

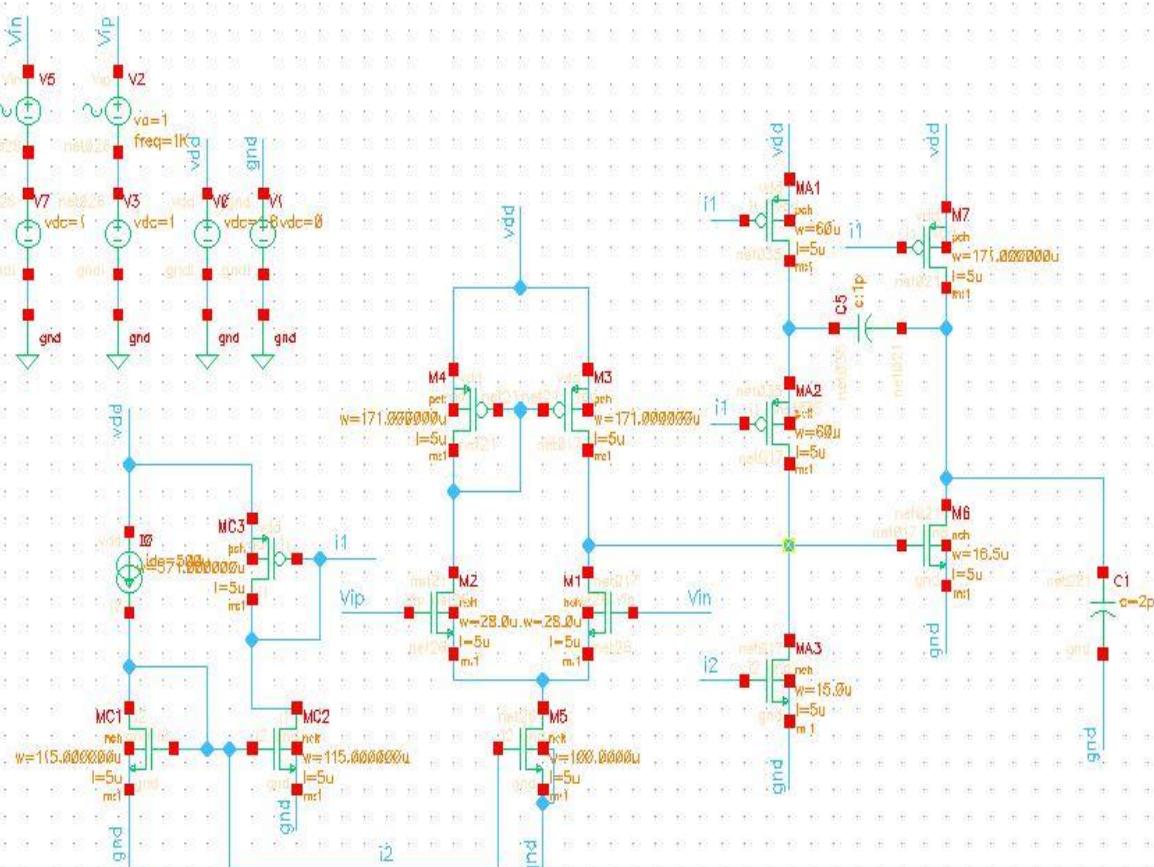
CLASS PROJECT

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Aim:-To design of a two-stage op-amp with indirect Ahuja compensation.

Schematic:-



Note:- The size of transistor are not the one in schematic.

* Final Project *

i. Given that.

$$\begin{aligned} \text{Gain} &> 60 \text{ db} > 1000. \\ \text{Phase Margin} &> 50^\circ \\ \text{Unity gain freq} &> 100 \text{ MHz} \\ \text{Power} &< 1 \text{ mW} \\ V_{dd} &= 1.8 \text{ V} \\ C_L &= 2 \text{ pF.} \end{aligned}$$

For two stage amplifier.

$$A_v(\text{total gain}) = A_1 * A_2$$

from above diagram

$$\begin{aligned} A_1 &= g_m (\gamma_{02} || \gamma_{04}) \\ A_2 &= g_m (\gamma_{06} || \gamma_{07}). \end{aligned}$$

$$A_v = \underline{g_m (\gamma_{02} || \gamma_{04}) * g_m (\gamma_{06} || \gamma_{07})}$$

$$1000 < g_m (\gamma_{02} || \gamma_{04}) * g_m (\gamma_{06} || \gamma_{07}).$$

(1)

Given Power budget < 1mW

$$P = V_{dd} (I_{davg})$$

$$\text{i.e. } (1.8) (I_{davg}) < 1 \text{ mW}$$

$$I_{davg} < \frac{1}{10^{-3}}$$

$$\boxed{I_{davg} < 555.5 \mu\text{A.}}$$

Thus we have to divide current in stage-1
stage-2 and buffer stage in such a
way that Phase margin and all criteria are

Satisfied. For ease of calculation take total drain current $I_d = 500 \mu A$.

* $G.B.W = 2\pi \times \text{Unity gain freq.}$

For $\text{PM} \geq 50^\circ$.

$$\tan^{-1}\left(\frac{G.BW}{P_2}\right) + \tan^{-1}\left(\frac{G.BW}{Z_1}\right) < 40^\circ$$

$$Z_1 = g_m z / C_C, G.BW = \frac{g_m}{C_C}, P_2 = \frac{g_m z}{(C_C + C_L)} \left(\frac{g_m C_L}{3} \right)$$

Assume that $\frac{G.BW}{Z_1} = \boxed{\frac{1}{5}} = \frac{g_m}{g_m z}$

$$\tan^{-1}\left(\frac{G.BW}{P_2}\right) + \tan^{-1}\left(\frac{1}{5}\right) < 40^\circ$$

$$\tan^{-1}\left(\frac{G.BW}{P_2}\right) < 40^\circ - 11.30^\circ$$

$$\tan\left(\frac{G.BW}{P_2}\right) < \tan(28.699)$$

$$\frac{G.BW}{P_2} < 0.5475$$

$$(0.5475)P_2 > G.BW$$

$$\frac{P_2}{P_2} > 1.827 \text{ GBW}$$

Keeping values of P_2 & G.BW & Assume $\frac{g_m C_L}{3} = 3$

$$\frac{3 g_m z}{C_C + C_L} > 1.827 \times \frac{g_m}{C_C}$$

$$\frac{g_{m2}}{C_C + C_L} > 0.61 \frac{g_m}{C_C}$$

$$(g_{m2} = 5 g_m)$$

$$\therefore \frac{5}{C_C + C_L} > \frac{0.61}{C_C}$$

$$5C_C > 0.61C_C + 0.61C_L$$

$$\frac{C_C}{C_C} > \frac{0.278}{2} C_L$$

$$\boxed{C_C > 0.287 \text{ pF}}$$

keeping parasitic capacitance in mind.
lets take

$$C_C = 500 \text{ fF. i.e. } 0.5 \text{ pF.}$$

$$u_{GBW} G_F > 100 \text{ MHz}$$

lets take if 110 MHz

$$\therefore g_{m1} = 2\pi \times (110 \text{ MHz}) \times 0.5 \text{ pF.}$$

$$g_{m1} = \frac{2 \times 3.14 \times 1.1 \times 10^{-4}}{345.4 \mu}$$

lets take $g_{m1} = 350 \mu$.

$$\therefore g_{m2} = 350 \mu \times 5 = \boxed{1.75 \text{ m}}$$

From HW 4.

$$g_m = \frac{2ID}{(V_G - V_{TH})}$$

$$(V_{DS} - V_T)_{nmos} = 0.446 \text{ V}$$

$$(V_G - V_{TH})_{p,mos} = 0.4213 \text{ V}$$

$$\frac{g_m}{2} \times 0.446 = I_{D5}$$

$$I_{D5}^2 = 78.09 \mu A$$

$I_{D5} \approx 80 \mu A$

For 2nd stage

$$\frac{g_m}{2} \times 0.4312 = I_{D7}$$

$$I_{D7} = 368.63 \mu A$$
$$I_{D7} \approx 370 \mu A.$$

$I_{D5} + I_{D7} = 450 \mu A$.
Rest $50 \mu A$ is given to buffer
Stage.

Thus current through

#	Stage 1 = $80 \mu A$
	Stage 2 = $370 \mu A$.
	Buffer = $50 \mu A$.

* In order to set gain = 3 of buffer stage, as assumed previously value of I_D buffer can be changed.

But total I_D is always kept < 555 .
to get Power $< 1 \text{ mW}$.

From the schematics :-

M_{C1} , M_{C2} & M_{C3} are transistors of current ref stage.
 M_{A1} , M_{A2} & M_{A3} are of Buffer stage.
& M_1 to M_7 are gain stages
amplifier.

* Designing MOSFETS of current mirror.

For calculation of all the transistors & make it easy L is kept to 5μ for all the transistors.

Value of L selected from g_m/g_{ds} vs g_m/I_d .

For NMOS

For PMOS

$$g_m = \frac{2I_D}{V_{GS} - V_{Th}}$$

$$\frac{g_m}{I_D} = \frac{2}{V_{GS} - V_{Th}}$$

$$g_m = \frac{2I_D}{V_{GS} - V_{Th}}$$

$$\frac{g_m}{I_D} = \frac{2}{V_{GS} - V_{Th}}$$

Thus for constant L g_m/I_D will remain constant.

$$g_m/I_D \approx 4.5$$

$$g_m/I_D \approx 4.75$$

From g_m/I_d vs I_d/W from figures in Appendix.

$$I_d/W = 4.33$$

$$I_d/W = 0.875$$

$$\therefore W = \frac{I_d}{4.33}$$

$$W = \frac{I_d}{0.875}$$

For $500\mu A$ I_d .

$$W = \frac{500}{4.33}$$

$$W = 115.47$$
$$W \approx 116 \mu m$$

Pmos

$$W = \frac{500}{0.875}$$

$$W = 571.42 \mu m$$
$$W \approx 572 \mu m.$$

$$\therefore [M_{G_1} = M_{G_2} = \frac{116 \mu m}{Sum.}]$$

$$[M_{G_3} = \frac{572 \mu m}{Sum.}]$$

For M_5 $I_S = 80 \mu A$.

$$\therefore W = \frac{80}{4.33}$$

$$W = 18.48 \mu m$$
$$W = 19 \mu m.$$

$$[(w/L)_{M_5} = (19/5)]$$

For M_7 $I_T = 370 \mu A$.

$$W = \frac{370}{4.33 \cdot 0.875}$$

$$W = 85.45 \mu m$$
$$W \approx 86 \mu m$$

$$[(w/L)_{M_7} = (86/5) \mu m]$$

Previously we assumed that. $gm\gamma_0/3 = 3$

i.e. $gm\gamma_0 = 9$ (gain of Buffer stage).

From gm/gds curve at $L = Su$ & $\omega = S_u$.
 $\gamma_0 \approx 300 K$

$$gm = \frac{9}{300 \times 10^3}$$

$$gm = 30 \text{ m}$$

This gives $I_0 = 20 \times 0.446/2$
 $= 6.7 \mu A$.

$I_0 \approx 7 \mu A$

$$\omega = \frac{I_0}{0.875}$$

$$\omega = \frac{I_0}{4.33}$$

 $= 1.62 \text{ rad}$

$$\omega = 8 \text{ rad/m.}$$

$$\text{For } MA_1, GMA_2 \frac{(\omega/L)}{= \left[\frac{(8/S)}{2} \right]}$$

$$\left\{ \text{For } MA_3, (\omega/L) = \left[\frac{1.62}{S} \right] \right.$$

* I_0 flowing through M_5 is divided into two equal parts flowing through M_1 and M_2 .

$$(I_d)_{M_1, M_2} = 40 \mu A.$$

$$\therefore W_{m_1, m_2} = \frac{1}{2} \times W_{m_5} = \frac{19}{2} = 9.5 \text{ u}$$

$$(W/L)_{m_1, m_2} = (9.5/5).$$

* For M₃ & M₄.

$$I_d = 40 \mu A$$

$$W = \frac{40 \mu A}{0.875}$$

$$W \approx 45.71$$

$$W = 45 \mu m$$

$$(W/L)_{m_3, m_4} = \left(\frac{45}{5} \right)$$

For M₆.

$$I_d = 370 \mu A$$

$$W = \frac{370}{0.875} \approx 428.85$$

$$W = \frac{370}{4.23} = 85.45$$

$$W \approx 86 \mu m$$

$$(W/L)_{M_6} = (86/5) \mu$$

* Transistor Size Summary

<u>Transistor</u>	<u>(W/L) (Values in μ)</u>
M_1, M_2	$(9.5/5)$
M_3, M_4	$(45/5)$
M_5	$(19/5)$
M_6	$(86/5)$
M_7	$(423/5)$
MC_1, MC_2	$(116/5)$
MC_3	$(572/5)$
$MA_1; MA_2$	$(8/5)$
MA_3	$(1.62/5)$

Note value of L is selected 5μ because from gm/gds V_{ds} gm/sd . If gives high value of g_m thus gain requirement of I_{ds} satisfied.

Appendix:-

