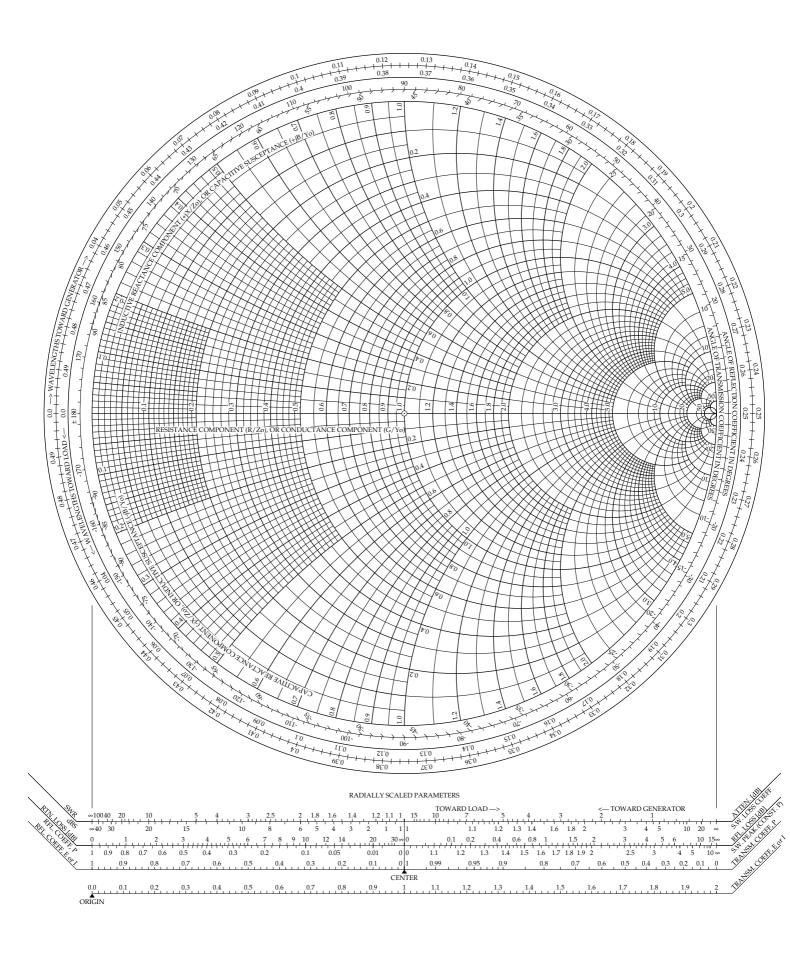
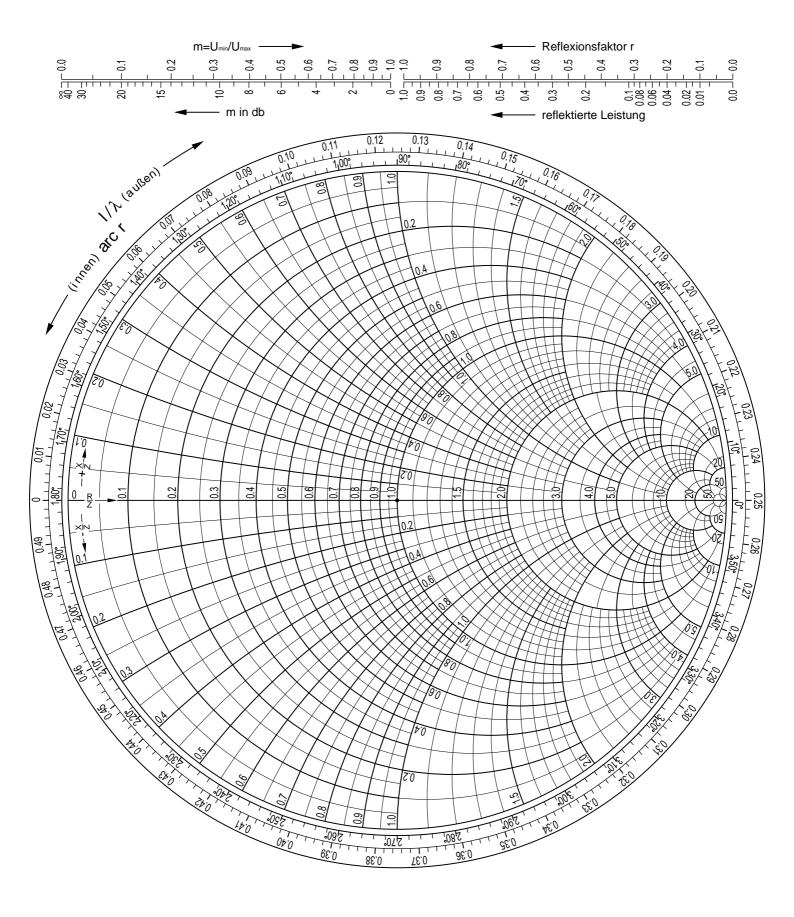
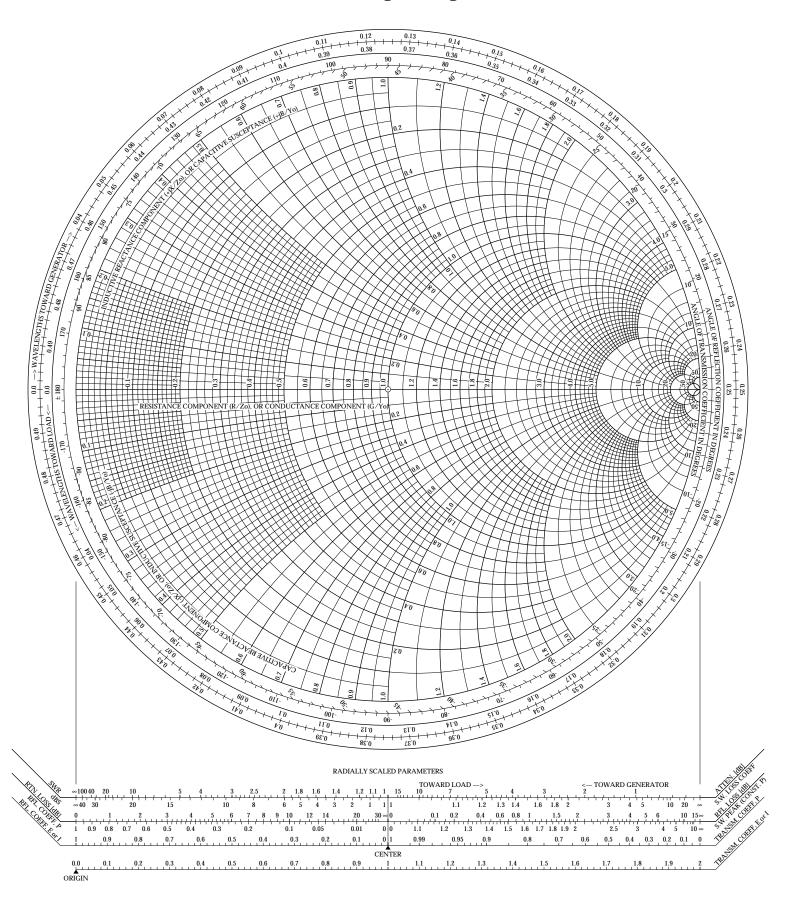
## **The Complete Smith Chart**





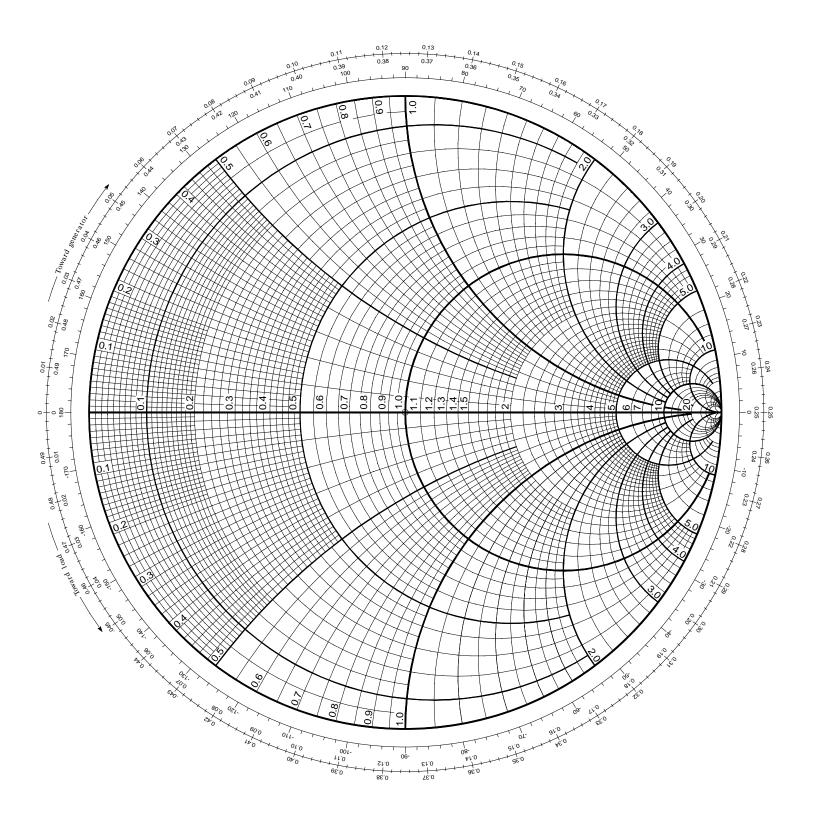
## **The Complete Smith Chart**

Black Magic Design



Name:	Smith-Diagramm (Widerstandsform)	Zu Aufgabe Nr.:	Bezugswellen- widerstand Z <sub>B</sub> =
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100 000 000 000 000 000 000 000 000 000	0.10 100° 100° 180° 180° 180° 180° 180° 18		100 024 025 026 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 027 028 028 028 028 028 028 028 028 028 028

## **Smith Chart**



## **Using the Smith Chart**

First **normalize the load** impedance by dividing by the characteristic impedance, and find this point on the chart.

When working in terms of **reactance**, an **inductive load** will be located on the top half of the chart, a **capacitive load** on the bottom half. It's the other way around when working in terms of **susceptance**.

Draw a **straight line** from the center of the chart through the normalized load impedance point to the edge of the chart.

Anchor a compass at the center of the chart and **draw a circle** passing through the normalized load impedance point. Points along this circle represent the normalized impedance at various points along the transmission line. **Clockwise movement** along the circle represents movement from the load toward the source, with one full revolution representing **1/2 wavelength** as marked on the outer edge of the Smith chart. The two points where the circle intersects the horizontal axis are the **voltage maxima** (right) and the **voltage minima** (left).

The point opposite the **impedance** (180° around the arc) is the **admittance**. The reason admittance (or susceptance) is useful is because admittances in parallel are simply added. (Admittance is the reciprocal of impedance; susceptance is the reciprocal of reactance.)

Reflection coefficient:

$$\rho = \frac{Z - Z_0}{Z + Z_0} = \underbrace{\frac{r + j \cdot x - 1}{r + j \cdot x + 1}}_{\text{normalized form}}$$

$$\underbrace{r_{\text{eal}}}_{\text{real}} + \underbrace{j \cdot x}_{\text{imag.}} = \underbrace{\frac{1 - \left(u^2 + v^2\right)}{\left(1 - u\right)^2 + v^2}}_{\text{real}} + \underbrace{j \cdot \frac{2 \cdot v}{\left(1 - u\right)^2 + v^2}}_{\text{imaginary}}$$

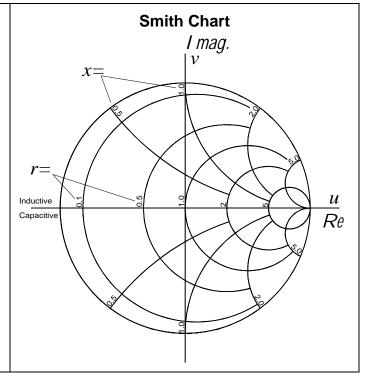
Reflection coefficient in the complex plane:  $\rho = u + j \cdot v$ 

Normalized load impedance:

$$R_{L(norm)} = \frac{1+\rho}{1+\rho} = r + j \cdot x$$

Input impedance:

$$Z_{in} = Z_0 \frac{1+\rho}{1-\rho} = Z_0 \frac{Z_L + jZ_0 \tan(\beta l)}{Z_0 + jZ_L \tan(\beta l)}$$
where  $\beta \lambda = 2\pi$ 



The u and v axes are normally not shown on the Smith Chart. With respect to these axes,  $\rho$  is zero when at the origin and one when on the outer circle. The distance from  $\rho$  to the origin in the magnitude of  $\rho$ . If  $\rho$  is greater than one, that means there is gain.

Using the Smith chart, we assume  $\alpha=0$ , otherwise the circular path taken around the chart would be a spiral.  $\alpha$  is the real part of the **complex propagation constant**  $\gamma$  where  $\gamma = \sqrt{ZY} = \alpha + j\beta$  and  $\beta\lambda = 2\pi$ .

