Duality

 $\frac{\text{Electric}}{\vec{\nabla} \times \vec{H}} = \vec{\gamma} \vec{E} + \vec{J}$

 $-\nabla x \vec{E} = 2 \vec{H}$

 $H = \nabla \times \vec{A}$

E = -2A + + → 7(7.A)

 $\nabla^2 \vec{A} - \hat{\vec{y}} \hat{\vec{z}} \vec{A} = -\vec{\vec{J}}$

Magnetic -VXE=ZH+M

VXH = ŷE

 $\vec{E} = -\nabla x \vec{F}$

H = -ŷF+ + \$ (3.F)

V-F- 92 F = - H

A(F)= SSJG() eiklift du FG)=SSJMG()=cklift) du

What is a magnetic convent! (Again)

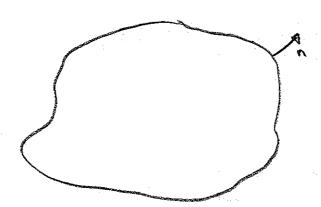
One can show using equations above that fields from the below sources are equal

7I

KL = 2 ISA bund of Ilm

Unqueness

Consider a surface



Now consider two solutions

Define the difference solution

From Power Percuetions

Let us force $J\vec{E} = 0$ & $J\vec{H} = 0$ on S

:. G(JEXJH*). ds = 0

So SSS(Re(2) | SH12 + Re(3) | SE12) du=0 8 SSS(Im(2) | SH21 - Im(3) | SE12) du=0

For a dessa pative medium $Re(\frac{1}{2}) > 0$ $Re(\frac{5}{2}) > 0$

8H=0 & SE=0 N S

Summary: If we specify the fields on S

There is only one unique solution

IN S

Actually its even more restrictive.

There is a unique solution \underline{W} S

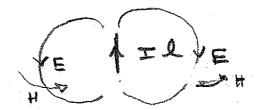
If \underline{I} $n \times \delta \vec{E} = 0$ on S

or 2) $n \times \delta \vec{H} = 0$ on S

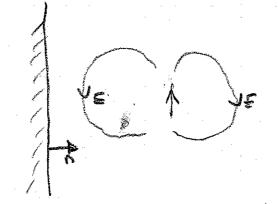
or 3) NOJE=0 on part of S & NOJHO other S.

Image Theory

Consider a short electric dipole



Put the dipole next to the ground plane



We must have $\vec{n} \times \vec{E} = 0$ on the ground plans

Frée Sprce

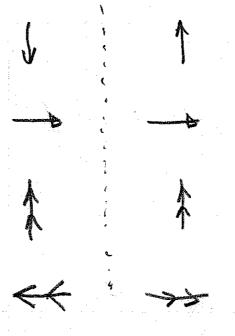
7

Satisfies this requirement & Fron Uniqueness Theorem is the only solution

Like Wise

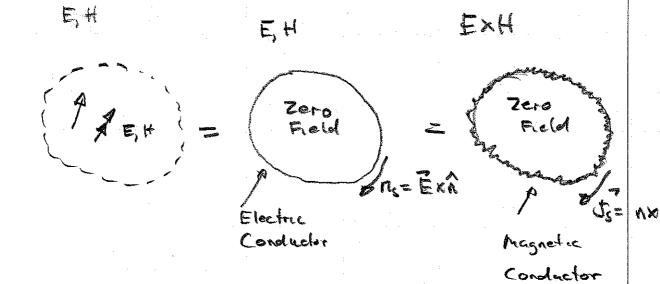
↑Il →Il ↑Ve >>ve

Is the same as

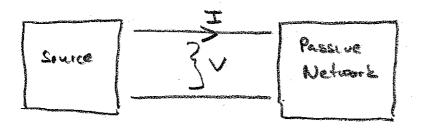


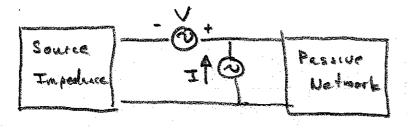
Equivalence Principle E, H Zero field Ms = Exn

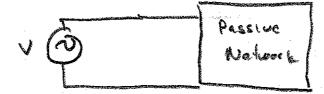
Since the field is zero inside S we can put any surface we want



Equipolence Principle in Circuit Theory

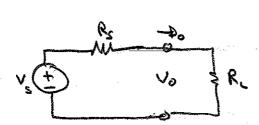






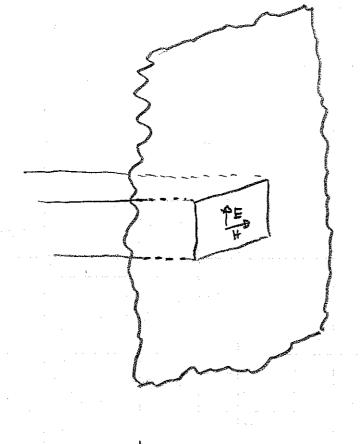
It (2) Passive Naturals

Check



t rs=lean

Frelds in a Half Space



$$\vec{F}(\vec{r}) = \iint 2\vec{E}(r') \times \hat{n} \frac{e^{jk/r-r'l}}{|\vec{r}-\vec{r}'|} d$$

Note that this is an Integral Equation

 $E = \nabla x F(r)$

E(r)= \text{\$\frac{1}{r-r'}\$} ds'

How does one solve integral equations

How does one solve integral equations

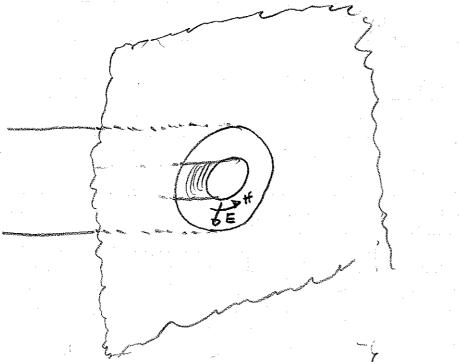
How does one solve integral equations

E(r') on the surface

usually 2) a) Guess at E(r') on surface

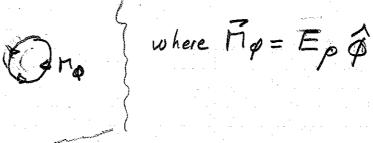
- b) come up with error term and use an appoximation for solving error term et.
- 3) On the surface, expand E(r) in terms of basis functions. Then multiply integral equation by basis functions (Galerkin approach) & integrate. The integral equation becomes a matrix equation. This is the basis for moment methods.

Coaxial line opening into a half space



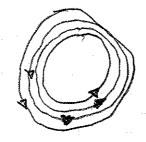
Note that the current at the end of an open coax is zero.

Assume that the voltage at the end



We can use method of images

Bince the E field is spead out over the radius 8 if b << >



Magnetic $\Delta KS = (\pi \rho^2) 2 E_p(\rho) \Delta \rho$ Coursent Loop $\langle KS \rangle = \int_a^b \pi \rho^2 2 E_p(\rho) d\rho$ $= \pi V \frac{(b^2 - a^2)}{\ln(b la)}$

Remember

$$Kl = 2IS \hat{\lambda}$$

$$2 = j\omega u$$

The Pual is also correct

$$II = ywe KS \hat{n}$$

$$II = y KS \hat{n}$$

$$unds of L$$

$$unds of L$$

$$unds of A$$

$$\overrightarrow{Il} \cong \left(\frac{V(b^2 - a^2)}{\ln(b \ln a)} \right)$$

$$\vec{A} = \sqrt[3]{\frac{V(b^2-a^2)}{\ln(b/a)}} \vec{Z} \frac{-uk|r|r}{\ln(b/a)}$$

$$A = \sqrt{2} \times A$$

$$\vec{E} = -\vec{2}\vec{A} + \vec{\gamma}\vec{\nabla}(\vec{\gamma}\cdot\vec{A})$$

Induction Theorem

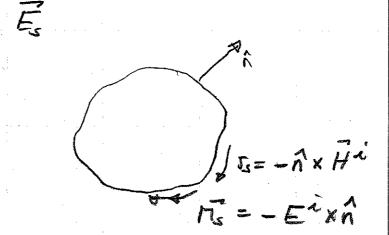
E E 1, ES

1 & Source

()



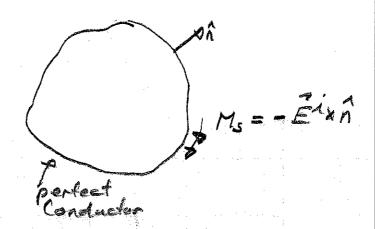
If we do not need to know the field inside the obstacle



What if the obstacle is a perfect conductor

Ēs

Js is shorted out on a perfect conductor.



Reciprocity

Consider à problems

Problem A

TA MA

Problem B

Eb, Ab

$$\nabla x H^b = \gamma E^b + J^b$$

$$-\nabla x E^b = z H^b + \Pi^b$$

Using)

Derive

Integrate over Space

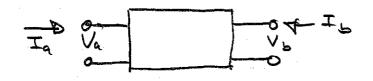
$$\mathcal{G}((E^{A} \times H^{b}) - (E^{b} \times H^{a}) \cdot dS$$

$$= (SS(E^{a} \cdot J^{b} - H^{a} \cdot \Pi^{b}) dV - SS(E^{b} \cdot J^{a} - H^{b} \cdot \Pi^{a}) dV$$

Bring the surface out to infinity $G((E^{A_{X}}H^{b})-(E^{b_{X}}H^{a}))-dS = 0$ because fields die away.

What does this mean?

Consider
$$J^6 = J^6 S(x-x_6)S(y-y_6')$$
 $M^6 = 0$
 $J^9 = J^9 S(x-x_4')S(y-y_4')$ $M^9 = 0$



$$\begin{bmatrix} V_{A} \\ V_{b} \end{bmatrix} = \begin{bmatrix} Z_{AA} & Z_{AB} \\ Z_{BA} & Z_{BB} \end{bmatrix} \begin{bmatrix} I_{q} \\ I_{b} \end{bmatrix}$$

Reciprocity means that

OR: The transmitting pattern is the same as the recioung pattern!

Physical Optics Approximation

Consider a region that is mostly emply but has an obstagle



The maderial properties of the region is a function of position

$$\hat{\mathcal{L}} = \hat{\mathcal{L}}(\vec{r}, \omega) \quad \hat{\mathcal{L}} = \mathcal{L}(\vec{r}, \omega)$$

Outside 5 the material properties are constant

constant
$$\hat{Z} = \hat{Z}_o(\omega)$$
 $\hat{y} = y_o(\omega)$

We can re-write the problem as $-\nabla \times \vec{E} = \hat{z}_o \vec{H} + (\hat{z}_T - \hat{z}_o) \vec{H} + \vec{M}^i$ $-\nabla \times \vec{H} = \hat{y}_o \vec{E} + (\hat{y}_T - \hat{y}_o) \vec{E} + \vec{J}^i$

Decompose the total field into incident and seatlered fields

$$-\nabla \times (\vec{E}_{1} + \vec{E}_{5}) = \hat{2}_{3}(\vec{H}_{1} + \vec{H}_{5}) + (\hat{2}_{7} - \hat{2}_{3})(\vec{H}_{1} + \vec{H}_{5}) + \vec{H}_{1}$$

$$\vec{\nabla} \times (\vec{H}_{1} + \vec{H}_{5}) = \gamma_{3}(\vec{E}_{1} + \vec{E}_{5}) + (\gamma_{7} - \gamma_{3})(\vec{E}_{1} + \vec{E}_{5}) + \vec{J}_{1}$$

Incident problem

 (\cdot)

$$-\nabla \times \vec{E}^{i} = 2\vec{H}^{i} + \vec{H}^{i}$$

$$-\nabla \times \vec{H}^{i} = \vec{y}_{o} \vec{E}^{s} + \vec{J}^{i}$$

Scattered problem

$$-\vec{\nabla} \times \vec{E}^{s} = 2 \cdot \vec{E}^{s} + \vec{\Pi}^{s}$$

$$\vec{\nabla} \times \vec{H}^{s} = \sqrt{2} \cdot \vec{E}^{s} + \vec{J}^{s}$$

$$\vec{H}^{S} = (\hat{Z}_{7} - \hat{Z}_{0}) H^{T} = J \omega (u_{7} - u_{0}) H^{T}$$

$$\vec{f}^{S} = (\hat{Y}_{7} - \hat{Y}_{0}) E^{T} = J \omega (\epsilon_{7} - \epsilon_{0}) E^{T} + O_{7} E^{T}$$

Assume a non-magnetic metal object since $\mathcal{U}_{\tau} = \mathcal{U}_{0}$ $\mathcal{H}^{s} = \mathcal{O}$ $\mathcal{F}^{s} = \mathcal{O}$ $\mathcal{E}_{\tau} = \mathcal{E}_{0}$ $\mathcal{J}^{s} = \sigma_{\tau} \mathcal{E}^{\tau}$

As= 47 SSS OF ET e-iklF-F" du'
Volume

as of \$00 of Et becomes a true surface current

 $\overline{A_s} = \frac{1}{4\pi} \iint_{Surface} J_{surface}(E^T) \frac{e^{-\iota k |\vec{r} - \vec{r}'|}}{|\vec{r} - \vec{r}'|} ds$

The surface current on a conductor is given by

Jourpace = Ax Hourface

Physical Optics Approx

- 1) Assume object large
- 2) Field negligible in shedow vegion
- 3) Surface of object "smooth"

FritEs

Frident
Wave

S' P

Using image theory we can assume

Junque 2 2 NX Hi on s'

As = 47 SS 2 n'x Hi(F') = -2 t [F-F'] ds'