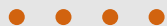


Dynamic Line Rating without field devices

David Carnicero Príncipe
Director: Jesús Varela Sanz
Co-director: Matteo Troncia



2nd of July 2024





Index

1. Context
2. Motivation
3. Objectives
4. Work State
5. Program



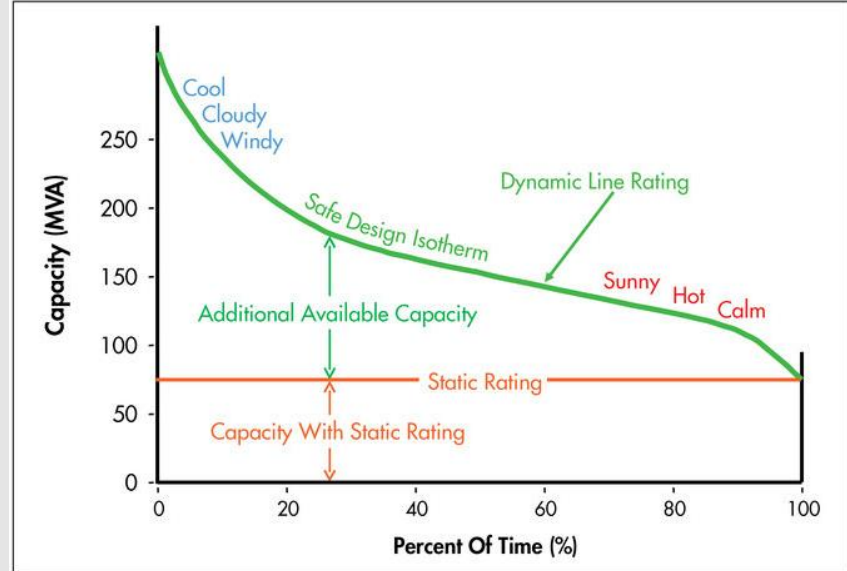
Static Line Rating

- ◇ Fixed Current Limit
- ◇ Calculated with Limit Conditions
- ◇ Summer and Winter Limit

Dynamic Line Rating

- ◇ Variable Current Limit
- ◇ Calculated with Real Time Conditions
- ◇ It depends on weather

Figure 1: Tapping into existing capacity above the static rating



Source: Valley Group

Dynamic Line Rating

1. CIGRE Technical Brochures: Guide for thermal rating calculations of overhead lines



2. IEEE Standard for Calculating the Current-Temperature Relationship of Bare Overhead Conductors

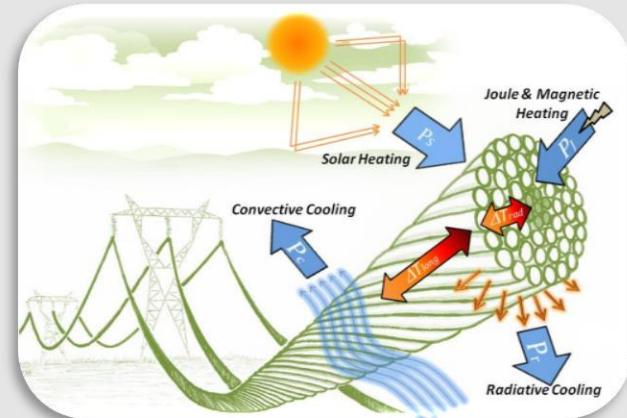


$$P_j + P_s = P_c + P_r$$

$$I^2 \cdot R + \text{Sun} = \text{Wind} + \text{Thermometer}$$



$$I = \sqrt{\frac{P_s - P_c - P_r}{R(T_{MAX})}}$$



Motivation



Current State

- High Cost
- Slow and Complex Instalaton
- Unusable for the Operator
- Conexión Lost



Thesis Approach

- Third Parties Weather Data
- No Equipmanet Needed
- Suitable For The Operator



Objectives



Weather
Measurement
Accuracy

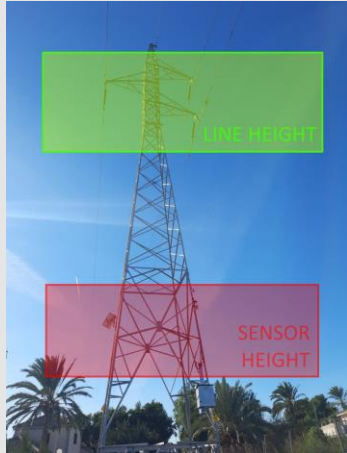


DLR
Equations
Inputs



Results
for Grid
Operation

Weather Measurement Accuracy



Objectives

- Field Devices Height Influence
- Weather Parameters Extrapolation
 - Orography
 - Annual Season
 - Vegetation



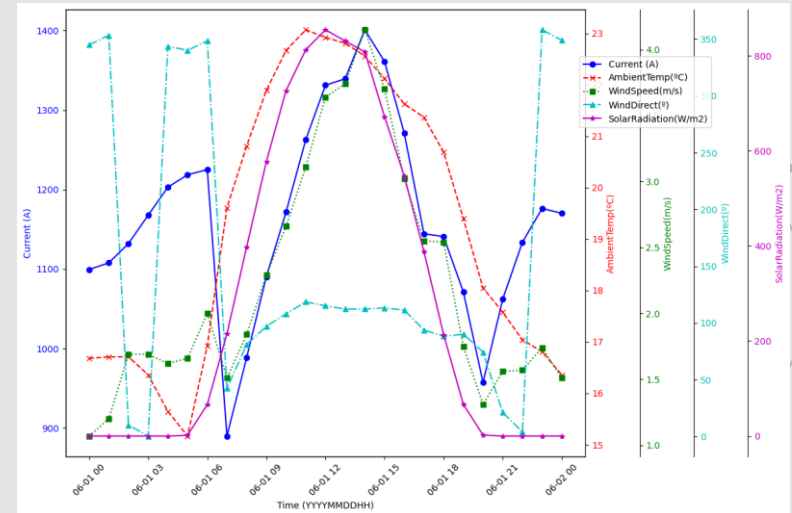
DLR Equations Inputs

Input

Conductor characteristics
Conductor outside diameter (mm)
Core diameter (mm)
Outer strand diameter (mm)
Maximum allowable conductor temp. (°C)
Emissivity
Solar absorptivity
Conductor ac resistance at 25°C (Ω/m)
Conductor ac resistance at 75°C (Ω/m)
Ambient conditions
Ambient air temperature (°C)
Wind speed (m/s)
Wind angle of attack (°)
Inclination β to the horizontal (°)
Height above sea level y (m)
Solar conditions
Azimuth of line (°)
Latitude (°)
Clearness of Atmosphere
Date
Reflectance of the ground (albedo)

Influence

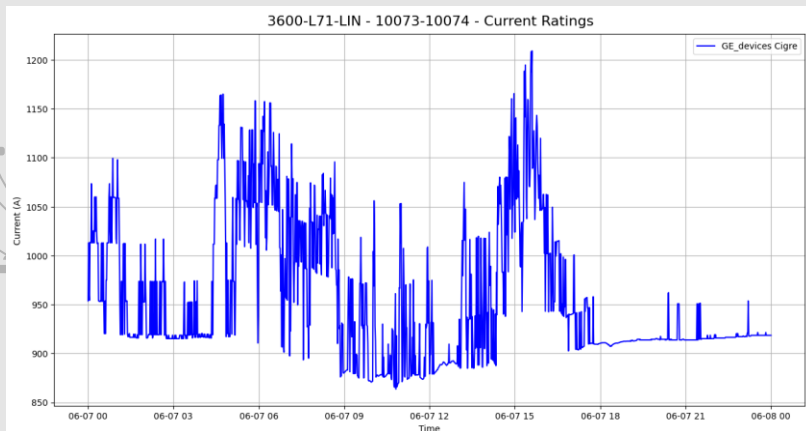
- Conductor Aging
- Ambient Pollution
- Operation History



Results for Grid Operation

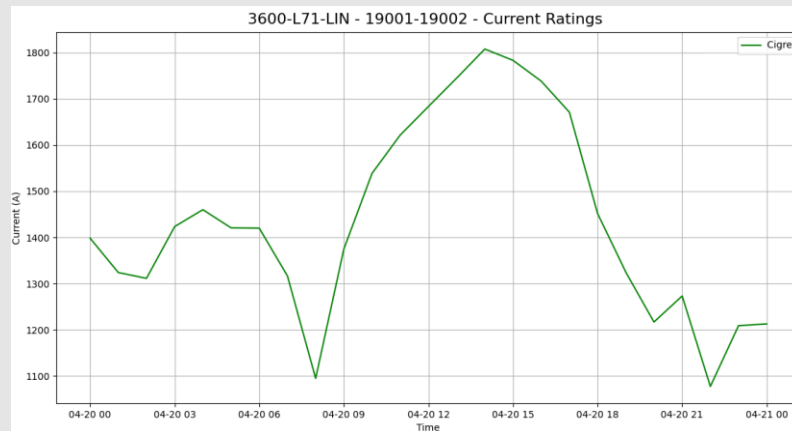
Actual DLR Output

Unstable Current Rating
Not Used

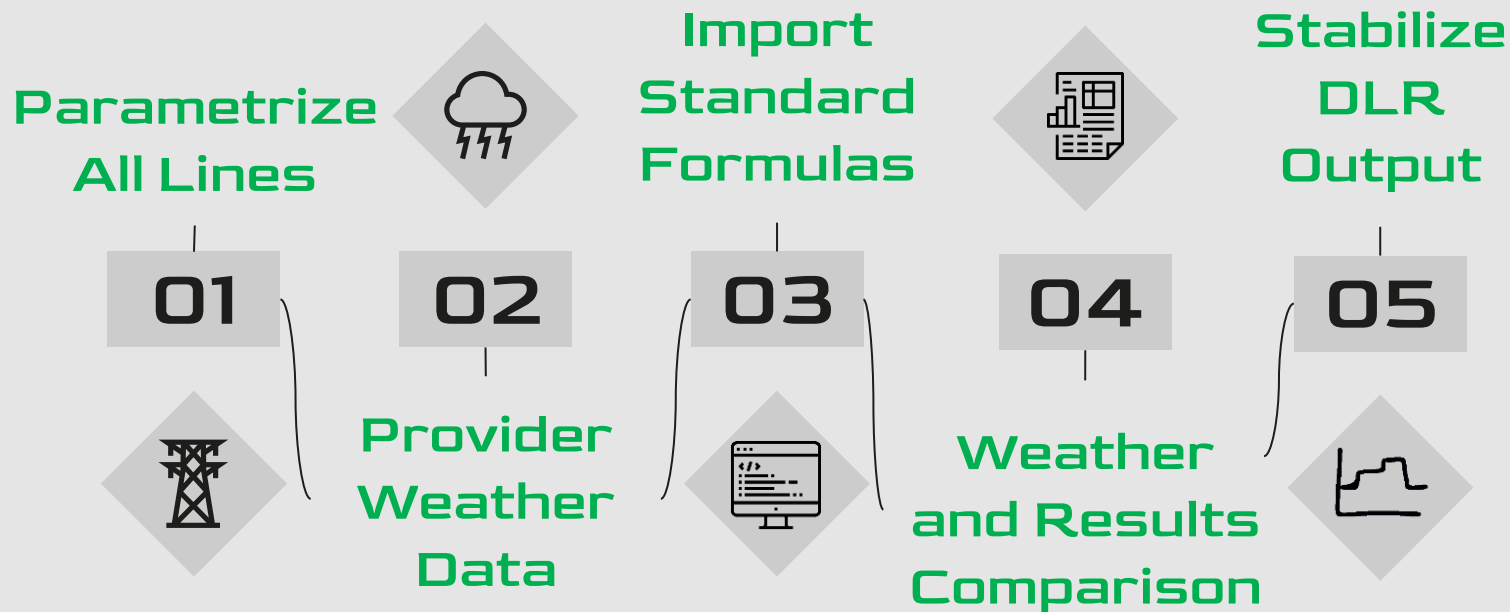


Thesis DLR Output

Stable Current Rating
Weather Forecasting
Forecasting Time Accuracy



Project Plan



• • • •

CURRENT PROGRESS

Parametrize All Lines

- Line ID
- Span ID
- Coordinates
- Conductor Type

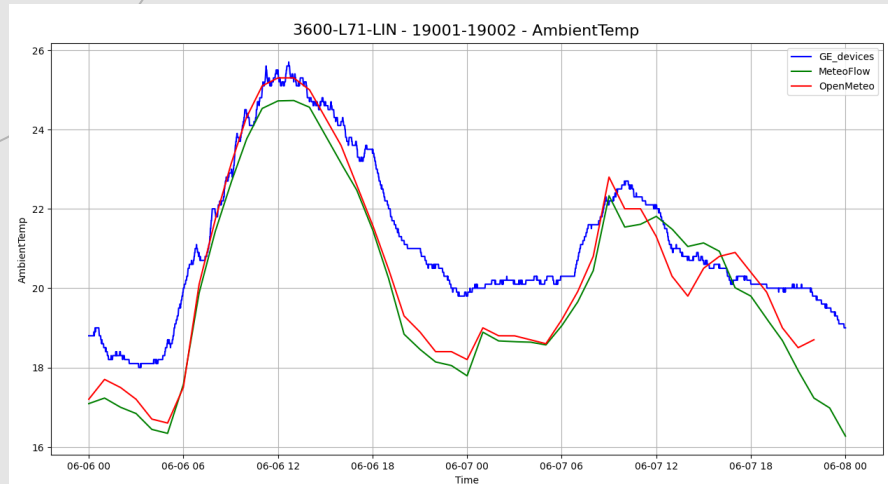
CODE	Conductor Diameter (mm)	Outer Wire Diameter (mm)	DC Resistance at 20°C (ohm/km)	DC Resistance at 75°C (ohm/km)
LA 175 OSTRICH	17.28	2.73	0.185	0.226
LA 180	17.5	2.5	0.1962	0.199
LA 280 HAWK	21.79	3.44	0.117	0.142
LA 300 HEN	22.42	3.2	0.116	0.142

```
1 Span, Latitude, Longitude, Angle, Elevation, SupportHeight, ConductorType, DeviceGE
2 18067-10068, 38.28067228313209, -0.7168867426924255, -125.86191453581152, 136.0, 21, LA 280 HAWK, no
3 10068-10069, 38.27913500356807, -0.7196091537613991, -125.58991971892864, 132.0, 21, LA 280 HAWK, no
4 10069-10070, 38.27737316169882, -0.7227450609474958, -125.59015024341508, 134.0, 21, LA 280 HAWK, no
5 10070-10071, 38.27501153839174, -0.726948046025888, -125.59335795634874, 115.0, 21, LA 280 HAWK, no
6 10071-10072, 38.27291721210064, -0.7306750076279667, -125.59432742888876, 126.0, 21, LA 280 HAWK, no
7 10072-10073, 38.271238913070206, -0.733661300553164, -125.59754904203258, 116.0, 21, LA 280 HAWK, no
8 10073-10074, 38.26960936583586, -0.7365626914224481, -125.552388293997, 117.0, 21, LA 300 HEN, yes
9 10074-10075, 38.26822462336136, -0.7390304188410167, -125.55488279842046, 120.0, 21, LA 280 HAWK, no
10 10075-10076, 38.26653754651623, -0.7420366283623947, -125.55600514842604, 118.0, 21, LA 280 HAWK, no
11 10076-10077, 38.26469796568913, -0.7453143306043013, -125.5582045634629, 114.0, 21, LA 280 HAWK, no
12 10077-10078, 38.26308873966309, -0.7481812905915681, -125.560649837833, 113.0, 21, LA 280 HAWK, no
13 10078-10079, 38.26113672985558, -0.7516585683026649, -125.56174242627462, 97.0, 21, LA 280 HAWK, no
```



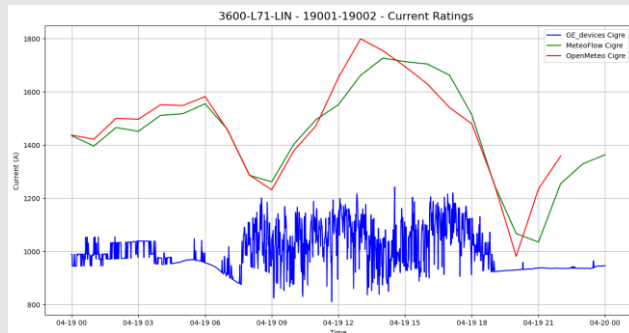
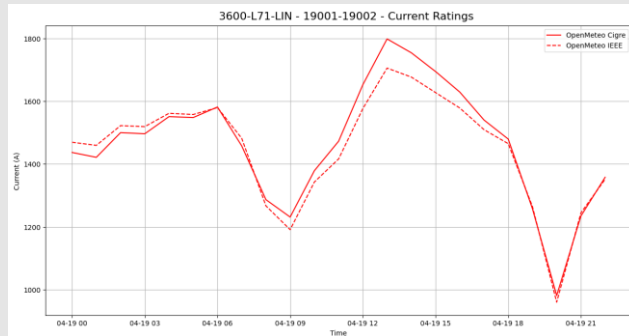
CURRENT PROGRESS

Get Weather Data from Providers



CURRENT PROGRESS

Import Standard Equations

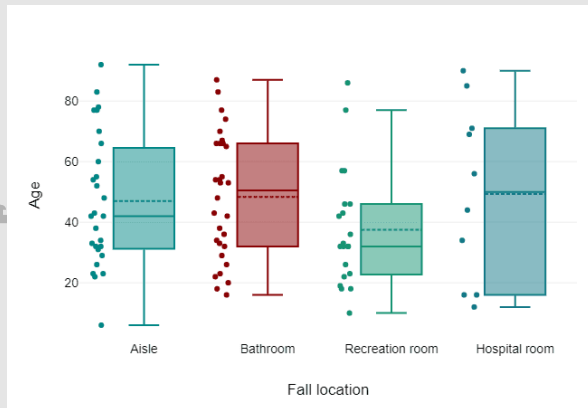


Convective heat loss	Solar heat gain
$T_f = 0.5 \cdot (T_s + T_a)$	$\delta_s = 23.4 \cdot \sin[2 \cdot \pi \cdot (284 + N^*)/365]$
$\lambda_f = 2.368 \cdot 10^{-2} + 7.23 \cdot 10^{-5} \cdot T_f - 2.763 \cdot 10^{-8} \cdot T_f^2$	$H_s = \arcsin(\sin(\varphi) \sin(\delta_s) + \cos(\varphi) \cos(\delta_s) \cos(Z))$
γ_0 (density of the air at sea level)	$\gamma_s = \arcsin(\cos(\delta_s) \cdot \sin(Z) / \cos(H_s))$
$\gamma = \frac{1.293 - 1.525 \cdot 10^{-4} \cdot \gamma + 6.379 \cdot 10^{-9} \cdot \gamma^2}{1 + 0.00367 \cdot T_f}$	$\eta = \arccos[\cos(H_s) \cdot \cos(\gamma_s - \gamma_c)]$
$\mu_f = (17.239 + 4.635 \cdot 10^{-2} \cdot T_f - 2.03 \cdot 10^{-5} \cdot T_f^2) \cdot 10^{-6}$	$I_{B(0)} = N_s \cdot \frac{1280 \cdot \sin(H_s)}{\sin(H_s) + 0.314}$
$v_f = \mu_f / \gamma$	$I_{B(y)} = I_{B(0)} \cdot \left[1 + 1.4 \cdot 10^{-4} \cdot y \left(\frac{1367}{I_{B(0)}} - 1 \right) \right]$
$R_s = d/2 \cdot (D - d)$	$I_d = (430.5 - 0.3288 \cdot I_{B(y)}) \cdot \sin(H_s)$
$Re = V \cdot D / v_f$	
$B; n$ (Table 4)	
$Nu_{90} = B \cdot Re^n$	$I_T = I_{B(y)} \cdot \left(\sin(\eta) + \frac{\pi}{2} \cdot F \cdot \sin(H_s) \right) + I_d \cdot \left(1 + \frac{\pi}{2} \cdot F \right)$
$Nu_\delta = Nu_{90} \cdot (0.42 + 0.58 \cdot \sin(\delta)^{0.90})$	
$P_{c,forced} = \pi \cdot \lambda_f \cdot (T_s - T_a) \cdot Nu_\delta$	
$Gr = \frac{D^3 \cdot (T_s - T_a) \cdot g}{(T_f + 273) \cdot v_f^2}$	
$Pr = c_f \cdot \mu_f / \lambda_f$	$P_s = \alpha_s \cdot I_T \cdot D$
$A; m$ (Table 5)	Electrical resistance
$Nu_{nat} = A \cdot (Gr \cdot Pr)^m$	$R_{ac}(T) = R_{ac}(T_1) + (T - T_1) \cdot \frac{R_{ac}(T_2) - R_{ac}(T_1)}{T_2 - T_1}$
$Nu_\beta = Nu_{nat} \cdot (1 - 6.76 \cdot 10^{-6} \cdot \beta^{2.5})$	Current calculation
$P_{c,nat} = \pi \cdot \lambda_f \cdot (T_s - T_a) \cdot Nu_\beta$	$I = \sqrt{\frac{P_r + P_c - P_s}{R_{ac}}}$
$P_c = \max(P_{c,forced}; P_{c,nat})$	
Radiative heat loss	
$P_r = \pi \cdot D \cdot \sigma_B \cdot \epsilon_s \cdot [(T_s + 273)^4 - (T_a + 273)^4]$	

NEXT STEPS

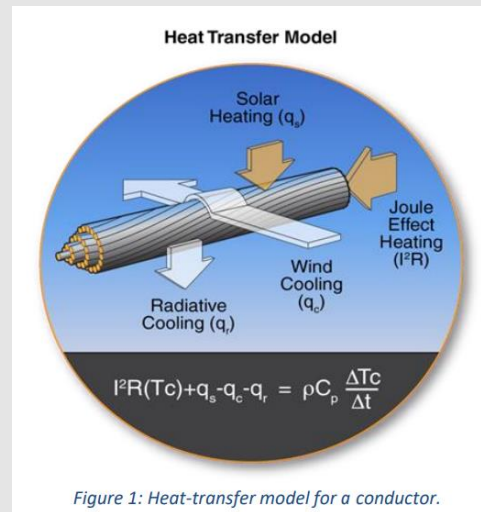
Weather and Results Comparison

- Accuracy Comparison
- Comparison with Field Devices
- Comparison between Providers



Stabilize the Output

- Grid Operator Needs
- Thermal Inertia



Dynamic Line Rating without field devices

David Carnicero Príncipe
Director: Jesús Varela Sanz
Co-director: Matteo Troncia



2nd of July 2024

