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DEPARTMENT OF ELECTRICAL AND COMPUTER ENGINEERING



WaveSphere: Final Report

A REPORT SUBMITTED AS A PARTIAL REQUIREMENT OF THE MICROPROCESSOR INTERFACING COURSE ICOM-5217

by

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1. Introduction

Although waves are abundant at sea and everyone who has been near a shoreline has seen and interacted with a wave, most people don't think about the wave-breaking phenomena when enjoying their time in the water. However, this topic is very important for the researchers at the Fluid Mechanics and Ocean Engineering Laboratories at the University of Puerto Rico at Mayagüez, which are directed by Dr. Miguel Canals. The natural physics and motion dynamics of the wave-breaking phenomena have not been thoroughly studied because of the difficulty encountered when trying to measure the characteristics of the waves.

A novel way to study these dynamics is by developing an instrument, also referred to from hereon as drifter, that will ride with the waves and take measurements during the wave-breaking process. This is the approach that the researches have taken as part of the NSF Funded project titled "Lagrangian Observations of Turbulence in Breaking Waves". Currently, the researchers working on this project have an assembled prototype with which they have been performing experiments. This drifter consists of a small spherical plastic casing which houses a series of sensors, a microSD card, a microcontroller and power management components.

However, their prototype has a series of issues that need to be addressed so that the overall functionality is improved. One example of a current issue is that design being used has an external button to activate the sphere. The way in which the button was mounted on the plastic spherical casing allowed for the water to leak inside the casing, damaging the electronic components. Another issue with the current design is the lack of location information. Once the drifter has been deployed and the experiment has concluded, the researchers must retrieve the drifter. However, they have lost drifters because the waves have taken them away, making them impossible to find.

The objective of this project is to improve the overall design of the drifter currently being used by the researchers by addressing the previously mentioned issues, as well as other issues not mentioned. Because the drifters will have more capabilities, a base station must also be designed so as to allow for easy management of the individual drifters through a custom application displayed to the user via a graphical interface.

This work presents the design process of a spherical drifter that will aid the researchers in taking the aforementioned measurements. A system overview is presented so as to give the reader a better idea of the solution proposed by this work. This is followed by a thorough discussion of the hardware and software design process. Figures, tables and calculations are presented along the way to support the claims made by this work and aid the reader in understanding certain aspects of the design process. Finally, a brief recommendation of work that could be done in the future to improve the current prototype is given.

¹From hereon, the word researchers and users will be used interchangeably.

2. Theoretical Background

In Progres...

In fluid mechanics, there are two ways to describe flow: Eulerian and Lagrangian. The Eulerian approach describes what is happening at a given location for a given time, whereas the Lagrangian approach describes the history of the particle exactly [2]. Looking at these two terms from a sensors point of view, an Eulerian sensor would be at a fixed position recording data over time, whereas a Lagrangian sensor would move with the particles of the fluid while recording data. It is easy to see that for the study of wave breaking phenomena a Lagrangian sensor would be preferable, as the path of the waves are unpredictable and an initial location cannot be determined before the event occurs.

The drifters are to be released within breaking waves to measure important variables in this process.

It was determined in [3] that the sphere diameter to wave height ratio should be minimize, which is why a spherical 7.5 cm diameter capsule was assembled.

3. System Overview

The proposed system consists of two parts, a spherical drifter which will be deployed right into the waves and a base station that will be used to control the drifters. The researchers that will use the drifters to conduct their experiments will use a personal watercraft (PWC) to deploy the drifters at the point where the wave breaks and retrieve them after the experiment has concluded. Figure 1 shows the scenario of a single experiment. The base station will reside in the PWC and the researchers will throw the drifters into an emerging wave so that when it breaks the drifter is already recording data from the sensors.

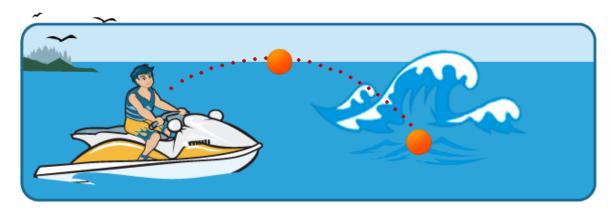


Figure 1: A graphical depiction of the deployment process of the drifters. Image adapted from [1].

3.1 Drifters

The drifters consist of a plastic sphere of about 7.5cm in diameter inside which all the electronic components reside. The plastic sphere can be opened and closed: the two halves of the sphere are threaded at the rim near the diameter so that they can be screwed in together. The drifters are equipped with various sensors, GPS and wireless modules, among other components. A detailed explanation of the components that make up the drifters follows.

Sensors

The drifters are equipped with an accelerometer to measure the changes in acceleration of the device, a gyroscope to measure the changes in orientation and a magnetometer to measure the orientation with respect to the Earth's magnetic north. All three sensors take data from three axes. Together, they make up what is known as a nine degree-of-freedom inertial measurement unit. As previously mentioned, the data collected from these three sensors will be used to determine the path that the drifter has taken within the wave.

GPS and XBee Modules

After an experiment has concluded, the users must manually retrieve the drifters from the water. To aid in this process, the drifters are equipped with a GPS and an XBee module. After all the necessary data has been collected, a process which takes about 30 seconds, the drifter will acquire its current location and send it to the base station through the Xbee module. This will allow the users to easily locate and retrieve the devices.

The Xbee Module also serves to receive commands from the base station in order to change between operating modes. The different operating modes of the sphere can be found in Section 9. It can also be used to wirelessly retrieve the acquired data from the drifter to the base station.

Battery Powered

Because of the necessity for portability, the drifters are battery powered. Each device is equipped with a Lithium-Ion 3.7V rechargeable battery. There is also a micro-USB port that can be used to recharge a depleted battery. In order to make the drifter air-tight so that no water can enter the spherical plastic case, the port used to recharge the battery resides inside the sphere, which is why it must be twisted open in order to access the port.

RF Wakeup Module

Since the plastic sphere has to be air-tight, adding a physical button or some other type of mechanism on the outside of the sphere in order to activate the drifters proved to be unfeasible as this could potentially create leaks which would damage the electronic components inside. In order to solve this problem, the drifter is equipped with an RF receiver and antenna that responds to 125kHz signals, the same ones found in RFID card

readers. The purpose of this module is to wake up the system and activate the drifter once the 125kHz signal has been applied. It replaces an external button or other external actuation mechanism.

SD Card and Mass Storage

The data acquired is stored in a microSD card which is on board the drifters. There are three ways to retrieve the data from the drifters: wirelessly through the XBee module, by removing the SD card and inserting it into a card reader connected to a computer or through the on board micro-USB port. The drifters are equipped with a module that allows them to behave like a mass storage device when connected to a computer. Thus the users can browse the files just as they would when browsing through the files in a thumb drive.

Indicator LEDs

There are four LED indicators that serve as the user interface. Each one has a different function as follows:

- **Red LED** When the red LED is on, it means that the system is powered on. If it starts flashing, it means that the battery level is low.
- **Blue LED** When the drifter is connected through the micro-USB port, the blue LED will turn on when the battery is charging. Once the battery is fully charged, the LED will turn off.
- **Green LED** The green LED will be on when the XBee ZB module is turned on and ready to transmit or receive data.
- **Amber LED** The amber LED will turn on when the GPS module has acquired a fix, or when it is able to acquire satellite signals to determine its position.

3.2 Base Station

The base station consists of an RFID reader, an XBee module and a computer on which a custom application with a graphical user interface (GUI) will reside. The GUI can manage and communicate with several drifters at the same time. The RFID reader and XBee ZB are powered through a USB port on the computer. A brief explanation of each of these components and their role on the system follows.

RFID Reader

The RFID Reader is used to generate a 125kHz signal that will be received by the RF Wakeup module inside the drifter. Once the drifter comes within a certain proximity of the RFID reader, it will be activated by the wakeup module.

XBee Module

The XBee module on the base station is the counterpart of that found inside the drifter:

it completes the communication path between the drifters and the host computer. Through this module, the host computer will be able to send commands to the drifters as well as receive the experimental data sent by the drifters to the base station. The module will then in turn pass the data to the host computer, completing the data transaction.

Graphical User Interface

The researcher's current experimental setup allows them to have a computer on board the PWC without risking water damage. The computer on the PWC is loaded with a custom application that consists of a Graphical User Interface (GUI). This application allows the users to communicate with the drifters in a simple manner. Through a series of windows and buttons the user can intuitively navigate through the application in order to perform tasks such as changing the operating modes of the spheres.

The full capabilities of the GUI along with instructions on how to navigate through it and perform the various tasks for which it was developed can be found in the User's Guide which located in Appendix A.

4. Block Diagram

Figure 2 shows the block diagram for each of the drifters while Figure 3 shows the block diagram for the base station. Both diagrams contain the model numbers of the components and, in the case of the drifter block diagram, the types of connections required to the microcontroller unit (MCU) and the amount of lines needed for each connection. A list of the components in each block diagram along with a brief explanation for each one follows.

Drifter Block Diagram

- 1. **Microcontroller** Needed in order to be able to control and establish the communication between components as well as process the output of the sensors.
- 2. **Battery** Required to provide the necessary power to the drifters because the electrical components are enclosed by a sphere.
- 3. **Power Management Circuit** Composed of an LDO, a battery charger and a battery meter. It is used to regulate the power provided by the battery, re-charge the battery once it has been depleted and to measure the amount of charge left on the battery.
- 4. **GPS Module** Needed in order to know the precise location of the drifters when the user has to recover them after they have been thrown at sea for an experiment.
- 5. **Gyroscope** Used to determine the rate of change of the orientation of the drifter while being carried by a wave.
- 6. **Accelerometer** Used to measure the acceleration of the drifter while being carried by the waves.
- 7. Magnetometer Used to determine the orientation of the drifter with respect to the

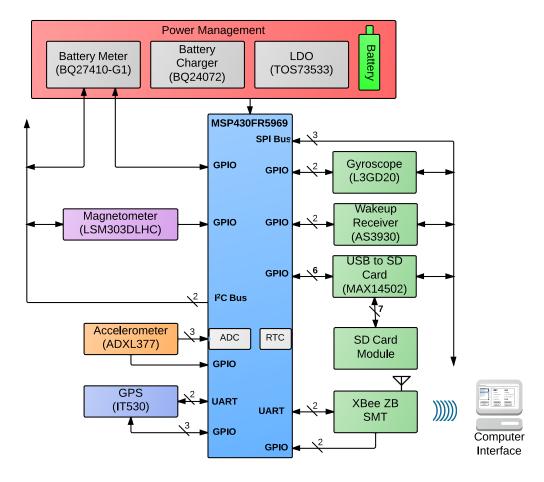


Figure 2: Block Diagram for the Drifter

Earth's magnetic north while it is being carried by a wave.

- 8. **Analog to Digital Converter (ADC)** Needed in order to take the data from the accelerometer, which has an analog output, and convert it to digital signals so that the MCU can read them. It is integrated within the MCU.
- 9. **SD Card and SD to USB Converter** The SD Card is used to save the data captured by the sensors during an experiment. The SD to USB converter will be used to allow the drifter to function as a mass storage device when connected to a Host computer via USB.
- 10. **XBee ZB Module** Used to connect the spheres with a central base so that data can be retrieved without having to open the spheres.
- 11. **RF Wakeup Module** Used to wirelessly wake up the drifter from low power mode via an RF signal.

Base Station Block Diagram

1. **XBee ZB Module** - Used to communicate with the drifters in order to send commands to switch operating modes and retrieve collected data.

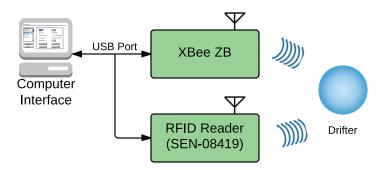


Figure 3: Block Diagram for the Base Station

- 2. **RFID Reader** Used to generate the 125kHz signal required by the RF Wakeup module in the drifters to wake them up from low power mode.
- Computer Used to run a custom application that will be used to send commands
 and data to the drifters through the XBee. A USB port in the computer will power
 the other devices in the base station.
- 4. **Power Management Circuit** Composed of an LDO, a battery charger and a battery meter. It is used to regulate the power provided by the battery, re-charge the battery once it has been depleted and to measure the amount of charge left on the battery.

5. Power Analysis

The power analysis consists of four main parts: logic compatibility, driving capability, power supply design and battery life estimate. The purpose of this analysis is to ensure that power requirements for each component are satisfied in order to guarantee their proper functionality. A supporting thermal analysis will be performed on selected ICs.

5.1 Logic Compatibility

Table 1 shows all the digital components in the system along with their input and output digital voltage levels. Only two digital components communicate with each other: the SD Card to USB converter IC and the SD Card itself. It is easy to see from Table 1 that the logic voltage levels between these two devices are compatible. In addition to this, all components communicate with the MCU. It can also be seen that all the devices are logically compatible with the MCU except for the battery gauge, which communicates with the MCU through an I^2C interface and has a V_{DD} of 2.5V. In order to make them compatible, a bi-directional logic level shifter from Texas Instruments was used and can be found in the schematic. It can be seen in the table that by using the aforementioned level shifter, communication between the battery gauge and the MCU is now possible.

Table 1: Component Logic Levels and I/O Currents

| Component | V_{DD} | V_{IH} | V_{IL} | V_{OH} | V_{OL} | I_{OUT} | I_{IN} | I_{LEAK} |
|----------------------------|----------|----------|----------|----------|----------|--------------------|----------|------------|
| MSP430FR5969 ² | 3.3 | 2.1 | 0.75 | 3.2 | 0.2 | 45 mA ³ | 50 nA | 50 nA |
| Magnetometer ⁴ | 3.3 | 2.64 | 0.66 | 3.3 | 0 | 3 mA | 10 μΑ | 10 μΑ |
| XBee | 3.3 | 2.64 | 0.66 | 2.706 | 0.594 | 4 mA | 0.5 μΑ | 0.5 μΑ |
| RF Wakeup | 3.3 | 1.914 | 0.99 | 2.9 | 0.4 | 21 mA | 100 nA | 100 nA |
| Gyroscope | 3.3 | 2.64 | 0.66 | 2.64 | 0.66 | 100 μΑ | 10 μΑ | 10 μΑ |
| GPS | 3.3 | 2 | 0.8 | 2.4 | 0.4 | 8 mA | 10 μΑ | 10 μΑ |
| Battery Gauge ⁵ | 2.5 | 1.2 | 0.6 | 2 | 0.4 | 3 mA | 10 μΑ | 0.3 μΑ |
| SD Card ⁶ | 3.3 | 2.06 | 0.83 | 2.48 | 0.41 | 100 μΑ | 10 μA | 10 μA |
| Power Switch | 3.3 | 2.2 | 1.1 | 3.3 | 0 | 10 mA | 0 mA | 0.3 μΑ |
| SD Card to USB | 3.3 | 2.06 | 0.83 | 2.48 | 0.41 | 100 μA | 2 μΑ | 1 μΑ |
| Converter | | | | | | | | |
| Level Shifter ⁷ | 2.5 | 1.7 | 0.7 | 2.5 | 0 | 100 μΑ | 20 μΑ | 10 μΑ |

5.2 Driving Capability

In order to ensure that no component draws more current than the one its driver can provide, a weakest driver analysis should be performed. Table 1 shows a list of the available currents found in the data sheets and other sources. The components and their connections are shown in the block diagram depicted in Figure 2.

Since I^2C is a standard, there would be no problems if the level shifter was not present. However, since this component is the weakest driver, the analysis must be performed. The output current of this component is $100 \,\mu\text{A}$ in order to maintain the voltage levels specified in Table 1. It can be seen that this current is greater than the sum of input currents of the components connected to the bus: $10 \,\mu\text{A}$ for the Gyroscope and $50 \,\text{nA}$ for the MCU.

Since the components connected through UART and Software UART are point to point connections and since the MCU has such a low input and leakage current, the Xbee and GPS modules will not have a problem driving the MCU. Finally, for the SPI Bus, the weakest driver is the Gyroscope with an output current of $100 \mu A$. It can be seen from Table 1, that this current is greater than the sum of input currents for the other components: $10 \mu A$ for the SD Card to USB Converter and 50 nA for the MCU.

With this analysis, one can conclude that all ICs can drive their respective loads

²Values used are for the MSP430FR572x as they are not available for the selected microprocessor.

³In full-drive mode

⁴Currents obtained from [4]

⁵Input and output currents obtained from [4]

⁶Voltages obtained from [5]

⁷Values for V_{OH} and V_{OL} taken at 100 μ A since the input and output current of the Battery Gauge does not exceed 10 μ A.

5.3 Power Supply Design

In order to design the power supply that will be used by the system, the worst case quiescent current of each component should be taken into account. Although not all components will be operating at the same time, it is ensured that the system will continue to function properly for the worst possible case by performing the analysis in this manner. To ensure proper operation of the system, the Low-Dropout Regulator (LDO) must supply enough current for the entire system. Table 2 shows a list of components along with the worst case quiescent current of each of them. By adding all the current, a maximum current consumption of 181 mA was determined. The LDO is rated for a maximum output of 500 mA, which is well above the determined usage. In order to complete the power supply circuit, a USB Battery Charger and a Battery Meter were added as well. Note that since the level shifters are powered by the 2.5V regulated output of the Battery Meter, they have not been included in these calculations.

Table 2: Worst Case Quiescent Currents for components

| Component | $I_{DD(Active)} (\mu A)$ |
|----------------------|--------------------------|
| MSP430FR5969 | 1600 |
| 3-Axis Accelerometer | 300 |
| Magnetometer | 110 |
| XBee | 45000 |
| RF Wakeup | 2.7 |
| Gyroscope | 6100 |
| GPS | 26140 |
| SD Card | 100000 |
| Power switch | 1 |
| SD to USB | 37 |
| LDO | 65 |
| Battery Charger | 1500 |
| Battery Meter | 103 |
| Total | 180958.7 |

5.4 Thermal Analysis

A thorough thermal analysis was performed on the MCU and all the power management ICs to determine whether they would exceed the thermal limits of their package under regular operation in our system. The expected operating junction temperature was calculated using the junction-to-ambient thermal resistance and the power dissipated by each IC. It was determined that no additional heat dissipation technique as needed to guarantee the proper operation of the ICs since all the calculated junction temperatures were well below the maximum operating junction temperature specified in the manufacturer's datasheets. The thorough and detailed analysis can be found in Appendix B.

6. Timing Analysis

Old timing analysis, copied because it had a good format, however must be updated with the new information. Need help from Samuel. Must add information on SW UART

The timing analysis consists of three main parts: Time bases, Point-to-point communication, and analog considerations. The purpose of this analysis is to ensure that no signal is transmitted at a faster frequency than the one its receiver can read, thus guaranteeing communications functionality and interoperability between all components and the MCU.

6.1 Time bases

This section compares the maximum external clock frequencies of all components and their communication ports to make sure that no component will be overclocked by the MCU and that all synchronous communication can be performed at the speed of the MCU's clock. Table 3 shows the frequency specifications for the components. Since the sample frequency will be a relatively low 250Hz, there is complete compatibility between the MCU and all components. The MCU can run at a clock frequency of up to 16MHz. For I²C communications, the standard of 10-100kHz will be used, since all components are compatible with it. For SPI communications, a rate of up to 2MHz can be used, since the slowest device, the RF wakeup receiver, operates at this frequency. The only component that will be communicating with the MCU through UART is the GPS receiver, which will be communicating at a 9600 baud rate and tolerates a 10% error.

Timers Two timers will be needed for sampling. The first timer will control the sample frequency for all the components. In order to sample at an accurate frequency of 256Hz, an external crystal with a low frequency of 38.400kHz will be used. To achieve this, the crystal will be connected to one of the timers, and the terminal count will be set to 150 with a prescale divider of one. The second timer will control the sampling time of 30 seconds. The prescaler of this timer will be set to 1 and the terminal count will be set to 38,400. 30 counts of the terminal register will produce the interrupt that will conclude the sampling mode.

Crystal Oscillators The reason why a 38.400kHz crystal was chosen is because the GPS communicates through UART with a 9600 baud rate. If a standard 32.768kHz crystal is used instead, the frequency divider would be 3.4, which would produce an effective baud rate of 9637.65bps. This translates to a maximum error of 17.19%, which is unacceptable for maintaining a stable communication link with the GPS module. This problem is solved by using a 38.400kHz crystal, which would produce an effective baud rate of 9600bps with 0.00% error with a frequency divider of 4. The use of a 38.400kHz crystal will not affect

real time keeping nor sampling rate, because a 256Hz signal can be obtained by counting 150 cycles of the crystal, and a second can be obtained by counting 38400, both of which fit into a 16bit timer compare register.

Additionally, a 12MHz crystal was added to comply with the USB-to-SD card reader specifications. The card reader comes preprogrammed to accept a 12MHz clock input that is used for the USB and SD subsystems.

Table 3: Component Operating Frequencies

| Component | Protocol | Frequency |
|---------------|------------------|---------------------|
| MCU | - | 4, 8, 12, or 16 MHz |
| ADC | - | 200ksps |
| Accelerometer | Analog | 500Hz |
| Battery Gauge | I ² C | 10-100kHz |
| Magnetometer | I ² C | 0-100kHz |
| Gyroscope | SPI | 0-10MHz |
| RF Wakeup | SPI | 0-2MHz |
| SD card | SPI | 0-25MHz |
| GPS | UART | 9,600 baud |
| Xbee | UART | 9,600 baud |

6.2 Point-to-point communication

This section outlines the minimum requirements for timing signals of the devices connected through GPIO. Table 4 shows the timing requirements for the components. These timing signals do not include forms of serial communication, such as UART, SPI and I²C. If a device requires a specific setup or hold time, the solution would be to set up a timer and count the specific number of clock ticks that the device requires.

need to update to add missing signals and remove the ones not being used

Table 4: Signal Timing Requirements of Components

| Signal | Time Required | |
|--------------------|---|--|
| GPS_DR (DR_INT) | Needs to be toggled by low-high-low with | |
| | >10ms pulse length | |
| GPS_FIX (UI_FIX) | Signal outputs 1s pulse every 2s during valid | |
| | fix condition | |
| GYR_CS (CS) | Setup time: 5ns, Hold time: 8ns | |
| GYR_DR (DRDY/INT2) | Interrupt: enabled until acknowledged by the | |
| | MCU | |

| Signal | Time Required |
|----------------------|--|
| MAG_DR (DRDY) | Interrupt: enabled when a new set of mea- |
| | surements are available |
| RF_WK (WAKE) | Not specified |
| RFWK_CS (CS) | Needs to be high as long as data needs to be |
| | read. 65 clock cycles to calibrate |
| SD_CD (HCRD_PRST) | Active when card present |
| SD_CS (CS) | Asserted 74 clock cycles |
| SU_BERR (!BERR/INT) | Low when error occurs, stays until error is |
| | cleared |
| SU_BUSY (!BUSY) | >100ms to complete enumeration/de- |
| | enumeration |
| SU_MODE (MODE) | Active during simple control |
| XB_DR (!DTR/SLEEP) | Not specified |
| XB_SLEEP (ON/!SLEEP) | Not specified |

6.3 Analog considerations

There is only one analog component in the system, the ADXL377 accelerometer. Care must be taken to ensure that the sampling rate of the MCU's ADC can be set to twice the frequency of the analog signal and that the input voltage range of the ADC is enough to allow for the output voltage swing of the ADXL377. The ADXL377 can output data at a maximum of 1000Hz. This means that the MCU's ADC must be capable of sampling at a rate of at least 2ksps. The MSP430FR5969's ADC is capable of sampling at 200ksps, which is well above the required value. The acceptable input voltage range is specified to be from 0V to +Vcc. Since the ADXL377 output voltage swing ranges from 0.1V to 2.8V, the accelerometer's output can be sampled without suffering from clipping distortion. This makes the ADXL377 compatible with the MCU.

A second consideration should be made when interfacing with an analog component: slew rate compatibility. There is no documented specification of the ADC's slew rate in the MSP430FR5969's data sheet. However, since the output of the accelerometer varies around 6.5 mV/g, the change in amplitude in the input signal should be small enough so that there will not be any slew rate distortion.

7. Hardware Reliability and Professional Component

7.1 Design Criteria

The system was designed based on three main criteria: Power and Energy Consumption, Sustainability and Durability, and Data Integrity. Several decisions were made in the design process to accommodate for these three criteria. A discussion of how these criteria were addressed from a hardware perspective follows.

7.1.1 Power and Energy Consumption

In order to minimize energy consumption, all of the selected ICs have a low-power mode. The only component that doesn't have a low power mode is the accelerometer, however a power switch was introduced between the power source and the IC which can be controlled via one of the MCU's GPIO pins. This allows for the implementation of a low-power mode for this component.

Another consideration made was in the battery selection. The selected battery has a voltage rating of 3.7V, which is close to the desired power supply voltage of 3.3V. Since the system uses a linear regulator to regulate the power supply at 3.3V, the closer the gap between the battery voltage and the desired power supply, the less energy lost in the regulator as heat.

7.1.2 Sustainability and Durability

Because the drifters are meant to be used in the water, it is important that the plastic casing surrounding the electronic components be durable and able to withstand the large accelerations encountered in the wave-breaking process. At the same time, the internal components must be secured to the casing so that they don't move around inside the plastic casing.

There is currently a Mechanical Engineering student in charge of designing a new plastic casing for the spheres which will later be fabricated for the ongoing NSF funded research project. However, in order to contribute to this criteria, the designed Printed Circuit Boards (PCBs) have holes to allow spacers and screws to fasten the PCB to the casing. This will prevent the PCB from being lose and rattling around inside the casing.

7.1.3 Data Integrity

How are we protecting data integrity

7.2 Limitations

Because of the space constraint on this project and the amount of components that need to fit into such a small enclosure, a custom two-tiered PCB was designed to hold all the components. However, altering the design of this PCB to introduce new components to the drifter is time-consuming and expensive. This is a great limitation of this implementation because the product is intended for a research project. Since the manner in which the drifters are to be applied is fairly novel and has not been thoroughly explored, it is safe to say that this prototype might undergo several changes before obtaining a final and optimal device that can capture all the data required by the researchers. Thus, the inability to easily upgrade the design can be a great limitation.

8. Hardware Level of Completion

Table 5 shows a list of hardware components along with their respective level of completion (LoC).

Table 5: List of Hardware Components and Level of Completion

| Component | LoC |
|-----------------------|------|
| Accelerometer | 100% |
| Professor Annotations | |
| | |
| | |
| | |
| Battery Meter | 100% |
| Professor Annotations | |
| | |
| | |
| | |
| Battery Charger | 100% |
| Professor Annotations | |
| | |
| | |
| | |
| GPS | 100% |
| Professor Annotations | |
| | |
| | |
| | |
| Gyroscope | 100% |

| Component | LoC |
|------------------------------------|------|
| Professor Annotations | |
| | |
| | |
| Magnatamatar | 100% |
| Magnetometer Professor Annotations | 100% |
| Troicssor Annotations | |
| | |
| | |
| RF Wakeup | 100% |
| Professor Annotations | , |
| | |
| | |
| CD | 1000 |
| SD Professor Annotations | 100% |
| Professor Affilotations | |
| | |
| | |
| Voltage Regulator | 100% |
| Professor Annotations | j |
| | |
| | |
| Xbee | 100% |
| Professor Annotations | 100% |
| 1 101C5501 Allifotations | |
| | |
| | |
| | |

9. System Operation Chart

Update Flowcharts and verify whether this text still applies

Operating charts describe the modes of operation and the flow of the system without much detail. Figure ?? shows the system's main flowchart, which depicts how the device goes in and out of each of its operating modes. A general but brief overview of the different modes of operation follows.

When the system is powered up it will perform an initialization sequence, which includes initializing all GPIO ports and memory variables. It will also enable global interrupts and the RF wakeup receiver interrupt while keeping all other interrupts disabled. Subsequently it will power down all other modules except the RF wakeup receiver.

When the initialization sequence is finished, the system will enter a very low power mode. This mode will be called shutdown mode. The system can be woken up by the RF wakeup receiver which will be listening for a specific signal from the user. When the system is interrupted from sleep by the RF wakeup receiver it will power on the XBee module, establish a ZigBee connection, and enable the XBee interrupt. Additionally, the system will power off the RF wakeup receiver and disable its corresponding interrupt.

Afterwards, the system will enter in another low power mode which will be referred to as standby mode. In this mode, the system will maintain an active ZigBee connection via the XBee module. The XBee module will be listening for specific signal from the base station. When it receives a signal, it will interrupt the MCU and set a flag corresponding to the signal that was received. Possible signals are meant for entering diagnostic, retrieval, sampling, status, or shutdown mode. A signal can also be a designation to exit diagnostic mode. The interrupt routine will then take the CPU to active mode, and the system will proceed to execute the service corresponding to the signal that was sent to the XBee module via the base station. After the service has finished executing, the system will return to standby mode where it will listen for more incoming commands.

10. Software Level of Completion

Table 6 shows a list of the system features and software functionality. The software features and expected functionality have been divided by the operating mode to which they belong to. All the operating modes are presented and discussed in Section 9.

Table 6: List of System Features and Functionality

| Main |
|--|
| Power on System with RF modulePower on Xbee and connect to base station |
| Professor Annotations |
| |
| Status Mode |

- Display SD Card Free Space on GUI
- Display Battery Level on GUI
- Display Drifter ID on GUI
- Allow users to switch between any of the other operating modes

Professor Annotations

Diagnostic Mode

- Display raw sensor measurements on GUI
- Display GPS location on GUI if available
- Display Battery Level on GUI

Professor Annotations

Sampling Mode

- Collect Data from three sensors: Accelerometer, Magnetometer and Gyroscope
- Sample at a frequency of 250Hz for a sampling window of 30 seconds
- Write Data to SD card

Professor Annotations

Location Mode

- Get data from GPS and send it through XBee
- Display received location data on GUI until the user exits this mode.

Professor Annotations

Retrieval Mode

- Read data from SD card and display on GUI
- Wirelessly transfer data from SD card to the GUI through the XBee
- Erase data from SD card.

Professor Annotations

Shut Down Mode

• Shut down all components and send MCU to low power mode



11. Future Work

Although a complete functional prototype was delivered, thorough field testing has yet to be performed because of time constraints. The calibration of the sensors can be different from board to board because of the different amounts of stress caused by the soldering process. Since data conversion takes place in the Graphical User Interface this means that a calibration mode should be added to the software. The software should take at least two parameters for each sensor axis: a scaling factor and an offset. Although there are very elaborated calibration processes and methods, these two parameters are essential to any calibration process.

In addition to this, during the late stages of the prototype development one of the researchers discovered from his gathered data that the gyroscope was very sensible to vibrations and changes in acceleration, something that will always occur because of the nature of the experiments being conducted with these drifters. The gyroscope used for this prototype suffers from the same negative effect as the one the researcher is using. Because of the advanced stage of development, it became unfeasible to change the selected gyroscope to one that was more resistant to these effects. Therefore, in a future version of the prototype a new gyroscope that is shock resistant needs to be chosen in order to yield better results.

12. References

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Appendix A: User's Guide

This section contains a guide with instructions on how to operate the drifters. It also describes the capabilities of the Graphical User Interface (GUI) and how it interacts with the drifters.

Appendix B: Extended Power Analysis

This section contains a more detailed explanation of how the battery life was estimated. It includes the assumptions made to generate the activity factors. In addition, it includes a thorough description of the calculations made in the thermal analysis.

Add Level Shifters and recalculate power. See if we can find a chart of Charge vs Voltage to determine the lower level of available charge to get a more real estimate. Should re-check MCU pins

B.1 Battery Life Estimate

In order to estimate the battery life, the average supply current was determined by using a weighted average based on the fraction of time each component is active. The weighted average formula used was: $I_{avg} = \alpha * I_{active} + (1 - \alpha) * I_{LPM}$, where α is the activity factor or the fraction of time the component is active. The following assumptions were made when determining the activity factor.

- The drifters will spend 10 minutes in "Locate Mode" before they are retrieved from the water.
- The drifters will spend 30 seconds in sampling mode.
- The drifters will spend 3 minutes in stand-by mode before they are deployed.
- The drifters will spend about 10 seconds transferring a single data file. The following assumptions were made to determine this time:
 - File Size: 200 kB * 8 = 16.000 kbits.
 - 80% of XBee maximum Speed: 250 kbps * 80% = 200 kbps.
 - 16,000 kbits / 200 kbps = 8 seconds, which can be rounded up to 10 seconds.

Table 7 shows a list of the components along with their active and low power mode supply current, determined activity factor, and weighted average supply current. It also shows the total average current consumption of the system which was determined to be around 70 mA. This means that a chosen 500 mAh battery will last for about 7.23 hours. Based on the current assumptions, a single throw or experiment will last for about 13.66 minutes, which means that the drifters will be able to perform at least 30 experiment trials under the current assumptions.

Table 7: Activity Factors Used to Estimate Battery Life

| Component | $I_{Active} (\mu A)$ | I_{LPM} (μ A) | α | $I_{AVG}(\mu A)$ | |
|----------------------|----------------------|----------------------|--------|------------------|--|
| Connected To LDO | | | | | |
| MSP430FR5969 | 1600 | 0.5 | 78.05% | 1248.91 | |
| 3-Axis Accelerometer | 300 | 0 | 3.66% | 10.98 | |
| Magnetometer | 110 | 1 | 3.66% | 4.9894 | |
| XBee | 45000 | 0.5 | 96.34% | 43353.02 | |
| RF Wakeup | 2.7 | 0.4 | 0.00% | 0.4 | |
| Gyroscope | 6100 | 5 | 3.66% | 228.077 | |

| Component | $I_{Active} (\mu A)$ | I_{LPM} (μ A) | α | $I_{AVG}(\mu A)$ | |
|-------------------------------|----------------------|-------------------------|---------|------------------|--|
| GPS | 26140 | 5 | 73.17% | 19127.98 | |
| SD Card | 100000 | 10 | 4.88% | 4889.512 | |
| Power switch | 1 | 0.3 | 3.66% | 0.32562 | |
| SD to USB | 37 | 1 | 100.00% | 37 | |
| Connected Directly to Battery | | | | | |
| LDO | 65 | 1 | 100.00% | 65 | |
| Battery Charger | 1500 | 6.5 | 0.00% | 6.5 | |
| Battery Meter | 103 | 4 | 100.00% | 103 | |
| Total | 180958.7 | 35.2 | - | 69075.69 | |
| Battery Capacity | 500 mAh | Hours of Use per charge | | 7.238436 | |
| Est. time per throw (min) | 13.66 mins | Throws | 31.7785 | | |

B.2 Thermal Analysis

Performing a thermal analysis on the system will reveal whether the operating temperature of the individual ICs is below their maximum rating. In order to perform this analysis, the junction temperature T_J will be calculated for the MCU and the power management ICs. The junction temperature is given by [6, 419]:

$$T_J = T_A + \theta_{JA} \cdot P_{diss}$$

where T_J is the estimated junction temperature, T_A is the ambient temperature (taken here to be $27^{\circ}C$), θ_{JA} is the junction-to-ambient thermal resistance and P_{diss} is the estimated power consumption of the device.

This formula is applied throughout the following sections to determine whether the MCU and the power ICs will be operating at a safe temperature or if they require additional heat dissipation mechanisms such as heat syncs, fans, etc.

B.2.1 Microcontroller

In order to estimate the average operating junction temperature for the MCU the power dissipated by the IC will first be calculated. The following formula, which was taken from [6, 419], will be used:

$$P_{diss} = V_{DD} \cdot \left(I_{DD(avg)} + \sum_{all \, pins} |I_{IO(avg)}| \right)$$

Although no information is available for the θ_{JA} of the MSP430FR5969, since this value depends on the package and the area exposed to the air, a device with the same package (48-pin QFN), the MSP430F5510, was found to have $\theta_{JA} = 28.6^{\circ}C/W$ and this value was instead used. In the same manner, although no information on the IO currents is available, the ones for the MSP430F5510 will be used instead.

In full drive mode, the MSP430F5510 can output upto 45mA through its IO pins while still maintaining a valid V_{OL} . Table 8 shows the assumed IO currents for each components.

| Pin | $I_{DD(Active)} (\mu A)$ | Qty | Total Current (µA) |
|--------|--------------------------|-------|--------------------|
| SPI | 100 | 3 | 300 |
| I^2C | 10 | 2 | 20 |
| UART | 1000 | 2 | 2000 |
| GPIO | 1000 | 21 | 21000 |
| | | Total | 23320 |

Table 8: Worst Case I/O current for microcontroller pins

Assuming an IO current of 23.32mA and an average supply current of 1.6mA, the total power dissipation can then be calculated to be:

$$P_{diss} = V_{DD} \cdot (1.6m + 23.32m)$$

$$P_{diss} = 82.24mW$$

Using $\theta_{JA} = 47.8^{\circ}C/W$, the total junction temperature is then given by:

$$T_J = 27 + 26.8 \cdot 0.08224$$
$$T_J = 29.20^{\circ}C$$

The datasheet states that the maximum junction temperature is $95^{\circ}C$, which means that in this application, the device is well under the maximum operating temperature rating and no additional heat dissipation mechanism is needed.

B.2.2 Low-Dropout Regulator

The datasheet for the TPS73501 contains a section on power dissipation and provides the following formula for calculating the power dissipation across the device:

$$P_{diss} = (V_{IN} - V_{OUT}) \cdot I_{OUT}$$

The voltage provided by the battery charger circuit is 3.925 V and the required output voltage is 3.3 V. The estimated output current required is 180.96 mA. In order to leave a margin of error, a rounded value of 200 mA will be used in this calculation. Thus, the power dissipated by the device is given by:

$$P_{diss} = (3.925 - 3.3) \cdot 200m$$
$$P_{diss} = 125mW = 0.125W$$

Since for this device, $\theta_{JA} = 47.8^{\circ}C/W$, the total junction temperature is then given by:

$$T_J = 27 + 47.8 \cdot 0.125$$

$$T_J = 32.98^{\circ}C$$

The datasheet states that the maximum junction temperature is $150^{\circ}C$, which means that in this application, the device is well under the maximum operating temperature rating and no additional heat dissipation mechanism is needed.

B.2.3 Battery Charger

The datasheet for the BQ24072 provides the following formula for estimating the power dissipation across the device.

$$P_{diss} = (V_{IN} - V_{OUT}) \cdot I_{OUT} + (V_{OUT} - V_{BAT}) \cdot I_{BAT}$$

The output voltage of the device is 5.5 V, while the input voltage is 5 V as dictated by the USB standard. The output current can be estimated to be 50mA by taking into account the two LEDs connected to this pin (at about 20mA per LED) and the LDO input (46 μ A) and rounding up to leave a margin for safety. The circuit was designed for a battery voltage of 3.7 V and a current of 800 mA.

$$P_{diss} = (5 - 3.925) \cdot 50m + (3.925 - 3.7) \cdot 500m$$
$$\boxed{P_{diss} = 166mW}$$

Since for this device, $\theta_{JA} = 39.47^{\circ}C/W$, the total junction temperature is then given by:

$$T_J = 27 + 39.47 \cdot 0.166$$
$$T_J = 33.55^{\circ}C$$

The datasheet states that the maximum junction temperature is $125^{\circ}C$, which means that in this application, the device is well under the maximum operating temperature rating and no additional heat dissipation mechanism is needed.

B.2.4 Battery Meter

Although the datasheet for the BQ27410 does not provide a direct formula for power dissipation and because the battery meter has an internal LDO, the formula used for the MCU IO pins will be combined with the power dissipation formula of the LDO to obtain a more robust estimate for the power dissipated.

$$P_{diss} = V_{DD} \cdot \left(\sum_{allpins} |I_{IO(avg)}| \right) + (V_{IN} - V_{OUT}) \cdot I_{OUT}$$

The IO pin output current for this device is between 0.5 and 1 mA. 1 mA will be used for the two I^2C pins, which gives a total IO current of 2 mA. The maximum supply current is 103 μ A and this will be used instead of the average supply current to leave a margin of safety. The input voltage is 5.5 V and the regulated output voltage is 2.5 V.

$$P_{diss} = 2.5 \cdot (2m) + (3.7 - 2.5) \cdot 0.103m$$

$$P_{diss} = 5.12 mW$$

Since for this device, $\theta_{JA} = 64.17^{\circ}C/W$, the total junction temperature is then given by:

$$T_J = 27 + 64.1 \cdot 0.00512$$
$$T_J = 27.33^{\circ}C$$

The datasheet states that the maximum junction temperature is $100^{\circ}C$, which means that in this application, the device is well under the maximum operating temperature rating and no additional heat dissipation mechanism is needed.

Appendix C: Work Distribution

This appendix contains a table showing a list of tasks performed for this project and the people assigned to each of them. Several tasks were assigned to two people because the pair-programming strategy was used for most software and hardware components so that the second person could validate the work of the first person and minimize errors in both software and hardware.

Needs to be updated with other tasks performed

Table 9: Work Distribution Table

| Task Title | Adrian | Daniel | Nelian | Samuel |
|---|----------|----------|----------|----------|
| Topic Research | ✓ | ✓ | ✓ | ✓ |
| Define System Requirements and Specifications | ✓ | ✓ | ✓ | √ |
| Define Essential Hardware and Software | √ | ✓ | ✓ | ✓ |
| Create System Block Diagram | | | √ | |
| Set up Project Website | | ✓ | | |
| Cover Page, Table of Contents, Report Format | √ | | | |
| Specifications: Requirements and Features | √ | ✓ | √ | √ |
| Specifications: Limitations | | | | ✓ |
| Market Description | | √ | | |
| Specifications: Essential HW/SW | | | √ | |
| Block Diagram | | | √ | |
| System Conception: Global System View | √ | | | |
| System Conception: UI Level | | | √ | |
| Design Criteria | | √ | | √ |
| Expert Opinion | | | √ | |
| Introduction | | ✓ | | |
| Abstract | | | | √ |
| Proof Reading | √ | ✓ | √ | ✓ |
| Project Journal | | | | ✓ |
| Project and Work Distribution Table | √ | | | |
| MCU Research | √ | ✓ | √ | ✓ |
| Other Components Research | √ | √ | √ | ✓ |
| Brainstorm: Discussion and Selection of MCU | ✓ | ✓ | ✓ | ✓ |
| Design Team Logo and Poster | | | √ | |
| Set up Git Repository | | ✓ | | |
| Component Selection | ✓ | ✓ | ✓ | ✓ |
| Update Block Diagram | √ | | | |
| Brainstorm: Software Plan (Operating Chart) | √ | ✓ | ✓ | √ |
| Build System Schematics | | | | √ |
| Cost Analysis | | | | √ |
| Timing Analysis and Diagrams | | | ✓ | |
| Power Analysis | √ | | | |

| Task Title | Adrian | Daniel | Nelian | Samuel |
|--|----------|----------|--------------|----------|
| Software Brainstorm Requirement Definition and | √ | √ | √ | √ |
| Verification | V | v | V | v |
| Use Case Diagrams | | | ✓ | |
| Design User Interface | | ✓ | | |
| Flow Charts, Module and Interface Design for | | | \(\) | |
| MCU Software | | | V | |
| Connect and Work with Accelerometer and Gy- | √ | | | |
| roscope | V | | | |
| Connect and Work with Magnetic Field and Light | | | | |
| Sensor | | | • | |
| Connect and Work with GPS Software and Hard- | | √ | | |
| ware Module | | | | |
| Connect and Work with SD Card Software and | | | | ✓ |
| Hardware Module | | | | |
| Connect and Work with Power Supply and Man- | ✓ | | | |
| agement | | | | |
| Connect and Work with Xbees | | √ | | |
| Implement Sampling Mode Software Module | √ | | | √ |
| Implement Transfer Mode Software Module | | √ | | |
| Implement Diagnostic Mode Software Module | | | | ✓ |
| Implement LED Controller Module | | | √ | |
| Software and Hardware Testing and Debugging | ✓ | ✓ | ✓ | ✓ |
| Implement Out of Memory Alert Software Mod- | | | | ./ |
| ule | | | | V |
| Implement Low Power State Software Module | ✓ | | | |
| Implement User Interface | | | ✓ | |
| Design and Make PCBs | | ✓ | | |
| Connect, Solder, Test | √ | | | |
| Field Testing (Water Tank) | √ | √ | √ | √ |
| Software Testing and Debugging | √ | √ | √ | √ |
| Hardware Testing and Debugging | √ | √ | √ | √ |