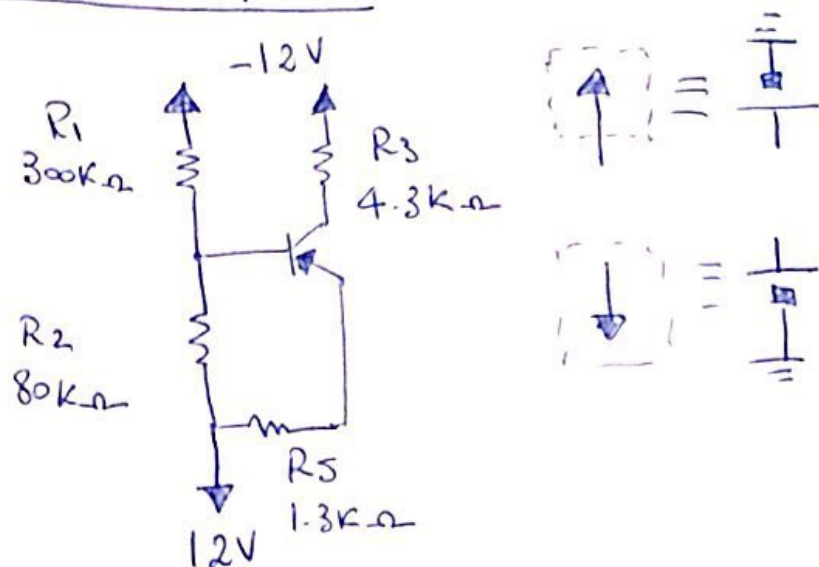


# MID TERM EXAMINATION II - SOLUTION

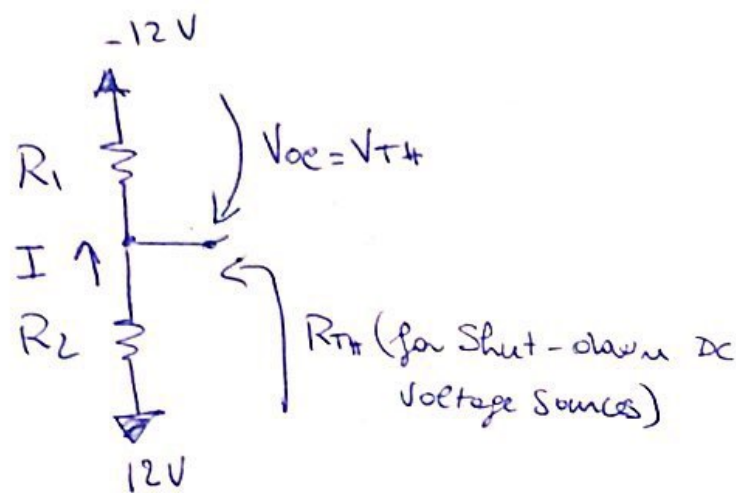
(1)

In order to sketch  $S_{outAC}$  and  $S_{outDC}$ , one will have to solve both the DC and the AC (small-signal) version of the circuit.

## DC ANALYSIS



It is convenient to reduce the circuit looking away (as left) from the base with its Thevenin equivalent circuit.



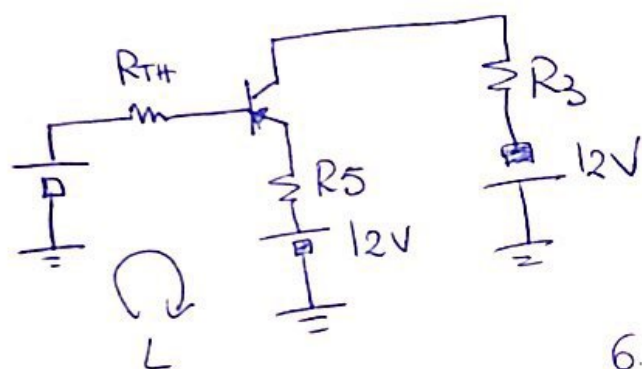
$$V_{TH} = -12 + I R_1$$

$$I = \frac{24}{380K} = 63.16 \mu A$$

$$V_{TH} = -12 + 63.16 \mu \cdot 300K =$$

$$= -12 + 18.948 = 6.948 V$$

$$R_{TH} = R_1 \parallel R_2 = 300K \parallel 80K = 63.1K$$



KVL @ L:

$$V_{TH} + I_B R_{TH} + V_{EB(on)} + I_E \cdot R_E - 12 = 0$$

ASSUMING THE BJT IN F-A MODE:

$$I_E = (B+1) I_B$$

Thus

$$6.94 + I_B \cdot 63.1K + 0.7 + I_B(B+1)(1.3K) - 12 = 0$$

(2)

$$I_B = \frac{12 - 6.94 - 0.7}{63.1 \text{ K} + (180.7 + 1) \cdot 1.3 \text{ K}} = \frac{4.36}{289.31} = 14.5 \mu\text{A}$$

$$I_C = \beta I_B = 2.63 \text{ mA} ; I_E = (\beta + 1) I_B = 2.65 \text{ mA}$$

The next step is to verify the assumption of F.A. mode operation for the BJT.

Since all junctions in the BJT have a threshold (or on) voltage of  $0.7 \text{ V}$ , the condition of active mode operation for the BJT is

$$V_{EB} > V_{EB(\text{on})} \text{ \& } V_{BC} < V_{BC(\text{on})} \text{ with } V_{EB(\text{on})} = V_{BC(\text{on})} = 0.7 \text{ V}$$

$$V_E = 12 - I_E R_5 = 8.55 \text{ V} ; V_B = 6.94 + I_B (63.1 \text{ K}) = 7.85 \text{ V}$$

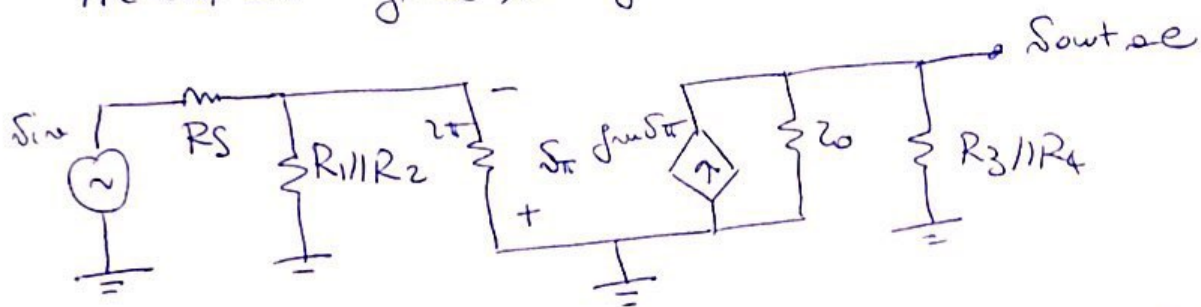
$$V_C = -12 + I_C R_3 = -0.681 \text{ V}$$

$$V_{EB} = 0.705 > V_{EB(\text{on})} \Rightarrow \text{B-E junction is forward biased.}$$

$$V_{BC} = 8.531 > V_{BC(\text{on})} \Rightarrow \text{B-C junction is reverse biased.}$$

Thus the assumption of the BJT operating in F.-A. mode is verified.

AC (Small-Signal) analysis.



$$g_m = \frac{I_C}{V_T} = \frac{2.63 \text{ mA}}{0.025 \text{ V}} = 0.101 \frac{\text{A}}{\text{V}} ; r_{\pi} = \frac{\beta}{g_m} = \frac{180.7}{0.101} = 1.7 \text{ K}\Omega$$

$$r_o = \frac{V_{CE} + V_A}{I_C} \approx \frac{1 \text{ V}}{I_C} \approx 4.5 \text{ K}\Omega$$

$$\bar{v}_o = g_m (r_o \parallel R_3 \parallel R_4) \bar{v}_\pi \quad (\bar{v}_o = \bar{v}_{out,se})$$

$$\bar{v}_\pi = -\bar{v}_{in} \cdot \frac{R_1 \parallel R_2 \parallel R_\pi}{R_S + R_1 \parallel R_2 \parallel R_\pi}$$

$$\bar{v}_{out,se} = -g_m (r_o \parallel R_3 \parallel R_4) \cdot \frac{R_1 \parallel R_2 \parallel R_\pi}{R_S + R_1 \parallel R_2 \parallel R_\pi} \bar{v}_{in} =$$

$$= -0.101 \cdot (41.5k \parallel 4.3k \parallel 10k) \cdot \frac{(300k \parallel 80k \parallel 1.7k) \bar{v}_{in}}{20k + 300k \parallel 80k \parallel 1.7k} =$$

$$= -\frac{1.731}{21.731} \cdot (283.2) \bar{v}_{in} = -0.079 (283.2) \bar{v}_{in} =$$

$$= -22.37 \bar{v}_{in}$$

$$\bar{v}_{out,se} = \bar{v}_{in} (-22.37) \text{ V}$$

$$\bar{v}_{out,D} = -22.37 \bar{v}_{in} + \bar{v}_C \quad \bar{v} =$$

$$= -22.37 \bar{v}_{in} - 0.681 \text{ V}$$

The SoutDC waveform is identical to the SoutAC waveform but it is shifted by  $-0.681$  w.r.t the origin of the voltage axis.

