



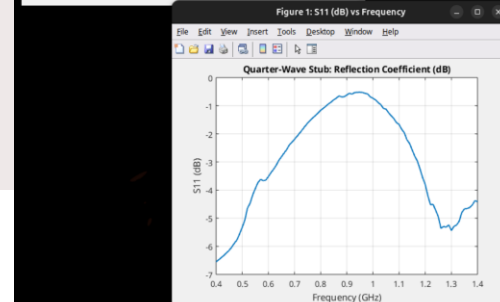
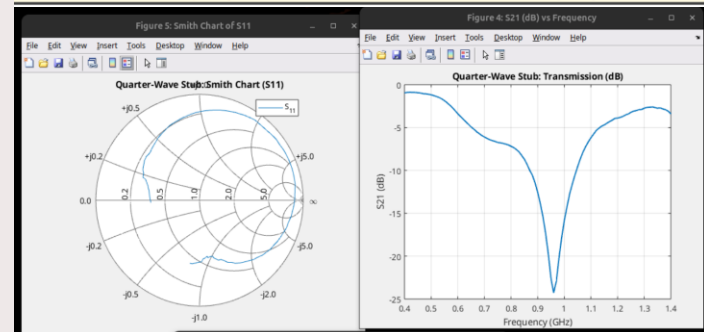
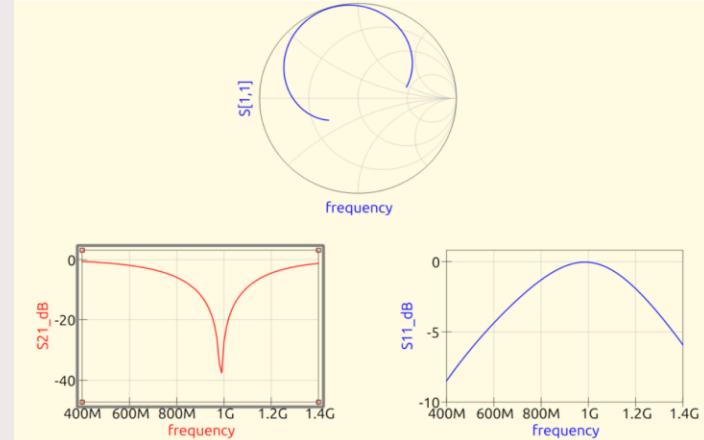
Antenna & Amplifier Laboratory Findings

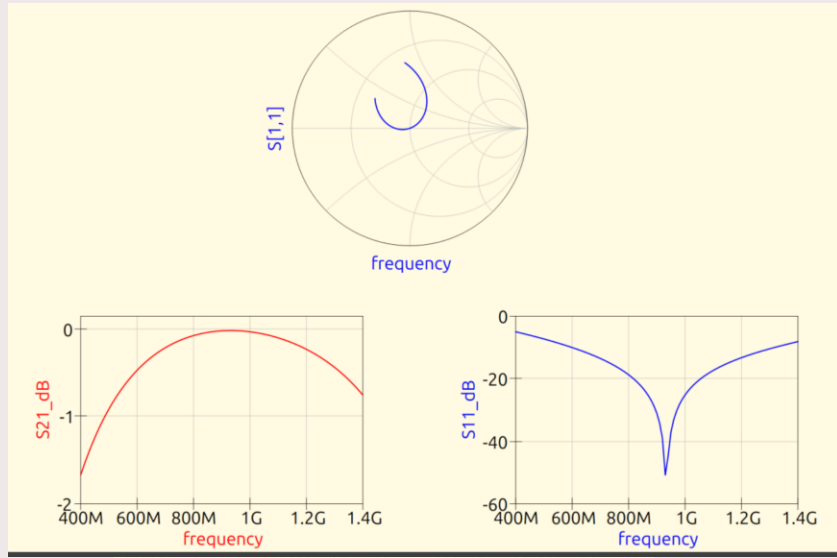
COMPONENTS AND WIRELESS TECHNOLOGY ORAL LAB EXAM – 01/04/2025

Daniel Tyukov

Lab 2 Findings – Quarter-Wave Stub Analysis

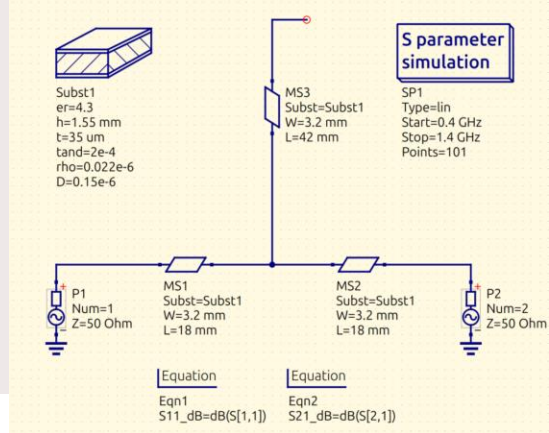
- At 1GHz, open stub behaves nearly like a short on the main line -> low reflection, high power transfer.
- At 500 MHz, it is not $\frac{1}{4}$ -wave -> mismatch and higher reflections.
- Stub is coplanar waveguide with approximately 50 ohms characteristic impedance.
- Reflection at 1 GHz: magnitude ~ 0.9188 , phase $\sim 1.47^\circ$, $Z_{in} \sim 1083 + j326$ ohms.



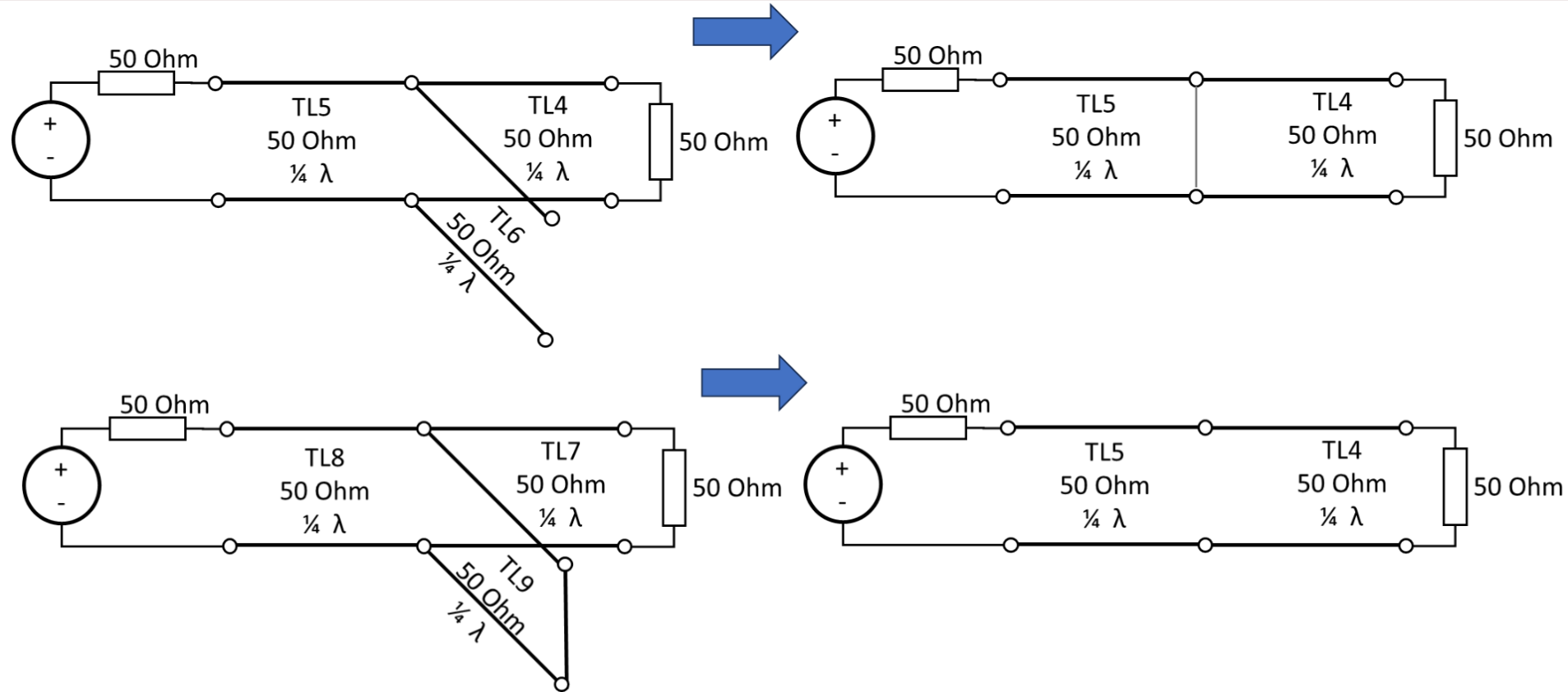


Additional Observations & Shorted Stub

- Measured results closely match simulations; slight offsets from cable losses/environment.
- Component can be used for impedance matching (e.g. antenna feed).
- Short-circuited stub inverts effect: minimal S_{11} at design freq and a passband response.
- Final check in QUCS: results confirm the transformation properties of both open- and short- circuited stubs.

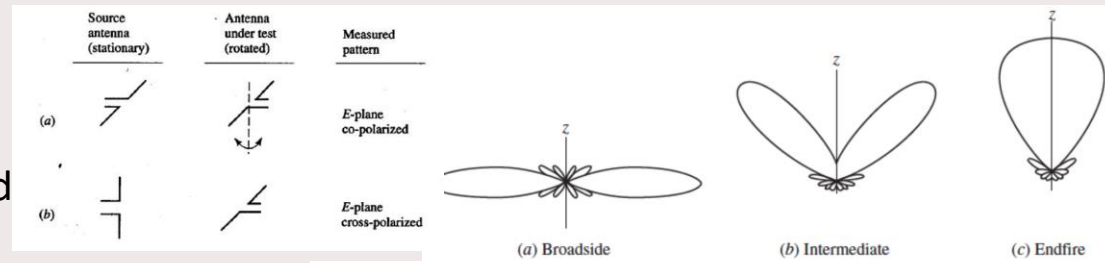


Extra: Expected Differences between Open- and Short- Stub

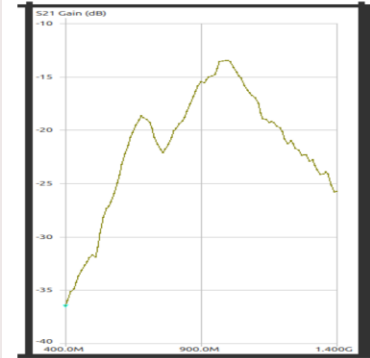


Lab 3 Antenna Measurements – Key Findings

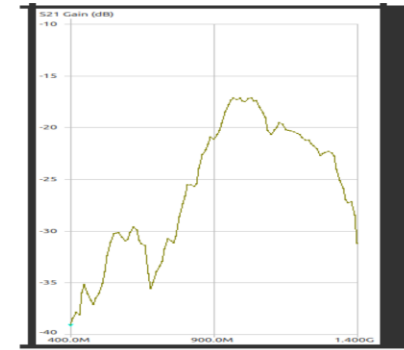
- **S11 and Power Transfer:** Dipole around 1GHz shows good match ($< -10\text{dB}$), meaning most power is delivered; bringing a hand close disrupts the near field, raising S11 (less power delivered).
- **Alignment (Port 2):** Best transmission with both dipoles broadside (maximum radiation), worst when endfire or cross-polarized.
- **Polarization:** Co-polarized dipoles yield highest S21; cross-polarized yields minimal coupling.
- **Friis Equation Gain:** Measured gain is lower than simulation; real-world losses (cables, environment) cause differences.



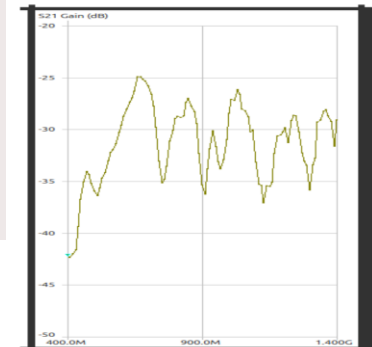
Broadside facing dipoles:

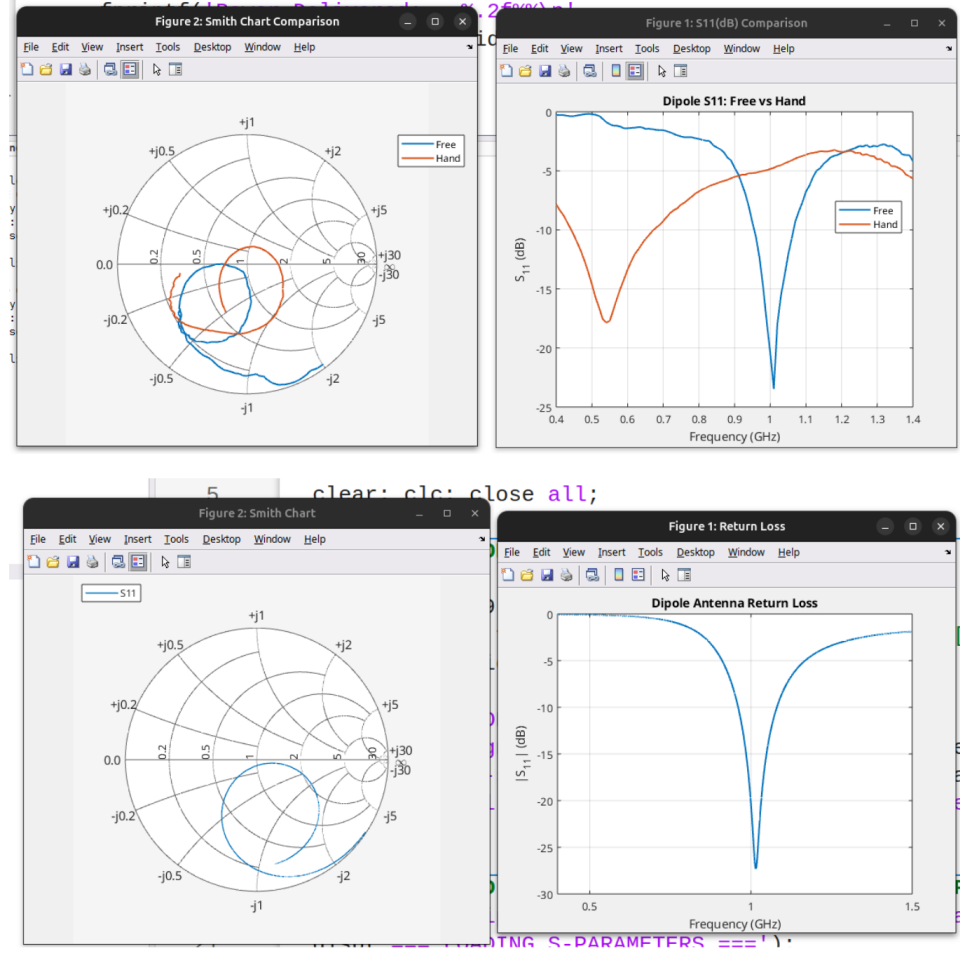


Endfire facing dipoles:



Co-polarized can be observed above, and cross polarized can be seen below:

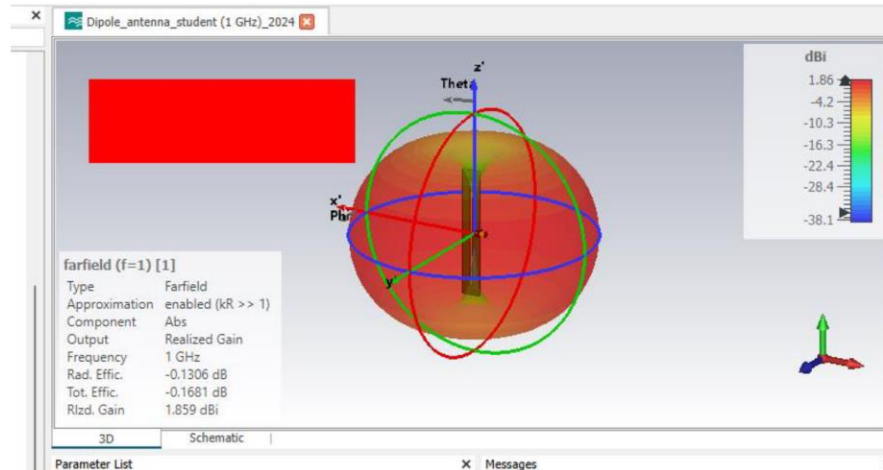




Antenna Simulations – CST & Comparisons

- **Dipole Length & Resonance:** ~150mm at 1.2GHz. After minor adjustments (114mm at 1GHz), S_{11} dips below -10dB near target frequency.
- **Radiation Pattern & Gain:** Classic doughnut shape, ~2dBi for an ideal half-wave dipole in free space; simulation close if well-meshed.
- **Symmetry & Polarization:** Pattern is symmetric (centre-fed), linear polarization from current along one axis.
- **Mesh Convergence:** Adaptive meshing confirms S_{11} and far-field stabilized. Most cells near feed/edges (highest field gradient).

Extra: CST showing dipole resonance



Number of freq. points: 1011

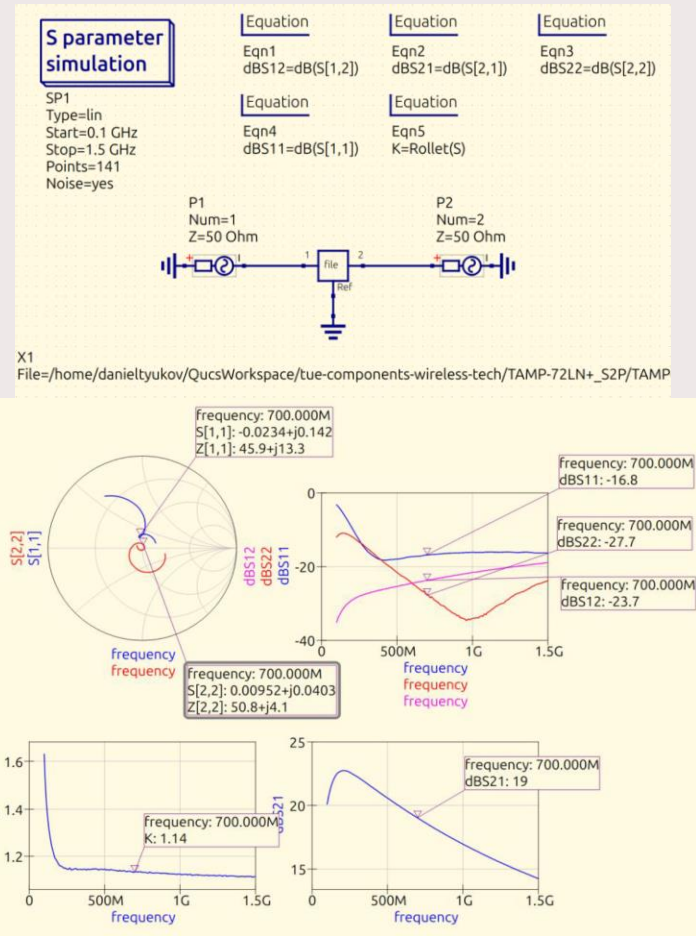
Found resonance near : 1.015 GHz

S11(dB) at resonance : -27.30 dB

Offset from design (MHz) : 14.90 MHz

Lab 5 Stand-Alone Amplifier Findings

- Using the TAMP-72LN+ S-parameter file in QUCS, we see:
 - S_{11} (input reflection), S_{12} (isolation), S_{21} (gain), S_{22} (output reflection).
 - K-factor > 1 , indicating unconditional stability over $\sim 400\text{-}700\text{MHz}$.
 - Gain $\sim 19\text{dB}$ at 700MHz , closely matching datasheet (about 18.7dB)
 - No external biasing needed: module has internal bias/matching; just supply 5V .
 - Minor deviations from datasheet due to simulation vs real conditions, but overall close

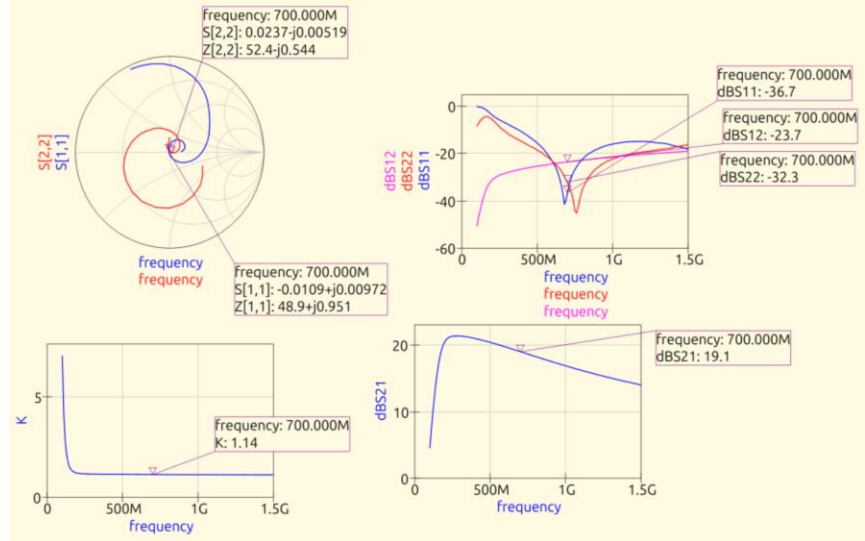
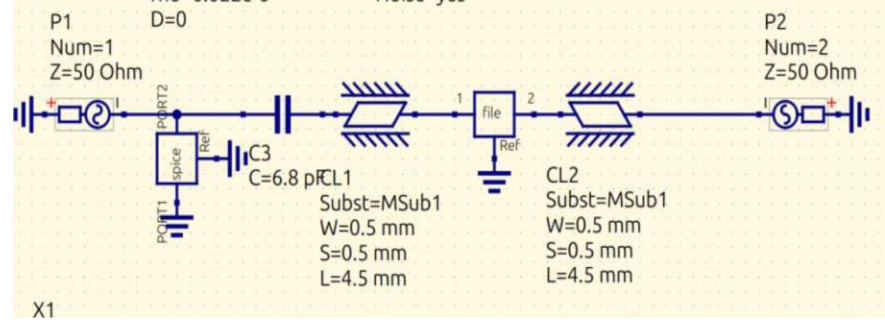
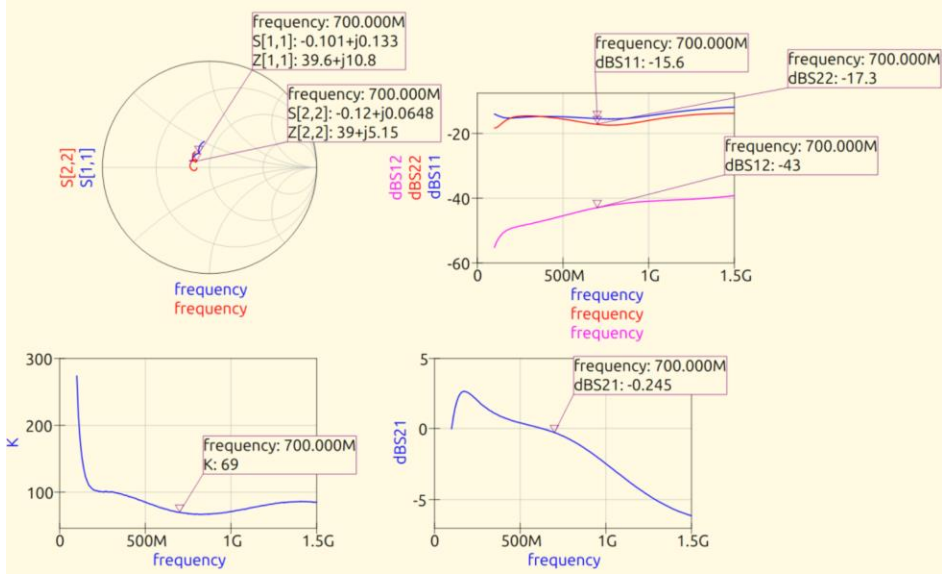
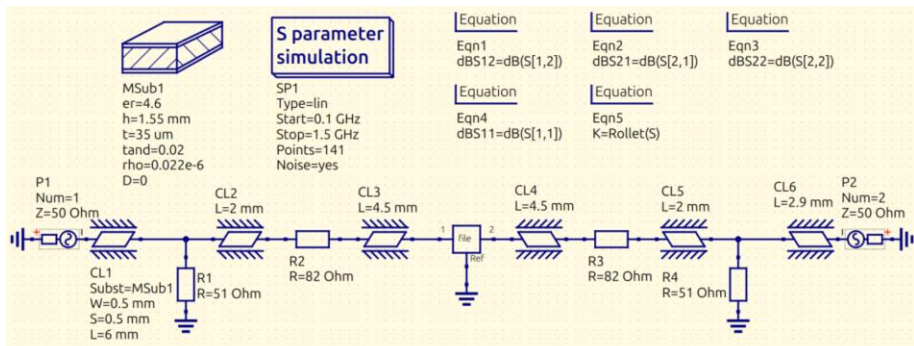


Original Board with Resistors:

- S21 drops significantly (19 dB \rightarrow near 0dB) because added load the amplifier
- Input (S11) and output (S22) reflections worsen from nearly 50 ohms to ~ 39 ohms, leading to mismatches.
- K-factor becomes very high (~ 69) due to extra damping, ensuring stability but sacrificing gain.
- Co-planar grounded spaces between components alter the line impedance.

Redesigned Board (Removing Resistors, Adding LC Matching):

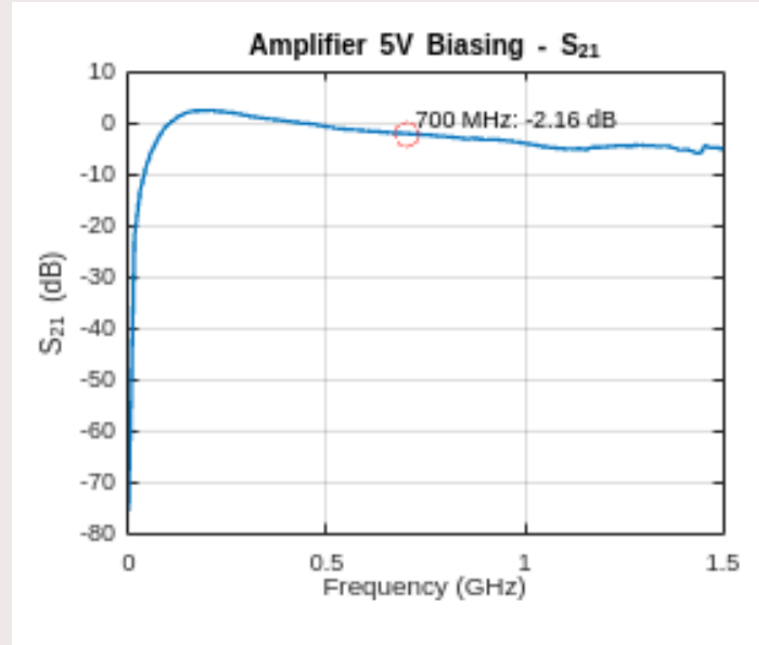
- Restore ~ 19 dB gain at 700 MHz (close to the stand-alone amplifier's performance).
- S11 and S22 improve (near 50 ohms) by adjusting the coplanar spacing and using shunt/series LC elements.
- Highlights that the original layout had ~ 39 ohms trace impedance (needed ~ 0.11 mm spacing for 50 ohms).
- Achieves stable operation ($K > 1$), matching typical stand-alone amplifier specs.



Measurement Results & Comparisons

- **Key S-Parameter Values at 700 MHz:**

- **No Bias:** $S_{11} = -16.49\text{ dB}$, $S_{21} = -29.10\text{ dB}$ (amplifier is off \rightarrow large attenuation), $S_{12} = -29.74\text{ dB}$, $S_{22} = -12.80\text{ dB}$.
- **5V Bias:** $S_{11} = -11.42\text{ dB}$, $S_{21} = -2.16\text{ dB}$, $S_{12} = -44.70\text{ dB}$, $S_{22} = -11.94\text{ dB}$.
- **1.4V Bias:** $S_{11} = -11.37\text{ dB}$, $S_{21} = -5.01\text{ dB}$, $S_{12} = -42.79\text{ dB}$, $S_{22} = -11.58\text{ dB}$



Observed gain ($\sim -2\text{ dB}$) is much lower than the $\sim 19\text{ dB}$ from simulation. Resistor pads and measurement factors (connector/cable losses, NanoVNA range limits, different LC components) heavily reduce net gain. S_{11} and S_{22} also differ because real PCB parasitics are not perfectly accounted for in simulation.

Explanations & Analysis

1. **Resistor Attenuation (80 ohm + 50 ohm):** Around 9.8dB input pad to avoid VNA compression.
2. **Extra Bias Resistor for 1.4V:** ~ 180 ohm in series $((5V - 1.4V)/0.02A = 180 \text{ ohm})$.
3. **NanoVNA Power vs. Amplifier Limits:** NanoVNA ~ 0 dBm output; amplifier can handle $\sim +27$ dBm. Well within limits.
4. **Input/Output Power Calculation:**
 - Input to amp ~ 0 dBm $- 9.8 \text{ dB} = -9.8 \text{ dBm}$.
 - Amp gain $\sim 19\text{dB} \rightarrow \sim +9.2 \text{ dBm}$ at amplifier output.
 - Another $\sim 9.8 \text{ dB}$ pad on output \rightarrow final $\sim -0.6 \text{ dBm}$ to the VNA.

The End, Thanks for Listening

