dB** in the microstrip line.

Conclusion:

The **Microstrip Line** is **less lossy** compared to the **Grounded Coplanar Line** due to **lower conductor and dielectric losses**. This is generally expected because in a grounded coplanar waveguide (GCPW), more of the current is concentrated along the edges, increasing conductor losses due to surface resistance effects.