## 11 ome of the Regulator: - Chumraikhali (2N-1:5x1:8m)

Purpose: - Orcinge (am Flushing)

Ang. Guround level: - 2:00 n PWD (C:56 ft PWD)

Highest W.L: - 3:5m PWD (11:8 ft PWD)

Lowest W.L: - (-) 1:7m PWD

Crest Level of embonk brent: - 5:0m PWD (16:45)

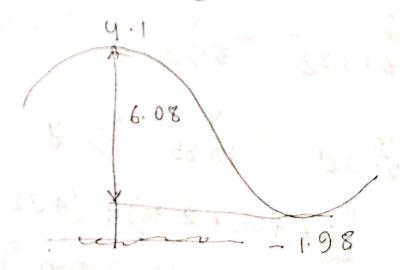
Top width of embonkment 6:0m (19:28 ft)

C/s slope: - 1:2

P/S 11:3

Invert level: - (-) 1:3m PWD (-) 1:00m PWD

Invert level: - (-) 1:3m PWD (-) 3:28 ft PWD



Catchment Area = 1000 Ha

Hydrologic Design: W.L at C/s = Agrg. Gin. Level + 1 Highest = 2:3m PWD 0  $H_{W} = 3.28 + 71.8 = 15.08$   $H_{W} = 3.28 + 7.56 = 10.851$ - 10.82 = 1.81 From figure 5, 8 = 180 cfs/vent Q = 80x5 = 400 efs/vent  $0_c = 0.315 \left(\frac{9}{8}\right)^{2/3} = 0.315 \left(\frac{400}{5}\right)^{2/3} = 5.85$  $\frac{D_{c}+D}{2} = \frac{5.85+6}{2} = 5.921$ 11.8+3.28 - 5.92 - 2.36 hrs  $\frac{6}{15.08^{\prime}} = \frac{7}{10.85} \Rightarrow \% = 4.32^{\prime}$ V = [2\*(400\*2'36)+(4'32-2'36)\*400] x3600 =9419200 eft for 12 hours Colebacat Arca - 100 = 222 cfs/vent

@ No of vent = Rrequired arrequired = C, I.A = 27\*1.9\*3.84 196 Cfs Luent given Arrea = 2100 Ha, (8'07 sq. miles) Qreq = 27 \* 1.9\* 8'07 = 413 cfs No of vent = From thumbrule 3~3:5 sq mile =) | Vent 2 vent is regained. Hydraulic Design Q = 400 efs/vent (This discharge 2.4 hours)  $a_{c} = \frac{400}{5} = 80 \text{ efs/f}$  $dc = (\frac{9^2}{9})^{24_3} = (\frac{80^2}{32 \cdot 2})^{24_3} = 5.84$  $V_e = \frac{q}{de} = \frac{80}{5.84} = 13.7 fps$ 

$$B_{c} = 5' + (2 \times 6'') = 6'$$

$$B_{1} = 6' + 2 \times 9' \text{ ton } 12' = 9.83'$$

$$d_{c} + \frac{\sqrt{c^{2}}}{2g} + Z_{c} = d_{1} + \frac{\sqrt{2}}{2g}$$

$$\Rightarrow 1.5 d_{c} + 3'' = d_{1} + \frac{\sqrt{2}}{2g}$$
At point (1) the discharge/f+ width  $a_{1}$  is given by
$$a_{1} = \frac{(80 \times 5)*}{9.83} = \frac{($$

1.5 \* 5.84 + 3' = d<sub>1</sub> + 
$$\frac{(50.5c)^2}{d_1^2 \times 2g^2}$$

=> 11.76' = d<sub>1</sub> +  $\frac{39.7}{d_1^2}$ 

Solving this d<sub>1</sub> = 2.07'

 $V_1 = \frac{4v_1}{d_1} = \frac{50.56}{2.07} = 25.15$  ft/sec

 $V_1 = \frac{4v_1}{d_1} = \frac{25.15}{32.2 * 2.07} = 3.08$ 

Length of Jump

We know,  $\frac{d_1}{d_1} = \frac{1}{2} \left[ \sqrt{1+8F^2} - 1 \right]$ 
 $\therefore \frac{d_2}{d_1} = \frac{1}{2} \left[ \sqrt{1+8F^2} - 1 \right]$ 

= 3.88

 $d_2 = 2.07 \times 3.88 = 8.04 \text{ ft}$ 

Length of Jump = 6.9 (8.04 - 2.07) = 41'

Bc + 2x 4 1 ton, 8° = 6' + \$ 2 x 41 tan 8° = 23.4' discharge/ft width at end 34.13×23.4 = 34.13×23.4 = 23.14 \* 8.92/ d2 = Tail water depth = 5.921 + 3 = 8.921 = 3'82 fps = 1'16 mis 17 should be Depth with respect to hydraulic Jump than [m5) 18 +11.  $R = 0.91 \left(\frac{a_2}{t}\right)^{1/3}$  $=0.91\left(\frac{34.13^{2}}{1.76}\right)^{1/3}$ Scour Depth = 1-25 R = 10/

0/5 11 11 = 12'

Us Scour level = V/s W.L -101 = 6.56 - 10 = -3.44 ft PWD sepur level = D/s Wil - 121 010 = 2.64' - 12' = -9.36 ft PWDcut off required = -3:28 - (-3:44) V/S 20'16' Y = -6.28 - (-9.36)= -3.081 (sog 3') Floor length and cut off by exit Gradiant H.W. L (R/s): 11.8++ PWD Retention level £C/s) = 7.56 ft pwb H = 11.8 - 7.56 = 4.241 d = 2\* H2 (GE)2×(x)2\*b2 GF = d X 2 TIX  $\frac{1}{7} = \frac{1}{d} \times \frac{1}{46\pi}$   $= \frac{2 + (4)^{2}}{(\frac{1}{7})^{2} \times (3'1416)^{2} + (130)^{2}}$   $\sqrt{A} = \frac{7 \times 4}{d \times \sqrt{A}}$  d = 0'05'< 43'->-1-30'-+9'-1Flogz Thickness

Floor length 
$$b = 130'$$

R/s depth of cutoff  $d = \frac{13\cdot12}{13\cdot12} 20'$ 

C/s

1  $d = 26'$ 

$$\frac{1}{2} = \frac{1}{2} = \frac{20}{130} = 0.15$$

$$c = 19 \left( \frac{D}{b} \right)^{1/2} + \frac{d+D}{b}$$

$$=19\left(\frac{18.5}{130}\right)^{12} + \frac{13.5}{130} = 0.1$$

$$P_{c_1} = 727. + 27$$

$$P_{c_1} = 38 - 2.5 - 2 = 33.5.7.$$

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$$P_3 = \frac{49}{100} \times 6 = 2.94'$$

$$P_2 = \frac{53\%}{100} \times 6 = 3'18'$$

$$P_{4} = \frac{33'F}{100} \times 6 = 2'01'$$

At point (3) 
$$t_3 = \frac{2.94}{1.4} = 2.1'$$

(1) (4)  $t_4 = \frac{2.01}{1.4} = 1.43'$ 

Floor length = 14.0 m $F_R = 3.31$ 

 $B_2 = 9 m | 00$ 

Pg : 100 x 6 = 9-991

1-6 = 50 E = 3 (E) tring #