

$$\sin \theta = x - \frac{x^3}{L^3} + \frac{x^5}{L^5} - \dots$$

t_i = Initial thickness

$$\cos \theta = 1 - \frac{x^2}{L^2} + \frac{x^4}{L^4} - \dots$$

t_f = final thickness

$$\tan \theta = x + \frac{x^3}{3} + \frac{2x^5}{15} + \dots$$

θ = Angle of bite

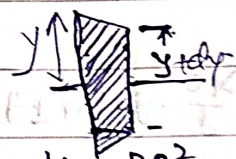
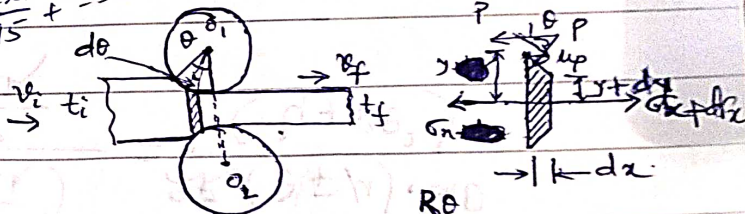
$d\theta$ = Angle of bite for small cross section of strip.

w = width (Assume unity)

v_i = Entry velocity, v_f = Exit velocity

$$v_i < v < v_f$$

P = Pressure Exerted by rolls on the strip.



$$y = \frac{t_f}{2} + \frac{R\theta^2}{2}$$

$$2(y+dy)(\sigma_x+d\sigma_x) - 2y\sigma_x + 2PRd\theta \sin \theta - 2\mu P \cos \theta \times R d\theta = 0$$

Since θ = very small.

$$2(y+dy)(\sigma_x+d\sigma_x) - 2y\sigma_x + 2PR\theta d\theta - 2\mu PR d\theta = 0$$

Neglecting higher order term

$$2y\sigma_x + 2y d\sigma_x + 2\sigma_x dy + 2d\sigma_x dy - 2y\sigma_x + 2PR\theta d\theta - 2\mu PR d\theta = 0$$

$$\Rightarrow 2y d\sigma_x + 2\sigma_x dy + 2PR\theta d\theta - 2\mu PR d\theta = 0$$

$$\Rightarrow 2 d(\sigma_x y) + PR(\theta d\theta - \mu d\theta) = 0$$

$$\Rightarrow \frac{d}{d\theta} (y\sigma_x) + RP(\theta - \mu) = 0 \Rightarrow \frac{d}{d\theta} (y\sigma_x) - (\mu - \theta)RP = 0$$

Principal stress $\sigma_x = \sigma_1$, $-P = \sigma_3$ $\sigma_2 = \frac{1}{2}(\sigma_x - P)$ $\left\{ \sigma_2 = \frac{\sigma_1 + \sigma_3}{2} \right.$

$$(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 = 6K^2 \quad \left\{ K = \text{shear yield stress} \right.$$

Substituting the value of σ_1, σ_2 & σ_3

$$\left[\sigma_x - \left\{ \frac{1}{2}(\sigma_x - P) \right\} \right]^2 + \left[\frac{1}{2}(\sigma_x - P) - (-P) \right]^2 + [-P - \sigma_x]^2 = 6K^2$$

$$\Rightarrow [P + \sigma_x = 2K] \Rightarrow \underline{\sigma_x = 2K - P}$$

$$\frac{d}{d\theta} (\gamma \cdot (2k - P)) = (\mu - \theta) RP = 0$$

As we know that friction force changes its direction after the element reaches crossed the neutral point.

Then eqn becomes:

$$\frac{d}{d\theta} [(2k - P) \gamma] = [(\pm \mu - \theta) RP] = 0$$

+ve Sign indicates region before neutral point

-ve Sign indicates region after neutral point.

$$2k\gamma \frac{d}{d\theta} (1 - \frac{P}{2k}) + (\theta \mp \mu) RP = 0$$

$$\Rightarrow 2\gamma \frac{d}{d\theta} (1 - \frac{P}{2k}) + (\theta \mp \mu) R \cdot \frac{P}{k} = 0$$

if $\theta = \text{small}$ then γ can be expressed in the form (dividing by R both side)

$$\gamma = \frac{t_f}{2} + \frac{R\theta^2}{2}$$

$$2(\frac{t_f}{2} + \frac{R\theta^2}{2}) \frac{d}{d\theta} (1 - \frac{P}{2k}) - (t_f + R\theta^2) \frac{d}{d\theta} (\frac{P}{2k}) + 2(\theta \mp \mu) R \cdot \frac{P}{2k} = 0$$

$$\Rightarrow \frac{d(\frac{P}{2k})}{\frac{P}{2k}} (t_f + R\theta^2) \frac{d}{d\theta} (\frac{P}{2k}) = 2(\theta \mp \mu) R \cdot \frac{P}{2k}$$

$$\Rightarrow \frac{d(\frac{P}{2k})}{\frac{P}{2k}} = \frac{2R(\theta \mp \mu) \cdot d\theta}{(t_f + R\theta^2)}$$

Integrating both sides

H = total pressure

\Rightarrow Integrating both sides.

$$\int \frac{d\left(\frac{P}{2K}\right)}{\left(\frac{P}{2K}\right)} = \int \frac{2R\theta d\theta}{(t_f + R\theta^2)} \mp \int \frac{2R\mu \cdot d\theta}{t_f + R\theta^2} + C_1$$

$$\text{or } \ln\left(\frac{P}{2K}\right) = \ln(t_f + R\theta^2) \mp 2\mu \sqrt{\frac{R}{t_f}} \tan^{-1}\left(\sqrt{\frac{R}{t_f}} \cdot \theta\right) + \ln\left(\frac{C}{2R}\right) \quad \text{where } C \text{ being an arbitrary constant}$$

or Assume $\lambda = 2 \sqrt{\frac{R}{t_f}} \tan^{-1} \sqrt{\frac{R}{t_f}} \theta$

$$\gamma = \frac{1}{2}(t_f + R\theta^2)$$

$$\ln\left(\frac{P}{2K}\right) = \ln(2\gamma) \mp \mu\lambda + \ln \frac{C}{2R}$$

$$\Rightarrow \ln\left(\frac{P}{2K}\right) = \ln\left(2\gamma \cdot \frac{C}{2R}\right) \mp \mu\lambda$$

$$= \ln\left(C \cdot \frac{\gamma}{R}\right) \mp \mu\lambda$$

$$\Rightarrow \frac{P}{2K} = C \cdot \frac{\gamma}{R} \Rightarrow \ln\left(\frac{\frac{P}{2K}}{C \cdot \frac{\gamma}{R}}\right) = \mp \mu\lambda$$

$$\Rightarrow \frac{P}{2K} = C \cdot \frac{\gamma}{R} \cdot e^{\mp \mu\lambda}$$

we know that
Applying $(\sigma_n + P) = 2k$

$$\Rightarrow \frac{\sigma_n}{2k} + \frac{P}{2k} = 1$$

$$\Rightarrow \frac{P}{2k} = 1 - \frac{\sigma_n}{2k}$$

applying boundary condition

$$\Rightarrow \frac{P_i}{2k} = 1 - \frac{\sigma_{xi}}{2k}$$

~~Substitution~~ $\frac{P}{2k} = C \cdot \frac{\gamma}{R} e^{\mp \mu \lambda}$

$$\Rightarrow \frac{P_i}{2k} = C \cdot \frac{\gamma}{R} \cdot e^{\mp \mu \left(2 \sqrt{\frac{R}{t_f}} \cdot \tan^{-1} \sqrt{\frac{R}{t_f}} \theta \right)}$$

$$\Rightarrow \frac{P_i}{2k} = 1 - \frac{\sigma_{xi}}{2k} = C \cdot \frac{\gamma}{R} \cdot e^{-\mu \lambda_i}$$

where $\lambda_i = 2 \sqrt{\frac{R}{t_f}} \cdot \tan^{-1} \left(\sqrt{\frac{R}{t_f}} \theta_i \right)$

$$\left\{ \begin{aligned} \frac{e^{\left(\frac{t_f + R \theta^2}{2R} \right)}}{2R} &= C \cdot \left(\frac{t_f}{2R} + \frac{\theta^2}{2} \right) \\ &= C \cdot \frac{t_f}{2R} \end{aligned} \right.$$

$$\frac{P_i}{2K} = \bar{C} \frac{t_i}{2R} \cdot e^{-\mu \lambda_i}$$

$$\begin{aligned} \lambda &= \frac{1}{R} \left(\frac{t_f}{2R} + \frac{R \theta_f^2}{2} \right) \\ &= \frac{1}{2R} \left(\frac{t_f}{R} + R \theta_f^2 \right) \\ &= \frac{1}{2R} \left(\frac{t_f}{R} + R \theta_f^2 \right) \end{aligned}$$

\bar{C} is constant before the neutral point is reached.

$$\text{hence } \bar{C} = \frac{2R}{t_i} \left(1 - \frac{6\sigma_i}{2K} \right) \cdot e^{+\mu \lambda_i}$$

for the region beyond the neutral point

$$\frac{P}{2K} = C \frac{t}{R} \cdot e^{+\mu \lambda}$$

$$\Rightarrow \frac{P_f}{2K} = C^+ \left(\frac{t_f}{2R} \right) \cdot e^{+\mu \lambda_f} = \left(1 - \frac{6\sigma_f}{2K} \right)$$

$$C^+ = \frac{2R}{t_f} \left(1 - \frac{6\sigma_f}{2K} \right) \cdot e^{-\mu \lambda_f}$$

$$= \frac{2R}{t_f} \left(1 - \frac{6\sigma_f}{2K} \right)$$

while

$$\lambda = \frac{2}{\sqrt{t_f}} \tan^{-1} \left(\sqrt{\frac{R}{t_f}} \theta_f \right)$$

$$= 0 \text{ because } \theta_f = 0$$

$$\therefore e^{-\mu \lambda_f} = 1 \quad \text{as } \frac{\theta_f}{1} = 0$$

now substituting the value of c^- & c^+ in eqn. (1)

$$\frac{P}{2K} = \bar{C} \cdot \frac{y}{R} \cdot e^{\pm \mu \lambda}$$

$$\left(\frac{P}{2K} \right)_{\text{before}} = \frac{2y}{t_i} \left(1 - \frac{\sigma_{xi}}{2K} \right) \cdot e^{-\mu \lambda}$$

$$\begin{aligned} \left(\frac{P}{2K} \right)_{\text{before}} &= \frac{2R}{t_i} \left(1 - \frac{\sigma_{xi}}{2K} \right) e^{+\mu \lambda_i} \cdot \frac{y}{R} \cdot e^{-\mu \lambda} \\ &= \frac{2y}{t_i} \left(1 - \frac{\sigma_{xi}}{2K} \right) \cdot e^{\mu(\lambda_i - \lambda)} \end{aligned}$$

$$\left(\frac{P}{2K} \right)_{\text{after}} = \frac{2y}{t_f} \left(1 - \frac{\sigma_{xf}}{2K} \right) \cdot e^{\mu \lambda}$$

$$\lambda = \frac{1}{\mu} \ln \left\{ \frac{t_f \left(1 - \frac{\sigma_{xi}}{2K} \right)}{t_i \left(1 - \frac{\sigma_{xf}}{2K} \right)} \right\} + \lambda_i$$

Determination of Roll separating force.

$$F = \int_0^{\theta_i} P R \cos \theta d\theta = \int_0^{\theta_i} P R d\theta \quad \text{since } d\theta = \sin \theta$$

$$F = \int_0^{\theta_n} P_{\text{after}} R d\theta + \int_{\theta_n}^{\theta_i} P_{\text{before}} R d\theta$$