

Homework 10 - Solution

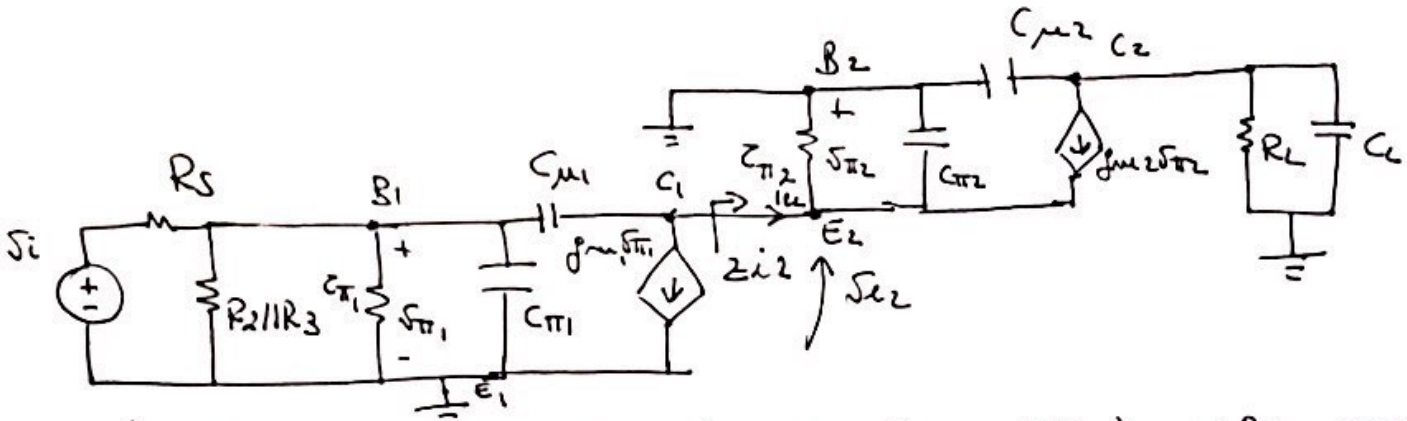
①

Assumption: $V_A = \infty$

Bandwidth = $f_H - f_L$

Determining f_H

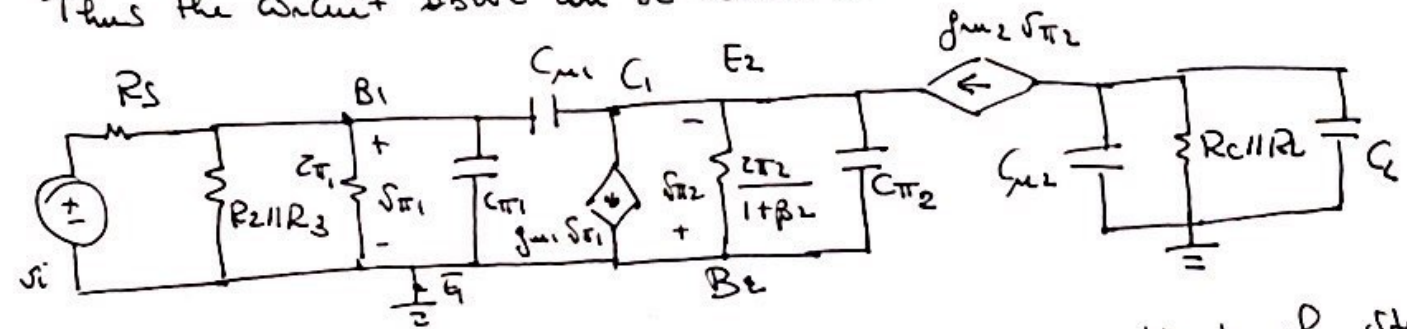
High frequency small-signal equivalent circuit



$$Z_{i2}^{-1} = \frac{i_{e2}}{v_{e2}} = \frac{1}{Z_{\pi 2}} + g_{m2} + sC_{\mu 2} = \left(\frac{1 + g_{m2}Z_{\pi 2}}{Z_{\pi 2}} + sC_{\mu 2} \right) = \frac{1 + \beta_2}{Z_{\pi 2}} + sC_{\mu 2}$$

$$Z_{i2} = \frac{Z_{\pi 2}}{\beta_2 + 1} \parallel \frac{1}{sC_{\mu 2}}$$

Thus the circuit above can be reduced to



$C_{\mu 1}$ is a capacitor between the input and the output of stage 1.

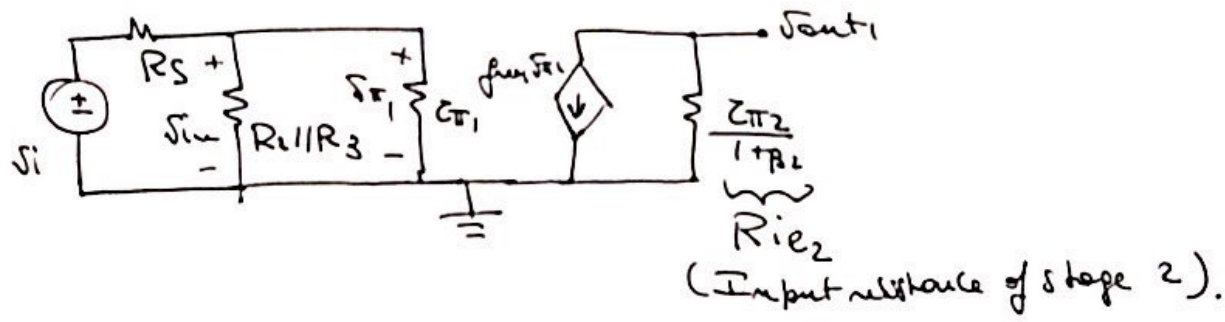
Using the Miller effect

$$C_{M1} = C_{\mu 1} [1 - A_{midband}] \quad \text{and} \quad C_{M2} = C_{\mu 1} \left[1 - \frac{1}{A_{midband}} \right]$$

As the gain of a CE stage is typically large we can take

$$C_{M2} \approx C_{\mu 1}$$

To determine C_{in} we need to calculate the amplifier voltage gain at midband. (2)

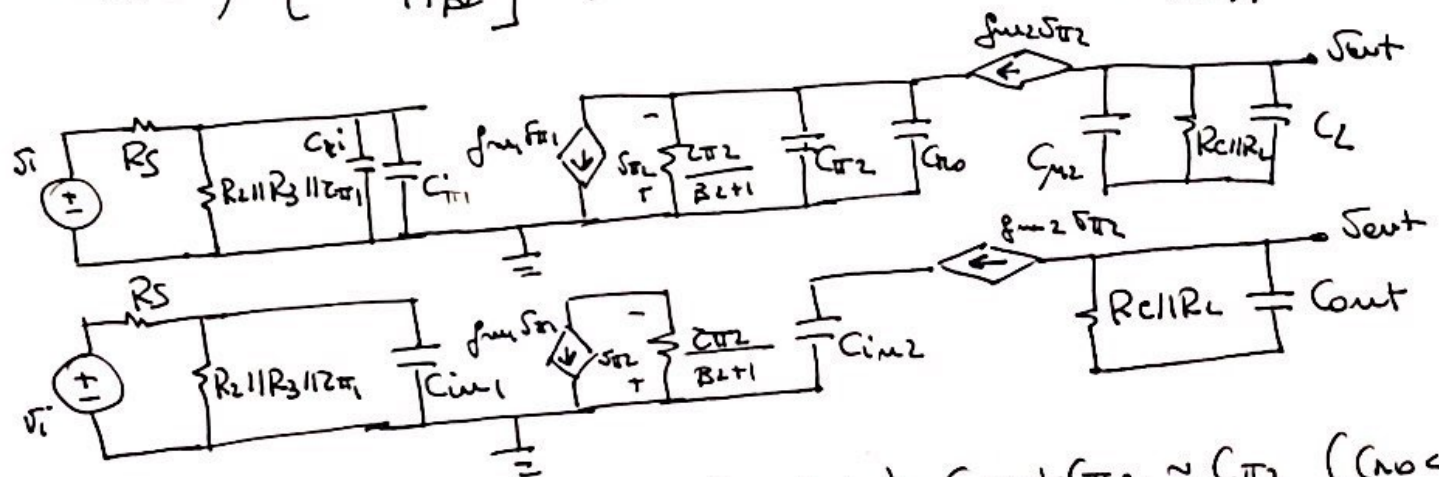


$$A_{v, \text{midband}} = \frac{v_{out1}}{v_{in1}} = -g_{m1} \frac{Z_{\pi 2}}{(1 + \beta_2)}$$

Thus

$$C_{in} = C_{\pi 1} \left[1 + \frac{g_{m1} Z_{\pi 2}}{1 + \beta_2} \right] \quad \text{Assuming } Z_{\pi 1} \approx Z_{\pi 2} \text{ (Reasonable assumption because } Q_1 \text{ and } Q_2 \text{ are biased at the same } I_{CQ}).$$

$$C_{in} \approx C_{\pi 1} \left[1 + \frac{\beta_2}{1 + \beta_2} \right] \approx C_{\pi 1} \cdot 2 = 2 C_{\pi 1}$$



$$C_{in1} = C_{\pi 1} + C_{in} \quad C_{in2} \text{ (or } C_{out1}) = C_{\pi 2} + C_{out} \approx C_{\pi 2} \quad (C_{out} \ll C_{\pi 2})$$

$$C_{out} \text{ (or } C_{out2}) = C_L + C_{\pi 2}$$

$$\tau_{in1} = C_{in1} R_{eqin1} = C_{in1} \cdot (R_S \parallel R_2 \parallel R_3 \parallel Z_{\pi 1}) = (C_{\pi 1} + C_{in}) (R_S \parallel R_2 \parallel R_3 \parallel Z_{\pi 1})$$

$$\tau_{in2} = C_{in2} R_{eqin2} \approx C_{\pi 2} \cdot \left(\frac{Z_{\pi 2}}{1 + \beta_2} \right)$$

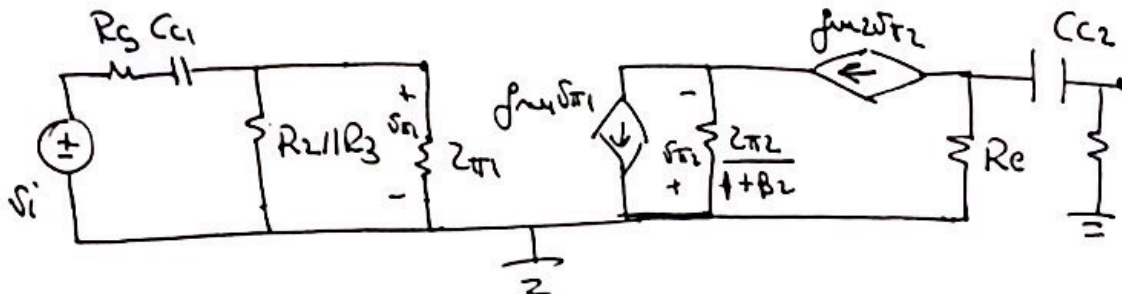
$$\tau_{out} = C_{out} R_{eqout} \approx C_L (R_C \parallel R_L)$$

For typical values of capacitors and resistors in the given circuit, the dominant time constant is τ_{out} (the largest of the 3).

Thus $f_H \approx \frac{1}{2\pi \tau_{out}} \approx \frac{1}{2\pi (C_{C1} + C_{C2})(R_{C1} \parallel R_L)}$

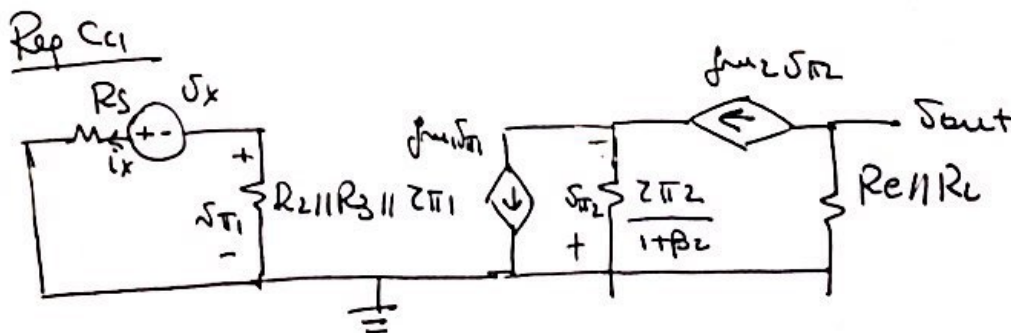
(3)

Assuming C_B and $C_E \gg C_{C1}$ and C_{C2} , we can determine f_L from the circuit below



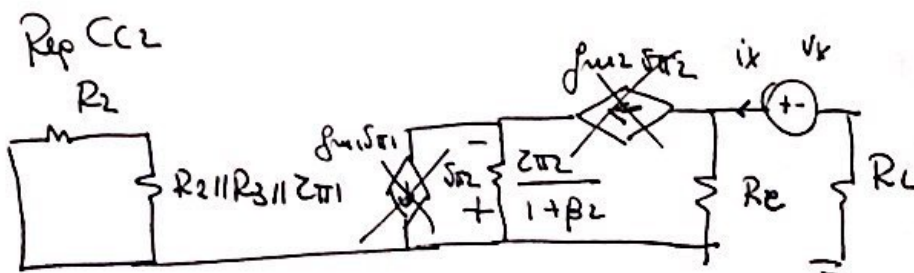
$$f_L \approx \sum_i^N \frac{1}{R_{eq_i} C_i} \quad C_i \begin{cases} C_{C2} \\ C_{C1} \end{cases} \quad N=2$$

$$f_L \approx \frac{1}{R_{eq_{C2}} C_{C2}} + \frac{1}{R_{eq_{C1}} C_{C1}}$$



$$R_{eq_{C1}} = \frac{V_x}{i_x}$$

$$R_{eq_{C1}} = R_S + R_2 \parallel R_3 \parallel Z_{\pi 1}$$



$$R_{eq_{C2}} = \frac{V_x}{i_x} = R_E \parallel R_L$$

$$V_{\pi 1} = 0 \Rightarrow g_m V_{\pi 1} = 0$$

$$V_{\pi 2} = 0 \Rightarrow g_m V_{\pi 2} = 0$$

$$f_L \approx \frac{1}{2\pi (R_S + R_2 // R_3 // Z_{\pi 1}) C_{c1}} + \frac{1}{2\pi C_{c2} (R_{e1} // R_L)} \approx$$

(4)

$$\approx \frac{1}{2\pi (R_S + Z_{\pi 1}) C_{c1}} + \frac{1}{2\pi C_{c2} (R_{e1} // R_L)}$$

Assuming $C_{c1} \approx C_{c2}$ $f_L \approx \frac{1}{2\pi (R_S + Z_{\pi 1}) C_{c1}}$ because $(R_S + Z_{\pi 1}) \ll R_{e1} // R_L$
typically

Thus

$$BW = f_H - f_L \approx \frac{1}{2\pi (C_L + C_{c2}) (R_{e1} // R_L)} - \frac{1}{2\pi (R_S + Z_{\pi 1}) C_{c1}}$$

As $f_H \gg f_L$ the $BW \approx f_H$ (Note: Don't panic if you had made this assumption to begin with and just calculated f_H . You will receive full credit for your work).