

# ECE 322L

## Electronics 2

02/11/20 - Lecture 7

Common Drain and Common Gate Amplifiers

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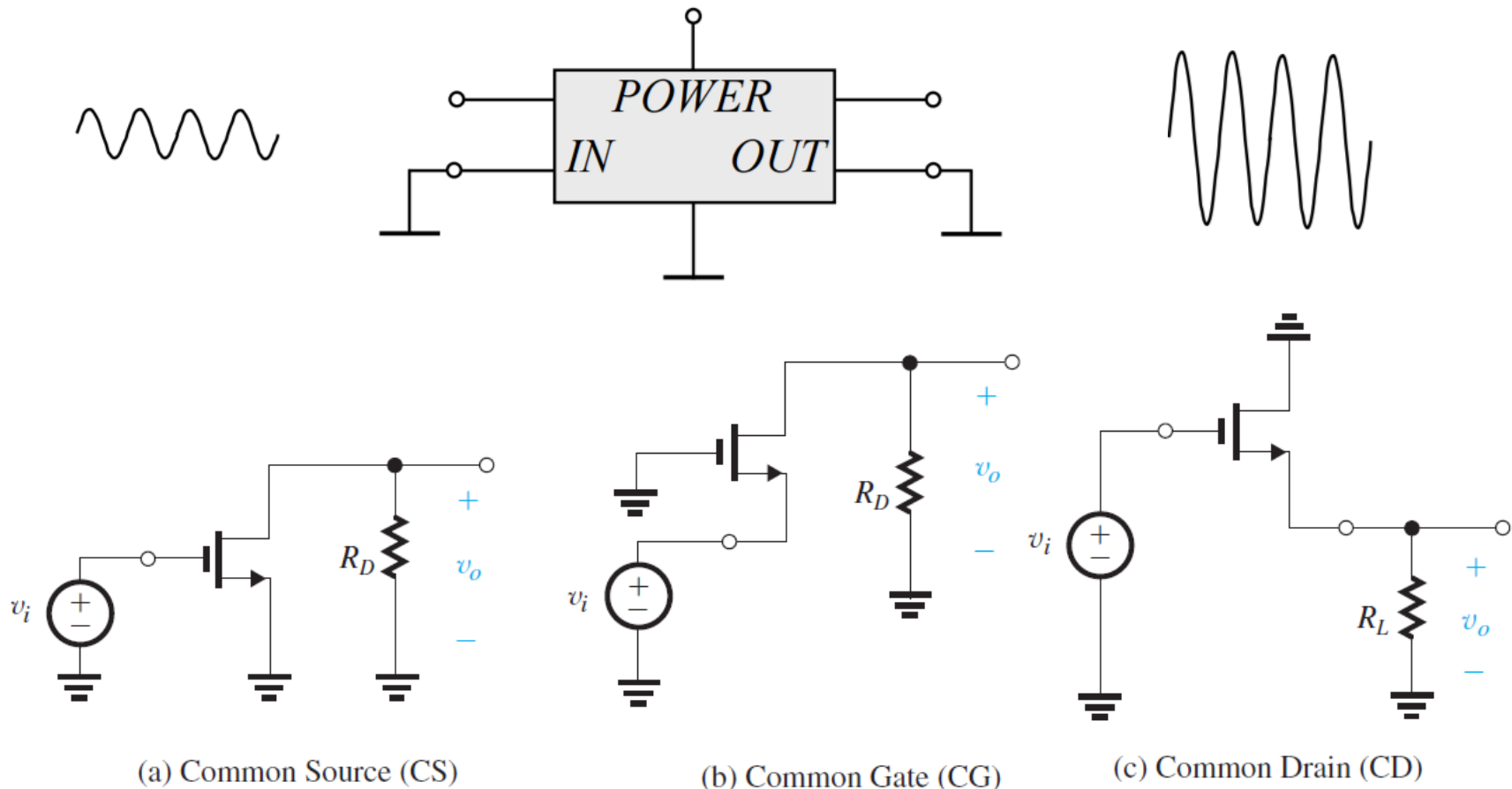
# Updates and Overview

- Midterm 1 next week, Feb 18<sup>th</sup>, 11:00 am-12:15 pm.
- Practice problems in view of the midterm 1:
  - Neamen: design example 4.4 and exercise problem 4.4.

Today:

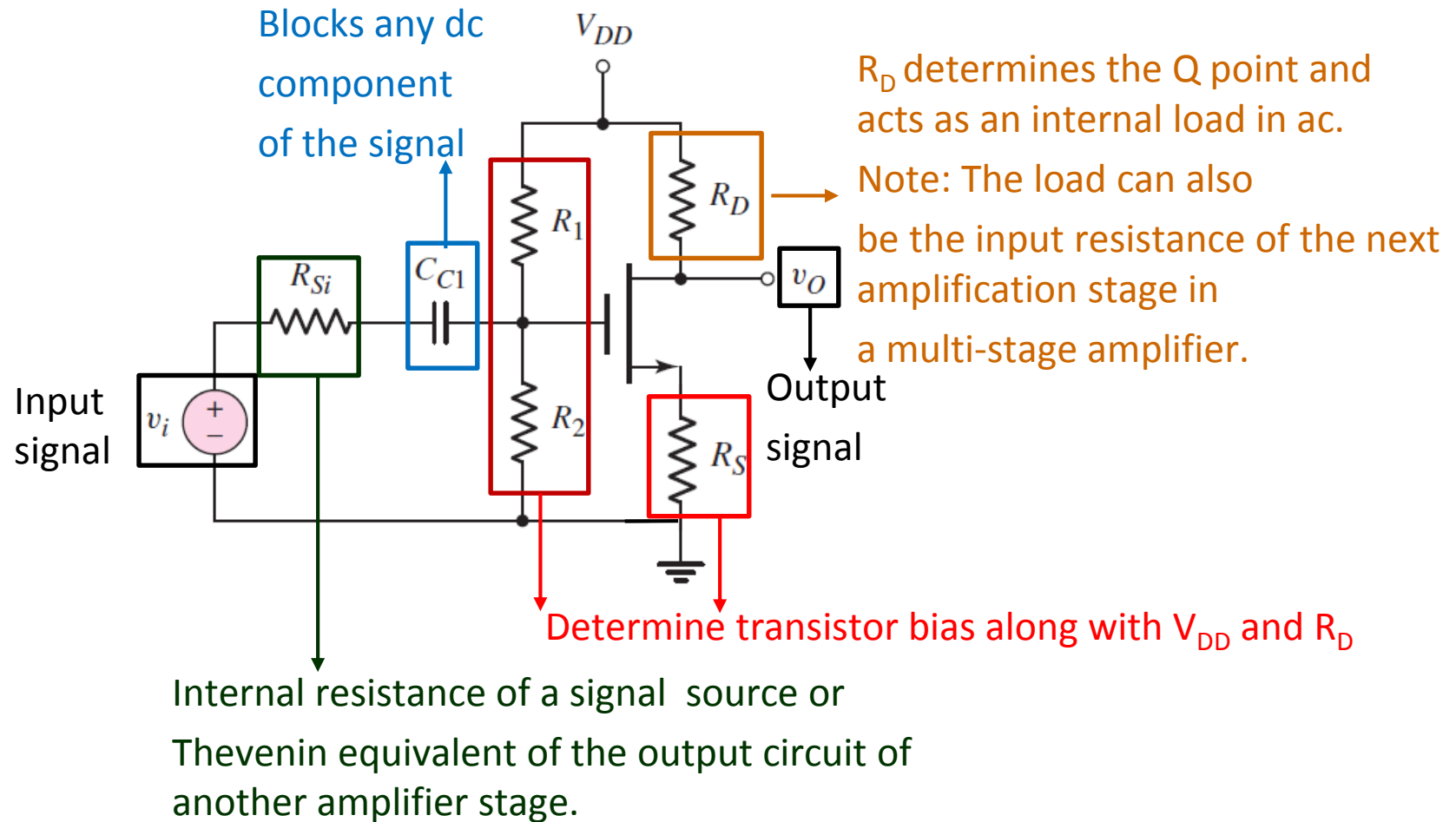
- Review of the common source (CS) amplifier
- Common Gate (CG) FET amplifiers  
(Neamen 4.5, S&S 5.6.5).
- Common Drain (CD) FET amplifiers  
(Neamen 4.4, S&S 5.6.6).

# Basic configurations for FET amplifiers



There are three basic configurations for connecting the MOSFET as an amplifier. Each of these configurations is obtained by connecting one of the three MOSFET terminals to ground, thus creating a two-port network with the grounded terminal being *common* to the input and output ports.

# Common Source (CS) Amplifier w/ $R_S$



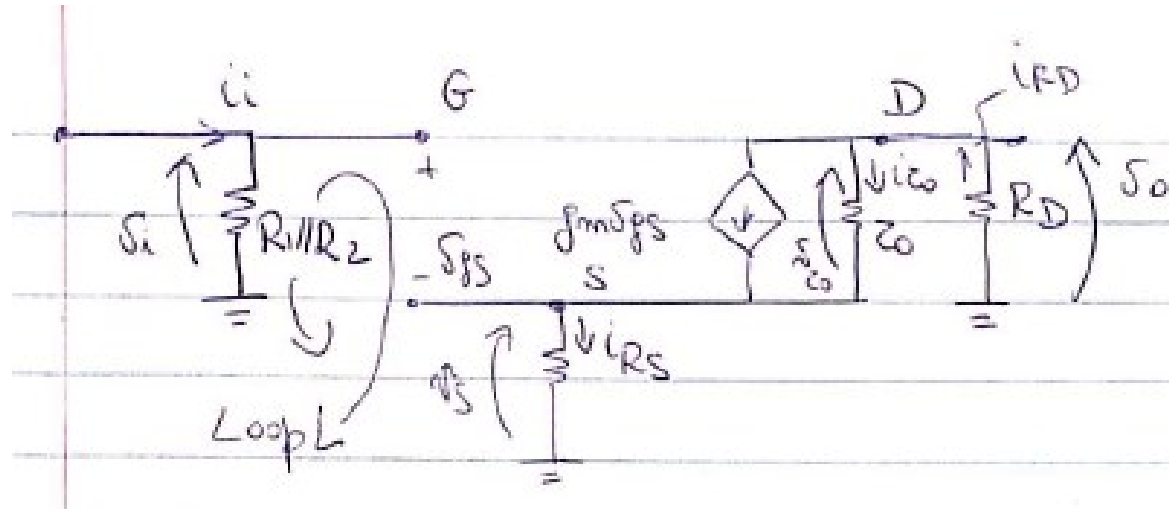
$C_{c1}$  is typically of the order of  $\sim 10\text{s } \mu\text{F}$ . This value guarantees a much smaller capacitor impedance than  $R_{si}$  for signal with frequencies higher than 2 kHz.

$$|Z_C| = \frac{1}{2\pi f C_C} = \frac{1}{2\pi (2 \times 10^3)(10 \times 10^{-6})} \cong 8 \Omega$$

$C_{c1}$  can then be replaced with a short-circuit in ac analysis of high frequency signals

# Common Source (CS) Amplifier w/ $R_s$

## Input resistance and amplifier gain



$$R_{in} = \frac{v_i}{i_i} = R_1 \parallel R_2$$

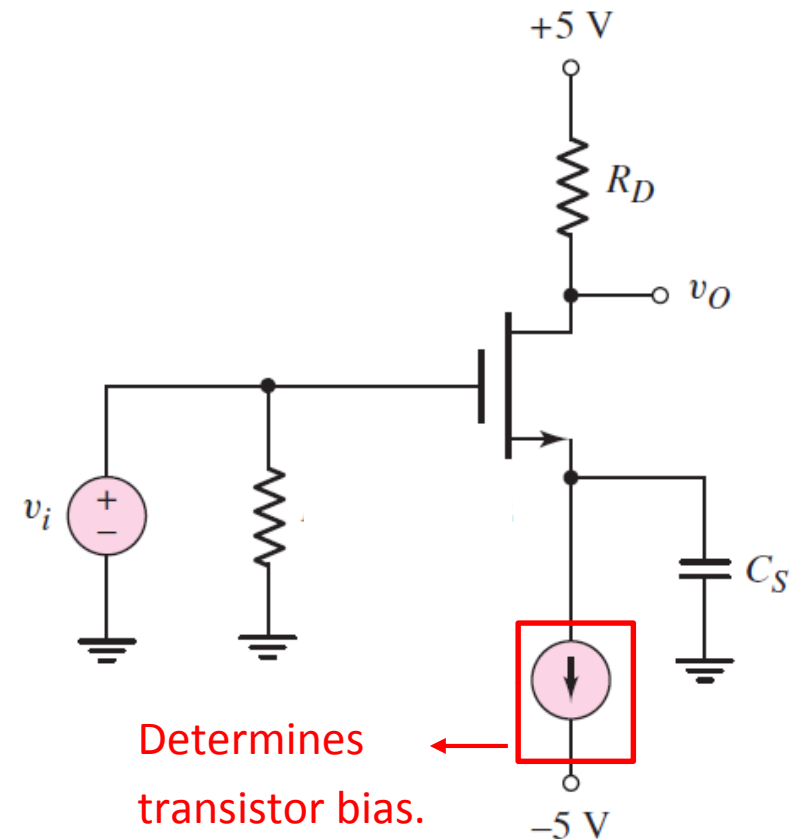
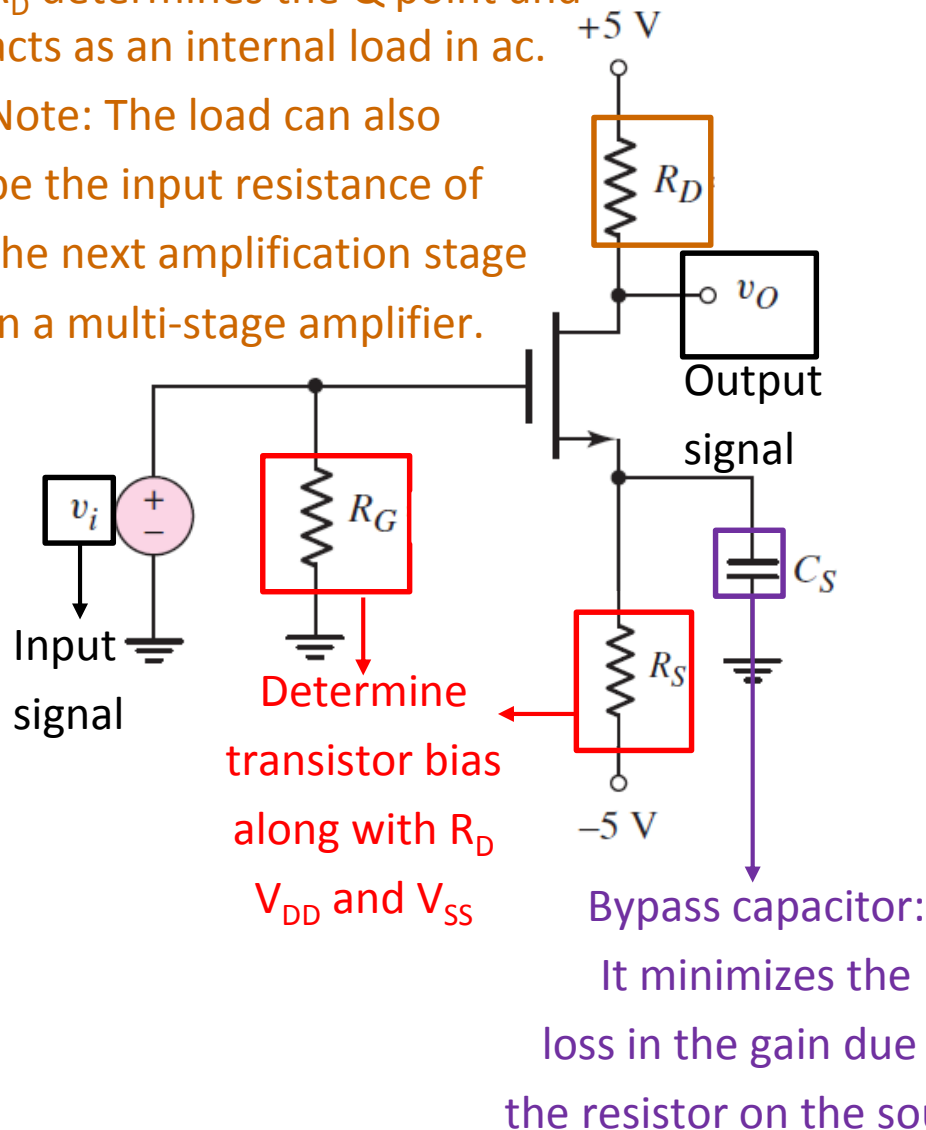
$$A_{vo} = \frac{v_o}{v_i} = - \frac{g_m R_D}{1 + g_m R_s + \frac{1}{r_o} (R_s + R_D)} \approx - \frac{g_m R_D}{1 + g_m R_s}$$

$$R_o = R_D \parallel [r_o + (1 + g_m r_o) R_s] \approx R_D \quad r_o \gg R_s + R_D$$

# Common Source (CS) Amplifier w/ Bypass Capacitor

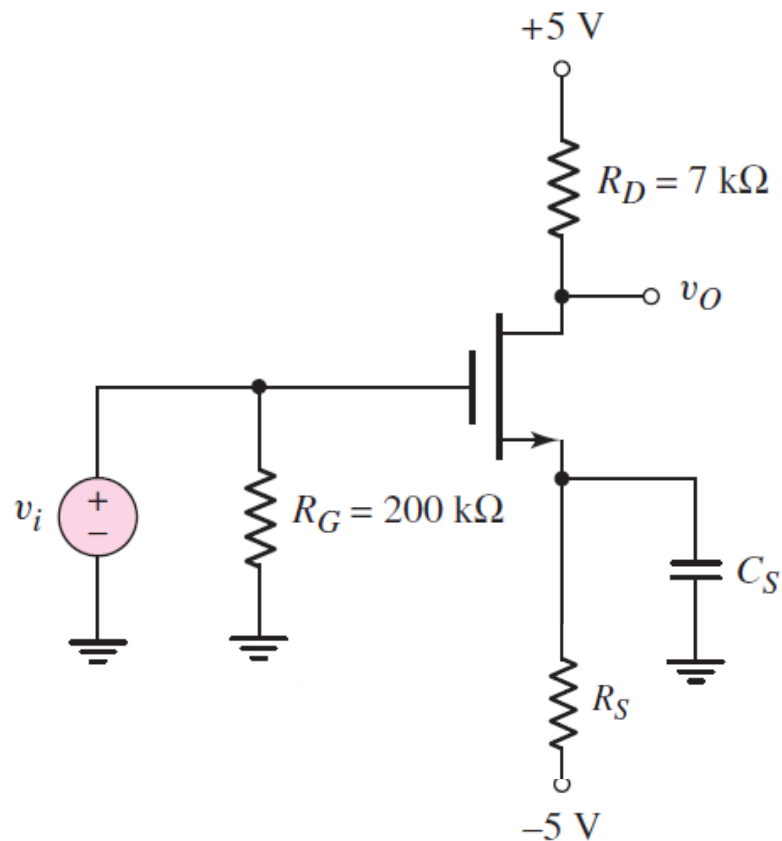
$R_D$  determines the Q point and acts as an internal load in ac.

Note: The load can also be the input resistance of the next amplification stage  
In a multi-stage amplifier.



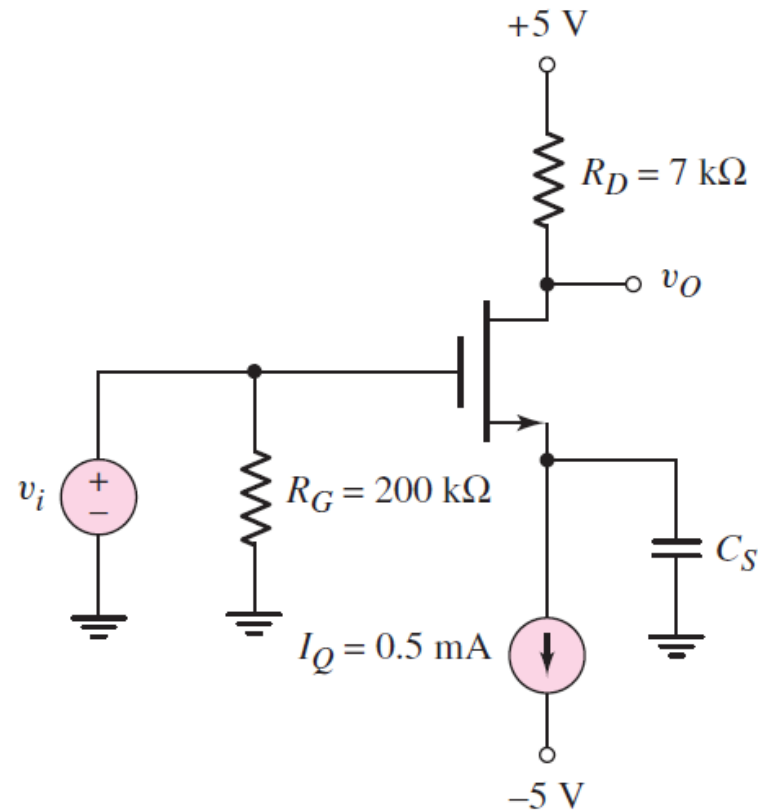
Note: the internal resistance of a real current source would affect the Q point just as  $R_S$  in the circuit on the lhs.

# Review: Common Source (CS) Amplifier



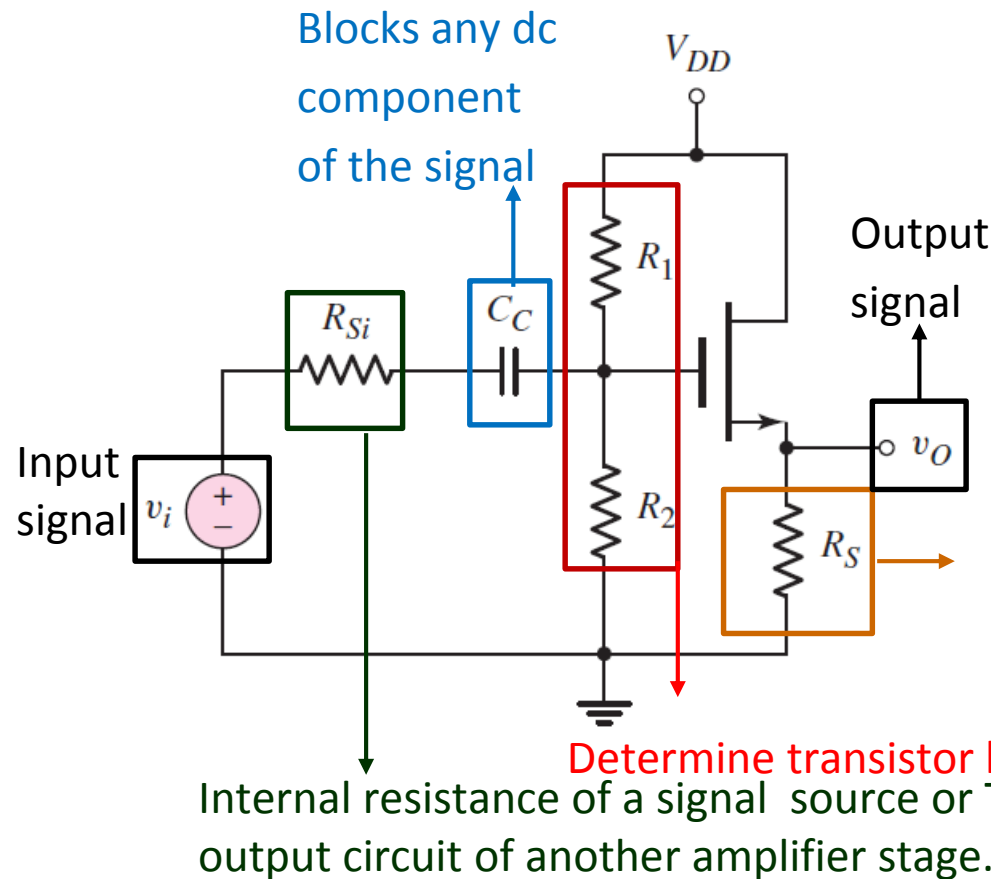
**High**  
 $R_i = R_G$

**Moderate**  
 $R_o \approx R_D$



**High**  
 $A_{vO} \approx -g_m R_D$

# Common drain (CD) FET amplifier



$R_S$  determines the Q point and acts as an internal load in ac.

Note: The load can also be the input resistance of the next amplification stage in a multi-stage amplifier.

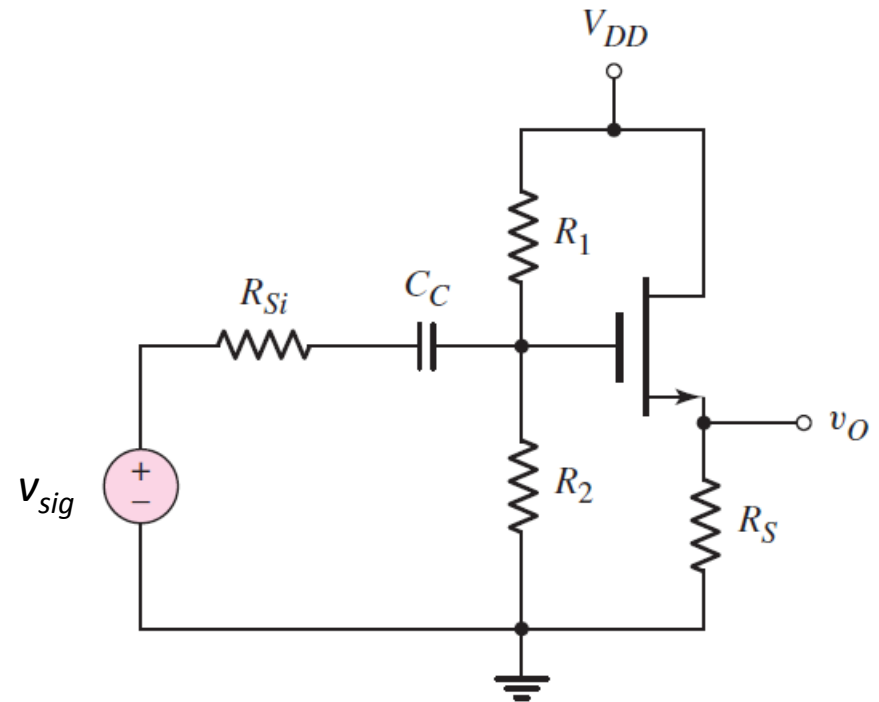
$C_{c1} \sim 10\text{s } \mu\text{F}$ . This value guarantees a much smaller capacitor impedance than  $R_{Si}$  for signal with frequencies higher than 2 kHz. It can be treated as a short-circuit in ac at those frequencies



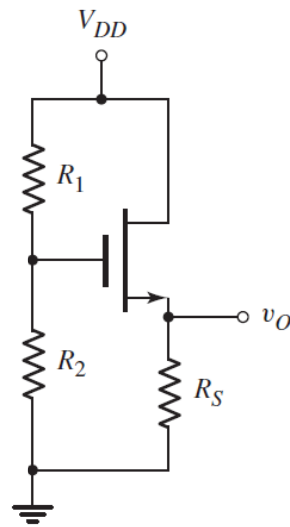
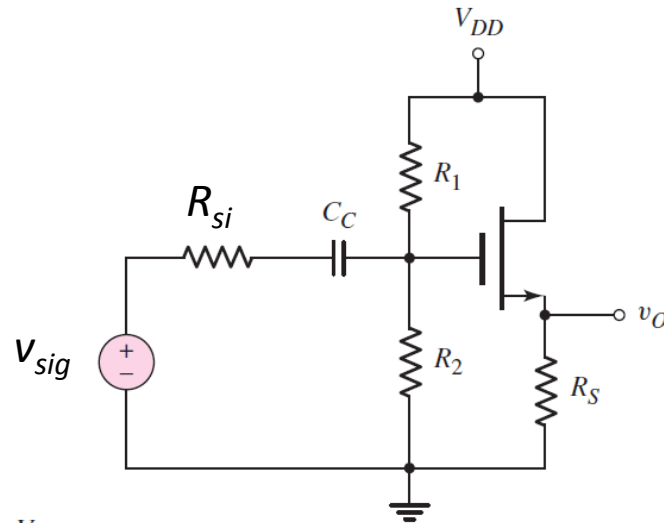
# In class problem 1

Sketch the AC and the small-signal equivalent circuit of the common drain amplifier below. Determine the expressions for the input and output resistance, the open circuit voltage gain, the amplifier gain and the overall voltage gain. Consider  $\lambda \neq 0$ .

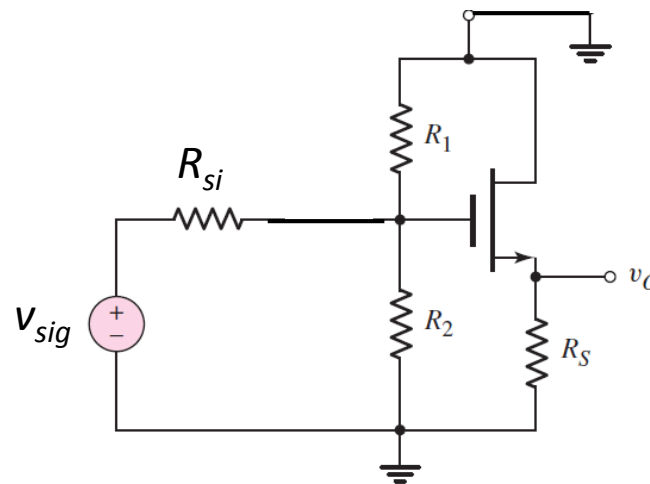
Assume a mid-band frequency for the input signal.



# In class problem 1-Solution

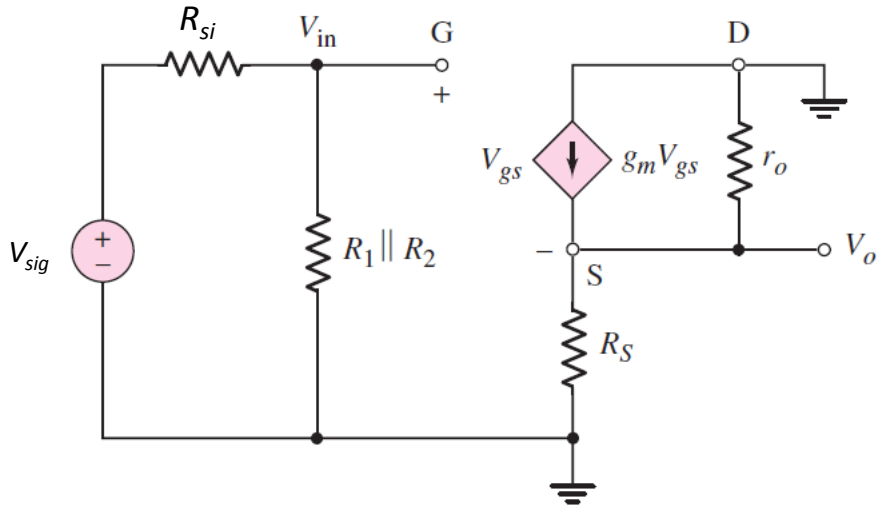
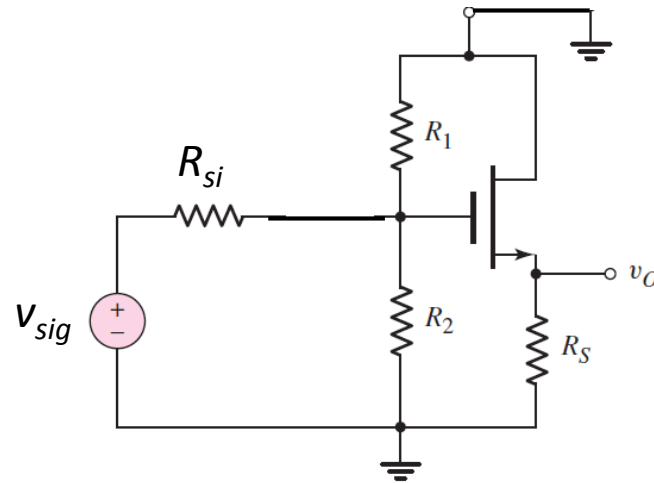


DC circuit

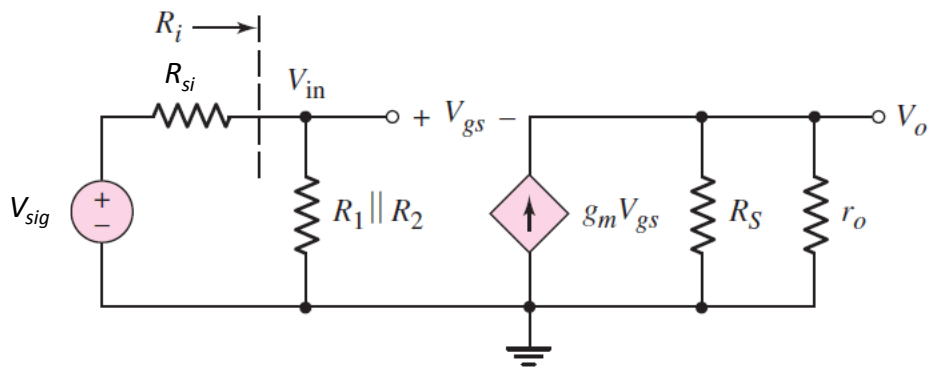


AC circuit

# In class problem 1-Solution

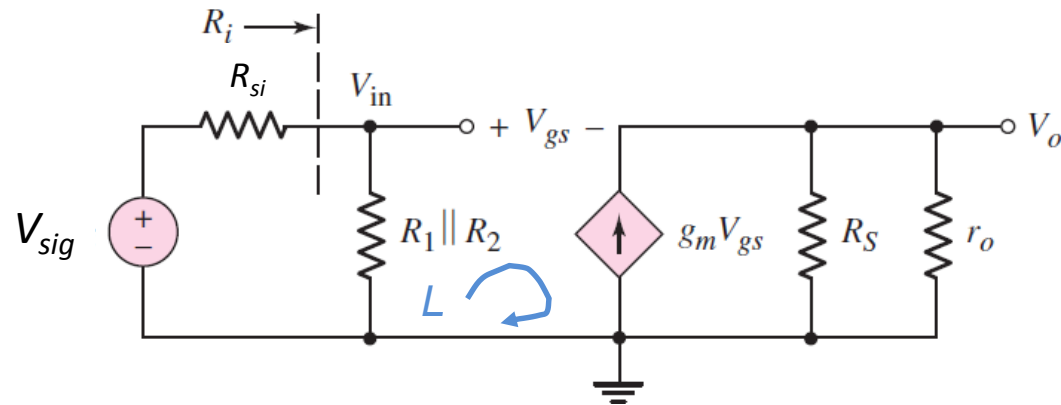


(a)



(b)

# In class problem 1-Solution



Input resistance

$$R_i = R_1 \parallel R_2$$

Gain

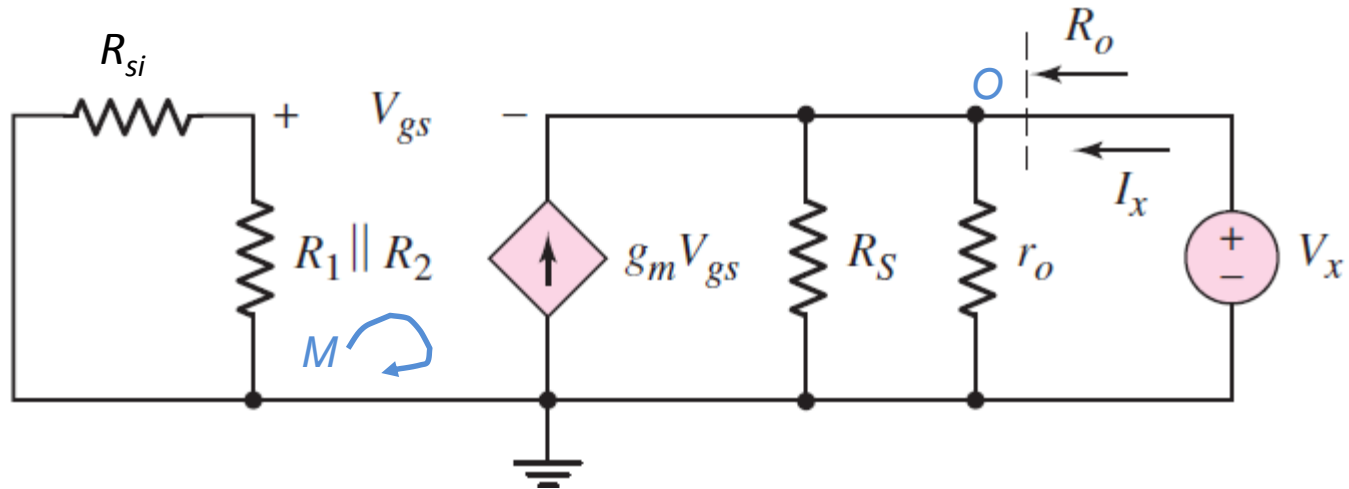
*KVL @ L*

$$V_o = (g_m V_{gs})(R_S \parallel r_o) \quad V_{in} = V_{gs} + V_o = V_{gs} + g_m V_{gs}(R_S \parallel r_o)$$

$$V_{gs} = \frac{V_{in}}{1 + g_m(R_S \parallel r_o)} = \left[ \frac{\frac{1}{g_m}}{\frac{1}{g_m} + (R_S \parallel r_o)} \right] \cdot V_{in} \quad A_v = \frac{V_o}{V_{in}} = \frac{g_m(R_S \parallel r_o)}{1 + g_m(R_S \parallel r_o)}$$

$$G_v = \frac{V_o}{V_{sig}} = \frac{g_m(R_S \parallel r_o)}{1 + g_m(R_S \parallel r_o)} \cdot \left( \frac{R_i}{R_i + R_{Si}} \right) = \frac{R_S \parallel r_o}{\frac{1}{g_m} + R_S \parallel r_o} \cdot \left( \frac{R_i}{R_i + R_{Si}} \right)$$

# In class problem 1-Solution



*KCL @ O*

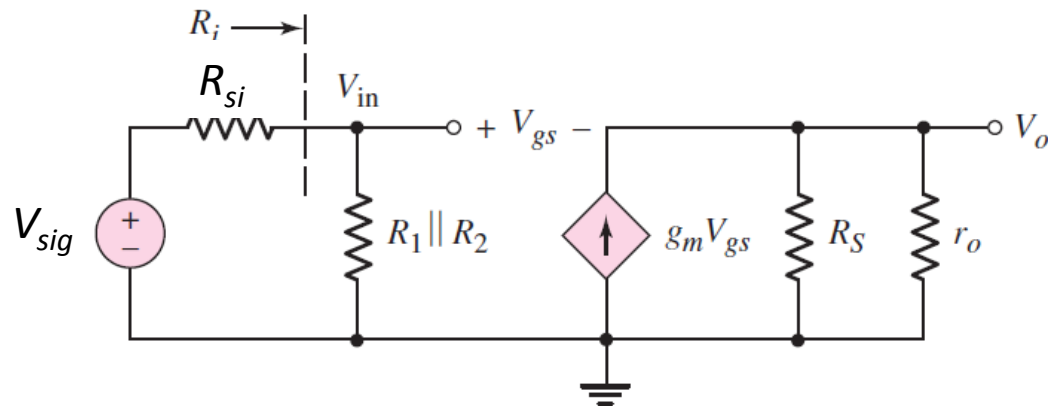
*KVL @ M*

$$R_o = \frac{V_x}{I_x} \quad I_x + g_m V_{gs} = \frac{V_x}{R_S} + \frac{V_x}{r_o} \quad V_{gs} = -V_x \quad I_x = V_x \left( g_m + \frac{1}{R_S} + \frac{1}{r_o} \right)$$

$$\frac{I_x}{V_x} = \frac{1}{R_o} = g_m + \frac{1}{R_S} + \frac{1}{r_o}$$

$$R_o = \frac{1}{g_m} \parallel R_S \parallel r_o$$

# In class problem 1-Solution



$$R_i = R_1 \parallel R_2$$

**High**

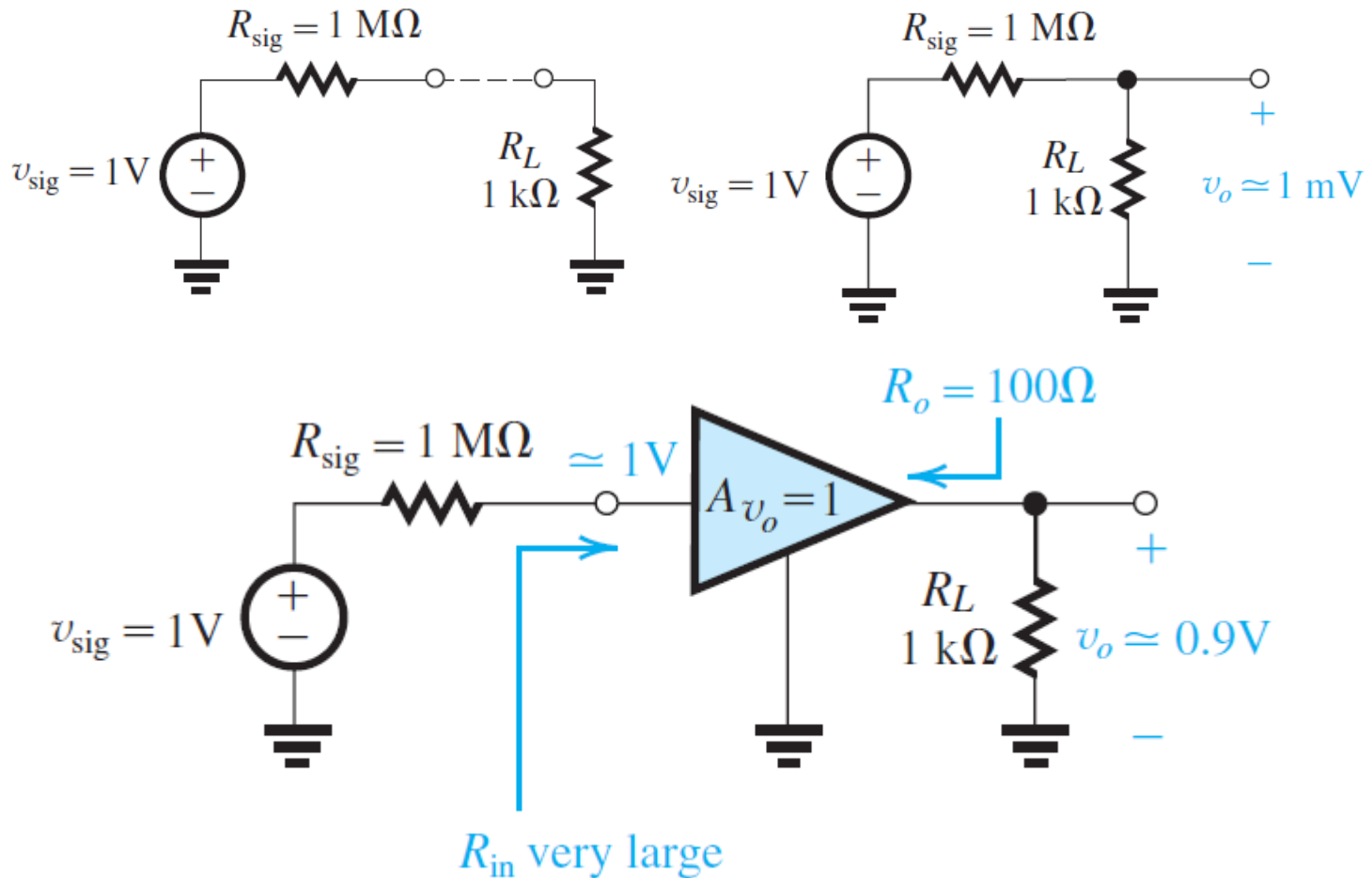
$$G_v = \frac{R_S \parallel r_o}{\frac{1}{g_m} + R_S \parallel r_o} \cdot \left( \frac{R_i}{R_i + R_{si}} \right) \quad \text{Positive and } \leq 1$$

$$R_o = \frac{1}{g_m} \parallel R_S \parallel r_o$$

**Low (Dominated by  $1/g_m$ )**

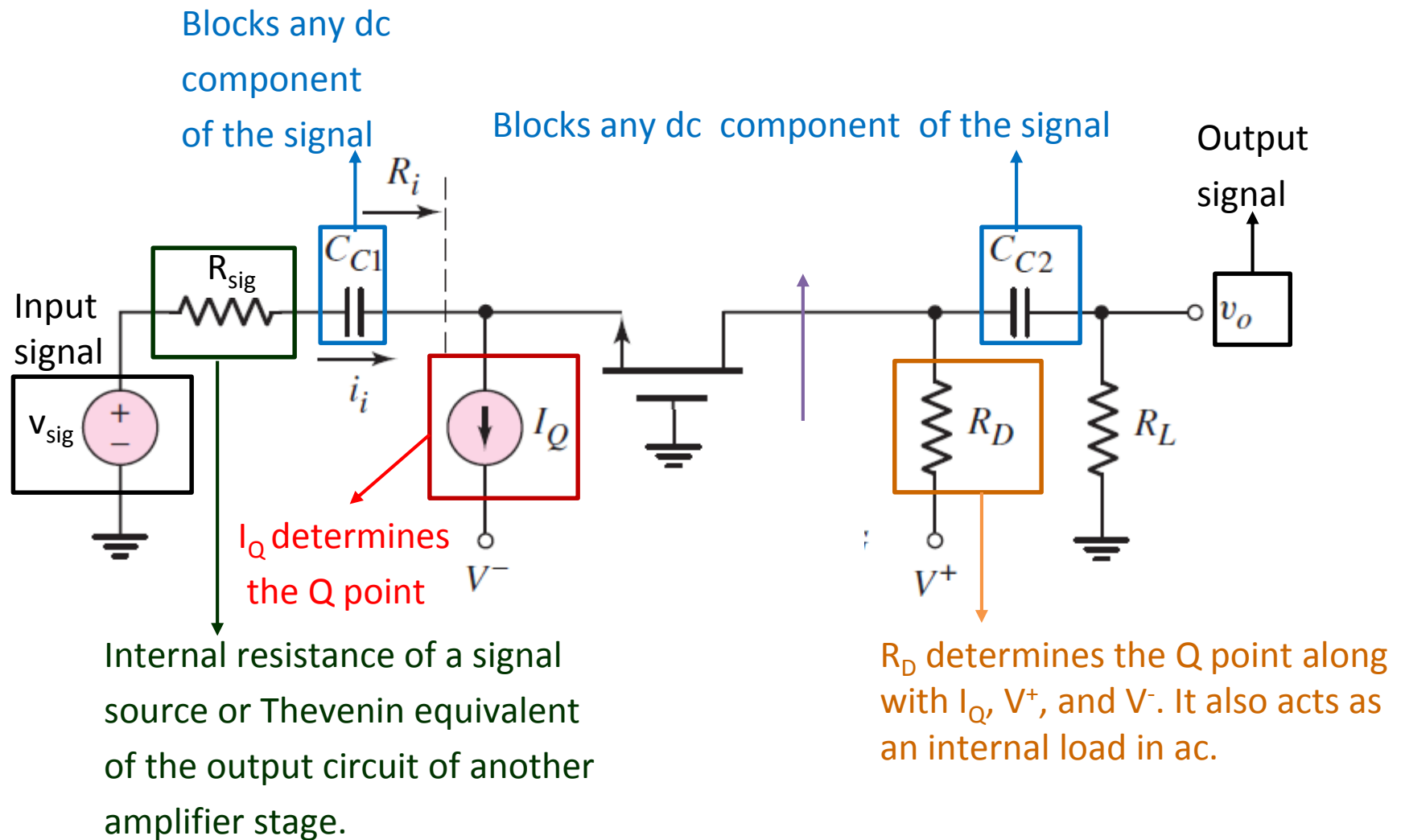
***Because the output signal is in phase with input signal and it has close amplitude to it, this circuit is also called the source follower.***

# Application of the source follower: Voltage buffer



***A source follower can be used to transfer a high amplitude voltage from a source with a large internal resistance to a load .***

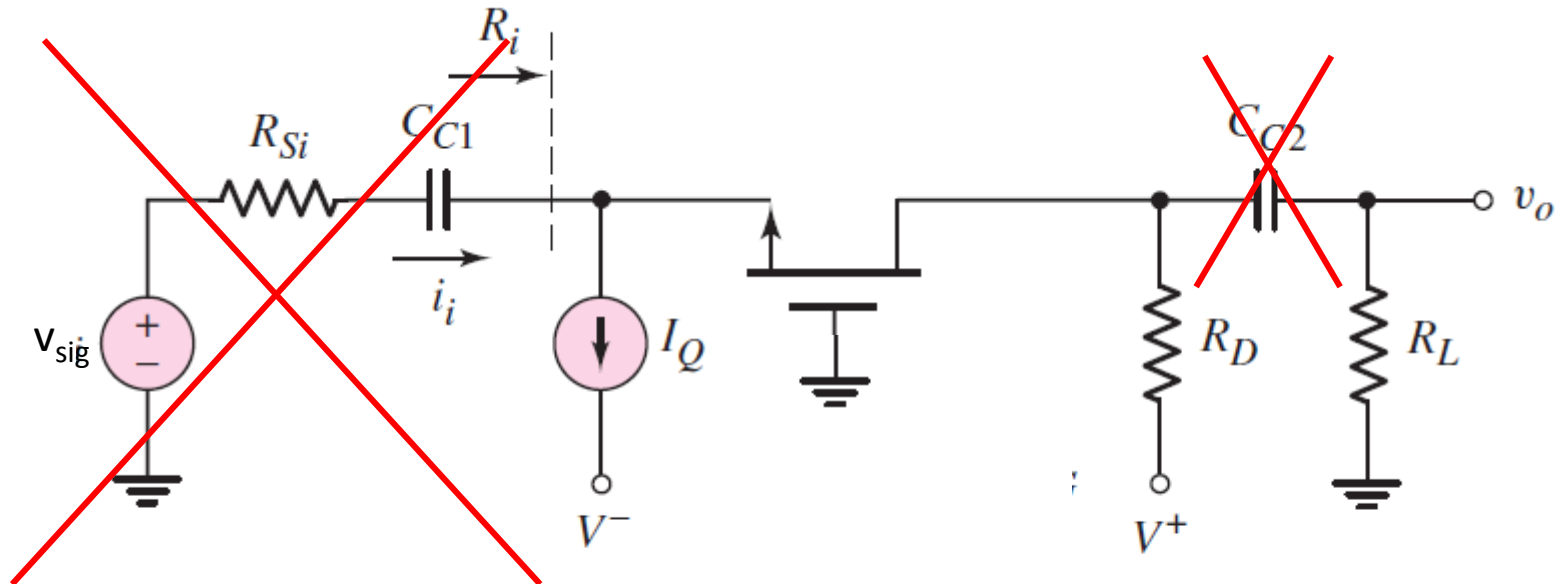
# Common Gate (CG) FET amplifier





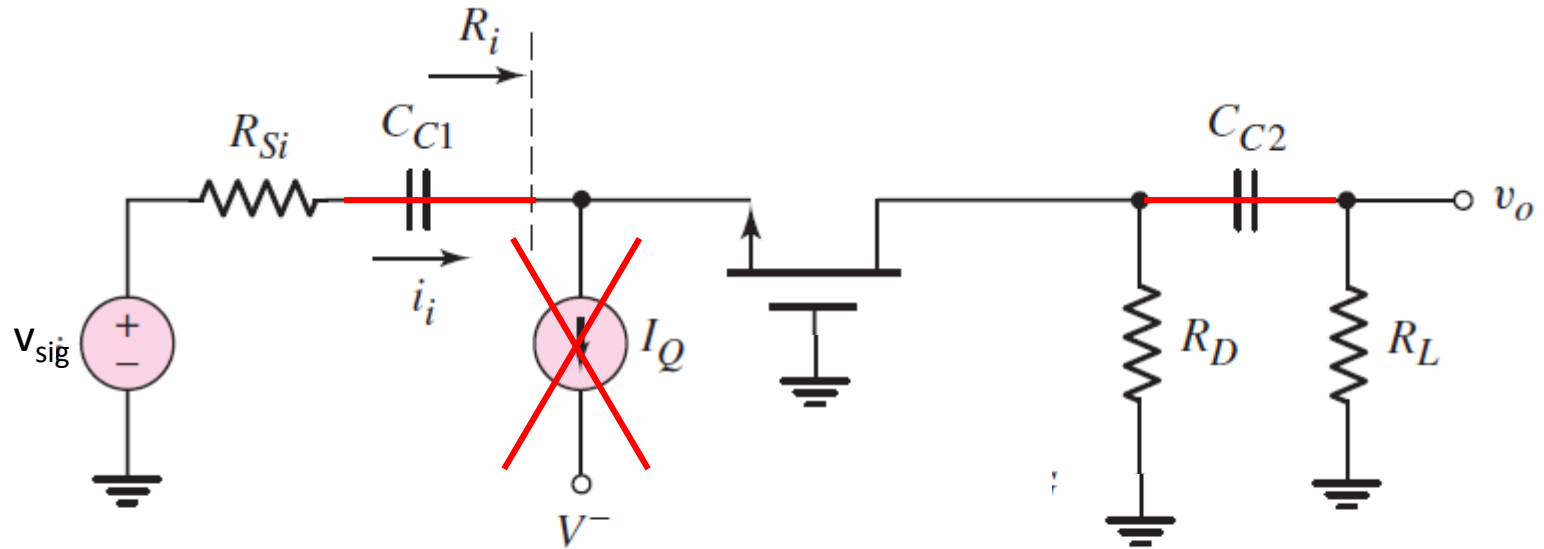
# Common Gate (CG) FET amplifier

## *DC circuit*



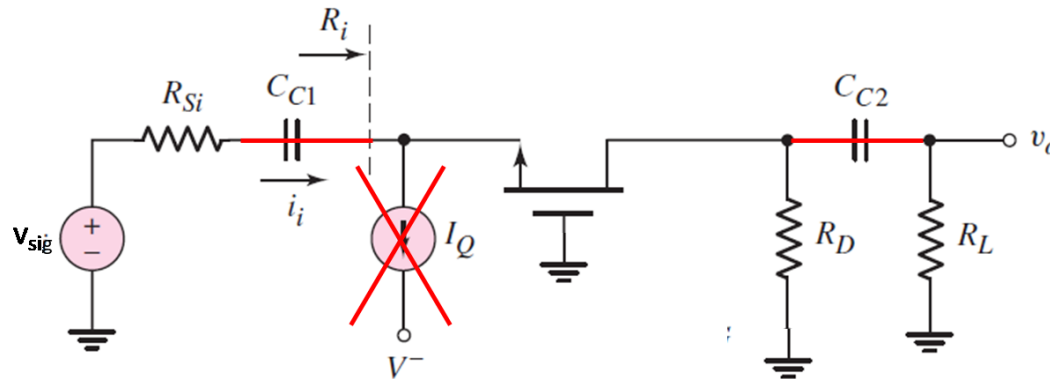
# Common Gate (CG) FET amplifier

## *AC circuit*

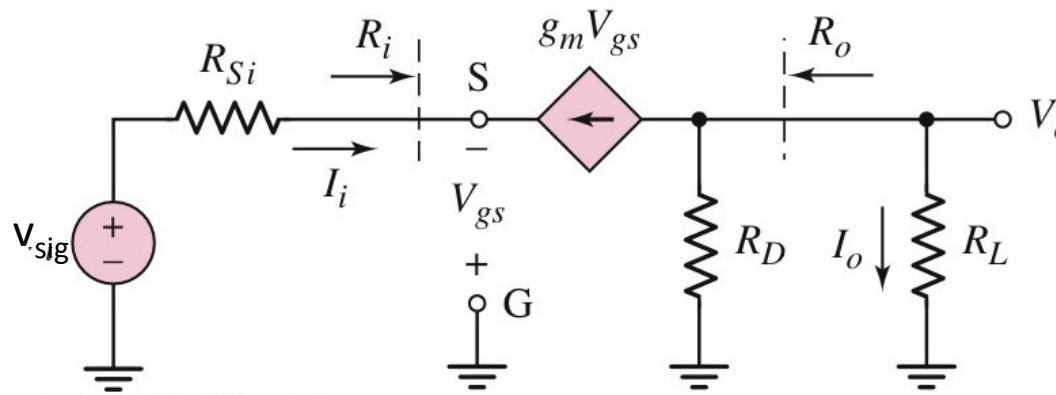


# Common Gate (CG) FET amplifier

*From AC to a small-signal equivalent circuit*



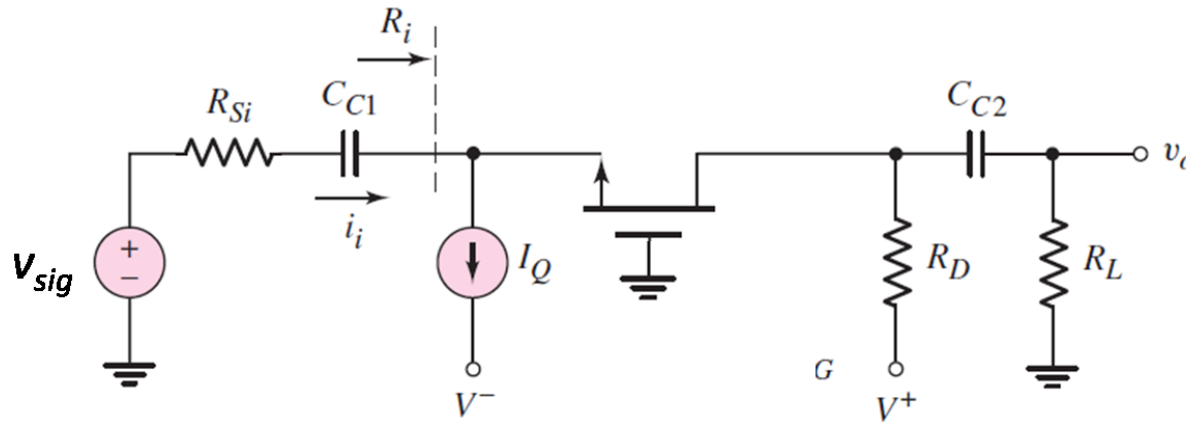
**AC circuit**



**Small-signal circuit**

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# Common Gate (CG) FET amplifier



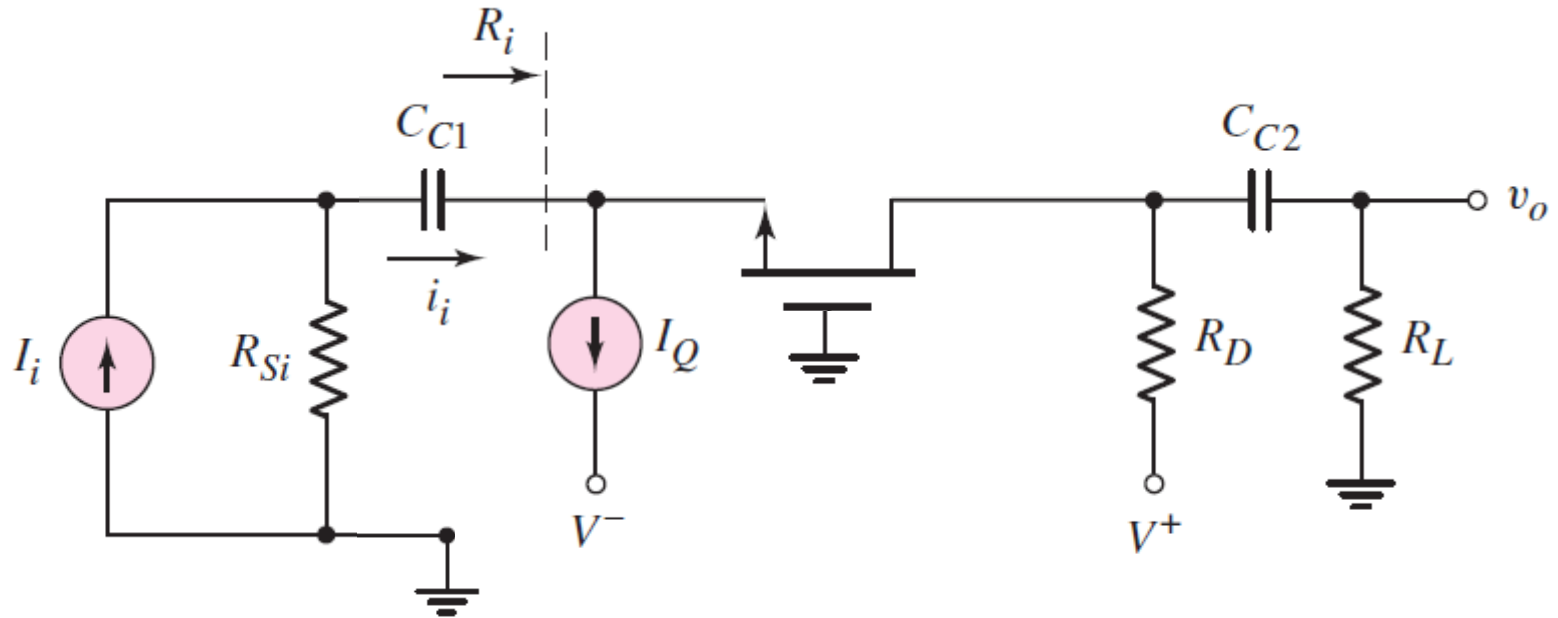
**Input resistance\***  $R_i = \frac{1}{g_m}$  **Low**

**Overall gain\***  $G_v = \frac{g_m(R_D \parallel R_L)}{1 + g_m R_{Si}}$  **Positive and large**

**Output resistance\***  $R_o = R_D$  **Low/Moderate**

- Practice calculating the performance parameters above and compare your approach to what is reported in the handout within the lecture 7 folder.

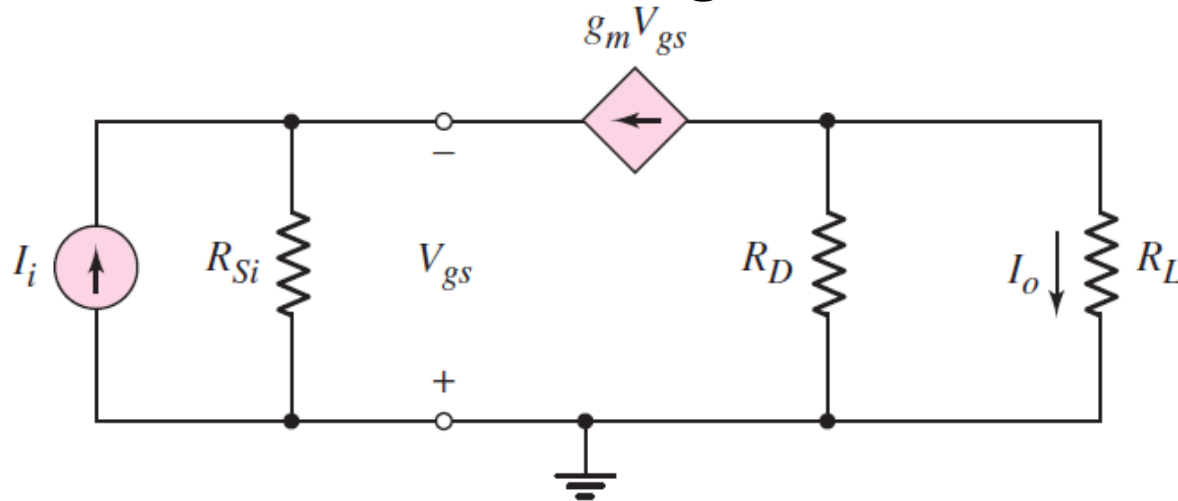
# Common Gate (CG) FET amplifier as current amplifier



# Common Gate (CG) FET amplifier as current buffer

## Current gain

$$A_i = \frac{I_o}{I_i}$$



$$I_o = \left( \frac{R_D}{R_D + R_L} \right) (-g_m V_{gs}) \quad I_i + g_m V_{gs} + \frac{V_{gs}}{R_{Si}} = 0$$

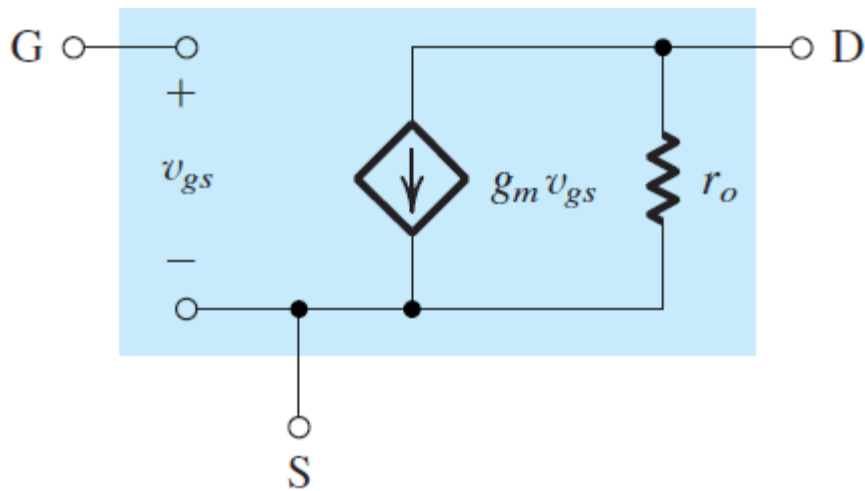
$$V_{gs} = -I_i \left( \frac{R_{Si}}{1 + g_m R_{Si}} \right) \quad A_i = \frac{I_o}{I_i} = \left( \frac{R_D}{R_D + R_L} \right) \cdot \left( \frac{g_m R_{Si}}{1 + g_m R_{Si}} \right)$$

**If  $R_D \gg R_L$  the current gain is close to 1 as  $g_m R_{Si} \gg 1$**

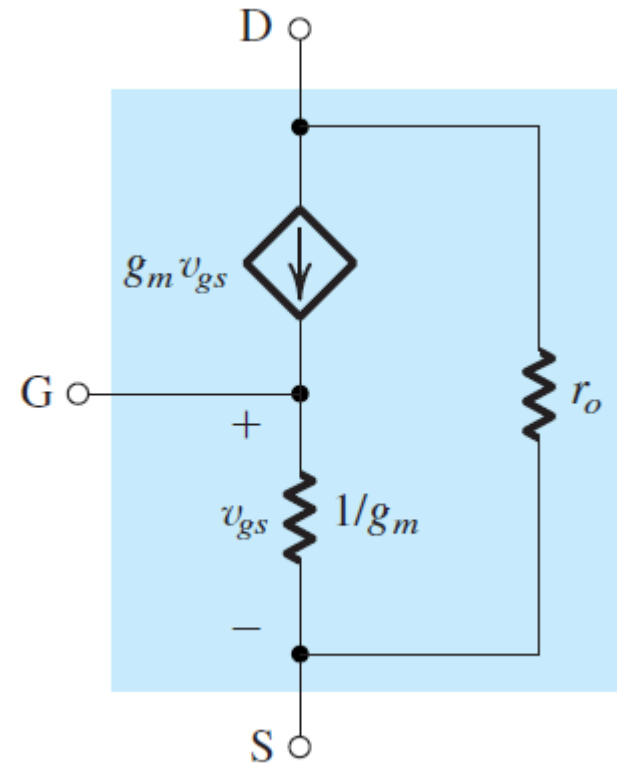
**Application: current buffer between high current sources with low internal resistance and high loads**

# Small-signal equivalent circuits

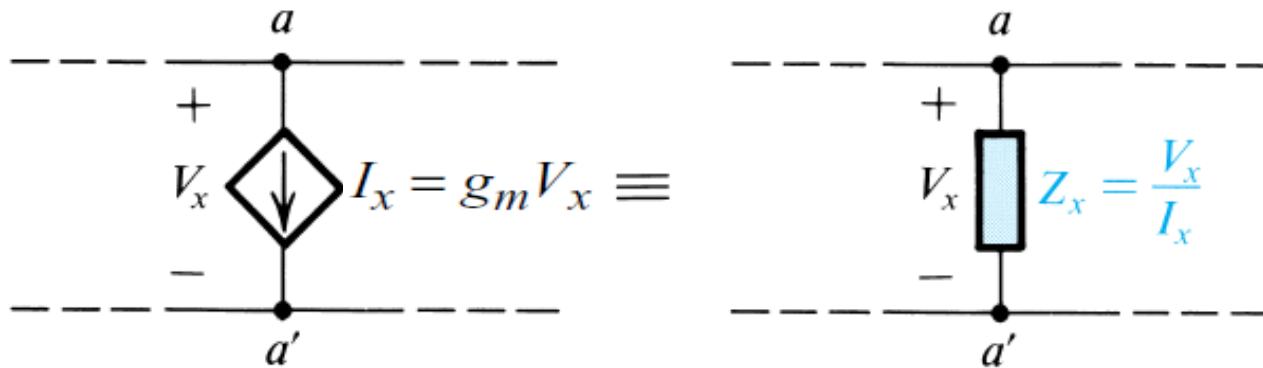
## $\Pi$ model



## T model



# Source-absorption theorem

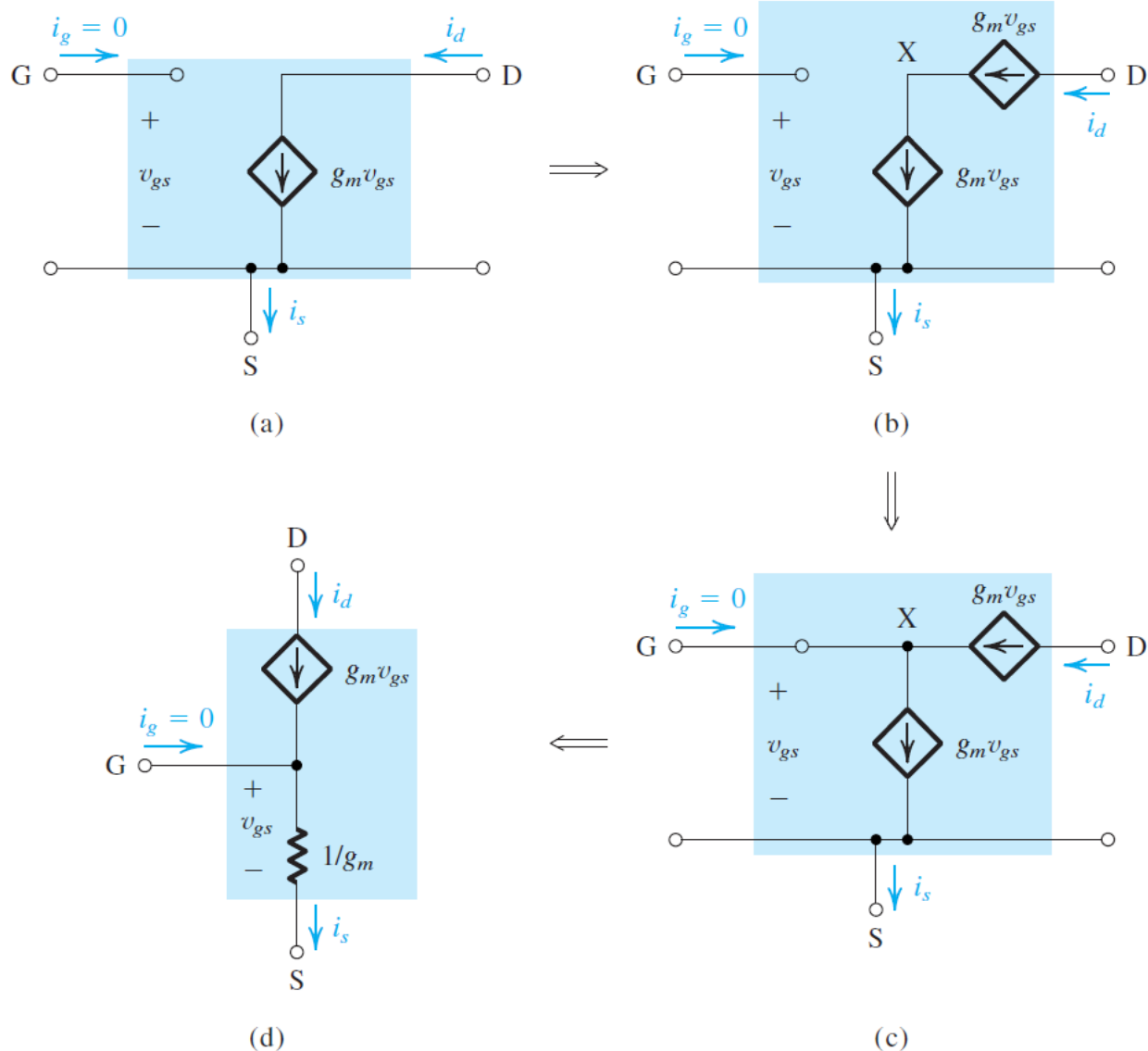


The current **source-absorption theorem** establishes that if, in one branch of the circuit with a voltage  $V_x$ , there is a dependent current **source** controlled by  $V_x$ , the **source** can be replaced by a simple impedance with value equal to the  $1/\text{source controlling factor}$ .

(S&S Appendix D)

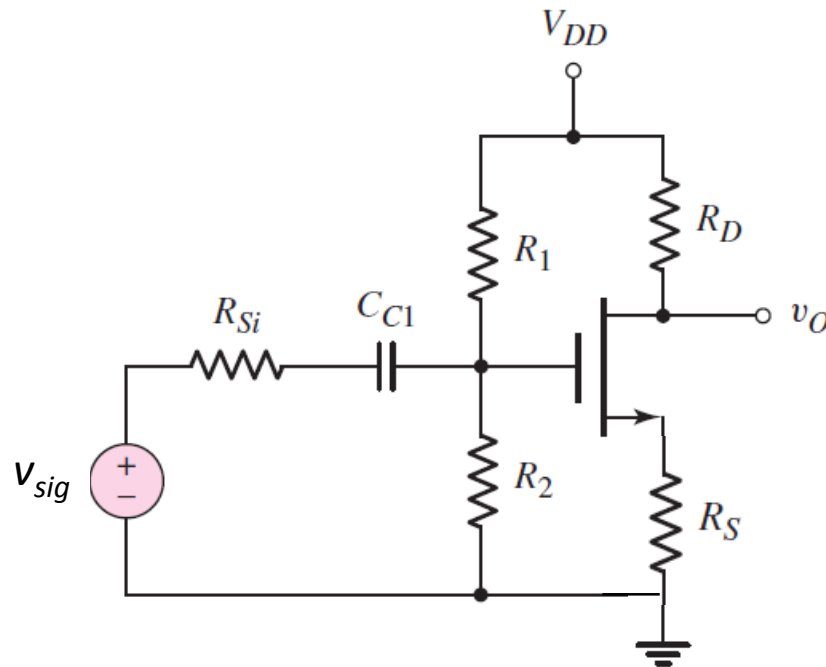


# Conversion from a $\Pi$ to a T model



# Take-home problem

Sketch the small-signal equivalent circuit of the common source amplifier below. Determine the expressions for the input and output resistance, the open circuit voltage gain, the amplifier gain and the overall voltage gain. Use a T model. Consider two cases:  $\lambda=0$  and  $\lambda \neq 0$ .



# Overview of lecture 8

- Comparison of the three basic amplifier configurations (Neamen 4.6, S&S 5.6.7)
- Single-stage IC MOSFET amplifiers
  - Amplifiers with enhancement load (Neamen 4.7.1-4.7.2)