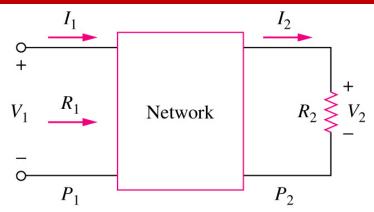
ECE 322L Electronics 2

Handout

Simple systems transfer functions and Bode plots (Neamen 7.2)

The decibel



The DECIBEL value is a logarithmic measurement of the ratio between two variables

Power gain is expressed in dB by the formula:

$$A_P = 10 \log a_P$$

Voltage gain is expressed by:

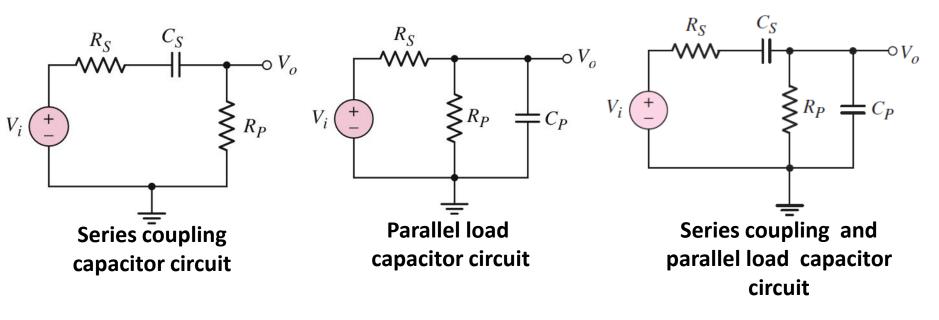
$$A_{V(dB)} = 20\log a_v$$

$$a_p = P_2/P_1$$
 and $a_v = V_2/V_1$

Magnitude	Decibel Value
0.001	-60
0.01	-40
0.1	-20
0.5	-6
$1/\sqrt{2}$	-3
1	0
$\sqrt{2}$	3
2	6
10	20
20	26
100	40

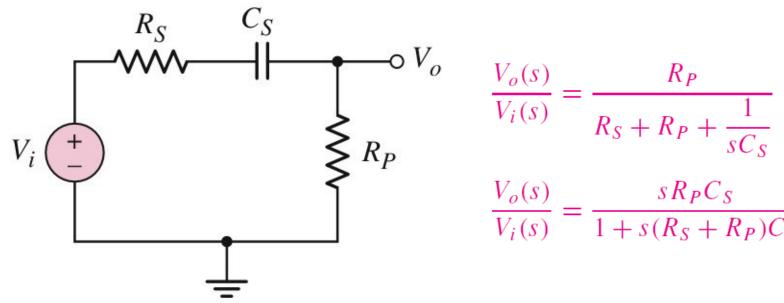
Selected transfer functions

It is useful to determine the frequency response of an amplifier are the transfer functions $T(s) = (V_{\Omega}/V_{i})$ of the circuits below.



$$T(s) = K \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)}$$

Series coupling capacitor circuit

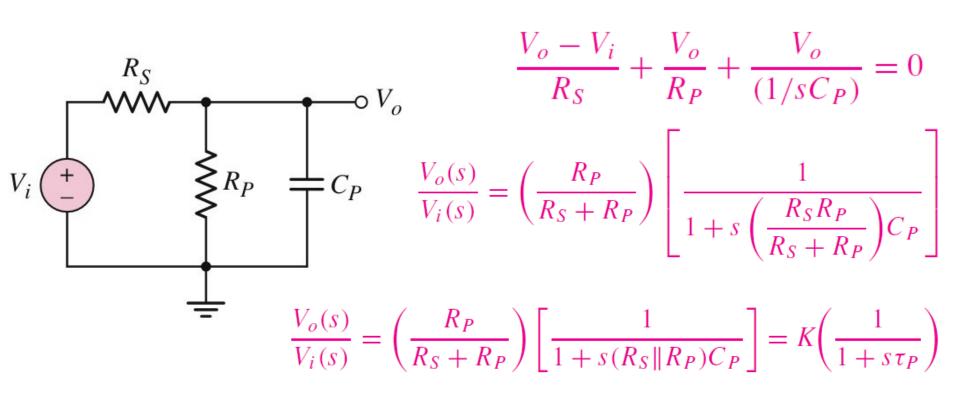


$$\frac{V_o(s)}{V_i(s)} = \frac{R_P}{R_S + R_P + \frac{1}{sC_S}}$$
$$\frac{V_o(s)}{V_i(s)} = \frac{sR_PC_S}{1 + s(R_S + R_P)C_S}$$

$$\frac{V_o(s)}{V_i(s)} = \left(\frac{R_P}{R_S + R_P}\right) \left[\frac{s(R_S + R_P)C_S}{1 + s(R_S + R_P)C_S}\right] = K\left(\frac{s\tau_s}{1 + s\tau_s}\right)$$

$$\tau_S = (R_S + R_P)C_S$$
Time constant

Parallel load capacitor circuit

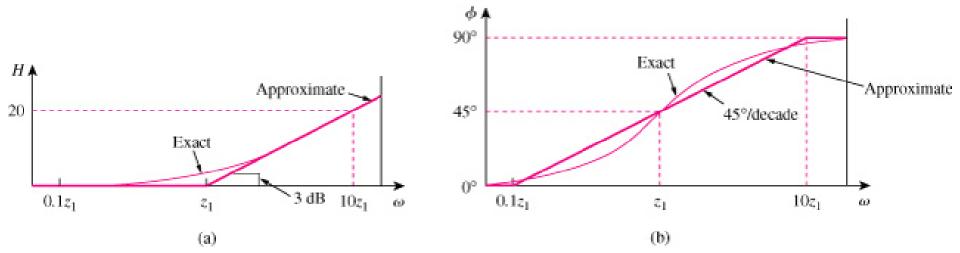


$$\tau_P = (R_S || R_P) C_P$$
Time constant

Bode plots

Approximate plots of the amplitude and phase of the transfer functions.

Semilog plots of the magnitude (in Decibels) and phase (in degrees) of a transfer function versus frequency.



Bode plots (approximate) and exact plots of the amplitude and phase of a generic transfer function $H(\omega)$.

How to sketch the Bode Plots

1. Put the transfer function in STANDARD FORM.

$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - \omega/z_2) \cdots (1 - \omega/z_m)}{(1 - \omega/p_1)(1 - \omega/p_2) \cdots (1 - \omega/p_n)}$$

- 2. Write the magnitude and phase equations from the STANDARD FORM.
- 3. Plot the magnitude (in dB) of each term separately.
- 4. Add all magnitude terms to obtain the magnitude transfer function.
- 5. Repeat 2-4 for the phase response.
- 6. The total magnitude response in Decibel units is the combination of the responses of different terms.
- 7. The total phase response in degrees is the summation and subtraction of the phase responses of different terms.

Next, we will examine how to plot different terms that may appear in a transfer function, such as K, $(s-z_i)$, and $(s-p_i)$.

Transfer function in s

$$T(s) = K \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)}$$

Transfer function in ω (Obtained from T(s) by setting s=j ω)

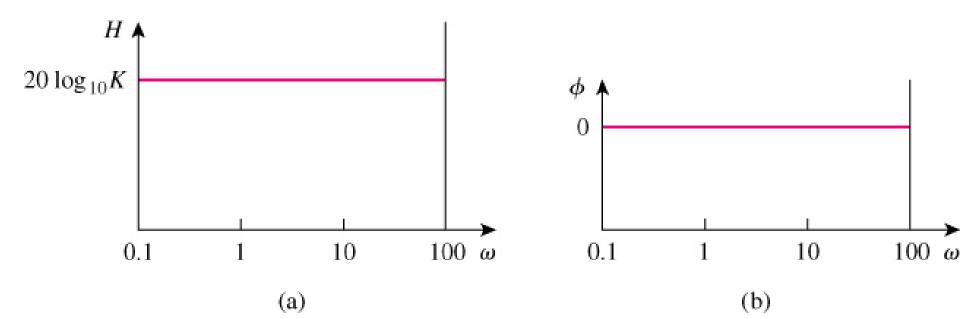
$$T(j\omega) = K \frac{(j\omega - z_1)(j\omega - z_2) \cdot \cdots \cdot (j\omega - z_m)}{(j\omega - p_1)(j\omega - p_2) \cdot \cdots \cdot (j\omega - p_n)}$$

$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - j\omega/z_2) \cdots (1 - j\omega/z_m)}{(1 - j\omega/p_1)(1 - j\omega/p_2) \cdots (1 - j\omega/p_n)}$$

Standard form of the transfer function

The constant term, K

$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - j\omega/z_2) \cdots (1 - j\omega/z_m)}{(1 - j\omega/p_1)(1 - j\omega/p_2) \cdots (1 - j\omega/p_n)}$$

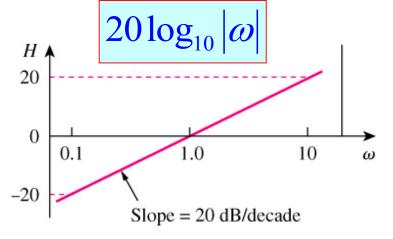


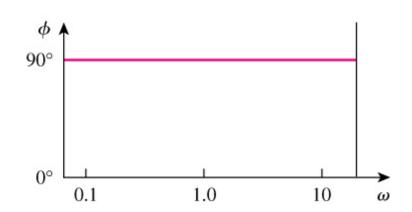
$$A + jB = Ke^{j\theta}$$
, where $K = \sqrt{A^2 + B^2}$ and $\theta = \tan^{-1}(B/A)$

Zeros-Zero at the origin (i.e., $z_1=0$)

$$T(j\omega) = K \frac{(j\omega)(1-j\omega/z_2) \cdots (1-j\omega/z_m)}{(1-j\omega/p_1)(1-j\omega/p_2) \cdots (1-j\omega/p_n)}$$

$$|j\omega| = \sqrt{0 + \omega^2} = \omega \quad \phi = \tan^{-1}\frac{\omega}{0} = 90^{\circ}$$





$$A + jB = Ke^{j\theta}$$
, where $K = \sqrt{A^2 + B^2}$ and $\theta = \tan^{-1}(B/A)$

Zeros-Simple zero not at the origin

$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - j\omega/z_2) \cdot \cdots \cdot (1 - j\omega/z_m)}{(1 - j\omega/p_1)(1 - j\omega/p_2) \cdot \cdots \cdot (1 - j\omega/p_n)}$$
$$20log_{10}|1 - \omega/z_1| \qquad \qquad \phi = \tan^{-1}\frac{\omega}{z_1}$$

Approximate the magnitude response of a simple zero by two linear curves before and after $\omega=z_1$

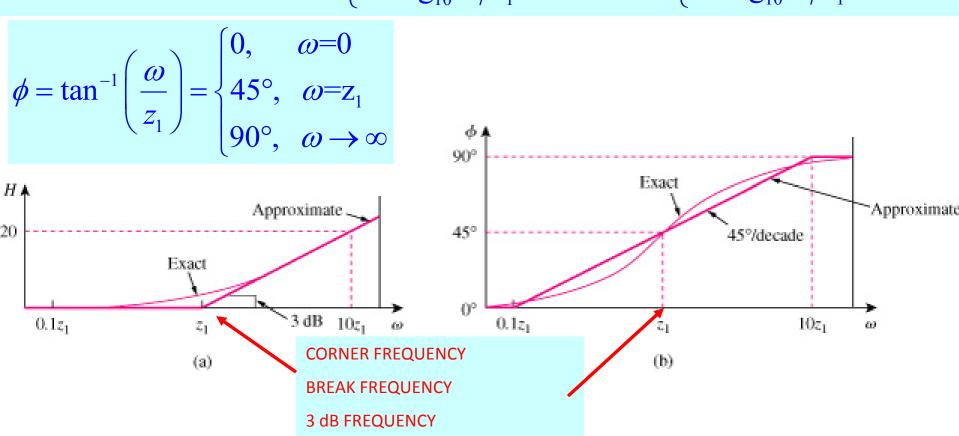
Approximate the phase response of a simple zero by three linear curves before $\omega=0.1z_1$ after $\omega=10z_1$ and between $\omega=0.1z_1$ and $\omega=10z_1$

$$H_{dB} = 20\log_{10}|1 - j\omega/z_1| = \begin{cases} 20\log_{10}1 = 0 & \omega \to 0 \\ 20\log_{10}\omega/z_1 & \omega \to \infty \end{cases} \approx \begin{cases} 0 \text{ dB} & \omega \le 0 \\ 20\log_{10}\omega/z_1 & \omega \ge 0 \end{cases}$$

$$\phi = \tan^{-1} \left(\frac{\omega}{z_1} \right) = \begin{cases} 0, & \omega = 0 \\ 45^{\circ}, & \omega = z_1 \\ 90^{\circ}, & \omega \to \infty \end{cases}$$

Zeros-Simple zero not at the origin

$$H_{dB} = 20\log_{10}|1 - j\omega/z_1| = \begin{cases} 20\log_{10}1 = 0 & \omega \to 0 \\ 20\log_{10}\omega/z_1 & \omega \to \infty \end{cases} \approx \begin{cases} 0 \text{ dB} & \omega \le 0 \\ 20\log_{10}\omega/z_1 & \omega \ge 0 \end{cases}$$



Poles-Pole at the origin (i.e., z1=0)

$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - \omega j/z_2) \cdots (1 - j\omega/z_m)}{(j\omega)(1 - j\omega/p_2) \cdots (1 - j\omega/p_n)}$$

$$20log_{10}|1/(j\omega)| = -20log_{10}|(j\omega)|$$

$$|j\omega| = \sqrt{0 + \omega^2} = \omega$$

$$-20log_{10}(\omega)$$

$$\omega$$

$$-20N dB/decade$$

$$-90N^{\circ}$$

 $A + jB = Ke^{j\theta}$, where $K = \sqrt{A^2 + B^2}$ and $\theta = \tan^{-1}(B/A)$

Poles-Simple pole not at the origin

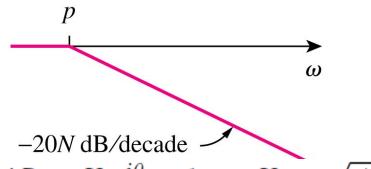
$$T(j\omega) = K \frac{(1 - j\omega/z_1)(1 - j\omega/z_2) \cdots (1 - j\omega/z_m)}{(1 - j\omega/p_1)(1 - j\omega/p_2) \cdots (1 - j\omega/p_n)}$$

Approximate the magnitude response of a simple zero by two linear curves before and after $\omega = z_1$

Approximate the phase response of a simple zero by three linear curves before ω =0.1z₁ after ω =10z₁ and between ω =0.1z₁ and ω =10z₁

$$20log_{10} \left| \frac{1}{1 - \frac{\omega}{p_1}} \right| = -20log_{10} \left| 1 - \frac{\omega}{p_1} \right| \qquad \phi = -\tan^{-1} \left(\frac{\omega}{p_1} \right) = \begin{cases} 0, & \omega = 0 \\ -45^{\circ}, & \omega = p_1 \\ -90^{\circ}, & \omega \to \infty \end{cases}$$

$$\phi = -\tan^{-1}\left(\frac{\omega}{p_1}\right) = \begin{cases} 0, & \omega = 0\\ -45^{\circ}, & \omega = p_1\\ -90^{\circ}, & \omega \to \infty \end{cases}$$



$$\frac{p}{10} \qquad p \qquad 10p$$

$$0^{\circ} \qquad \omega$$

 $A + jB = Ke^{j\theta}$, where $K = \sqrt{A^2 + B^2}$ and $\theta = \tan^{-1}(B/A)$ $-90N^{\circ}$

How to sketch the Bode Plots

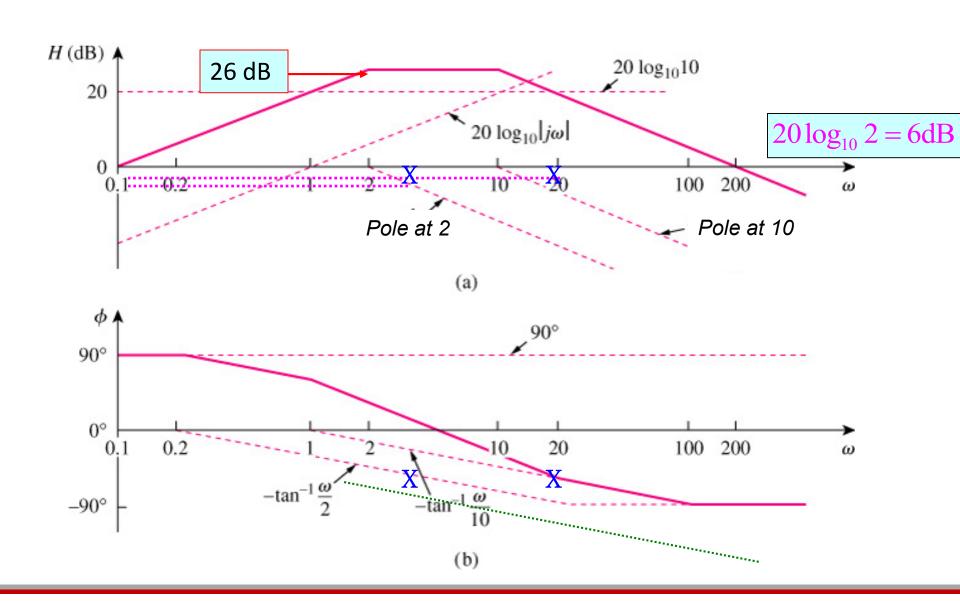
- 1) Draw the line of each individual term of the transfer function on the graph
- 2) Follow the combined gain-pole-zero at the origin line back to the left side of the graph.
- 3) Add the constant offset, 20 log10(K), to the value where the pole/zero at the origin line intersects the left side of the graph.
- 4) Apply the effect of the poles/zeros not at the origin working from left (low values) to right (higher values) of the poles/zeros.

Problem 1

Sketch the Bode Plots for the transfer function below

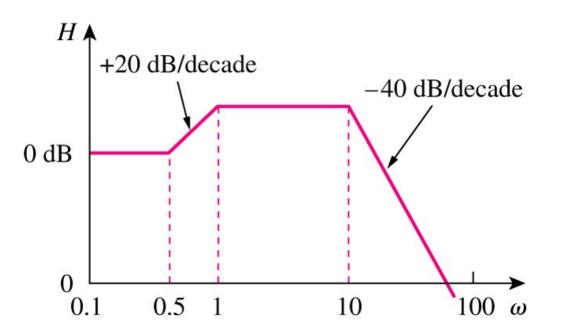
$$H(\omega) = \frac{200j\omega}{(j\omega - 2)(j\omega - 10)}$$

Problem 1, solution



Problem 2

Obtain the transfer function for the Bode plot given.



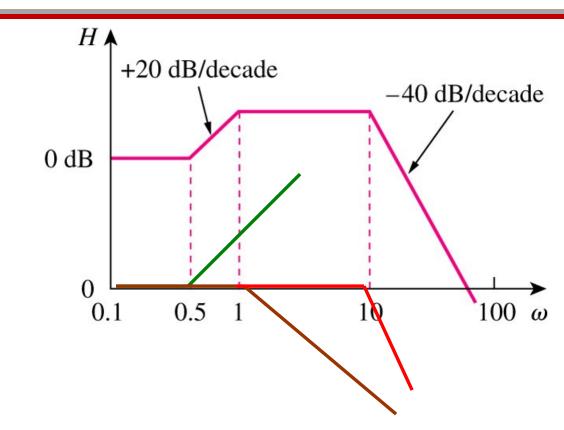
Problem 2, solution

Obtain the transfer function for the given Bode plot.

Hint: The transfer function has no zeros or poles in the origin.

A zero at
$$\omega = 0.5$$
, $1 + i\omega/0.5$

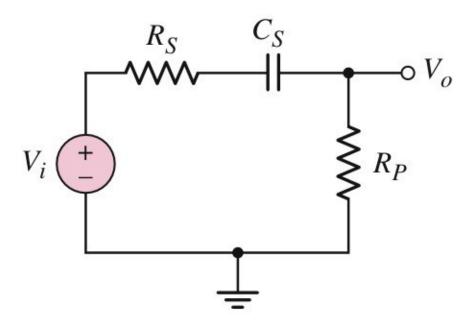
A pole at
$$\omega = 1$$
, $\frac{1}{1 + j\omega/1}$



Two poles at
$$\omega = 10$$
, $\frac{1}{(1+j\omega/10)^2}$

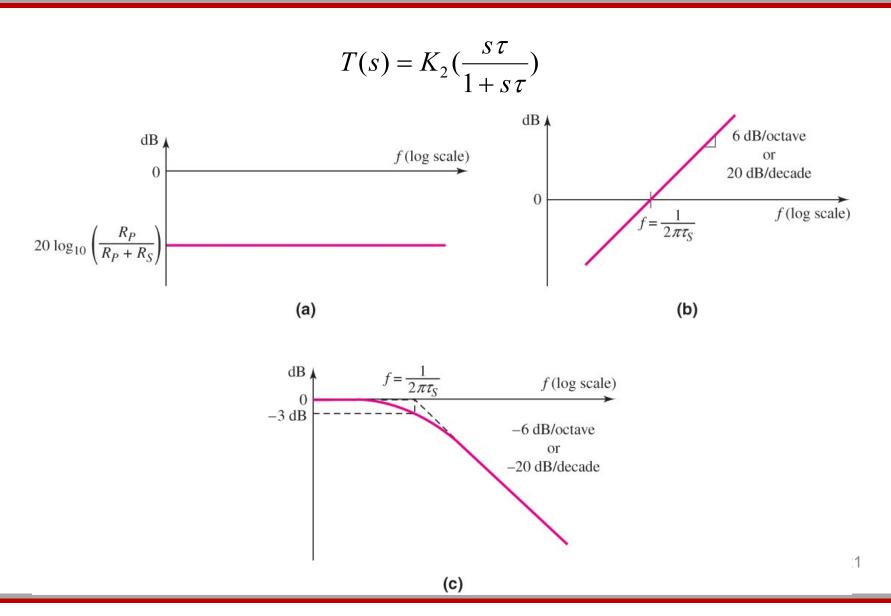
$$H(\omega) = \frac{1 + j\omega/0.5}{(1 + j\omega/1)(1 + j\omega/10)^2} = \frac{(1/0.5)(0.5 + j\omega)}{(1/100)(1 + j\omega)(10 + j\omega)^2} = \frac{200(s + 0.5)}{(s + 1)(s + 10)^2}$$

Series coupling capacitor circuit

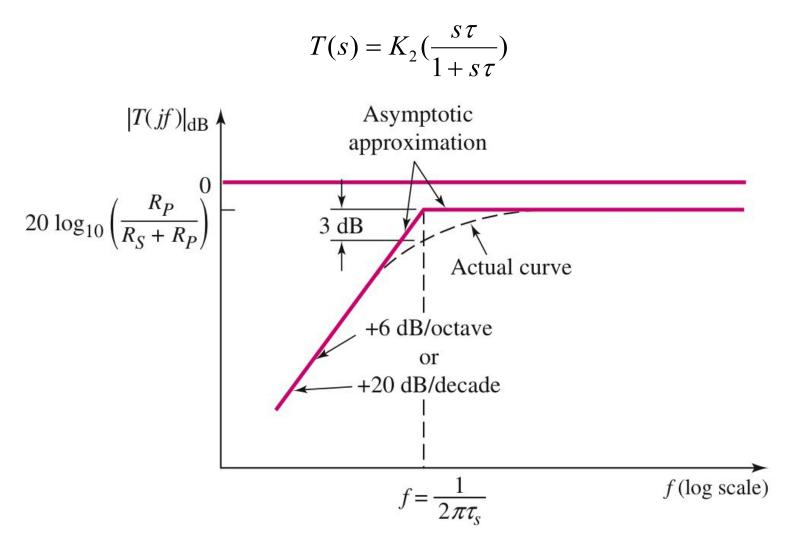


$$\frac{V_o(s)}{V_i(s)} = \left(\frac{R_P}{R_S + R_P}\right) \left[\frac{s(R_S + R_P)C_S}{1 + s(R_S + R_P)C_S}\right] = K\left(\frac{s\tau_s}{1 + s\tau_s}\right)$$

Series coupling capacitor circuit-Bode plot



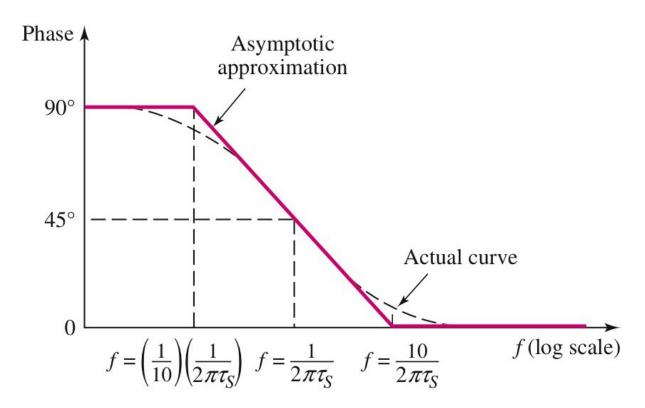
Series coupling capacitor circuit-Bode plot



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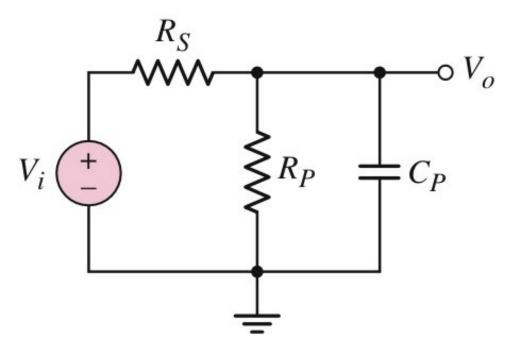
Series coupling capacitor circuit-Bode plots

$$T(s) = K_2(\frac{s\tau}{1 + s\tau})$$



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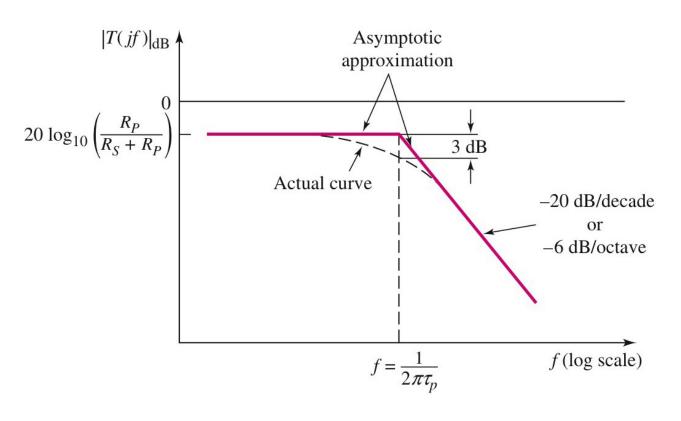
Parallel load capacitor circuit



$$\frac{V_o(s)}{V_i(s)} = \left(\frac{R_P}{R_S + R_P}\right) \left[\frac{1}{1 + s(R_S || R_P)C_P}\right] = K\left(\frac{1}{1 + s\tau_P}\right)$$

$$\tau_P = (R_S || R_P) C_P$$
Time constant

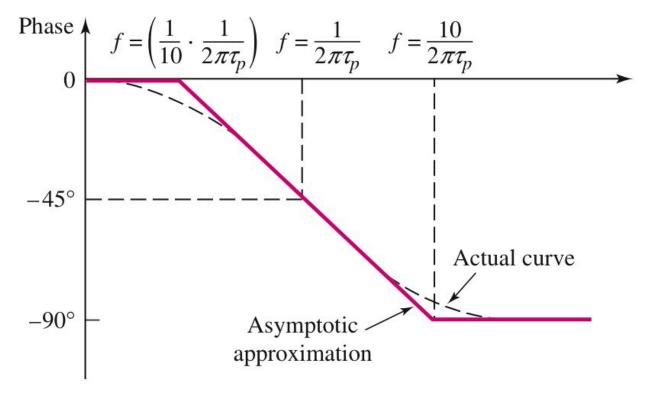
Parallel load capacitor circuit-Bode plots



$$\frac{V_o(s)}{V_i(s)} = \left(\frac{R_P}{R_S + R_P}\right) \left[\frac{1}{1 + s(R_S || R_P)C_P}\right] = K\left(\frac{1}{1 + s\tau_P}\right)$$

$$\tau_P = (R_S || R_P)C_P$$
Time constant

Parallel load capacitor circuit-Bode plots



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$$\frac{V_o(s)}{V_i(s)} = \left(\frac{R_P}{R_S + R_P}\right) \left[\frac{1}{1 + s(R_S || R_P)C_P}\right] = K\left(\frac{1}{1 + s\tau_P}\right)$$

$$\tau_P = (R_S || R_P)C_P$$
Time constant