

Model Approximation of Thermo-Fluidic Diffusion Processes in Spatially Interconnected Structures

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Thermo-Fluidic Processes

Mutual effect of thermal energy on interacting solids and fluids.

Thermo-Fluidic Processes

Mutual effect of thermal energy on interacting solids and fluids.

1. Coupled Distributed Parameter Systems.
2. Energy exchange of interacting physical phenomena over boundaries.

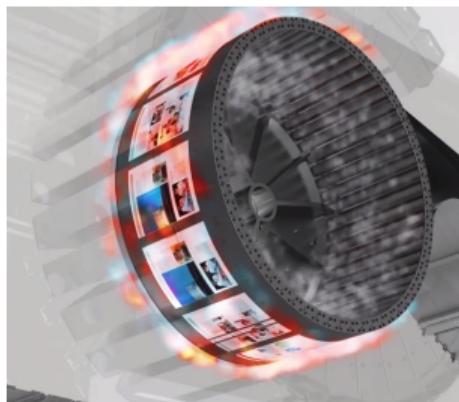
Thermo-Fluidic Processes: Examples

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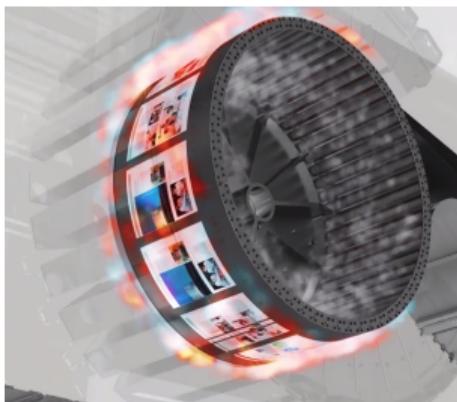
Thermo-Fluidic Processes: Examples

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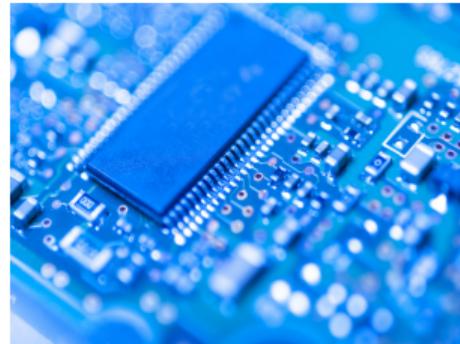
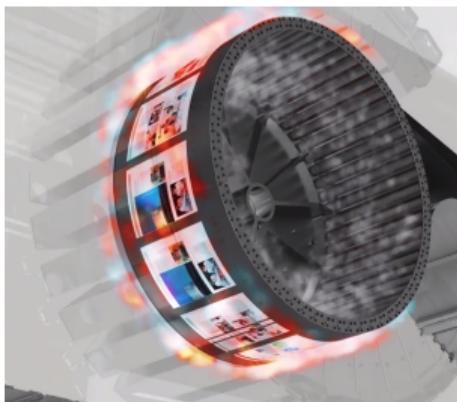
Thermo-Fluidic Processes: Examples

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Problem

How to fully exploit the mutual interaction among different physical phenomena for solving model-based problems?

Specifically:

1. Preserving the boundary conditions at the spatial interconnection.
2. Dealing with multi-varibale coupled problems.
3. Solving the boundary control problems.

Problem

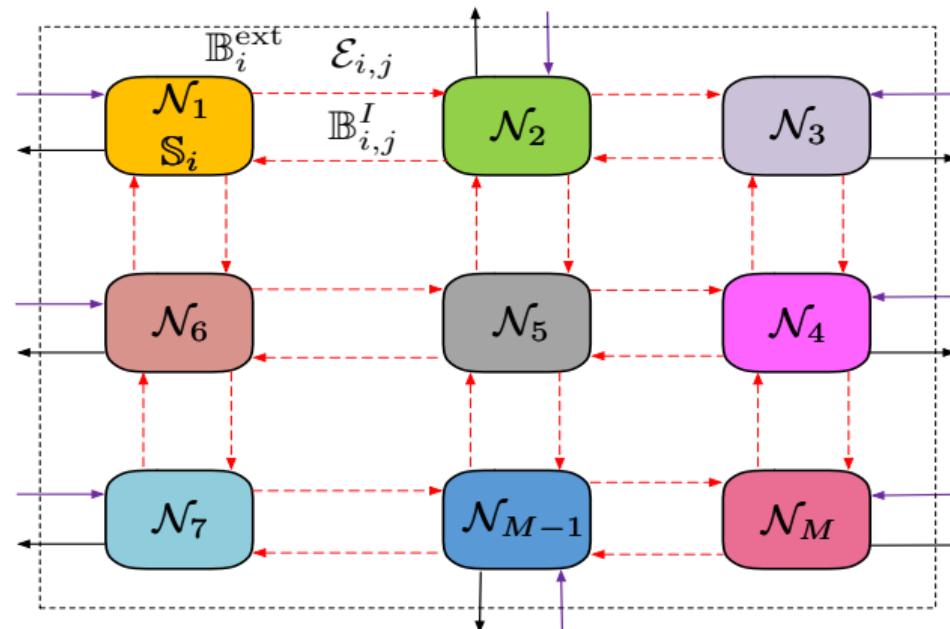
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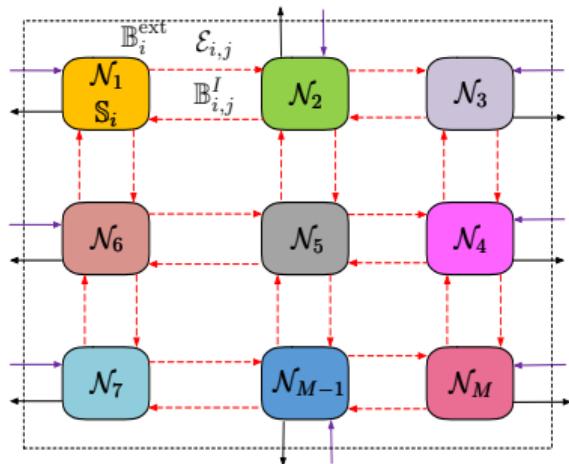
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Modeling Framework: Graph Theoretic Description

In a graph, individual systems are a set of Nodes that interact through Edges.



Modeling Framework: Topology Description

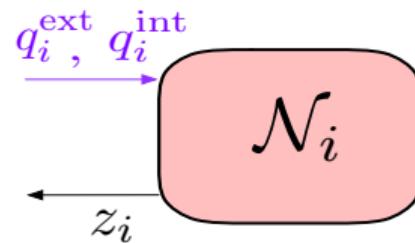


Topology

1. A finite connected graph $\mathcal{G} = (\mathcal{N}, \mathcal{E})$
2. An adjacency matrix A , with $A = A^T$.

- ▶ $\mathcal{N}_i \in \mathcal{N}$ denotes the local dynamics of the node.
- ▶ $\mathcal{E}_{i,j} \in \mathcal{E}$ denotes the interconnection of adjacent nodes.

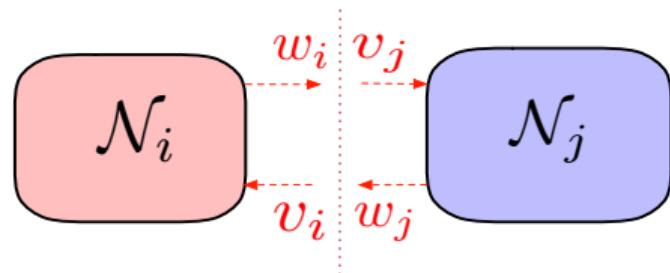
Modeling Framework: Governing Dynamics



$$\text{Model}(D_i) \begin{cases} \mathcal{E}_i \frac{\partial z_i}{\partial t} = \mathcal{A}_i z_i + \mathcal{B}_i^{\text{int}} q_i^{\text{int}} \\ \mathcal{A}_i z_i := [\nabla \cdot K_i(s) \nabla] z_i \end{cases}$$

$$\text{External boundaries } (B_i^{\text{ext}}) \begin{cases} \mathcal{H}_i^{\text{ext}} z_i = q_i^{\text{ext}} \\ \mathcal{H}_i^{\text{ext}} z_i := [\kappa_i(s) \frac{\partial}{\partial b_i^{\text{ext}}} + H_i^{\text{ext}}(s)] z_i \end{cases}$$

Modeling Framework: Governing Dynamics



Interface boundaries($B_{i,j}^I$)

$$\left\{ \begin{array}{l} \begin{bmatrix} w_i \\ w_j \end{bmatrix} = \begin{bmatrix} 0 & I \\ I & 0 \end{bmatrix} \begin{bmatrix} v_i \\ v_j \end{bmatrix}, \\ \text{or} \\ \begin{bmatrix} \mathcal{P}_{i,j}^w - \mathcal{L}_{i,j} \mathcal{P}_{i,j}^v \\ z_i \\ z_j \end{bmatrix} = 0. \end{array} \right.$$

Modeling Framework: Summary

1. A finite and connected graph $\mathcal{G} = (\mathcal{N}, \mathcal{E})$.
2. A symmetric adjacency matrix A .
3. Every node \mathcal{N}_i describes local thermal-fluidic diffusion

$$\mathcal{N}_i = (\mathbb{S}_i, \mathbb{B}_i^{\text{ext}}, \mathbb{B}_i^{\text{int}}, D_i, B_i^{\text{ext}}).$$

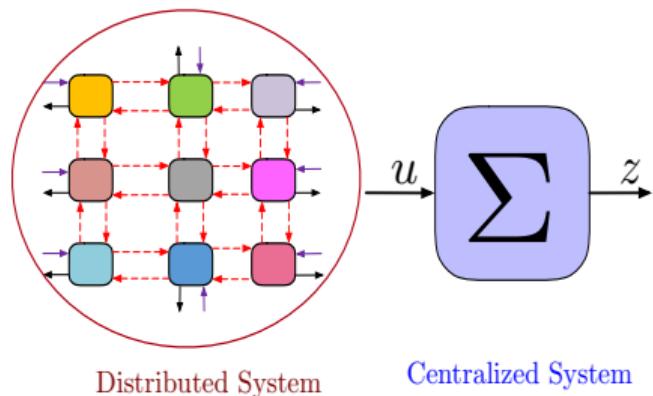
4. Every edge $\mathcal{E}_{i,j}$ describes the interconnection of thermal and fluidic process

$$\mathcal{E}_{i,j} = (\mathbb{B}_{i,j}^I, B_{i,j}^I).$$

The above defined problem can be proven to be well-posed.

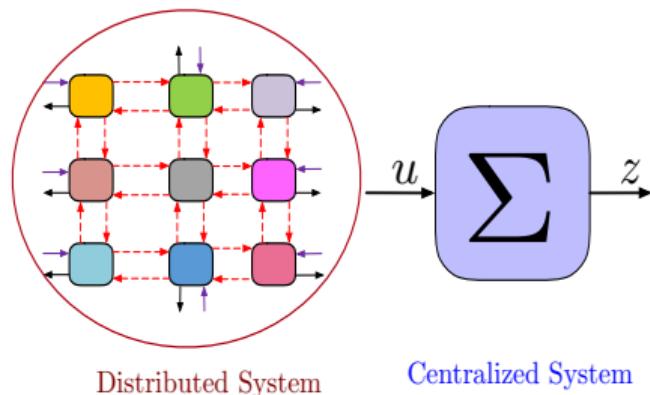
Step 1: Separation of Solution

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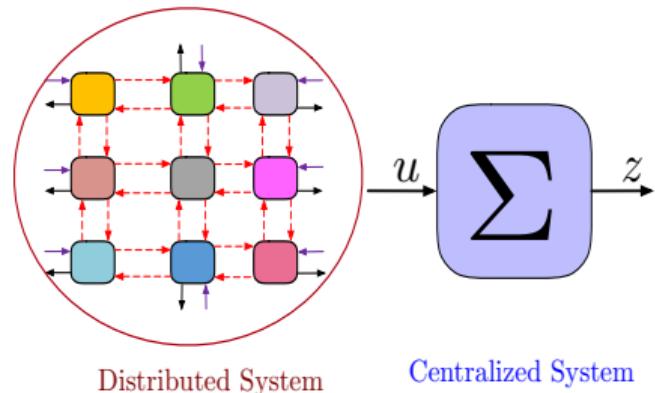


A) Homogenization

$$\begin{bmatrix} z_1 \\ \vdots \\ z_M \end{bmatrix} := \begin{bmatrix} x_1 \\ \vdots \\ x_M \end{bmatrix} + \mathcal{G} \begin{bmatrix} q_1^{\text{ext}} \\ \vdots \\ q_M^{\text{ext}} \end{bmatrix}$$

Step 1: Separation of Solution

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B) Define an extended state space (Σ)

$$\underbrace{\begin{bmatrix} \mathcal{E} & 0 \\ 0 & I \end{bmatrix}}_{\mathbf{E}} \begin{bmatrix} \dot{x} \\ \dot{q}^{\text{ext}} \end{bmatrix} = \underbrace{\begin{bmatrix} \mathcal{A} & \mathcal{A}\mathcal{G} \\ 0 & 0 \end{bmatrix}}_{\mathbf{A}} \begin{bmatrix} x \\ q^{\text{ext}} \end{bmatrix} + \underbrace{\begin{bmatrix} \mathcal{B}^{\text{int}} & -\mathcal{E}\mathcal{G} \\ 0 & I \end{bmatrix}}_{\mathbf{B}} \begin{bmatrix} q^{\text{int}} \\ \dot{q}^{\text{ext}} \end{bmatrix}$$

Step 2. Parametrization & Approximation of Solution

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Solution Expansion: $\underbrace{\begin{bmatrix} x \\ q^{\text{ext}} \end{bmatrix}}_{x^e} = \sum_{m=1}^{\infty} \underbrace{\begin{bmatrix} \Theta_m^x(t) & 0 \\ 0 & \Theta_m^q(t) \end{bmatrix}}_{\Theta_m(t)} \underbrace{\begin{bmatrix} \Phi_m^x(s) \\ \Phi_m^q(s) \end{bmatrix}}_{\Phi_m(s)}.$

Signal Projection: $\hat{x}^e(s, t) = \sum_{m=1}^H \Theta_m(t) \Phi_m(s)$

Residual System: $\mathbf{R}(x^e) := \mathbf{E} \frac{\partial x^e}{\partial t} - \mathbf{A}x^e - \mathbf{B}u = 0.$

System Projection: $\langle \Phi_m, \mathbf{R}(\hat{x}^e) \rangle = 0; \quad \forall m \in \{1, \dots, H\}.$

Feedback Control Problem: LQ optimal problem

The system: $\mathbf{E} \frac{\partial x^e}{\partial t} = \mathbf{A}x^e + \mathbf{B}u$.

Cost Functional: $J(x^e, u) := \int_0^\infty \langle P(s)x^e, x^e \rangle dt + \int_0^\infty \langle R(s)u, u \rangle dt$

Controller: $u = -K(x^e)$

K is the stabilizing, positive semi-definite, self-adjoint solution to the generalized OARE.

Feedback Control Problem: In Finite Dimension

The projected system: $\langle \Phi_m, \mathbf{R}(\hat{x}^e) \rangle := E_n \dot{\hat{x}}^e = A_n \hat{x}^e + B_n \hat{u}$.

Cost Functional: $J(\hat{x}^e, \hat{u}) := \int_0^\infty \langle \hat{x}^e, P_n \hat{x}^e \rangle dt + \int_0^\infty \langle \hat{u}, R_n \hat{u} \rangle dt$

Controller: $u = -K_n \hat{x}^e$

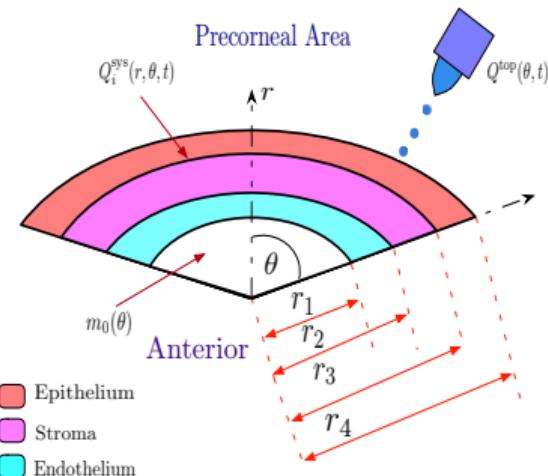
K_n is the stabilizing, positive semi-definite, symmetric solution to the generalized ARE.

Need to solve sparse matrix equalities (Use ADI, Krylov, S).

Example: Boundary Control of Ophthalmic Drug Delivery

Goal: Corneal Topography

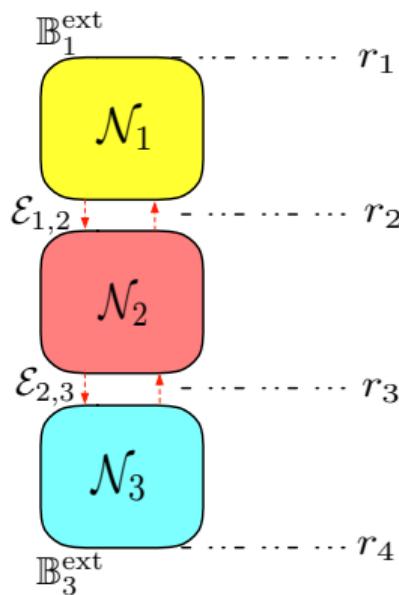
Determine topical drug concentration to achieve dilation across pupil.



Specifics

1. The pre-corneal area has leakage in radial direction due to tears.
2. The anterior chamber has leakage due to drug transport by systemic membrane.
3. Angular directions are insulated.

Example: Boundary Control of Ophthalmic Drug Delivery



Topology

1. The nodes are $\{\mathcal{N}_1, \mathcal{N}_2, \mathcal{N}_3\}$. The edges are $\{\mathcal{E}_{1,2}, \mathcal{E}_{2,3}\}$.
 - 2.
 3. For \mathcal{N}_i , $\mathbb{S}_i = [r_i, r_{i+1}]$ for $i = \{1, 2, 3\}$. $\mathbb{B}_1^{\text{ext}} = r_1$, $\mathbb{B}_3^{\text{ext}} = r_4$ and $\mathbb{B}_2^{\text{ext}} = \emptyset$.
 4. For every edge $\mathcal{E}_{i,j}$, $\mathbb{B}_{1,2}^I = r_2$ and $\mathbb{B}_{2,3}^I = r_3$.
- $$A = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 0 & 1 \\ 0 & 1 & 0 \end{bmatrix}.$$

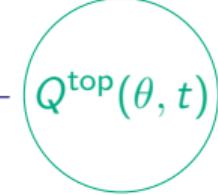
Example: Boundary Control of Ophthalmic Drug Delivery

Model:

$$\frac{\partial m_i(r, \theta, t)}{\partial t} = \frac{D_i}{r} \frac{\partial}{\partial r} \left(r \frac{\partial m_i(r, \theta, t)}{\partial r} \right) + \frac{D_i}{r^2} \left(\frac{\partial^2 m_i(r, \theta, t)}{\partial \theta^2} \right).$$

External Boundary conditions:

$$h_1^{-1} D_1 \frac{\partial m_1(r_1, \theta, t)}{\partial r} = [m_1(r_1, \theta, t) - m_0(\theta)],$$

$$h_4^{-1} D_3 \frac{\partial m_3(r_4, \theta, t)}{\partial r} = -[m_3(r_4, \theta, t) - Q^{\text{top}}(\theta, t)].$$


Interface Boundary conditions $i, j = 1, 2$:

$$\begin{bmatrix} I & -I \\ D_i \frac{\partial}{\partial b_{i,j}^I} & -D_j \frac{\partial}{\partial b_{i,j}^I} \end{bmatrix} \begin{bmatrix} m_i(r_{i+1}) \\ m_j(r_{j+1}) \end{bmatrix} = 0.$$

Example: Boundary Control of Ophthalmic Drug Delivery

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Conclusion and Future work

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Conclusion

1. Generic framework to explicitly include the spatial interconnection.
2. Interconnection is viewed as an exchange of interface input-output.
3. Reduced order solution of a well-posed boundary control systems.

Future Work

1. Interconnection in the view of dissipation.
2. Considering time varying topology (e.g. drying of papers).
3. Including multi-physics models (e.g. fluid dynamics, thermo-elasticity).

Thank You

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