

Buckling-6

Title

Lateral buckling of a simply supported cruciform column subjected to a concentric axial load

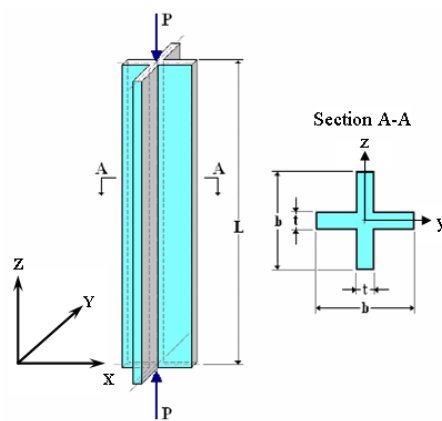
Description

A simply supported cruciform column consisted of narrow rectangular fins undergoes a vertical load P applied at the centroid of the top end. The buckling loads are determined for the three cases in which the column is divided into 10 and 20 beam elements and 80 plate elements. The computed buckling loads are then compared with the analytical exact solution.

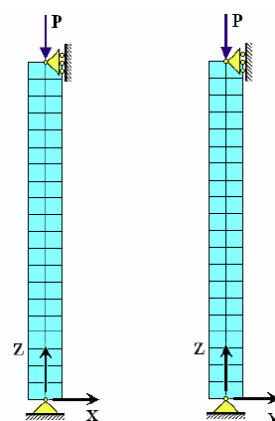
Case 1: 10 Beam elements evenly divided vertically

Case 2: 20 Beam elements evenly divided vertically

Case 3: 80 Plate elements evenly divided into 20 segments vertically



(a) Beam element model



(b) Plate element model

Structural geometry and boundary conditions

Model

Analysis Type

Lateral torsional buckling

Unit System

kN, mm

Dimension

Length 3000mm

Element

Beam element and plate element (thick type without drilling dof)

Material

Young's modulus of elasticity $E = 200\text{kN/mm}^2$

Poisson's ratio $\nu = 0.25$

Section Property

Beam element : combined section in a cruciform shape - thickness 6mm, width 300mm

Plate element : thickness 6mm, width 150mm, height 150mm

Boundary Condition

Bottom end is pinned, and top end is roller.

Load

$P = 1.0\text{ kN}$

Results

Buckling Analysis Results

Case 1: Beam elements (total 10 elements)

Buckling load

| Mode | UX | UY |
|-------------------|------------|-------------|
| BUCKLING ANALYSIS | | |
| Mode | Eigenvalue | Tolerance |
| 1 | 458,085966 | 0,0000e+000 |

Case 2: Beam element (total 20 elements)

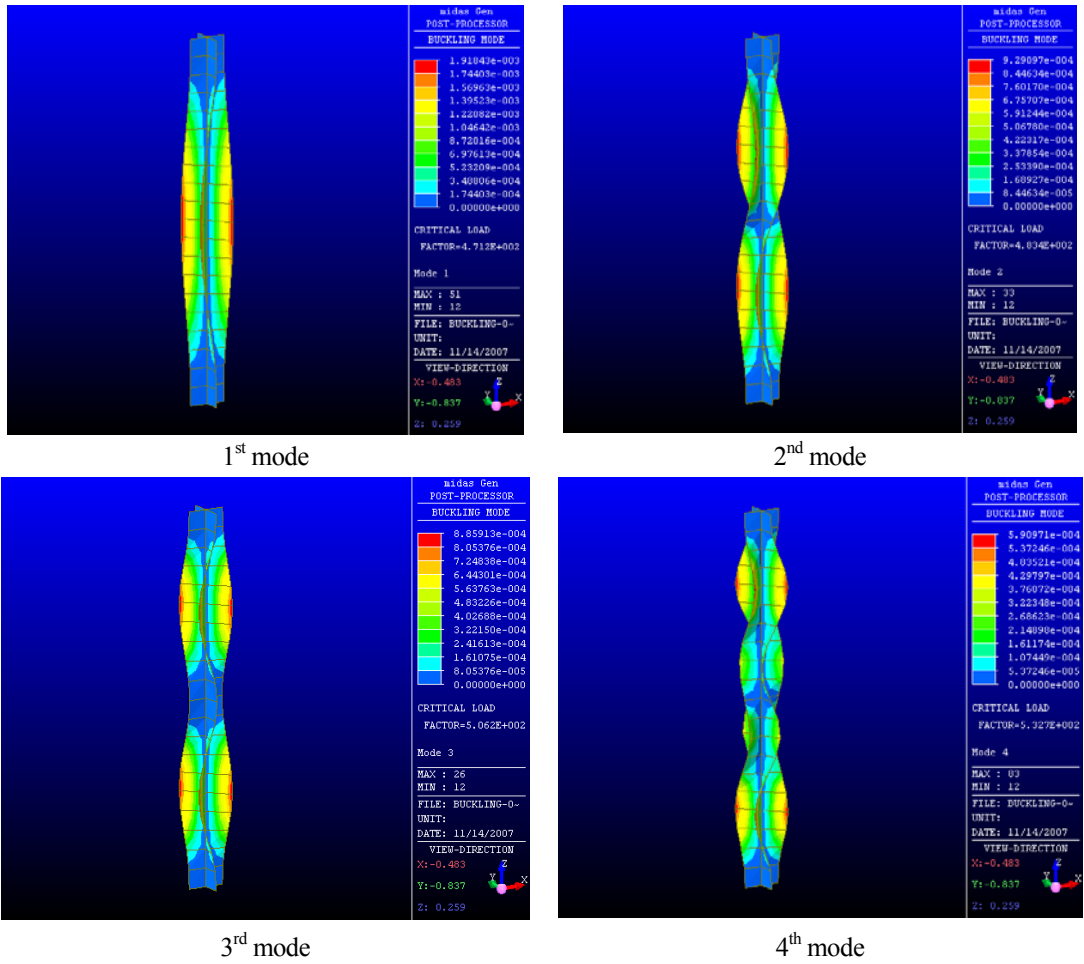
Buckling load

| Mode | UX | UY |
|-------------------|------------|-------------|
| BUCKLING ANALYSIS | | |
| Mode | Eigenvalue | Tolerance |
| 1 | 458,085966 | 0,0000e+000 |

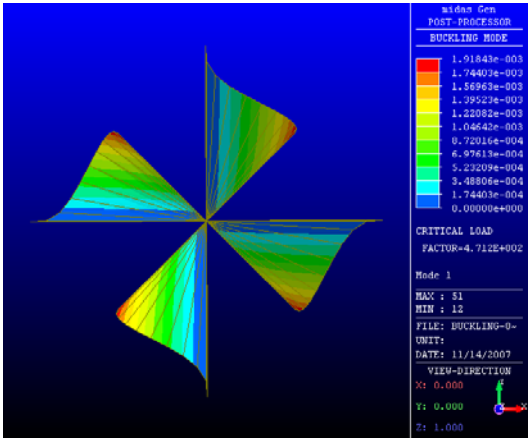
Case 3: Plate element (total 80 elements)

Buckling load

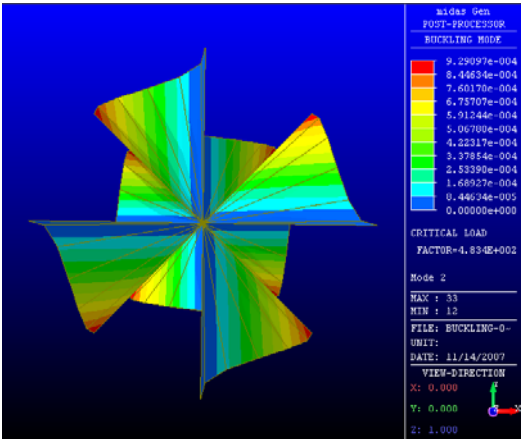
| Mode | UX | UY |
|-------------------|------------|-------------|
| BUCKLING ANALYSIS | | |
| Mode | Eigenvalue | Tolerance |
| 1 | 471,201398 | 4,4933e-010 |
| 2 | 483,422443 | 6,6010e-009 |
| 3 | 506,200573 | 8,0022e-009 |
| 4 | 532,748321 | 5,2235e-009 |



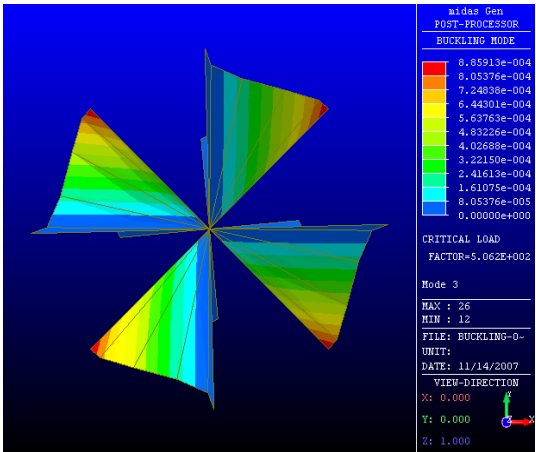
Isometric view of buckling modes of Case 3



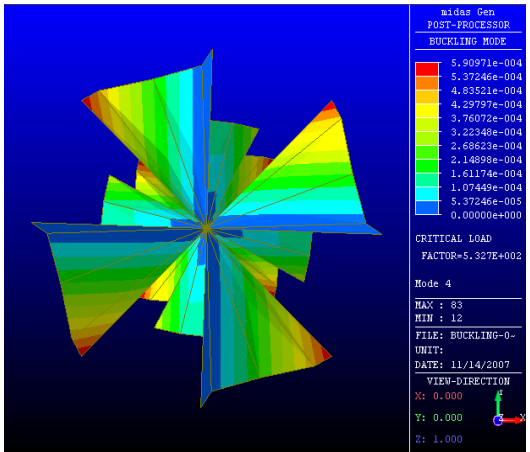
1st mode



2nd mode



3rd mode



4th mode

Perspective Top view of buckling modes of Case 3

Comparison of Results

| Case | Theoretical solution | Type of element | No. of total elements | Critical load for 1 st buckling | Unit: kN |
|------|----------------------|-----------------|-----------------------|--|----------|
| | | | | | Error |
| 1 | | Beam element | 10 | 458.086 | 0.00% |
| 2 | 458.086 | Beam element | 20 | 458.086 | 0.00% |
| 3 | | Plate element | 80 | 471.201 | 2.86% |

From the theory of elastic stability (Timoshenko and Gere [1]), the analytical solution for the tip critical load P_{cr} is defined by the following expression:

$$P_{cr} = \frac{GI_{xx}A}{I_y + I_z} = \frac{I_{xx}A}{I_y + I_z} \times \frac{E}{2(1 + \nu)}$$

where,

E = Young's modulus of elasticity

G = shear modulus of elasticity

ν = poisson's ratio

I_y = moment of inertia about local y-axis

I_z = moment of inertia about local z-axis

I_{xx} = torsional moment of inertia

Substituting the material and sectional properties into the above equation gives the following result:

$$P_{cr} = \frac{I_{xx}A}{I_y + I_z} \times \frac{E}{2(1 + \nu)} = \frac{4.339636 \times 10^4 \times 3.564 \times 10^3}{2 \times 1.350529 \times 10^7} \times \frac{200}{2(1 + 0.25)}$$

$$= 458.086 \text{ kN}$$

Reference

1. Timoshenko, S.P., and Gere, J.M., (1961). *Theory of Elastic Stability*, McGraw-Hill, New York.