

Introduction

The analytic element method (AEM) is a gridless technique for modeling groundwater flow problems in which each feature that affects groundwater flow is described using an analytical solution. Superposition of these solutions can be used to gain insight into complex geohydrological problems. The advantages of AEM are that no spatial or temporal discretization is required and that the locations of elements are exact. The head can be computed at any location and at any time within the model domain. One disadvantage is that the computation of the head requires computing the contribution of each element in the model, causing models with many elements to become somewhat computationally intensive.

Though computational solutions exist to mitigate these downsides, finite difference (FD) groundwater models such as Modflow 6 are highly efficient and capable of modeling large-scale heterogeneous groundwater flow problems. However, these numerical groundwater models require both temporal and spatial discretization. This requires the modeler to make choices that fit the problem. In mixed-scale problems, e.g. local head changes in a large aquifer system, trade-offs between computation time and level of detail have to be considered. Combining the strengths of both modeling techniques provides the large-scale performance of FD models and adds the gridless refinement of AEM models.

The goal of this research is to tightly couple an analytic element model to a finite difference model.

Analytic Model of a Finite Difference Cell

The coupling of FD and AEM is demonstrated by replacing one cell in the FD model with an analytic element model. An analytic element model of that cell requires the following elements:

- boundary elements to control the fluxes in/out of the AEM model
- any internal elements that affect groundwater flow (e.g. wells)
- a constant

Solving these models simultaneously requires communication between the two models such that the water balance is met.

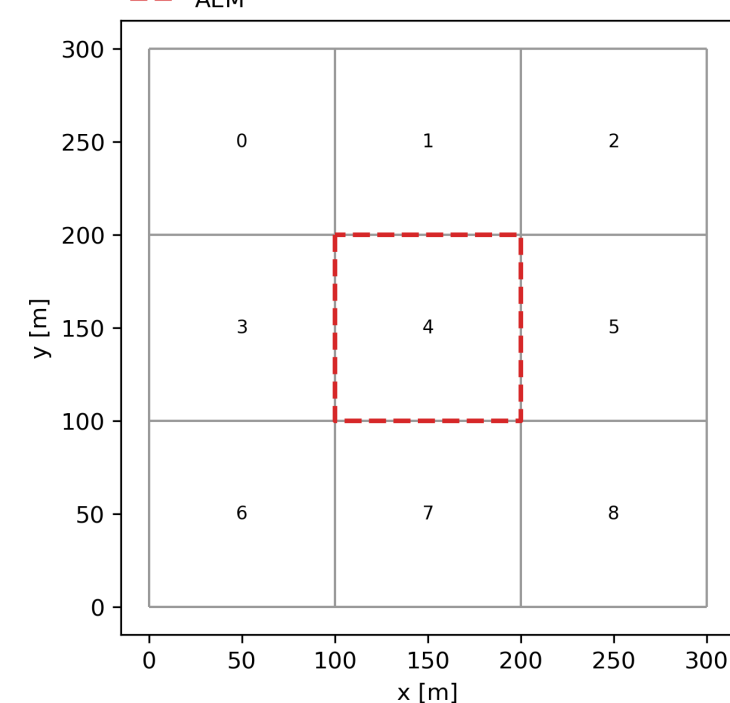


Fig. 1: FD model where the middle cell is replaced by an AEM model.

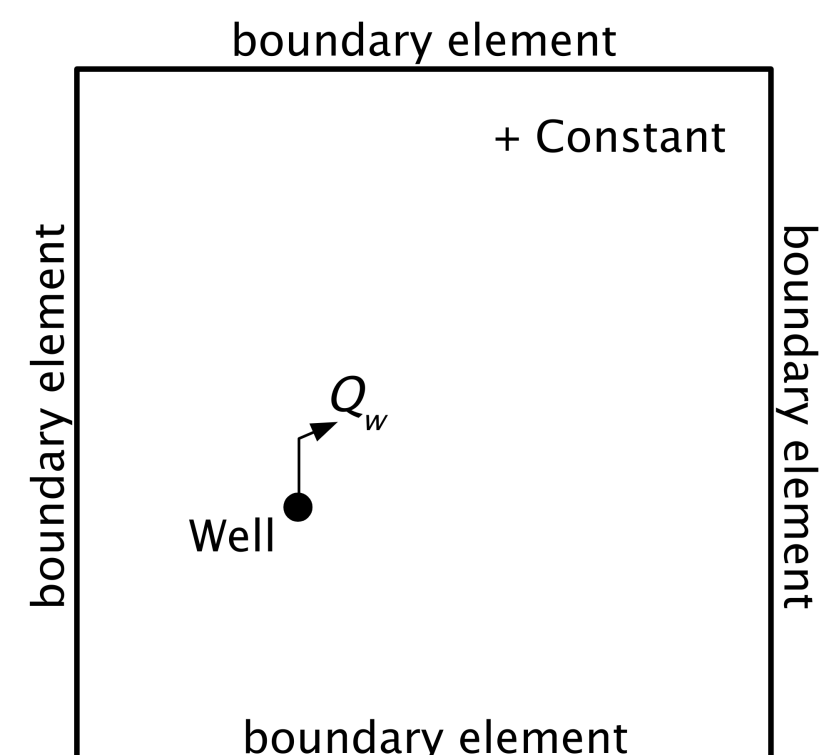


Fig. 2: A conceptual AEM model of a finite difference cell.

General Head Boundary Line Element

The boundary elements facilitate the communication between the AEM model and the FD model. The boundary element is set up as general head boundary. The normal flux q_n over the element is uniform but unknown. The flux is driven by the difference between some specified head h_{FD} and the mean head along the element h_m , multiplied by a conductance term C (Eq. 1). The conductance is computed from the FD cell midpoint to the cell boundary.

$$Q_n = q_n \Delta y \Delta z = C (h_{FD} - h_m) \quad (1)$$

The analytic solution of the boundary element is derived through separation of variables in elliptic coordinates [4]. The solutions for a line-sink and line-doublet are added together as this gave the most accurate results.

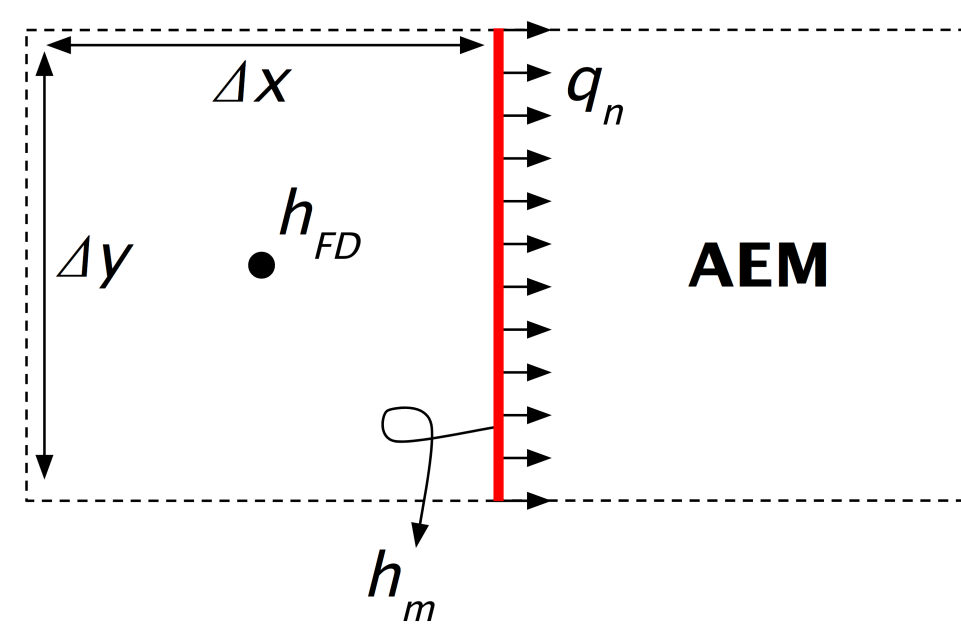


Fig. 5: Schematic showing the general head boundary element between an FD cell and an AEM model.

Benchmark Problem 1: Two Wells in Uniform Flow

Two wells are pumping from a confined aquifer with uniform flow from west to east. The eastern well is pumping at $75 \text{ m}^3/\text{d}$ and the western well is pumping at $50 \text{ m}^3/\text{d}$. The FD model dimensions are 5×5 .

Parameter	Value	Units
Aquifer thickness	10	m
Horizontal conductivity	10	m/d
Porosity	0.3	-
Uniform flow	0.001	m/m

Tab. 1: Model properties

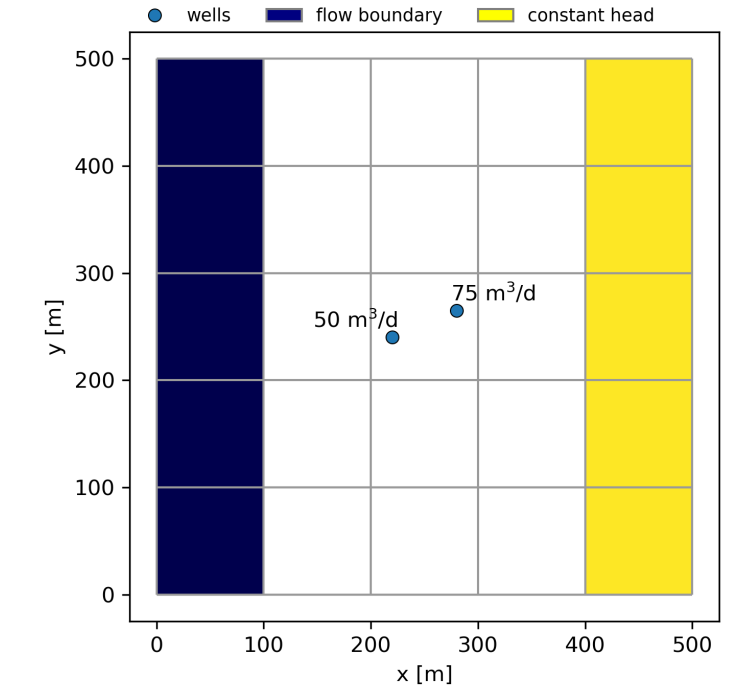


Fig. 7: Example model with 2 wells in uniform flow.

The wells are both located within one cell in the FD model. The FD model is therefore not able to compute separate capture zones for each well. The coupled FD+AEM model is able to closely match the exact solution, despite the coarse $100 \times 100 \text{ m}$ resolution of the FD model.

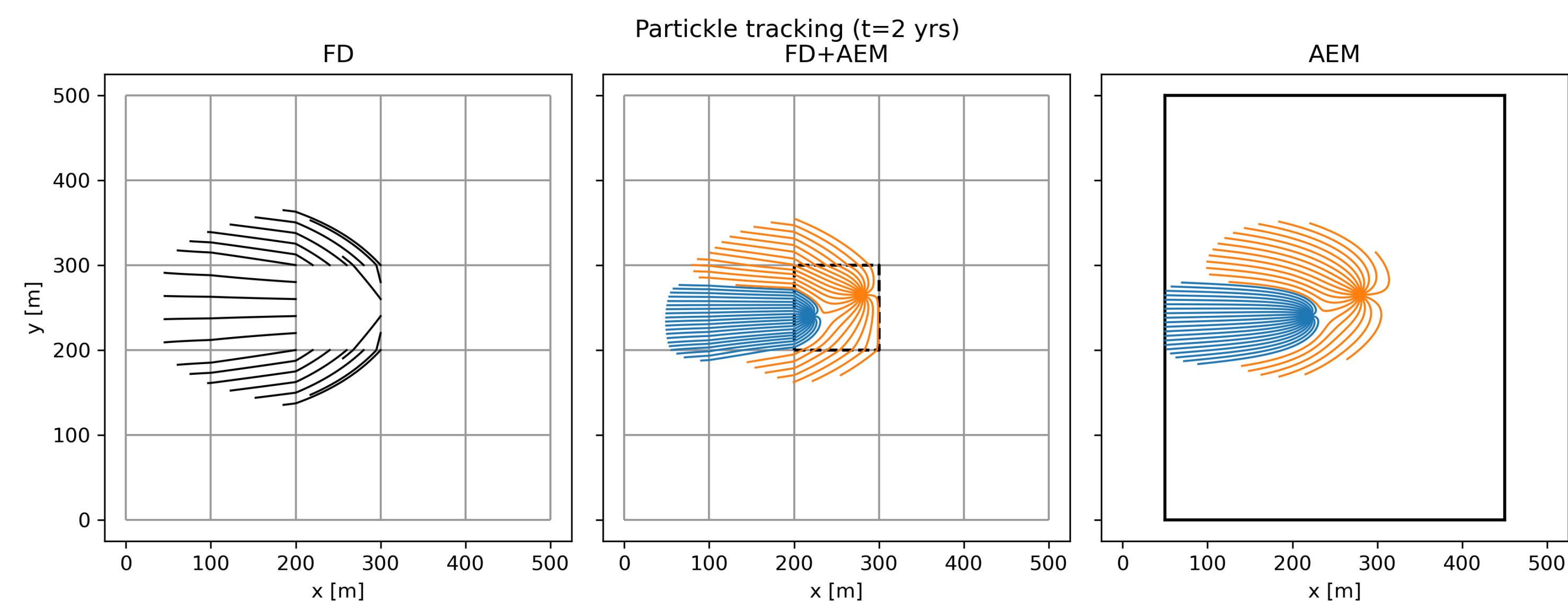


Fig. 8: Comparison of particle tracks for FD model, coupled FD and AEM model and the exact analytic solution.

Conclusions

- AEM has potential as a local refinement method for an FD model. The head and flow can be computed at any point within the AEM cell: infinite refinement of cell.
- Promising early results coupling FD and AEM models for wells in a single confined aquifer.
- General head boundary elements are flexible and satisfy the water balance. Using this element it should be straightforward to replace multiple FD cells with an AEM model.
- AEM code is written in Python and has an object-oriented structure similar to TimML and TTim. Elements developed in this research can be easily integrated into TimML or TTim.

Next Steps

- Extend solution to semi-confined and transient flow in multi-aquifer systems.
- Integrate analytic elements into the TimML/TTim Python packages.
- Replace the top-layer (e.g. drainage system) in an FD model with an AEM model.
- Test method on a real-world example, e.g. compute flow around a drinking water production well field.
- Couple directly with Modflow 6 using the Modflow API. Create an MF6-AEM package.

Analytic Element Models

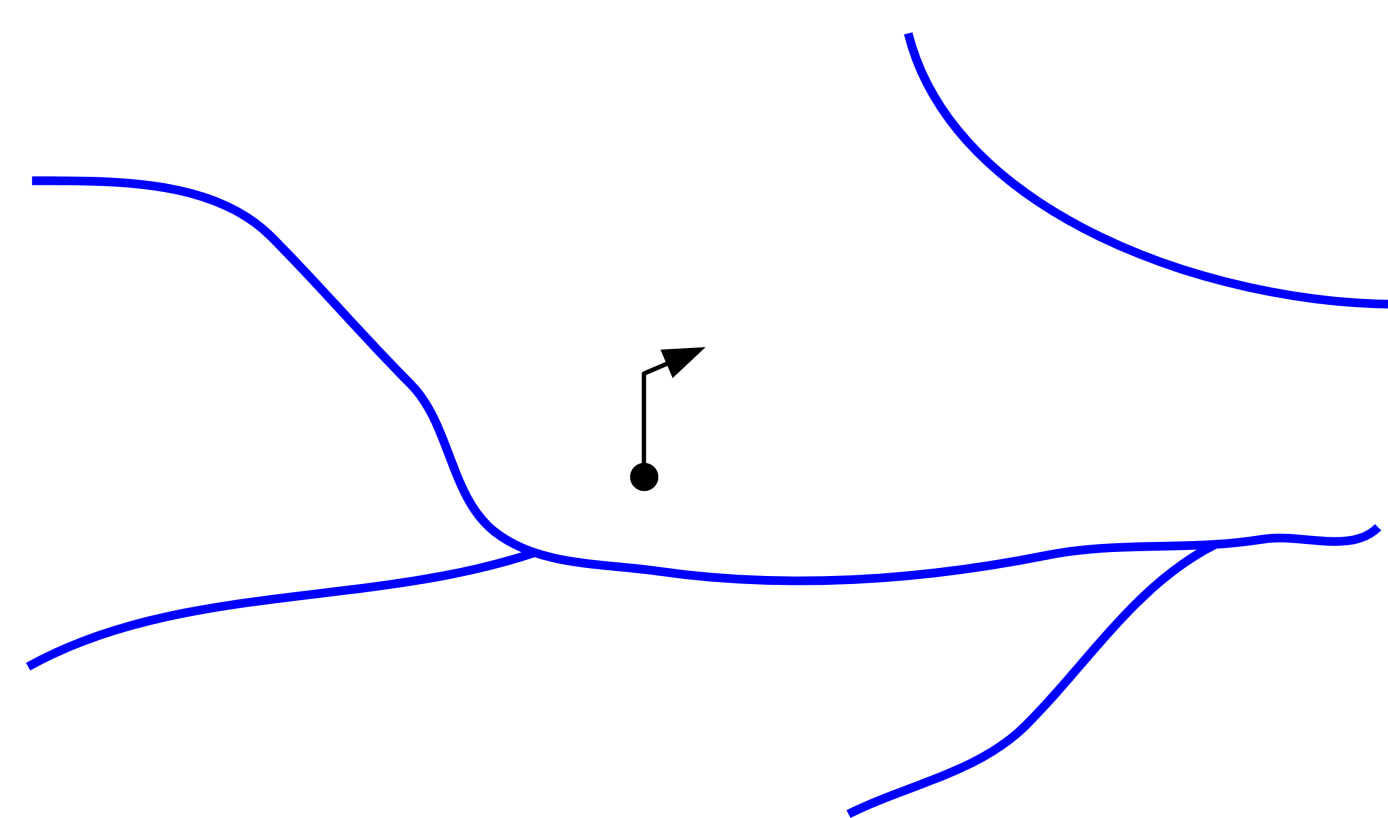


Fig. 3: An example of an Analytic Element Model.

Advantages:

- No grid, head/flow can be computed at any point.
- Features can be modeled at exact locations, no snapping to grid.

Disadvantages:

- Modeling highly heterogeneous systems requires a lot of elements and is computationally intensive.

Implementation:

- The analytic solutions used in the research were programmed in Python following the TimML object-oriented structure [1, 2]. Many more elements were added as part of researching the most flexible and robust method for coupling with FD models.

Finite Difference Models

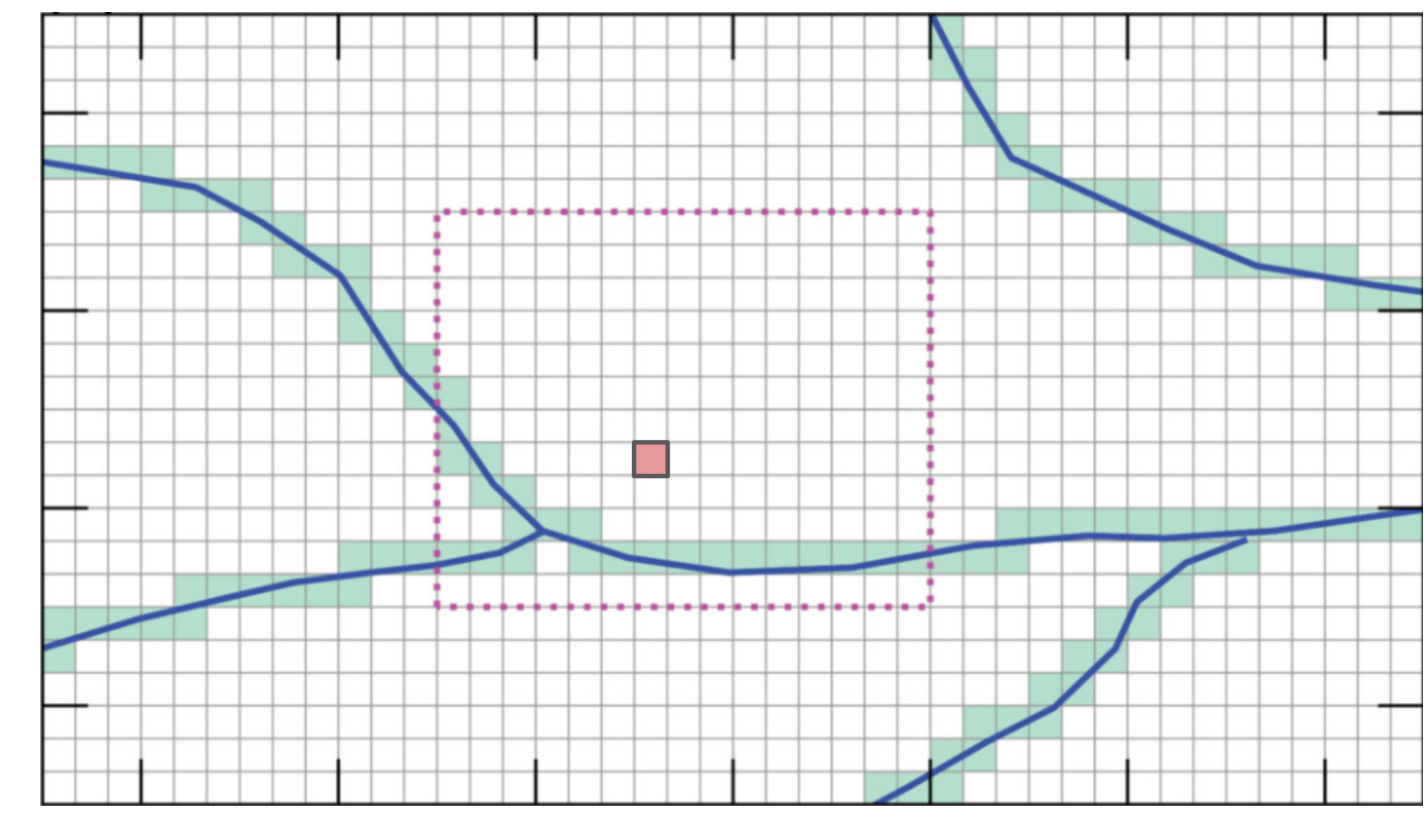


Fig. 4: An example of a Finite Difference Model [3].

Advantages:

- Fast and efficient for large-scale heterogeneous problems.
- Large-scale regional models are often available as finite difference groundwater models.

Disadvantages:

- Spatial and temporal discretization have to be defined.
- Grid has to be adapted to local features.

Implementation:

- A simple finite difference model for single confined aquifers was used in the research. The finite difference implementation was programmed in Python. Modflow 6 was not initially used as accessing and modifying the relevant parts of the code was inconvenient at this stage of the project.

Solving AEM and FD simultaneously

The equations for the FD model and AEM model are written in matrix form $\mathbf{A}\vec{x} = \mathbf{b}$. The FD equation for the replaced cell is removed. The equations of the neighboring FD cells are modified:

- the mean head along the boundary elements is substituted into the FD equations
- the conductances are adjusted accordingly, from cell midpoint to cell boundary

The AEM equations use the head from the neighboring FD cells to compute the flux entering the AEM model (Eq. 1).

Solving for \vec{x} yields the heads of the FD cells and the parameters of the analytic elements.

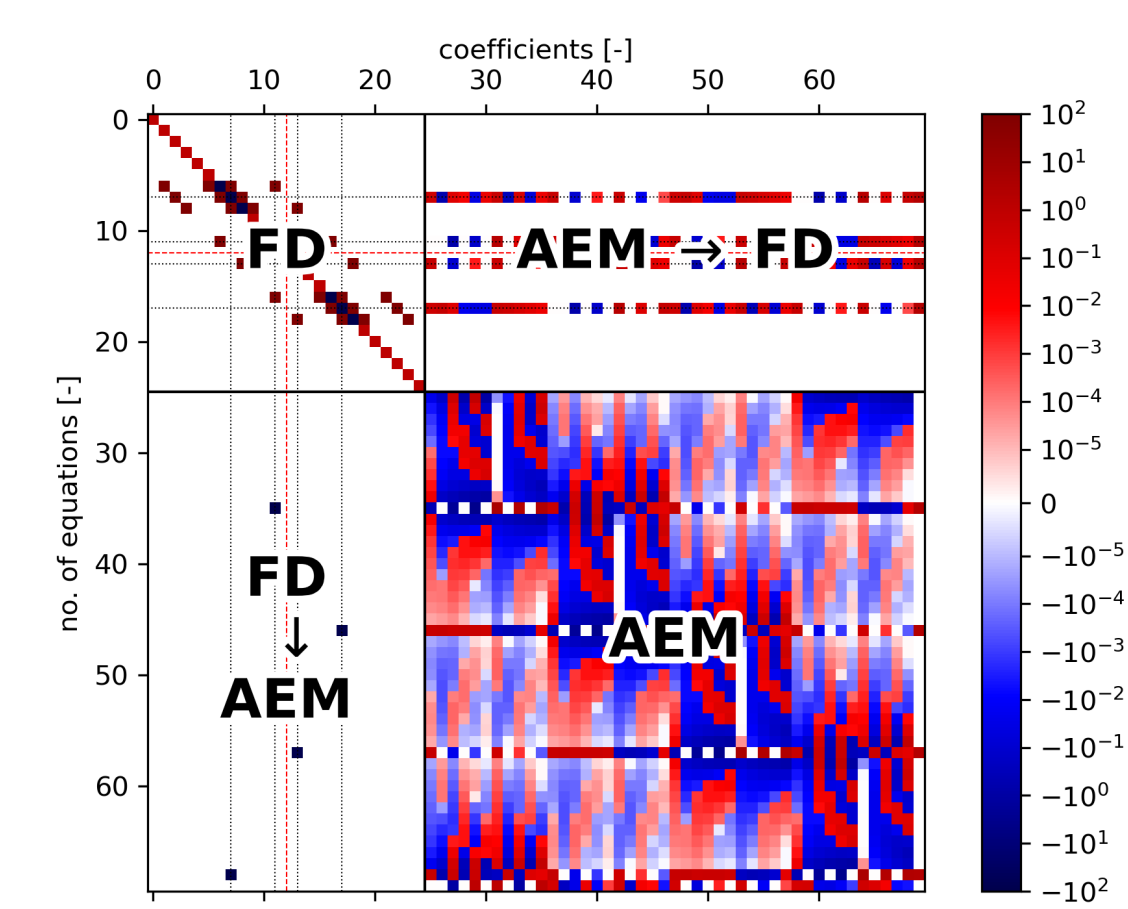


Fig. 6: The coefficients of the equations (matrix \mathbf{A}) for the coupled FD+AEM solution.

Benchmark Problem 2: Pumping and Injection in One Cell

An injection and a pumping well of equal magnitude supply and extract water in a confined aquifer at a rate of $150 \text{ m}^3/\text{d}$. Both wells lie within the same cell in the FD model. The model is bounded by a constant head boundary. The model parameters are also shown in Table 1.

The FD model cannot compute a sensible solution since the net pumping rate within the cell is $0 \text{ m}^3/\text{d}$. The coupled FD+AEM solution provides a reasonable estimate of the flow-net and the 15-year capture zone compared to the exact solution.

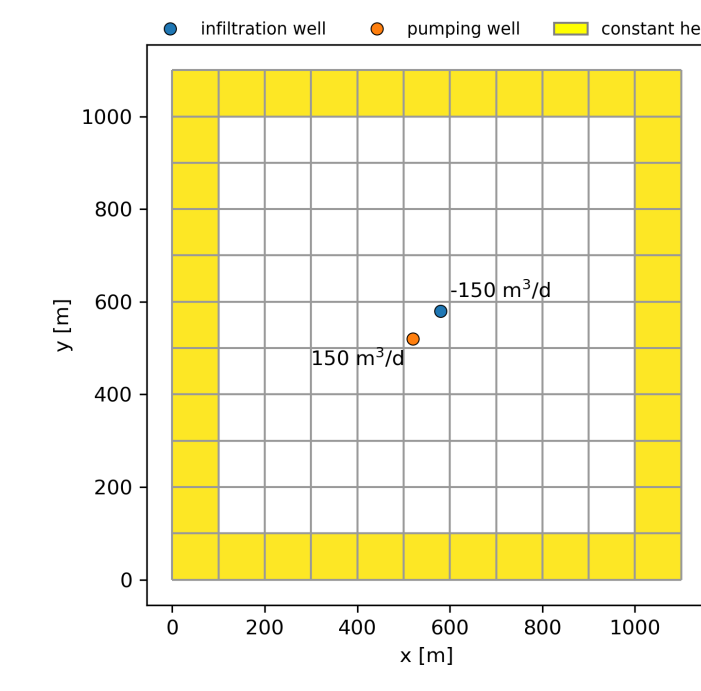


Fig. 9: Example model with injection and pumping in one cell.

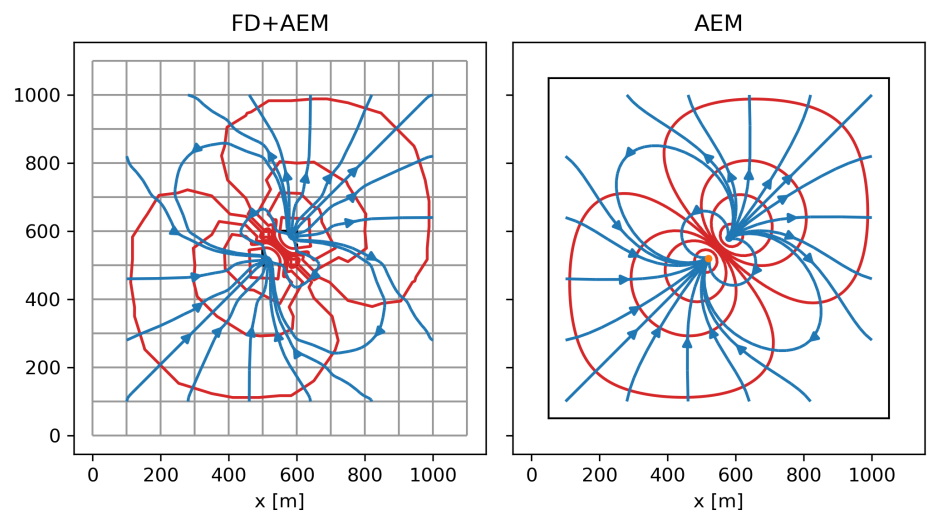


Fig. 10: Flow net of the coupled FD+AEM solution and the exact solution.

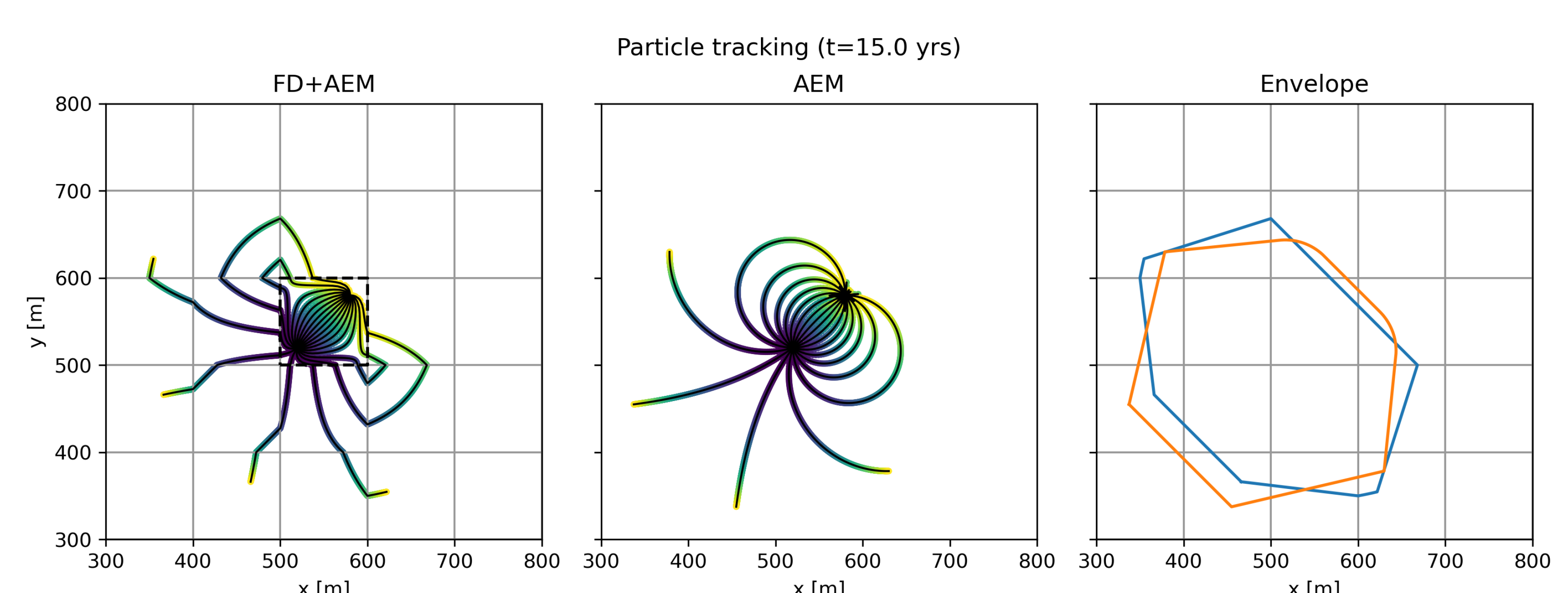


Fig. 11: Comparison of particle tracks for FD model, coupled FD+AEM model and the exact analytic solution.

References

- [1] Mark Bakker and Victor A. Kelson. Writing Analytic Element Programs in Python. *Groundwater*, 47(6):828–834, 2009. ISSN 1745-6584. doi: 10.1111/j.1745-6584.2009.00583.x. URL <https://onlinelibrary.wiley.com/doi/abs/10.1111/j.1745-6584.2009.00583.x>.
- [2] Mark Bakker and Vincent Post. *Analytical Groundwater Modeling : Theory and Applications Using Python*, volume First edition. CRC Press, Leiden, 2022. ISBN 978-1-138-02939-2.
- [3] Joseph D. Hughes, Christian D. Langevin, Scott R. Paulinski, Joshua D. Larsen, and David Brakenhoff. FloPy Workflows for Creating Structured and Unstructured MODFLOW Models. *Groundwater*, n/a(n/a), 2023. ISSN 1745-6584. doi: 10.1111/gwat.13327. URL <https://onlinelibrary.wiley.com/doi/abs/10.1111/gwat.13327>.
- [4] Mark Bakker. Derivation and relative performance of strings of line elements for modeling (un)confined and semi-confined flow. *Advances in Water Resources*, 31(6):906–914, June 2008. ISSN 0309-1708. doi: 10.1016/j.advwatres.2008.02.005.

Link to PDF

