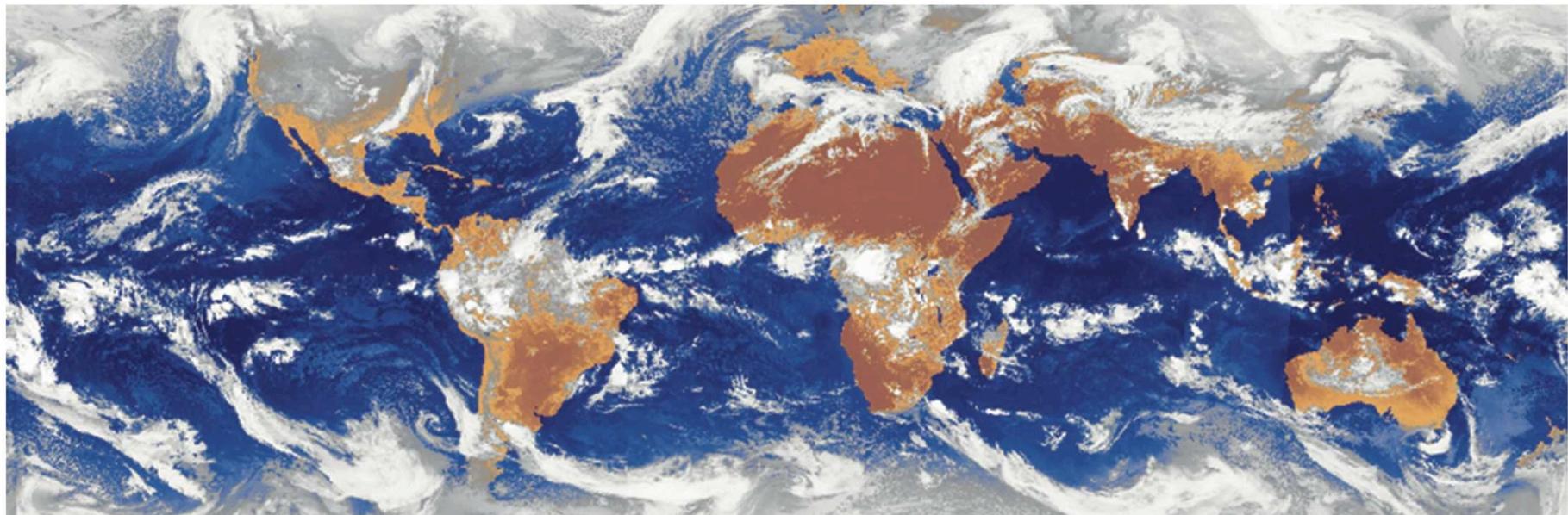


# Cloud mixing and cloud mixing feedbacks

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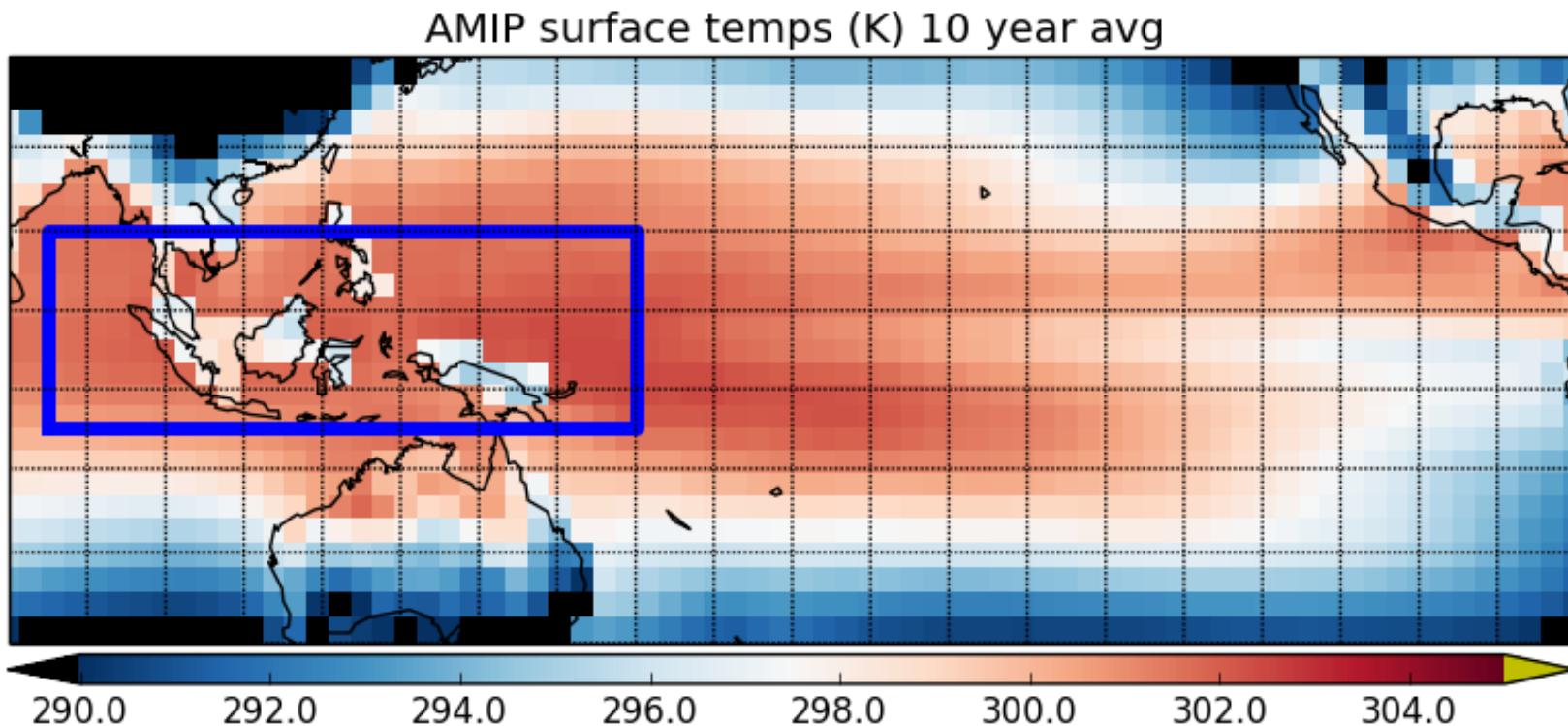


# Introduction

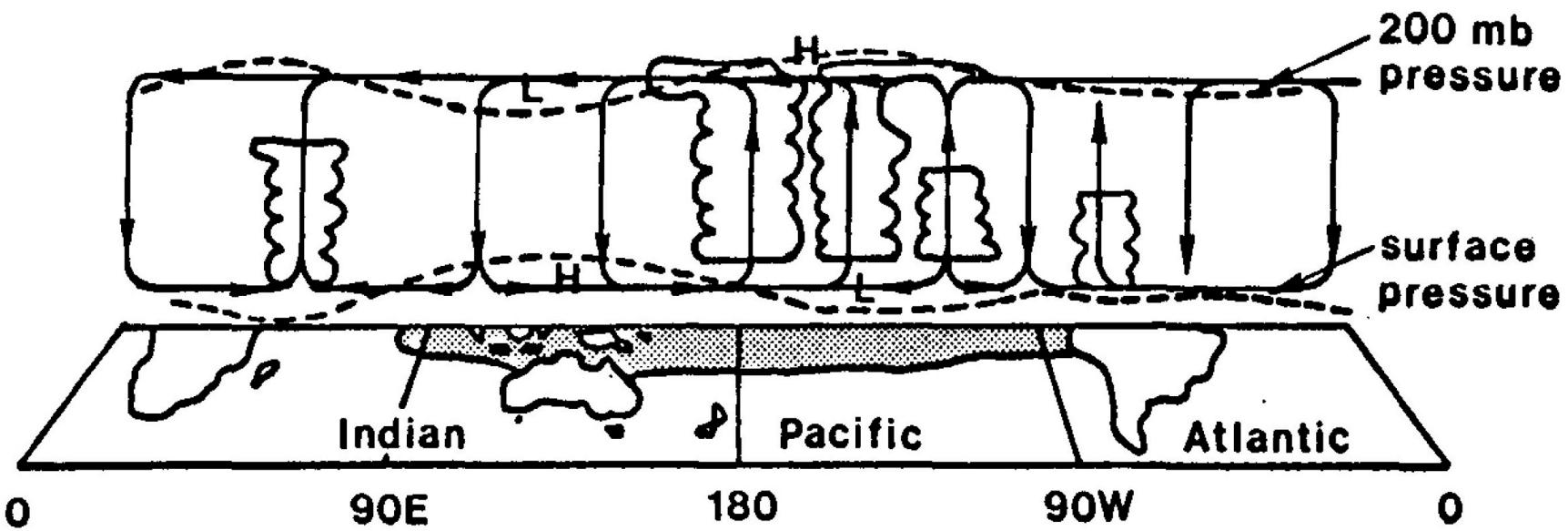
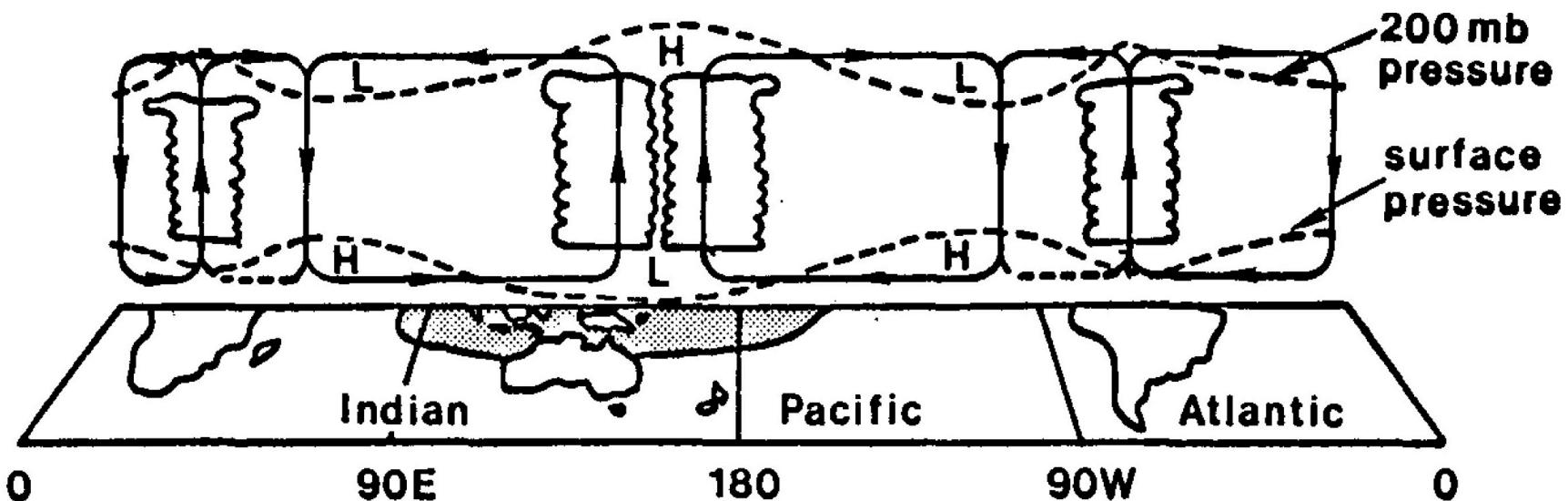
- Focus on small scale convection (cloud tops < 700 hPa) at scales from ocean-wide (GCM) to GCM gridcell (SCM), to individual clouds (25 meters)
- **Questions**
  - How does the parameterization of convective transport in large scale models contribute to their equilibrium climate sensitivity?
  - What can we learn about convective mixing from high resolution cloud models, and how can this inform parameterization development?
- **Three sections:**
  - Moisture transport and climate sensitivity in CMIP5 models (after Sherwood, Bony and Dufresne, Nature, Jan 2, 2014)
  - Results from the CGILS single column model and large eddy intercomparison of shallow convection (Zhang and 33 co-authors (incl. KvS and PHA), JAMES, vol. 5, Dec. 2013.
  - High resolution LES of entrainment and detrainment in shallow cumulus (Dawe and Austin 2011a,b, 2012, 2013), papers at <http://www.cafc.ubc.ca>

## Part 1: Linking boundary layer mixing to cloud feedback

Deep convection in the tropical warm pool is tightly coupled to boundary layer clouds in the subtropics

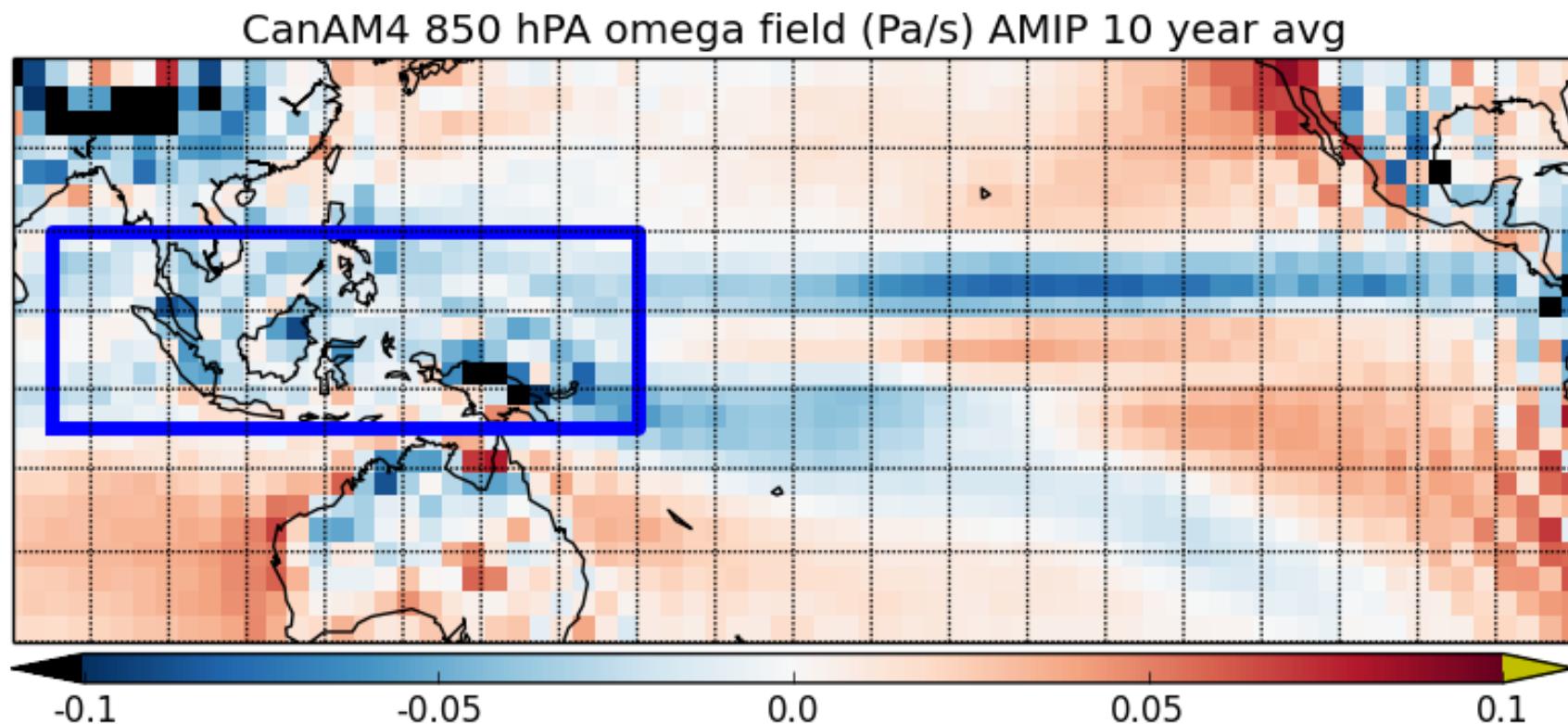


# Walker circulation connects the west/east Pacific

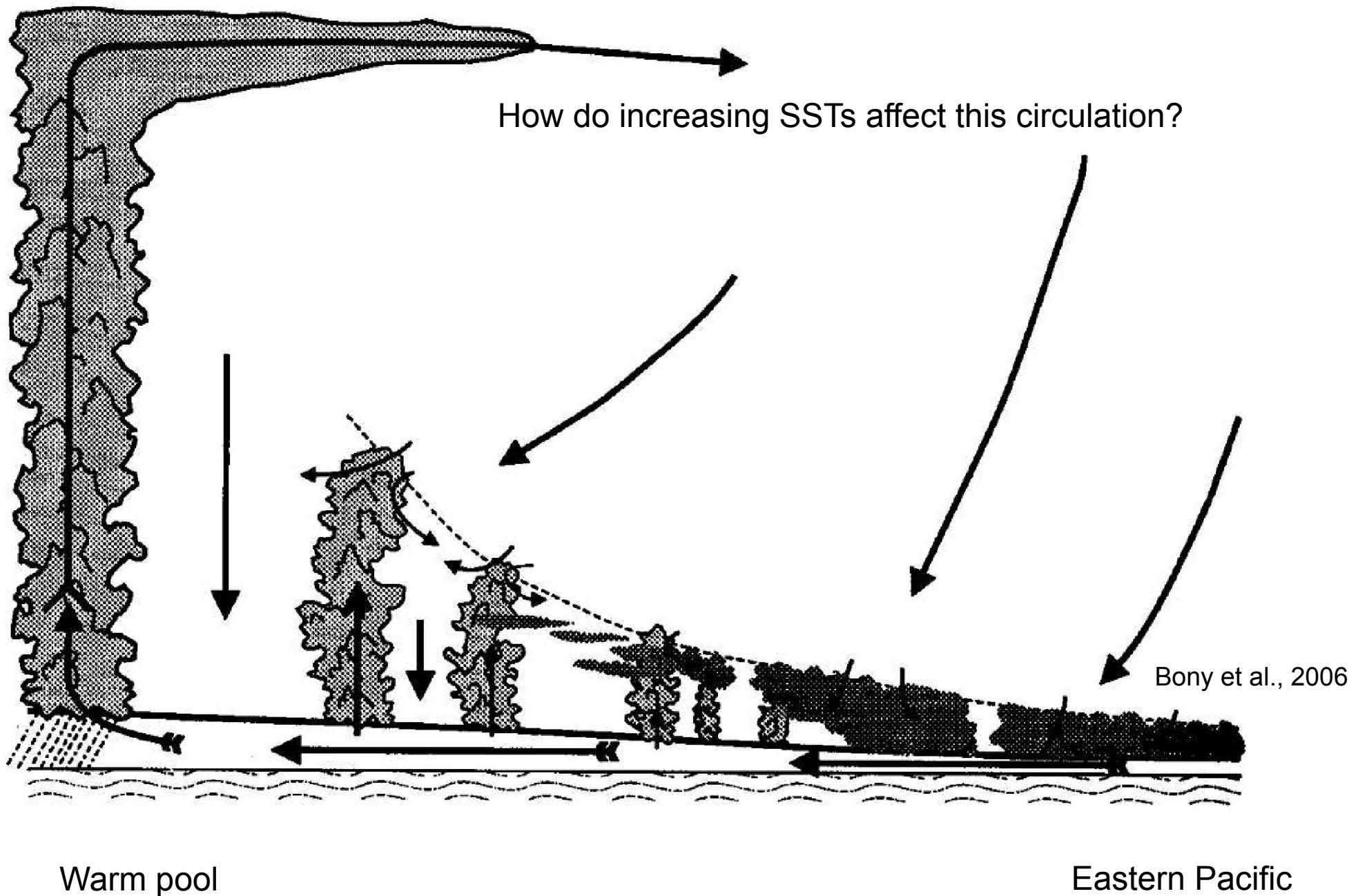


Webster, 1983

# Large scale vertical velocity at 850 hPa, CanAM4, current climate



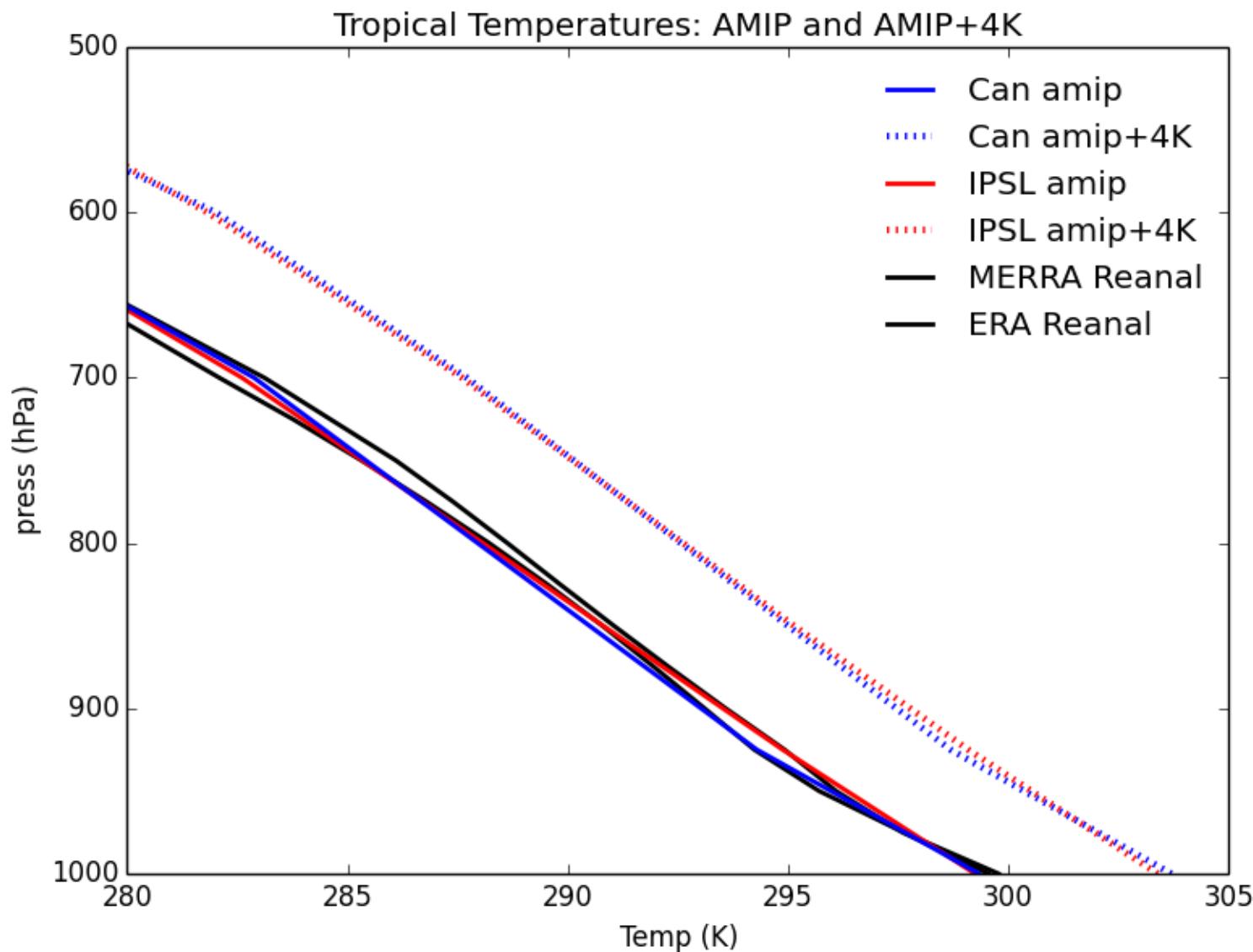
# Two box model of the tropical circulation



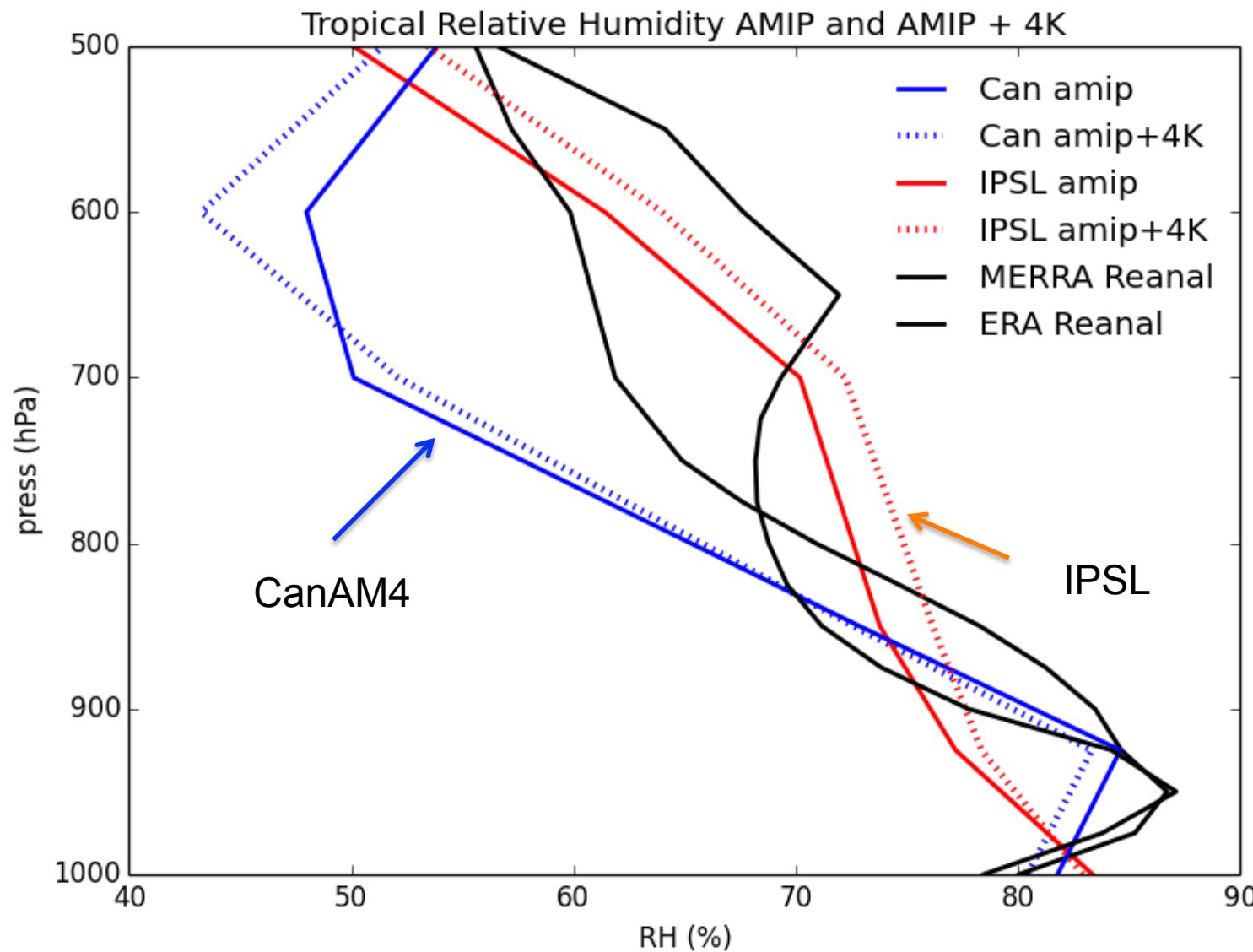
Decreasing large scale subsidence will affect cloud cover, feedback on net radiation



# Vertical temperature structure in tropics: CanAM4 and IPSL agree with reanalysis



Relative humidity: CanAM4 significantly drier than reanalysis at 700 hPa

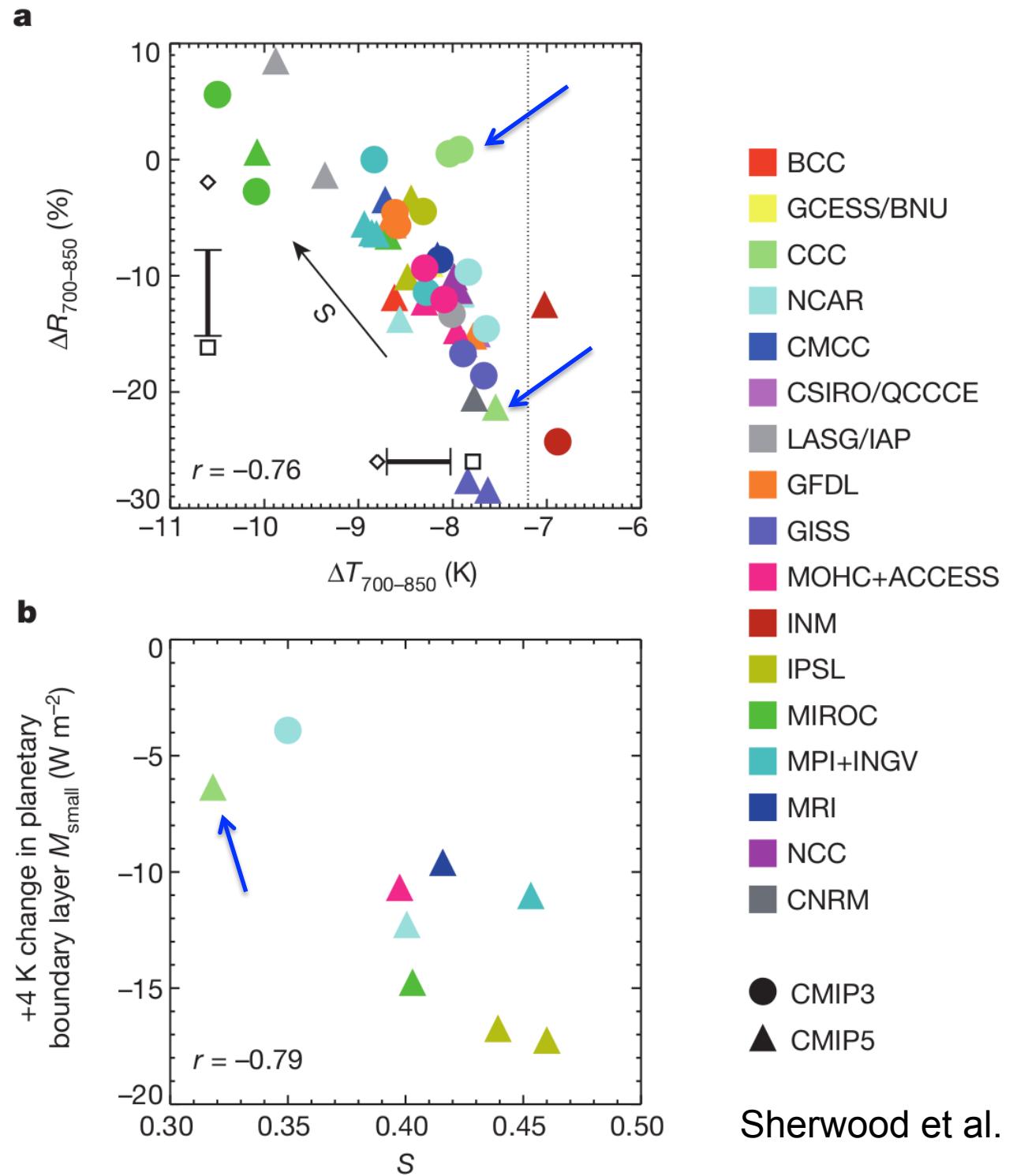


Sherwood et al. define a metric of “mixing strength”  $S$  in the tropics as:

$$S = (\Delta RH_{700-850} - \Delta T_{700-850}/9.)/2.$$

Models with large  $S$  have higher T and/or higher RH At 700 hPa. The hypothesis Is that this is because of active vertical mixing.

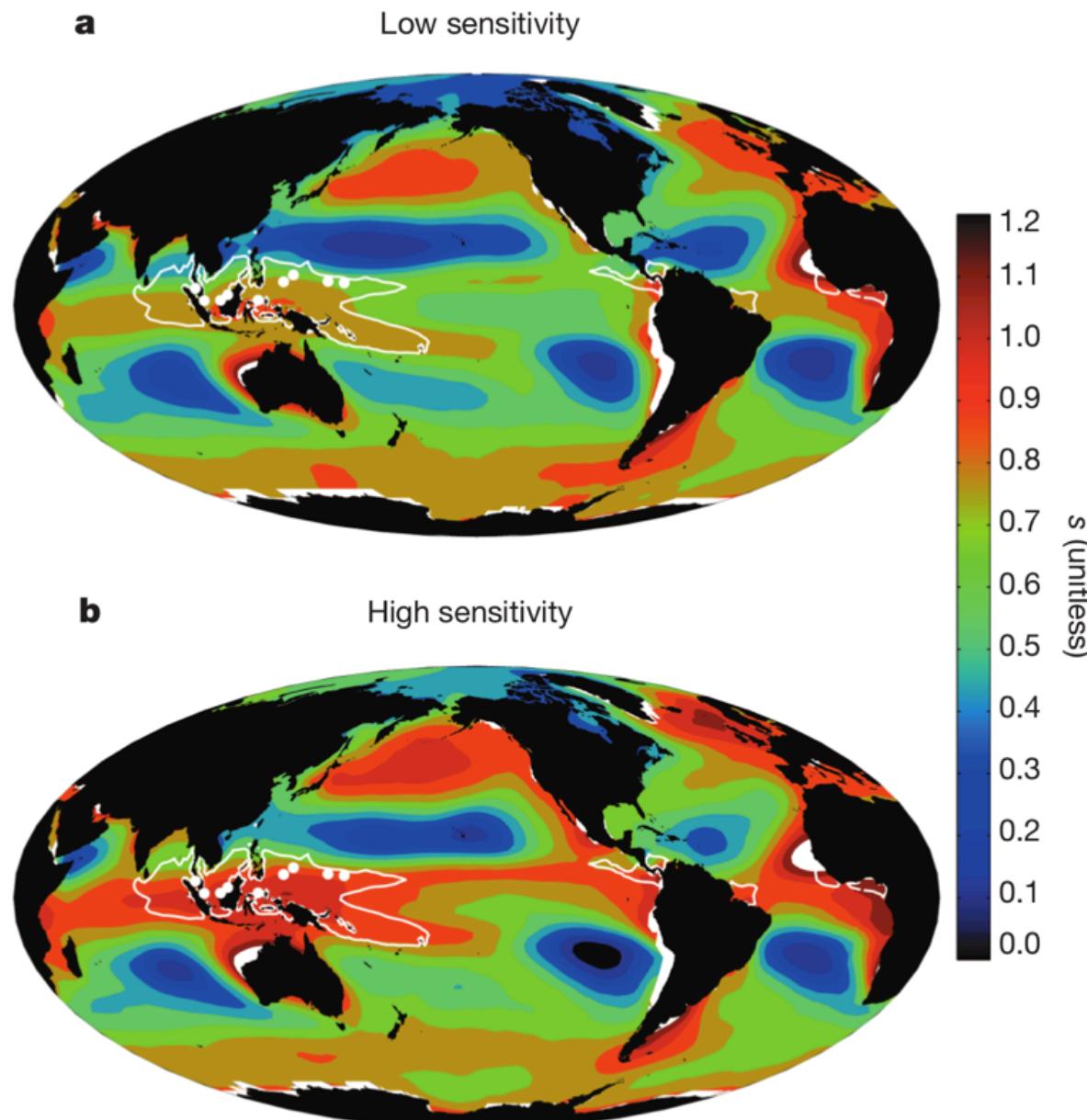
Models with active mixing tend to mix less in the AMIP+4K scenario – this reduces low-level cloud fraction and produces a positive cloud feedback



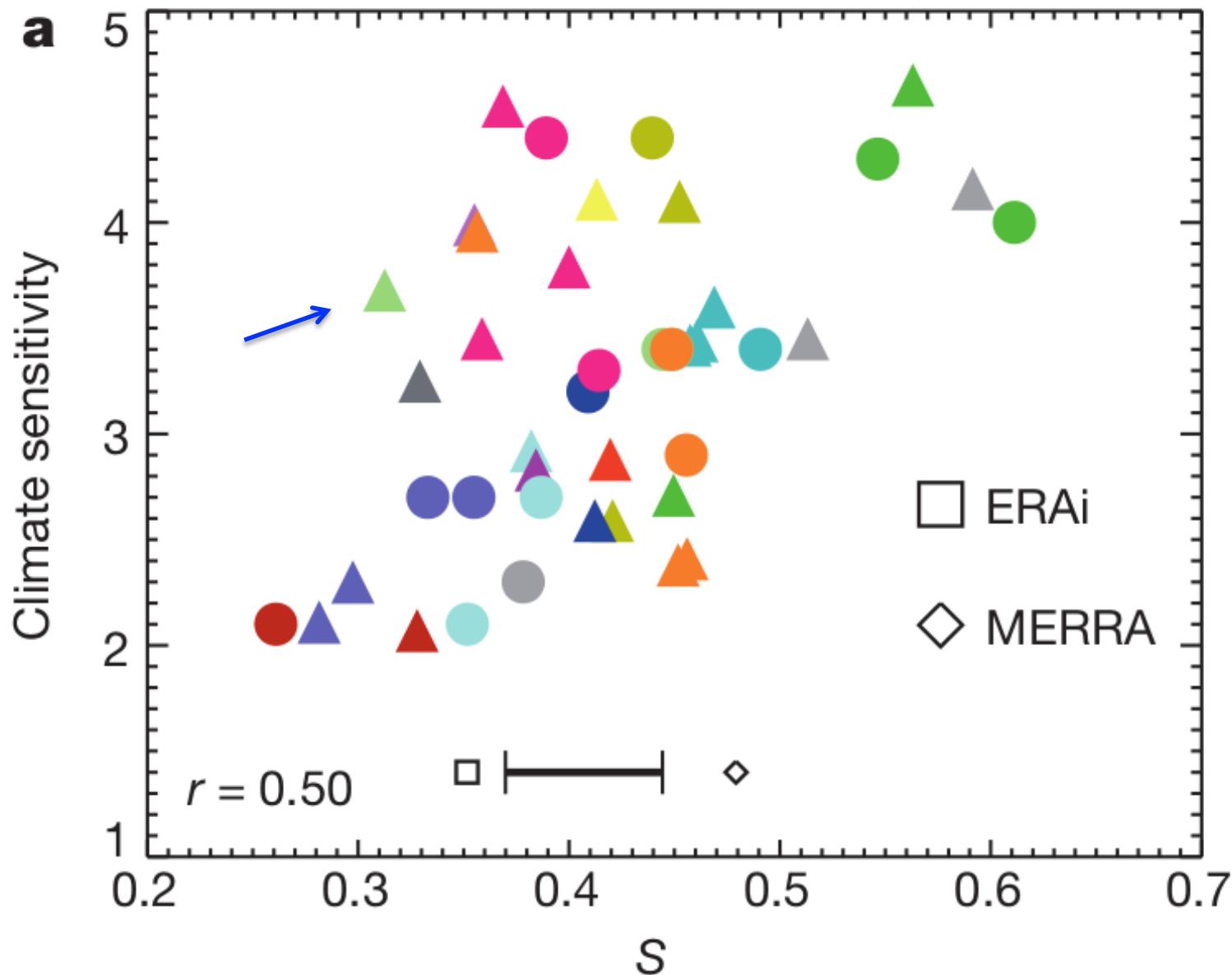
Sherwood et al.

Segment models into low (ECS < 3 K/doubling) and high (ECS > 3.5 K/doubling) groups

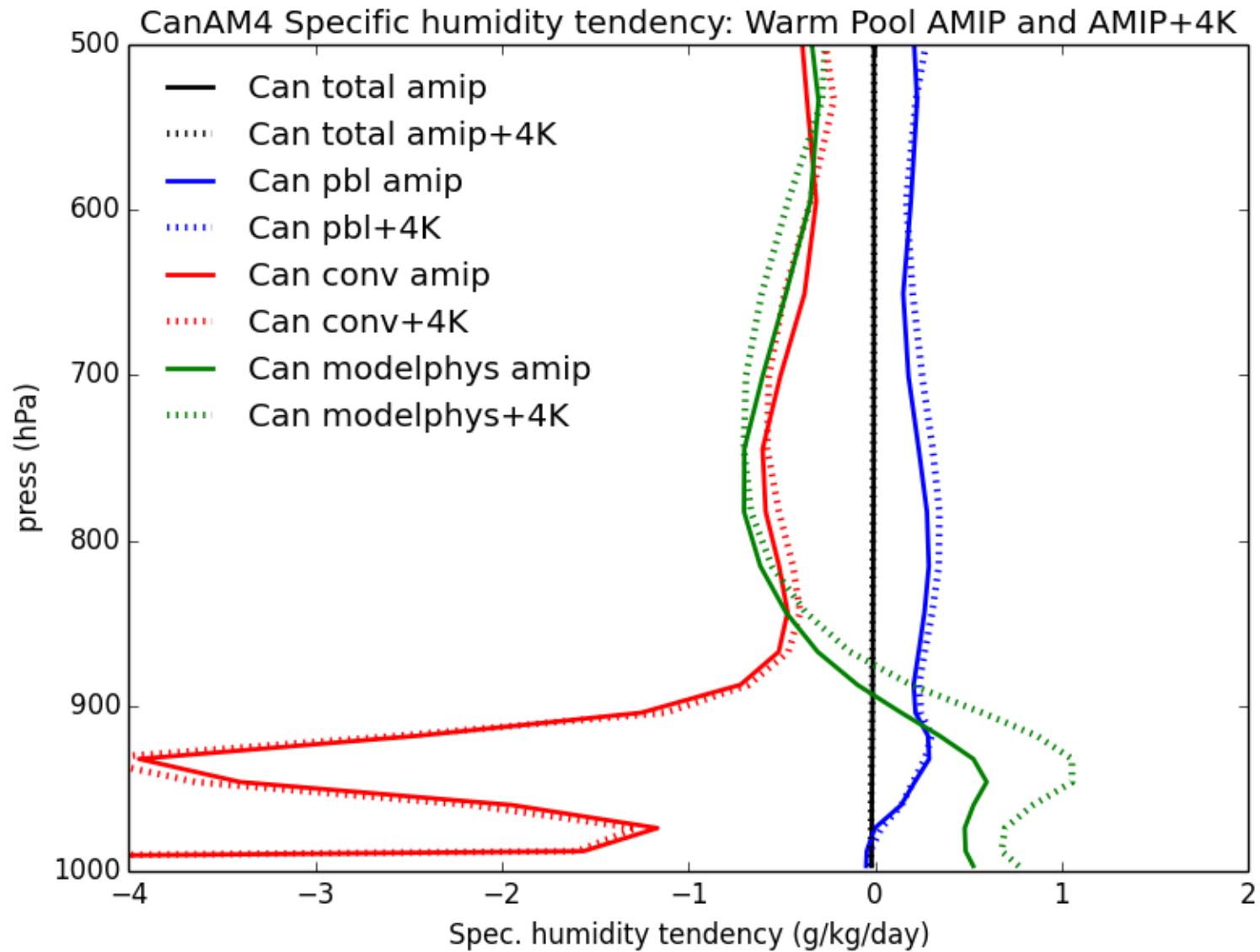
Major difference is strength of mixing in the tropics



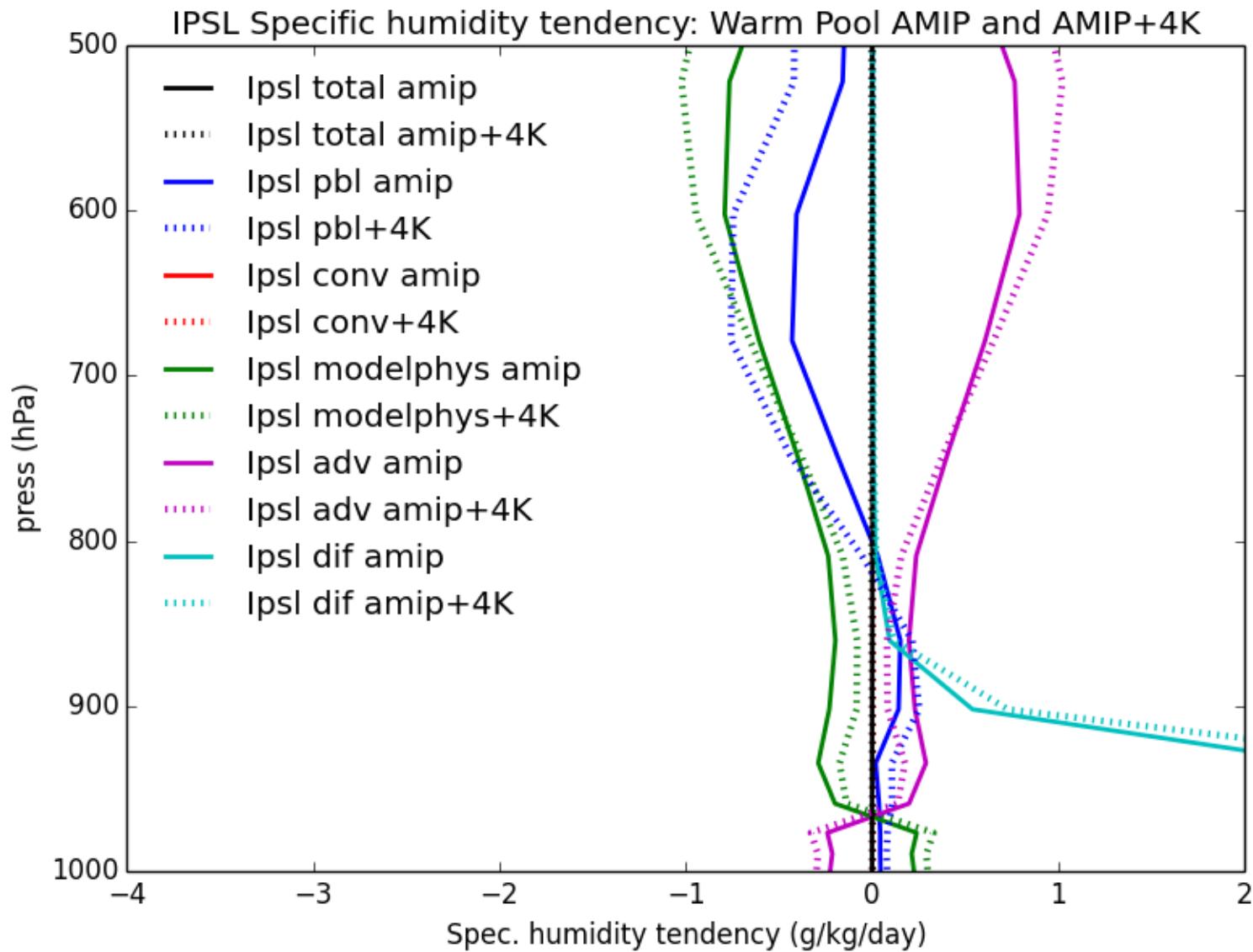
CanAM4 is atypical in the sense that it is weakly mixing but sensitive



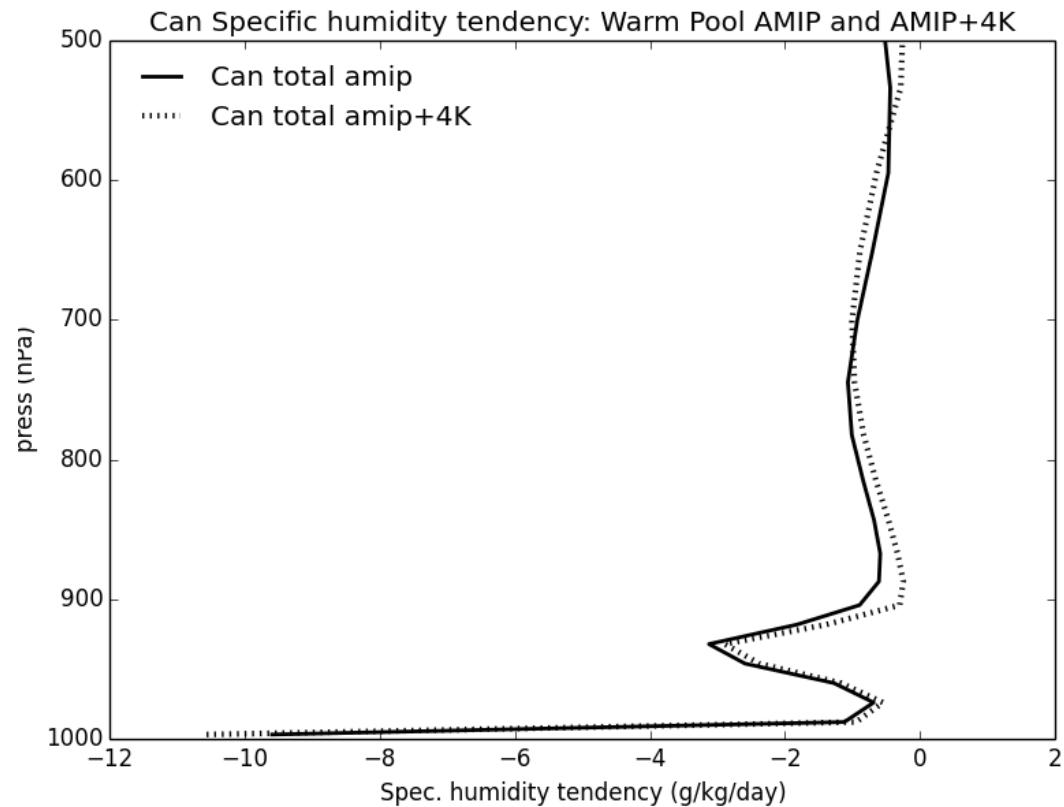
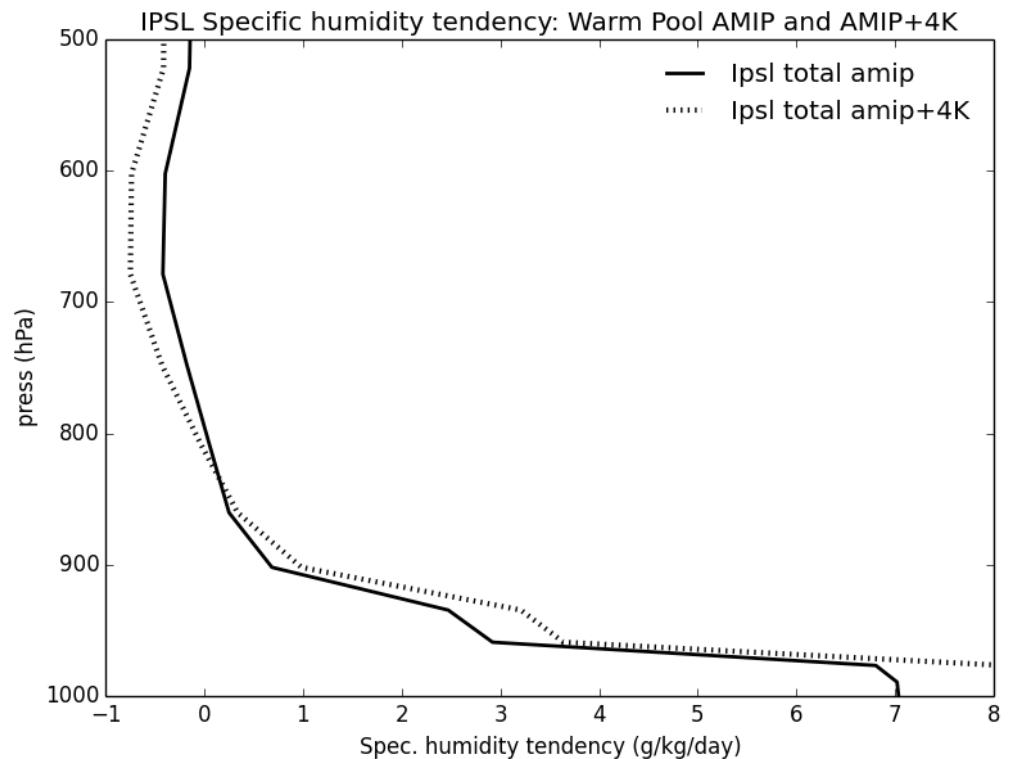
Specific humidity tendency indicates drying due to convection/turbulence dominates



IPSL shows larger response/increased drying in AMIP+4K



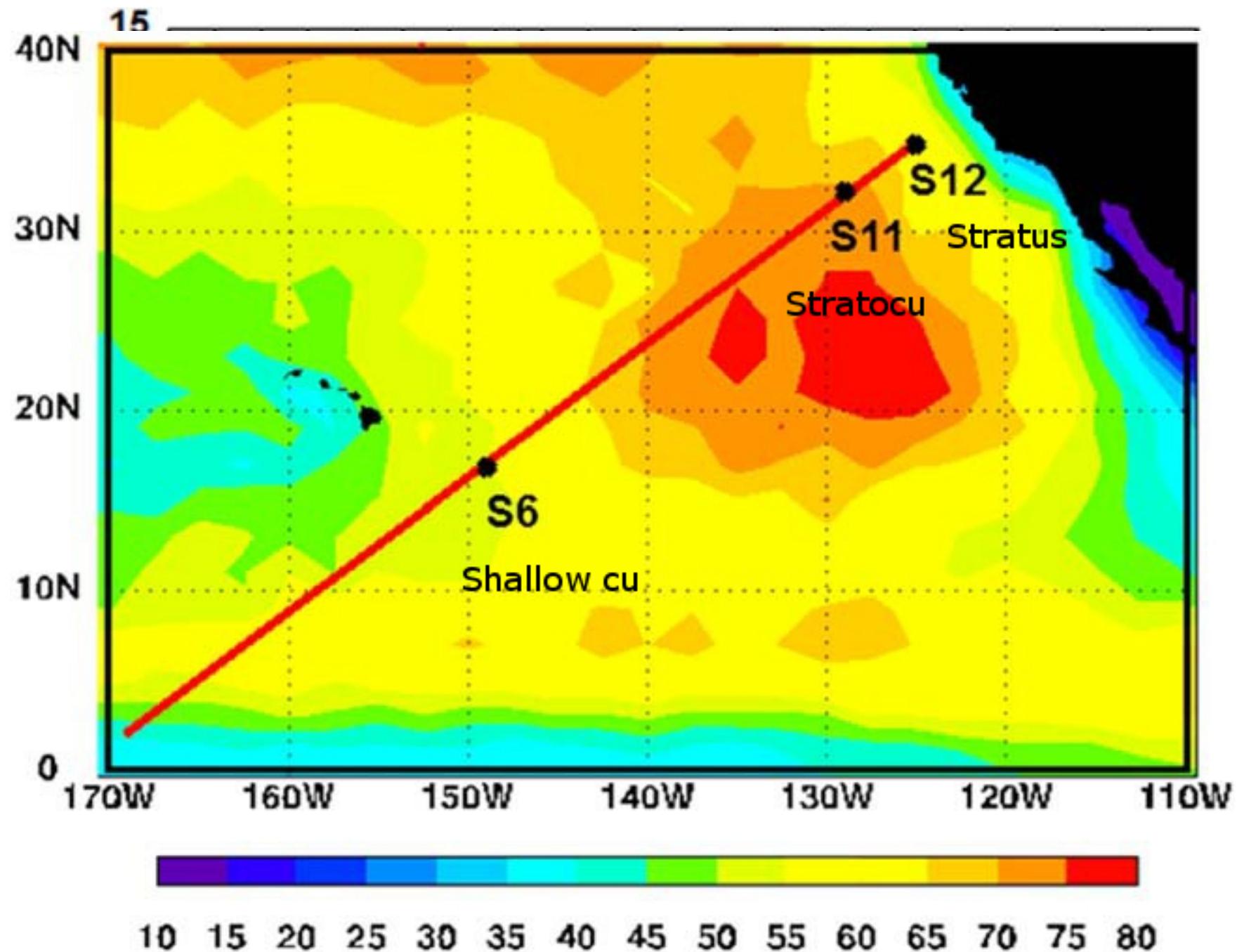
# Total specific humidity tendencies, CanAM4 and IPSL



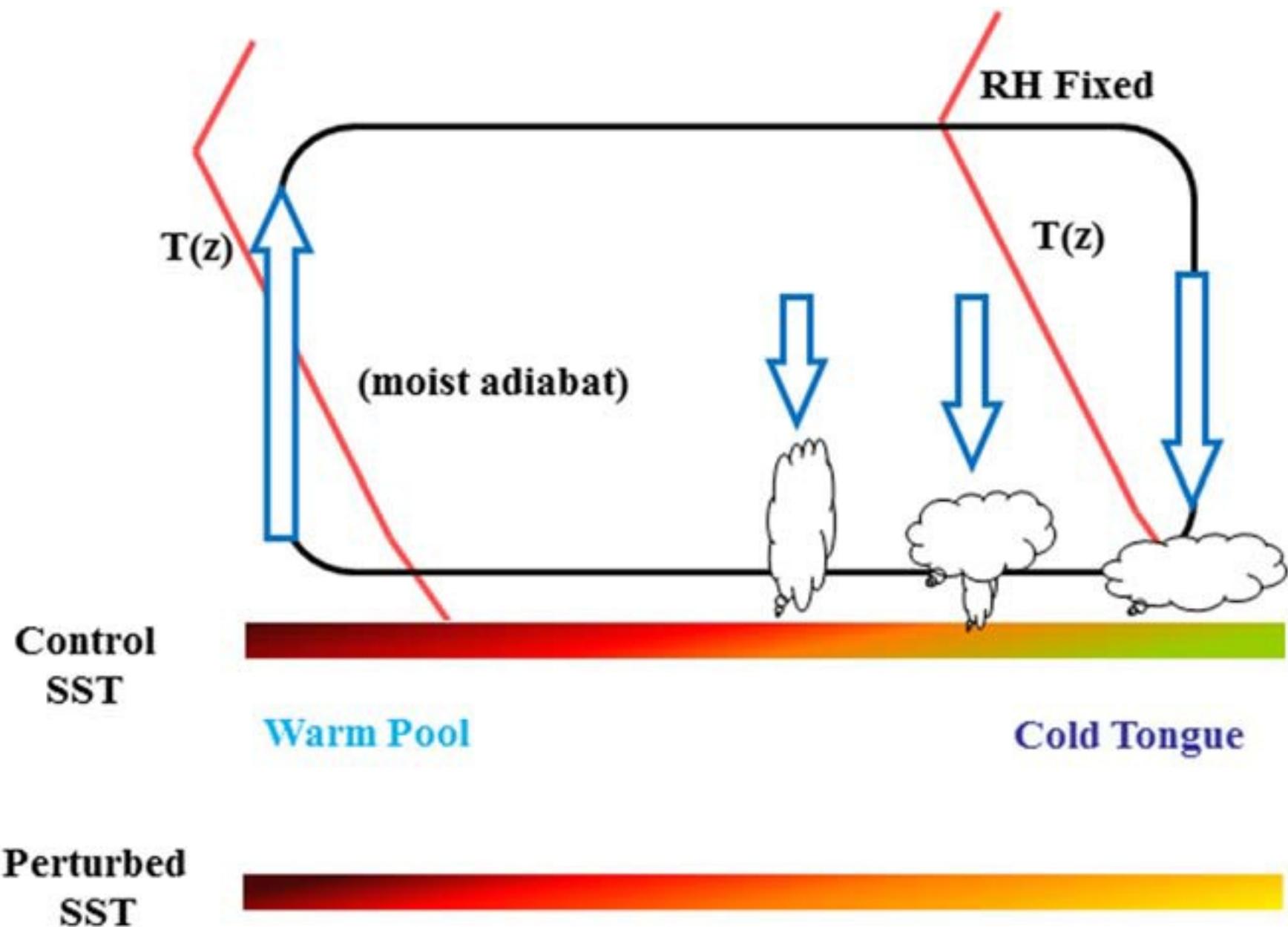
- In the absence of a mixing feedback in CanAM4, what is producing the large climate response? (Feedback analysis with Jason and Knut using ISCCP simulator output)
- How should boundary layer/convection be modified in CanAM4 to get more accurate moisture profiles in the tropics? (new SCM/CRM tropical convection intercomparison with Norm and Yanping)

Part 1 summary

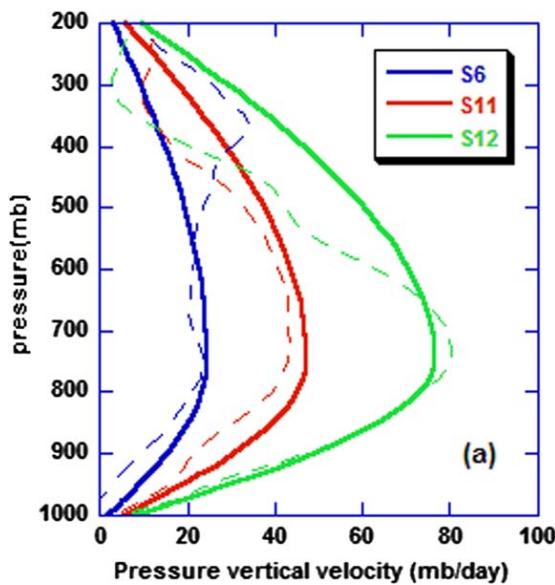
# CGILS intercomparison of single column models and large eddy simulations



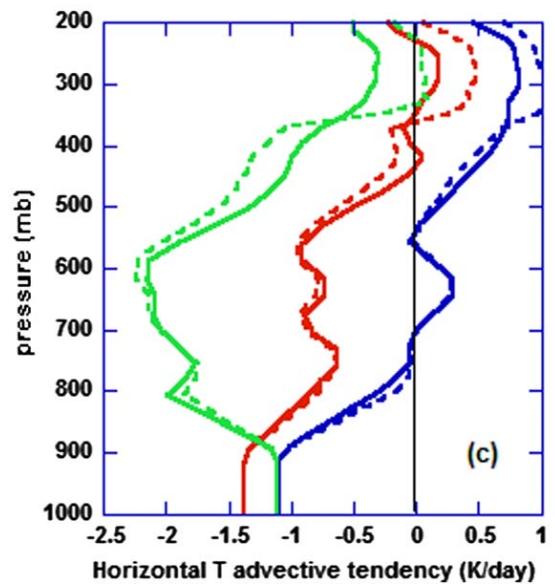
Basic idea -- simulate AMIP+4K in a single column assuming weak temperature gradient



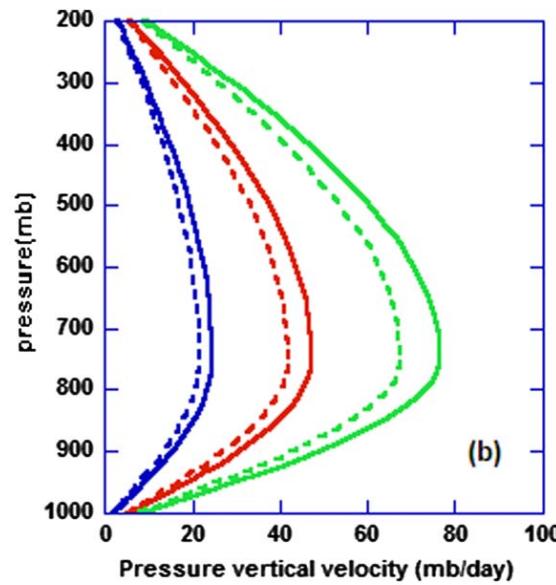
Subsidence in  
Current climate



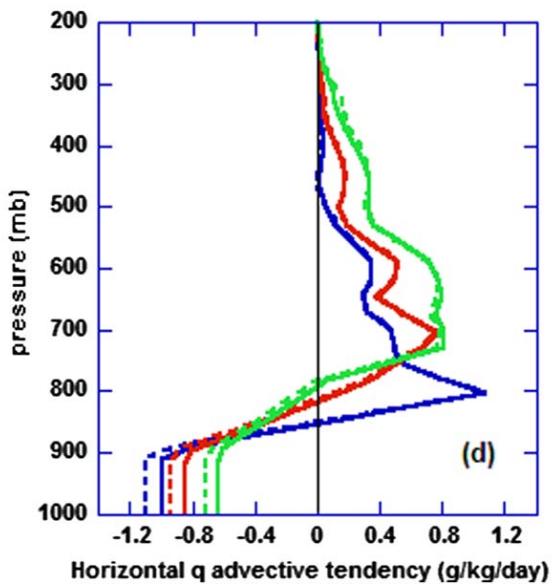
Specified large  
scale temperature  
tendency

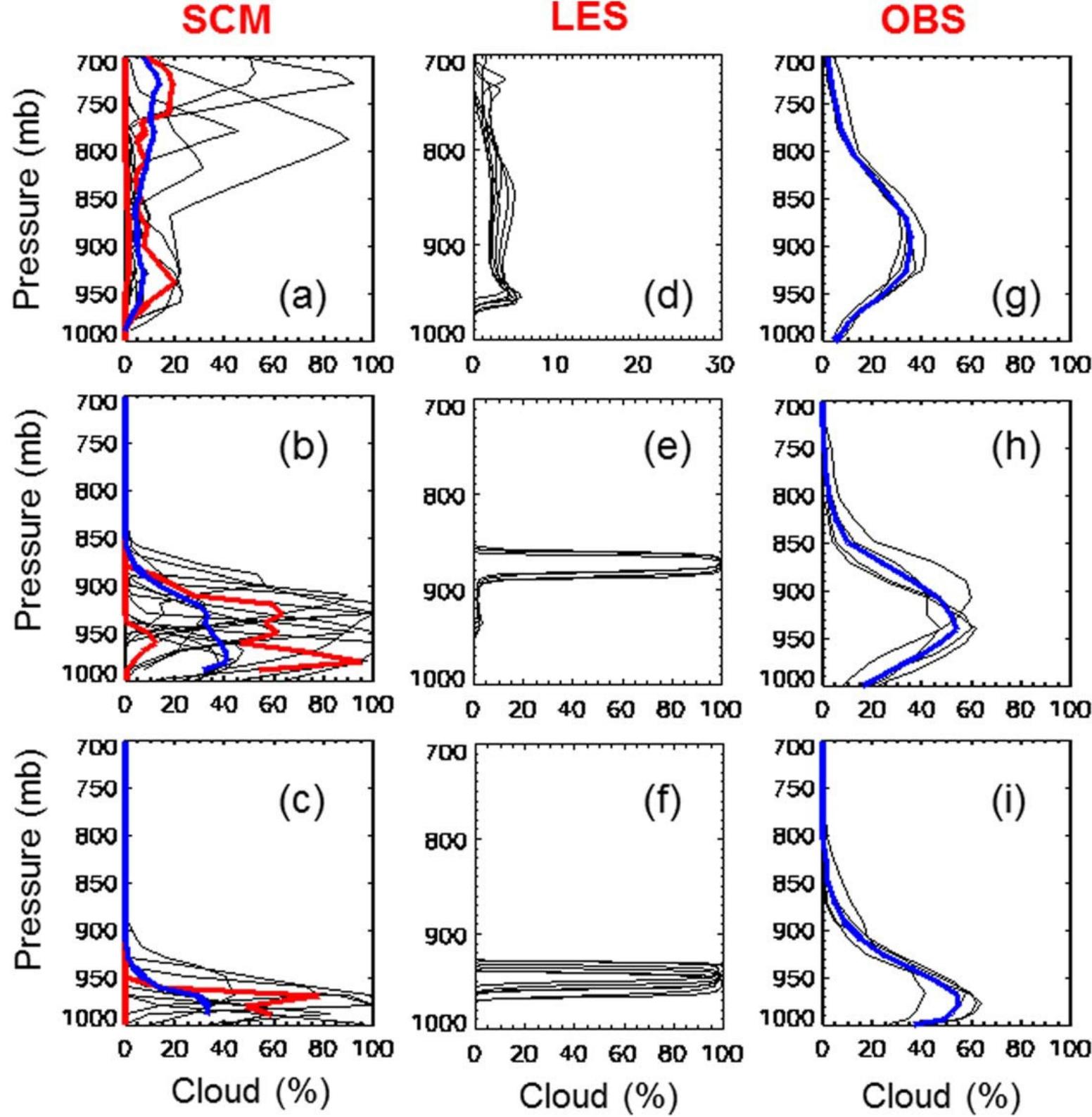


Subsidence in  
+4K climate (dashed)



Specified large  
scale moisture  
tendency





Shallow Cu

**S6**

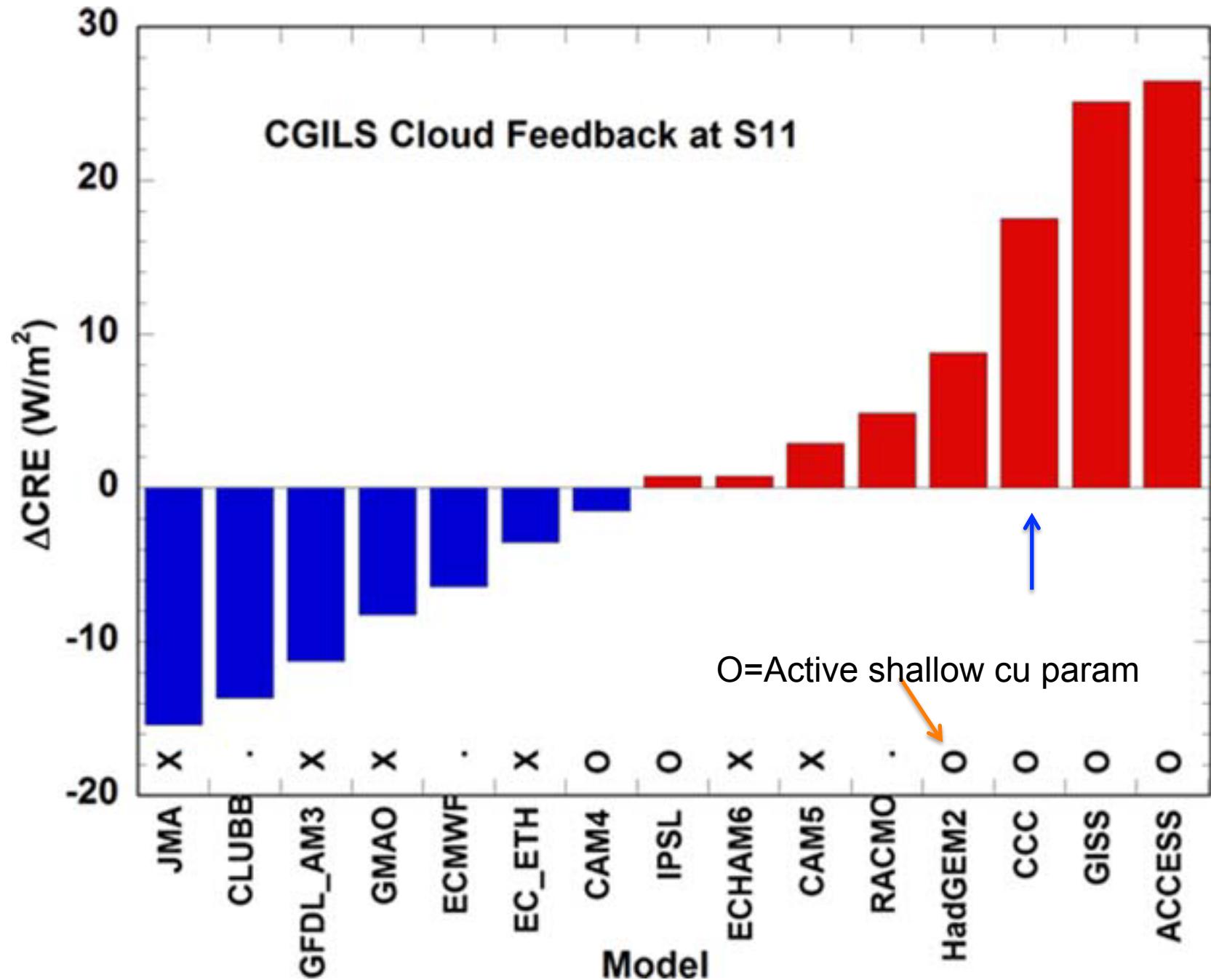
Stratocu

**S11**

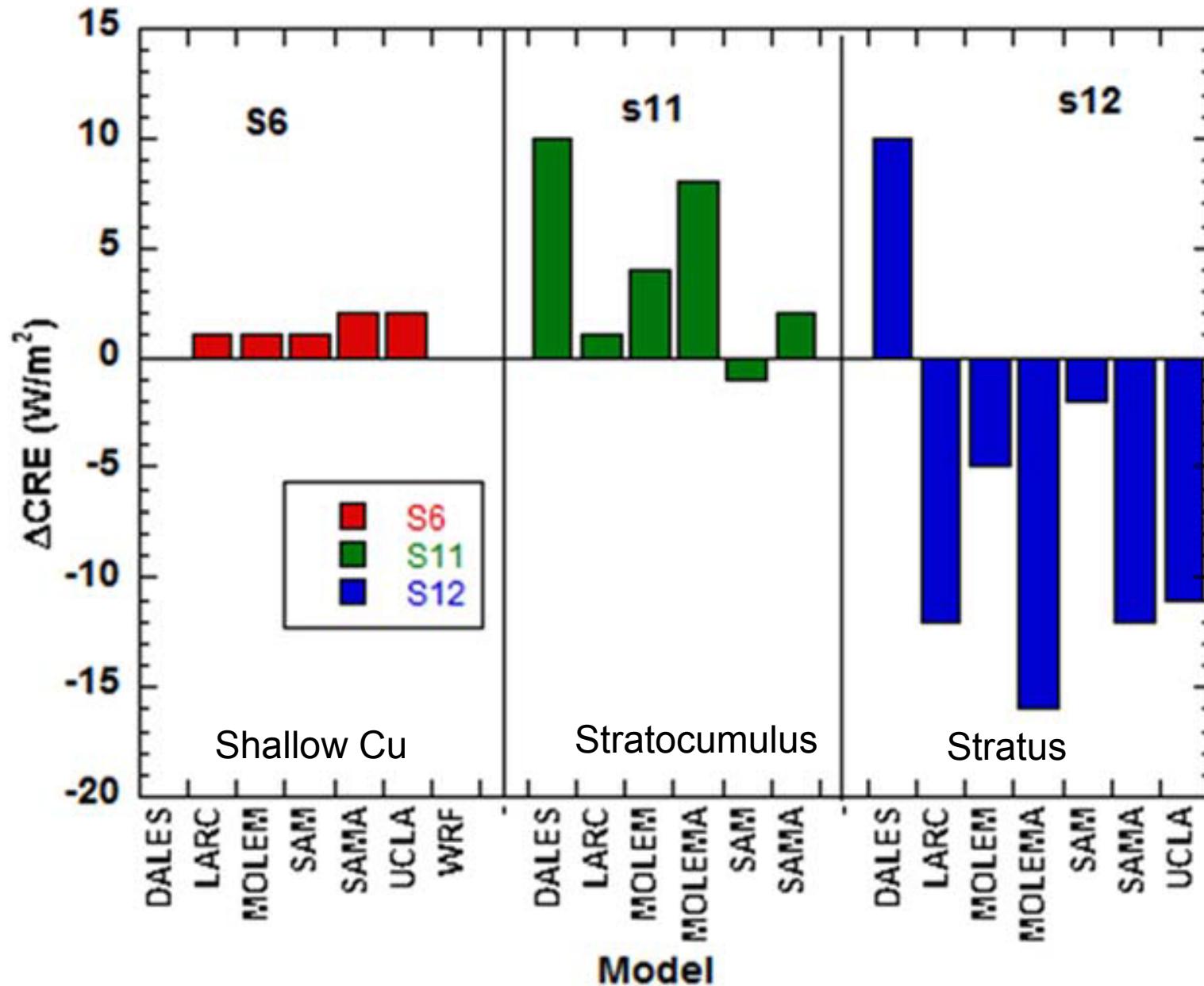
Stratus

**S12**

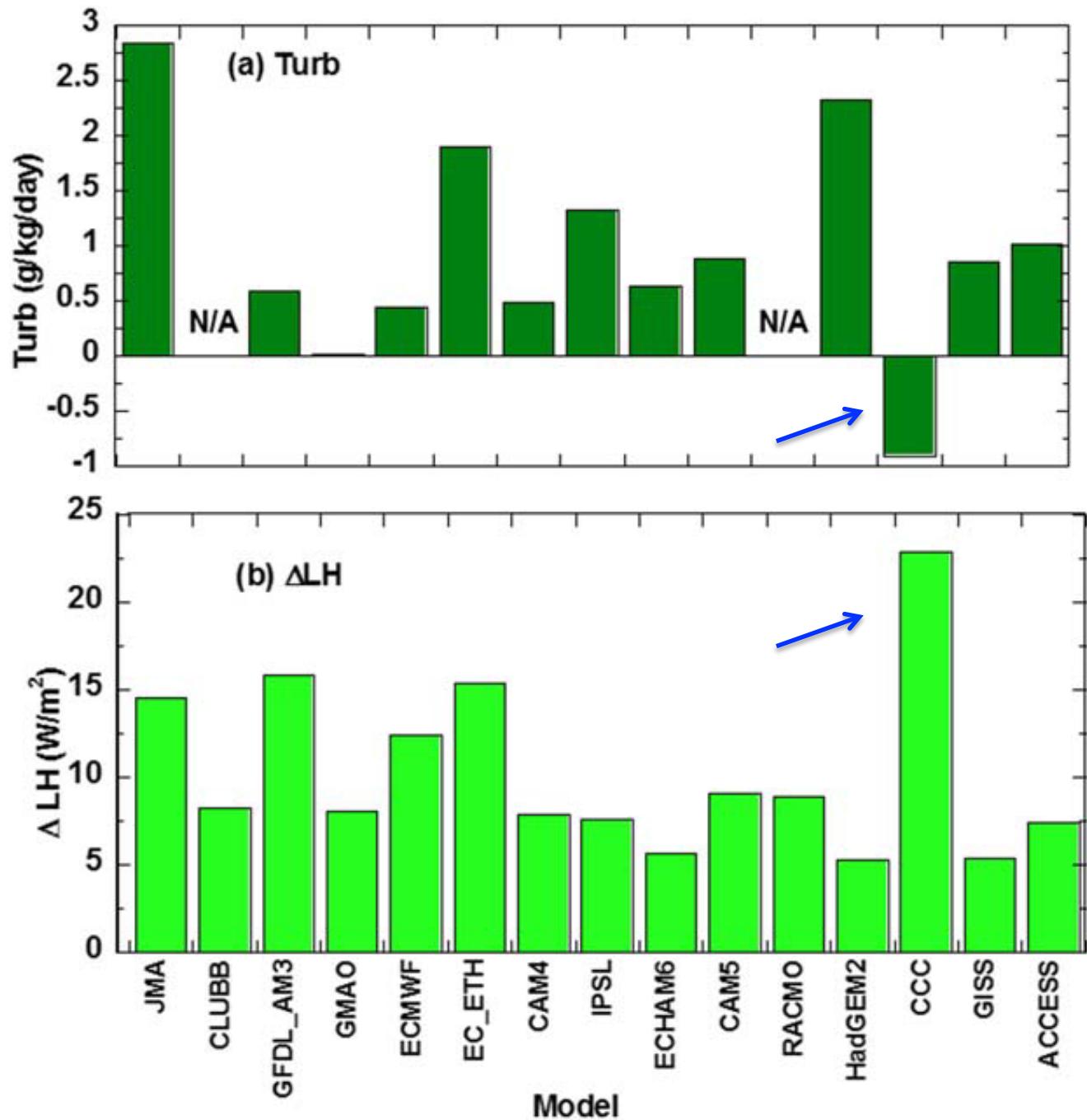
No consensus on sign or magnitude of stratocumulus cloud feedback



Most large eddy simulations have positive feedback at S11 (although significantly smaller)



Warming response for CanAM4 is to reduce turbulence and significantly increase surface vapor flux

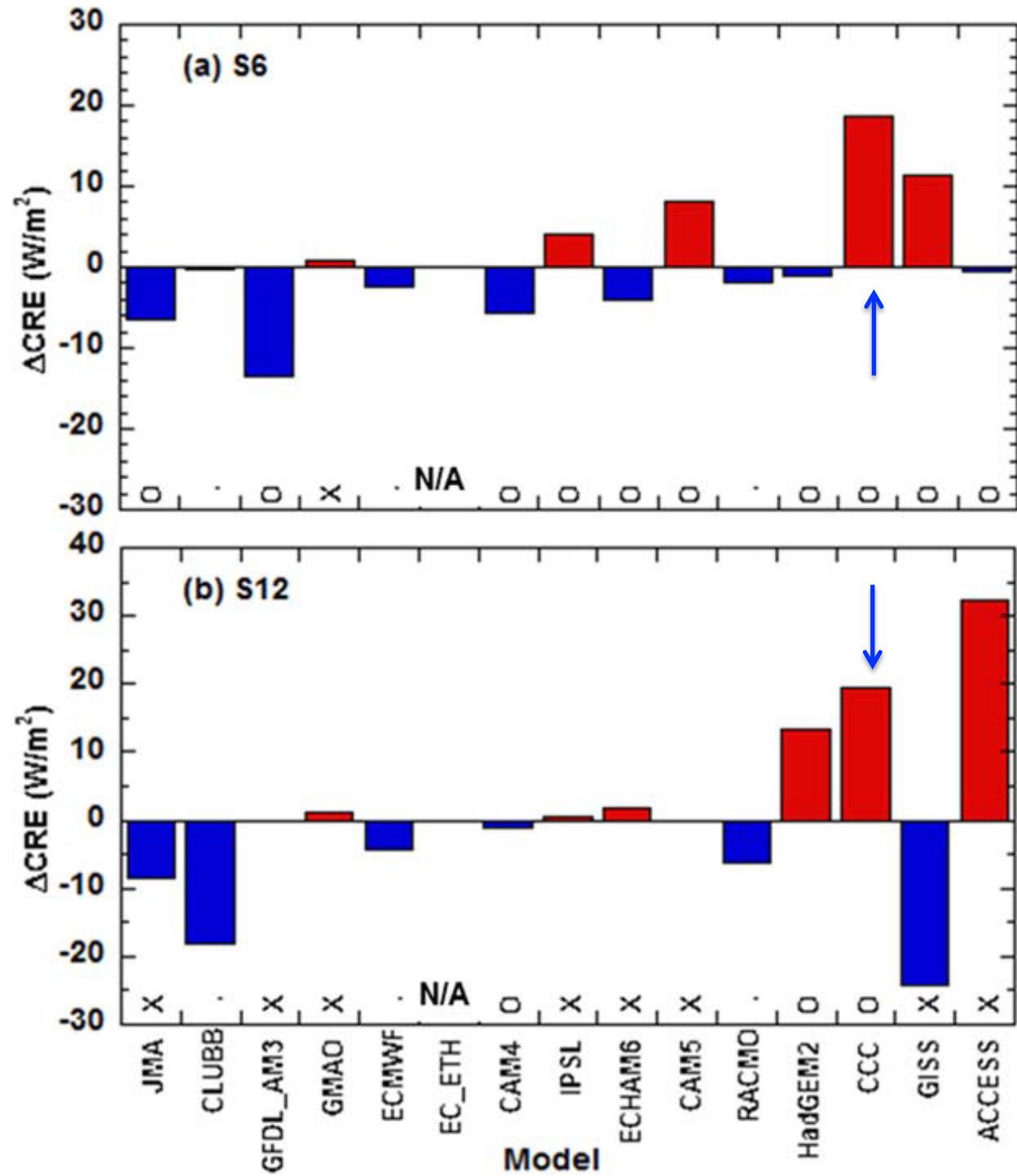


CanAM4 exhibits large positive feedback for Both Shallow Cu regime And for stratus

LES have small positive feedback for shallow cu, large negative feedback for stratus.

Part II summary: SCM shows Significant low cloud feedbacks In all cloud categories in the subsidence regime in the Eastern subtropical Pacific.

Next steps: return CGILS cases with new TKE boundary Layer parameterization



## Entrainment: Some definitions and a simple mixing parameterization:

$$E = -\frac{1}{A} \oint_{\hat{\mathbf{n}} \cdot (\mathbf{u} - \mathbf{u}_i) < 0} \rho \hat{\mathbf{n}} \cdot (\mathbf{u} - \mathbf{u}_i) dl \quad (kg \, m^{-3} \, s^{-1}) \quad \text{Entrainment rate}$$

$$D = \frac{1}{A} \oint_{\hat{\mathbf{n}} \cdot (\mathbf{u} - \mathbf{u}_i) > 0} \rho \hat{\mathbf{n}} \cdot (\mathbf{u} - \mathbf{u}_i) dl \quad (kg \, m^{-3} \, s^{-1}) \quad \text{Detrainment rate}$$

$$M = \rho w \quad (kg \, m \, s^{-2}) \quad \text{Vertical mass flux}$$

$$M_{core} \frac{\partial \phi_{core}}{\partial z} = E(\phi_{env} - \phi_{core}) \quad \text{Cloud core tracer plume budget, constant cloud fraction}$$

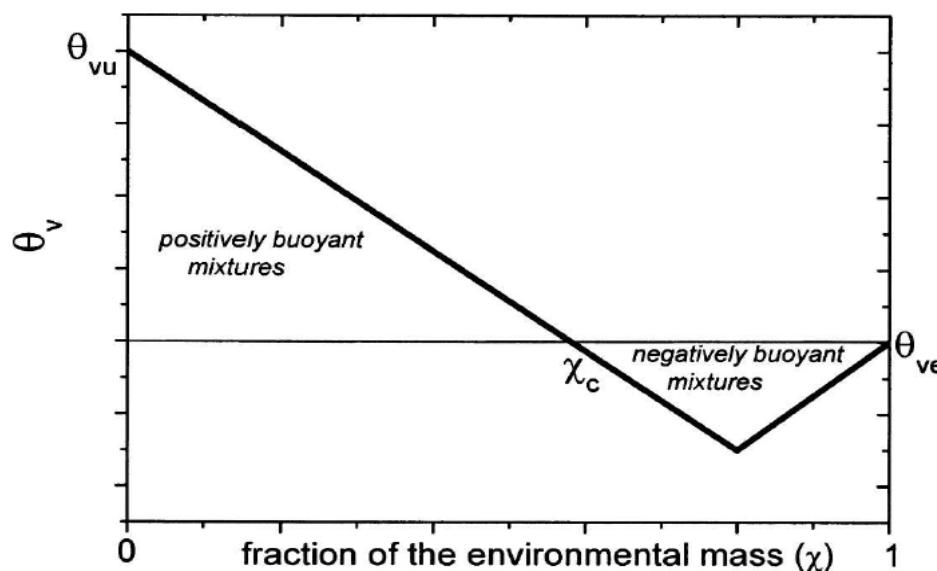
$$\rho \frac{\partial \phi_{env}}{\partial t} = D(\phi_{core} - \phi_{env}) \quad \text{Environment tracer budget}$$

$$\epsilon = E/M_{core}, \quad \delta = D/M_{core} \quad (s^{-1}) \quad \text{Fractional entrainment and detrainment rates}$$

# Background

- BOMEX and ARM-diurnal simulations with SAM 6.8.2 LES
- 25 m grid size in x,y,z on ~ 6 km x 6 km horizontal domain
- One minute snapshots
- 4362 tracked clouds over 12 simulation hours
- Filter out clouds smaller than 16 gridcells (50% of population, 5% of mass flux)
- 120,000 individual samples of entrainment and detrainment rates with coincident samples of buoyancy, vertical velocity, environmental stability, critical mixing fraction  $\chi_c$

$\chi_c$



Movie: Cloud tracking for life-cycle measurements of entrainment/detrainment  
in the UBC-SAM LES

- Question: Do LES measurements of direct entrainment/detrainment provide constraints on parameterizations of  $\epsilon$  and  $\delta$ , e.g:

$$\epsilon = \frac{\alpha B}{w^2} - \frac{1}{w} \frac{\partial w}{\partial z}$$

$$\epsilon = \epsilon_0$$

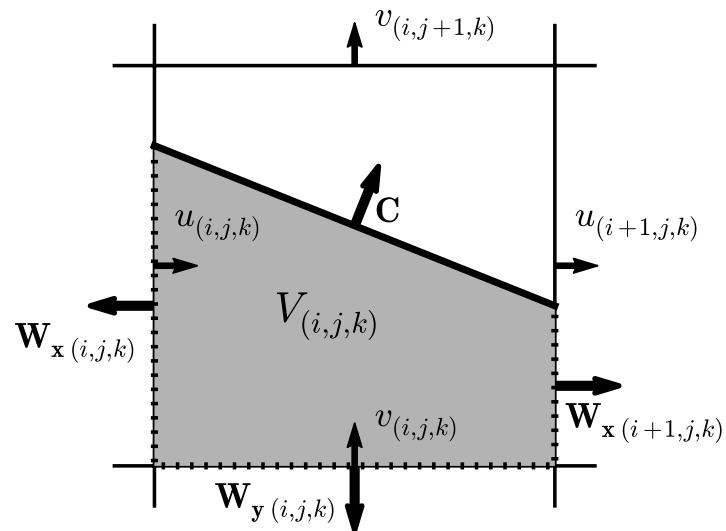
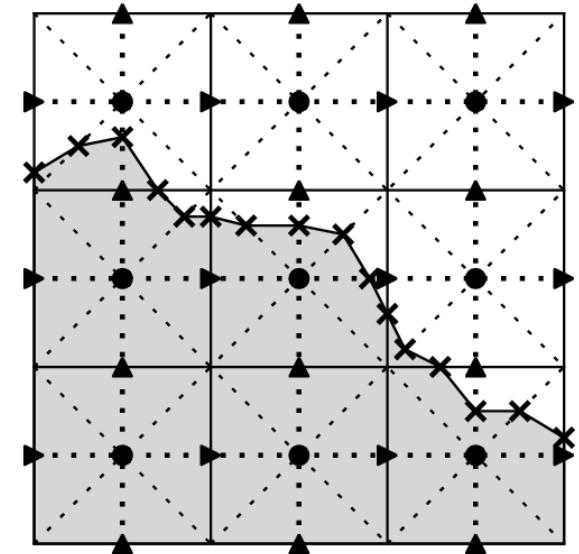
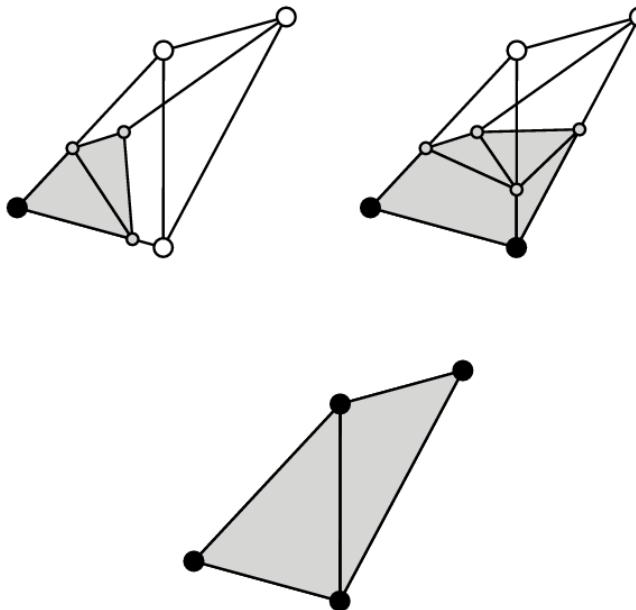
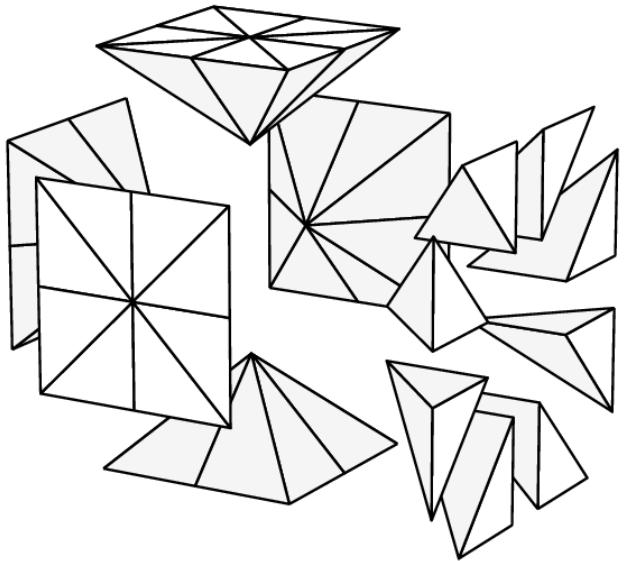
$$\epsilon = \frac{n}{\tau_p} \frac{1}{w_p}$$

$$\epsilon = \epsilon_0 \chi_c^2$$

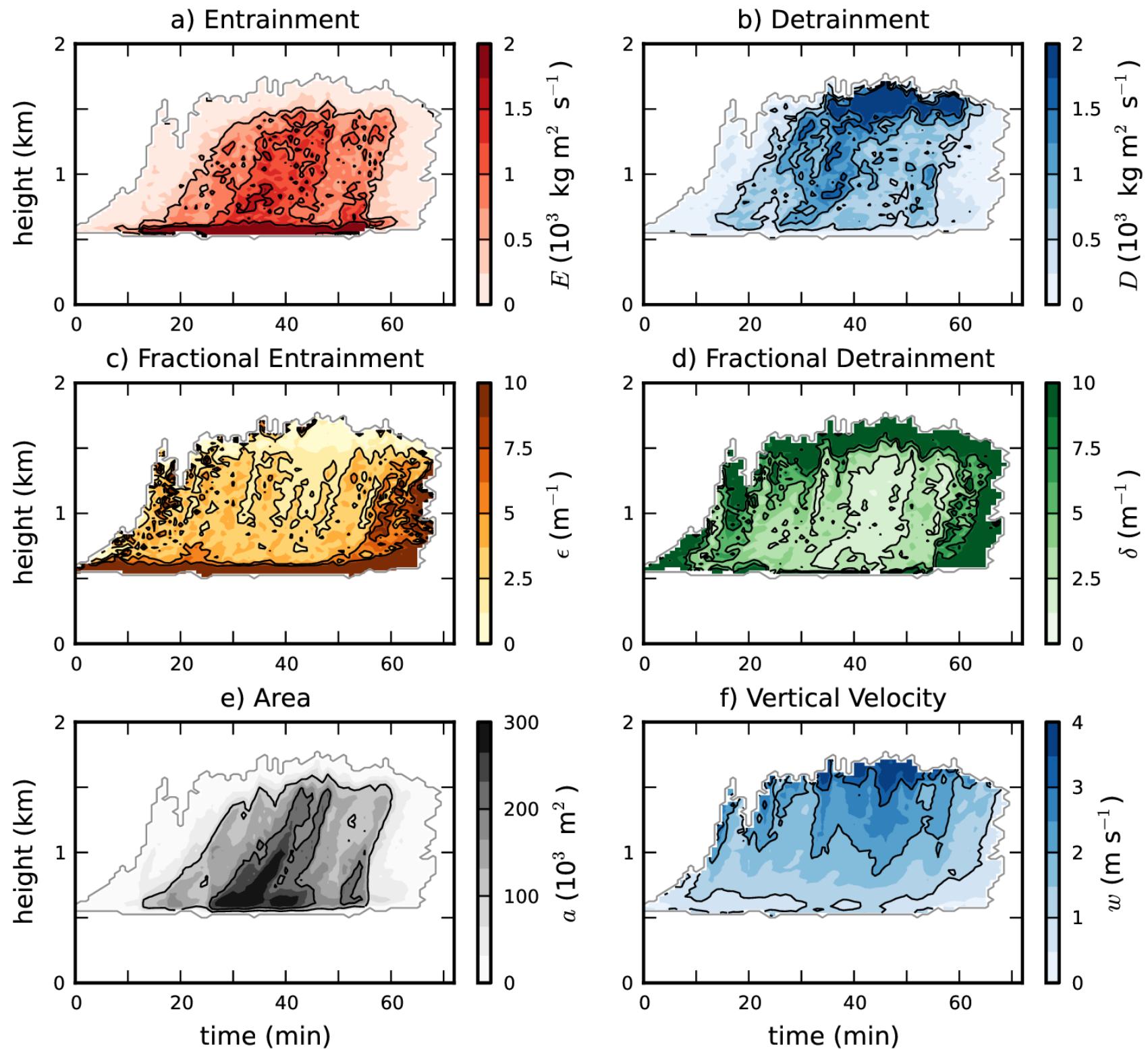
$$\epsilon = c_e z^{-1}$$

$$\delta = \epsilon_0 (1 - \chi_c)^2$$

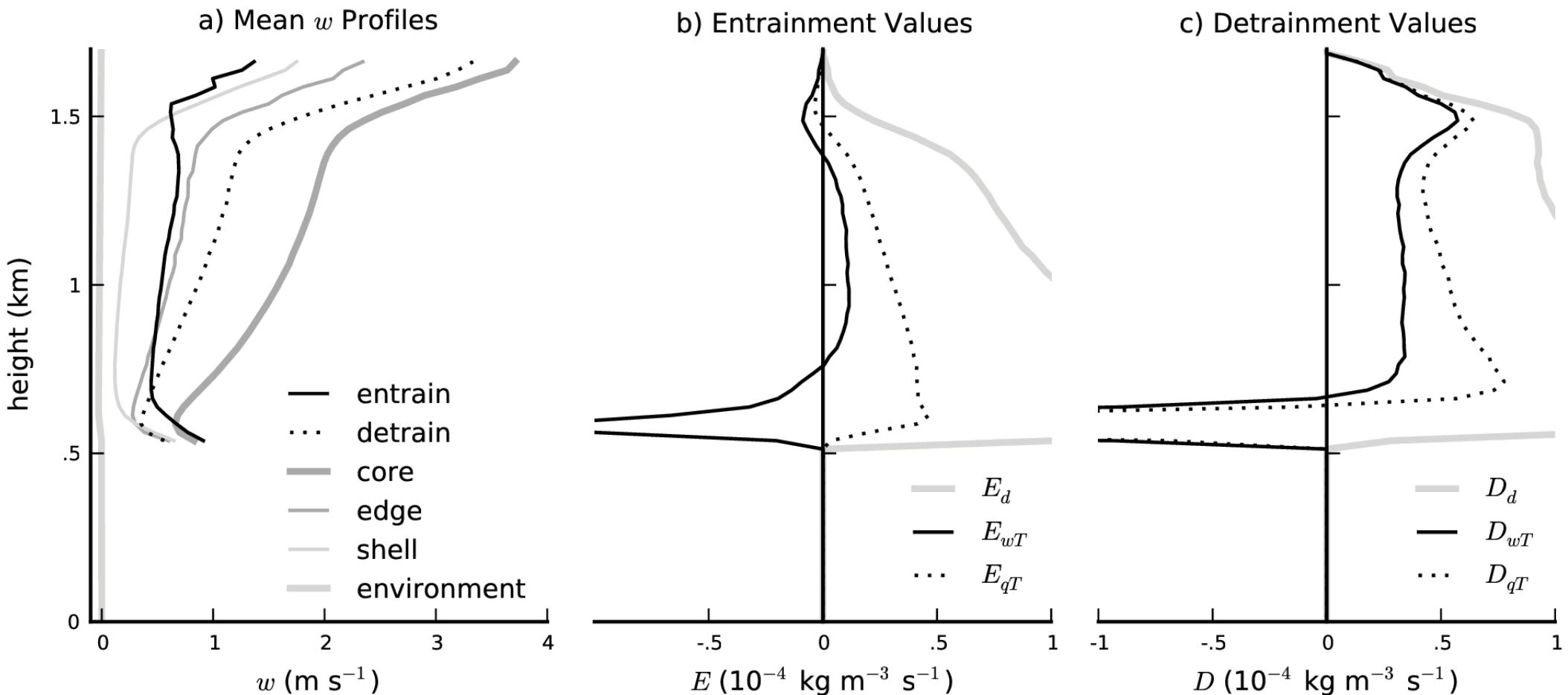
# Tetrahedral interpolation and the direct entrainment calculation



Dawe and Austin, MWR 2011

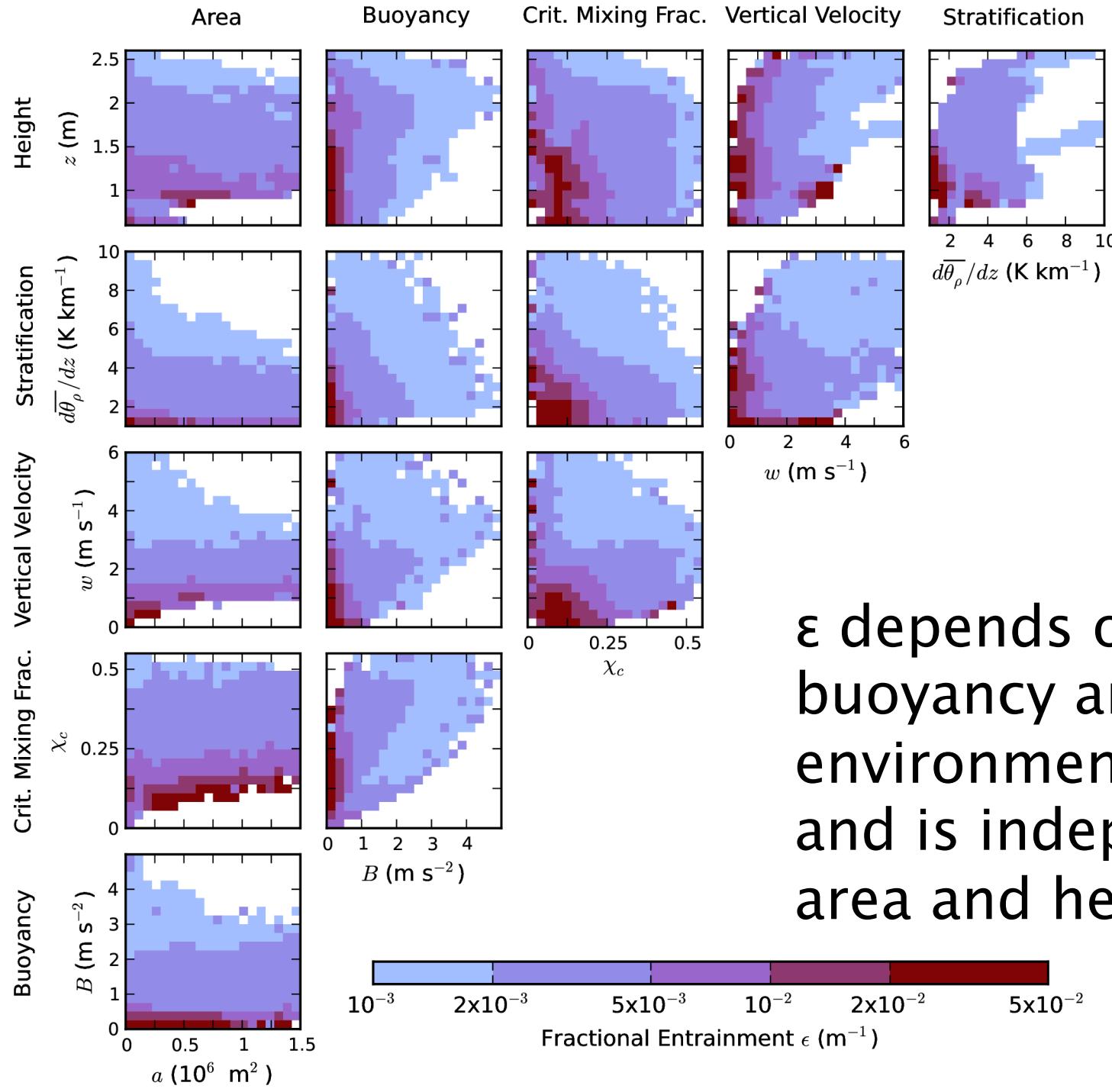


# Direct vs. bulk thermodynamic entrainment

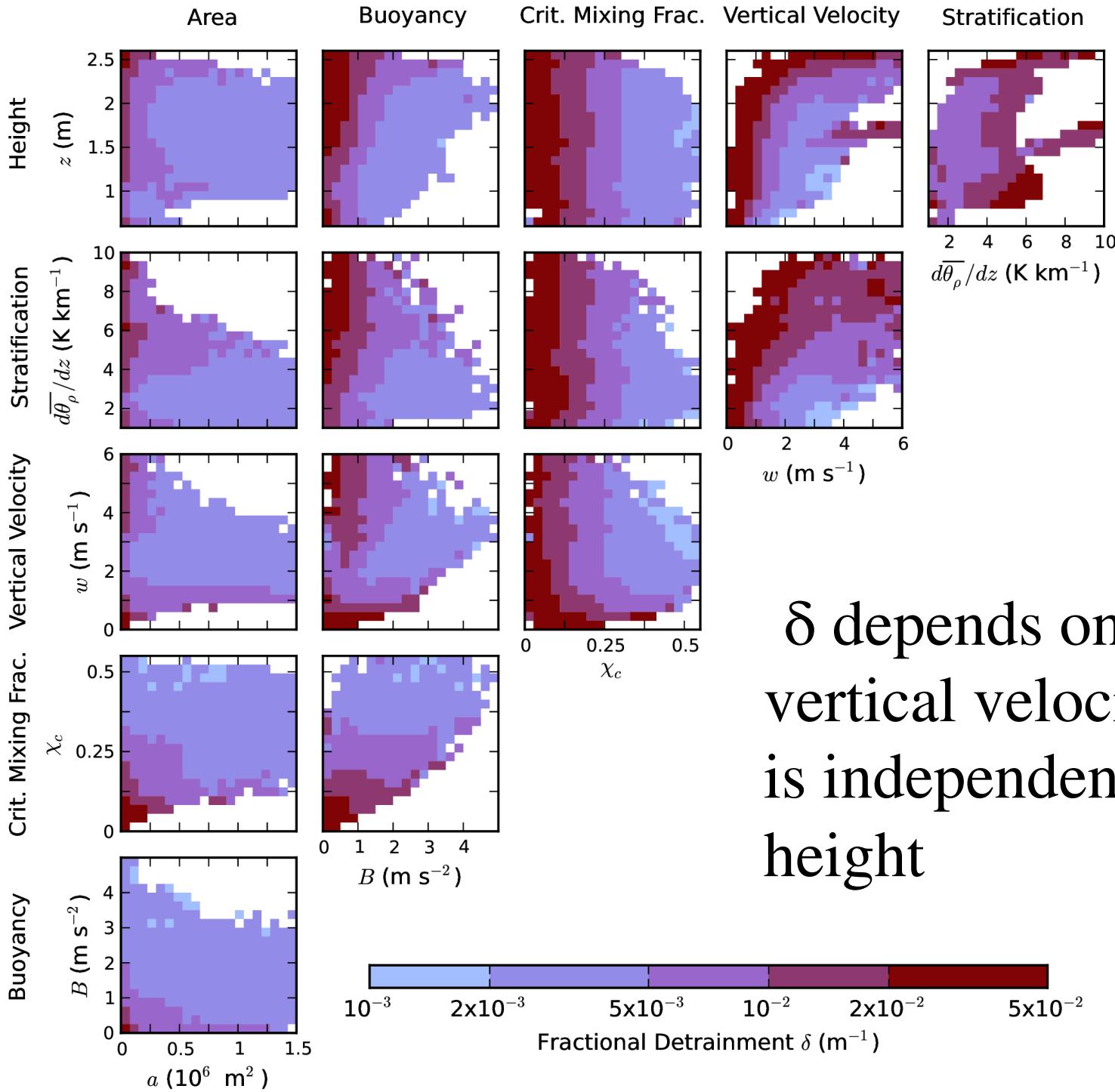


Dawe and Austin, JAS, 2011

Direct entrainment rates more than twice those calculated by budget calculations that assume mixing between mean cloud and environment (and note difference between tracer and momentum entrainment rates)



$\epsilon$  depends on  
buoyancy and local  
environmental stability  
and is independent of  
area and height



$\delta$  depends on mean vertical velocity and  $\chi_c$  and is independent of area and height

Quantify this with the mutual information,  $I(X;Y)$

$$I(X) = \ln\left(\frac{1}{P(x)}\right) = -\ln(P(x)) \quad \text{Self information}$$

$$H = -\int P(x)\ln(P(x))dx \quad \text{Entropy}$$

$$I(X;Y) = H(X) - H(X|Y) \quad \text{Mutual information}$$

$$I(X;Y) = \int P(x,y)\ln\left(\frac{P(x,y)}{P(x)P(y)}\right)dxdy$$

# Mutual information

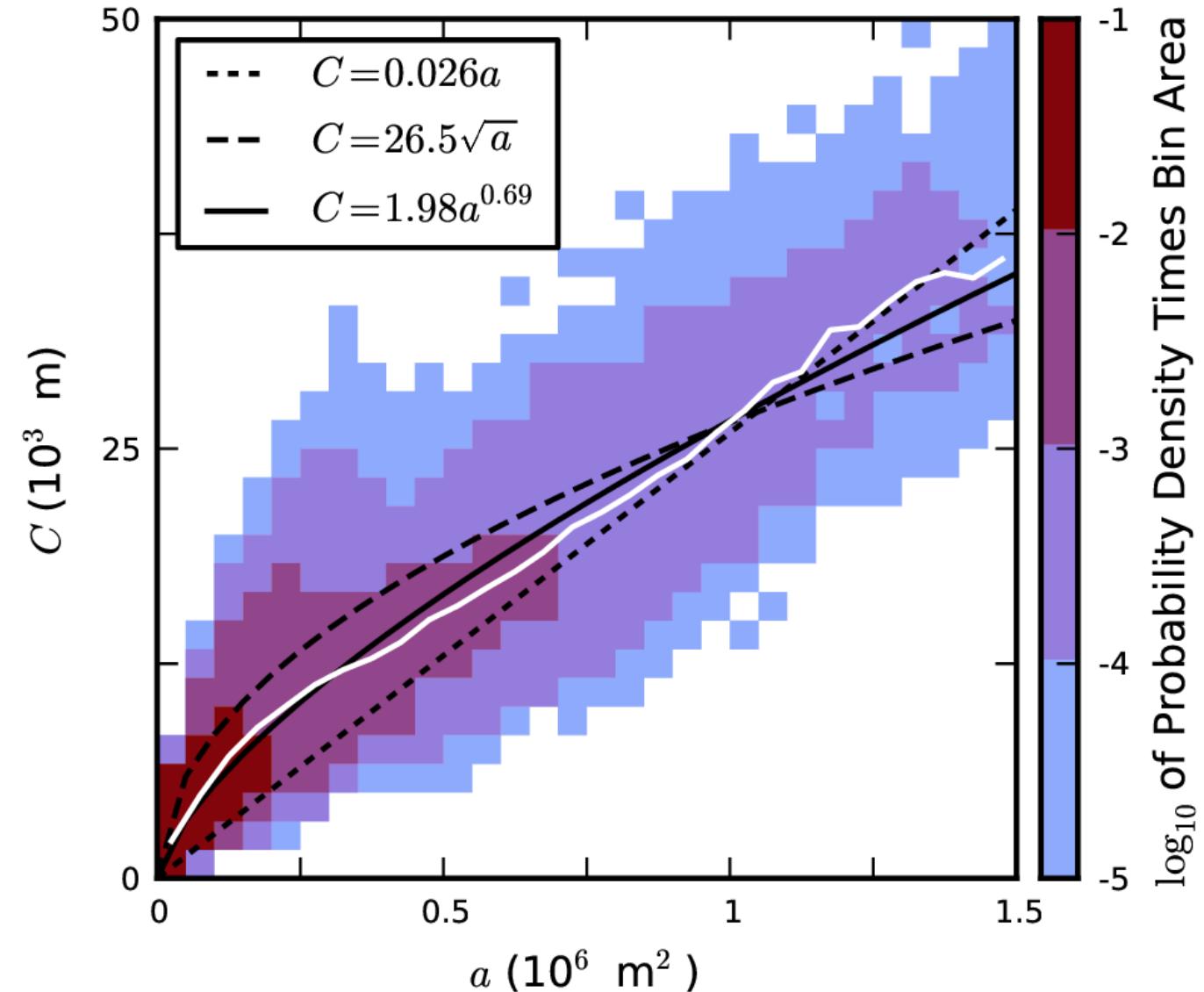
Entrainment

Variable	MI	Noise
$I(\log_{10} \epsilon; z)$	0.104	0.002
$I(\log_{10} \epsilon; w)$	0.214	
$I(\log_{10} \epsilon; a)$	0.036	
$I(\log_{10} \epsilon; B)$	0.419	
$I(\log_{10} \epsilon; \chi_c)$	0.259	
$I(\log_{10} \epsilon; d\bar{\theta}_\rho/dz)$	0.130	
$I(\log_{10} \epsilon; z B)$	0.07	0.01
$I(\log_{10} \epsilon; w B)$	0.06	
$I(\log_{10} \epsilon; a B)$	0.03	
$I(\log_{10} \epsilon; \chi_c B)$	0.07	
$I(\log_{10} \epsilon; d\bar{\theta}_\rho/dz B)$	0.13	
$I(\log_{10} \epsilon; z B, d\bar{\theta}_\rho/dz)$	0.12	0.10
$I(\log_{10} \epsilon; w B, d\bar{\theta}_\rho/dz)$	0.08	0.07
$I(\log_{10} \epsilon; a B, d\bar{\theta}_\rho/dz)$	0.09	0.07
$I(\log_{10} \epsilon; \chi_c B, d\bar{\theta}_\rho/dz)$	0.11	0.09

Detrainment

Variable	MI	Noise
$I(\log_{10} \delta; z)$	0.027	0.002
$I(\log_{10} \delta; w)$	0.216	
$I(\log_{10} \delta; a)$	0.152	
$I(\log_{10} \delta; B)$	0.184	
$I(\log_{10} \delta; \chi_c)$	0.353	
$I(\log_{10} \delta; d\bar{\theta}_\rho/dz)$	0.054	
$I(\log_{10} \delta; z \chi_c)$	0.04	0.02
$I(\log_{10} \delta; w \chi_c)$	0.17	
$I(\log_{10} \delta; a \chi_c)$	0.08	
$I(\log_{10} \delta; B \chi_c)$	0.03	
$I(\log_{10} \delta; d\bar{\theta}_\rho/dz \chi_c)$	0.04	
$I(\log_{10} \delta; z \chi_c, w)$	0.27	0.13
$I(\log_{10} \delta; a \chi_c, w)$	0.11	0.09
$I(\log_{10} \delta; B \chi_c, w)$	0.12	0.08
$I(\log_{10} \delta; d\bar{\theta}_\rho/dz \chi_c, w)$	0.17	0.09

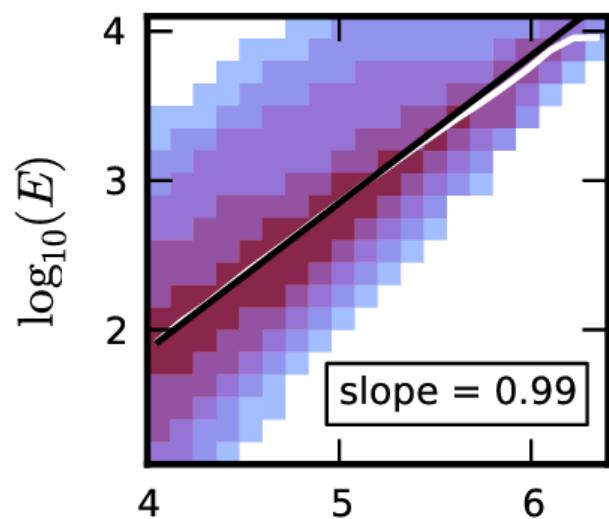
## Cloud Circumference vs Area



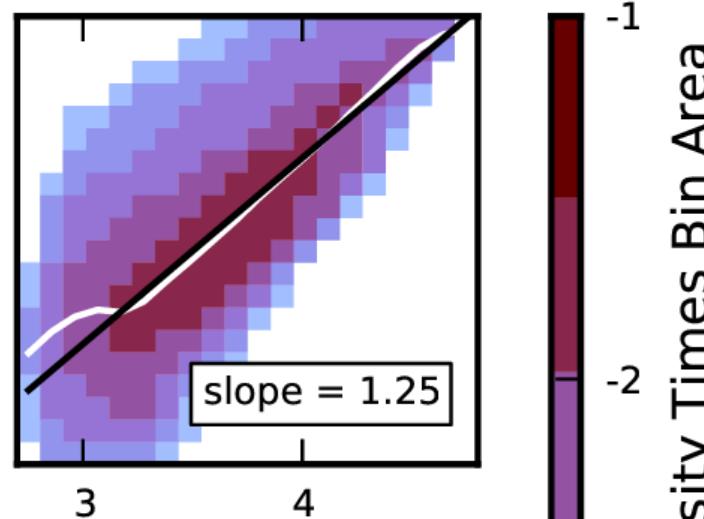
Best fit  
functional  
relationships

Clouds are not cylinders, but Circumference and Area have a scaling relationship:  $C \sim a^{0.7}$

a)  $E$  vs Area

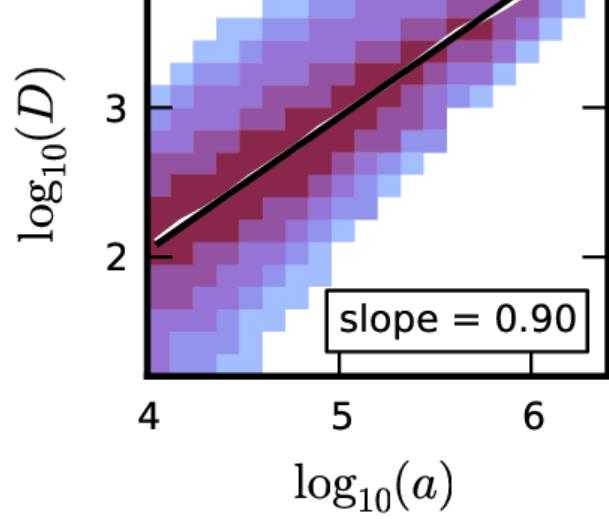


b)  $E$  vs Circumference

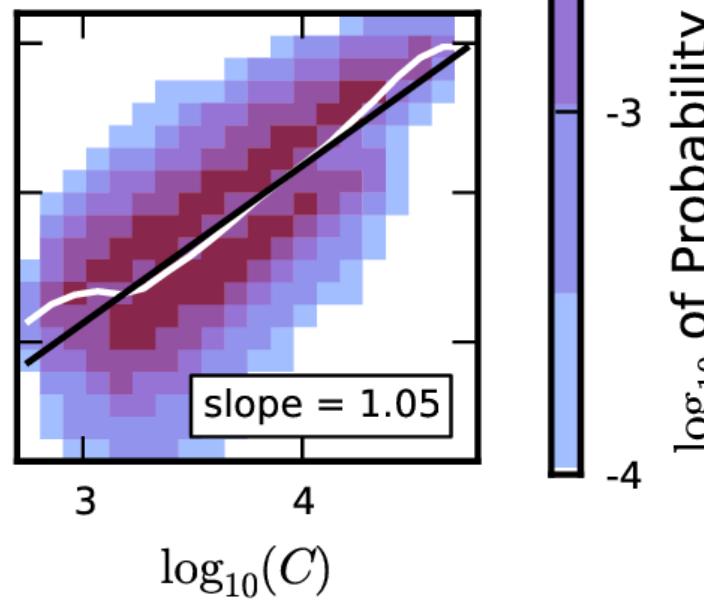


Dimensional  
entrainment  $E$   
and  
detrainment  $D$

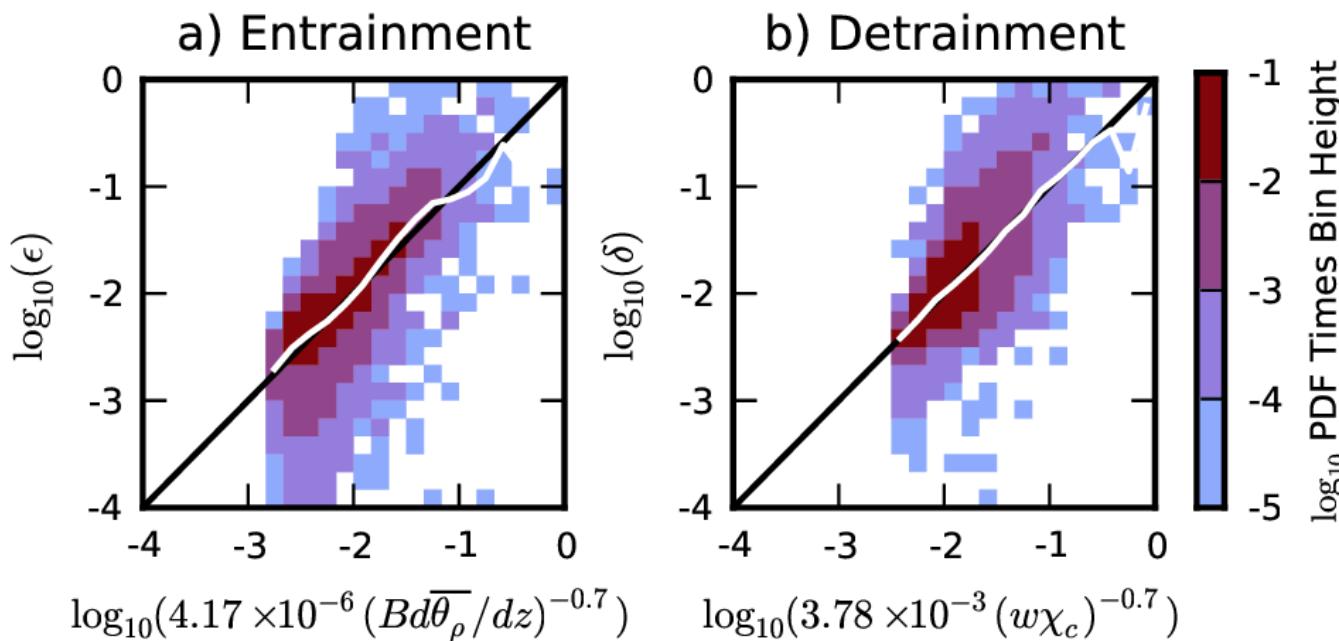
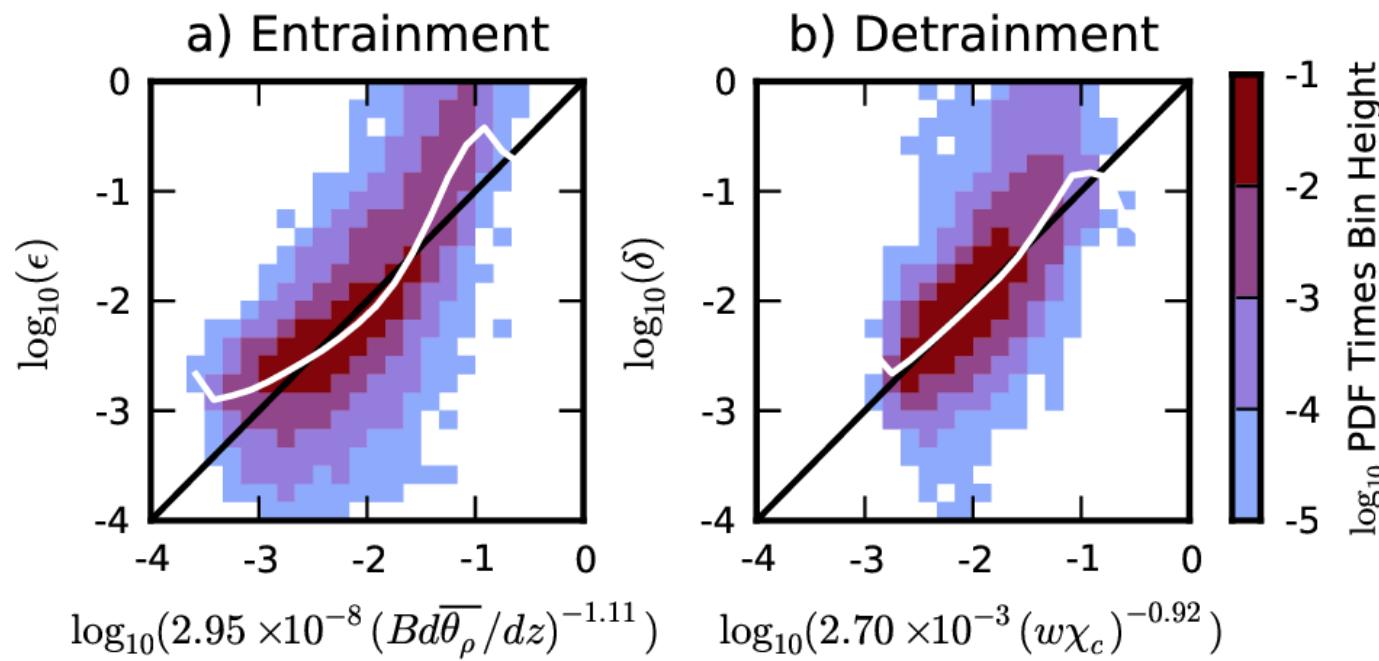
c)  $D$  vs Area



d)  $D$  vs Circumference



$E \sim \text{Area}$  while  $D \sim \text{Circumference}$



Fit to individual values of  $\epsilon, \delta$

$$\epsilon \propto (Bd\theta / dz)^{-1.11}$$

$$\delta \propto (w\chi_c)^{-0.92}$$

Fit to ensemble average  $\epsilon, \delta$

$$\epsilon \propto (Bd\theta / dz)^{-0.7}$$

$$\delta \propto (w\chi_c)^{-0.7}$$

# To Summarize:

$$\epsilon \propto (B d\theta / dz)^{-0.7} \quad \delta \propto (w \chi_c)^{-0.7} \quad \text{LES}$$

$$\epsilon = \frac{\alpha B}{w^2} - \frac{1}{w} \frac{\partial w}{\partial z}$$

$$\epsilon = \frac{\eta}{\tau_p} \frac{1}{w_p} \quad \epsilon = \epsilon_0 \chi_c^2$$

$$\epsilon = \epsilon_0$$

$$\epsilon = c_e z^{-1}$$

$$\delta = \epsilon_0 (1 - \chi_c)^2$$

Tropical simulations with the UBC SAM model (radiative-convective equilibrium and weak  
~~Non-perturbative general circulation model simulation~~ GASS-WTG SCM/CRM  
intercomparison

## Cloud Entrainment vs Area

Entrainment is often parameterized by:

$$E = k \frac{M}{R} = k \frac{\rho a w}{R}$$

The rationale for this is simple.

$$C = 2\pi R = 2 \frac{a}{R} \quad v_E = v_o w \quad E = \rho C v_E = 2v_o \frac{\rho a w}{R}$$

However, we find  $E = k\rho a$ . This implies  $\rho C v_E = k\rho a$

There are two possibilities:

1. If the cloud is a cylinder, then

$$v_E = kR/2$$

2. If the cloud is not a cylinder, then

$$C = \frac{ka}{v_o w}$$