

Homework) Questions:

Question 1d & e :  $f: \mathbb{R}^n \rightarrow \mathbb{R}$        $\frac{\partial}{\partial x_j} \left( \frac{\partial f}{\partial x_i} \right) = \frac{\partial}{\partial x_i} \left( \frac{\partial f}{\partial x_j} \right)$

e)  $\frac{\partial^2 f}{\partial x^2} = \frac{\partial}{\partial x} \frac{\partial f}{\partial x} = \frac{\partial}{\partial x} \left( \left[ \frac{\partial f}{\partial x_1} \cdots \frac{\partial f}{\partial x_n} \right] \right)$  general.

$$= \begin{bmatrix} \frac{\partial^2 f}{\partial x_1^2} & \frac{\partial^2 f}{\partial x_1 \partial x_n} \\ \vdots & \vdots \\ \frac{\partial^2 f}{\partial x_n \partial x_1} & \frac{\partial^2 f}{\partial x_n^2} \end{bmatrix}$$

d) A is not sym.

not true that  $\frac{\partial^2 f}{\partial x_i \partial x_j} \neq A_{ij}$

is equal to  $\frac{\partial^2 f}{\partial x_i \partial x_j} = \frac{1}{2} (A_{ij} + A_{ji})$

Homework 2 questions:

uniqueness of eigenvectors...

$$A = P D P^{-1} = \begin{bmatrix} v_1 \cdots v_n \end{bmatrix} \begin{bmatrix} \lambda_1 & & \\ & \ddots & \\ & & \lambda_n \end{bmatrix} \begin{bmatrix} v_1 \cdots v_n \end{bmatrix}^{-1}$$

$\uparrow$                            $\uparrow$   
 $E \in \mathbb{C}^{n \times n}$                    $E^{-1} \in \mathbb{C}^{n \times n}$   
 (diagonal)                  (diagonal)

$$E = \begin{bmatrix} r_1 e^{i\phi} & & \\ & \ddots & \\ & & r_n e^{i\phi} \end{bmatrix} \quad E^{-1} = \begin{bmatrix} \bar{r}_1 e^{-i\phi} & & \\ & \ddots & \\ & & \bar{r}_n e^{-i\phi} \end{bmatrix}$$

$$P E = \begin{bmatrix} r_1 v_1 e^{i\phi} & & \\ & \ddots & \\ & & r_n v_n e^{i\phi} \end{bmatrix} \quad E^{-1} P^{-1} = (\bar{P} \bar{E})^{-1}$$

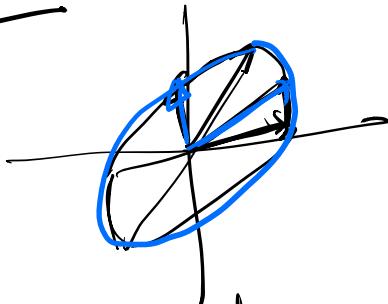
$$E = \begin{bmatrix} e^{i\phi} & \\ & \bar{e}^{-i\phi} \end{bmatrix} \propto \begin{bmatrix} c\phi & -s\phi \\ s\phi & c\phi \end{bmatrix}$$

$$\begin{bmatrix} u & v \end{bmatrix} \begin{bmatrix} \cos\phi & -\sin\phi \\ \sin\phi & \cos\phi \end{bmatrix} = \begin{bmatrix} u' & v' \end{bmatrix}$$

$u' = \cos\phi u + \sin\phi v$  etc.

$$E^{-1} = \begin{bmatrix} \cos\phi & \sin\phi \\ -\sin\phi & \cos\phi \end{bmatrix}$$

Pictures:



Condition Number:

$$y = Ax \quad A \text{ ill conditioned} \quad \text{for a particular } y, x \text{ is huge}$$

$$x = A^{-1}y \quad \text{essentially cols together}$$


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LECTURE NOTES:

Clarifications:

$$1) \dot{x} = Ax + Bu \rightarrow \lambda = a+bi \text{ eval} \quad \text{stability } \underbrace{\text{Re}(\lambda)}_a < 0$$

$$x(t+1) = \bar{A}x(t) + \bar{B}u(t) \quad \bar{\lambda} \text{ eval } \bar{A} \quad \text{stability } |\bar{\lambda}| < 1$$

look at  $\bar{A} = e^{A\Delta t}$  consistent.

$(\bar{A})^t$  if  $|\bar{\lambda}_i| < 1 \quad \forall i \quad \bar{\lambda}_i^t \rightarrow 0$  if  $|\bar{\lambda}_i| < 1$

$$2) \text{ if } M = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix} \quad \text{evals}(M) = \text{evals}(A) \cup \text{evals}(D)$$

$$\text{evecs: } \lambda v = Av \quad M \begin{bmatrix} v \\ 0 \end{bmatrix} = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix} \begin{bmatrix} v \\ 0 \end{bmatrix} = \lambda \begin{bmatrix} v \\ 0 \end{bmatrix}$$

$$\mu w = Dw$$

$$M \begin{bmatrix} x \\ w \end{bmatrix} = \begin{bmatrix} A & B \\ 0 & D \end{bmatrix} \begin{bmatrix} x \\ w \end{bmatrix} = \mu \begin{bmatrix} x \\ w \end{bmatrix}$$

$$\Rightarrow \mu x = Ax + Bw \Rightarrow x = (\mu I - A)^{-1}Bw$$

subtleties if  $\mu$  is also eval of  $A$   
general picture.

### Interpretations of Controllability

Not controllable if

- $B$  is ll to a left evec.

$$A = PDP^{-1}$$

$$[A^{n-1}B \dots ABB] = P[D^{n-1}\tilde{P}^{-1}B \dots D\tilde{P}^{-1}B \tilde{P}^{-1}B]$$

$$\text{condition} \Rightarrow \tilde{P}^{-1}B = \begin{bmatrix} * \\ 0 \\ * \\ \vdots \end{bmatrix} \rightarrow D\tilde{P}^{-1}B = \begin{bmatrix} * \\ 0 \\ * \\ \vdots \end{bmatrix}$$

$$= \tilde{P}_{\text{ith row}} \begin{bmatrix} \dots & \dots & \dots \\ 0 & 0 & 0 & \dots \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix} \Rightarrow \text{one the columns never shows up}$$

$$e_i^T \tilde{P}^{-1}P \begin{bmatrix} \dots & \dots & \dots \\ 0 & 0 & 0 & \dots \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix} = [0 \dots 0]$$

$\Rightarrow$  controllability matrix has a left nullspace

$\Rightarrow$  not full row rank.

Transform Coords on dynamics

$$\dot{x} = Ax + Bu \quad \text{plug in } x = Tz \Rightarrow \dot{z} = \tilde{T}^{-1}ATz + \tilde{T}^{-1}Bu$$

in Z coords  $\begin{bmatrix} (\bar{T}^{-1} A \bar{T})^{n-1} \bar{T}^{-1} B & \dots & \end{bmatrix}$

$$\begin{bmatrix} \bar{T}^{-1} A^{n-1} B & \dots & \bar{T}^{-1} A B \bar{T}^{-1} B \end{bmatrix}$$

$$\bar{T}^{-1} \begin{bmatrix} A^{n-1} B & \dots & A B B \end{bmatrix}$$

Not observable ...

$C \perp \rightarrow$  a right eigenvector  
"output direction"

Not controllable if

not enough inputs for repeats eigenvals.

example  $\lambda_1 = \lambda_2$   $D = \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix}$   $\bar{B} = \mathbb{R}^{n \times 1}$

in the eigen vector coords ...

$$\begin{bmatrix} D^{n-1} \bar{B} & \dots & D \bar{B} \bar{B} \end{bmatrix} \quad \bar{B} = \begin{bmatrix} \bar{b} \\ x \\ z \end{bmatrix} \in \mathbb{R}^2$$

If you choose  $w \in \mathbb{R}^2$   
st.  $w^T \bar{b} = 0$

left multiply ...

$$\underbrace{w^T}_{} \underbrace{\begin{bmatrix} \lambda_1^n \bar{b} & \lambda_1^{n-2} \bar{b} & \dots & \end{bmatrix}}_{\downarrow} = \begin{bmatrix} \lambda_1^n w^T \bar{b} & \lambda_1^{n-2} w^T \bar{b} & \dots & \end{bmatrix} = \begin{bmatrix} 0 & \dots & 0 \end{bmatrix}$$

$w^T$  can't be  $\perp$  to  $\begin{pmatrix} \lambda_1^{n-1} 0 \\ 0 \lambda_2^{n-1} \end{pmatrix} \bar{b}$   $\notin \begin{pmatrix} \lambda_1^{n-2} \\ \lambda_2^{n-2} \end{pmatrix} \bar{b}$  etc.

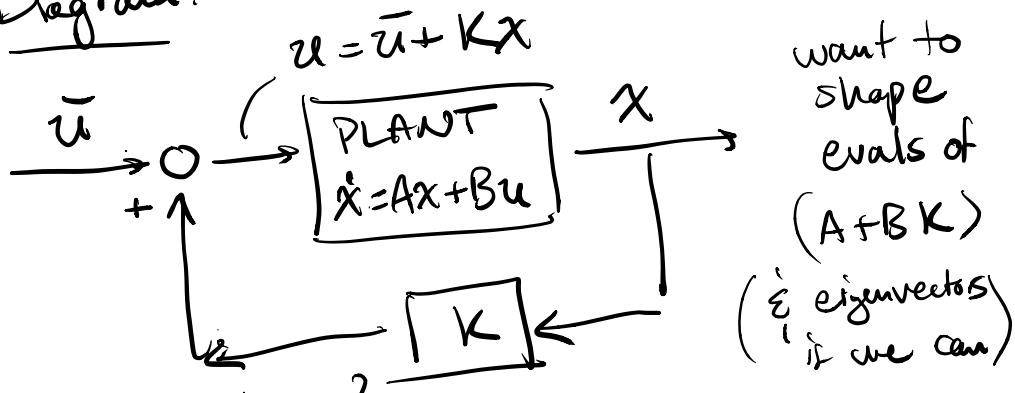
If  $\lambda_1 \neq \lambda_2$

but if  $\lambda_1 = \lambda_2$  then

## FEEDBACK CONTROL & OBSERVER DESIGN:

$$\dot{x} = Ax + Bu \quad \text{want } u = \bar{u} + Kx \Rightarrow \dot{x} = (A+BK)x + B\bar{u}$$

Block Diagram:



What if no access to  $x$ ?

measurement  $y = Cx$  where  $C$  is not invertible

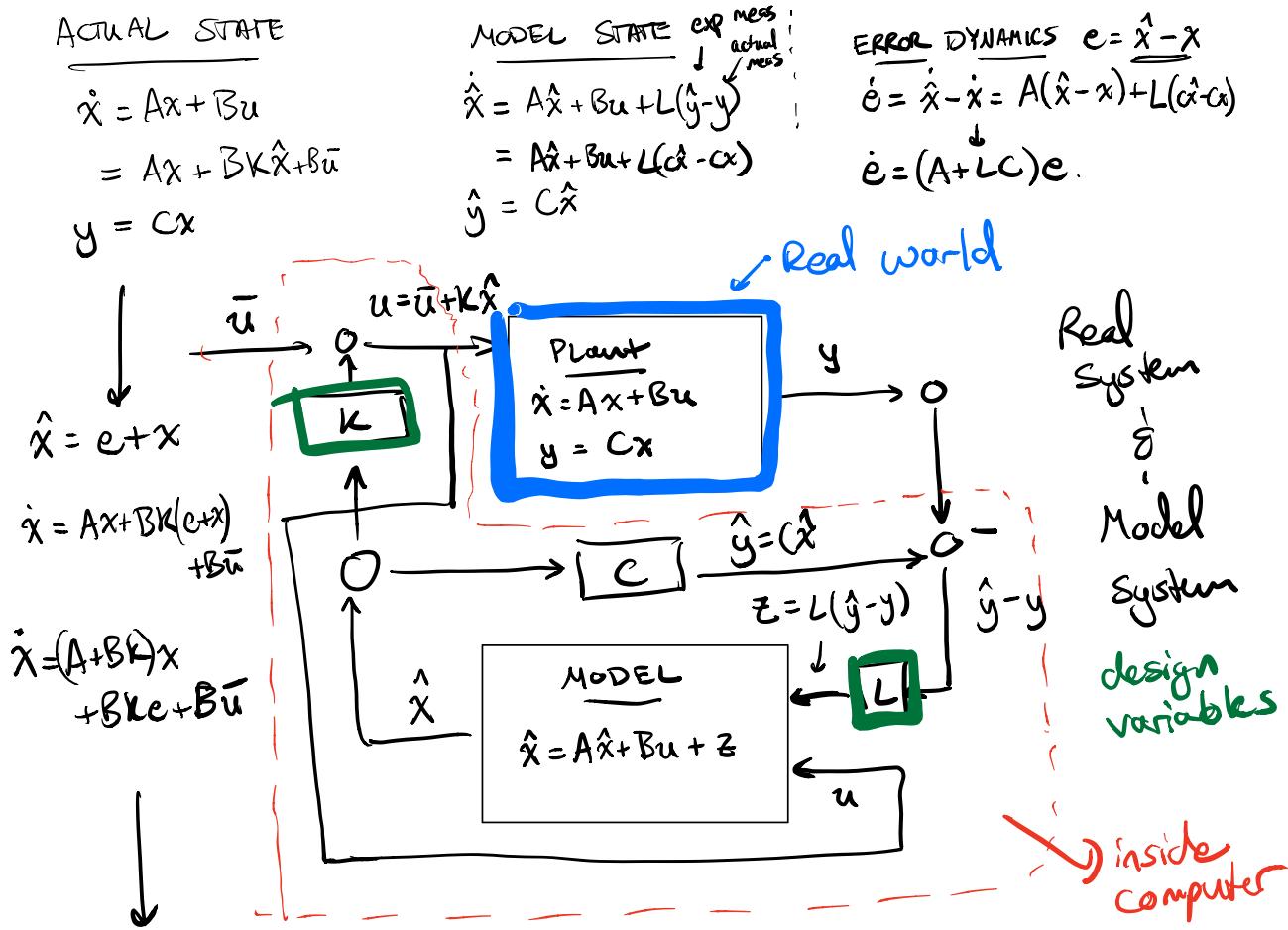
1. Model state:  $\hat{x}$

2. Use  $y$  as input  $\therefore$

to the model  
dynamics  
to drive  $\hat{x}$  to  $x$

3. Use control  $u = \bar{u} + K\hat{x}$

observer  
design



Full Dynamics: (in terms of  $x$  &  $e$ )

$$\begin{bmatrix} \dot{x} \\ \dot{e} \end{bmatrix} = \underbrace{\begin{bmatrix} A + BK & BK \\ 0 & A + LC \end{bmatrix}}_{\text{evals of } A+BK \text{ & } A+LC} \begin{bmatrix} x \\ e \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} \bar{u}$$

evals of  
this full system  
matrix just depend on

evals of  $A+BK$   
&  
evals of  $A+LC$

$\Rightarrow$  design  $K$  to stabilize  $A+BK$   
design  $L$  to stabilize  $A+LC$  separately

$\Rightarrow$  separation principle

mathematically the same  $A+BK \leftrightarrow A^T+C^T L^T$

How to pick  $K \in L$ :

simplest case where  $B \in \mathbb{R}^{n \times 1}$  ( $C \in \mathbb{R}^{1 \times n}$ )

$\Rightarrow$  choose the evals of the closed loop system.

picking evals  $\rightarrow$  choosing <sub>loop</sub> characteristic polynomial

want  $\det(\lambda I - A - BK) = \prod_i (\lambda - \lambda_i) = \lambda^n + \beta_{n-1}\lambda^{n-1} + \dots + \beta_1\lambda + \beta_0$

design choice  $\xrightarrow{\text{can compute}}$

Assume  $\det(\lambda I - A) = \lambda^n + \alpha_{n-1}\lambda^{n-1} + \dots + \alpha_1\lambda + \alpha_0$

pick  $K$  to change char poly from  $\underbrace{\quad}_{\text{given}}$

$\textcircled{1} \rightarrow \textcircled{2}$

Consider system of form  $\dot{z} = \bar{A}z + \bar{B}u$

where  $\bar{A} = \begin{bmatrix} -\alpha_{n-1} - \alpha_{n-2} - \dots - \alpha_1 - \alpha_0 \\ 1 & 0 & & & 0 \\ 0 & 1 & & & \\ 0 & & \ddots & & \\ 0 & & & 1 & 0 \end{bmatrix}$   $\bar{B} = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$   $\leftarrow$  controllable canonical form

$$\det(\lambda I - \bar{A}) = \lambda^n + \alpha_{n-1}\lambda^{n-1} + \dots + \alpha_1\lambda + \alpha_0$$

if we choose  $\bar{K} = [\alpha_{n-1} - \beta_{n-1} \dots \alpha_0 - \beta_0]$

use this gain  $\rightarrow$  closed loop  
char poly is  
as we want

Question :

can we find a similarity  
transform that  
converts our original  
system to this form

$$\dot{x} = Ax + Bu$$

want  $T$  invertible

$$\text{s.t. } x = Tz$$

Answer : yes if the  
system is  
controllable

$$T^{-1}AT = \bar{A} \quad ; \quad T^{-1}B = \bar{B}$$

Note:  $[\bar{A}^{n-1} \bar{B} \dots \bar{A}\bar{B} \bar{B}]$  is always invertible  
if  $T$  exists ... then we have

$$\underbrace{[\bar{A}^{n-1} \bar{B} \dots \bar{A}\bar{B} \bar{B}]}_{\bar{M}} = T^{-1} \underbrace{[A^{n-1} B \dots AB B]}_M$$

if  $M$  is invertible  $\Leftrightarrow$  the system is controllable

then ... 
$$T^{-1} = \bar{M}M^{-1}$$
  $\leftarrow$  similarity transform

Feedback:  $Kx = KTz = \bar{K}z$

$$\Rightarrow K = \bar{K}T^{-1} = \bar{K}\bar{M}M^{-1}$$

- pole placement using controllable canonical form

- another version of  
this is Ackermann's Formula

what if  $B \in \mathbb{R}^{n \times m}$ ?

- multiple choices for  $K$  that give  
the desired eigenvalues  $\rightarrow$  freedom to  
choose eigenvectors

- place command works multi input  
systems.  
pick eigenvalues.

$\rightarrow$  chooses eigenvectors to  
minimize the condition # of  $X$   
where the cols of  $X$  are the eigenvectors  
of  $A+BK$

$$\begin{aligned} X^T X &= \begin{bmatrix} -x_1^T \\ -x_n^T \end{bmatrix} \begin{bmatrix} x_1 & \dots & x_n \end{bmatrix} \\ &= \begin{bmatrix} x_1^T x_1 & \dots & x_1^T x_n \\ x_n^T x_1 & \dots & x_n^T x_n \end{bmatrix} \end{aligned}$$

↳ defines the shape of  $X$

Polar Decomposition: if  $X$  is square invertible ...

$$X = \underbrace{X}_{\substack{\text{ROT} \in \\ \text{REFLECTION}}} \underbrace{(X^T X)^{-1/2}}_{\substack{\text{pos def} \\ \text{determined} \\ \text{by relative} \\ \text{shape of cols}}} = \underbrace{(X X^T)^{1/2}}_{\substack{\text{pos} \\ \text{def} \\ \text{by relative} \\ \text{shape of} \\ \text{rows}}} \underbrace{(X X^T)^{-1/2} X}_{\substack{\text{rot} \in \\ \text{reflection}}}$$

like a rotation  
but might not  
have determinant  
of 1

like complex #5  $z = r e^{i\phi}$

$$X = \underbrace{R}_{\substack{\text{rot. reflection}}} \underbrace{P}_{\substack{\text{pos def}}}$$

Condition #

Singular Value Decomposition

for any  $X \in \mathbb{C}^{n \times m}$

$$X = U \sum_{i=1}^m \sigma_i V_i^*$$

$$U \in \mathbb{C}^{n \times n}, \Sigma \in \mathbb{C}^{m \times m}, V \in \mathbb{C}^{m \times m}$$

another rotation Stretching first rotation

$\Sigma$ : diagonal & positive

$$\Sigma = \begin{bmatrix} \sigma_1 & 0 \\ 0 & \sigma_m \end{bmatrix}$$

$\sigma_i$ : non zero evals of  
 $(X^T X)^{1/2} \in (X X^T)^{1/2}$   
or equivalently  
square roots of the evals  
of  $X^T X \in X X^T$

SVD: works on matrix of any dimension

$$X = [U_1 | U_2] \begin{bmatrix} \bar{\Sigma} & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_1^* \\ V_2^* \end{bmatrix} \Rightarrow U_1: \text{orthonormal basis for } R(X)$$

Condition #  $\frac{\sigma_{\max}(X)}{\sigma_{\min}(X)}$

$U_2: \text{orthonormal basis for } N(X^*)$

$V_1: \text{orthonormal basis for } R(X^*)$

$V_2: \text{orthonormal basis for } N(X)$

If  $X$  is invertible:

$$\bar{X}^{-1} = (U \Sigma V^*)^{-1} = V \bar{\Sigma}^{-1} U^*$$

$$\bar{\Sigma}^{-1} = \begin{bmatrix} \bar{\Sigma} \end{bmatrix} = \begin{bmatrix} \frac{1}{\sigma_1} & & \\ & \ddots & \\ & & \frac{1}{\sigma_k} \end{bmatrix} \text{ if } \sigma_{\max} \gg \sigma_{\min}$$

$$\begin{bmatrix} \text{huge} \\ \approx \\ \text{small} \end{bmatrix}$$

Closed loop matrix

$$A+BK = X D \bar{X}^{-1} \quad \text{if } X \text{ is poorly conditioned}$$

= relatively close to 0

$$(A+BK)X(0) = X D \bar{X}^{-1} X(0)$$

pick  $D$  to have evals you want the amplitude of  $\bar{X}X(0)$  could be big

if  $X$  is poorly conditioned.

singular value then  $\bar{X}^{-1}$  gets huge in certain directions

place command for multi input systems chooses  $X$  to be as well conditioned as possible.

« Robust Pole Assignment in Linear State Feedback (1985)  
Kautsky, Nichols  
Van Dooren.

## LINEAR TIME VARYING SYSTEMS & LINEARIZATION

### CONTINUOUS TIME

$$\dot{x}(t) = A(t)x(t) + B(t)u(t)$$

State transition Matrix:  $e^{A(t-t_0)} \rightarrow \phi(t, t_0)$

solution to  $\dot{\phi}(t, t_0) = A(t)\phi(t, t_0)$   
with i.c.  $\phi(t_0, t_0) = I$

- $\phi(t, t_0) = I$
- $\phi(t_0, t) = \phi^{-1}(t, t_0)$   $\phi(t, t_0)$ : map between initial cond. and cond. at time  $t$
- $\phi(t, t_0) = \phi(t, t')\phi(t', t_0)$
- $\dot{\phi}(t, t_0) = A(t)\phi(t, t_0)$

$$x(t) = \phi(t, t_0)x(t_0)$$

+ no control input

$$x(t) = \phi(t, t_0)x(t_0) + \int_0^t \phi(t)\mathbf{B}(t)u(t)dt$$

General form for computing  
this is Peano-Baker  
series  $\rightarrow$  nested integrals  
ugly.

### LINEARIZATION OF NONLIN. DYN

$$\dot{x} = f(x, u, t)$$

nominal control trajectory:  $\bar{u}(t)$

plug into dynamics  
to get nominal state:  $\bar{x}(t)$

solution to integrating the dynamics

will apply control  $u = \bar{u} + \Delta u = \bar{u} + K\Delta x$

addition to  
control to stabilize around trajectory

### DISCRETE TIME

$$x[t+1] = A[t]x[t] + B[t]u[t]$$

state transition matrix:  $A^t \rightarrow A[t] \times \dots \times A[0]$

$$x[t+1] = A[t] \dots A[0]x[0] + \sum_{\tau=0}^{t-1} A[\tau] \times \dots \times A[\tau+1] B[\tau] u[\tau] + B[t] u[t]$$

$$X(t) = \bar{X}(t) + \underline{\Delta X(t)}$$

perturbations  
to the state

$$\dot{\bar{X}} = \dot{\bar{X}} + \dot{\Delta X} = f(\bar{x} + \Delta x, \bar{u} + \Delta u, t)$$

$$\dot{\bar{X}} + \dot{\Delta X} = f(\bar{x}, \bar{u}, t) + \frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t} \Delta x + \frac{\partial f}{\partial u} \Big|_{\bar{x}, \bar{u}, t} \Delta u$$

$$\dot{\Delta X} = \left[ \frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t} \Delta x + \frac{\partial f}{\partial u} \Big|_{\bar{x}, \bar{u}, t} \Delta u \right] \Rightarrow$$

LIN. TIME VARYING PERTURBATION DYNAMICS

IN THE LTI CASE:

$$A \text{ in continuous time} \rightarrow e^{At}$$

discrete time.

$$\frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t} \text{ in cont time} \rightarrow I + \Delta t \frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t}$$

$$\begin{aligned} \Delta X[t+1] &= \Delta X[t] + \Delta t \frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t} \Delta x[t] \\ &\quad + \Delta t \frac{\partial f}{\partial u} \Big|_{\bar{x}, \bar{u}, t} \Delta u[t] \\ &= \left[ I + \Delta t \frac{\partial f}{\partial x} \Big|_{\bar{x}, \bar{u}, t} \right] \Delta x[t] \end{aligned}$$

FORWARD EULER INTEGRATION. +  $\Delta t \frac{\partial f}{\partial u} \Big|_{\bar{x}, \bar{u}, t} \Delta u[t]$

$\Leftarrow$  first terms in the Taylor exp of the state trans matrix.

## LYAPUNOV STABILITY THEORY:

IDEA: define an "energy" function for a system & then show that it decreases along trajectories of the system  $\rightarrow$  way to show stability.

used in linear systems & nonlinear systems  
 $\rightarrow$  related to linear quadratic regulator (LQR)

the cost-to-go in the LQR problem acts like a Lyapunov function

LEMMA: Function  $F(t)$  s.t.

$$\dot{F}(t) \leq \lambda F(t) \Rightarrow F(t) \leq e^{\lambda t} F(0)$$

PROOF: define  $u(t) = e^{-\lambda t} F(t)$

$$\text{take deriv. } \frac{d}{dt} u(t) = -\lambda e^{-\lambda t} F(t) + e^{-\lambda t} \dot{F}(t) \leq -\underbrace{\lambda e^{-\lambda t} F(t)}_{\text{terms cancel}} + \underbrace{\lambda e^{-\lambda t} F(t)}_{\dot{F}(t)}$$

$$u(t) \leq 0$$

$$u(t) = e^{-\lambda t} F(t) \leq u(0) = F(0)$$

$$\Rightarrow e^{-\lambda t} F(t) \leq F(0) \Rightarrow F(t) \leq e^{\lambda t} F(0)$$

If we know the derivative of a scalar function is always bounded by some scalar times the function value  $\rightarrow$  then we can use that scalar value  $\lambda$  as decay rate that bounds the function

$\rightarrow$  useful when  $\lambda < 0$

because  $e^{\lambda t} \rightarrow 0 \Rightarrow F(t) \rightarrow 0$

$F(t)$ : energy type function

Apply to linear systems:

Consider function  $F(x(t)) = x(t)^T P x(t)$  where  $P=P^T > 0$   
is symmetric PD

and  $x$  evolves according to  $\dot{x} = Ax$

$$\begin{aligned}\dot{F} &= \frac{\partial F}{\partial x} \dot{x} = x^T P \dot{x} + \dot{x}^T P x \quad \leftarrow \\ &\text{"Lie derivative"} = x^T P A x + x^T A^T P x = x^T (A^T P + P A) x\end{aligned}$$

Note: for a matrix  $Q = Q^T > 0$

$$\lambda_{\min}(Q) |x|^2 \leq x^T Q x \leq \lambda_{\max}(Q) |x|^2$$

suppose  $A^T P + P A = -Q$  for some  $Q = Q^T > 0$

$$\begin{aligned}\dot{F}(x(t)) &= -x^T Q x \leq -\lambda_{\min}(Q) |x|^2 \leq -\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} x^T P x \\ &\quad \downarrow \quad \downarrow \\ &\text{from } \lambda_{\min}(Q) |x|^2 \leq x^T Q x \quad \frac{x^T P x}{\lambda_{\max}(P)} \leq |x|^2\end{aligned}$$

Note: the negative signs.

$$\dot{F}(x(t)) \leq -\underbrace{\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)}}_{< 0} F(t) \Rightarrow F(t) \leq e^{-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} t} F(0)$$

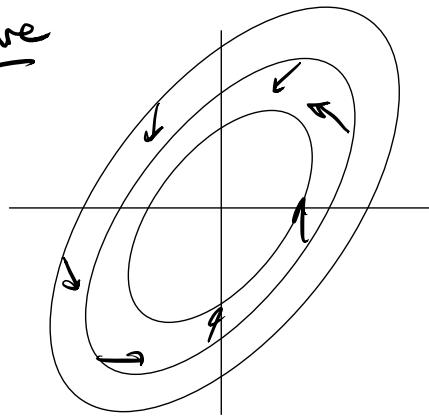
Note:  $F(x(t)) = x^T P x > 0$  for  $x \neq 0$

$$F(0) = 0$$

$$\text{since } -\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} < 0 \Rightarrow e^{-\frac{\lambda_{\min}(Q)}{\lambda_{\max}(P)} t} F(0) \rightarrow 0 \Rightarrow F(x(t)) \rightarrow 0$$

since  $F = 0$  only at  $x(t) = 0 \rightarrow x(t) \rightarrow 0$

Picture



If we show  $\dot{x}$  always makes  $F(x)$  decrease then we can use this to show stability.

