

add comparision of simulation result to anytical and plot them

## FORCE Calculation - z direction displ.

This section deals with calculation of force acting on spheroid when kept inside the magnetic field in different configurations.

This section deals with configuration of applied magnetic field where it is displaced only in z-direction.

→ force acting on a spheroid kept inside a magnetic field can be evaluated using maxwell stress Tensor.

### Normal Vector Calculation → (Spherical co-ordinates)

This calculation is shown in detail in Section B(b) or 'Normal vector to surface of Spheroid.nb'.

$$\boxed{\text{normal}} \vec{n} = (R - R_s \cos(2\theta))^2 \sin\theta, -4R_s \cos\theta \sin^2\theta (R - R_s \cos(2\theta)), 0$$

↳ referenced from eqn. 126. — ①e

• now, we convert this normal vector  $\vec{n}$  from spherical co-ordinates to cartesian co-ordinates.

This is achieved by multiplying it with transformation matrix.

### SphTo Car

$$M_{S \rightarrow C} = \begin{pmatrix} \sin\theta \cos\phi & \cos\theta \cos\phi & -\sin\phi \\ \sin\theta \sin\phi & \cos\theta \sin\phi & \cos\phi \\ \cos\theta & -\sin\theta & 0 \end{pmatrix} \quad \text{--- ②e}$$



$\vec{n}_c \rightarrow$  normal in cartesian coordinates

PAGE NO. :

DATE: / /

$$\vec{n}_c = M_{S \rightarrow c} \cdot \vec{n}$$

$$\boxed{n_x} \quad \vec{n}_c^x = (R - 2Rs - 3Rs \cos(2\theta)) (R - Rs \cos(2\theta)) \cos\phi \sin\theta$$

$$\boxed{n_y} \quad \vec{n}_c^y = (R - 2Rs - 3Rs \cos(2\theta)) (R - Rs \cos(2\theta)) \sin\theta \sin\phi$$

$$\boxed{n_z} \quad \vec{n}_c^z = \cos\theta (R + 2Rs - 3Rs \cos(2\theta)) (R - Rs \cos(2\theta)) \sin\theta$$

Area element of Spheroid

$$dA_i = \hat{n}_i ds \quad \text{--- (4)e}$$

where  $\hat{n}_i$  = unit normal vector in  $i^{\text{th}}$  direction

$ds = \|\vec{n}\| d\theta d\phi \rightarrow$  differential area element for any surface. --- (5)e

$$dA_i = \frac{n_i}{\|\vec{n}\|} \|\vec{n}\| d\theta d\phi = n_i d\theta d\phi \quad \text{--- (6)e}$$

$$\left. \begin{array}{l} A_x \\ A_y \\ A_z \end{array} \right\} \begin{array}{l} dA_x = n_x d\theta d\phi \\ dA_y = n_y d\theta d\phi \\ dA_z = n_z d\theta d\phi \end{array} \quad \text{--- (7)e}$$

Hence, initially we used a normal vector rather than a unit normal vector.



Magnetic field at the surface of Spheroid  $\rightarrow$

$B_{out}(\theta, \phi) |_{r=r(0)}$  calculated in eq 42d is used directly over here.

$$\downarrow \quad \text{Bout}_{spheroid} \quad \text{Bout}_{surf}(\theta, \phi) = B_{out}(\theta, \phi) |_{r=r(0)} \quad \text{--- (8) e}$$

Converting the magnetic field at the surface of spheroid in cartesian coordinates.  $\rightarrow$

Using the matrix defined in eq. 2e, it can be converted easily.

$$B_{out, cart, surf}(\theta, \phi) = M_{s \rightarrow c} \cdot B_{out, surf}(\theta, \phi) \quad \text{--- (9) e}$$

$$\downarrow$$

$$\boxed{B_{out cart}}$$

Now, we define

$$\boxed{B_{out}^2} \quad B_{out, cart, surf, sq}(\theta, \phi) = (B_{out, cart, surf}(\theta, \phi))^2 \quad \text{--- (10) e}$$

$$\left. \begin{array}{l} B_x \\ B_y \\ B_z \end{array} \right\} = \left. \begin{array}{l} B_x^{out, cart, surf}(\theta, \phi) \\ B_y^{out, cart, surf}(\theta, \phi) \\ B_z^{out, cart, surf}(\theta, \phi) \end{array} \right\} \quad \text{--- (11) e}$$



$$f = \int \nabla \cdot \vec{T} dV \quad \text{--- (12)e}$$

$$= \oint \vec{T} \cdot \hat{n} dS = \oint \vec{T} \cdot \vec{n} d\theta d\phi \quad \text{--- (13)e}$$

$$T_{ij} = \frac{1}{\mu_0} \left( B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right) + \frac{1}{\mu_0} \left( E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right) \quad \text{--- (14)e}$$

Since, there is no electric field

$$T_{ij} = \frac{1}{\mu_0} \left( B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right) \quad \text{--- (15)e}$$

$$T_{xx} = \frac{1}{\mu_0} \left( B_x^2 - \frac{1}{2} B^2 \right) = \frac{1}{2\mu_0} \left( B_x^2 - B_y^2 - B_z^2 \right) \quad \text{--- (16)e}$$

$$T_{xy} = \frac{1}{\mu_0} (B_x B_y) \quad \text{--- (17)e}$$

$$T_{xz} = \frac{1}{\mu_0} (B_x B_z) \quad \text{--- (18)e}$$

$$f_x = \oint T_{xx} dA_x + \oint T_{xy} dA_y + \oint T_{xz} dA_z \quad \text{--- (19)e}$$

$$= \oint T_{xx} n_x d\theta d\phi + \oint T_{xy} n_y d\theta d\phi + \oint T_{xz} n_z d\theta d\phi$$

$(f_{x1}) \quad 19e-1 \quad (f_{x2}) \quad 19e-2 \quad (f_{x3}) \quad 19e-3$

Similarly  $f_y$  direction can be written as.

$$f_y = \int T_{yy} dA_y + \int T_{yx} dA_x + \int T_{yz} dA_z \quad \text{--- (20)e}$$

$$= \oint T_{yy} n_y d\theta d\phi + \oint T_{yx} n_x d\theta d\phi + \oint T_{yz} n_z d\theta d\phi$$

$\hookrightarrow (f_{y1}) \quad \hookrightarrow (f_{y2}) \quad \hookrightarrow (f_{y3})$

$$f_z = \oint T_{zz} n_z d\theta d\phi + \oint T_{zy} d\theta d\phi n_y + \oint T_{zx} d\theta d\phi n_x$$

$(f_{z1}) \quad (f_{z2}) \quad (f_{z3}) \quad \hookrightarrow (f_{z4})$

$$F = (f_x, f_y, f_z) \quad \text{--- (22)e}$$