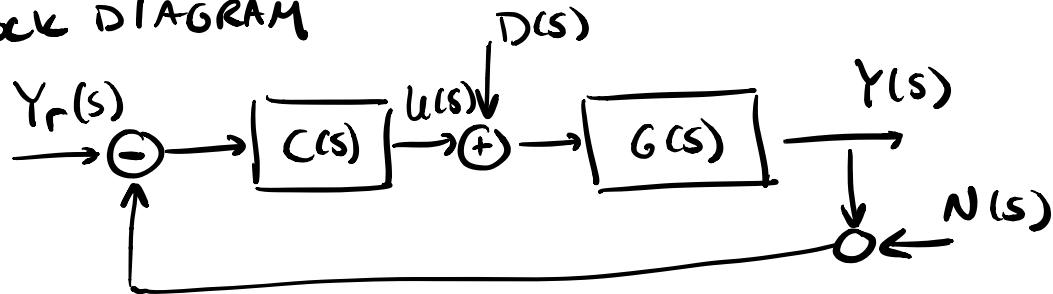


REVIEW:

PLANT & CONTROLLER

BLOCK DIAGRAM



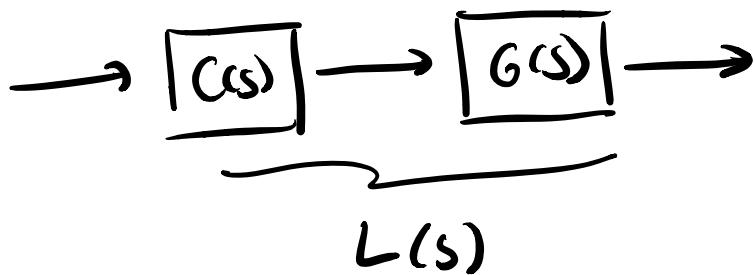
$$Y(s) = G(s)(U(s) + D(s))$$

$$U(s) = C(s)(Y_r(s) - Y(s) - N(s))$$

$$\underline{Y(s)} = \underline{G(s)C(s)}(Y_r(s) - \underline{Y(s)} - \underline{N(s)}) + \underline{G(s)D(s)}$$

$$(1 + \underline{G(s)C(s)})\underline{Y(s)} = \underline{G(s)C(s)}[Y_r(s) - \underline{N(s)}] \\ + \underline{G(s)D(s)}$$

$L(s) = G(s)C(s)$  : open loop transfer function



$$Y(s) = \frac{L(s)}{1+L(s)} [Y_r(s) - N(s)] + \frac{G(s)}{1+L(s)} D(s)$$

$1+L(s) = 0$  characteristic eqn.

roots determine the stability...

BIBO stability: roots of  $1+L(s)$  in the OLTIP.

Track a reference signal  $Y_r(s)$  . . .

Error:  $E(s) = Y(s) - Y_r(s)$

$$\underline{E(s)} = \frac{L(s)}{1+L(s)} [Y_r(s) - N(s)] + \frac{G(s)}{1+L(s)} D(s) - Y_r(s)$$

$$= \left( \frac{L(s)}{1+L(s)} - 1 \right) Y_r(s) - \frac{L(s)}{1+L(s)} N(s) + \frac{G(s)}{1+L(s)} D(s)$$

$$= \underbrace{-\frac{1}{1+L(s)} Y_r(s)}_{\text{Want no steady state error from}} + \underbrace{\frac{G(s)}{1+L(s)} D(s)}_{\text{reference signal (tracking)}} - \underbrace{\frac{L(s)}{1+L(s)} N(s)}_{\text{disturbance (disturbance rejection)}}$$

Want  
no steady state error from  
reference signal (tracking)  
disturbance (disturbance rejection)

## FINAL VALUE THM:

$f(t)$  w Laplace Transform  $F(s)$

$F(s)$  has poles in OHP w at most 1 pole at the origin.

$$\begin{aligned} \lim_{t \rightarrow \infty} f(t) &= \lim_{s \rightarrow 0} s F(s) \\ &= \lim_{s \rightarrow 0} \frac{\beta_k s^k + \dots + \beta_1 s + \boxed{\beta_0}}{\alpha_n s^n + \dots + \alpha_1 s + \boxed{\alpha_0}} \end{aligned}$$

$$E(s) = \underbrace{\frac{-1}{1+L(s)} Y_r(s)}_{\text{Tracking}} + \underbrace{\frac{G(s)}{1+L(s)} D(s)}_{\text{Disturbance}} - \frac{L(s)}{1+L(s)} N(s)$$

$$L(s) = G(s) C(s) = \frac{\text{num}_G}{\text{den}_G} \frac{\text{num}_C}{\text{den}_C}$$

### Tracking

$$\frac{-1}{1+L(s)} Y_r(s) = \frac{-\text{den}_G \text{den}_C}{\text{den}_G \text{den}_C + \text{num}_G \text{num}_C} Y_r(s)$$

$$\frac{G(s)}{1+L(s)} D(s) = \frac{\text{num}_G \text{den}_C}{\text{den}_G \text{den}_C + \text{num}_G \text{num}_C} D(s)$$

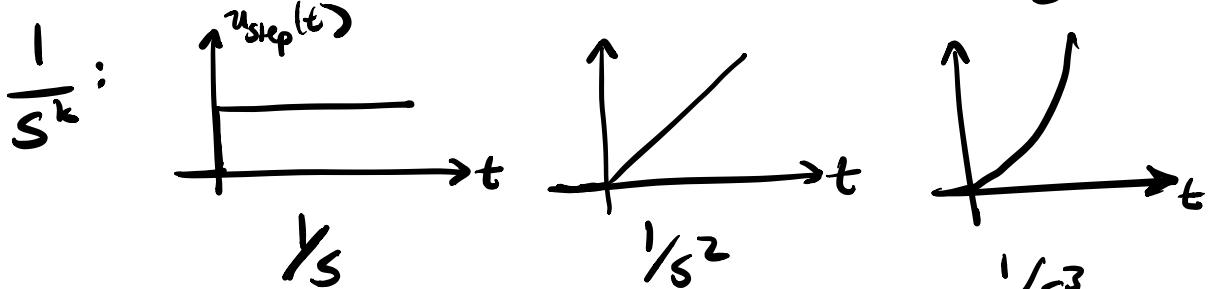
### WANT

$$\lim_{s \rightarrow 0} s \frac{1}{1+L(s)} Y_r(s) = 0$$

$$\lim_{s \rightarrow 0} s \frac{G(s)}{1+L(s)} D(s) = 0$$

### Disturbance Rejection

lets assume  $Y_r(s) = \frac{1}{s^k}$  or  $D(s) = \frac{1}{s^k}$



want ↓

$$\lim_{s \rightarrow 0} \frac{\text{den}_G + \text{den}_C}{\text{den}_G + \text{num}_G + \text{num}_C} \frac{s}{s^k} = 0$$

$$\lim_{s \rightarrow 0} \frac{\text{num}_G + \text{den}_C}{\text{den}_G + \text{den}_C + \text{num}_G + \text{num}_C} \frac{s}{s^k} = 0$$

trying to get a constant term in the denominator of these expressions ↴

no constant term in the top...

set  $\text{den}_C(s) = s^k$

works for tracking  
but not for  
disturbance rejection

what if  $\text{den}_C(s) = s^{k-1}$

get  $\lim_{s \rightarrow 0} \frac{\text{den}_G}{\text{den}_G + \text{num}_G + \text{num}_C}$   
ms or  $ms^2$

$$\lim_{s \rightarrow 0} \frac{\text{num}_G + \text{den}_C}{\text{den}_G + \text{den}_C + \text{num}_G + \text{num}_C} \frac{s}{s^k}$$

single integrator or double integrator

$\frac{1}{ms}$

velocity control

$\frac{1}{ms^2}$

position control

} Newton's  
2nd law.

once we've picked the  $\text{den}_C$   
 (for disturbance rejection/tracking)  
 pick the  $\text{num}_C(s)$  for stability:

$$\frac{\text{den}_G(s)}{\text{den}_C(s)} + \frac{\text{num}_G(s)}{\text{num}_C(s)} = 0$$

want roots in OLHP       $\searrow$  DOF for stability.

Ex.  $G(s) = \frac{1}{ms^2}$

$$\frac{ms^2(s^k)}{ms^{k+2}} + \frac{1}{\underbrace{\text{num}_C(s)}} = 0$$

$$ms^{k+2} + \text{num}_C(s) = 0 \quad ]$$

- all terms of  $\text{num}_C(s)$  need positive coeffs.

$$\text{num}_C(s) = \underline{\beta_{k+1}s^{k+1}} + \dots + \underline{\beta_1s} + \underline{\beta_0}$$

$\beta_{k+1}, \dots, \beta_1, \beta_0 > 0$  necessary for stability.

determine conditions on  $\beta$ 's using  
 the Routh - Hurwitz test.

RH Test:  $s^5 + bs^4 + cs^3 + ds^2 + es + f = 0$

$$\begin{array}{cccccc} s^5 & 1 & c & e & 0 \\ s^4 & \underline{b} & d & \cancel{f} & 0 \\ s^3 & \boxed{\frac{c-d}{b}} & \frac{bc-1d}{b} & \boxed{\frac{c-f}{b}} & \frac{be-f}{b} & 0 \end{array}$$

$$s^2 \boxed{\frac{d-b^2e-fb}{bc-d}} \quad f \quad 0$$

$$s^1 \boxed{\frac{eb-f}{b} - \frac{(bcf-df)(bc-d)}{bd(bc-d)-(b^2e-fb)b}} \quad 0$$

$$s^0 \quad f \quad \frac{eb-f}{b} - \frac{cf-df}{d-\frac{b^2e-fb}{bc-d}}$$

$$\frac{eb-f}{b} - \frac{(bcf-df)(bc-d)}{bd(bc-d)-(b^2e-fb)b}$$

### Conditions

$$1 > 0$$

$$b > 0$$

$$c > \frac{d}{b}$$

$$\frac{d - b^2 e - fb}{bc - d} > 0$$

$$\frac{eb - f}{b} \frac{(bcf - df)(bc - d)}{bd(bc - d) - (b^2 e - fb)b} > 0$$

$$f > 0$$

could show that these conditions  
imply that  $b, c, d, e, f > 0 \Leftarrow$

stability for

Nec & Suff

$$\bullet s^2 + bs + c$$

$$b, c > 0$$

$$\bullet s^3 + as^2 + bs + c$$

$$a, b, c > 0$$

$$ab > c$$

Disturbance Rejection for Sinusoidal Input.  
and Tracking.

$$D(s) = \frac{\omega}{s^2 + \omega^2} = \frac{\omega}{\underline{(s+i\omega)(s-i\omega)}}$$

$$d(t) = \sin(\omega t)$$

## Tracking

$$\lim_{s \rightarrow 0} \frac{\text{den}_c \text{den}_c}{(\text{den}_c + \text{num}_c \text{num}_c) s^2 + \omega^2} \frac{s \omega}{s^2 + \omega^2}$$

these are only marginally stable

want to set  $\text{den}_c = s^2 + \omega^2$

what if now there is a step input?

$$\lim_{s \rightarrow 0} \frac{\text{num}_G (s^2 + \omega^2)}{\text{den}_c \text{den}_c + \text{num}_G \text{num}_c} \frac{s \omega}{s^{k-1}} \rightarrow$$

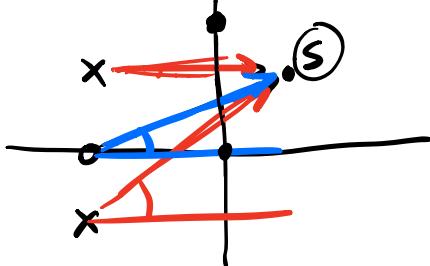
won't have  
disturbance  
rejection  
for step inputs

need  $\text{den}_c(s) = s^k (s^2 + \omega^2)$

## Transfer Functions

$$G(s) = \frac{\beta_k s^k + \dots + \beta_1 s + \beta_0}{\alpha_n s^n + \dots + \alpha_1 s + \alpha_0}$$

$$= \frac{(s - z_1) \dots (s - z_k)}{(s - p_1) \dots (s - p_n)}$$



## Disturbance Rejection

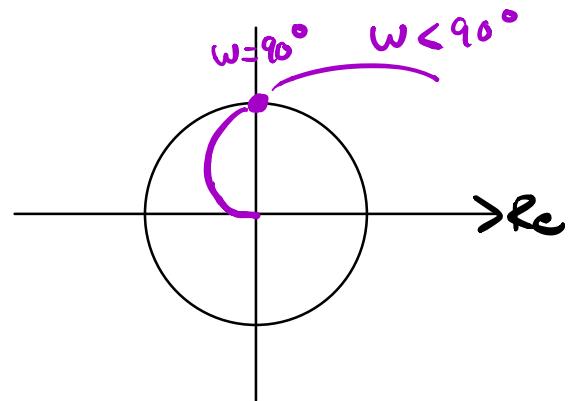
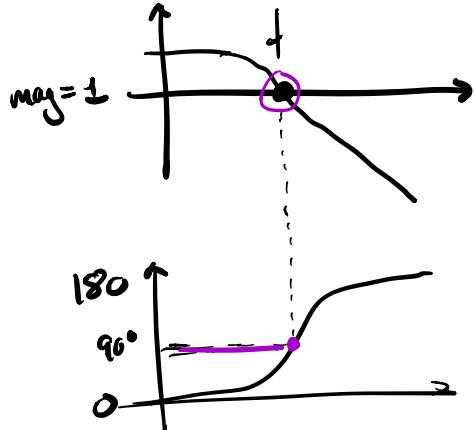
$$\lim_{s \rightarrow 0} \frac{\text{num}_c \text{den}_c}{(\text{den}_c + \text{num}_c \text{num}_c) s^2 + \omega^2} \frac{s \omega}{s^2 + \omega^2}$$

$G(i\omega)$

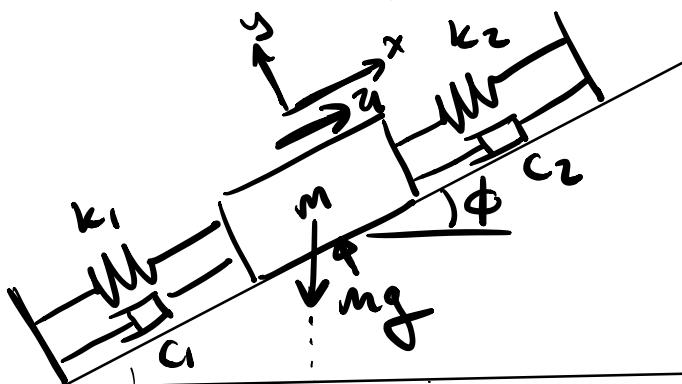
$$G(s) = \frac{\prod_j |s - z_j|}{\prod_{j'} |s - p_j|} e^{i(\sum_j \alpha(s - z_j) - \sum_{j'} (s - p_j))}$$

magnitude  
- Bode plot

phase  
Bode plot.



Dynamics Modeling:

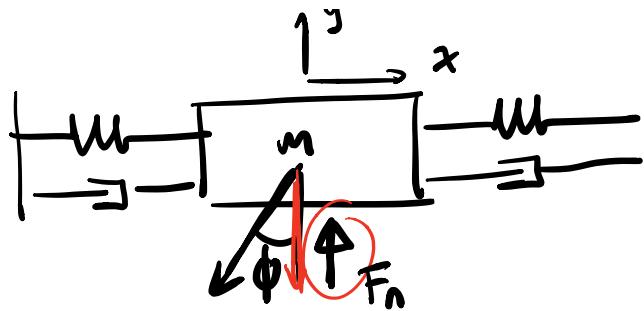


Deriving Eqs of Motion:

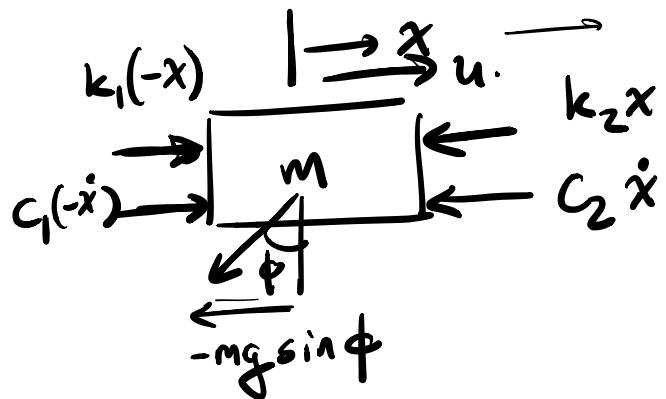
$$\text{FBD: } \sum F_x = m \ddot{x}$$

$$\sum F_y = m \ddot{y}$$

"



$$\begin{aligned}\sum F_y &= F_n - mg \cos \phi = 0 \\ F_n &= mg \cos \phi\end{aligned} \rightarrow$$



$$\begin{aligned}\sum F_x &= k_1(-x) - k_2 x \\ c_1(-\dot{x}) - c_2 \dot{x} - mg \sin \phi + u &= m \ddot{x}\end{aligned}$$

$$\ddot{x} = \frac{1}{m} \left( -(k_1 + k_2)x - (c_1 + c_2)\dot{x} - mg \sin \phi + u \right)$$

$$z = \begin{bmatrix} x \\ \dot{x} \end{bmatrix}$$

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{-(k_1+k_2)}{m} & -\frac{(c_1+c_2)}{m} \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix} u + \begin{bmatrix} 0 \\ g \sin \phi \end{bmatrix}$$

$$s^2 X(s) - \dot{X}(0) - sX(0) = -\frac{(k_1+k_2)}{m} X(s) - \frac{c_1+c_2}{m} (sX(s) - X(0))$$

$$-\frac{1}{s} g \sin \phi + \frac{1}{m} U(s)$$

$$\left( s^2 + \frac{c_1+c_2}{m}s + \frac{k_1+k_2}{m} \right) X(s) = \dot{X}(0) + sX(0) + \frac{c_1+c_2}{m} X(0) - g \sin \phi + \frac{1}{s}$$

$$+ \frac{1}{m} \underline{U(s)}$$

$$X(s) = \frac{1}{\left( s^2 + \frac{c_1+c_2}{m}s + \frac{k_1+k_2}{m} \right)} \left( \cancel{\dot{X}(0) + sX(0)} + \frac{c_1+c_2}{m} \cancel{X(0)} - g \sin \phi \right)$$

$$+ \frac{1}{m \left( s^2 + \frac{c_1+c_2}{m}s + \frac{k_1+k_2}{m} \right)} \underline{U(s)}$$