

## ESTIMATES OF RADIOACTIVE DECAY BY THE EMISSION OF NUCLEI HEAVIER THAN $\alpha$ -PARTICLES<sup>†</sup>

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**Abstract:** We estimate the lifetimes for radioactive decay of a nucleus by the emission of  $\alpha$ -particles or heavier fragments like  $^{14}\text{C}$ , by treating these processes as extreme cases of spontaneous fission. The lifetime is accordingly written as a frequency factor of the order of collective nuclear oscillations ( $10^{-21}$ – $10^{-22}$  sec) times a Gamow penetrability factor for the appropriate deformation-energy barrier. For the very asymmetric decays, an approximation to the barrier is obtained by combining the Coulomb repulsion between the fragments with the nuclear proximity potential (up to contact) and interpolating smoothly between the contact configuration and the configuration of the parent nucleus. We give a closed formula for the penetrability factor and find that, to within about one power of ten, we can account for the recently observed branching ratios between  $\alpha$ -particle and  $^{14}\text{C}$  emissions from  $^{222,223,224}\text{Ra}$ . We apply our method to calculate branching ratios for other exotic decays (involving isotopes of O and Ne among others) and estimate that there may be a number of such decays that will be accessible to observation.

### 1. Introduction

The recently discovered <sup>1)</sup> spontaneous radioactive decay of  $^{223}\text{Ra}$  into  $^{209}\text{Pb}$  by the emission of  $^{14}\text{C}$  has been confirmed in refs. <sup>2,3)</sup>, and similar decays of  $^{222}\text{Ra}$  into  $^{208}\text{Pb}$  and of  $^{224}\text{Ra}$  into  $^{210}\text{Pb}$  have been reported in ref. <sup>3)</sup>. The ratios of the rates of these exotic decay modes to the corresponding rates of  $\alpha$ -particle emission are given in ref. <sup>3)</sup> as  $(3.7 \pm 0.5) \times 10^{-10}$ ,  $(6.1 \pm 0.8) \times 10^{-10}$  and  $(4.3 \pm 1.1) \times 10^{-11}$  for  $^{222}\text{Ra}$ ,  $^{223}\text{Ra}$  and  $^{224}\text{Ra}$ , respectively. In refs. <sup>1,3)</sup> these experimental branching ratios have been compared only with the ratios of Gamow penetrability factors for pure Coulomb barriers, cut off at a sharp (contact) distance, parameterized as  $r_0 (A_1^{1/3} + A_2^{1/3})$ , where  $A_1$ ,  $A_2$  are the mass numbers of the two decay fragments. Values of  $r_0$  in the range of 1.15–1.25 fm were tried in ref. <sup>1)</sup> with the result that the Gamow factors would, by themselves, lead to branching ratios several orders of magnitude higher than the observed values. In ref. <sup>1)</sup> the conclusion is drawn that, in the case of  $^{223}\text{Ra}$ , the emission rate of  $^{14}\text{C}$  may be understood as a barrier-penetration phenomenon

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slowed down by a “preformation probability factor” in the range of  $7 \times 10^{-5}$ – $4 \times 10^{-7}$  times the preformation probability for  $\alpha$ -emission from the same nucleus.

In this paper, we would like to draw attention to the fact that, if a more realistic estimate of the potential-energy barrier is used in the penetrability calculation, the branching ratios come out to be reasonably close to the three measured values (without the use of any adjustable parameters and without invoking hypothetical preformation probability factors). This appears to us consistent with the point of view that the emission of fragments like  $^{14}\text{C}$  – and even, to a certain extent,  $\alpha$ -emission – may be looked upon simply as extremely asymmetric types of spontaneous fission<sup>4)</sup>. In such an approach one expects to be able to estimate the decay lifetime as the product of a frequency factor of the order of nuclear collective oscillations (in the range  $10^{-22}$ – $10^{-21}$  sec) times a penetrability factor through a properly estimated deformation–energy barrier. There is no room in such fission-like calculations for preformation factors of *several* powers of ten. Thus, in the case of uranium fission, for example, one does not have to wait for a barium fragment, say, to be preformed inside the parent nucleus. The barium is not “preformed”, but takes shape as part of the geometrical deformation process, i.e. as part of the process of barrier penetration itself.

## 2. The barrier penetrability calculation

To implement this point of view, we have constructed deformation-energy barriers by modifying the Coulomb repulsion between the fragments by the nuclear proximity potential up to contact of the fragments, and continuing beyond contact by an interpolation to the configuration of the parent nucleus. Fig. 1 shows such barriers for the decay of  $^{222}\text{Ra}$  by  $\alpha$  and by  $^{14}\text{C}$  emission (see also fig. 2). The abscissa is in fm and gives the major axis  $L$  (i.e. the extreme extension) of the configuration in question (upper scale) or the distance  $z$  between the near surfaces of the fragments (lower scale). The value  $L = L_c = 2(C_1 + C_2) = 2r_c$  corresponds to contact of the fragments, assumed spherical and with radii  $C_1$  and  $C_2$  ( $r_c$  is the center separation at contact). Down to contact the potential was calculated using the canonical proximity potential of refs.<sup>5,6)</sup> without the adjustment of any parameters. After contact, when the two fragments are fusing, the proximity treatment soon becomes inapplicable. To estimate the appearance of the deformation energy below contact, we had recourse to a smooth power-law interpolation between  $L = 2r_c$  and  $L = L_0 = 2C$ , where  $C$  corresponds to the radius of the compound system (the parent nucleus). (For this value of  $L$  the deformation potential is zero by definition.) This is a somewhat arbitrary prescription for interpolating the deformation energy between  $V(\text{contact})$  and  $V=0$  but, as seen from fig. 1, only a relatively small part of the potential-energy barrier is affected by this pre-scission uncertainty. The major part of the barrier, even in the case of  $^{14}\text{C}$  emission, corresponds to configurations of *separated fragments*. This makes an estimate of the deformation energy for these

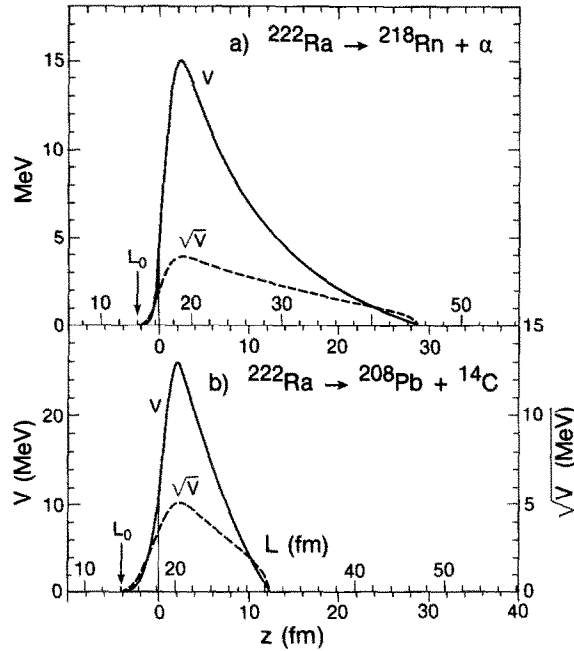


Fig. 1. The deformation-energy barrier  $V(L)$  for the emission of an  $\alpha$ -particle (a), or a  $^{14}\text{C}$  nucleus (b), from  $^{222}\text{Ra}$ . The dashed curves are the integrands in the penetrability integral. The total extension of the configuration is  $L$  and the distance between the near surfaces of the fragments is  $z$ . Most of the barrier corresponds to separated fragments (the region to the right of the vertical line at  $z=0$ ).

very asymmetric divisions far easier and more reliable than for conventional fission processes.

The explicit expression for the deformation energy  $V(L)$  is

$$V(L) = \begin{cases} M_1 + M_2 - M + Z_1 Z_2 e^2 / r + V_p(z), & \text{for } L > L_c \\ a(L - L_0)^\nu, & \text{for } L_0 < L < L_c, \end{cases} \quad (1)$$

$$(2)$$

where  $r = L - C_1 - C_2$  is the separation between fragment centers and  $a$  and  $\nu$  are parameters determined by the requirement of a smooth fit at  $L = L_c$ . In the above,  $M_1$ ,  $M_2$  are the masses (or mass defects) in MeV and  $Z_1$ ,  $Z_2$  the atomic numbers of the two fragments,  $e^2 = 1.4400 \text{ MeV} \cdot \text{fm}$ , and  $V_p(z)$  is the nuclear proximity interaction given by

$$V_p(z) = K\Phi(z/b), \quad (3)$$

where  $K = 4\pi\bar{R}\gamma b$ ,  $\bar{R}$  is the reduced radius of the system, given by  $C_1 C_2 / (C_1 + C_2)$ ,  $\gamma$  is the nuclear surface tension coefficient,  $b$  is the width (diffuseness) of the nuclear surface and  $\Phi$  is the universal nuclear proximity function. The particular power-law interpolation defined by eq. (2), with the exponent  $\nu$  determined by the requirement of smooth continuity, has no theoretical foundation and was chosen for algebraic

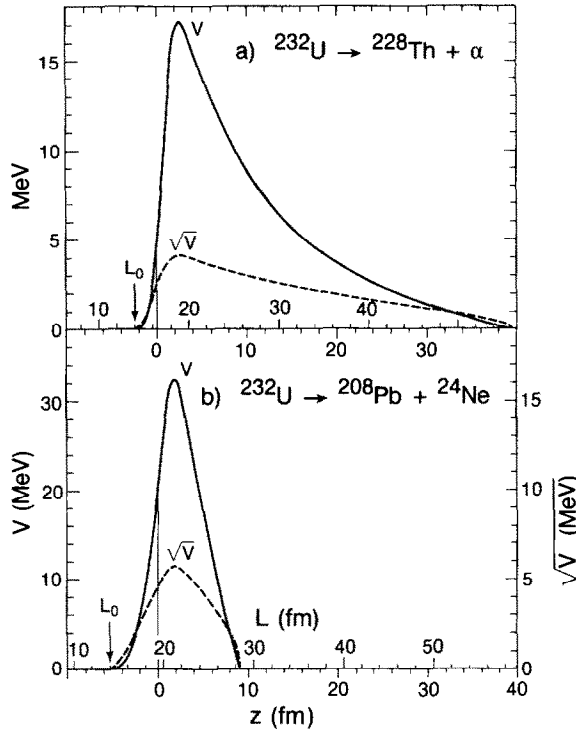


Fig. 2. Same as fig. 1, but for the decay of  $^{232}\text{U}$ .

convenience. (Theoretically, the potential energy of a system near equilibrium should be quadratic in the deformation energy, suggesting  $\nu = 2$ . On the other hand, the zero-point motion in the disintegration degree of freedom puts the energy level of the disintegrating nucleus above the minimum in the potential energy, with the result that the barrier to be penetrated does not begin until a finite deviation of the deformation from the value corresponding to the potential-energy minimum, at which point the barrier comes in with a finite derivative. Such behaviour might be mocked up by a relatively *high* value of  $\nu$ . Examples of actual values of  $\nu$ , given by eq. (10) below, are 4.678 for  $\alpha$ -decay and  $\nu = 3.366$  for  $^{14}\text{C}$  decay of  $^{222}\text{Ra}$ .)

We have used the following formulae from refs. <sup>5,6</sup>):

$$\gamma = 0.9517[1 - 1.7826((N - Z)/A)^2] \text{ MeV/fm}^2, \quad (4)$$

where  $N$ ,  $Z$ ,  $A$  refer to the neutron, proton and mass numbers of the parent nucleus,  $b = 1 \text{ fm}$ , and the (“central”) radius  $C_i$  ( $C_1$ ,  $C_2$  or  $C$ ) is given in terms of the effective sharp radius  $R_i$  by

$$C_i = R_i - b^2/R_i, \quad (5)$$

where a semi-empirical formula for  $R_i$  is given in ref. <sup>5)</sup> as

$$R_i = 1.28A_i^{1/3} - 0.76 + 0.8A_i^{-1/3} \text{ fm}. \quad (6)$$

The Gamow penetrability factor  $G$  is given by

$$\begin{aligned} G &= \exp \left[ (2/\hbar) \int_{z_0}^{z_{\text{exit}}} \sqrt{2M_r V} dz \right] \\ &= \exp \left[ 2\sqrt{2A_r}(\sqrt{mc^2}/\hbar c) \int_{z_0}^{z_{\text{exit}}} \sqrt{V} dz \right] \\ &= \exp [(0.43749/\sqrt{\text{MeV}})(b/\text{fm})\sqrt{A_r S}], \end{aligned} \quad (7)$$

where  $M_r$  is the effective mass appropriate to the disintegration degree of freedom, and which we take to be simply the reduced mass of the separating fragments, since most of the barrier penetration is taking place in the post-scission regime. The reduced mass number  $A_1 A_2 / A$  is denoted by  $A_r$  and  $mc^2$  is the nuclear mass unit, which we took as 931.5 MeV. The penetrability integral  $S$  is given by

$$S = \int_{\zeta_0}^{\zeta_{\text{exit}}} \sqrt{V(\zeta)} d\zeta, \quad (8)$$

where  $\zeta = z/b$ ,  $\zeta_0 \equiv (L_0 - L_c)/b = 2(C - C_1 - C_2)/b$  and  $\zeta_{\text{exit}}$  is defined by  $V(\zeta_{\text{exit}}) = 0$ . The integral  $S$  may be evaluated analytically in the interval  $\zeta_0 < \zeta < 0$  as well as beyond the point where the proximity potential is negligible, say  $\zeta > 6$ . In the intermediate range,  $0 < \zeta < 6$ , numerical integration has to be resorted to. If Simpson's rule is used with seven ordinates  $\sqrt{V_0}, \sqrt{V_1}, \dots, \sqrt{V_6}$  at  $\zeta = 0, 1 \dots 6$ , we find the following quite accurate approximation for  $S$ :

$$\begin{aligned} S &= \sqrt{V_0} [(-\zeta_0)^{-1} + \frac{1}{2}(V'_0/V_0)]^{-1} \\ &\quad + \frac{1}{3}[(\sqrt{V_0} + \sqrt{V_6}) + 2(\sqrt{V_2} + \sqrt{V_4}) + 4(\sqrt{V_1} + \sqrt{V_3} + \sqrt{V_5})] \\ &\quad - \rho_6 \sqrt{V_6} + (D/\sqrt{Q}) \tan^{-1} \sqrt{V_6/Q}, \end{aligned} \quad (9)$$

where  $\rho_6 = (r_c/b) + 6$  is the center separation in units of  $b$  at  $\zeta = 6$ ,  $D = Z_1 Z_2 e^2 / b$  and  $Q = M - M_1 - M_2$  is the energy release in the disintegration. The first term in  $S$  (the contribution from the range  $\zeta_0 < \zeta < 0$ ) is obtained by making use of the following expressions for  $\nu$  and  $a$  (which result from applying the smooth continuity condition on  $V$  at  $z = 0$ ):

$$\nu = -\zeta_0 V'_0 / V_0, \quad (10)$$

$$a = V_0 / (-\zeta_0)^\nu, \quad (11)$$

where

$$\begin{aligned} V'_0 &= \left. \frac{dV}{d\zeta} \right|_{\zeta=0} = -Z_1 Z_2 e^2 b / r_c^2 + K\Phi'(0) \\ &= -Db^2 / r_c^2 + 0.9270K. \end{aligned} \quad (12)$$

To calculate  $\Phi(\zeta)$ , the approximation given in ref. <sup>6)</sup> may be used:

$$\Phi(\zeta) \approx \begin{cases} -4.41 e^{-\zeta/0.7176}, & \text{for } \zeta \geq 1.9475 \\ -1.7817 + 0.9270\zeta + 0.01696\zeta^2 - 0.05148\zeta^3, & \text{for } 0 \leq \zeta \leq 1.9475. \end{cases} \quad (13)$$

Alternatively (and this is what we used)  $\Phi(\zeta)$  is tabulated in ref. <sup>4)</sup>. The seven values of  $\Phi$  required to evaluate eq. (9) are as follows:  $\Phi(0) = -1.7817$ ,  $\Phi(1) = -0.8594$ ,  $\Phi(2) = -0.2689$ ,  $\Phi(3) = -0.0674$ ,  $\Phi(4) = -0.0167$ ,  $\Phi(5) = -0.0042$ ,  $\Phi(6) = -0.0010$ .

### 3. Results

Table 1 shows, in column 2, the measured branching ratios (the ratios  $\tau_\alpha/\tau_C$  of the lifetimes for  $\alpha$  and  $^{14}\text{C}$  emission) compared with the calculated ratios of the penetrability factors,  $G_\alpha/G_C$  (column 3). The next column gives the ratios  $(G_\alpha/G_C):(\tau_\alpha/\tau_C)$ . We see that the penetrability ratios are within one power of ten of the branching ratios. Since the penetrability factors  $G_C$  (column 6) are of the order of 32–38 powers of 10, agreement to within one power of ten implies an accuracy in the penetrability integrals (involving the estimated deformation-energy barriers) of some 3%.

To test the absolute values of the lifetimes  $\tau_\alpha$ ,  $\tau_C$  that would be expected on the basis of this fission-like theory, we write

$$\tau_\alpha = \tau_0^\alpha G_\alpha, \quad (15)$$

$$\tau_C = \tau_0^C G_C, \quad (16)$$

where  $\tau_0^\alpha$ ,  $\tau_0^C$  are the frequency factors mentioned earlier, which ought to fall in the general range  $10^{-22}$ – $10^{-21}$  sec. Column 9 shows the value of  $\tau_0^\alpha$  deduced from the experimental  $\alpha$ -lifetime and the calculated  $G_\alpha$ , and column 10 shows the corresponding quantity  $\tau_0^C$  for  $^{14}\text{C}$  decay. We note that in the case of  $\alpha$ -decay the values of  $\tau_0^\alpha$

TABLE I  
 $\alpha$ -particle and  $^{14}\text{C}$  emissions from three isotopes of Ra

Parent nucleus	Experimental $\tau_\alpha/\tau_C$	Calculated $G_\alpha/G_C$	$\frac{G_\alpha}{G_C} : \frac{\tau_\alpha}{\tau_C}$	Calculated $G_\alpha$	Calculated $G_C$
$^{222}\text{Ra}$	$(3.7 \pm 0.5) \times 10^{-10}$	$1.678 \times 10^{-9}$	4.5	$2.884 \times 10^{23}$	$1.718 \times 10^{32}$
$^{223}\text{Ra}$	$(6.1 \pm 0.8) \times 10^{-10}$	$6.895 \times 10^{-9}$	11.3	$4.717 \times 10^{26}$	$6.842 \times 10^{34}$
$^{224}\text{Ra}$	$(4.3 \pm 1.1) \times 10^{-11}$	$6.150 \times 10^{-11}$	1.43	$4.378 \times 10^{27}$	$7.119 \times 10^{37}$
	Experimental $\tau_\alpha$ [sec]	Experimental $\tau_C$ [sec]	Deduced $\tau_0^\alpha$ [sec]	Deduced $\tau_0^C$ [sec]	
$^{222}\text{Ra}$	38	$1.03 \times 10^{11}$	$1.32 \times 10^{-22}$	$5.98 \times 10^{-22}$	
$^{223}\text{Ra}$	$0.985 \times 10^6$	$1.62 \times 10^{15}$	$2.09 \times 10^{-21}$	$2.36 \times 10^{-20}$	
$^{224}\text{Ra}$	$0.311 \times 10^6$	$7.23 \times 10^{15}$	$0.71 \times 10^{-22}$	$1.02 \times 10^{-22}$	

are about what one might expect, with the decay of the odd- $A$  nucleus  $^{223}\text{Ra}$  showing a hindrance factor of about 20 relative to its even-even neighbours. In the case of  $^{14}\text{C}$  decay the value of  $\tau_0^C$  for  $^{222}\text{Ra}$  is in the expected range, for  $^{223}\text{Ra}$  there seems to be present a hindrance factor of about 40 relative to  $^{222}\text{Ra}$  and for  $^{224}\text{Ra}$  there seems to be an *enhancement* of about a factor of 6 with respect to  $^{222}\text{Ra}$ .

#### 4. Discussion

The reasons why the present calculations give penetrability ratios several orders of magnitude smaller than those in ref. <sup>1)</sup> are actually two: the inclusion of the nuclear proximity interaction and the use of more realistic nuclear radii (eqs. (5) and (6)). The nuclear proximity attraction reduces the height and width of the barrier to be penetrated, and this is relatively more pronounced for the  $\alpha$ -particle than for  $^{14}\text{C}$ . This is because the proximity attraction is proportional to the reduced radius  $C_1 C_2 / (C_1 + C_2)$ , which scales (approximately) as the cube root  $A_2^{1/3}$  of the mass number of the small fragment, whereas the Coulomb repulsion scales approximately as the atomic number  $Z_2$ , roughly proportional to  $A_2$ . The ratio of the nuclear to the Coulomb potential, proportional to  $A_2^{-2/3}$ , increases with decreasing  $A_2$ .

The other reason for the enhanced emission of  $\alpha$ -particles in the present calculations is the use of realistic nuclear radii. First of all, one must realize that the radius relevant for locating the surfaces of interacting nuclei is the central radius  $C$  or the approximately equivalent half-density radius  $C_{1/2}$  (where the nuclear density has dropped to half its central value) and not the effective sharp radius  $R$ , which is the quantity approximately proportional to  $A^{1/3}$  [see ref. <sup>5)</sup>]. Now the central radius  $C$  (or  $C_{1/2}$ ) would not be proportional to  $A^{1/3}$  even if nuclei were incompressible and  $R$  were exactly proportional to  $A^{1/3}$ . Instead,  $C$  is related (approximately) to  $R$  by eq. (5). (This equation is a consequence of a simple piece of geometry, namely the greater weight carried by the tail of a diffuse density distribution, due to the geometrical  $r^2$ -weighting of radial volume integrals.) The result is that  $C$  falls below  $R$  by an amount that increases with decreasing size of the nucleus [see ref. <sup>5)</sup>]. For the light nuclei in question, the difference can be quite substantial. Thus, according to eqs. (5) and (6), the effective sharp radius  $R$  is 1.776 fm for an  $\alpha$ -particle and 2.657 fm for  $^{14}\text{C}$ , whereas the central radii  $C$  are 1.213 fm and 2.281 fm, respectively. (These values are close to the measured half-density radii for  $^4\text{He}$  and  $^{12}\text{C}$  [ref. <sup>7)</sup>].) The corresponding values of  $R/A^{1/3}$  are 1.119 fm for the  $\alpha$ -particle and 1.102 for  $^{14}\text{C}$ , in conformity with the approximate incompressibility of nuclei. On the other hand, if one tried (incorrectly) to reproduce the central radii by a formula of the type  $r_0 A^{1/3}$ , one would have to use  $r_0 = 0.764$  fm for  $A = 4$  and  $r_0 = 0.946$  fm for  $A = 14$ , values that would be considered quite unconventional, and significantly smaller for the  $\alpha$ -particle than for  $^{14}\text{C}$ .

Our semi-empirical formulae for the central radii  $C$ , although fairly realistic, do not reproduce the measured half-density radii exactly. For example, the half-density

radius of  ${}^4\text{He}$  is given in ref. <sup>7)</sup> as 1.33–1.34 fm. Using  $C_2 = 1.335$  fm (instead of 1.213 fm) would give, for the case of  ${}^{222}\text{Ra}$  decay, a penetrability factor  $G_\alpha = 4.946 \times 10^{22}$ . This represents an enhancement of  $\alpha$ -emission by a factor 5.83. Such enhancements would lead to calculated penetrability ratios of  $2.88 \times 10^{-10}$ ,  $1.18 \times 10^{-9}$  and  $1.05 \times 10^{-11}$  in the case of  ${}^{222}\text{Ra}$ ,  ${}^{223}\text{Ra}$  and  ${}^{224}\text{Ra}$ , which numbers differ from the measured branching ratios by factors of 0.78, 1.93 and 0.24 (instead of the 4.5, 11.3 and 1.43 in table 1).

A better estimate of the radius of  ${}^{14}\text{C}$  might lead to similar changes in the calculated penetrability ratios. In any case, at the level of agreement to within a factor of 10 or so (corresponding to a few percent accuracy in the penetrability integrals), the measured branching ratios for the three Ra isotopes can be accounted for in terms of a fission-like treatment of the disintegrations. The absolute values of the lifetimes indicate the presence of hindrance factors for the odd- $A$  nucleus  ${}^{223}\text{Ra}$  not accounted for by the present treatment. (Such odd-nucleon hindrance factors are a familiar feature of both  $\alpha$ - and fission-decay systematics.) The unexplained enhancement of the  ${}^{14}\text{C}$  decay of  ${}^{224}\text{Ra}$  with respect to  ${}^{222}\text{Ra}$ , implied by our estimates of  $\tau_0^C$ , underlines the need for caution in making more than qualitative predictions as regards the lifetimes (and branching ratios) for other exotic decays. Also, when the emission of heavier and heavier fragments comes into question, one should bear in mind the serious limitation of the present estimates, based as they are on a deformation energy which combines the Coulomb and proximity forces of *spherical* fragments down to contact, and a schematic interpolation (together with the continued use of a reduced mass  $M_r$ ) below contact. In the limit of fission into comparable fragments it is, of course, well known that such a treatment would give meaningless results: the actual deformation energies and fission barriers of heavy nuclei bear no resemblance whatever to what a calculation based on spherical fragments would suggest. Thus, for fragments heavier than  ${}^{14}\text{C}$ , it will at some stage be essential to consider in quantitative detail the appearance of the potential-energy barrier in the regime where the two-sphere approximation is not adequate (i.e. for  $L \leq L_c$ ) and to calculate properly the effective mass in the disintegration degree of freedom in this regime. Fig. 2b illustrates the case of  ${}^{232}\text{U} \rightarrow {}^{208}\text{Pb} + {}^{24}\text{Ne}$ , where this problem might already be a serious one. About 23% of the penetrability integral comes in this case from the region  $L_0 < L < L_c$ , where we use an arbitrary and uncertain interpolation. Adding to this the expected modifications in the barrier caused by fragment deformations and neck formation, one might well expect that a fair fraction of the potential-energy barrier could be significantly changed by a more adequate treatment. Without being able to estimate quantitatively at this stage how soon beyond  ${}^{14}\text{C}$  these effects will come in and how drastic they will be, it seems fairly safe to conjecture that, by and large, the two-sphere approximation, used in the present work, will tend to overestimate the height of the potential-energy barrier for the heavier fragments because the inclusion of a richer variety of deformation variables would allow the disintegrating system to seek out a more favorable path



in configuration space in the process of barrier penetration. One may even speculate that the enhancement of  $^{14}\text{C}$  emission in the case of  $^{224}\text{Ra}$  (compared to  $^{222}\text{Ra}$ ) could be a precursor of such fragment-deformation effects, the daughter nucleus  $^{210}\text{Pb}$  being somewhat more deformable than the doubly magic nucleus  $^{208}\text{Pb}$ . On the other hand, the effective mass for barrier penetration in the pre-scission regime might well be significantly different – in particular, higher than – the assumed reduced mass  $M_r$ . (In a hydrodynamic treatment the effective mass tends to be smaller than  $M_r$  for small deformations, but quantal effects tend to increase the effective mass above the hydrodynamical value, sometimes by considerable factors.) Thus, in estimating the lifetimes against decay by the emission of fragments even heavier than  $^{14}\text{C}$ , it is an open question whether the anticipated *lowering* of the barrier height, or a possible *increase* of the effective mass in the pre-scission regime, will gain the upper hand. (In the extreme case of near-symmetric spontaneous fission of very heavy elements, it is clear that the barrier-lowering effect has to win, since the fission barrier height goes to zero and so the penetrability integral has to vanish independently of the value of the effective mass.) As an illustration of the uncertainties associated with the schematic treatment of the pre-scission stage we note that if the pre-scission contribution to the penetrability integral were increased by a factor of 1.5, the  $\alpha$ -decay lifetime of  $^{222}\text{Ra}$  would be increased by a factor of 1.8 and the  $^{14}\text{C}$  decay lifetime by a factor of 66.

TABLE 2

Some properties of disintegrations to isotopes of Pb with calculated penetrability ratios  $> 10^{-12}$

Disintegration	$G_a/G_X$	$\frac{G_a/G_X}{G_a/G_C}$	$G_X$	$G_a$
$^{221}\text{Ra} \rightarrow ^{207}\text{Pb} + ^{14}\text{C}$	$8.181 \times 10^{-12}$	1	$5.307 \times 10^{33}$	$4.342 \times 10^{22}$
$^{222}\text{Ra} \rightarrow ^{208}\text{Pb} + ^{14}\text{C}$	$1.678 \times 10^{-9}$	1	$1.718 \times 10^{32}$	$2.884 \times 10^{23}$
$^{223}\text{Ra} \rightarrow ^{209}\text{Pb} + ^{14}\text{C}$	$6.895 \times 10^{-9}$	1	$6.842 \times 10^{34}$	$4.717 \times 10^{26}$
$^{224}\text{Ra} \rightarrow ^{210}\text{Pb} + ^{14}\text{C}$	$6.150 \times 10^{-11}$	1	$7.119 \times 10^{37}$	$4.378 \times 10^{27}$
$^{225}\text{Ra} \rightarrow ^{211}\text{Pb} + ^{14}\text{C}$	$6.992 \times 10^{-10}$	1	$2.781 \times 10^{40}$	$1.944 \times 10^{31}$
$^{226}\text{Ra} \rightarrow ^{212}\text{Pb} + ^{14}\text{C}$	$3.081 \times 10^{-11}$	1	$4.229 \times 10^{43}$	$1.303 \times 10^{33}$
$^{230}\text{Th} \rightarrow ^{208}\text{Pb} + ^{22}\text{O}$	$3.520 \times 10^{-12}$	0.0021	$2.616 \times 10^{46}$	$9.209 \times 10^{34}$
$^{231}\text{Th} \rightarrow ^{209}\text{Pb} + ^{22}\text{O}$	$1.263 \times 10^{-10}$	0.0183	$1.744 \times 10^{49}$	$2.203 \times 10^{39}$
$^{232}\text{Th} \rightarrow ^{210}\text{Pb} + ^{22}\text{O}$	$1.332 \times 10^{-12}$	0.0217	$2.327 \times 10^{52}$	$3.100 \times 10^{40}$
$^{233}\text{Th} \rightarrow ^{211}\text{Pb} + ^{22}\text{O}$	$1.185 \times 10^{-12}$	0.0017	$7.488 \times 10^{54}$	$8.873 \times 10^{42}$
$^{231}\text{U} \rightarrow ^{207}\text{Pb} + ^{24}\text{Ne}$	$3.954 \times 10^{-12}$	0.4833	$2.877 \times 10^{42}$	$1.138 \times 10^{31}$
$^{232}\text{U} \rightarrow ^{208}\text{Pb} + ^{24}\text{Ne}$	$4.872 \times 10^{-11}$	0.0290	$1.485 \times 10^{42}$	$7.235 \times 10^{31}$
$^{233}\text{U} \rightarrow ^{209}\text{Pb} + ^{24}\text{Ne}$	$3.747 \times 10^{-11}$	0.0054	$3.748 \times 10^{45}$	$1.404 \times 10^{35}$
$^{233}\text{U} \rightarrow ^{208}\text{Pb} + ^{25}\text{Ne}$	$2.556 \times 10^{-10}$	0.1523	$5.493 \times 10^{44}$	$1.404 \times 10^{35}$
$^{234}\text{U} \rightarrow ^{208}\text{Pb} + ^{26}\text{Ne}$	$1.565 \times 10^{-12}$	0.0009	$1.981 \times 10^{47}$	$3.100 \times 10^{35}$

With all these reservations in mind we prepared a survey of nominal penetrability factors for a large number of potentially interesting disintegrations, using the equations described in this paper. This included all disintegrations ending in the isotopes of lead from  $^{206}\text{Pb}$  to  $^{214}\text{Pb}$ , the emitted fragments being all the isotopes of Be, B, C, O, Ne, Mg, Si and S for which the atomic masses are listed in Wapstra *et al.*'s 1984 compilation, ref. <sup>8</sup>). (The parent nuclei were thus various isotopes of Rn, Fr, Ra, Th, U, Pu, Cm and Cf. Some of these have dominant  $\beta$ -decay branches and would not be relevant candidates for the study of heavy-particle radioactivity.) In most cases the penetrability ratios  $G_\alpha/G_X$  (X stands for the emitted fragment) were many orders of magnitude less favourable than in the three cases listed in table 1, but there were notable exceptions. In table 2 we have listed some particulars

TABLE 3  
Some properties of disintegrations to isotopes of Hg, Tl and Bi, with calculated penetrability ratios  $>10^{-12}$

Disintegration	$G_\alpha/G_X$	$G_X$	$G_\alpha$
$^{231}\text{Th} \rightarrow ^{207}\text{Hg} + ^{24}\text{Ne}$	$2.466 \times 10^{-12}$	$8.931 \times 10^{50}$	$2.203 \times 10^{39}$
$^{231}\text{Th} \rightarrow ^{206}\text{Hg} + ^{25}\text{Ne}$	$2.278 \times 10^{-10}$	$9.668 \times 10^{48}$	$2.203 \times 10^{39}$
$^{232}\text{Th} \rightarrow ^{206}\text{Hg} + ^{26}\text{Ne}$	$3.666 \times 10^{-11}$	$8.455 \times 10^{50}$	$3.100 \times 10^{40}$
$^{233}\text{Th} \rightarrow ^{207}\text{Hg} + ^{26}\text{Ne}$	$8.687 \times 10^{-12}$	$1.021 \times 10^{54}$	$8.873 \times 10^{42}$
$^{221}\text{Fr} \rightarrow ^{207}\text{Tl} + ^{14}\text{C}$	$7.988 \times 10^{-12}$	$1.089 \times 10^{35}$	$8.698 \times 10^{23}$
$^{222}\text{Fr} \rightarrow ^{208}\text{Tl} + ^{14}\text{C}$	$1.283 \times 10^{-11}$	$5.373 \times 10^{37}$	$6.894 \times 10^{26}$
$^{223}\text{Fr} \rightarrow ^{209}\text{Tl} + ^{14}\text{C}$	$4.481 \times 10^{-12}$	$2.485 \times 10^{40}$	$1.114 \times 10^{29}$
$^{224}\text{Fr} \rightarrow ^{210}\text{Tl} + ^{14}\text{C}$	$7.814 \times 10^{-12}$	$2.259 \times 10^{43}$	$1.765 \times 10^{32}$
$^{229}\text{Ac} \rightarrow ^{207}\text{Tl} + ^{22}\text{O}$	$7.315 \times 10^{-11}$	$7.455 \times 10^{46}$	$5.454 \times 10^{36}$
$^{230}\text{Ac} \rightarrow ^{208}\text{Tl} + ^{22}\text{O}$	$3.293 \times 10^{-11}$	$7.453 \times 10^{49}$	$2.454 \times 10^{39}$
$^{231}\text{Ac} \rightarrow ^{209}\text{Tl} + ^{22}\text{O}$	$1.926 \times 10^{-11}$	$2.011 \times 10^{52}$	$3.873 \times 10^{41}$
$^{232}\text{Ac} \rightarrow ^{210}\text{Tl} + ^{22}\text{O}$	$4.915 \times 10^{-12}$	$1.252 \times 10^{55}$	$6.156 \times 10^{43}$
$^{231}\text{Pa} \rightarrow ^{207}\text{Tl} + ^{24}\text{Ne}$	$9.448 \times 10^{-12}$	$9.798 \times 10^{43}$	$9.258 \times 10^{32}$
$^{232}\text{Pa} \rightarrow ^{208}\text{Tl} + ^{24}\text{Ne}$	$2.210 \times 10^{-11}$	$2.620 \times 10^{47}$	$5.792 \times 10^{36}$
$^{233}\text{Pa} \rightarrow ^{209}\text{Tl} + ^{24}\text{Ne}$	$2.327 \times 10^{-12}$	$3.329 \times 10^{50}$	$7.746 \times 10^{38}$
$^{232}\text{Pa} \rightarrow ^{207}\text{Tl} + ^{25}\text{Ne}$	$2.701 \times 10^{-10}$	$2.144 \times 10^{46}$	$5.792 \times 10^{36}$
$^{234}\text{Pa} \rightarrow ^{209}\text{Tl} + ^{25}\text{Ne}$	$1.232 \times 10^{-12}$	$2.637 \times 10^{52}$	$3.247 \times 10^{40}$
$^{233}\text{Pa} \rightarrow ^{207}\text{Tl} + ^{26}\text{Ne}$	$4.017 \times 10^{-10}$	$1.929 \times 10^{48}$	$7.746 \times 10^{38}$
$^{234}\text{Pa} \rightarrow ^{208}\text{Tl} + ^{26}\text{Ne}$	$1.775 \times 10^{-11}$	$1.829 \times 10^{51}$	$3.247 \times 10^{40}$
$^{235}\text{Pa} \rightarrow ^{209}\text{Tl} + ^{26}\text{Ne}$	$2.227 \times 10^{-12}$	$4.925 \times 10^{53}$	$1.097 \times 10^{42}$
$^{235}\text{Np} \rightarrow ^{207}\text{Tl} + ^{28}\text{Mg}$	$1.101 \times 10^{-12}$	$5.557 \times 10^{45}$	$6.116 \times 10^{33}$
$^{223}\text{Ac} \rightarrow ^{209}\text{Bi} + ^{14}\text{C}$	$1.564 \times 10^{-10}$	$1.954 \times 10^{33}$	$3.056 \times 10^{23}$
$^{224}\text{Ac} \rightarrow ^{210}\text{Bi} + ^{14}\text{C}$	$7.249 \times 10^{-11}$	$4.467 \times 10^{35}$	$3.238 \times 10^{25}$
$^{225}\text{Ac} \rightarrow ^{211}\text{Bi} + ^{14}\text{C}$	$1.629 \times 10^{-12}$	$1.546 \times 10^{39}$	$2.519 \times 10^{27}$

of all disintegrations for which  $G_\alpha/G_X$  was calculated to be greater than  $10^{-12}$ . The list includes the decay of three additional isotopes of Ra by  $^{14}\text{C}$  emission, four isotopes of Th decaying by  $^{22}\text{O}$  emission and four isotopes of U decaying by the emission of  $^{24}\text{Ne}$ ,  $^{25}\text{Ne}$  or  $^{26}\text{Ne}$ . Column 3 in table 2 shows the calculated penetrability ratios normalized to the corresponding ratios for disintegrations involving a  $^{14}\text{C}$  fragment and the same daughter isotope of Pb.

In table 3 we give the results of a similar search for disintegrations with calculated penetrability ratios  $>10^{-12}$ , but with isotopes of Hg, Tl and Bi as end products. We also considered decays involving fragments with an odd atomic number (ending up in either Tl, Pb or Bi isotopes), but there was not a single candidate of this type with a penetrability ratio  $>10^{-12}$ .

Other decays than those shown in tables 2 and 3 might eventually become observable with improvements in the detection techniques. One should, however, keep in mind that for the heavier fragments the ratios  $G_\alpha/G_X$  in tables 2 and 3 are very uncertain, as stressed before. The observation of even one of the cases involving O or Ne isotopes would be extremely valuable in providing information on whether there was, in fact, an improvement in the branching ratios resulting from the anticipated effect of fragment deformations during barrier penetration.

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