

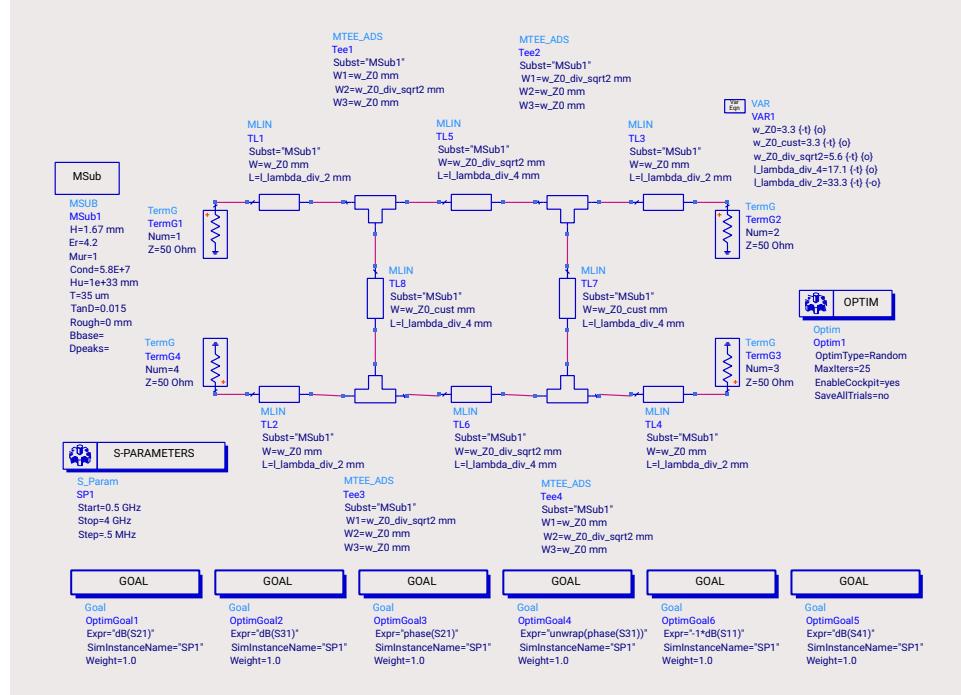
# Design Status Report

## EENG530 Final Project Group 3

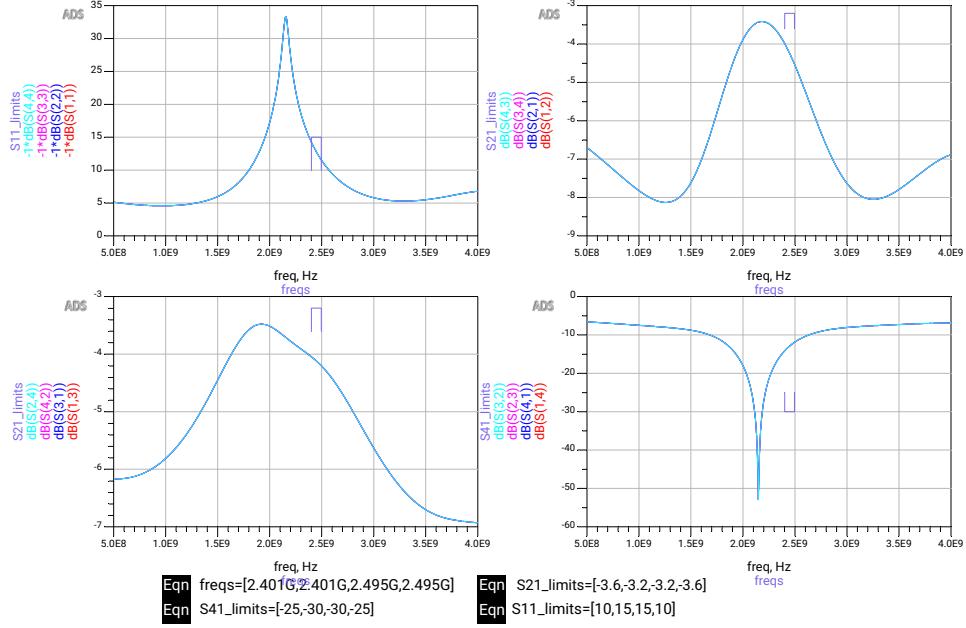
Names: Jacob Hulvey, Jack Mullen, Dawit Yerdeea

### 90 Degree Branchline Hybrid Coupler:

- We have started tuning/optimizing the implemented microstrip lines but are struggling to meet the required specifications over the full bandwidth.
- Schematic with optimizer and goals:



- Responses with Goals:



### 90 Degree 20dB coupled-line Coupler:

- We are currently calculating even and odd impedance values and implementing these values within the linecalc tool to achieve the desired effect.
- From here, the plan is to continue tuning dimensional values with the optimization tool to achieve the most ideal effect.
- We are currently a little bit hung up on getting the ideal response from the linecalc output values.

$$\begin{aligned}
 20\text{dB} \quad C \rightarrow & \quad -20\text{dB} = 20 \log |S_{31}| \\
 & |S_{31}| = 0.01 = |C| \\
 |C| = \frac{|Z_C - Z_0|}{|Z_C + Z_0|} \rightarrow & \quad Z_0 = Z_C \cdot \frac{1+C}{1-C} = Z_C \cdot 0.818182 \\
 Z_C = \sqrt{Z_0 Z_0} \rightarrow & \quad Z_C = \sqrt{\frac{1+C}{1-C}} Z_0 = 55.2770798 \\
 Z_0 = 45.767079
 \end{aligned}$$

**LineCalc/untitled**

File Simulation Options Help

Component

Type MCLIN ID MClin: CLin1

Substrate Parameters

|      |              |
|------|--------------|
| ID   | MSub1        |
| H    | 1.67 mm      |
| Er   | 4.2 N/A      |
| Mur  | 1 N/A        |
| Cond | 58000000 N/A |
| Hu   | 1e+33 mm     |
| T    | 35 um        |

Physical

|   |              |
|---|--------------|
| W | 3.218250 mm  |
| S | 2.206810 mm  |
| L | 17.174700 mm |
|   | N/A          |

Synthesize Analyze

Calculated Results

KE = 3.43507  
KO = 2.93044  
AE\_DB = 0.105124  
AO\_DB = 0.0920873  
SkinDepth = 0.052585

Values are consistent

**LineCalc/untitled**

File Simulation Options Help

Component

Type MLIN ID MLIN: TL1

Substrate Parameters

|      |              |
|------|--------------|
| ID   | MSub1        |
| H    | 1.67 mm      |
| Er   | 4.2 N/A      |
| Mur  | 1 N/A        |
| Cond | 58000000 N/A |
| Hu   | 1e+33 mm     |
| T    | 35 um        |

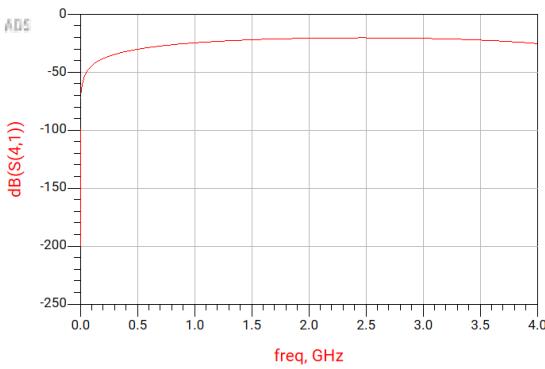
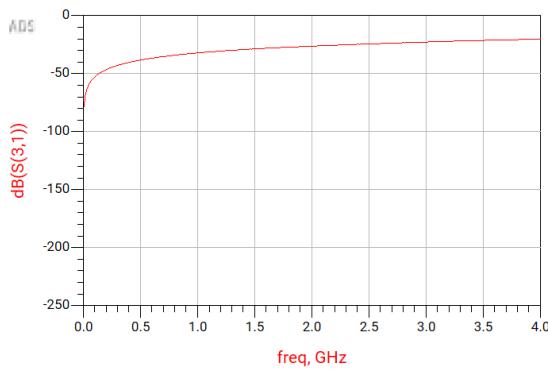
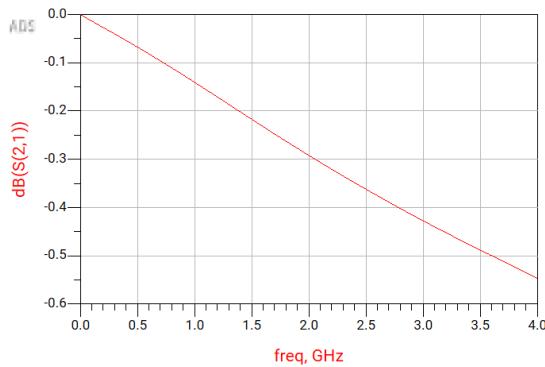
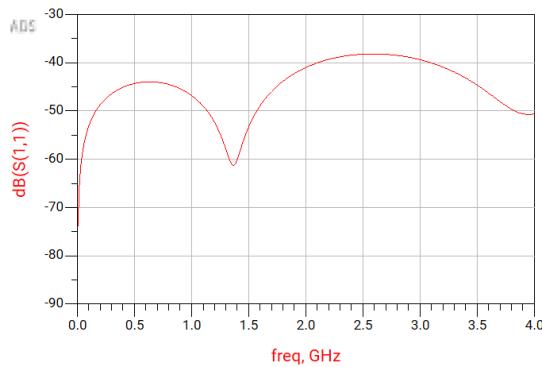
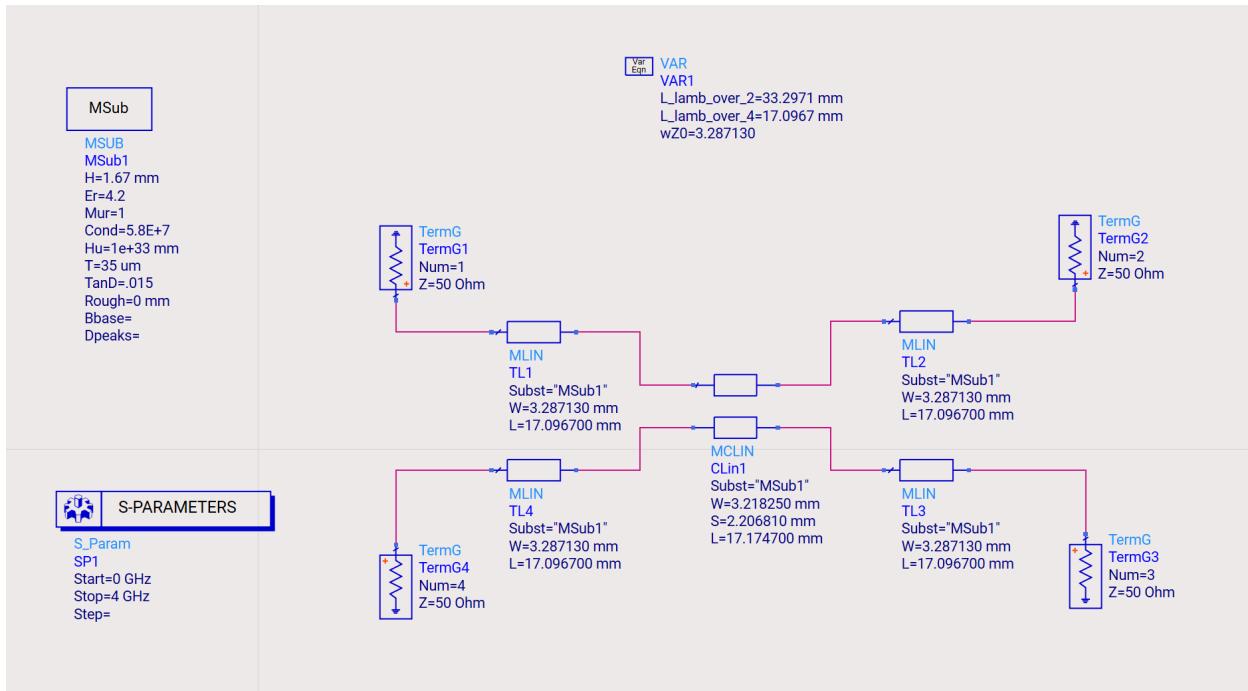
Physical

|   |              |
|---|--------------|
| W | 3.287130 mm  |
| L | 17.096700 mm |
|   | N/A          |
|   | N/A          |

Synthesize Analyze

Calculated Results

K\_Eff = 3.20682  
A\_DB = 0.0988891  
SkinDepth = 0.052585



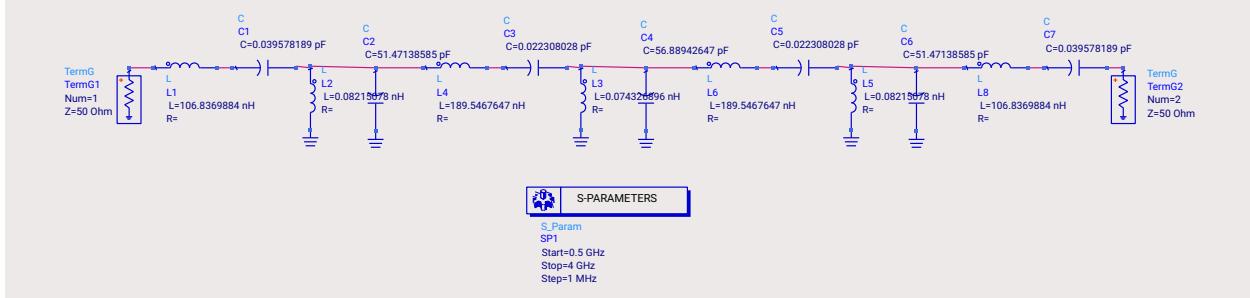
## Chebyshev Bandpass Filter:

- We are currently trying to convert an ideal bandpass filter to a stepped impedance or open stub bandpass filter.
  - We have found a Chebyshev table with passband ripple of  $0.1\text{ dB}$  (see below). We are going to use this level of passband ripple because the filter will not work as well when we round to  $0.1\text{ mm}$  increments due to manufacturing limitation.

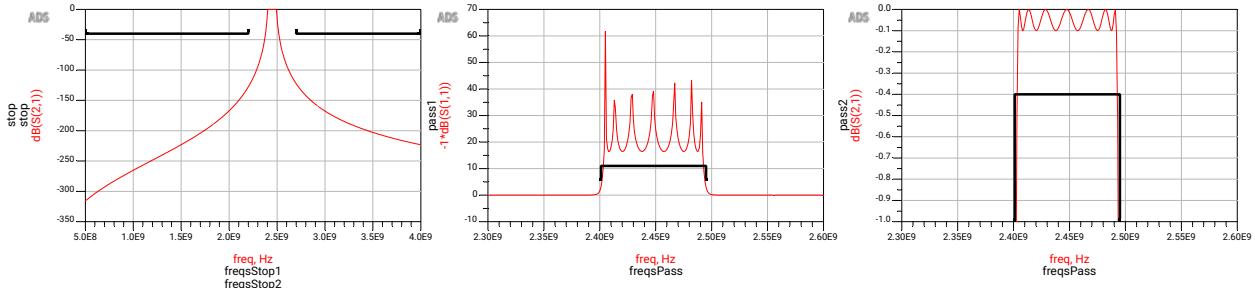
|   | $R_S/R_L$ | $C_1$ | $L_2$  | $C_3$  | $L_4$  | $C_5$  | $L_6$  | $C_7$  |
|---|-----------|-------|--------|--------|--------|--------|--------|--------|
| 5 | 1.000     | 1.301 | 1.556  | 2.241  | 1.556  | 1.301  |        |        |
|   | 0.900     | 1.285 | 1.433  | 2.380  | 1.488  | 1.488  |        |        |
|   | 0.800     | 1.300 | 1.282  | 2.582  | 1.382  | 1.738  |        |        |
|   | 0.700     | 1.358 | 1.117  | 2.868  | 1.244  | 2.062  |        |        |
|   | 0.600     | 1.470 | 0.947  | 3.269  | 1.085  | 2.494  |        |        |
|   | 0.500     | 1.654 | 0.778  | 3.845  | 0.913  | 3.055  |        |        |
|   | 0.400     | 1.954 | 0.612  | 4.720  | 0.733  | 3.886  |        |        |
|   | 0.300     | 2.477 | 0.451  | 6.196  | 0.550  | 5.237  |        |        |
|   | 0.200     | 3.546 | 0.295  | 9.127  | 0.366  | 7.889  |        |        |
|   | 0.100     | 6.787 | 0.115  | 17.957 | 0.182  | 15.745 |        |        |
|   | $\infty$  | 1.581 | 1.807  | 1.766  | 1.417  | 0.651  |        |        |
| 6 | 1.355     | 0.942 | 2.080  | 1.659  | 2.247  | 1.534  | 1.277  |        |
|   | 1.429     | 0.735 | 2.249  | 1.454  | 2.544  | 1.405  | 1.029  |        |
|   | 1.687     | 0.542 | 2.600  | 1.183  | 3.064  | 1.185  | 2.174  |        |
|   | 2.000     | 0.414 | 3.068  | 0.958  | 3.712  | 0.979  | 2.794  |        |
|   | 2.500     | 0.310 | 3.765  | 0.749  | 4.651  | 0.778  | 3.645  |        |
|   | 3.333     | 0.220 | 4.927  | 0.551  | 6.195  | 0.580  | 4.996  |        |
|   | 5.000     | 0.139 | 7.250  | 0.361  | 9.261  | 0.384  | 7.618  |        |
|   | 10.000    | 0.067 | 14.220 | 0.178  | 18.427 | 0.190  | 15.350 |        |
|   | $\infty$  | 1.534 | 1.884  | 1.831  | 1.749  | 1.394  | 0.638  |        |
| 7 | 1.000     | 1.262 | 1.520  | 2.239  | 1.680  | 2.239  | 1.520  | 1.262  |
|   | 0.900     | 1.242 | 1.395  | 2.361  | 1.578  | 2.397  | 1.459  | 1.447  |
|   | 0.800     | 1.255 | 1.245  | 2.548  | 1.443  | 2.624  | 1.362  | 1.697  |
|   | 0.700     | 1.310 | 1.083  | 2.819  | 1.283  | 2.942  | 1.233  | 2.021  |
|   | 0.600     | 1.417 | 0.917  | 3.205  | 1.209  | 3.384  | 1.081  | 2.444  |
|   | 0.500     | 1.595 | 0.753  | 3.764  | 0.928  | 4.015  | 0.914  | 3.018  |
|   | 0.400     | 1.885 | 0.593  | 4.618  | 0.742  | 4.970  | 0.738  | 3.855  |
|   | 0.300     | 2.392 | 0.437  | 6.054  | 0.556  | 6.569  | 0.557  | 5.217  |
|   | 0.200     | 3.428 | 0.286  | 8.937  | 0.369  | 9.770  | 0.372  | 7.890  |
|   | 0.100     | 6.570 | 0.141  | 17.603 | 0.184  | 19.376 | 0.180  | 15.813 |
|   | $\infty$  | 1.575 | 1.858  | 1.921  | 1.827  | 1.734  | 1.379  | 0.631  |
| n | $R_S/R_L$ | $L_1$ | $C_2$  | $L_3$  | $C_4$  | $L_5$  | $C_6$  | $L_7$  |
|   |           | $R_S$ | $L_1$  | $L_2$  | $L_3$  | $L_4$  | $C_5$  | $L_6$  |

- Using the 7<sup>th</sup> order filter coefficients above we converted to real lumped element capacitance and inductance:

- Then we implemented the values as lumped elements. Lumped Element Schematic:



- Lumped Element Simulation results and constraints:



- We are currently trying an open stub bandpass filter using the following testing schematic (values have not yet been updated):

