

# Homework 7

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## Problem 1

We first introduced the notion of impulse response in Chapter 1, and here in Chapter 5 we discussed the importance of knowing the impulse response of FIR filter networks. With that said, if the  $y(n)$  output of a discrete system is equal to the system's  $x(n)$  input sequence:

- (a) Draw the unit impulse response of such a system.
- (b) Draw the block diagram (structure) of that system.
- (c) What is the frequency magnitude response of such a system? Prove your answer

**Answer:**

A)  $y[n] = T\{x[n]\}$

$x[n] \rightarrow \boxed{T\{\}} \rightarrow y[n]$

$y[n] = \sum_{k=m_1}^{m_2} b_k x[n-k]$

example

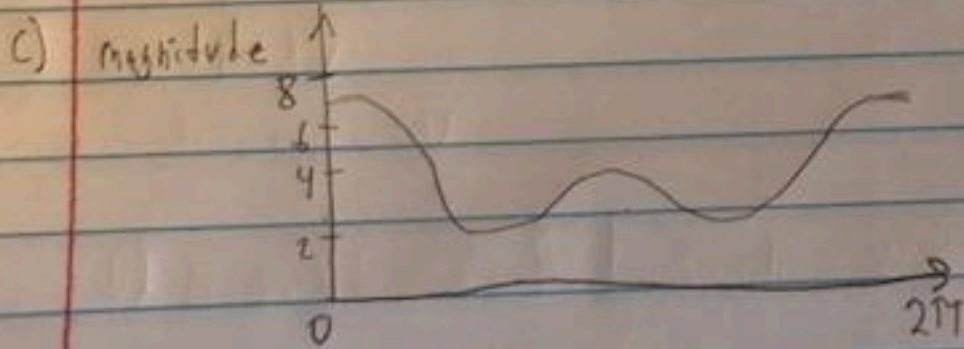
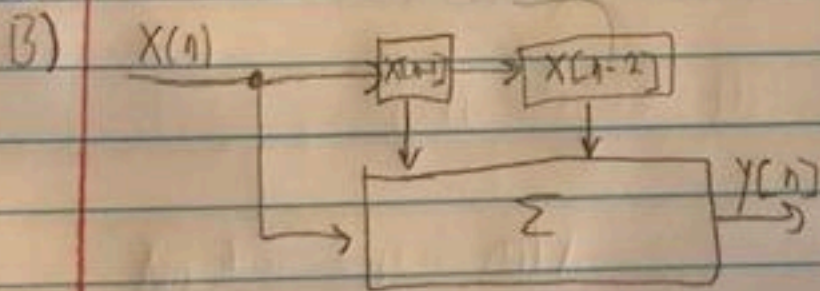
$y[n] = \{x[n]\}^3$

$= \min\{x[n], x[n-1], x[n-2]\}$

$= x[n] - x[n-1]$

$= \frac{1}{2}[x[n] + x[n-1]]$

$m_1, m_2$  are finite



## Problem 2

Consider a simple analog signal defined by  $x(t) = \cos(2\pi 800t)$  shown in Figure P5-2. The FIR lowpass filter has a passband extending from  $-400$  Hz to  $+400$  Hz, a passband gain of unity, a transition region width of  $20$  Hz, and a stopband attenuation of  $60$  dB.

- Draw the spectral magnitude of  $x(n)$  showing all spectral components in the range of  $-2f_s$  to  $+2f_s$ .
- Draw the spectral magnitude of  $y(n)$  showing all spectral components in the range of  $-2f_s$  to  $+2f_s$ .
- What is the time-domain peak amplitude of the sinusoidal  $y(n)$  output?

**Answer:**

```
fs = 1000; %sampling speed
t=0:1/1:fs

x= cos(2*pi*800*t);
fpass= 400;

lowpass(x,fpass,fs);
```

A)

```
lowpass(x,fpass,2000);
```

B)

```
lowpass(x,fpass,2000);
```

C) 1.082 is the peak domain amplitude

### Problem 3

Assume we want to filter the audio signal from a digital video disc (DVD) player as shown in Figure P5-3. The filtered audio signal drives, by way of a digital-to-analog (D/A) converter, a speaker. For the audio signal to have acceptable time synchronization with the video signal, video engineers have determined that the time delay of the filter must be no greater than  $6 \times 10^{-3}$  seconds. If the  $f_s$  sample rate of the audio is  $48$  kHz, what is the maximum number of taps in the FIR filter that will satisfy the time delay restriction? (Assume a linear-phase FIR filter, and zero time delay through the D/A converter.)

**Answer:**

$$\frac{1}{2}(x - 1) = (6 * 10^{-3}) * 48000$$

$$x - 1 = 576$$

$$x = 577$$

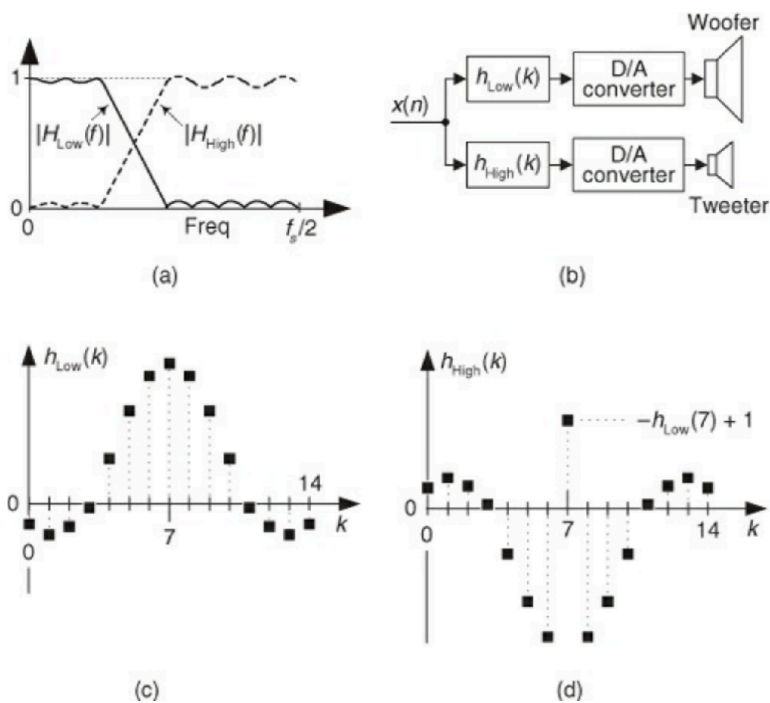
The maximum number of taps is 577

## Problem 4

There are times when we want to build a lowpass filter and a highpass filter that are complementary. By “complementary” we mean that a highpass filter’s passband covers the frequency range defined by a lowpass filter’s stopband range. This idea is illustrated in Figure P5- 4(a). An example of such filters is an audio system, shown in Figure P5-4(b), where the lowfrequency spectral components of an  $x(n)$  audio signal drive, by way of a digital-to-analog (D/A) converter, a low-frequency speaker (woofer). Likewise, the high-frequency spectral components of  $x(n)$  drive a high-frequency speaker (tweeter). Audio enthusiasts call Figure P5-4(b) a “crossover” network. Assuming that the lowpass filter is implemented with a 15-tap FIR filter whose  $h_{\text{Low}}(k)$  coefficients are those in Figure P5-4(c), the complementary highpass filter will have the coefficients shown in Figure P5-4(d). Highpass coefficients  $h_{\text{High}}(k)$  are defined by

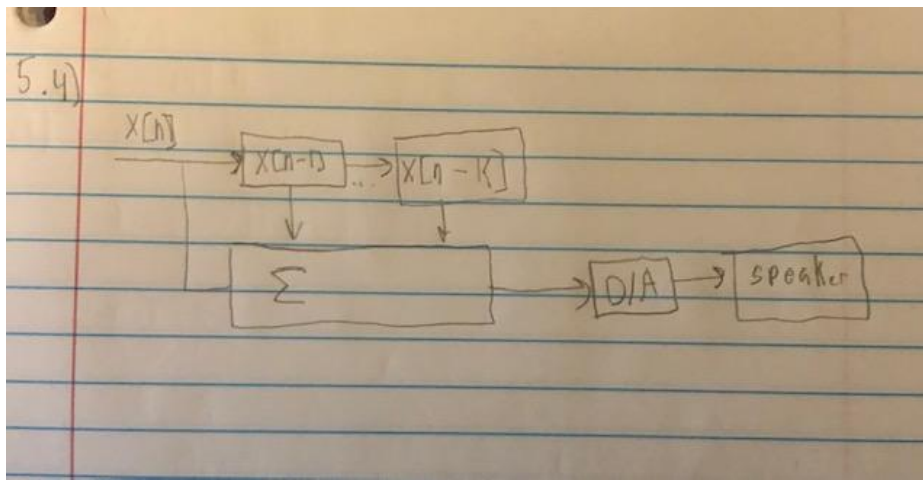
$$h_{\text{High}}(k) = \begin{cases} -h_{\text{Low}}(k), & \text{when } k \neq 7 \\ -h_{\text{Low}}(k) + 1, & \text{when } k = 7. \end{cases}$$

Figure P5-4



Here is the problem: Draw a block diagram of a system that performs the process in P5-4(b) where only the  $h_{\text{Low}}(k)$  lowpass FIR filter need be implemented.

**Answer:**



## Problem 5

Think about a discrete System A, shown in Figure P5-5, that has an undesirable amplitude (gain) loss by a factor 0.5 (−6 dB), whose output requires lowpass linear-phase filtering. What can we do in the design of the lowpass FIR filter so the filter has an amplitude gain of 2 to compensate for System A's amplitude loss?

**Answer:**

To compensate for system A's amplitude loss a lowpass FIR filter can be designed so the filter has an amplitude gain of 2.

$$y[n] = \sum_{k=N}^{M-1} h[k]x[n-k]$$

$$d[n] = \delta[n-1]$$

$$|y[n]| = |h[n] * x[n]|$$

from this you get

$$\left| \sum_{k=-\infty}^{\infty} h[k] * x[n-k] \right| \leq \sum_{k=-\infty}^{\infty} |h[k] * x[n-k]| \leq \sum_{k=-\infty}^{\infty} |h[k]|$$

The summation of the last term is finite if  $h[n]$  is absolutely summable if it is not absolutely summable consider the signal

$$x[n] = \sin(h[n])$$

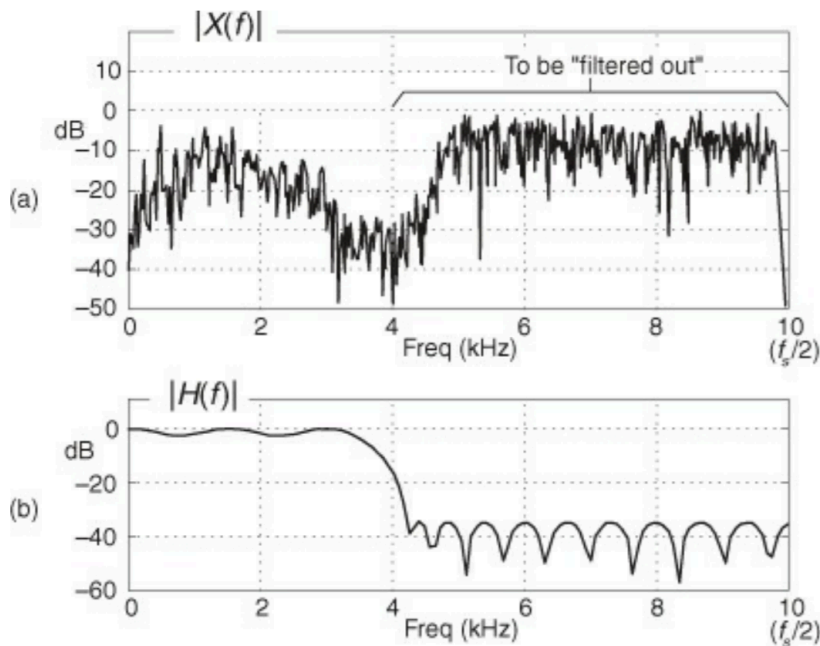
$x[n]$  is bounded since the only values it takes is -1,0,1

## Problem 6

Let's assume we have an  $x(n)$  time sequence, whose  $f_s$  sample rate is 20 kHz, and its  $|X(f)|$  spectral magnitude is that shown in Figure P5-6(a). We are required to design a linear-phase lowpass FIR filter that will attenuate the undesired high-frequency noise indicated in Figure P5-6(a). So we design a lowpass FIR filter whose

frequency magnitude response is the  $|H(f)|$  shown in Figure P5-6(b) and assume our filter design exercise is complete. Sometime later, unfortunately, we learn that the original  $x(n)$  sequence's sample rate was not 20 kHz, but is in fact 40 kHz

**Figure P5-6**



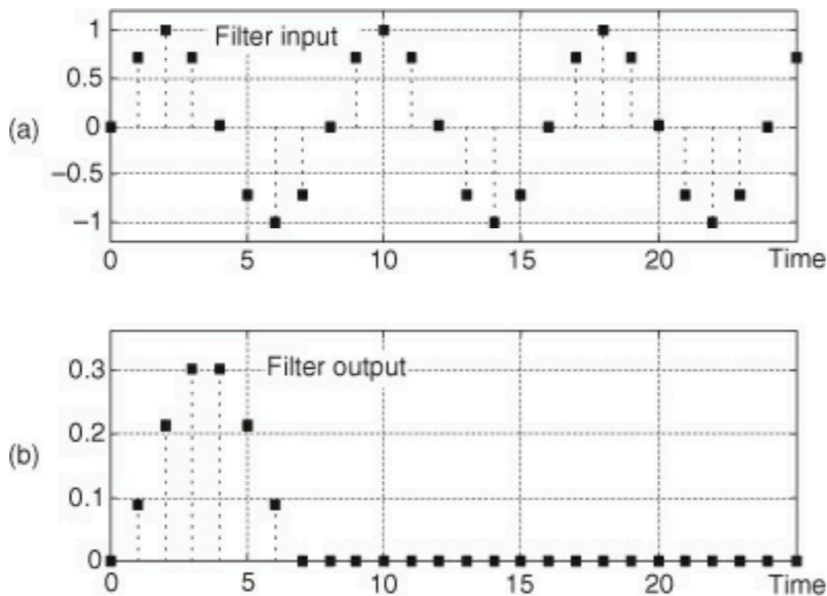
Here is the problem: What must we do to our lowpass filter's  $h(k)$  coefficients, originally designed based on a 20 kHz sample rate, so that they will still attenuate  $x(n)$ 's undesired high-frequency noise when the  $f_s$  sample rate is actually 40 kHz?

**Answer:**

For the lowpass filter to work the  $h(k)$  coefficient must be divided by 2 because 40kHz is double 20kHz.

## Problem 7

Here is an interesting little problem. Think about applying the sinusoidal input sequence shown in Figure P5-7(a) to an 8-point moving average FIR filter. The filter's output sequence is that depicted in Figure P5-7(b).



(a) What characteristic of the filter's frequency response causes the filter's output sequence to go to all zeros as shown in Figure P5-7(b)?

(b) In Figure P5-7(b), what do we call those initial nonzero-valued filter output samples?

**Answer:**

A) The magnitude response reached zero so the gain contribution of the moving average filter at this frequency is 0

B) The nonzero-valued filter output samples are called the transient response of the filter

## Problem 8

Are abrupt (sudden) changes in the amplitude of a continuous, or discrete, signal associated with low or high frequencies?

**Answer:**

Abrupt changes in the amplitude are associated with a high frequency

## Problem 9

Consider an FIR filter whose impulse response is shown in Figure P5-9(a). Given the  $x(n)$  filter input sequence shown in Figure P5-9(b):

(a) What is the length, measured in samples, of the nonzero-valued samples of the filter's output sequence?

(b) What is the maximum sample value of the filter's output sequence?

**Answers:**

A) The length of the nonzero-valued samples of the filter's output sequence is 5

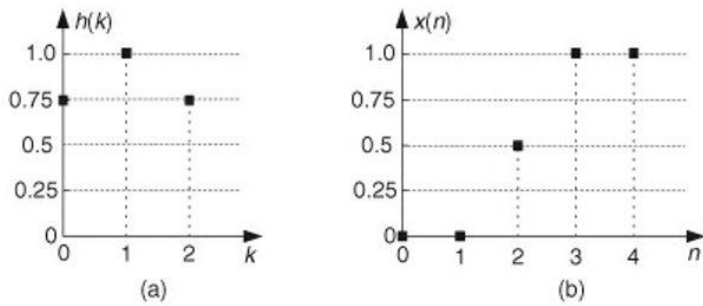
B) The maximum sample value of the filter's output sequence is 2



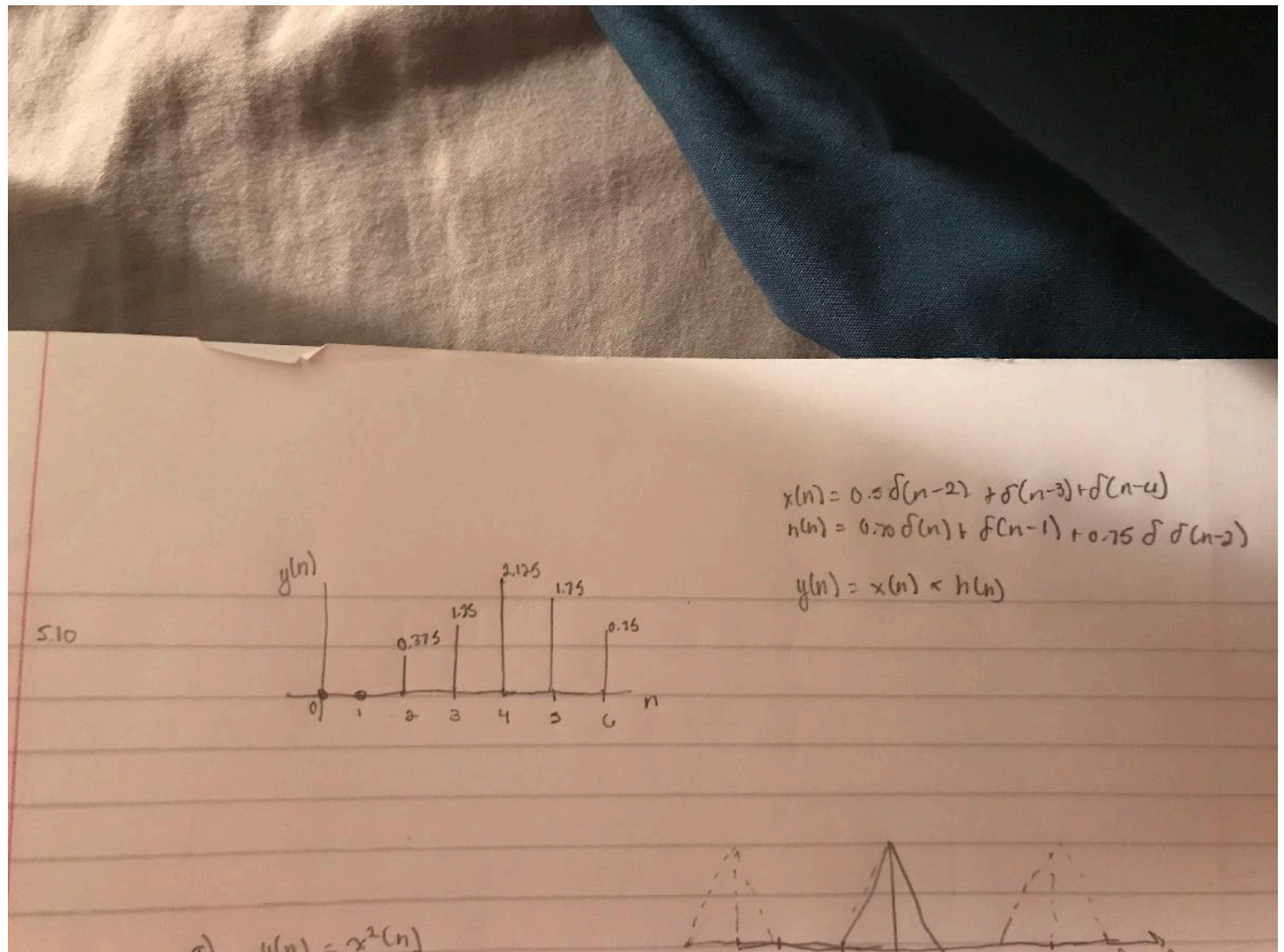
## Problem 10

Consider an FIR filter whose impulse response is that shown in Figure P5-10(a). Given the  $x(n]$  filter input sequence shown in Figure P5-10(b), draw the filter's output sequence.

Figure P5-10



Answer:

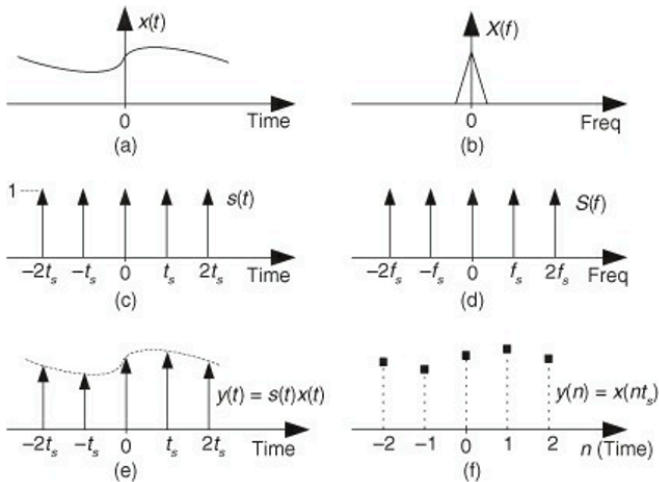




## Problem 11

Regarding the material in this chapter, it's educational to revisit the idea of periodic sampling that was presented in Chapter 2. Think about a continuous  $x(t)$  signal in Figure P5-11(a) whose spectrum is depicted in Figure P5-11(b). Also, consider the continuous periodic infinitely narrow impulses,  $s(t)$ , shown in Figure P5-11(c). Reference [28] provides the algebraic acrobatics to show that the spectrum of  $s(t)$  is the continuous infinitely narrow impulses,  $S(f)$ , shown in Figure P5-11(d). If we multiply the  $x(t)$  signal by the  $s(t)$  impulses, we obtain the continuous  $y(t) = s(t)x(t)$  impulse signal shown by the arrows in Figure P5-11(e).

**Figure P5-11**



Now, if we use an analog-to-digital converter to represent those  $y(t)$  impulse values as a sequence of discrete samples, we obtain the  $y(n)$  sequence shown in Figure P5-11(f). Here is the problem: Briefly discuss what we learned in this Chapter 5 that tells us the spectrum of the  $y(n)$  samples comprises periodic replications of the  $X(f)$  in Figure P5-11(b). Your brief discussion should confirm the material in Chapter 2 which stated that discrete-time sequences have periodic (replicated) spectra.

### Answer:

The spectrum of the  $y(n)$  samples comprises of periodic replications of the  $X(f)$  because in Chapter 5 we learned that in Finite Impulse Response Filters, the filter's effect on the sequence  $x[n]$  is described in the frequency domain by the convolution theorem:

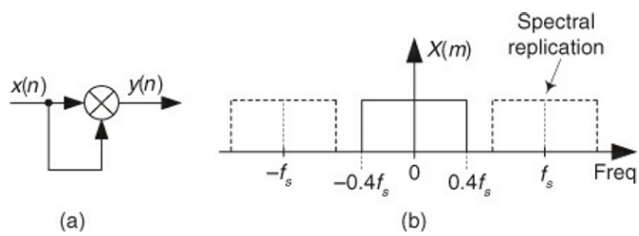
$$Y(\omega) = X(\omega) * H(\omega) \text{ and } y[n] = x[n] * h[n]$$

where  $\omega = 2\pi f$ , changes the units of frequency ( $f$ ) to *cycles/sample* and the periodicity to 1. When the  $x[n]$  sequence has a known sampling-rate,  $f_s$  *samples/second*, the substitution  $\omega = 2\pi f / f_s$  changes the units of frequency ( $f$ ) to *cycles/second* and the periodicity to  $f_s$ . The value  $\omega = \pi$  corresponds to a frequency of  $f = f_s/2$  *Hz* =  $1/2$  *cycles/sample*, which is the Nyquist frequency.

## Problem 12

Now that we're familiar with the powerful convolution theorem, think about the discrete system shown in Figure P5-12(a).

**Figure P5-12**



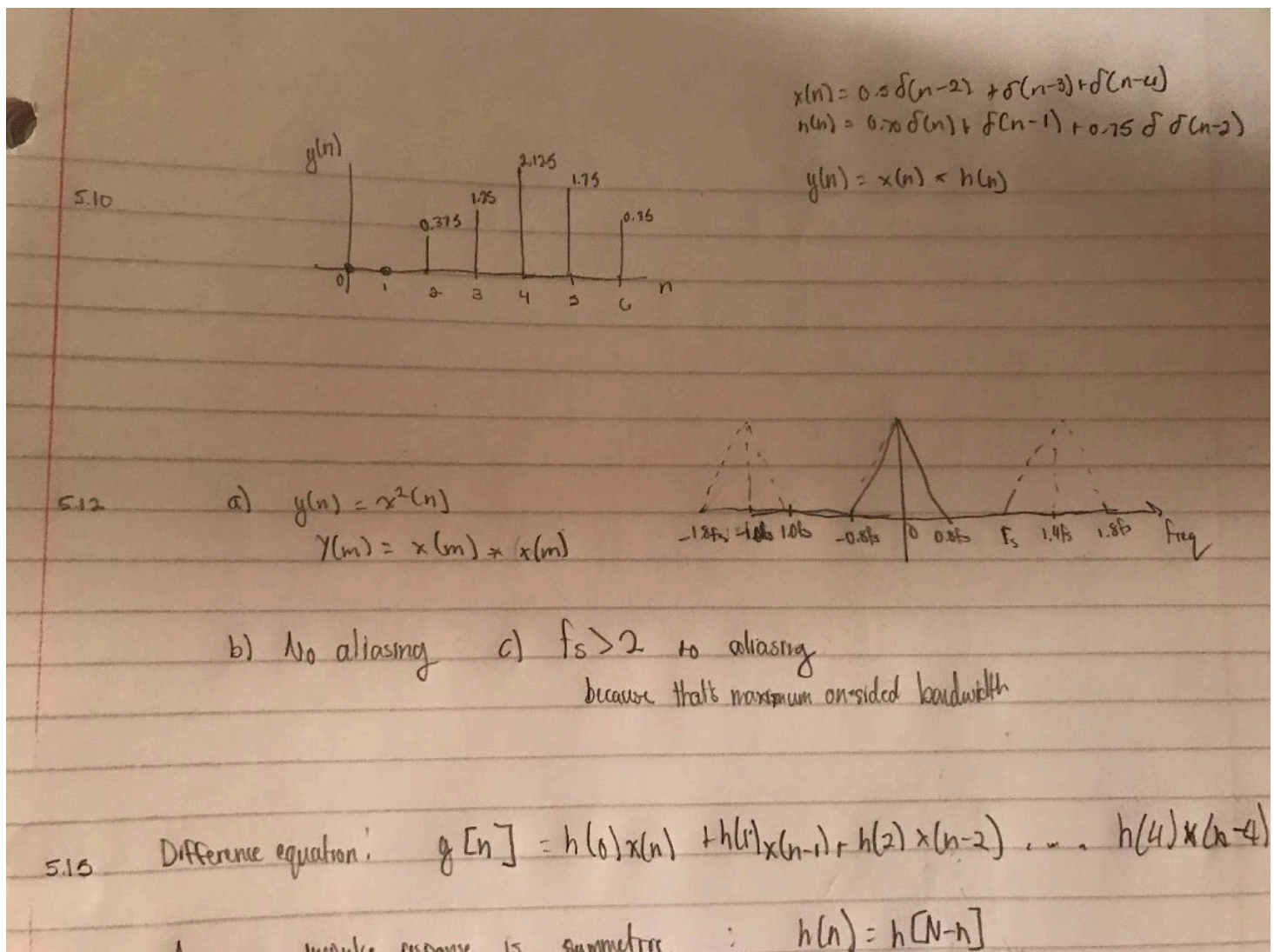
Given that  $x(n)$ 's spectrum is the  $X(m)$  shown in Figure P5-12(b):

(a) Draw the  $Y(m)$  spectrum of sequence  $y(n)$ . (We're not worried about the vertical axis scale here, merely the frequency axis and spectral shape of  $Y(m)$ .)

(b) Will aliasing errors occur in the  $y(n) = x(n)^2$  output? (That is, will spectral replications in  $Y(m)$  overlap each other?)

(c) What is  $x(n)$ 's maximum one-sided bandwidth that will avoid aliasing errors in  $y(n)$ ? (Stated in different words, what is the maximum one-sided bandwidth of  $x(n)$  that will avoid overlapped spectral replications in  $Y(m)$ ?)

**Answer:**



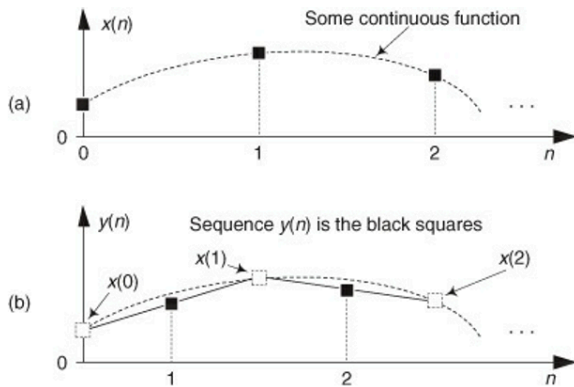
## Problem 13

It's likely that you have heard of the process called linear interpolation. It's a computationally simple (but not terribly accurate) scheme for estimating sample values of a continuous function in between some given  $x(n)$  sample values of that function. For the  $x(n)$  time samples in Figure P513(a), linear interpolation is the process of computing the intermediate  $y(n)$  samples shown as the black squares in Figure P5-13(b). That is, the interpolated sample  $y(1)$  is the value lying on the center of the straight line connecting  $x(0)$  and  $x(1)$ , the interpolated sample  $y(2)$  is the value lying on the center of the straight line connecting  $x(1)$  and  $x(2)$ , and so on. Given this process of linear interpolation:

(a) What is the equation defining  $y(n)$  in terms of the  $x(n)$  samples?

(b) The implementation of linear interpolation is often called a filter because we build interpolators using tapped-delay line structures, just like standard FIR filter structures. Draw the block diagram of a linear interpolation filter that computes  $y(n)$  from the input  $x(n)$  sequence.

Figure P5-13



**Answer:**

a)  $y(n) = y(n+1) + (x(n) - x(n-1)) (y(n+1) - y(n-1)) / (x(n+1) - x(n-1))$

b)

## Problem 14

Consider a linear-phase lowpass FIR filter whose coefficients are

$$h_1(k) = [-0.8, 1.6, 25.5, 47, 25.5, 1.6, -0.8],$$

and whose DC gain,  $H_1(0)$ , is equal to 99.6. If we change those coefficients to

$$h_2(k) = [-0.8, 1.6, Q, 47, Q, 1.6, -0.8],$$

we obtain a new DC gain equal to 103.6. What is the value of  $Q$ ?

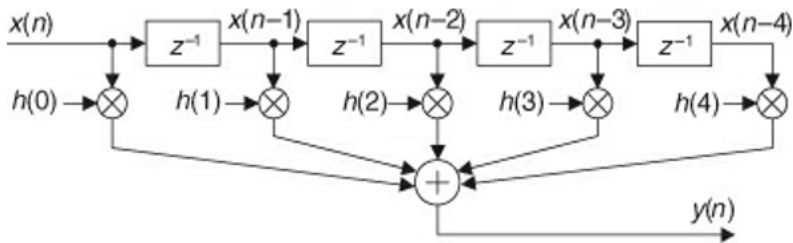
**Answer:**

$$Q = 27.5$$

## Problem 15

Figure P5-15 shows a linear-phase 5-tap FIR filter.





DSP engineers always seek to reduce the number of multipliers in their systems. Redesign the filter in Figure P5-15 to a form that reduces the number of necessary multiplications per output sample. Draw the block diagram of your new design.

Hint: Write the difference equation for the  $y(n)$  output sequence, and recall the relationships between the filter's coefficients.

**Answer:**

b) no aliasing c)  $f_s > 2$  to aliasing because that's maximum on-sided bandwidth

5.15 Difference equation:  $y[n] = h(0)x[n] + h(1)x[n-1] + h(2)x[n-2] + \dots + h(4)x[n-4]$

Assuming impulse response is symmetric:  $h(n) = h[N-n]$

so  $y(n) = h_0 [x(n) + x(n-4)] + h(1) [x(n-1) + x(n-3)] + h(2)x(n-2)$

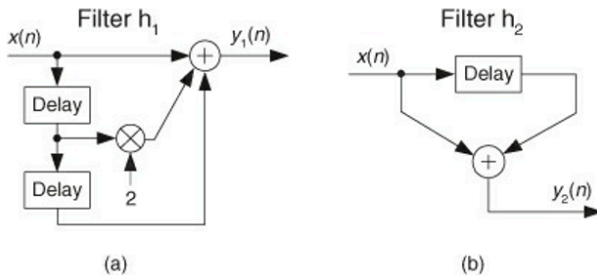
512-12

## Problem 16

The two linear-phase lowpass filters in Figure P5-16 have very similar frequency responses, but those responses are not identical except at a single frequency. If we replaced Filter h1 with Filter h2 to reduce our filtering computational workload, determine the frequency,  $\omega_0$ , where the two  $H_1(\omega)$  and  $H_2(\omega)$  frequency responses are equal.

Hint: Begin by creating closed-form equations for  $H_1(\omega)$  and  $H_2(\omega)$  using the discrete-time Fourier transform (DTFT).

**Figure P5-16**



**Answer:**

## Problem 17

The following is a useful problem regarding the 3-tap nonrecursive FIR filter shown in Figure P5-17(a). The problem's solution shows us how to design computationally efficient narrowband noise reduction filters. If  $|h_1| \leq 2$ , the filter will have an  $|H(\omega)|$  frequency magnitude response having two nulls at  $\pm\omega_n$  as shown in Figure P5-17(b). (Here, the frequency axis value of  $\pi$  radians/sample corresponds to a cyclic frequency of half the sample rate,  $f_s/2$ .)

(a) Assume we have a low-frequency signal of interest that's contaminated with high-level narrowband noise located at  $\pm 3.35$  MHz when the sample rate is  $f_s = 8.25$  MHz as shown in Figure P5-17(c). To attenuate that noise, for what value of  $h_1$  will the 3-tap FIR filter's nulls be located at the noise center frequency of  $\pm 3.35$  MHz? Show your work.

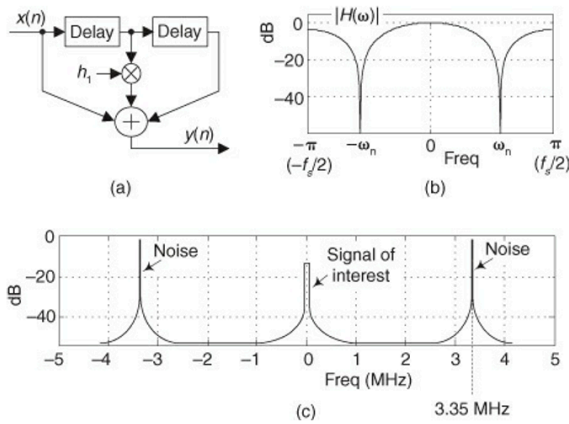
Hint: Use the discrete-time Fourier transform (DTFT) of the filter's impulse response to create a closed-form equation for the filter's  $H(\omega)$  frequency response in terms of the coefficient  $h_1$  and frequency  $\omega$ . Next, obtain the expression for  $h_1$  in terms of the filter's null frequency  $\omega_n$ .

(b) What is the DC gain (gain at zero Hz) of our 3-tap FIR filter?

(c) Explain why the filter has a linear, or nonlinear, phase response.



Figure P5-17



**Answer:**

a)  $h_1 = 1.997$

b) DC gain =  $3 \times 10^{-3}$

c) linear phase because phase  $H(e^{j\omega}) = -\omega$

## Problem 18

What characteristic must the coefficients of an FIR filter have to ensure that its frequencydomain phase response is a linear function of frequency (i.e., linear phase)?

**Answer:**

We know that the frequency domain phase is linear when the coefficients are symmetrical around the center.

## Problem 19

Quickfilter Technologies Inc. produces a tapped-delay line FIR filter chip (Part #QF1D512) that has an astounding  $N = 512$  taps. When a new filter input sample is applied to the chip, how many addition operations must this chip perform to compute a single filter output sample?

**Answer:**

512 addition operations must be performed

## Problem 20:

```
S20 = 255;
fs20 = 8*10^6;
Group_delay = (S20 - 1)/(2*fs20)
```

15uSeconds

### Problem 21:

```
time_delay = 600/(2*pi*400)
```

### Problem 22:

22)

a)

$$G = \frac{17-1}{2} = 8.5 \text{ samples}$$

b) Since it is a "symmetrical

$$H(\omega) = -\omega(17-1)/2 = -$$

$$G = \frac{-d(H(\omega))}{d(\omega)} = 8.5$$

### Problem 23:

### Problem 24:

Time synchronization requires **4 unit delays**

### Problem 25:

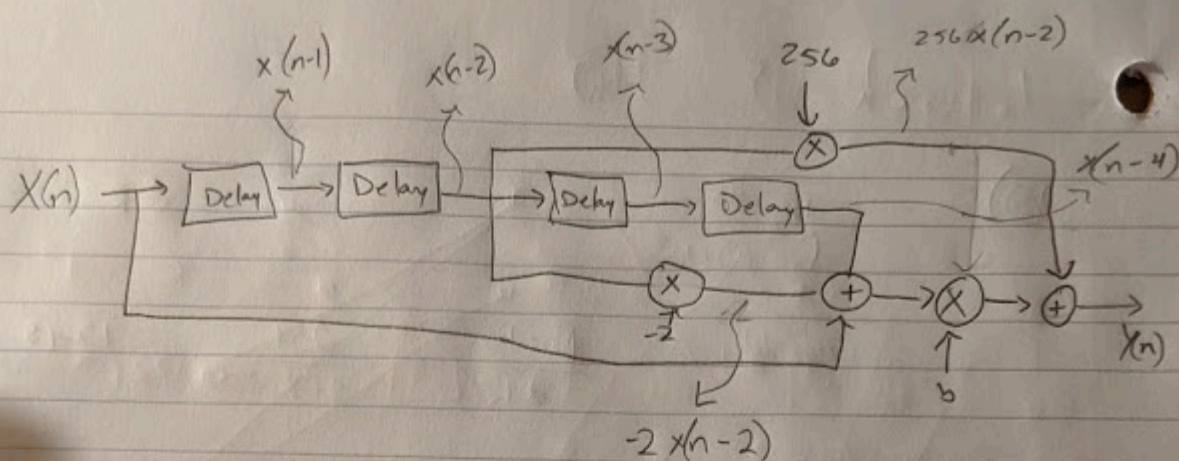
### Problem 27:

$$191 = \frac{55}{22 * (f_{\text{stop}} - f_{\text{pass}})}$$

$$(f_{\text{stop}} - f_{\text{pass}}) = 0.01308f_s$$

### Problem 28:





a)

$$y[n] = 256 x[n-2] + b [x[n-4] - 2x[n-2] + x[n]]$$

$$y[n] = (256 - 2b) x[n-2] + b [x[n-4] + x[n]]$$

b) DFT

$$Y(e^{j\Omega}) = (256 - 2b) e^{-j2\Omega} X(e^{j\Omega}) + b [e^{-j4\Omega} X(e^{j\Omega}) + X(e^{j\Omega})]$$

$$Y(e^{j\Omega}) = X(e^{j\Omega}) [(256 - 2b) e^{-j2\Omega} + b e^{-j4\Omega} + b]$$

$$\frac{Y(e^{j\Omega})}{X(e^{j\Omega})} = b e^{-j4\Omega} + (256 - 2b) e^{-j2\Omega} + b$$

$$= e^{-j2\Omega} (2b \cos 2\Omega - 2b + 256)$$

Phase Response

$$\angle \frac{Y(e^{j\Omega})}{X(e^{j\Omega})} = -2\Omega$$

c) Group Delay =  $-\frac{d}{d\Omega} \left[ \frac{Y}{X} \right]$

$$= -\frac{d}{d\Omega} [-2\Omega]$$

$$= 2$$

## Problem 29: