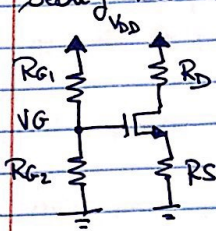


## Midterm examination I-Solutions

## Design problem

One possible strategy to change the operating point of the transistor without altering the layout is to keep the load line fixed and move the Q point along the load line.



Load line  

$$I_D = \frac{V_{DD} - V_{DS}}{R_D + R_S}$$

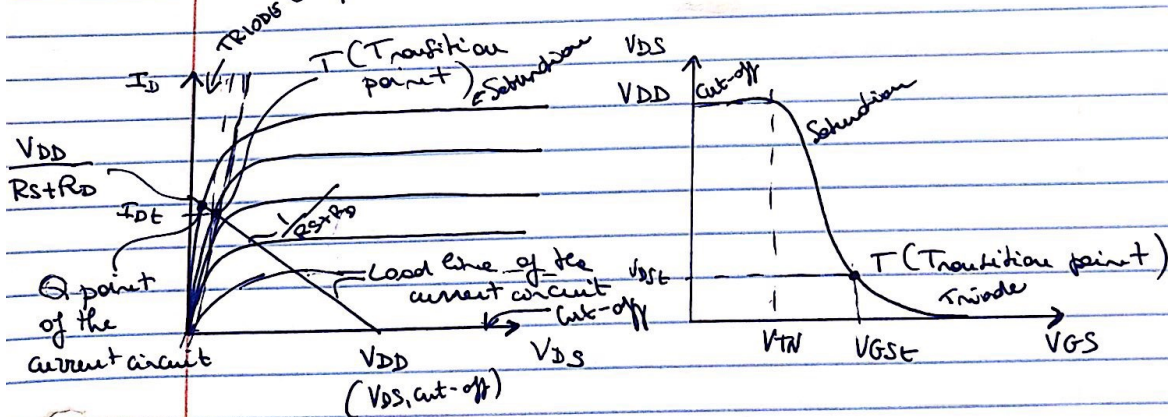
$$I_D = 0 \Rightarrow V_{DS} = V_{DD} = 5V$$

$$V_{DS} = 0 \Rightarrow I_D = \frac{V_{DD}}{R_S + R_D} = 3.3 \mu A$$

We are basically setting  $V_{DD}$ ,  $R_S$ , and  $R_D$  to the values provided in the original circuits, i.e., the one which operates in the linear region.

We choose to move the Q point along the load line towards saturation by lowering the  $V_{GS}$ .

See graphs below.



As  $R_S$  is fixed at  $0.5k\Omega$ , we can only lower the  $V_{GS}$  by lowering the  $V_G$ .

(2)

$$V_G = V_{DD} \frac{R_{G2}}{R_{G1} + R_{G2}}$$

$$V_{DD} \frac{R_{G2}}{R_{G1} + R_{G2}} - R_S I_{DQ, \text{new}} = V_{GSQ, \text{new}}$$

Let  $I_{DQ, \text{new}}$ ,  $V_{GSQ, \text{new}}$ , and  $V_{DSQ, \text{new}}$  be the coordinates of the Q point in the middle of the saturation region.

$$I_{DQ, \text{new}} = \frac{I_{Dt} - I_{D, \text{cut-off}}}{2} + I_{D, \text{cut-off}}$$

$$V_{DSQ, \text{new}} = \frac{V_{DS, \text{cut-off}} - V_{DS, t}}{2} + V_{DS, t}$$

$$V_{GSQ, \text{new}} = \frac{V_{GS, t} - V_{GS, \text{cut-off}}}{2} + V_{GS, \text{cut-off}}$$

The subscript "t" indicates voltages and current at the transition point (between the saturation and the triode region).

The subscript "cut-off" indicates voltages and current at the cut-off point on the transition point between the cut-off and the saturation region.

$$I_{D, \text{cut-off}} = 0 \quad V_{GS, \text{cut-off}} = V_{TN} \quad V_{DS, \text{cut-off}} = V_{DD}$$

Next, we need to calculate the coordinates of the transition point T.

At the transition point:

$$V_{DS, t} = V_{GS, t} - V_{TN}$$

$$I_{Dt} = K_n V_{DS, t}^2$$

$$V_{DS, t} = V_{DD} - (R_D + R_S) I_{Dt} = V_{DD} - (R_D + R_S) K_n V_{DS, t}^2$$

$$K_n (R_D + R_S) V_{DS, t}^2 + V_{DS, t} - V_{DD} = 0$$

$$0.8125 (1.5) V_{DS, t}^2 + V_{DS, t} - 5 = 0$$

$$1.21875 V_{DS, t}^2 + V_{DS, t} - 5 = 0$$

③

$$V_{DSt} = \frac{-1 \pm \sqrt{1 + 27.36}}{2.736} = \frac{-1 \pm 5.32}{2.736} \quad \begin{matrix} \swarrow -2.21V \\ \searrow 1.58V \end{matrix}$$

$$V_{GSt} = 1.58V + 1 = 2.58V$$

$$I_{Dt} = 2.27\mu A$$

$$I_{DQ, new} = 1.13\mu A; V_{DSQ, new} = 3.25V; V_{GSQ, new} = 1.73V$$

Note that  $V_{GSQ, new} > V_{TN}$  and  $V_{DSQ, new} > V_{GSQ, new} - V_{TN}$ , which means that the transistor is in saturation at this new Q point.

Now that we have calculated the coordinates of the Q point we can use the values of  $V_{GSQ, new}$  and  $I_{DQ, new}$  to determine the required values of  $R_{G1}$  and  $R_{G2}$  to achieve the Q point in the middle of the saturation region.

$$\frac{V_{DD} R_{G2}}{R_{G1} + R_{G2}} - R_S I_{DQ, new} = V_{GSQ, new}$$

$$5 \cdot \frac{R_{G2}}{R_{G1} + R_{G2}} - 0.5 \cdot 1.13 = 1.73$$

$$\frac{R_{G2}}{R_{G1} + R_{G2}} = 0.471; \frac{R_{G2}}{R_{G1} + R_{G2}} = \frac{R_{G1} \parallel R_{G2}}{R_{G1}} = 0.471$$

$$\frac{R_{G1} \parallel R_{G2}}{R_{G1}} = 0.471$$

As  $R_{G1} \parallel R_{G2}$  determines the input resistance of the amplifier, it should be of the order of a 100s of  $k\Omega$  to  $M\Omega$ s. Let's select  $R_{G1} \parallel R_{G2} = 100k\Omega$ .

④

$$R_{G1} // R_{G2} = 100 \text{ k}\Omega$$

$$\frac{100 \text{ k}\Omega}{R_{G1}} = 0.471$$

$$R_{G1}$$

$$R_{G1} = 212.3 \text{ k}\Omega$$

$$\frac{R_{G1} R_{G2}}{R_{G1} + R_{G2}} = 100 \text{ k}\Omega$$

$$R_{G1} + R_{G2}$$

$$\frac{R_{G2}}{R_{G1} + R_{G2}} = 0.471$$

$$R_{G1} + R_{G2}$$

$$R_{G2} = 0.471 R_{G1} + 0.471 R_{G2}$$

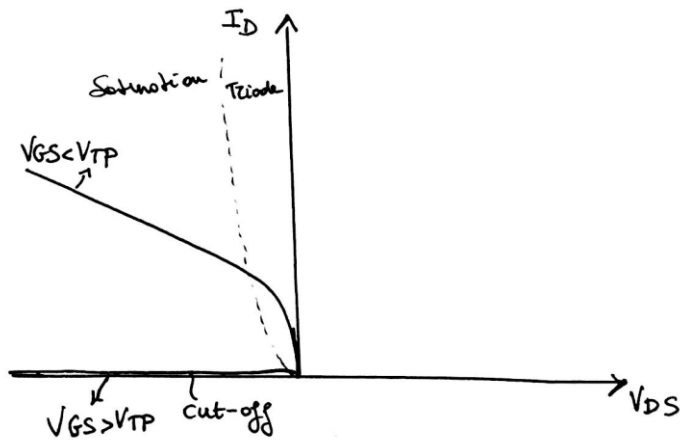
$$R_{G2} (1 - 0.471) = 0.471 R_{G1}$$

$$0.529 R_{G2} = 0.471 R_{G1}$$

$$R_{G2} = 189.02 \text{ k}\Omega$$

### Extra credit questions

1.



2. A resistor ( $R_S$ ) between the source and ground in a common source amplifier is beneficial in DC because it improves the stability of the Q point by implementing a feedback loop between the output current ( $I_D$ ) and the input voltage ( $V_{GS}$ ). However, large  $R_S$  will also reduce the  $V_{DS}$  and bring the Q point close to the transition point or even out of saturation. As a result, the amplified signal may be distorted. Additionally,  $R_S$  also decreases the small-signal voltage gain.