Dynamics and Parameters of Arducopter

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1 Dynamics

We define the position and velocity of the quadcopter in the intertial frame as $x = (x, y, z)^T$ and $\dot{x} = (\dot{x}, \dot{y}, \dot{z})^T$. Similarly, we define the roll, pitch, and yaw angles in the body frame as $\theta = (\phi, \theta, \psi)^T$, and the corresponding angular velocities equal to $\dot{\theta} = (\dot{\phi}, \dot{\theta}, \dot{\psi})^T$. We can convert these angular velocities into the angular velocity vector using the relation:

$$\omega = \begin{bmatrix} 1 & 0 & -s_{\theta} \\ 0 & c_{\theta} & c_{\theta}s_{\phi} \\ 0 & -s_{\theta} & c_{\theta}c_{\phi} \end{bmatrix} \dot{\theta}$$
 (1)

We can relate the body and inertial frame by a rotation matrix R which goes from the body frame to the inertial frame. This matrix is derived by using the ZYZ Euler angle conventions and successively undoing the yaw, pitch and roll.

$$R = \begin{bmatrix} c_{\theta}c_{\psi} - c_{\theta}s_{\phi}s_{\psi} & -c_{\psi}s_{\phi} - c_{\phi}c_{\theta}s_{\psi} & s_{\theta}s_{\psi} \\ c_{\theta}c_{\psi}s_{\phi} + c_{\phi}s_{\psi} & c_{\phi}c_{\theta}c_{\psi} - s_{\phi}s_{\psi} & -c_{\psi}s_{\theta} \\ s_{\phi}s_{\theta} & c_{\phi}s_{\theta} & c_{\theta} \end{bmatrix}$$
(2)

For a given vector \vec{v} in the body frame, the corresponding vector is given by $R\vec{v}$ in the inertial frame.

Let ω_i represent the angular velocity of the *i*th propeller. The thrust generated by each of the propellers (in the body frame) can be written as:

$$T_B = \sum_{i=1}^4 T_i = k \begin{bmatrix} 0\\0\\\sum \omega_i^2 \end{bmatrix}$$
 (3)

where k is some appropriately dimensioned constant.

1.1 Linear motion

The global drag force on the quadcopter can be modeled as a force proportional to the linear velocity in each direction:

$$F_D = \begin{bmatrix} -k_d \dot{x} \\ -k_d \dot{y} \\ -k_d \dot{z} \end{bmatrix} \tag{4}$$

In the inertial frame, the acceleration of the quadcopter is due to thrust, gravity and linear friction. Thus, the equations of motion of the quadcopter for linear motion are given as:

$$m\ddot{\vec{x}} = \begin{bmatrix} 0\\0\\-mg \end{bmatrix} + RT_B + F_D \tag{5}$$

where \vec{x} is the position of the quadcopter, g is the acceleration due to gravity, F_D is the drag force, and T_B is the thrust vector in the body frame. The equations can be simplified as:

$$\begin{bmatrix} \ddot{x} \\ \ddot{y} \\ \ddot{z} \end{bmatrix} = \frac{1}{m} \begin{bmatrix} s_{\psi} s_{\theta} k \sum \omega_i^2 - k_d \dot{x} \\ -c_{\psi} s_{\theta} k \sum \omega_i^2 - k_d \dot{y} \\ c_{\theta} k \sum \omega_i^2 - k_d \dot{z} - mg \end{bmatrix}$$
 (6)

1.2 Rotational Motion

Let the propellers i=1 and i=3 be on the roll axis, spinning clockwise, and i=2 and i=4 be on the pitch axis, spinning anticlockwise. Then the contribution of torque on the quadcopter from the *i*th propeller, about the Z axis (yaw axis) in steady state flight ($\dot{\omega} \approx 0$) is given by:

$$\tau_z = (-1)^{i+1} b w_i^2 \tag{7}$$

where b is some appropriately dimensioned constant. The torque on the quadcopter in the body frame is then given by:

$$\tau_{B} = \begin{bmatrix} \tau_{\phi} \\ \tau_{\theta} \\ \tau_{\psi} \end{bmatrix} = \begin{bmatrix} Lk(\omega_{1}^{2} - \omega_{3}^{2}) \\ Lk(\omega_{2}^{2} - \omega_{4}^{2}) \\ b(\omega_{1}^{2} - \omega_{2}^{2} + \omega_{3}^{2} - \omega_{4}^{2}) \end{bmatrix}$$
(8)

where L is the distance from the center of the quadcopter to any of the propellers.

The rotational equations of motion can be derived using Euler's equations for rigid body dynamics. Expressed in vector form, Euler's equations are written as:

$$I\dot{\omega} + \omega \times (I\omega) = \tau \tag{9}$$

where ω is the angular velocity vector, I is the inertia matrix, and τ is a vector of external torques. Assuming that $I = diag(I_{xx}, I_{yy}, I_{zz})$, the body frame rotational equations of motion are given as:

$$\begin{cases}
I_{xx}\ddot{\phi} = \omega_y \omega_z (I_{yy} - I_{zz}) + \tau_x \\
I_{yy}\ddot{\theta} = \omega_x \omega_z (I_{zz} - I_{xx}) + \tau_y \\
I_{zz}\ddot{\psi} = \omega_x \omega_y (I_{xx} - I_{yy}) + \tau_z
\end{cases}$$
(10)

Let $x_1 = [x, y, z]^T$, $x_2 = [\dot{x}, \dot{y}, \dot{z}]^T$, $x_3 = [\phi, \theta, \psi]^T$, and $x_4 = [\omega_x, \omega_y, \omega_z]^T$. Thus, we can write the state space equations for the evolution of our state as:

$$\begin{aligned}
\dot{x}_{1} &= x_{2} \\
\dot{x}_{2} &= \frac{1}{m} \begin{bmatrix} s_{\psi} s_{\theta} k \sum \omega_{i}^{2} \\ -c_{\psi} s_{\theta} k \sum \omega_{i}^{2} - mg \end{bmatrix} - k_{d} x_{2} \\
\dot{c}_{\theta} k \sum \omega_{i}^{2} - mg \end{bmatrix} \\
\dot{x}_{3} &= \begin{bmatrix} 1 & \frac{s_{\phi} s_{\theta}}{c_{\theta}} & \frac{c_{\phi} s_{\theta}}{c_{\theta}} \\ 0 & c_{\phi} & -s_{\phi} \\ 0 & \frac{s_{\phi}}{c_{\theta}} & \frac{c_{\phi}}{c_{\theta}} \end{bmatrix} x_{4} \\
\dot{c}_{1} &= \frac{c_{\phi} - (I_{yy} - I_{zz})(\omega_{y} \omega_{z})}{I_{xx}} \\
\dot{c}_{2} &= \frac{c_{\phi} - (I_{zz} - I_{xx})(\omega_{x} \omega_{z})}{I_{yy}} \\
\dot{c}_{3} &= \frac{c_{\phi} - (I_{zz} - I_{xx})(\omega_{x} \omega_{z})}{I_{xx}} \\
\dot{c}_{4} &= \frac{c_{\phi} - (I_{zz} - I_{yy})(\omega_{x} \omega_{y})}{I_{yy}} \\
\dot{c}_{4} &= \frac{c_{\phi} - (I_{xx} - I_{yy})(\omega_{x} \omega_{y})}{I_{xy}} \\
\dot{c}_{4} &= \frac{c_{\phi} - (I_{xx} - I_{yy})(\omega_{x} \omega_{y})}{I_{xy}} \\
\dot{c}_{4} &= \frac{c_{\phi} - (I_{xx} - I_{yy})(\omega_{x} \omega_{y})}{I_{xy}} \\
\dot{c}_{5} &= \frac{c_{\phi} - c_{\phi}}{c_{\phi}} \\
\dot{c}_{7} &= \frac{$$

2 Parameters

2.1 Copter Dynamics Parameters

The necessary parameters for the dynamic modeling of the quadcopter are included in both the linear motion equation and the rotational equation of motion.

2.1.1 Linear Motion

In the linear motion equations (3), (4) and (5), the following parameters must be measured directly or indirectly:

m - mass of the quadcopter = 1.32 kg k - relation between the RPM of the rotor and the thrust k_d - friction coefficient

2.1.2 Rotational Motion

In the rotational motion equations, described by (8) and (10), the parameters to be measured are

 I_{xx} - moment of inertia in X direction = 0.014 $kg\ m^2$ I_{yy} - moment of inertia in Y direction = 0.014 $kg\ m^2$

 I_{zz} - moment of inertia in Z direction = 0.037 kg m^2

L - Distance between the center of the quadcopter to any of the propellers = 0.275 m

b - Propeller drag coefficient

2.2 Motor Dynamics Parameters

The relation between the angular velocity and input voltage could be linearized as:

$$\dot{\omega}_m = -A\omega_m + Bu + C \tag{12}$$

where u is the input voltage. Here, the parameters to be determined are A, B, and C.

2.3 Experiments to determine the parameters

The mass of the quadcopter was measured using a spring scale as m = 1.32kg. The distance between opposite rotors is 55 cm, and the XY coordinate of the center of mass is assumed to lie at the midpoint of opposite rotors, i.e. at a distance of 27.5 cm from any rotor.

2.3.1 Moment of Inertia about yaw axis

To calculate the moment of inertia about yaw axis, a bifilar pendulum was used. The quadcopter was suspended in a horizontal position by vertical strings attached to its left and right arms, and given a small angular displacement about the yaw axis. The quadcopter performs oscillations, and the moment of inertia can be measured using the equation:

$$I_{zz} = \frac{mgT^2d^2}{4\pi^2l}$$
 (13)

where T is the time period of oscillations, and 2d is distance between the two strings, and l is the length of the strings. We measured T=3.25s, l=264cm, and d=17cm which results in a moment of inertia of

$$I_{zz} = 0.037 kgm^2 (14)$$

2.3.2 Moment of inertia about pitch and roll axes

To find the moment of inertia about pitch and roll axes, first, the Z coordinate of the center of mass needed to be measured. For this, the quadcopter was suspended using one string attached to one of its arm, and this was repeated for all four arms. By measuring the angle that the quadcopter made with the vertical for all the four cases using the IMU, we were able to calculate the Z coordinate of the center of mass. For all four arms, the quadcopter was suspended using symmetric points (edge hole of the lower part of arm) and the angles made with vertical were calculated as:

Left arm = 6.7° Front arm = 4.6° Right arm = 7.9° Back arm = 6.4°

Using trigonometry, and assuming that the XY coordinate of center of mass lies at the midpoint of rotors, the height of the center of mass was calculated as the average of height given by all four arms (with respect to the lower edge of the arms): h = 3.1cm.

Now, two experiments were performed. In the first case, the quadcopter was suspended by strings attached to its left and right arms (at the same points where they were attached for calculating the center of mass), and given a small angular displacement about the roll axis. The time period of oscillation was measured. A similar experiment was performed by attaching strings on the front and back arms and measuring the time period for a pitch oscillations. Using this data, the roll and pitch moments of inertia can be calculated as:

$$I = \frac{mghT^2}{4\pi^2} - mh^2 \tag{15}$$

The time period for roll and pitch axes were calculated as $T_{roll} = 1.354s$ and $T_{pitch} = 1.345s$. Since the two axes are symmetric, the time periods were expected to be similar. Averaging the two time periods, results in T = 1.350s, which gives the moment of inertia value as:

$$I_{xx} = I_{yy} = 0.014kgm^2 (16)$$