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Outline of Presentation

- Components
- Basic Design Requirements
- Allowable Stresses
- Design of Unreinforced Masonry
- Design of Reinforced Masonry
- Stability Requirements
- Strength Design of Slender Walls and Shear Walls
- Earthquake Resistant Design
- Strengthening of Masonry Buildings for Earthquake
- Confined Masonry

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Masonry Structures

THE WORLD BANK
IBRD • IDA | WORLD BANK GROUP

Session 25

Date: 6 February 2022

Professor, Department of Civil Engineering, BUET Raquib Ahsan, PhD

S-8A SEng PRP Training Program



Relevant Chapters of BNBC 2020

- Part 5 Chapter 2 Sec 2.2.4
- Part 6 Chapter 7
- Part 7

Components



Mortar

Components

Table 6.7.1: Mix Proportion and Strength of Commonly used Mortars

Masonry unit

Mortar

Grout

Grade of	Mix Prop	Mix Proportion by	Minimum Compressive Strength at 28
Mortar	Volun	Volume 1, 2	days, N/mm²
	Cement	Sand	
M1		က	10
M2		4	7.5
M3	1	2	S
M4		9	8
M5		7	2
M6		8	1
			BELLEVILLE OF THE BELLEVILLE O
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Metal ties and anchors

Reinforcement

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Grout

ASTM C476

Volume	
ð	ı
Proportions	
Grout	l
Conventional	
TABLE 1	

Туре	Parts by Volume of Portland Cement or Biended Cement	Parts by Volume of Hydrated Lime or Lime Putty	Aggr Measured in a Dan	Aggregate, Measured in a Damp, Loose Condition
			Fine	Coarse
Fine grout	-	0-1/10	21/4 –3 times the sum of the volumes of the cementitious	
Coarse grout	-	0-7/0	materials 214 –3 times the sum of the volumes of the cementitious materials	1–2 times the sum of the volumes of the cementitious materials

Masonry Units

- Common building clay bricks (BDS 208)
- Burnt clay hollow bricks (BDS 1263)
- Burnt clay facing bricks (BDS 1250)
- Hollow concrete blocks (BDS EN 772)
- Others



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ASTM A82/A82M: Cold Drawn Steel Wire for Concrete

Reinforcement

Reinforcement

ASTM A996/A996M: Rail-Steel Deformed and Plain Bars

Basic Design Requirements

ASTM A996/A996M: Axle-Steel Deformed and Plain Bars

ASTM A706/A706M: Low-Alloy Steel Deformed Bars

ASTM A767/A767M: Zinc-Coated (Galvanized) Steel Bars

ASTM A775/A775M: Epoxy - Coated Reinforcing Steel Bars

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Design Considerations

- Working stress design
- Linear stress-strain distribution
- Small eccentricity of loading

Metal Ties and Anchors

- ASTM A82/A82M: Wire Anchor and Ties
- ASTM A1008/A1008M: Sheet Metal Anchors and Ties







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02/06/2022 ICC INTERNATIONAL CODE COUNCIL® $L_{eff} = 2.0L$ $L_{eff} = 0.9L$ Cross wall Cross wall **Effective Length** URP | RAJUK | S-8 COMPONENT $L_{eff}=1.0L$ Cross wall L > H/8 $L_{eff} = 0.8L$ Cross wall $L_{eff} = 1.5L$ Cross wall L' > H/8Opening 02/06/2022

Steel beam

Column: $w \le 3t$

and date

Wall: w > 3t

Effective Height

Effective Height of a Wall with Opening

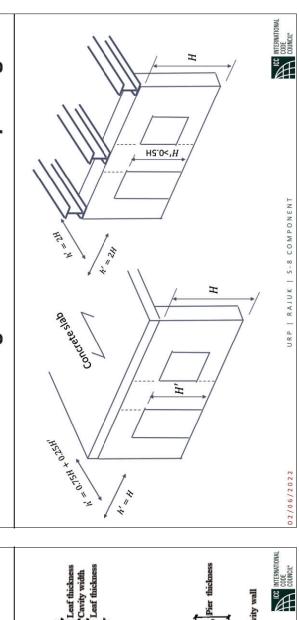
Effective Thickness

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Case (b)

Case (a)



t₁ Leaf thickness

Pier width

Pier width

Pier thickness

Cavity wall

Pier spacing

Pier spacing
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Leaf thickness t₂ Cavity width

Pier spacing

Wall thickness

Loads

Loads and load combination according to Part 6 Chapter 2.

 $t_{eff} = kt_w$

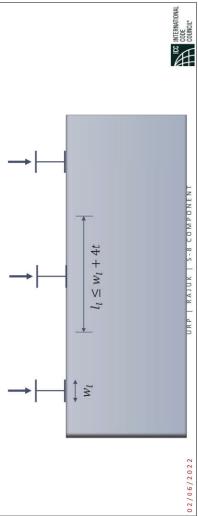
Effective Thickness

Pilaster

Main wall

 d_{l}

 The angle of dispersion of vertical load on walls shall be taken as not more than 30° from the vertical.



t_p/w_p $t_p/t_w = 1$ $t_p/t_w = 2$ t_p/t_w $= 6$ 1.0 1.4 2.0 $= 2.0$ $= 8$ 1.0 1.3 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.2 1.7 1.2 1.7 1.2 1.2 1.2 1.3 $1.$	d _M /d ₁	$t_p/t_w=1$		
802 7 7 7 7 7 7 7	ω &	The second secon	$t_p/t_w=2$	$t_p/t_w=3$
	80	1.0	1.4	2.0
		1.0	1.3	1.7
	10	1.0	1.2	1.4
	15	1.0	1.1	1.2
st Linear interpolation is permitted for obtaining intermediate values of k	20 or more		1.0	1.0
	* Linear interpola	tion is permitted for obtain	ing intermediate valu	es of k

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Minimum Design Demension

- Load bearing walls: $t \ge 250 \text{ mm}$
- Parapet:
- $t \ge 200 \, \text{mm}$
 - $h \le 4t$

Slenderness Ratio

- Walls:
- Slenderness ratio = lesser of $^{h'}/_{teff}$ or $^{Leff}/_{teff}$
 - Slenderness ratio ≤ 20
- Columns:
- Slenderness ratio = $h'/_{teff}$
 - Slenderness ratio ≤ 12



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Allowable Compressive Stresses

- If no special inspection all the allowable stresses shall be reduced by 50%.
- Axial compressive stress

$$a = \frac{f_m'}{5} \left[1 - \left(\frac{h'}{42t} \right)^3 \right]$$

Allowable Stresses

• RM

$$= \left(\frac{f_m'}{5} + \frac{A_s}{1.5A_n'} F_{sc}\right) \left[1 - \left(\frac{h'}{42t}\right)^3\right]$$

Compressive stress in Flexure

$$F_b = 0.33 f_m' \le 10 \,\mathrm{N/mm}^2$$

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Allowable Tensile Stress

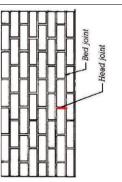
	Normal to
xural Tension, Ft	Normal to Bed Joints
Table 6.7.2: Flex	Masonry

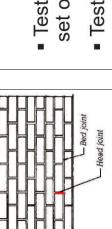
Masonry	Normal to Bed Joints N/mm²	Normal to Head Joints N/mm²
Solid Units	0.20	0.40
Hollow Units	0.12	0.25
Table 6.7.3: Tens	Table 6.7.3: Tension Normal to Head Joints, Ft	

	1
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\$	1
Normal	
able 6.7.3: Tension Normal to Head Joints,	
7.3:	Maccon
9	2
able	

Concrete Uni N/mm²	0.40	0.25
Clay Units N/mm²	0.35	0.22
Masonry	Solid Units	Hollow Units

For Types M₃ and M₄ mortar, the values shall be reduced by 25 percent.







When 50% of the allowable

ASTM E447: Prism Test

Compressive Strength of Masonry

- Test prior to construction: A set of five masonry prisms
- Testing during construction:
- When full allowable stresses are used in design: A set of three prisms for each 500 square meters of wall.
- stresses are used in design: No

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Allowable Stresses in Reinforcement

Allowable Shear Stress

Shear stress for flexural members

 $F_{\nu} = 0.083 \sqrt{f_m'}$ $F_v = 0.25 \sqrt{f_m'}$

· URM :

• RM:

- Tensile stress
- Deformed bars: $F_{\rm s}=0.5f_{\rm y}\le 165~{\rm N/mm^2}$
- Ties, anchors and plain bars: $F_{\rm S}=0.4f_{\rm y}\leq 135~{\rm N/mm^2}$
- Compressive stress
- Shear walls: $F_{sc} = 0.4f_y \le 165 \text{ N/mm}^2$
- Flexural members: $F_{sc}=0.5f_y \le 165 \,\,\mathrm{N/mm^2}$
- Bond stress
- Plain Bars: 0.30 N/mm²
- Deformed Bars: 1.0 N/mm²

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 $\leq 0.40 \text{ N/mm}^2$

• For clay units: $F_v = 0.025 \sqrt{f_m'}$

• URM

Shear stress for shear walls

0.20 N/mm²

 M1 or M2 Mortar: For concrete units:

M3 Mortar:

 $\leq 0.75 \text{ N/mm}^2$ $\leq 0.25 \text{ N/mm}^2$

Modulus of Elasticity

a) Modulus of Elasticity for Masonry:

$$E_m = 750 f_m' \le 15,000 \text{ N/mm}^2$$

b) Modulus of Elasticity for Steel

$$E_{\rm s} = 2,00,000 \, \, \rm N/mm^2$$

c) Shear Modulus of Masonry

$$G = 0.4E_m \text{ N/mm}^2$$

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Allowable Shear Stress for RM Shear Walls

F
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Table 6.7.4: Allowable Shear Stress for Reinforced Masonry Shear Walls. $F_{\cdot\cdot\cdot}$
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Masonry Wall	PA/W	F _v , N/mm²	Maximum Allowable N/mm²
Masonry taking	<1 <1	$\frac{1}{36} \left(4 - \frac{M}{Vd} \right) \sqrt{f_m'}$	$\left(0.4-0.2\frac{M}{Vd}\right)$
all shear	≥ 1	$0.083\sqrt{f_m'}$	0.17
Reinforcement	^ 1	$\frac{1}{24} \left(4 - \frac{M}{Vd} \right) \sqrt{f_m'}$	$\left(0.6-0.2\frac{M}{Vd}\right)$
taking ali snear	≥ 1	$0.125\sqrt{f_m'}$	0.37

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Design of Reinforced Masonry

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Assumptions and Stresses

- Assumptions:
- a) Masonry carries no tensile stress.b) Reinforcement is completely bonded.
- Members Subjected to Axial Compression:

$$f_a = \frac{P}{A_e}$$

• Members Subjected to Shear Force:
$$f_v=\frac{v}{bjd}; \quad A_v=\frac{sV}{F_sd}; \quad s\leq \frac{d}{2} \text{ or } 600 \text{ mm}$$

Members Subjected to Flexural Stress:

$$f_b = \frac{M}{bd^2} \left(\frac{2}{jk}\right); \qquad f_S = \frac{M}{A_S j_S}$$



Design of Unreinforced Masonry

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Design of Unreinforced Masonry

■ Members Subjected to Axial Compression:
$$f_a = \frac{P}{A_e}$$

Members Subjected to Flexure:

$$f_b = \frac{Mc}{I}$$

Members Subjected to Shear:

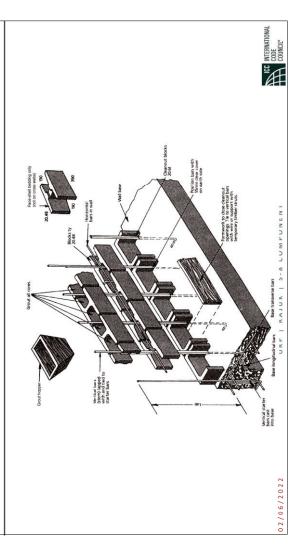
$$f_v = \frac{V}{A_e}$$

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Reinforcement Requirements and Details



Stability Requirements

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Stability Requirements

Height to width ratio of building does not exceed

Table 6.7.9: Thickness and Spacing of Stiffening Walls

5
Exceed 1 to 3 storeys (m) (mm)
3.2
3.2
3.4
5.0

* Storey height and maximum spacing as given are centre to centre dimensions.

Reinforcement Requirements and Details

- Maximum reinforcement size:
- . 35 mm
- 6% of cell area without splice
 - 12% of cell area with splice
- Spacing of longitudinal reinforcement:
- Clear distance between parallel bars $\geq d_b$ or 25 mm
- Clear distance from any surface of masonry unit ≥ 6 mm for fine grout or 12 mm for coarse grout
- Clear Cover
- 20 mm when not exposed to weather c 0 3
 - 40 mm when exposed to weather
- 50 mm when exposed to soil

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$$M_{cr} = Sf_r$$

When $M_{ser} \leq M_{cr}$,

 $\Delta_S = \frac{5M_S h^2}{48E_m I_g}$



When $M_{cr} < M_{ser} < M_n$, $\Delta_{s} = \frac{5M_{cr}h^2}{48Em^{l}g} + 5\frac{(M_{ser} - M_{cr})h^2}{48Em^{l}cr}$

Fully Grouted

Partially Grouted

 $\Delta_s \le 0.007h$

Table 6.7.13: Values of the Modulus of Rupture, $f_{\cdot \cdot}$

			COUNCIL
Partially Grouted	Not allowed	$0.21\sqrt{f_m'} \le 0.65 \mathrm{N/mm^2}$	PONENT
Fully Grouted	$0.17\sqrt{f_m'} \le 0.65 \mathrm{N/mm^2}$	$0.33\sqrt{f_m'} \le 1.2 \text{ N/mm}^2$	URP RAJUK S-8 COMPONENT
Type of Masonry	Solid Masonry	Hollow Unit Masonry	02/06/2022

Design of Shear Walls

- lacktriangle For axial load axial load with flexure $\phi=0.65$
- lacktriangle For members with $f_{oldsymbol{
 u}}$ less than 410 N/mm 2 and with symmetrical reinforcement, ϕ may be increased linearly to 0.85 as ϕP_n decreases from $0.10f_m'A_e$ or $0.25P_b$ to zero.
- ullet For shear $\phi=0.60$. The shear strength reduction factor may be strength exceeds the shear corresponding to development of its nominal flexural strength for the factored load combination. increased to 0.80 for any shear wall when its nominal shear

Strength Design of Slender Walls and Shear Walls

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Design of Slender Walls

 $f_m' \le 40 \text{ N/mm}^2$ $\frac{P_w + P_f}{A_g} \le 0.04 f''_w;$

 $t \ge 150 \, \mathrm{mm}$

 $\rho_{max} \le 0.5 \rho_b$

$$M_u = \frac{w_u h^2}{8} + P_u - \frac{e}{2} + \left(P_{uw} + P_{uf}\right) \Delta_u$$

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Nominal Strength

 $\blacksquare f'_m$ shall not be less than 7 N/mm² or greater than 20 N/mm².

 \bullet Axial strength: $P_o=0.85f_m'(A_e-A_s)+f_yA_s$

Shear strength:

Earthquake Resistant Design

Table 6.7.14: Maximum Nominal Shear Strength Values

$\frac{V_n}{A_e\sqrt{f_m}}$	72.0	48.0
$\frac{M^*}{Vd}$	≤ 0.25	≥1.00

* M is the maximum bending moment that occurs simultaneously with the shear load V at the section under consideration. Interpolation may be by straight line for M/Vd values between 0.25 and 1.00.

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General

- All masonry structures constructed in the Seismic Zones 2, 3 and 4 shall be designed in accordance with these provisions.
- Crushing strength not less than 12 N/mm² shall be used.
- Mortar not leaner than M₃ shall be used.

Boundary Member

- Boundary members shall be provided when the failure mode is flexure and the maximum extreme fibre stress exceeds $0.2f_m'$.
- corresponding masonry compressive stress exceeds $\ 0.4f_m^\prime.$ The minimum length of the boundary member shall be 3 times the When the failure mode is flexure, boundary member shall be provided to confine all vertical reinforcement whose thickness of the wall.
- Boundary members shall be confined with minimum of 10 mm diameter bars at a maximum of 200 mm spacing.



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Band

- lacktriangle The band shall be made of reinforced concrete with $f_{\rm c}^{\prime}$ not less than 20 N/mm2 or reinforced brickwork in cement mortar not leaner than 1: 4.
- The bands shall be to the full width of the wall and not less than 75 mm in depth and shall be reinforced.

Table 6.7.16: Band Reinforcement

Zones	rialli Miliu Steel Bars	nign Strengtn Deformed Bars	LINKS
2,3	2 - 12 mm dia, one on each face of the wall with suitable cover	2 - 12 mm dia, one on each face 2 - 10 mm dia, one on each face 6 mm dia, 150 mm c/c of the wall with suitable cover of the wall with suitable cover	6 mm dia, 150 mm c/c
4	2 - 16 mm dia, one on each face of the wall with suitable cover	2 - 16 mm dia, one on each face 2 - 12 mm dia, one on each face 6 mm dia, 150 mm c/c of the wall with suitable cover of the wall with suitable cover	6 mm dia, 150 mm c/c

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Roof

Lintel Band

Lintel Band

Floor

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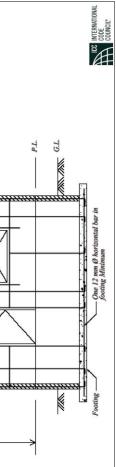
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Provisions for Seismic Zone 4

- constructed in accordance with requirements for Seismic Zone 2 and 3. All masonry structures built in Seismic Zone 4 shall be designed and
- The sum of the areas of horizontal and vertical reinforcement shall be at least 0.002 times the gross cross-sectional area of the wall.
- The area of reinforcement in either direction shall not be less than 0.0007 times the gross cross-sectional area of the wall.
- The spacing of reinforcement shall not exceed 1.20 m.
- The diameter of reinforcing bar shall not be less than 10 mm.



Provisions for Seismic Zone 2 and 3

- Vertical reinforcement of at least 12 mm diameter shall be provided continuously from support to support at each corner, at each side of each opening, at the ends of walls and at a maximum spacing of 1.2 m horizontally throughout the wall
- Horizontal reinforcement not less than 12 mm diameter shall be provided:
- · at the bottom and top of wall openings and shall extend at least 40 bar diameters, with a minimum of 600 mm, past the opening,
- continuously at structurally connected roof and floor levels and at the top of walls,
- at the bottom of the wall or in the top of the foundations when dowelled to the wall

One 12 mm Ø min., at Bond Beam Lintel Reinforcement: (may be used as part of required horizontal reinforcement) Vertical Reinforcement: Min. One 12 mm Ø or Equiv. at 1.2 m c/c max. Typ. - Horizontal Reinforcement:
One 12 mm @ min. or Equiv.
at 3.00 m c/c max, for Seismic
Zone 2 (at 1.2 m c/c max, for
Seismic Zone 3) Jamb Reinforcement: One 12 mm Ø or Equiv., min 40d or 600 mm min. Typ. One 12 mm Ø, min. at Bond Beam

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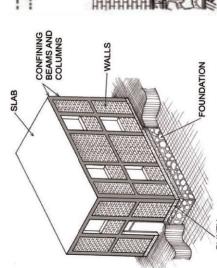
Strengthening of Masonry Buildings

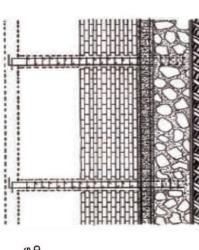
Confined Masonry

for Earthquake



Confined Masonry





Seismic	No. of		Strengthening Arrangements to be Provided.
Zones	Storey		
1	Up to 4	a	a) Masonry mortar shall not be leaner than M_3
2, 3	Up to 2 with	a)	Masonry mortar shall not be leaner than M_3
	pitched roof	(q	By lintel and roof band (Sec 7.8.6.3)
		C	By vertical reinforcement at corners and junctions of walls (Sec 7
		P	d) Bracing in plan at tie level for pitched roof st
	3 to 4	a	a) Masonry mortar shall not be leaner than $M_{ m 3}$
		þ	By lintel and roof band (Sec 7.8.6.3)
		0	By vertical reinforcement at corners and junctions of walls (Sec 7
		ਰ	Vertical reinforcement at jambs of openings (Sec 7.8.6.5)
		(e	Bracing in plan at tie level for pitched roof st
4	Up to 4	a	Masonry mortar shall not be leaner than M_3
		Q	b) By lintel and roof band (Sec 7.8.6.3)

7.8.6.4)

7.8.6.4)

• At tie level all the trusses and the gable end shall be provided with diagonal bracing in plan so as to transmit the lateral shear due to earthquake force to the gable walls acting as shear walls at the ends.

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c) By vertical reinforcement at corners and junctions of walls (Sec 7.8.6.4)

d) Vertical reinforcement at jambs of openings (Sec 7.8.6.5)

Bracing in plan at tie level for pitched roof*

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Vertical and Horizontal Confining Elements

- Vertical confining elements should be placed:
- (a) at the free edges of each structural wall element;
- (b) at both sides of any wall opening with an area of more than $1.5 \,\mathrm{m}^2$;
- (c) within the wall, if necessary, in order not to exceed a spacing of 5 m between the confining elements;
- (d) at the intersections of structural walls, wherever the confining elements imposed by the above rules are at a distance larger than 1.5 m.
 - Horizontal confining elements shall be placed in the plane of the wall at every floor level and in any case with a vertical spacing of not more than 4 m.

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Confined Masonry Details

- Confining elements should have a cross-sectional area not less than 0.02 m², with a minimum dimension of 150 mm in the plan
- The longitudinal reinforcement may not have a cross-sectional area less than 300 mm², nor than 1 percent of the crosssectional area.
- Stirrups not less than 6 mm in diameter and spaced not more than 300 mm should be provided.
- Column ties should preferably have 135° hooks. . At a minimum, 6 mm ties at 200 mm spacing should be provided. It is recommended to use 6 mm ties at 100 mm spacing in the column end-zones



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Comparison with RC Frame

Component	Confined masonry construction	RC frame construction
Gravity and lateral load- resisting system	Masonry wall: Main load bearing component. Tie beams and columns: Confining component only.	Beams and columns: Main load bearing components. Masonry wall: Non-load bearing infill only.
Foundation construction	Strip footing	Isolated footing
Superstructure construction sequence	First walls and then columns and beams and floors at last.	First columns, then beams and floors and walls at last.

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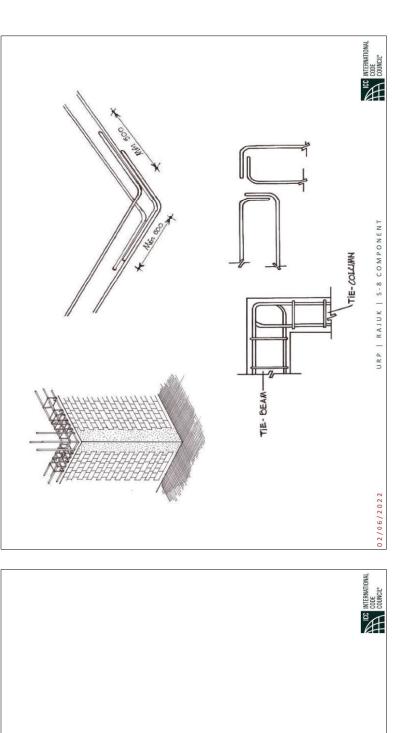
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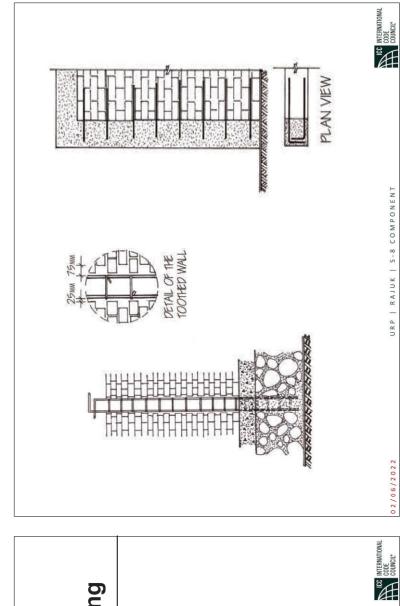


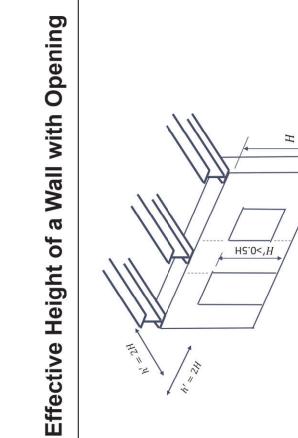
Architectural Guideline

- Building length-to-width ratio should not exceed 4.
- The walls should be continuous up.
- Openings should be placed in the same position.
- At least two fully confined walls in each direction.
- Minimum wall density and maximum building height:
- For seismic zones 1 and 2: 2% and 4-storey
 - For seismic zone 3: 4% and 3-storey
- For seismic zone 4: 5% and 2-storey

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Questions? Thank you

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Effective Height of a Wall with Opening