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# Extended Abstract: L.U.N.A. - A Laser-Mapping Unidirectional Navigation Actuator

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## 0.1 Motivation, Problem Statement, Related Work

To foster new advances in the latter, specifically for underground environments, the Defense Advanced Research Projects Agency (DARPA) of the US Defense Department established the yearly “SubT” Challenge in 2017. In this challenge, teams are tasked to “Drive novel approaches and technologies to allow warfighters and first-responders to rapidly map, navigate, and search dynamic underground environments.” [1] proving the demand for further research in this domain. One subtask of this challenge is building an accurate 3D model of the environment, i.e., mapping the surroundings. This paper shows a proof of concept of a such a novel approach and validates it with experiments.

One such approach using a 2D laser scanner to scan 3D indoor environments has been proposed in [4]. The authors mount a 2D laser scanner on a cylindrical structure. An operator then initiates a rolling motion by manually pushing the contraption. This enables the scanner to sense the 3D environment successfully. However, manually pushing the scanner is not practical, especially for long scans.

Previous work includes our RADLER (RADial LasER scanning device), which consists of a 2D laser scanner attached to the axle of a unicycle [2]. An operator pushes the unicycle along a requested path. The inherent rotation of the wheel creates a radial 3D laser scanning pattern. However, this approach still requires an operator, therefore does not fulfill the autonomy requirements.

A more autonomous approach was taken by Fang et al. [3]. The authors mounted a rotating 2D laser-scanner on top of a turtle-bot thus removing the need of an operator. In contrast to the RADLER however, the turtle-bot does not provide an inherent rotation. Therefore an additional actuator is required to create the radial 3D scanning-pattern.

This paper builds upon the results of the RADLER and has a specific application of mapping lunar craters autonomously in mind. We propose a novel approach to low-cost 3D laser scanning using a 2D laser scanner inside a spherical robot based on impulse by conservation of angular momentum (IBCOAM): the L.U.N.A.-sphere (Laser-mapping Unidirectional Navigation Actuator). The 2D laser scanner is fixed to the spherical structure, hence a similar situation as with the RADLER is given: the inherent rotation of the sphere creates a radial 3D scanning pattern. Using the format of a spherical robot permits the system to be designed more compact. Additionally, the spherical shell doubles as a protective layer for the actuators, sensors and electronics. This is especially valuable for applications in rough terrain or scenarios in which non-minimal impact is expected, such as space applications. During a launch, withstanding large G-forces is a necessary requirement, which can be better implemented using the spherical format. Furthermore, an operator is no longer required given a drive implemented in the robot.

## 0.2 Technical Approach

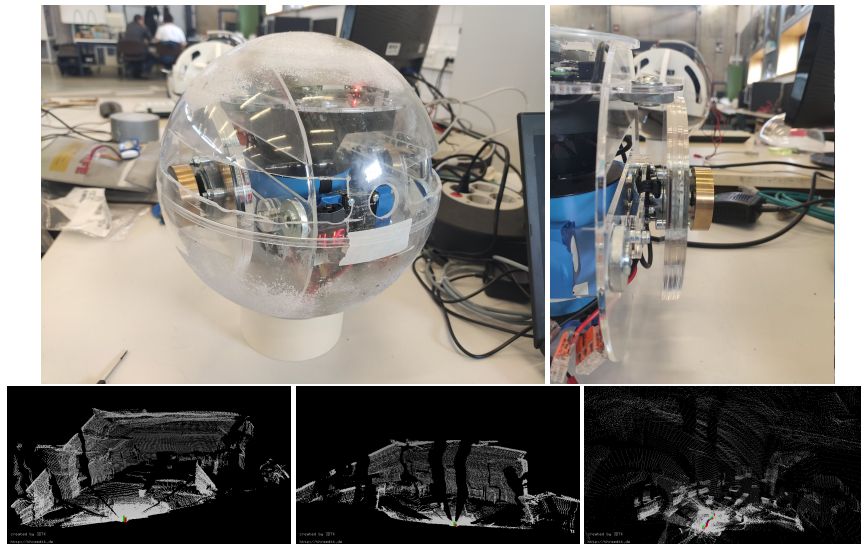
The L.U.N.A robot is a sphere robot. It carries a laser-scanner which measures 540 points in one line. Therefore, when the sphere is rolling, L.U.N.A is capable to reconstruct the environment three-dimensional. To accomplish the rotation L.U.N.A has 2 flywheels. As result of the impulse-momentum theorem, for a change of the momentum of the flywheels, an impulse, rooted in a force, is needed. The motors provide this force, and according to Newtons' third, a force is applied back, resulting in the opposite change of momentum of the sphere. So the rotation of the sphere is not a direct consequence of the angular momentum of the flywheels, but rather of the impulse needed to spin them. Figure 0.1 shows a CAD blueprint of the overall interior layout of the mechanical structure of the L.U.N.A sphere, ignoring the outside sphere, flywheels and wiring. The the LMS-100-10000 laser scanner is mounted to the supporting structural components which are made of acrylic glass. The two brushless motors were each placed on one side of the supporting structure. The motors are mounted with spacers, that leave room for the side IMU underneath one of the motors. Two other IMUs are placed in front of and beneath the laser to ensure coverage of all axes. The flywheels are a combination of bass and acrylic glass, as combination of high weight by brass and on the outer radius transparency by the acrylic.

Figure 0.1 shows the final hardware setup of the robot. In order to reduce complexity with respect to the 3D-transformation calculations, the laser scanner was placed at the center of a spherical acrylic glass shell as precisely as possible. This limits the laser scanners movement to rotational movement and removes translational movement completely.

Three separete IMUs keep track of the pose of the sphere. Each IMU is placed in such a way that the IMUs Z-axis corresponds to one possible rotation axis of the sphere. Therefore, each IMU is perpendicular to the other two. Combining the axes measurements leads to a "virtual" IMU, which emulates being an IMU positioned at the center of the sphere. Hence, isolating the measurements of the resulting virtual IMU to only the rotation in the given axis. The IMUs also ship with accelerometers that are used to determine the full pose of the sphere. Each IMU calculates their pose separately, using a quaternion extended Kalman filter (QEKF). However, combining those poses into one does not have any positive effect, but only makes the software more resource demanding and slow. Thus only the pose of the bottom IMU's accelerometer is used to keep track of the pose.

A controller was implemented that measures the extend of the vibrations using standard deviations of the non-rotating axes of the IMU and adjusts the throttle of the motors accordingly. Considering the translational velocity of the sphere in a controller is not possible. The speed of the sphere is calculated by the rotational speed, which is why slippage of the sphere causes such a controller not to produce the desired motion.

For the processing of the point cloud the 3D Toolkit (3DTK) was used. Therefore only the time-stamped raw data of the IMUs and laser scanner is transferred and the estimation of the pose and the SLAM algorithm itself is performed externally.



(a) Test with limited movement and no exterior shell. (b) Test with limited movement and exterior shell. (c) Test with exterior shell and full movement.

Fig. 0.1: Hardware setup and laser-scanning Results of the L.U.N.A sphere prototype The Hardware including notches in the shell and friction granule (middle left). IMU (beneath supporting structure) and brushless motor including flywheel mass (above supporting structure)(middle right).

## **0.4 Experiments completed or scheduled**

All Experiments have been completed.

Multiple Basic-Roll-Tests: as the driving mechanism is not the common approach, where the rotation of a non-homogenous mass-distribution leads to the rotation, there where several basic tests for the driving mechanism conducted.

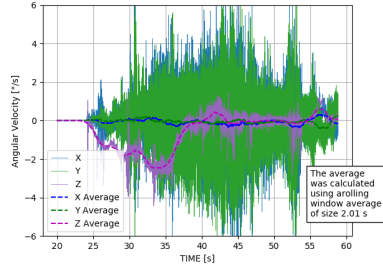
Outdoor and indoor scanning-Tests: the environment-scanning was tested indoor and outdoor.

Stress-Test for the micro-controller: evaluating the amount of required tasks capable by the micro-controller itself and therefore scaling the need of an server-structure.

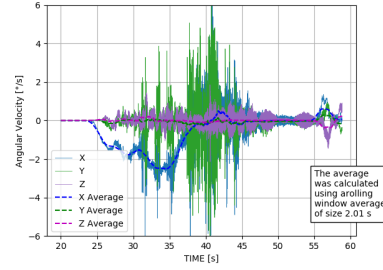
Single-IMU vs Triple-IMU test: the difference between the use of a single IMU and the triple-IMU approach presented in [0.2](#) was tested.

## 0.5 Main Experimental Insights

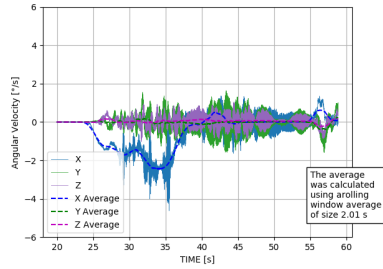
The experiments lead to multiple hardware and software improvements. The impulse by conservation of angular momentum drive accelerates the L.U.N.A. sphere reliably. Figure 0.2 shows the angular acceleration of the whole sphere measured by the IMU system in one test run. Furthermore, it shows that the acceleration along the rotational axis of the flywheels rises while the accelerations along the other axes remain lower, albeit are noisy. However, it also shows the decrease in noise due to the combination of the IMU measurements. The vibrations and tilt of the robot contribute to the velocities along the other axes. The vibrations are results of inexact drilling of the flywheels such that there is an unbalance. At the main test site the ground is a hard, clean and low friction concrete floor. In such a scenario the vibrations add up and lead to slippage. However, a rubber surface (a running track) absorb the vibrations, such that the acceleration process happens reliably. Furthermore the tests regarding the laser-scanning showed the need of further improvement like re-positioning the laser-scanner and the need for cutting windows into the sphere.



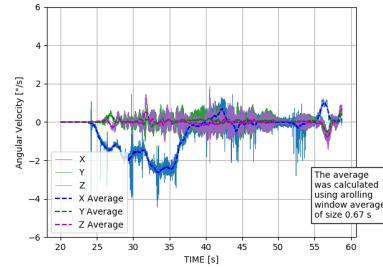
(a) IMU 1: Z-Axis corresponds to Sphere X-Axis



(b) IMU 2: Z-Axis corresponds to Sphere Z-Axis



(c) IMU 3: Z-Axis corresponds to Sphere Y-Axis



(d) Merged virtual IMU. Maps the Z-Axis of all other IMUs to the rotational axes.

Fig. 0.2: Angular velocity measurements of singular IMUs and the combined IMU.

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### Authors Note

In an attempt to abide by the [Fair-Principles](#) of open science the authors provided all code developed and further information at their [GitHub](#) page.





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