

California State University, Los Angeles



ME 409 – Mechanical Engineering Analysis

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1. Abstract

The purpose of this study is to analyze a non-homogenous system. To better understand this, the approach for calculating our results will be by building a mathematical model with a programming aid such as Matlab. This mathematical model is used towards the non-homogenous system which in this case is known as a mixture problem with two separate tanks. The method used in this study for calculating is known as the Method of Undetermined Coefficients. The findings reveal different equations or solutions when using the method of Undetermined Coefficients when changing the values of Tank 1 and Tank 2. Furthermore, a total of 50 combinations were made to fully understand the methods used and determining the amounts of salt for both Tank 1 and Tank 2.

Nomenclatures:

Greek Symbol	Meaning	Unit
λ	Scalar (Real or Complex Number)	—

2. Introduction

One of the main applications of differential equations in general is known as Modeling. Modeling is the process of writing a differential equation to describe a physical situation that is occurring. Most of the differential equations that are used in industry for engineers are there because somebody, at some point modeled a situation and came up with the differential equation that we are using. There are times when the modeling problem is a non-homogenous system, enabling the undetermined coefficients method to be used when calculating the differential equation.

2.1 Overview and Purpose

In the modeling system problem that we will be solving starts with a substance that is being dissolved in a liquid. This liquid entering the tank may or may not contain

more of the substance that is being dissolved in it. The liquid leaving the tank will contain the substance dissolved in it. We know that if $Q(t)$ gives the amount of the substance that is being dissolved in the liquid in the tank at any time t we want to develop a differential equation that when it is solved, it will give us an expression for $Q(t)$.

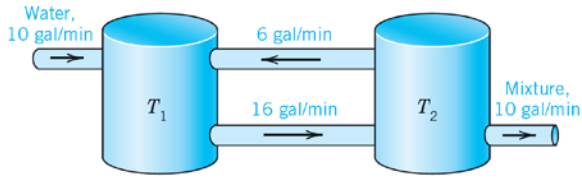
The main assumption that we are making in this problem is that the concentration of the substance in the liquid is uniform throughout the tank. Taking into consideration that there are two tanks that are being interconnected with liquid while potentially entering both and with an exit.

Our team has made the following assumptions for this situation involving two tanks. First of all, the inflow and outflow from each tank are equal, or in a simpler detail the volume in each tank is constant. Next, the concentration of contaminate in each tank will be the same at each point in the tank. Also, the concentration of contaminate in the outflow of the tank 1 will be the same as the concentration in tank 1, while the concentration of contaminate in the outflow from tank 2 will be the same as the concentration in tank 2. In addition, the outflow from tank 1 will be exiting tank 1 and reaching tank 2. The total liquid will be exiting the system completely.

As mentioned before, our team is dealing with a system containing two tanks. The first tank initially contains 200 gallons of water with 160 lb of salt within being dissolved. The second tank initially contains 100 gallons of pure water while the liquid is pumped throughout the system and the mixtures are kept uniform while being stirred. Our team proposed the idea for calculating the solution with the method of undetermined coefficients for this non-homogenous system.

2.2 Statement of the Problem

1.) Tank T1 in Fig. 101 initially contains 200 gal of water in which 160 lb of salt are dissolved. Tank T2 initially contains 100 gal of pure water. Liquid is pumped through the system as indicated, and the mixtures are kept uniform by stirring. Find the amounts of salt $y_1(t)$ and $y_2(t)$ in T1 and T2, respectively.



2.) Repeat the same problem for which T1 contains: 50, 100, 150, 200, 250 gal of water and T2 contains 10, 20, 50, 200, 500 gal of water. (25 combinations)

3.) Repeat the same problem if the flow from tank T1 to T2 changes from 1,2,5,10,20 gal/min and T2 to T1 1,2,5,10,100 gal/min. (25 combinations)

3. Theory and Principles

In this study, most of our linear systems will consist of two linear Ordinary Differential Equations (ODEs) in two unknown functions $y_1(t), y_2(t)$,

$$y_1' = a_{11} y_1 + a_{12} y_2$$

$$y_2' = a_{21} y_1 + a_{22} y_2$$

In addition, a linear system of n first-order Ordinary Differential Equations (ODEs) in n unknown functions is of the form

$$y_1' = a_{11} y_1 + a_{12} y_2$$

$$y_2' = a_{21} y_1 + a_{22} y_2$$

.....

$$y_n' = a_{n1} y_1 + a_{n2} y_2 + a_{nn} y_n$$

3.1 Matrices

The (constant or variable) coefficients form a **2x2 matrix** A , that are,

an array

$$A = [a_{jk}] = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}$$

In addition, the coefficients in the equation form an **n matrix**

$$A = [a_{jk}] = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & a_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ a_{n1} & a_{n2} & \dots & a_{nn} \end{bmatrix}$$

The a_{11}, a_{12}, \dots are called **entries**, the horizontal lines **rows**, and the vertical lines **columns**. Thus, in the equation, the first row is $[a_{11} \ a_{12}]$, the second row is $[a_{21} \ a_{22}]$ and the first and second columns are

$$\begin{bmatrix} a_{11} \\ a_{21} \end{bmatrix} \text{ and } \begin{bmatrix} a_{12} \\ a_{22} \end{bmatrix}.$$

In the “**double subscript notation**” for various entries, the first subscript is that one that denotes the *row* and the second the *column* in which the entry stands. Similarly in the previous equation. The **main diagonal** is the diagonal $a_{11} \ a_{12} \ \dots \ a_{nn}$, hence $a_{11} \ a_{12}$.

We shall need only **square matrices**, that is, matrices with the same number of rows and columns, as in the previous equations in this project.

3.2 Vectors

A **column vector** x with n **components** such as these $x_1 \ \dots, x_n$ is of the form

$$x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}, \quad \text{thus if } n = 2, \quad x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

Similarly, a **row vector** v is of the following form below,

$$v = [v_1 \ \dots \ v_n], \quad \text{thus if } n = 2, \quad v = [v_1 \ v_2]$$

3.3 Equality

Now we move on to calculations with matrices and vectors. Two $n \times n$ matrices will be *equal* if and only if corresponding entries are equal as well. For example, let's take this for instance, Thus for $n = 2$, let

$$A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \text{ and } B = \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix}$$

Then $A = B$ if and only if

$$a_{11} = b_{11}, \quad a_{12} = b_{12}$$

$$a_{21} = b_{21}, \quad a_{22} = b_{22}$$

Now, two column vectors (or two row vectors) are *equal* if and only if they both have n components and corresponding components are equal as well. For example, let

$$v = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \quad \text{and} \quad x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

then $v = x$ if and only if $v_1 = x_1, v_2 = x_2$

3.4 Addition

This is performed by adding the corresponding entries (or components). The matrices must both be $n \times n$, and vectors must both have the same number of components. For example, for $n = 2$,

$$\mathbf{A} + \mathbf{B} = \begin{bmatrix} a_{11} + b_{11} & a_{12} + b_{12} \\ a_{21} + b_{21} & a_{22} + b_{22} \end{bmatrix}, \quad \mathbf{v} + \mathbf{x} = \begin{bmatrix} v_1 + x_1 \\ v_2 + x_2 \end{bmatrix}$$

3.5 Matrix Multiplication.

The product $\mathbf{C} = \mathbf{AB}$ (in this order) of two $n \times n$ matrices $\mathbf{A} = [a_{jk}]$ and $\mathbf{B} = [b_{jk}]$ is the $n \times n$ matrix $\mathbf{C} = [c_{jk}]$ with entries the following;

$$c_{jk} = \sum_{m=1}^n a_{jm} b_{mk}$$

$$j = 1, \dots, n \quad \text{and} \quad k = 1, \dots, n$$

Let us keep caution with the following note; Matrix multiplication is **not commutative** $\mathbf{AB} \neq \mathbf{BA}$.

Furthermore, a multiplication of an $n \times n$ matrix \mathbf{A} by a vector \mathbf{x} with n components is defined by the same rule: $\mathbf{v} = \mathbf{Ax}$ is the vector with the n components

$$v_j = \sum_{m=1}^n a_{jm} x_m \quad j = 1, \dots, n$$

3.6 Differentiation

Now we will move on to Systems of ODEs as Vector Equations. The *derivative* of a matrix (or vector) with variable entries (or components) is obtained by differentiating each entry (or component). By using the

matrix multiplication and differentiation, we can now write the following;

$$\mathbf{y}' = \begin{bmatrix} y'_1 \\ y'_2 \end{bmatrix} = \mathbf{Ay} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$$

Similarly, the $n \times n$ matrix \mathbf{A} and a column vector \mathbf{y} with n components, namely, $\mathbf{y}' = \mathbf{Ay}$. The vector equation is equivalent to two equations for the components, and these are precisely the two ODEs in the first equation.

3.7 Inverse Matrix

The $n \times n$ unit matrix \mathbf{I} is the $n \times n$ matrix with main diagonal 1, 1, ..., 1 and all of the other entries that are zero. If, for a given $n \times n$ matrix \mathbf{A} , there is a $n \times n$ matrix \mathbf{B} such that $\mathbf{AB} = \mathbf{BA} = \mathbf{I}$, then \mathbf{A} is called nonsingular and \mathbf{B} is called the Inverse of \mathbf{A} and is denoted by \mathbf{A}^{-1} so the following is true;

$$\mathbf{AA}^{-1} = \mathbf{A}^{-1}\mathbf{A} = \mathbf{I}$$

The inverse will exist if the determinant $\det \mathbf{A}$ of \mathbf{A} is not zero. If \mathbf{A} has not inverse, then we will call it a singular. For example is $n = 2$, then

$$\mathbf{A}^{-1} = \frac{1}{\det \mathbf{A}} \begin{bmatrix} a_{11} & -a_{12} \\ -a_{21} & a_{22} \end{bmatrix}$$

Where the determinant of \mathbf{A} is

$$\det \mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = a_{11}a_{22} - a_{12}a_{21}$$

3.8 Eigenvalues, Eigenvectors

This next process is quite important and useful. The Eigenvalues and eigenvectors will be very important during the process of calculating our solution.

Let $\mathbf{A} = [a_{jk}]$ be an $n \times n$ matrix. Consider the following equation;

$$\mathbf{Ax} = \lambda \mathbf{x}$$

where λ is a scalar (a real or complex number) to be determined and \mathbf{x} is a vector to be determined. Now, for every λ , a solution is $\mathbf{x} = \mathbf{0}$. A scalar λ such that it holds for some vector $\mathbf{x} \neq \mathbf{0}$ is called an **eigenvalue** of \mathbf{A} , and this

vector is called an **eigenvector** of **A** corresponding to this eigenvalue λ .

$$(\mathbf{A} - \lambda \mathbf{I})\mathbf{x} = \mathbf{0}$$

These are n linear algebraic equations in the n unknowns x_1, \dots, x_n (the components of \mathbf{x}). For these equations to have a solution $\mathbf{x} \neq \mathbf{0}$, the determinant of the coefficient matrix $\mathbf{A} - \lambda \mathbf{I}$ must be zero. For example, we only need this only for $n = 2$. Then the following is

$$\begin{bmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

In components,

$$(a_{11} - \lambda)x_1 + a_{12}x_2 = 0$$

$$a_{21}x_1 + (a_{22} - \lambda)x_2 = 0$$

Now, $\mathbf{A} - \lambda \mathbf{I}$ is singular if and only if its determinant $\det(\mathbf{A} - \lambda \mathbf{I})$, called the **characteristic determinant** of **A** (also for general n), is zero. This will give us the following;

$$\begin{aligned} \det(\mathbf{A} - \lambda \mathbf{I}) &= \begin{vmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{vmatrix} \\ &= (a_{11} - \lambda)(a_{22} - \lambda) - a_{12} a_{21} \\ &= \lambda^2(a_{11} + a_{22})\lambda + a_{11} a_{22} - a_{12} a_{21} = 0 \end{aligned}$$

This quadratic equation in λ is called the **characteristic equation** of **A**. Its solutions are the eigenvalues λ_1 and λ_2 of **A**. First determine these. Then use with $\lambda = \lambda_1$ to determine an eigenvector $\mathbf{x}^{(1)}$ of **A** corresponding to λ_1 . Finally use with $\lambda = \lambda_2$ to find an eigenvector $\mathbf{x}^{(2)}$ of **A** corresponding to λ_2 . Note that if \mathbf{x} is an eigenvector of **A**, so is $k\mathbf{x}$ with any $k \neq 0$.

3.9 Nonhomogeneous Linear Systems of ODEs

We will now move on to the situation where the linear system of the Ordinary Differential Equation is Non-homogenous. Here we will use the method for solving nonhomogeneous linear systems of ODEs;

$$\mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g}$$

where the vector $\mathbf{g}(t)$ is not identically zero. We assume $\mathbf{g}(t)$ and the entries of the $n \times n$ matrix $\mathbf{A}(t)$ to be continuous on some interval J of the t -axis. From a

general solution $\mathbf{y}^{(h)}(t)$ of the homogeneous system $\mathbf{y}' = \mathbf{A}\mathbf{y}$ on J and a **particular solution** $\mathbf{y}^{(p)}(t)$ of $\mathbf{y}' = \mathbf{A}\mathbf{y}$.

$$\mathbf{y} = \mathbf{y}^{(h)}(t) + \mathbf{y}^{(p)}(t)$$

\mathbf{y} is called a **general solution** of (1) on J because it includes every solution of $\mathbf{y}' = \mathbf{A}\mathbf{y}$ on J .

3.10 Method of Undetermined Coefficients

Now for the actual use of the method. Just as for a single ODE, this method is suitable only if the entries of **A** are constants and the components of **g** are constants, positive integer powers of t , exponential functions, or cosines and sines. For instance, in such a case, a particular solution $\mathbf{y}^{(p)}$ is assumed in a form similar to **g**; for instance, $\mathbf{y}^{(p)} = \mathbf{u} + \mathbf{v}t + \mathbf{w}t^2$ if **g** has components quadratic in t , with **u**, **v**, **w** to be determined by substitution into $\mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g}$.

4. Data Analysis

4.1. Analysis of Calculation and Tables

4.1.1 Sample Calculation using Method of Undetermined Coefficients for Original Problem

The following calculation demonstrates a sample calculation or the original problem in finding the equations to determine the amount of salt in Tank 1 and Tank 2. This was done by hand before using the aid of Matlab to see if the solution would match. Verification was very crucial for our team. Here is our sample calculation:

Given:

$T_1 = 200 \text{ gal}, 160 \text{ lb salt}, \text{Inflow} = 6 \text{ gal/min}, \text{Outflow} = 16 \text{ gal/min}$

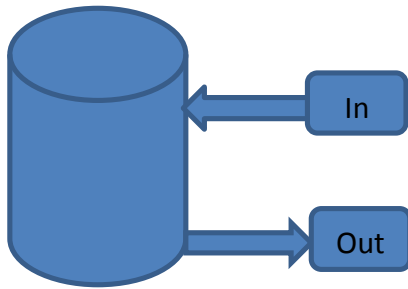
$T_2 = 100 \text{ gal}, \text{pure water}, \text{Inflow} = 16 \text{ gal/min}, \text{Outflow} = 10 \text{ gal/min}$

Required:

$y_1(t)$ and $y_2(t)$ in T_1 and T_2

Solution:

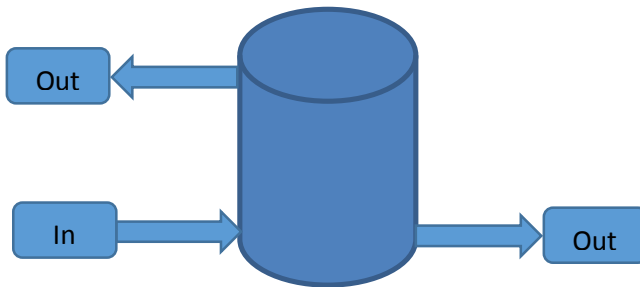
Free Body Diagram (FBD):



$$y_1' = \frac{\text{Inflow}}{\text{min}} - \frac{\text{Outflow}}{\text{min}} = \frac{6}{100}y_2 - \frac{16}{200}y_1$$

$$= -0.08y_1 + 0.06y_2$$

Free Body Diagram (FBD):



$$y_2' = \frac{\text{Inflow}}{\text{min}} - \frac{\text{Outflow}}{\text{min}} = \frac{16}{200}y_2 - \frac{6}{200}y_1 - \frac{10}{200}y_1$$

$$= -0.08y_1 + 0.06y_2$$

$$y' = \mathbf{A}y$$

$$\begin{bmatrix} y_1' \\ y_2' \end{bmatrix} = \begin{bmatrix} -0.08 & 0.06 \\ 0.08 & -0.16 \end{bmatrix}$$

$$(\mathbf{A} - \lambda \mathbf{I}) = \mathbf{0}$$

$$\det(\mathbf{A} - \lambda \mathbf{I}) = \begin{vmatrix} -0.08 - \lambda & 0.06 \\ 0.08 & -0.16 - \lambda \end{vmatrix}$$

Eigenvalues

$$(-0.08 - \lambda)(-0.16 - \lambda) - (0.08)(0.06)$$

$$= 0.128 + 0.08\lambda + 0.16\lambda + \lambda^2$$

$$- 0.048$$

$$\lambda^2 + 0.24\lambda + 0.008$$

$$\lambda = \frac{(-0.24) \pm \sqrt{(0.24)^2 - 4(1)(0.008)}}{2(1)}$$

$$= \frac{(-0.24) \pm \sqrt{0.0256}}{2(1)}$$

$$= \frac{(-0.24) \pm 0.16}{2(1)}$$

$$\lambda = -0.2 \text{ and } \lambda = -0.4$$

Eigenvectors for $\lambda = -0.2$

$$\begin{bmatrix} -0.08 - (-0.2) & 0.06 \\ 0.08 & -0.16 - (-0.2) \end{bmatrix}$$

$$\begin{bmatrix} -0.08 & 0.06 \\ 0.08 & -0.16 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} -0.08 & 0.06 & | & 0 \\ 0.08 & -0.16 & | & 0 \end{bmatrix} \rightarrow \begin{bmatrix} 0.12 & 0.06 \\ 0.0696 & 0.0448 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$0.12x_1 + 0.06x_2 = 0$$

$$\frac{0.12}{0.12}x_1 = \frac{0.06}{0.12}x_2$$

$$x_1 = -0.5x_2 \quad x_1 = 1$$

$$\frac{1}{-0.5} = \frac{-0.5}{-0.5}x_2 \quad x_2 = -2$$

$$\begin{bmatrix} 1 \\ -2 \end{bmatrix} \text{ for } \lambda = -0.2$$

Eigenvectors for $\lambda = -0.04$

$$\begin{bmatrix} -0.08 - (-0.04) & 0.06 \\ 0.08 & -0.16 - (-0.04) \end{bmatrix}$$

$$\begin{bmatrix} -0.04 & 0.06 \\ 0.08 & -0.12 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} -0.04 & 0.06 & | & 0 \\ 0.08 & -0.12 & | & 0 \end{bmatrix} \rightarrow \begin{bmatrix} -0.0635 & -0.1152 \\ 0.08 & -0.12 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$0.8x_1 - 0.12x_2 = 0$$

$$\frac{0.08}{0.08}x_1 = \frac{0.12}{0.08}x_2$$

$$x_1 = 1.5x_2 \quad x_2 = 1$$

$$x_1 = 1.5(1) \quad x_1 = 1.5$$

$$\begin{bmatrix} 1.5 \\ 1 \end{bmatrix} \text{ for } \lambda = -0.04$$

$$y = c_1 x^{(1)} e^{\lambda_1 t} + c_2 x^{(2)} e^{\lambda_2 t}$$

$$y = c_1 \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} e^{\lambda_1 t} + c_2 \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} e^{\lambda_2 t}$$

$$y = c_1 \begin{bmatrix} 1 \\ -2 \end{bmatrix} e^{-0.2t} + c_2 \begin{bmatrix} 1.5 \\ 1 \end{bmatrix} e^{-0.04t}$$

$$\begin{bmatrix} 160 \\ 0 \end{bmatrix} = c_1 \begin{bmatrix} 1 \\ -2 \end{bmatrix} + c_2 \begin{bmatrix} 1.5 \\ 1 \end{bmatrix}$$

$$160 = c_1 + 1.5c_2$$

$$0 = -2c_1 + c_2$$

$$c_2 = 2c_1$$

$$160 = c_1 + 1.5(2c_1)$$

$$\frac{160}{4} = \frac{4}{4} c_1$$

$$c_1 = 40$$

$$0 = -2c_1 + c_2$$

$$0 = -2(40) + c_2$$

$$c_2 = 80$$

$$y_1 = 40e^{-0.2t} + 120e^{-0.04t}$$

$$y_2 = -80e^{-0.2t} + 80e^{-0.04t}$$

4.1.2 Sample Table Data for Part 1

Eigenvalues	Vector V11	Vector V22	Constants for y1	Constants for y2
-0.04	1	1	40	-80
-0.2	-2	0.6666 66667	120	80
T(min)	y1		T(min)	y2
0	0		0	160
1	11.364 69489		1	148.0439 628
2	20.223 70403		2	137.5867 634
3	27.048 70405		3	128.3829 178

4	32.225 18599		4	120.2304 132
5	36.068 10495		5	112.9628 68
6	38.834 69193		6	106.4431 118
7	40.734 9422		7	100.5579 275
8	41.940 20153		8	95.21374 517
9	42.590 19503		9	90.33311 466
10	42.798 78102		10	85.85181 685
11	42.658 66102		11	81.71649 686
12	42.245 23508		12	77.88272 515
13	41.619 75758		13	74.31340 888
14	40.831 9201		14	70.97749 017
15	39.921 96542		15	67.84887 907
16	38.922 41761		16	64.90557 904
17	37.859 49779		17	62.12896 988
18	36.754 28268		18	59.50321 961
19	35.623 65241		19	57.01480 212
20	34.481 06602		20	54.65210 125
21	33.337 19573		21	52.40508 588
22	32.200 44574		22	50.26504 3
23	31.077 37643		23	48.22435 836
24	29.973 05111		24	46.27633 62
25	28.891 31953		25	44.41505 082
26	27.835 0494		26	42.63522 441
27	26.806 31558		27	40.93212 632
28	25.806 55447		28	39.30148 99

29	24.836 69009		29	37.73944 39
30	23.897 23678		30	36.24245 552
31	22.988 38298		31	34.80728 338
32	22.110 05945		32	33.43093 835
33	21.261 99471		33	32.11065 096
34	20.443 76014		34	30.84384 424
35	19.654 80656		35	29.62811 095
36	18.894 49383		36	28.46119 447
37	18.162 11485		37	27.34097 272
38	17.456 91484		38	26.26544 449
39	16.778 1069		39	25.23271 794
40	16.124 88443		40	24.24100 066
41	15.496 4311		41	23.28859 122
42	14.891 9287		42	22.37387 182
43	14.310 56337		43	21.49530 198
44	13.751 53046		44	20.65141 298
45	13.214 03827		45	19.84080 298
46	12.697 31094		46	19.06213 271
47	12.200 59054		47	18.31412 165
48	11.723 13867		48	17.59554 461
49	11.264 23755		49	16.90522 857
50	10.823 19066		50	16.24204 999
51	10.399 32324		51	15.60493 212
52	9.9919 82377		52	14.99284 276
53	9.6005 37		53	14.40479 206

54	9.2243 77723		54	13.83983 05
55	8.8629 16533		55	13.29704 707
56	8.5155 86415		56	12.77556 749
57	8.1818 40898		57	12.27455 263
58	7.8611 53561		58	11.79319 692
59	7.5530 17491		59	11.33072 697
60	7.2569 44726		60	10.88640 016
61	6.9724 65681		61	10.45950 339
62	6.6991 2856		62	10.04935 181
63	6.4364 98779		63	9.655287 691
64	6.1841 58374		64	9.276679 284
65	5.9417 05431		65	8.912919 799
66	5.7087 53516		66	8.563426 371
67	5.4849 31121		67	8.227639 104
68	5.2698 81115		68	7.905020 151
69	5.0632 60218		69	7.595052 828
70	4.8647 38488		70	7.297240 776
71	4.6739 98813		71	7.011107 148
72	4.4907 36436		72	6.736193 836
73	4.3146 58476		73	6.472060 73
74	4.1454 83483		74	6.218285 006
75	3.9829 40997		75	5.974460 44
76	3.8267 71123		76	5.740196 757
77	3.6767 24128		77	5.515119
78	3.5325 60043		78	5.298866 926

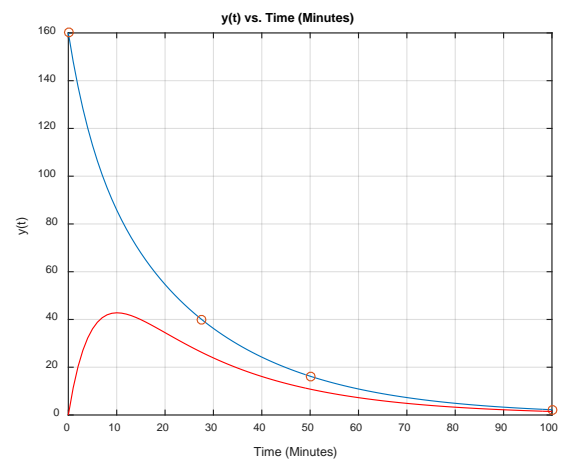
79	3.3940 4829		79	5.091094 428
80	3.2609 67315		80	4.891468 979
81	3.1331 04237		81	4.699671 097
82	3.0102 5451		82	4.515393 834
83	2.8922 21599		83	4.338342 281
84	2.7788 1667		84	4.168233 096
85	2.6698 58285		85	4.004794 051
86	2.5651 72115		86	3.847763 595
87	2.4645 90663		87	3.696890 434
88	2.3679 52996		88	3.551933 129
89	2.2751 04489		89	3.412659 71
90	2.1858 96577		90	3.278847 303
91	2.1001 8652		91	3.150281 775
92	2.0178 3717		92	3.026757 389
93	1.9387 16759		93	2.908076 476
94	1.8626 98683		94	2.794049 119
95	1.7896 613		95	2.684492 847
96	1.7194 87741		96	2.579232 345
97	1.6520 65714		97	2.478099 172
98	1.5872 87334		98	2.380931 492
99	1.5250 48942		99	2.287573 816
100	1.4652 50946		100	2.197876 749

4.2 Data Analysis Plot Graphs

The following analysis was made with the aid of Matlab programming. The following graphs demonstrate the mathematical model for the differential equation. The

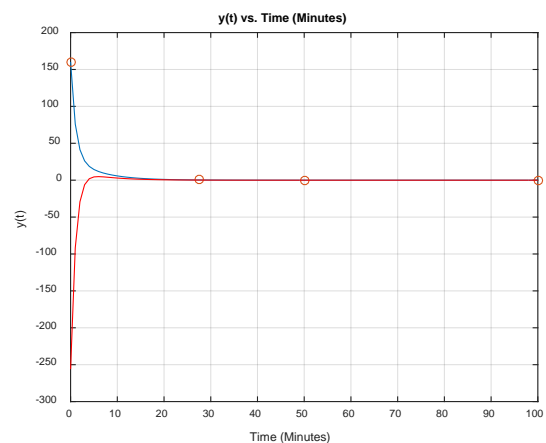
differential equation was then plotted to demonstrate the function over time. The team began with graphing a plot for the Part 1. Following up with the modeling system, the graphs were then made for Part 2 and Part 3 to demonstrate the change of gallons of water and change of flow of the water, respectively. The following graphs show the complete run for Part A since it was only 1 run. Next, the graphs for Part 2 and Part 3 only show for the first 5 runs, respectively. This was done to save time and demonstrate how the function will be changing over time.

4.2.1 Graph for Part 1

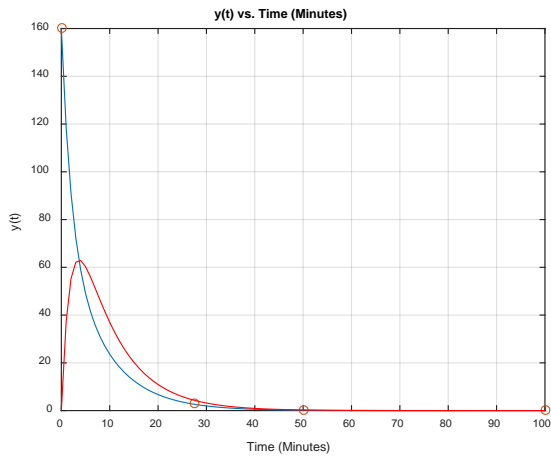
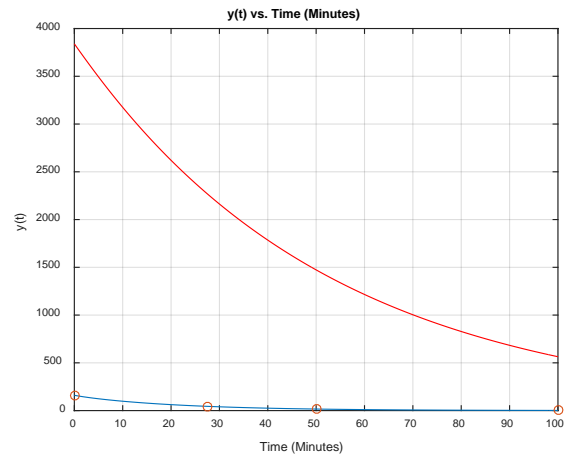
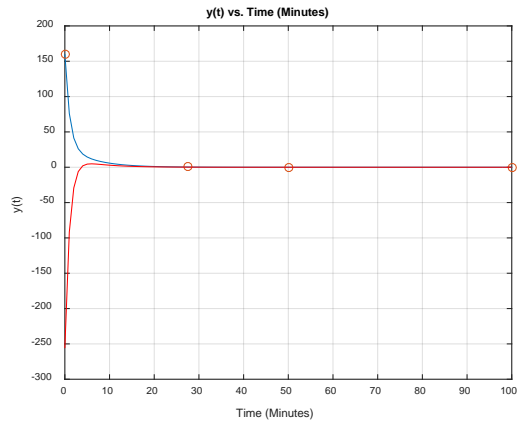


Graph 1: Part 1 1st Run

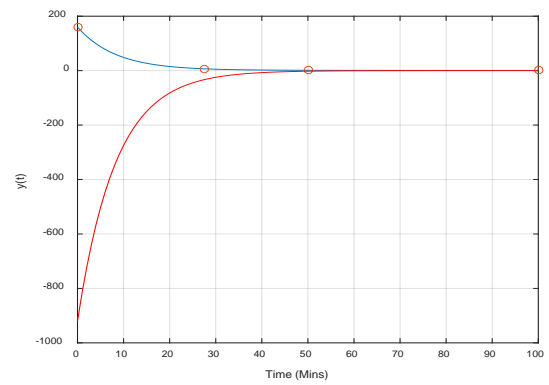
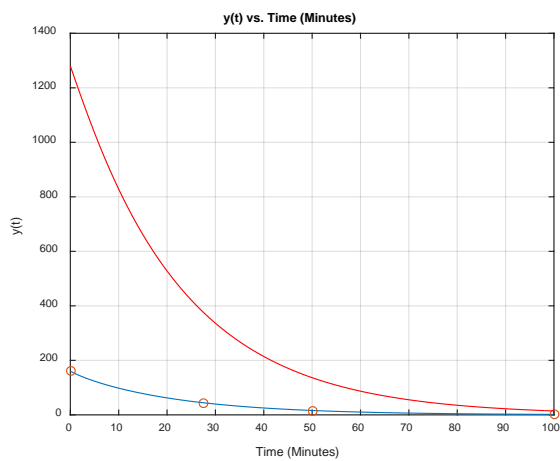
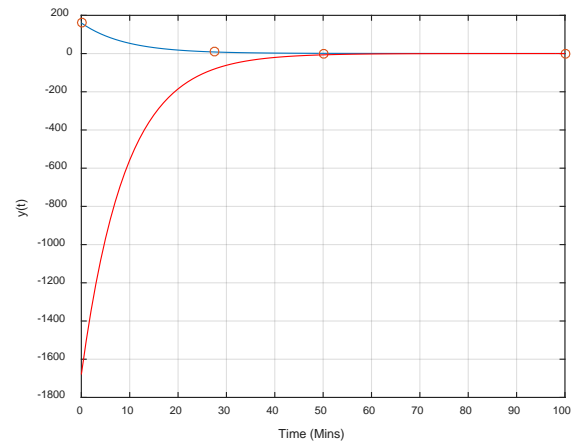
4.2.2 Graphs for Part 2

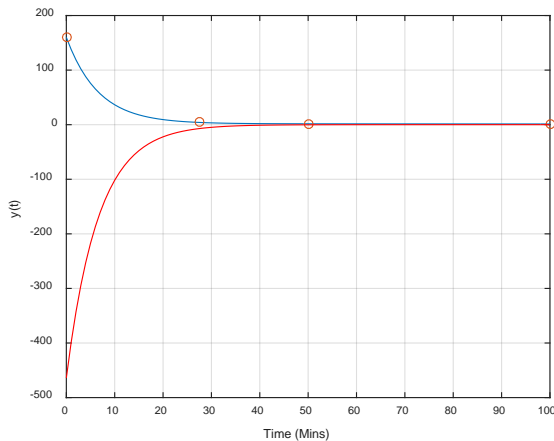


Graph 2: Part 2 1st Run

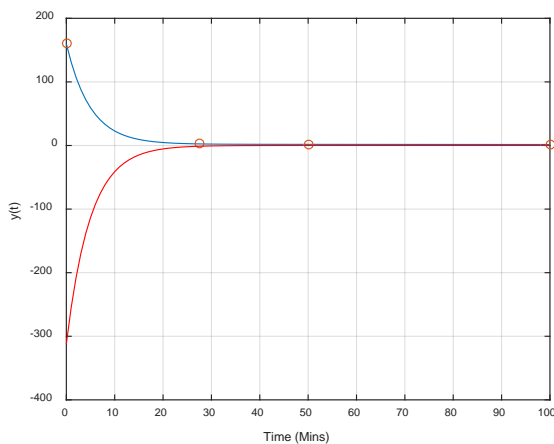


4.2.3 Graphs for Part 3

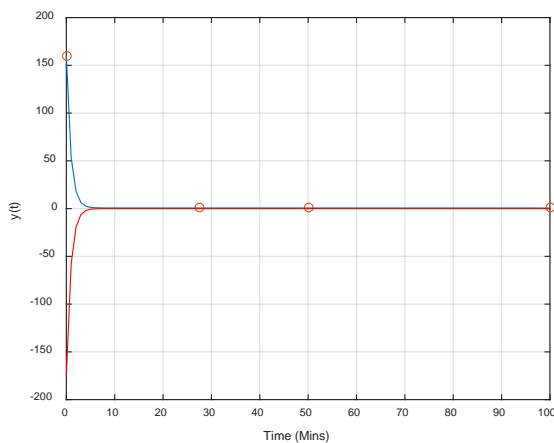




Graph 9: Part 3 3rd Run



Graph 10: Part 3 4th Run



Graph 11: Part 3 5th Run

5. Results and Discussion

Our team managed to compute a differential equation model for the non-homogeneous system involving two tanks. The mixture problem was an ideal situation for our understanding of modeling systems. The eigenvectors and eigenvalues were shown to be quite different when solving each mathematical model. For Part 1, this was basic due to the fact that we had everything given in terms of what we needed to solve the non-homogeneous system. For Part 2, we had to change the gallons for the tank 1 and tank 2. When this was applied, the values were prompted to change. This concept was also seen in Part 3, when the flow of water was changed for tank 1 and tank 2. When the flow was changed as well, the values given to us were quite different as well. Each graph shows a differential equation for tank 1 and tank 2. The graphs show the differences between times for each tank and also it displays differences of each. At some point, both differential equations will intersect at a neutral point in which shows the mixture of liquid and a substance (salt) combine into one and thus revealing a mixture flow throughout the function. Overall, the graphs give us an understanding where the mixture is occurring and conclude this understanding of non-homogeneous system. The results give us a great ideal of information to see how this non-homogeneous system behaves as a mathematical model in a differential equation.

6. Conclusion

This cumulative study on modeling a differential equation for a non-homogeneous system involving a mixture of two tanks was a great opportunity to broaden our understanding. This situation gave us a broad idea of what modeling differential equation is like and how to show a functional mathematical model with the aid of programming such as Matlab. The values show different outcomes when the differential equation for the modeling system were created. This project allowed us to see how the differential equations behave when plotted and helps us view what is occurring over time. The overall task was completed for the first part with a great understanding. The team then proceeded to repeat the same problem when T1 contained different values

such as 50, 100, 150, 200, 250 gal of water and while T2 contained 10, 20, 50, 200, 500 gal of water. This allowed us to see different situations for our modeling systems. Once this was completed, the team repeated the same problem when the flow from tank T1 to T2 changes with different values such as 1,2,5,10,20 gal/min and while T2 to T1 with the following values 1, 2,5,10,100 gal/min. We did a total of 25 combinations for both the second and third parts of this project giving us a total of 50 combinations. Overall, the study of modeling a non-homogenous system was enlightening and can be concurrently applied practically in research and design within the engineering industry.

7. References

[1] Kreyszig, Erwin. "Systems of ODEs. Phase Plane. Qualitative Methods." *Advanced Engineering Mathematics*. 10th ed. Hoboken, New Jersey: John Wiley & Sons Inc., 2011. 124-165. Print.

[2] "Differential Equations - Modeling." *Differential Equations - Modeling*. Paul's Online Math Notes, n.d. Web. 04 June 2016.
<<http://tutorial.math.lamar.edu/Classes/DE/SystemsModeling.aspx>>.

[3] "Differential Equations - Undetermined Coefficients." *Differential Equations - Undetermined Coefficients*. Paul's Online Math Notes, n.d. Web. 04 June 2016.
<<http://tutorial.math.lamar.edu/Classes/DE/UndeterminedCoefficients.aspx>>.

[4] "Differential Equations - Modeling with First Order DE's." *Differential Equations - Modeling with First Order DE's*. Paul's Online Math Notes, n.d. Web. 04 June 2016.
<<http://tutorial.math.lamar.edu/Classes/DE/Modeling.aspx>>.

8. Appendix

8.1 Part 1 Matlab Code

8.1.1 Run 1

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=100;
a12=b/c
d=16;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=200;
a21=d/f
g=10;
h=100;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 40 e^(-0.04)t + 120 e^(-0.2)t
% Y2 = 26.68 e^(-0.04)t - 240 e^(-0.2)t
```

8.2 Part 2 Matlab Code

8.2.1 Run 1

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=10;
a12=b/c
d=16;
f=50;
```

```
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=10;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 13.98 e^(-0.1844)t + 146.01 e^(-1.7356)t
% Y2 = 3.1615 e^(-0.1844)t - 344.49 e^(-1.7356)t
```

8.2.2 Run 2

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=20;
a12=b/c
d=16;
f=50;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=20;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
```

```

V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 31.01 e^(-0.1681)t + 128.98
e^(-0.9519)t
% Y2 = 15.70 e^(-0.1681)t - 271.70
e^(-0.9519)t

```

8.2.3 Run 3

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=50;
a12=b/c
d=16;
f=50;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=50;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 80 e^(-0.124)t + 80 e^(-
0.516)t
% Y2 = 130.4 e^(-0.124)t - 130.4 e^(-
0.516)t

```

8.2.4 Run 4

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)

```

```

b=6;
c=200;
a12=b/c
d=16;
f=50;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=200;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 18.0323 e^(-0.3549)t +
141.9677 e^(-0.0451)t
% Y2 = -20.98 e^(-0.3549)t + 1300.99
e^(-0.0451)t

```

8.2.5 Run 5

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=500;
a12=b/c
d=16;
f=50;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=500;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 6.5153 e^(-0.3328)t + 153.487
e^(-0.0192)t
% Y2 = -6.9316 e^(-0.3328)t + 3846.92
e^(-0.0192)t

```

8.2.6 Run 6

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1)+ a12(Y2)
b=6;
c=10;
a12=b/c
d=16;
f=100;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1)+ a22(Y2)
d=16;
f=100;
a21=d/f
g=10;
h=10;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 6.5153 e^(-0.0962)t + 153.4847
e^(-1.6638)t
% Y2 = 0.6932 e^(-0.0962)t - 384.69
e^(-1.6638)t

```

8.2.7 Run 7

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1)+ a12(Y2)
b=6;
c=20;
a12=b/c
d=16;
f=100;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1)+ a22(Y2)
d=16;
f=100;
a21=d/f
g=10;
h=20;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 13.98 e^(-0.0922)t + 146.01
e^(-0.8678)t
% Y2 = 3.1579 e^(-0.0922)t - 344.49
e^(-0.8678)t

```

8.2.8 Run 8

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1)+ a12(Y2)
b=6;
c=50;
a12=b/c
d=16;
f=100;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1)+ a22(Y2)
d=16;
f=100;

```

```

a21=d/f
g=10;
h=50;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 40 e^(-0.08)t + 120 e^(-0.40)t
% Y2 = 26.68 e^(-0.08)t - 240 e^(-
0.40)t

```

8.2.9 Run 9

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=200;
a12=b/c
d=16;
f=100;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=100;
a21=d/f
g=10;
h=200;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]

```

```

b = [160;0];
C = inv(J)*b
% Y1 = 40 e^(-0.2)t + 120 e^(-0.04)t
% Y2 = -53.32 e^(-0.2)t + 480 e^(-
0.04)t

```

8.2.10 Run 10

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=500;
a12=b/c
d=16;
f=100;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=100;
a21=d/f
g=10;
h=500;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 13.98 e^(-0.1736)t + 120 e^(-
0.0184)t
% Y2 = -15.80 e^(-0.1736)t + 1722.46
e^(-0.0184)t

```

8.2.11 Run 11

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=10;
a12=b/c
d=16;

```



```

f=150;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=150;
a21=d/f
g=10;
h=10;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 4.23 e^(-0.065)t + 153.76 e^(-1.64)t
% Y2 = 0.294 e^(-0.065)t - 393.40 e^(-1.64)t

```

8.2.12 Run 12

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=20;
a12=b/c
d=16;
f=150;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=150;
a21=d/f
g=10;
h=20;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);

```

```

V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 8.9071 e^(-0.0632)t + 151.0929 e^(-0.8434)t
% Y2 = 1.291 e^(-0.0632)t - 371.0690 e^(-0.8434)t

```

8.2.13 Run 13

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=50;
a12=b/c
d=16;
f=150;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=150;
a21=d/f
g=10;
h=50;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 25.1205 e^(-0.0578)t + 134.8795 e^(-0.3688)t
% Y2 = 10.221 e^(-0.0578)t - 294.67 e^(-0.3688)t

```

8.2.14 Run 14

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=200;
a12=b/c
d=16;
f=150;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=150;
a21=d/f
g=10;
h=200;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 61.6467 e^(-0.1515)t + 98.3533
e^(-0.0352)t
% Y2 = -92.026 e^(-0.1515)t + 234.248
e^(-0.0352)t
```

8.2.15 Run 15

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=500;
a12=b/c
d=16;
f=150;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=150;
a21=d/f
```

```
g=10;
h=500;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 22.2404 e^(-0.1210)t +
137.7596 e^(-0.0176)t
% Y2 = -26.641 e^(-0.1210)t + 1022.2
e^(-0.0176)t
```

8.2.16 Run 16

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=10;
a12=b/c
d=16;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=200;
a21=d/f
g=10;
h=10;
i= 6;
a22= -i/h-g/h
```

```
A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
```

```

b = [160;0];
C = inv(J)*b
% Y1 = 3.1303 e^(-0.0491)t + 156.8693
e^(-1.6309)t
% Y2 = 0.1615 e^(-0.0491)t - 405.4924
e^(-1.6309)t

```

8.2.17 Run 17

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)

```

```

b=6;
c=20;
a12=b/c
d=16;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=200;
a21=d/f
g=10;
h=20;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 6.1557 e^(-0.0481)t + 153.4847
e^(-0.8319)t
% Y2 = 0.6932 e^(-0.0481)t - 384.69
e^(-0.8319)t

```

8.2.18 Run 18

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=50;
a12=b/c
d=16;

```

```

f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)

```

```

d=16;
f=200;
a21=d/f
g=10;
h=50;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 18.0323 e^(-0.0451)t +
141.9677 e^(-0.3549)t
% Y2 = 5.2473 e^(-0.0451)t - 325.24
e^(-0.3549)t

```

8.2.19 Run 19

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)

```

```

b=6;
c=200;
a12=b/c
d=16;
f=200;
a11=-d/f

```

```

% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)

```

```

d=16;
f=200;
a21=d/f
g=10;
h=200;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)

```

```

[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 80 e^(-0.0310)t + 80 e^(-0.1290)t
% Y2 = 130.64 e^(-0.0310)t - 130.64 e^(-0.1290)t

```

8.2.20 Run 20

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=500;
a12=b/c
d=16;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=200;
a21=d/f
g=10;
h=500;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 31.0102 e^(-0.0952)t + 128.98 e^(-0.0168)t
% Y2 = -39.258 e^(-0.0952)t + 679.26 e^(-0.0168)t

```

8.2.21 Run 21

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=10;
a12=b/c
d=16;
f=250;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=250;
a21=d/f
g=10;
h=10;
i= 6;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 2.4835 e^(-0.0394)t + 157.5156 e^(-1.6246)t
% Y2 = 0.1018 e^(-0.0394)t - 409.7 e^(-1.6246)t

```

8.2.22 Run 22

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=20;
a12=b/c
d=16;
f=250;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=250;
a21=d/f

```

```

g=10;
h=20;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 5.1315 e^(-0.0388)t + 154.8586
e^(-0.8252)t
% Y2 = 0.4315 e^(-0.0388)t - 392.96
e^(-0.8252)t

```

8.2.23 Run 23

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=50;
a12=b/c
d=16;
f=250;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=250;
a21=d/f
g=10;
h=50;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]

```

```

b = [160;0];
C = inv(J)*b
% Y1 = 13.98 e^(-0.0369)t + 146.0110
e^(-0.3471)t
% Y2 = 3.1594 e^(-0.0369)t + 344.498
e^(-0.3471)t

```

8.2.24 Run 24

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=200;
a12=b/c
d=16;
f=250;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=250;
a21=d/f
g=10;
h=200;
i= 6;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 65.6316 e^(-0.0275)t + 94.3684
e^(-0.1165)t
% Y2 = 79.9458 e^(-0.0275)t + 165.276
e^(-0.1165)t

```

8.2.25 Run 25

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=6;
c=500;
a12=b/c
d=16;
f=250;

```

```

a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=250;
a21=d/f
g=10;
h=500;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 40 e^(-0.080)t + 120 e^(-
0.0160)t
% Y2 = -53.332 e^(-0.080)t + 480 e^(-
0.0160)t

```

8.3 Part 3 Matlab Code (Flow Changes)

8.3.1 Run 1

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=1;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
g=10;
h=100;
i= 1;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)

```

```

Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 0.7159 e^(-0.0045)t + 159.284
e^(-0.1103)t
% Y2 = 0.0339 e^(-0.0045)t - 1680.03
e^(-0.1103)t

```

8.3.2 Run 2

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=2;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
g=10;
h=100;
i= 2;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 1.1831 e^(-0.0041)t + 158.81
e^(-0.1209)t
% Y2 = 0.0511 e^(-0.0041)t - 920 e^(-
0.1209)t

```

8.3.3 Run 3

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=5;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
g=10;
h=100;
i= 5;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 2.0244 e^(-0.0025)t + 157.97
e^(-0.2025)t
% Y2 = 0.0512 e^(-0.0025)t - 312.049
e^(-0.2025)t
```

8.3.4 Run 4

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=10;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
```

```
g=10;
h=100;
i= 10;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 2.0244 e^(-0.0025)t + 157.97
e^(-0.2025)t
% Y2 = 0.0512 e^(-0.0025)t - 312.049
e^(-0.2025)t
```

8.3.5 Run 5

```
% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=100;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
g=10;
h=100;
i= 100;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
```

```

b = [160;0];
C = inv(J)*b
% Y1 = 0.6590 e^(-0.0005)t + 159.34
e^(-1.1045)t
% Y2 = 0.00296 e^(-0.-0005)t - 175.19
e^(-1.1045)t

```

8.3.6 Run 6

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=1;
c=100;
a12=b/c
d=2;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=2;
f=200;
a21=d/f
g=10;
h=100;
i=1;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 158.44 e^(-0.1110)t + 1.5535
e^(-0.0090)t
% Y2 = -1600.08 e^(-0.1110)t + 0.1537
e^(-0.0090)t

```

8.3.7 Run 7

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=2;
c=100;
a12=b/c
d=2;

```

```

f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=2;
f=200;
a21=d/f
g=10;
h=100;
i=2;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 2.5203 e^(-0.0082)t + 157.47
e^(-0.1218)t
% Y2 = 0.2253 e^(-0.0082)t - 880.23
e^(-0.1218)t

```

8.3.8 Run 8

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=5;
c=100;
a12=b/c
d=2;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=2;
f=200;
a21=d/f
g=10;
h=100;
i=5;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)

```



```

[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 3.7937 e^(-0.0065)t + 156.20
e^(-0.1535)t
% Y2 = 0.2644 e^(-0.0065)t - 448.24
e^(-0.1535)t

```

8.3.9 Run 9

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=10;
c=100;
a12=b/c
d=2;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=2;
f=200;
a21=d/f
g=10;
h=100;
i= 10;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 4.094 e^(-0.0049)t + 153.905
e^(-0.2051)t
% Y2 = 0.2094 e^(-0.0049)t - 300.29
80 e^(-0.2051)t

```

8.3.10 Run 10

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=100;
c=100;
a12=b/c
d=2;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=2;
f=200;
a21=d/f
g=10;
h=100;
i= 100;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 1.3136 e^(-0.0009)t + 158.68
e^(-1.1091)t
% Y2 = 0.01195 e^(-0.0009)t - 174.4
e^(-1.1091)t

```

8.3.11 Run 11

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=1;
c=100;
a12=b/c
d=5;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=5;
f=200;
a21=d/f

```

```

g=10;
h=100;
i= 1;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 5.0208 e^(-0.0222)t + 154.97
e^(-0.1128)t
% Y2 = 1.4289 e^(-0.0222)t - 1361.43
e^(-0.1128)t

```

8.3.12 Run 12

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=2;
c=100;
a12=b/c
d=5;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=5;
f=200;
a21=d/f
g=10;
h=100;
i= 2;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]

```

```

b = [160;0];
C = inv(J)*b
% Y1 = 7.619 e^(-0.02)t + 152.381
e^(-0.1250)t
% Y2 = 1.904 e^(-0.02)t - 761.9 e^(-
0.1250)t

```

8.3.13 Run 13

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=5;
c=100;
a12=b/c
d=5;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=5;
f=200;
a21=d/f
g=10;
h=100;
i= 5;
a22= -i/h-g/h

```

```

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 10.368 e^(-0.0157)t + 149.631
e^(-0.1593)t
% Y2 = 1.9294 e^(-0.0157)t - 401.92
e^(-0.1593)t

```

8.3.14 Run 14

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=10;
c=100;
a12=b/c
d=5;

```

```

f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=5;
f=200;
a21=d/f
g=10;
h=100;
i= 10;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 10.54 e^(-0.0117)t + 149.45
e^(-0.2133)t
% Y2 = 1.3937 e^(-0.0117)t - 281.38
e^(-0.2133)t

```

8.3.15 Run 15

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=100;
c=100;
a12=b/c
d=5;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=5;
f=200;
a21=d/f
g=10;
h=100;
i= 100;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)

```

```

[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 3.2518 e^(-0.0022)t + 156.74
e^(-1.1228)t
% Y2 = 0.0741 e^(-0.0022)t - 172.07
e^(-1.1228)t

```

8.3.16 Run 16

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=1;
c=100;
a12=b/c
d=10;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=10;
f=200;
a21=d/f
g=10;
h=100;
i= 1;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 15.857 e^(-0.0126)t + 144.14
e^(-0.1174)t
% Y2 = 11.761 e^(-0.0126)t - 971.74
e^(-0.1174)t

```

8.3.17 Run 17

```
% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=2;
c=100;
a12=b/c
d=10;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=10;
f=200;
a21=d/f
g=10;
h=100;
i= 2;
a22= -i/h-g/h

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 20.64 e^(-0.0328)t + 139.359
% e^(-0.1322)t
% Y2 = 12.559 e^(-0.0328)t - 572.53
% e^(-0.1322)t
```

8.3.18 Run 18

```
% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=5;
c=100;
a12=b/c
d=10;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=10;
f=200;
a21=d/f
```

```
g=10;
h=100;
i= 5;
a22= -i/h-g/h

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 136.56 e^(-0.1707)t + 23.431
% e^(-0.0293)t
% Y2 = -329.68 e^(-0.1707)t + 9.705
% e^(-0.0293)t
```

8.3.19 Run 19

```
% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=10;
c=100;
a12=b/c
d=10;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=10;
f=200;
a21=d/f
g=10;
h=100;
i= 10;
a22= -i/h-g/h

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
```

```

b = [160;0];
C = inv(J)*b
% Y1 = 21.791 e^(-0.0219)t + 138.208
e^(-0.2281)t
% Y2 = 6.119 e^(-0.0219)t - 246.12
e^(-0.2281)t

```

8.3.20 Run 20

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=100;
c=100;
a12=b/c
d=10;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=10;
f=200;
a21=d/f
g=10;
h=100;
i=100;
a22=-i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 6.3979 e^(-0.0044)t + 153.6
e^(-1.1456)t
% Y2 = 0.2917 e^(-0.0044)t - 168.28
e^(-1.1456)t

```

8.3.21 Run 21

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=1;
c=100;
a12=b/c
d=100;

```

```

f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=100;
f=200;
a21=d/f
g=10;
h=100;
i=1;
a22=-i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 4.7920 e^(-0.5124)t + 153.208
e^(-0.0976)t
% Y2 = -5.954 e^(-0.5124)t + 6165.47
e^(-0.0976)t

```

8.3.22 Run 22

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=2;
c=100;
a12=b/c
d=100;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=100;
f=200;
a21=d/f
g=10;
h=100;
i=2;
a22=-i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)

```

```

[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 9.2063 e^(-0.5247)t + 150.79
e^(-0.0953)t
% Y2 = -7.9708 e^(-0.5247)t + 3051.31
e^(-0.0953)t

```

8.3.23 Run 23

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=5;
c=100;
a12=b/c
d=100;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=100;
f=200;
a21=d/f
g=10;
h=100;
i= 5;
a22= -i/h-g/h

```

```

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 20.64 e^(-0.5608)t + 139.35
e^(-0.0892)t
% Y2 = -25.11 e^(-0.5608)t + 1145.03
e^(-0.0892)t

```

8.3.24 Run 24

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=10;
c=100;
a12=b/c
d=100;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=100;
f=200;
a21=d/f
g=10;
h=100;
i= 10;
a22= -i/h-g/h

A=[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 35.43 e^(-0.6193)t + 124.56
e^(-0.0807)t
% Y2 = -42.25 e^(-0.6193)t + 522.23
e^(-0.0807)t

```

8.3.25 Run 25

```

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=100;
c=100;
a12=b/c
d=100;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=100;
f=200;
a21=d/f
g=10;

```

```

h=100;
i= 100;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1);
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 48.754 e^(-0.0319)t + 111.24
e^(-1.5681)t
% Y2 = 22.824 e^(-0.0319)t - 118.81
e^(-1.5681)t

```

8.4 Part 1 Matlab Code (Including Plots)

8.4.1 Run 1

```

clear
clear all
clc

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)
b=6;
c=100;
a12=b/c
d=16;
f=200;
a11=-d/f
% Tank 2
% Y' = Inflow/Min - Outflow/Min
% Y' = a21(Y1) + a22(Y2)
d=16;
f=200;
a21=d/f
g=10;
h=100;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
roots(P)
% Eigenvalues
Eigenvalues = eig(A)

```

```

% Eigenvectors
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1);
V2 = V(:,2);
V22 = V2/V(1,2);

Vectors = table(V22,V11)
% Displaying Eigenvalues and
Eigenvalues in a table
K = table (Eigenvalues,V22,V11)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
% Solving for Constants
C = inv(J)*b
% Y1 = 40 e^(-0.2)t + 120 e^(-0.04)t
% Y2 = -80 e^(-0.2)t + 80 e^(-0.04)t

% To plot y(t) we must model y(t) =
C1(y1)+C2(y2)
% Where C are the constants C1 and C2
t = [0 27.5 50 100]';
y = [160 40.1080 16.2420 2.1979]';
T = (0:27.5:50:100)';
% Modeling y(t) = C1(y1)+C2(y2)= 40
e^(-0.2)t + 120 e^(-0.04)t
Y1 = [exp(-0.2*T) exp(-0.04*T)]*C;
% % % Solving for T and Y
% Modeling y(t) = C1(y1)+C2(y2)= -80
e^(-0.2)t + 80 e^(-0.04)t
z = [-80 80]'
Y2 = [exp(-0.2*T) exp(-0.04*T)]*z
% Displaying Tables for T,Y1 and T2,Y2
B = table(T,Y1)
w = table(T,Y2)
plot(T,Y1,'-',t,y,'o',T,Y2,'r')
title('y(t) vs. Time (Minutes)')
xlabel('Time (Minutes)')
ylabel(' y(t)')
grid

```

8.5 Part 2 Matlab Code (Including Plots)

8.5.1 Run 1

```

clear
clear all
clc

% Tank 1
% Y' = Inflow/Min - Outflow/Min
% Y' = -a11(Y1) + a12(Y2)

```

```

b=6;
c=20;
a12=b/c
d=16;
f=50;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=16;
f=50;
a21=d/f
g=10;
h=20;
i= 6;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 31.01 e^(-0.1681)t + 128.98
e^(-0.9519)t
% Y2 = 15.70 e^(-0.1681)t - 271.70
e^(-0.9519)t

% To plot y(t) we must model y(t) =
C1(y1)+C2(y2)
% Where C are the constants C1 and C2
t = [0 27.5 50 100]';
y = [160 0.33142 0.0069384 1.5524e-
06]';
T = (0:27.5:50:100)';
% Modeling y(t) = C1(y1)+C2(y2)=
31.01 e^(-0.1681)t + 128.98 e^(-
0.9519)t
Y1 = [exp(-0.1681*T) exp(-
0.9519*T)]*C;
% % % Solving for T and Y
% Modeling y(t) = C1(y1)+C2(y2)=
15.70 e^(-0.1681)t - 271.70 e^(-
0.9519)t
z =[15.70 -271.70]'
Y2 = [exp(-0.1681*T) exp(-0.9519*T)]*z
% Displaying Tables
B = table(T,Y1)
w = table(T,Y2);

```

```

plot(T,Y1,'-',t,y,'o',T,Y2,'r')
title('y(t) vs. Time (Minutes)')
xlabel('Time (Minutes)')
ylabel(' y(t)')
grid

```

8.6 Part 3 Matlab Code (Including Plots)

8.6.1 Run 1

```

% Tank 1
% Y'= Inflow/Min - Outflow/Min
% Y'= -a11(Y1)+ a12(Y2)
b=1;
c=100;
a12=b/c
d=1;
f=200;
a11=-d/f
% Tank 2
% Y'= Inflow/Min - Outflow/Min
% Y'= a21(Y1)+ a22(Y2)
d=1;
f=200;
a21=d/f
g=10;
h=100;
i= 1;
a22= -i/h-g/h

A =[a11 a12;a21 a22]
P = poly(A)
Eig = eig(A)
[V,D] = eig(A);
V1 = V(:,1);
V11 = V1/V(1,1)
V2 = V(:,2);
V22 = V2/V(1,2)
% C1 + 1.5C2 = 160
% -2C1 + C2 = 0
J = [V22,V11]
b = [160;0];
C = inv(J)*b
% Y1 = 0.7159 e^(-0.0045)t + 159.284
e^(-0.1103)t
% Y2 = 0.0339 e^(-0.0045)t - 1680.03
e^(-0.1103)t

% To plot y(t) we must model y(t) =
C1(y1)+C2(y2)
% Where C are the constants C1 and C2
t = [0 27.5 50 100]';
y = [160 8.7399 1.2129 0.45906]';
T = (0:27.5:50:100)';

```



```

% Modeling  $y(t) = C1(y1)+C2(y2)= 40$ 
 $e^{(-0.2)t} + 120 e^{(-0.04)t}$ 
Y1 = [exp(-0.0045*T) exp(-
0.1103*T)]*C;
% % % Solving for T and Y
% Modeling  $y(t) = C1(y1)+C2(y2)= -80$ 
 $e^{(-0.2)t} + 80 e^{(-0.04)t}$ 
z =[0.0339 -1680.03]'
Y2 = [exp(-0.0045*T) exp(-0.1103*T)]*z
% Displaying Tables
B = table(T,Y1)
w = table(T,Y2)
plot(T,Y1,'-',t,y,'o',T,Y2,'r')
xlabel('Time (Mins)')
ylabel(' y(t)')
grid

```