



A Hybridizable Discontinuous Galerkin formulation for Fluid-Structure Interaction

Jason P. Sheldon

Scott T. Miller

Jonathan S. Pitt

Distribution Statement A

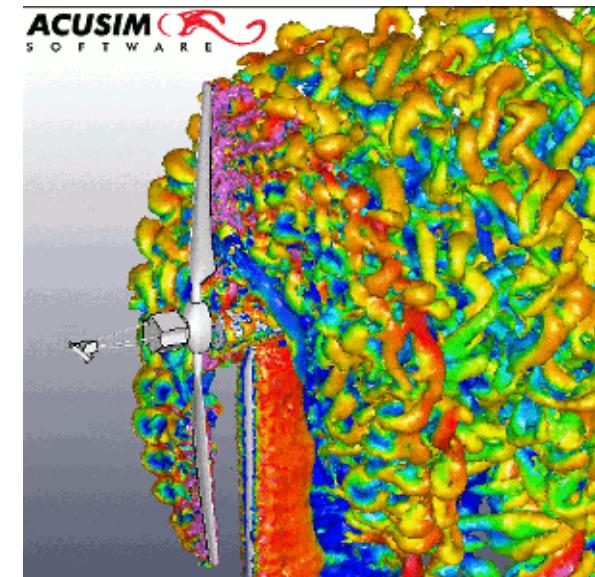
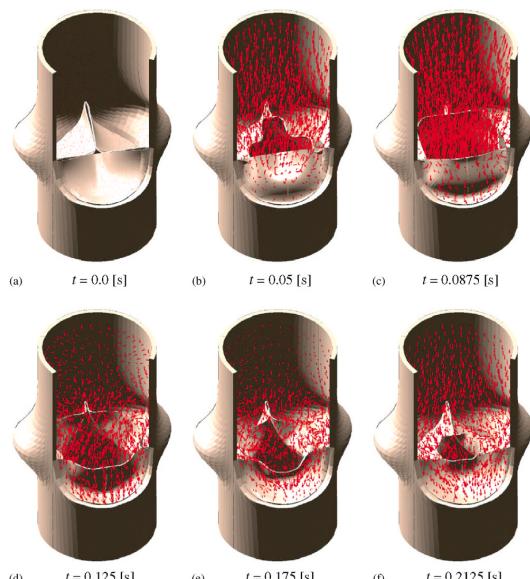
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Fluid-Structure Interaction (FSI)

The interaction of a deformable structure with a surrounding or internal fluid



Source

- <http://www.sciencedirect.com/science/article/pii/S0021929002002440>
- http://en.wikipedia.org/wiki/Cerebrospinal_fluid
- <http://www.acusim.com/html/apps/windTurbFSI.html>

Problem statement

High-order accurate FSI calculations are often too computationally expensive for real-world problems

Solution requirements

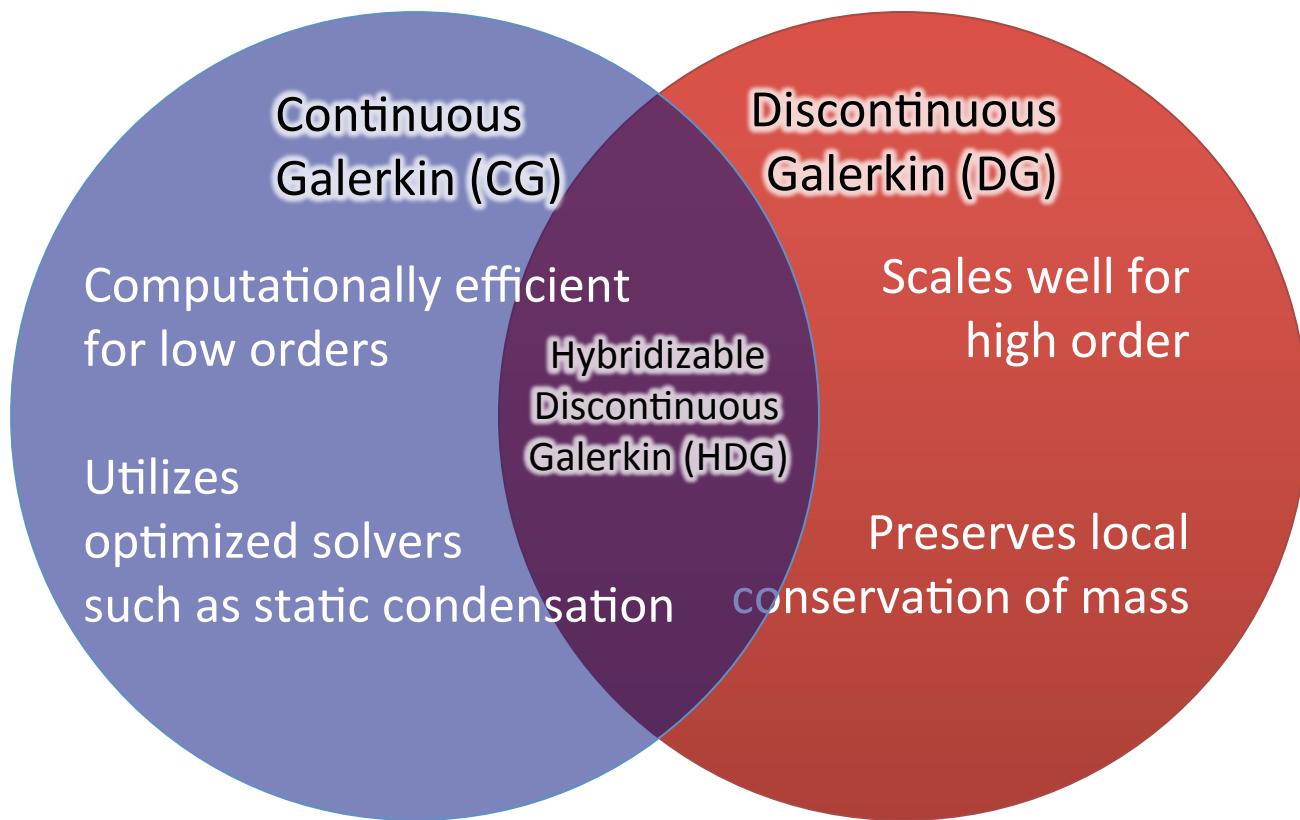
High-order accurate computations

Reasonable computational expenses

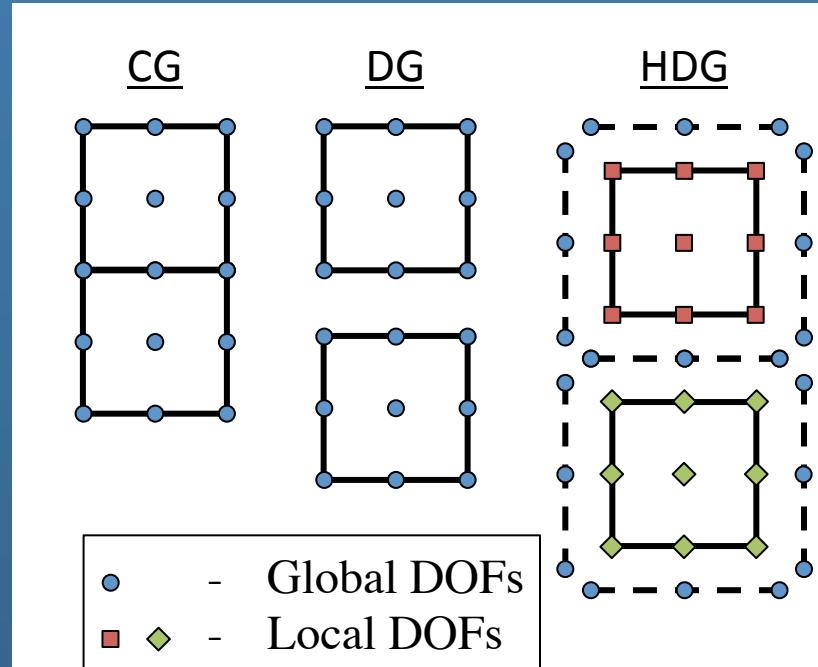
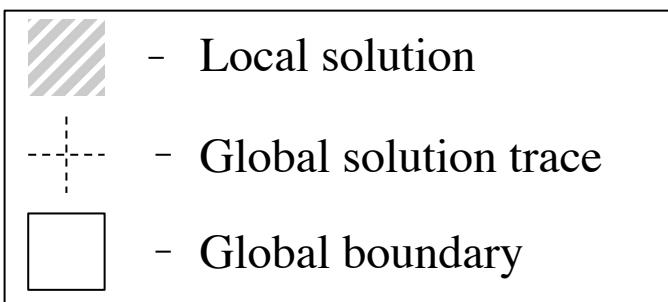
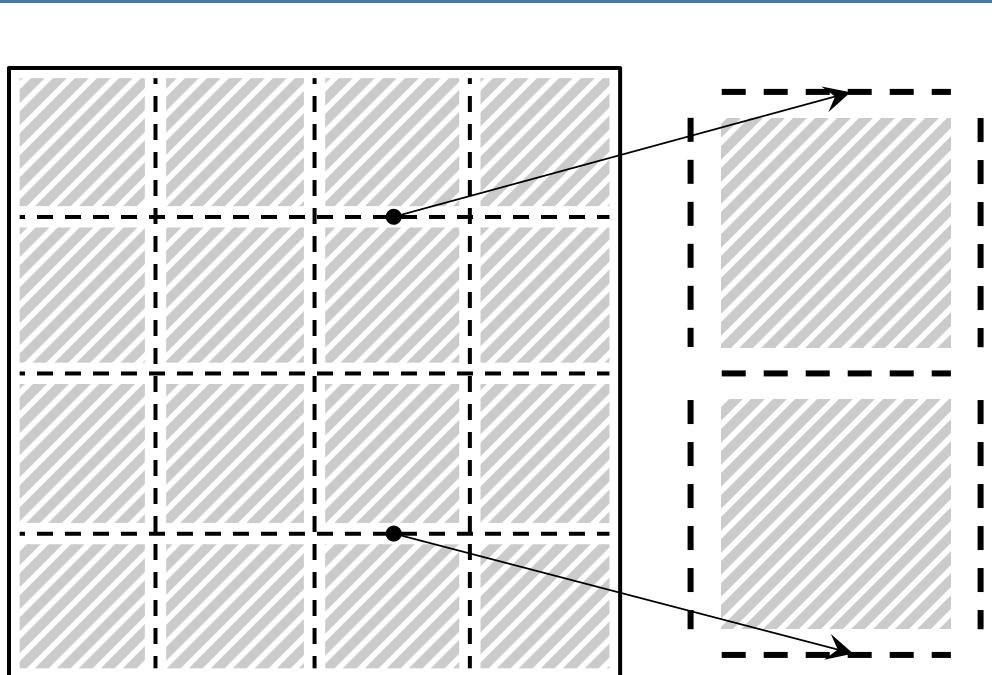
Proposed solution

Develop the first FSI model that uses the state of the art hybridizable discontinuous Galerkin (HDG) method

HDG – best of both worlds



HDG discretized domain

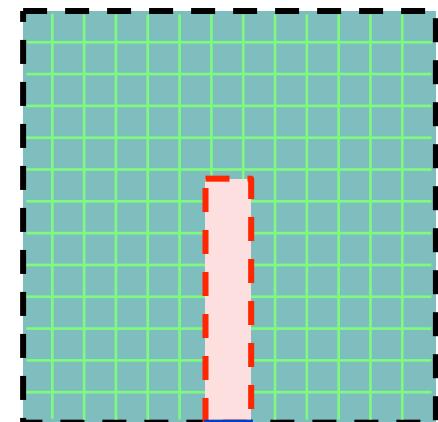
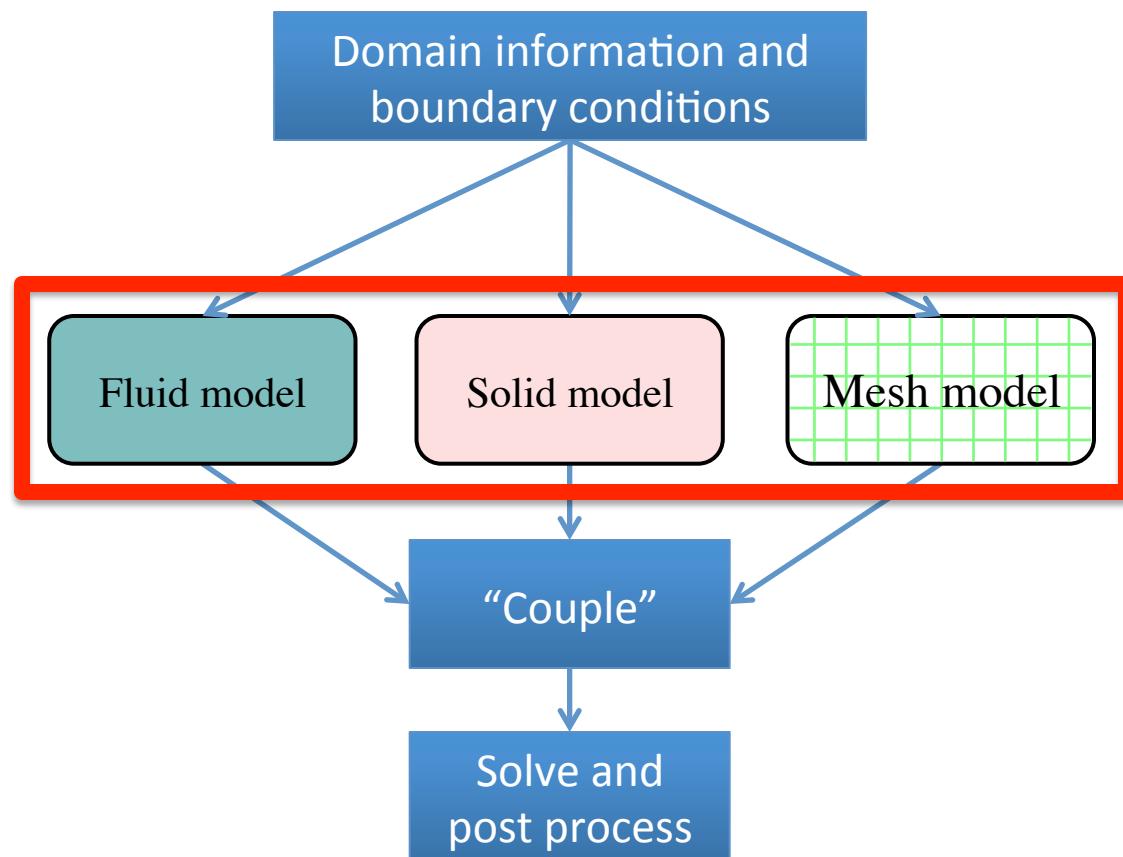


Example: 2D 1x2 quadratic elements

Variables: $\mathbf{u}, \mathbf{v}, \mathbf{e}$ - 8 global DOFs per (●)
 CG: 120 global DOFs
 DG: 144 global DOFs

Variables: $\mathbf{u}, \mathbf{v}, \mathbf{e}$ - 8 local DOFs per (■, ◆)
 $\boldsymbol{\mu}$ - 2 global DOFs per (●)
 HDG: 42 global DOFs
 + 72 local DOFs per cell

Fluid-structure interaction modeling



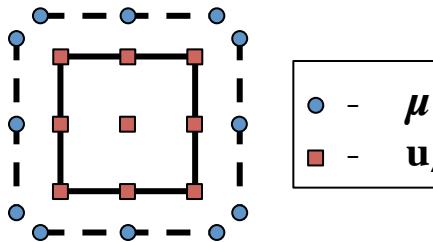
- Fluid Domain
- Solid Domain
- Mesh Domain
- Fluid-Solid Interface
- Fluid Boundary
- Solid Boundary

Linear elastostatics: HDG discretization

Strong form

$$-\operatorname{Div} (\mathbb{C}[\mathbf{e}]) = \mathbf{b}$$

$$\mathbf{e} - \operatorname{Sym}(\operatorname{Grad} \mathbf{u}) = \mathbf{0}$$



- ↓
1. Weight by weighting functions ($\tilde{\mathbf{u}}, \tilde{\mathbf{e}}$)
 2. Integrate over cell (K)
 3. Integrate by parts > boundary terms (Γ)

Weak form

$$\int_K \operatorname{Grad} \tilde{\mathbf{u}} : \mathbb{C}(\mathbf{e}) d\Omega - \int_{\Gamma} \tilde{\mathbf{u}} \cdot \widehat{\mathbb{C}(\mathbf{e})} \mathbf{n} d\Gamma = \int_K \tilde{\mathbf{u}} \cdot \mathbf{b} d\Gamma$$

$$\int_K \tilde{\mathbf{e}} : \mathbf{e} d\Omega - \int_K \operatorname{Sym}(\tilde{\mathbf{e}}) : \operatorname{Grad} \mathbf{u} d\Omega + \int_{\Gamma} \operatorname{Sym}(\tilde{\mathbf{e}}) \mathbf{n} \cdot (\mathbf{u} - \boldsymbol{\mu}) d\Gamma = 0$$

Flux continuity

$$\int_{\Gamma} \tilde{\boldsymbol{\mu}} \cdot \widehat{\mathbb{C}(\mathbf{e})} \mathbf{n} d\Gamma = 0$$

Stabilization

$$\widehat{\mathbb{C}(\mathbf{e})} := \mathbb{C}(\mathbf{e}) - \mathbf{S}(\mathbf{u} - \boldsymbol{\mu}) \otimes \mathbf{n}$$

Linear elastostatics: HDG discretization

Weak form

$$\int_K \text{Grad } \tilde{\mathbf{u}} : \mathbb{C}(\mathbf{e}) d\Omega - \int_{\Gamma} \tilde{\mathbf{u}} \cdot \widehat{\mathbb{C}(\mathbf{e})} \mathbf{n} d\Gamma = \int_K \tilde{\mathbf{u}} \cdot \mathbf{b} d\Gamma$$

$$\int_K \tilde{\mathbf{e}} : \mathbf{e} d\Omega - \int_K \text{Sym}(\tilde{\mathbf{e}}) : \text{Grad } \mathbf{u} d\Omega + \int_{\Gamma} \text{Sym}(\tilde{\mathbf{e}}) \mathbf{n} \cdot (\mathbf{u} - \boxed{\boldsymbol{\mu}}) d\Gamma = 0$$

$$\widehat{\mathbb{C}(\mathbf{e})} := \mathbb{C}(\mathbf{e}) - \mathbf{S}(\mathbf{u} - \boxed{\boldsymbol{\mu}}) \otimes \mathbf{n} \quad \int_{\Gamma} \tilde{\boldsymbol{\mu}} \cdot \widehat{\mathbb{C}(\mathbf{e})} \mathbf{n} d\Gamma = 0$$

$$\left(\begin{array}{c|c} \text{local} \times \text{local} & \text{local} \times \text{global} \\ \hline \text{global} \times \text{local} & \text{global} \times \text{global} \end{array} \right) \left\{ \begin{array}{c} \text{sol}_{\text{local}} \\ \hline \text{sol}_{\text{global}} \end{array} \right\} = \left\{ \begin{array}{c} \text{RHS}_{\text{local}} \\ \hline \text{RHS}_{\text{global}} \end{array} \right\}$$

Using the Schur complement, any equation of the form

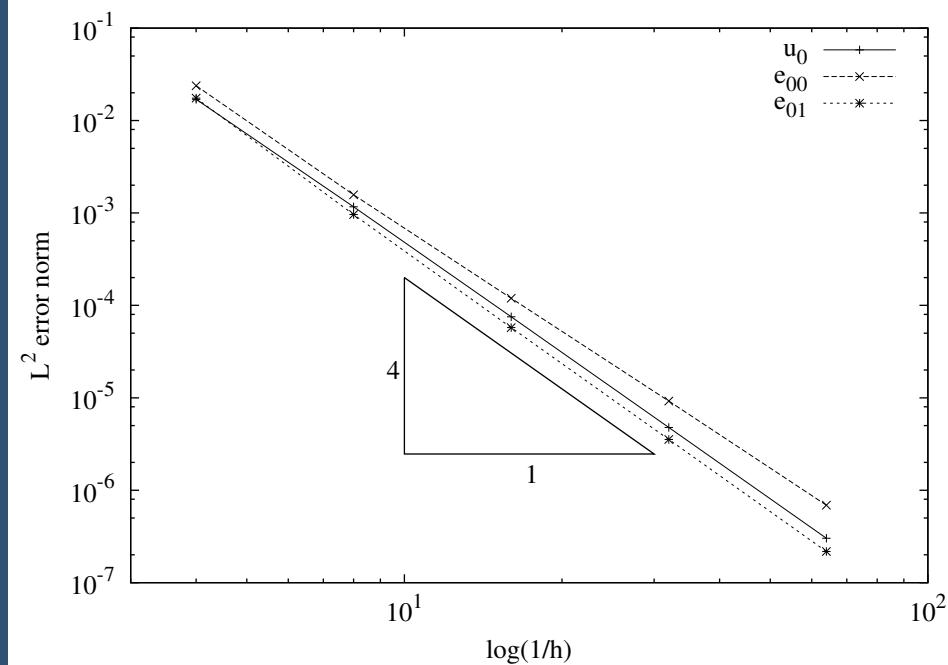
$$\begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} U \\ \boxed{\Lambda} \end{pmatrix} = \begin{pmatrix} F \\ G \end{pmatrix},$$

can be rearranged into the following system of equations:

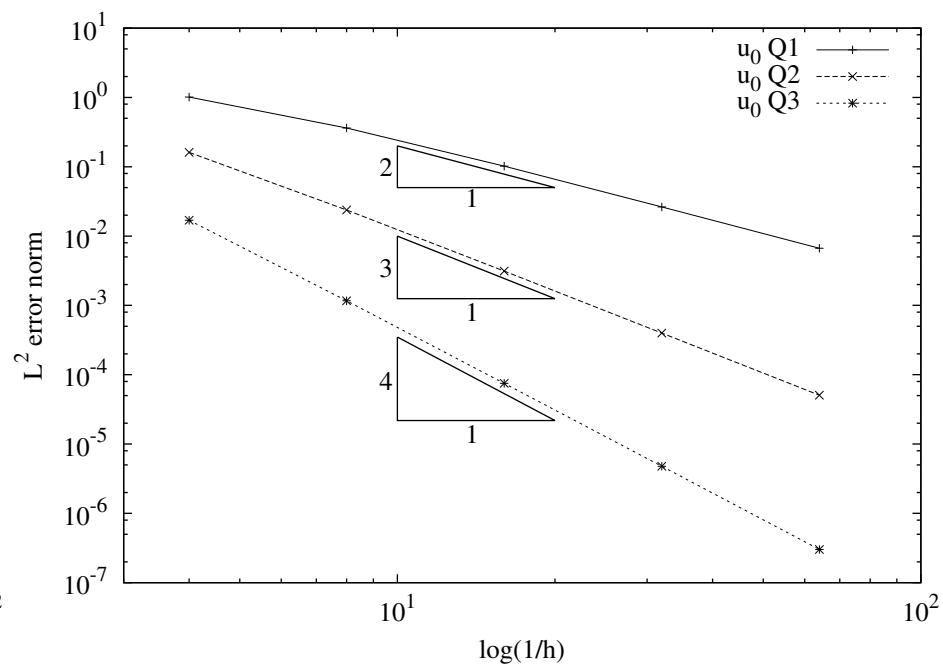
$$(D - CA^{-1}B)\boxed{\Lambda} = G - CA^{-1}F, \\ AU = F - BA\Lambda.$$

Linear elastostatics: verification

h-refinement (Q3)

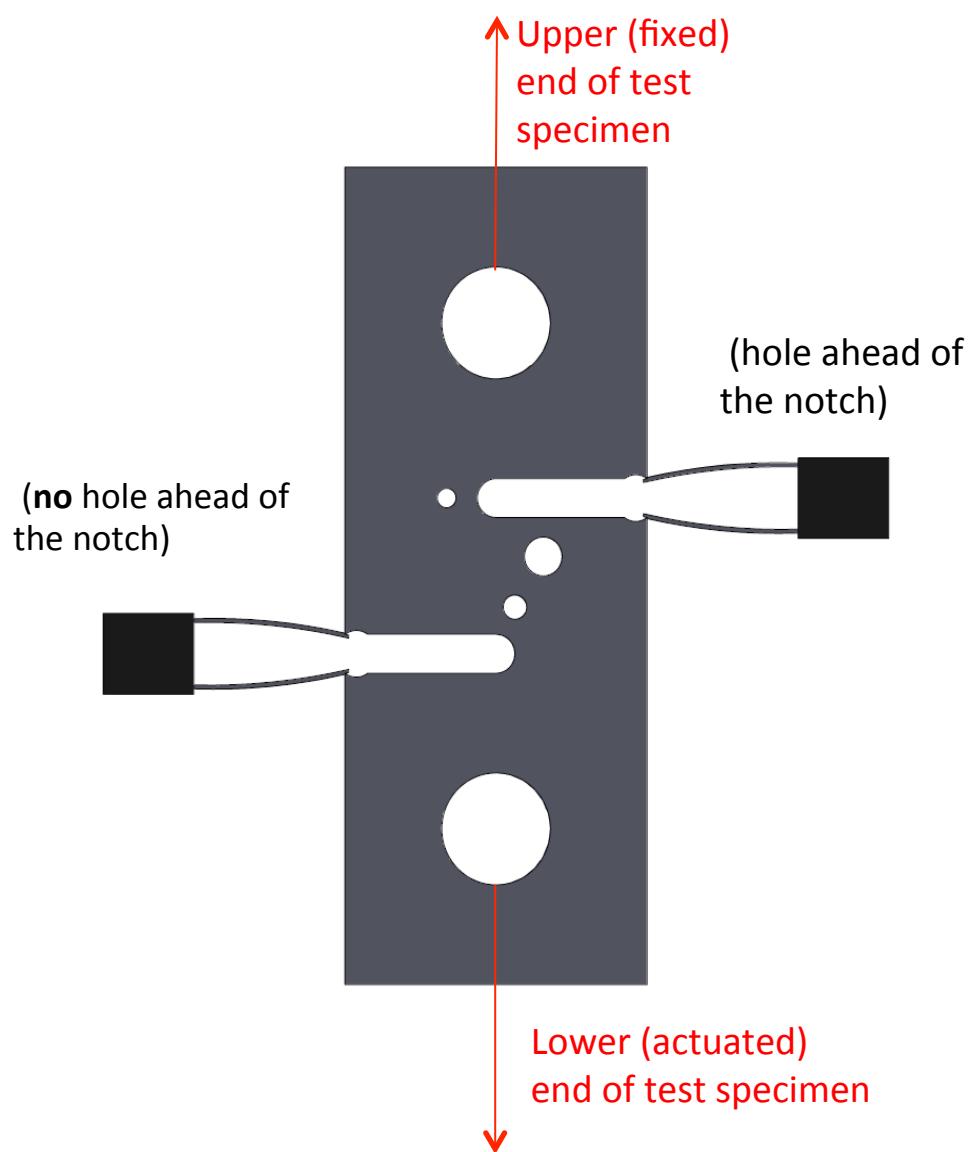


p-refinement



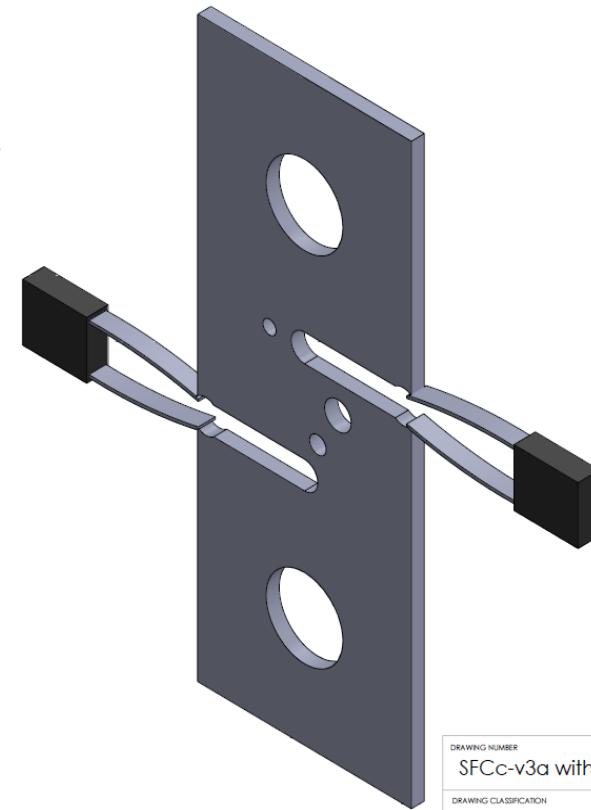
All errors converge at the expected rate of h^{p+1}
 Manufactured solution function of sines and cosines
 Pure Dirichlet boundary conditions

Preliminary results: Sandia geometry



Source

- The 2014 Sandia Fracture Challenge (SFC2)

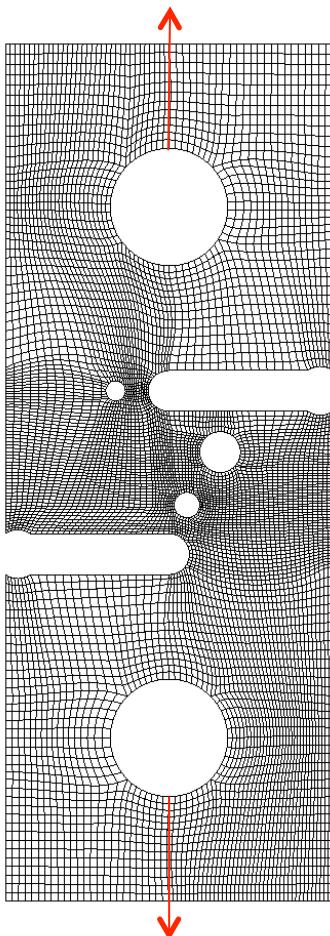


DRAWING NUMBER
SFCc-v3a with COD g
DRAWING CLASSIFICATION
UNCLASSIFIED
SIZE B CAGEC 14213 SCALE

Preliminary results: Sandia geometry

Undeformed mesh

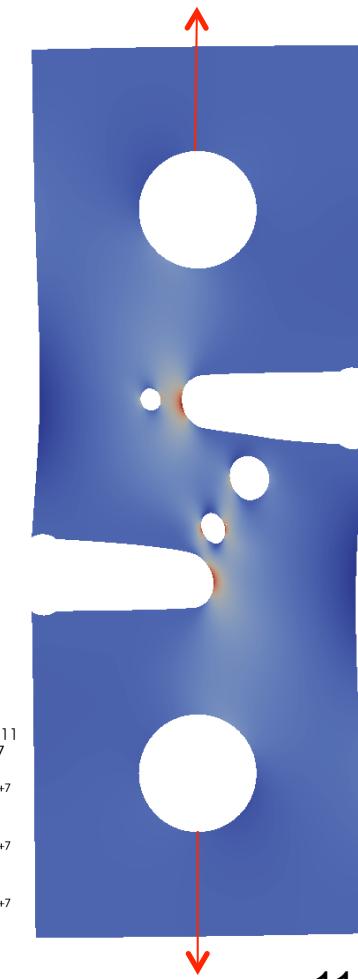
7777 cells



Element Order	Local # of DOFs	Increase from Q1	Global # of DOFs	Increase from Q1
Q1	186648	—	63720	—
Q3	746592	300%	127440	100%
Q5	1679832	800%	191160	200%
Q7	2986368	1500%	254880	300%

Size of global system increases minimally, even for high orders!

Deformed solution
Showing stress



Nonlinear elastodynamics: governing equations

Variables: \mathbf{u} , \mathbf{v} , \mathbf{E} - local
 $\boldsymbol{\mu}$ - global

Restricted to hyperelastic materials
(Saint Venant-Kirchhoff)

Weak form

$$\int_K \tilde{\mathbf{u}} \cdot \rho \frac{\partial \mathbf{v}}{\partial t} dK + \int_K \text{Grad } \tilde{\mathbf{u}} : \mathbf{F} \mathbb{C}(\mathbf{E}) dK - \int_{\Gamma} \tilde{\mathbf{u}} \cdot \hat{\mathbf{h}} d\Gamma = \int_K \tilde{\mathbf{u}} \cdot \mathbf{b} dK$$

$$\int_K \tilde{\mathbf{E}} : \mathbf{E} dK - \int_K \text{Sym}(\tilde{\mathbf{E}}) : \text{Grad } \mathbf{u} dK - \int_K \frac{1}{2} \tilde{\mathbf{E}} : (\text{Grad } \mathbf{u})^T \text{Grad } \mathbf{u} dK + \int_{\Gamma} \text{Sym}(\tilde{\mathbf{E}}) \mathbf{n} \cdot (\mathbf{u} - \boldsymbol{\mu}) d\Gamma = 0$$

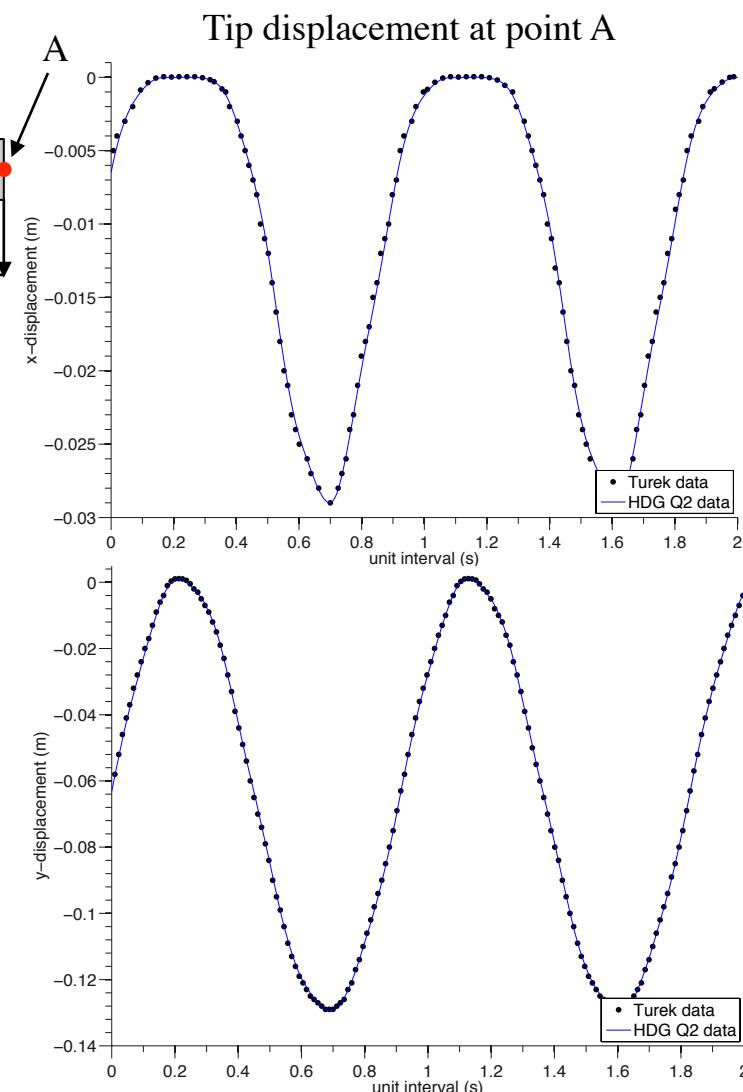
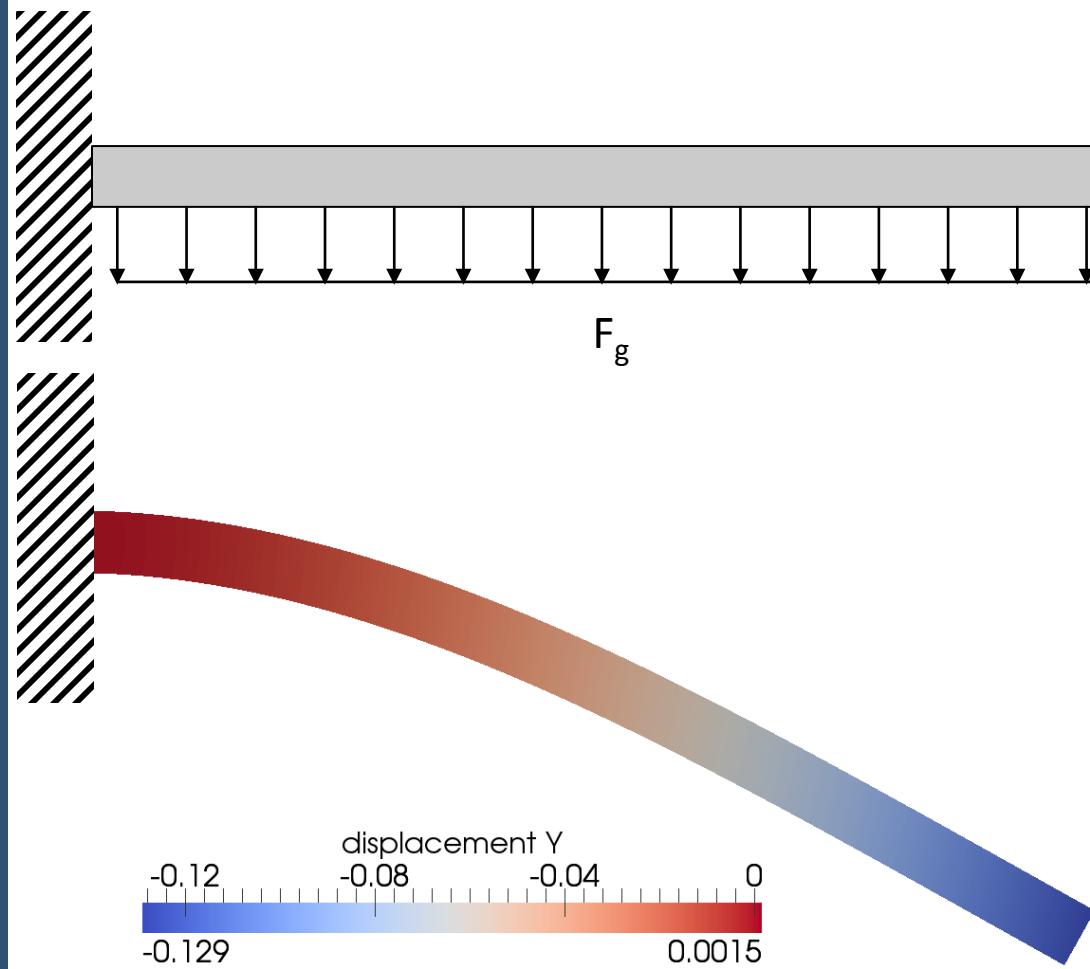
$$\int_K \tilde{\mathbf{v}} \cdot \frac{\partial \mathbf{u}}{\partial t} dK - \int_K \tilde{\mathbf{v}} \cdot \mathbf{v} dK = 0$$

$$\int_{\Gamma} \tilde{\boldsymbol{\mu}} \cdot \hat{\mathbf{h}} d\Gamma = 0$$

where $\hat{\mathbf{h}} := [\mathbf{F} \mathbb{C}(\mathbf{E})] \mathbf{n} - \mathbf{S}(\mathbf{u} - \boldsymbol{\mu})$

$$\mathbf{F} = \mathbf{I} + \text{Grad } \mathbf{u}$$

Preliminary results: Turek and Hron CSM3



Source

- Proposal for numerical benchmarking of fluid-structure interaction between an elastic object and laminar incompressible flow, Turek 2006

Navier-Stokes: governing equations

Variables: $\mathbf{v}, p, \mathbf{L}$ - local
 $\boldsymbol{\nu}, \psi$ - global

Weak form

$$\int_K \tilde{\mathbf{v}} \cdot \frac{\partial \mathbf{v}}{\partial t} dK - \int_K \text{grad } \tilde{\mathbf{v}} : \mathbf{v} \otimes \mathbf{v} - \nu \mathbf{L} dK + \int_K \tilde{\mathbf{v}} \cdot \text{grad } p_k dK + \int_{\Gamma} \tilde{\mathbf{v}} \cdot \hat{\mathbf{h}}^* d\Gamma = \int_K \tilde{\mathbf{v}} \cdot \mathbf{f} dK$$

$$\int_K \tilde{\mathbf{L}} : \mathbf{L} dK - \int_K \tilde{\mathbf{L}} : \text{grad } \mathbf{v} dK + \int_{\Gamma} \tilde{\mathbf{L}} \mathbf{n} \cdot (\mathbf{v} - \boldsymbol{\nu}) d\Gamma = 0$$

$$- \int_K \text{grad } \tilde{p}_k \cdot \mathbf{v} dK + \int_{\Gamma} \tilde{p}_k \boldsymbol{\nu} \cdot \mathbf{n} d\Gamma = 0$$

$$\int_{\Gamma} \tilde{\mathbf{v}} \cdot \hat{\mathbf{h}} d\Gamma = 0$$

$$\int_{\Gamma} \tilde{\psi} \boldsymbol{\nu} \cdot \mathbf{n} d\Gamma = 0$$

Flux stabilization

$$\hat{\mathbf{h}} := [\mathbf{v} \otimes \mathbf{v} - \nu \mathbf{L} + p \mathbf{I}] \mathbf{n} + \mathbf{S} (\mathbf{v} - \boldsymbol{\nu})$$

$$\hat{\mathbf{h}}^* := [\mathbf{v} \otimes \mathbf{v} - \nu \mathbf{L}] \mathbf{n} + \mathbf{S} (\mathbf{v} - \boldsymbol{\nu})$$

Introduce ψ to close the system

$$\psi := \frac{1}{|K|} \int_K p dK$$

Remove the kernel of the gradient

$$\int_{\Omega} p d\Omega = 0$$

Arbitrary Lagrangian-Eulerian (ALE) transformation

HDG ALE transform

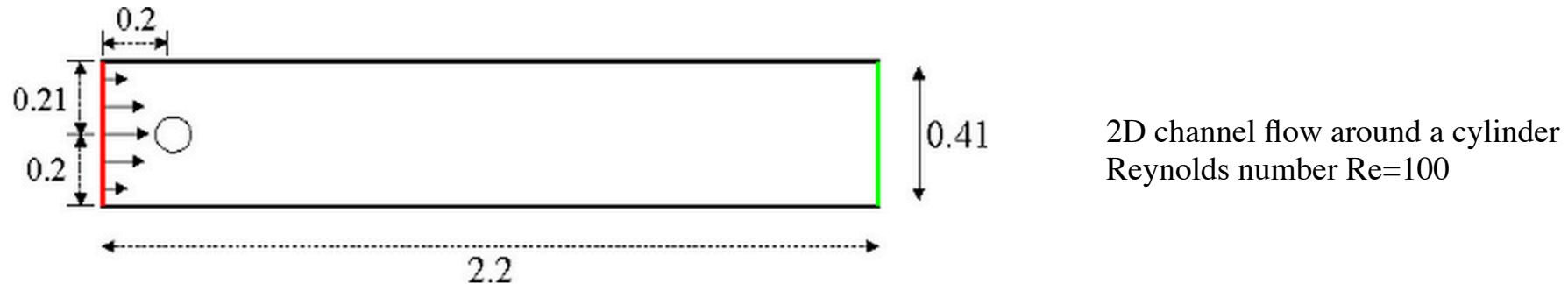
$$\mathbf{L} = \text{grad } \mathbf{v} = \text{Grad } \mathbf{v}_f \mathbf{F}_m^{-1} = \mathbf{L}_f,$$

$$\frac{\partial \mathbf{v}}{\partial t} = \frac{\partial \mathbf{v}_f}{\partial t} - \mathbf{L}_f [\mathbf{v}_m],$$

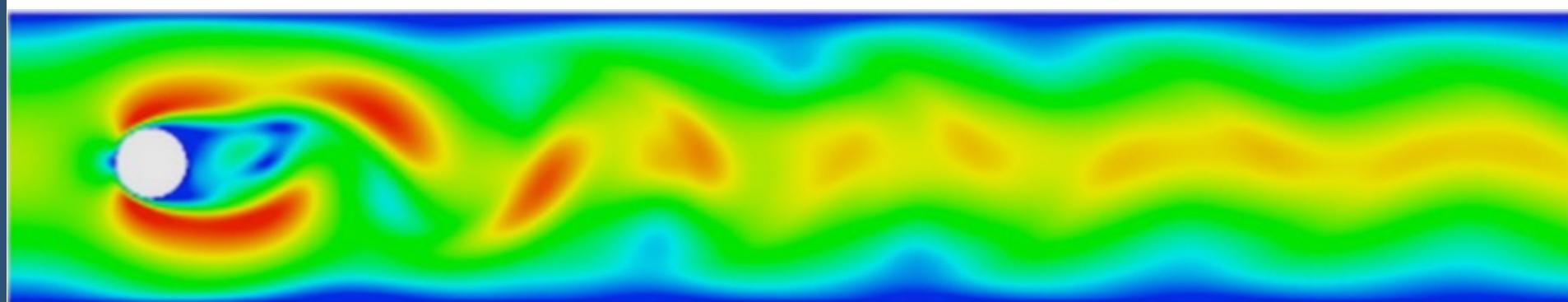
Auxiliary HDG variables
simplify ALE transformation

Integration domain ALE transform

$$\int_{\Omega_F(t)} f(\mathbf{x}) d\mathbf{x} = \int_{\Omega_F(0)} f_f(\mathbf{X}) J_m d\mathbf{X},$$



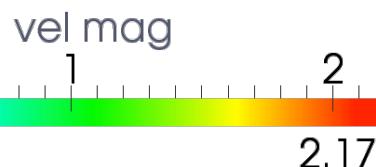
2D channel flow around a cylinder
Reynolds number $Re=100$



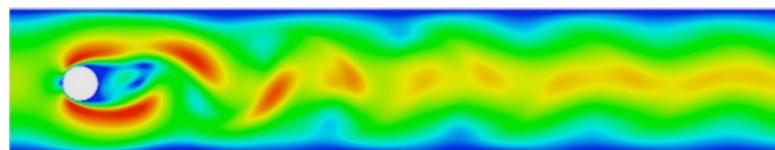
Source

- http://www.featflow.de/en/benchmarks/cfdbenchmarking/flow/dfg_benchmark2_re100.html

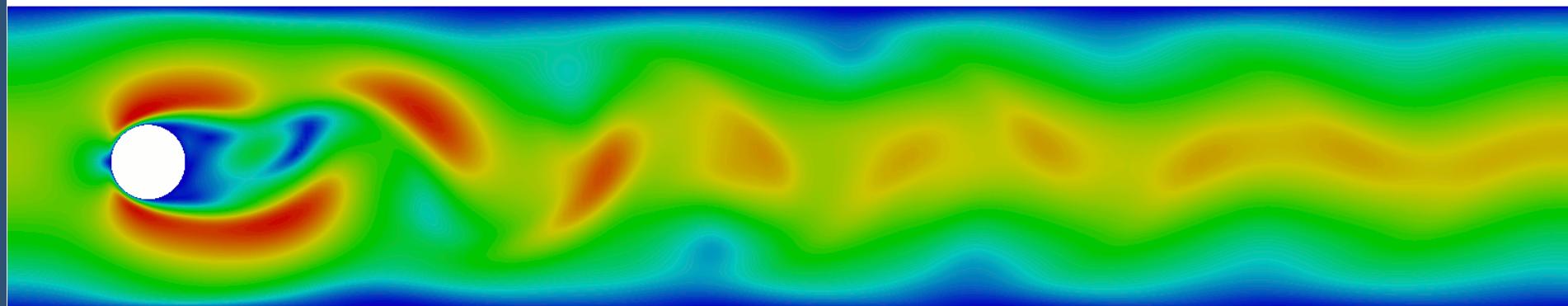
Preliminary results: flow over cylinder



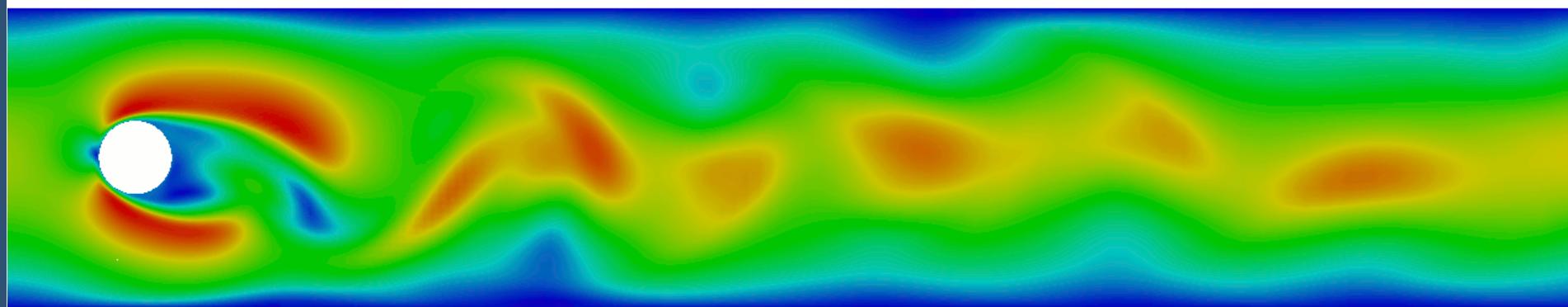
DFG benchmark ->



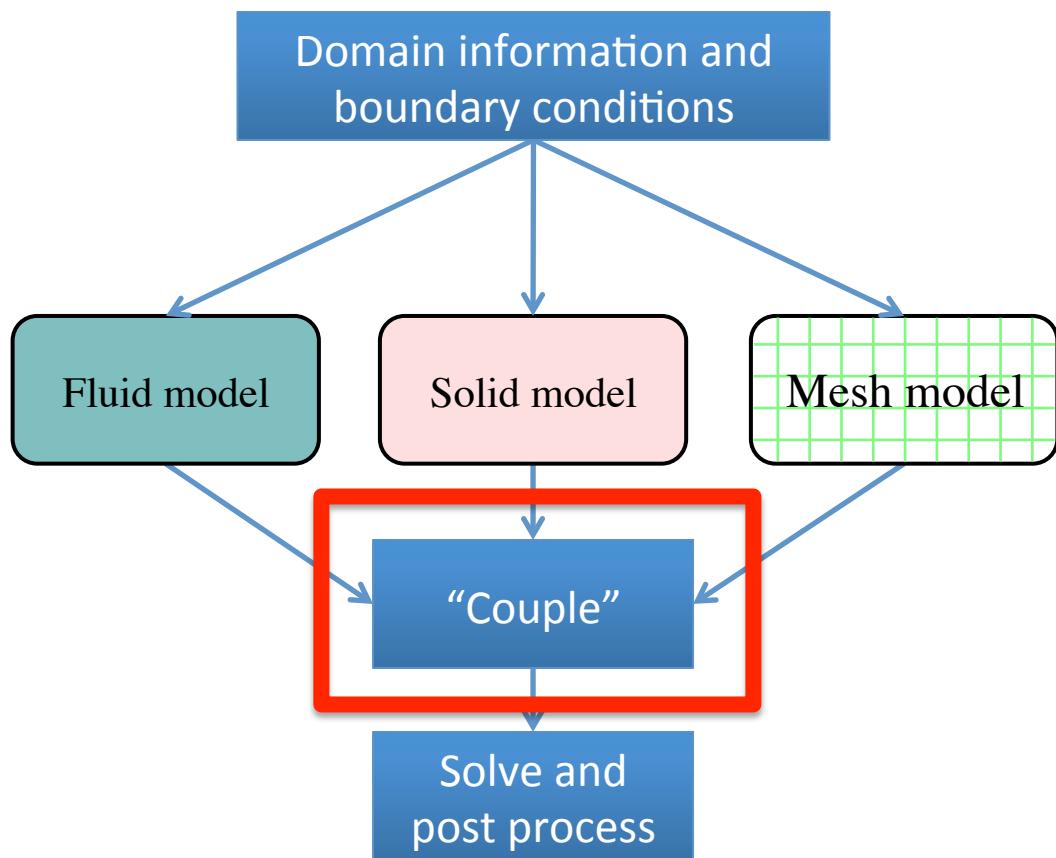
Matching HDG Navier-Stokes with DFG benchmark



ALE HDG Navier-Stokes proof of concept: oscillating cylinder

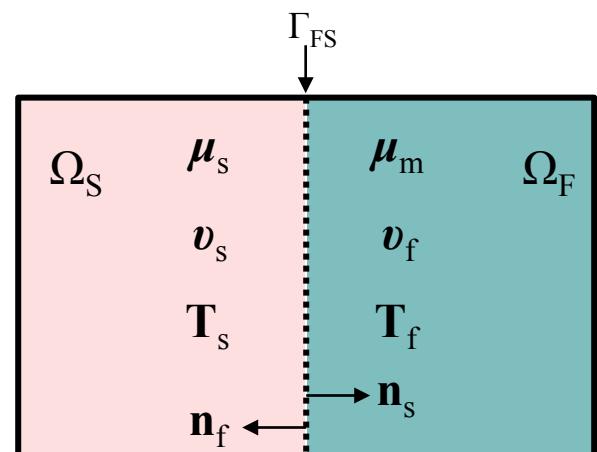


Fluid-Structure interaction modeling



Monolithic Coupling

$$\begin{bmatrix} \text{Solid System Matrix} & \text{Solid Fluid Coupling} & \text{Solid Mesh Coupling} \\ \text{Fluid Solid Coupling} & \text{Fluid System Matrix} & \text{Fluid Mesh Coupling} \\ \text{Mesh Solid Coupling} & \text{Mesh Fluid Coupling} & \text{Mesh System Matrix} \end{bmatrix} \begin{bmatrix} \text{Solid Unkns} \\ \text{Fluid Unkns} \\ \text{Mesh Unkns} \end{bmatrix} = \begin{bmatrix} \text{Solid RHS} \\ \text{Fluid RHS} \\ \text{Mesh RHS} \end{bmatrix}$$



Proposed HDG FSI formulation

Problem 1 (Fluid sub-problem)

Find $\{\mathbf{L}_f^h, \mathbf{v}_f^h, p_f^h, \mathbf{v}_f^h, \psi_f^h\} \in \mathcal{L}_f^h \times \mathbf{V}_f^h \times Q_f^h \times \mathcal{V}_f^h \times \Psi_f^h$ such that

$$\begin{aligned} & \left(\tilde{\mathbf{v}}_f, \rho_f J_m \frac{\partial \mathbf{v}_f^h}{\partial t} \right)_{K_f} + (\tilde{\mathbf{v}}_f, \rho_f J_m \mathbf{L}_f^h [\mathbf{v}_f^h - \mathbf{v}_m^h])_{K_f} + (\tilde{\mathbf{v}}_f, J_m \mathbf{F}_m^{-\top} [\text{Grad } p_f^h])_{K_f} \\ & \quad + (\text{Grad } \tilde{\mathbf{v}}_f, \mu_f J_m \mathbf{L}_f^h \mathbf{F}_m^{-\top})_{K_f} + \langle \tilde{\mathbf{v}}_f, \hat{\mathbf{T}}[\mathbf{n}]_f^* \rangle_{\partial K_f} = (\tilde{\mathbf{v}}_f, J_m \mathbf{f}_f)_{K_f}, \\ & (\tilde{\mathbf{L}}_f, J_m \mathbf{L}_f^h)_{K_f} - (\tilde{\mathbf{L}}_f, J_m \text{Grad } \mathbf{v}_f^h \mathbf{F}_m^{-1})_{K_f} + \langle \tilde{\mathbf{L}}_f \mathbf{F}_m^{-\top} [\mathbf{n}_f], J_m (\mathbf{v}_f^h - \mathbf{v}_f^h) \rangle_{\partial K_f} = 0, \\ & \quad - (\mathbf{F}_m^{-\top} [\text{Grad } p_f^h], J_m \mathbf{v}_f^h)_{K_f} + \langle \mathbf{F}_m^{-\top} [\mathbf{n}_f] \tilde{p}_f^h, J_m \mathbf{v}_f^h \rangle_{\partial K_f} = 0, \\ & \langle \tilde{\mathbf{v}}_f, \hat{\mathbf{T}}[\mathbf{n}]_f \rangle_{\partial \mathcal{T}_f^h \setminus \Gamma_{\text{FSI}}} + \langle \tilde{\mathbf{v}}_f, \hat{\mathbf{T}}[\mathbf{n}]_f + \hat{\mathbf{T}}[\mathbf{n}]_s \rangle_{\Gamma_{\text{FSI}}} + \langle \tilde{\mathbf{v}}_f, \mathbf{S}_f (\mathbf{v}_f^h - \mathbf{v}_s^h) \rangle_{\Gamma_{\text{FSI}}} = \langle \tilde{\mathbf{v}}_f, J_m \mathbf{g}_{N_f} \rangle_{\Gamma_N}, \\ & \quad \langle \tilde{\psi}_f, J_m \mathbf{F}_m^{-\top} [\mathbf{n}_f] \cdot \mathbf{v}_f^h \rangle_{\partial \mathcal{T}_f^h} = 0, \\ & \quad (p_f^0, J_m p_f^0)_{\mathcal{T}_f^h} = 0, \end{aligned}$$

$\forall \{\tilde{\mathbf{L}}_f, \tilde{\mathbf{v}}_f, \tilde{p}_f, \tilde{\mathbf{v}}_f, \tilde{\psi}_f\} \in \mathcal{L}_f^h \times \mathbf{V}_f^h \times Q_f^h \times \tilde{\mathcal{V}}_f \times \Psi_f^h$, where

$$\begin{aligned} p_f^0 + p_f^k &= p_f^h \\ \hat{\mathbf{T}}[\mathbf{n}]^* &:= -\mu_f J_m \mathbf{L}_f^h \mathbf{F}_m^{-\top} [\mathbf{n}_f] + \mathbf{S}_f (\mathbf{v}_f^h - \mathbf{v}_f^h), \\ \hat{\mathbf{T}}[\mathbf{n}]_f &:= J_m [-\mu_f \mathbf{L}_f^h + (p_f^k + \psi_f^h) \mathbf{I}] \mathbf{F}_m^{-\top} [\mathbf{n}_f] + \mathbf{S}_f (\mathbf{v}_f^h - \mathbf{v}_f^h), \\ \mathbf{S}_f &:= \left(\frac{\mu_f}{l_f} + \rho_f |\mathbf{v}_f^h|_{L2} \right) \mathbf{I}, \end{aligned}$$

Problem 2 (Solid sub-problem)

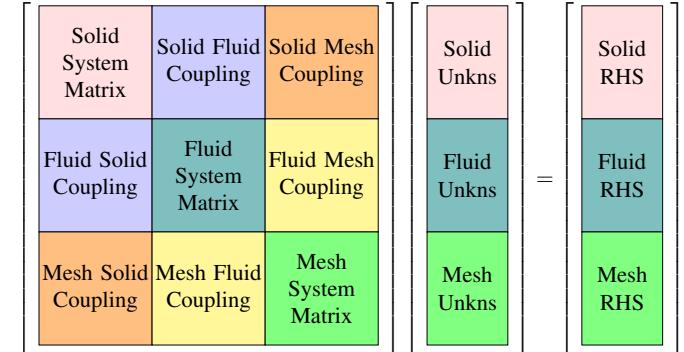
Find $\{\mathbf{u}_s^h, \mathbf{v}_s^h, \mathbf{E}_s^h, \boldsymbol{\mu}_s^h, \boldsymbol{\nu}_s^h\} \in \mathbf{U}_s^h \times \mathbf{V}_s^h \times \mathcal{E}_s^h \times \mathbf{M}_s^h \times \mathcal{V}_s^h$, such that

$$\begin{aligned} & \left(\tilde{\mathbf{v}}_s, \rho_s \frac{\partial \mathbf{v}_s^h}{\partial t} \right)_{K_s} + (\text{Grad } \tilde{\mathbf{v}}_s, \mathbf{F}_s \mathbb{C}_s (\mathbf{E}_s^h))_{K_s} + \langle \tilde{\mathbf{v}}_s, \hat{\mathbf{T}}[\mathbf{n}]_s \rangle_{\partial K_s} = (\tilde{\mathbf{v}}_s, \mathbf{b}_s)_{K_s}, \\ & (\tilde{\mathbf{E}}_s, \mathbf{E}_s^h)_{K_s} - (\text{Sym}(\tilde{\mathbf{E}}_s), \text{Grad } \mathbf{u}_s^h)_{K_s} - \left(\frac{1}{2} \tilde{\mathbf{E}}_s, (\text{Grad } \mathbf{u}_s^h)^T \text{Grad } \mathbf{u}_s^h \right)_{K_s} \\ & \quad + \langle \text{Sym}(\tilde{\mathbf{E}}_s) \mathbf{n}, (\mathbf{u}_s^h - \boldsymbol{\mu}_s^h) \rangle_{\partial K_s} = 0, \\ & \left(\tilde{\mathbf{u}}_s, \frac{\partial \mathbf{u}_s^h}{\partial t} \right)_{K_s} - (\tilde{\mathbf{u}}_s, \mathbf{v}_s^h)_{K_s} = 0, \\ & \langle \tilde{\boldsymbol{\mu}}_s, \mathbf{u}_s^h \rangle_{\partial K_s} - \langle \tilde{\boldsymbol{\mu}}_s, \boldsymbol{\mu}_s^h \rangle_{\partial K_s} = 0, \\ & \langle \tilde{\mathbf{v}}_s, \hat{\mathbf{T}}[\mathbf{n}]_s \rangle_{\partial \mathcal{T}_s^h \setminus \Gamma_{\text{FSI}}} + \langle \tilde{\mathbf{v}}_s, \hat{\mathbf{T}}[\mathbf{n}]_s + \hat{\mathbf{T}}[\mathbf{n}]_f \rangle_{\Gamma_{\text{FSI}}} + \langle \tilde{\mathbf{v}}_s, \mathbf{S}_s (\mathbf{v}_s^h - \mathbf{v}_f^h) \rangle_{\Gamma_{\text{FSI}}} = \langle \tilde{\mathbf{v}}_s, \mathbf{g}_{N_s} \rangle_{\Gamma_{N_s}}, \end{aligned}$$

$\forall \{\tilde{\mathbf{u}}_s, \tilde{\mathbf{v}}_s, \tilde{\mathbf{E}}_s, \tilde{\boldsymbol{\mu}}_s, \tilde{\mathbf{v}}_s\} \in \mathbf{U}_s^h \times \mathbf{V}_s^h \times \mathcal{E}_s^h \times \tilde{\mathbf{M}}_s \times \mathcal{V}_s^h$, where

$$\begin{aligned} \mathbf{F}_s &= \mathbf{I} + \text{Grad } \mathbf{u}_s^h \\ \hat{\mathbf{T}}[\mathbf{n}]_s &:= -[\mathbf{F}_s \mathbb{C}_s (\mathbf{E}_s^h)] \mathbf{n}_s + \mathbf{S}_s (\mathbf{v}_s^h - \mathbf{v}_s^h), \\ \mathbf{S}_s &:= \frac{\mu_s}{l_s} \mathbf{I}. \end{aligned}$$

Monolithic Coupling



Problem 3 (Mesh sub-problem)

Find $\{\mathbf{u}_m^h, \mathbf{F}_m^h, \boldsymbol{\mu}_m^h\} \in \mathbf{U}_m^h \times \mathcal{F}_m^h \times \mathbf{M}_m^h$ such that

$$\begin{aligned} & (\text{Grad } \tilde{\mathbf{u}}_m, \mathbb{C}_m (\mathbf{F}_m^h))_K - \langle \tilde{\mathbf{u}}_m, \hat{\mathbf{T}}[\mathbf{n}]_m \rangle_{\partial K} = (\text{Grad } \tilde{\mathbf{u}}_m, \mathbb{C}_m (\mathbf{I}))_K - \langle \tilde{\mathbf{u}}_m, \mathbb{C}_m (\mathbf{I}) \mathbf{n}_m \rangle_{\partial K} + (\tilde{\mathbf{u}}_m, \mathbf{b})_K, \\ & (\tilde{\mathbf{F}}_m, \mathbf{F}_m^h)_K - (\tilde{\mathbf{F}}_m, \text{Grad } \mathbf{u}_m^h)_K + \langle \tilde{\mathbf{F}}_m \mathbf{n}_m, (\mathbf{u}_m^h - \boldsymbol{\mu}_m^h) \rangle_{\partial K} = (\tilde{\mathbf{F}}_m, \mathbf{I})_K, \\ & \langle \tilde{\mathbf{u}}_m, \hat{\mathbf{T}}[\mathbf{n}]_m \rangle_{\partial \mathcal{T}_m^h \setminus \Gamma_{\text{FSI}}} + \langle \tilde{\boldsymbol{\mu}}_m, \boldsymbol{\mu}_m^h - \boldsymbol{\mu}_s^h \rangle_{\Gamma_{\text{FSI}}} = \langle \tilde{\mathbf{u}}_m, \mathbb{C}_m (\mathbf{I}) \mathbf{n}_m \rangle_{\partial \mathcal{T}_m^h \setminus \Gamma_{\text{FSI}}} + \langle \tilde{\boldsymbol{\mu}}_m, \mathbf{g}_N \rangle_{\partial \Omega_N}, \end{aligned}$$

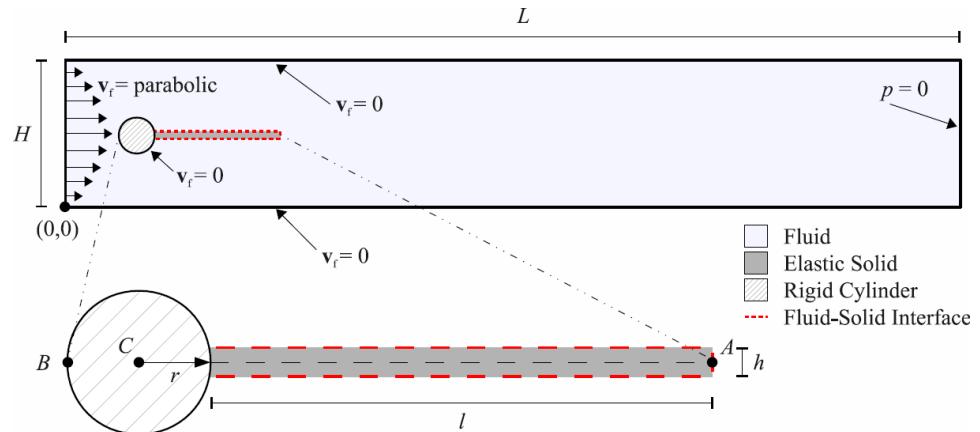
$\forall \{\tilde{\mathbf{u}}_m, \tilde{\mathbf{F}}_m, \tilde{\boldsymbol{\mu}}_m\} \in \mathbf{U}_m^h \times \mathcal{F}_m^h \times \tilde{\mathbf{M}}_m$, where

$$\begin{aligned} \hat{\mathbf{T}}[\mathbf{n}]_m &:= \mathbb{C}_m (\mathbf{F}_m^h) \mathbf{n}_m - \mathbf{S}_m (\mathbf{u}_m^h - \boldsymbol{\mu}_m^h), \\ \mathbf{S}_m &:= \frac{\mu}{l} \mathbf{I}. \end{aligned}$$

Actually implementing this in deal

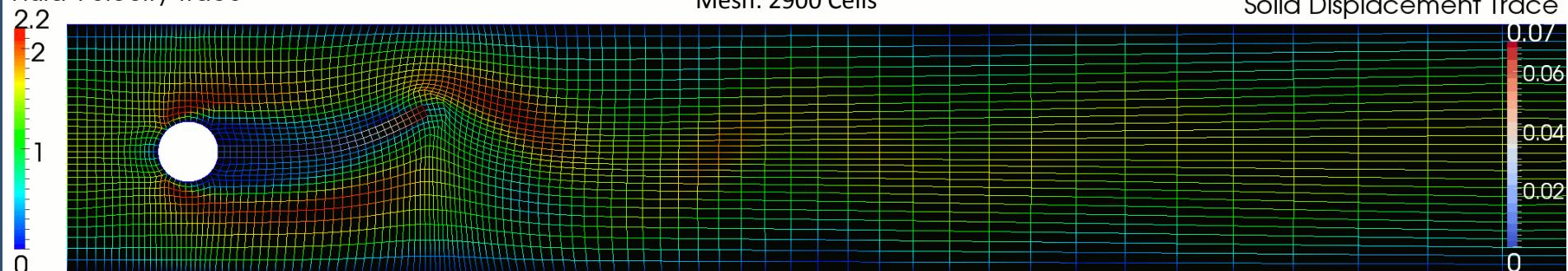
- **Multiple Triangulations (for each material)**
 - and sets of dofhandlers, fe-systems, etc
- **Using blockmatrix system**
 - Each diagonal block gets a different physics model
- **Fluid-solid interface (off-diagonal blocks)**
 - We have two sets of global (trace) degrees of freedom unlike everywhere else in the domain
 - Face/point tracking between abutting trias
 - Use weak form of coupling conditions with single point quadrature from the adjacent tria
 - Need global-global coupling!
 - Don't want to couple the local and global solutions

Turek-Hron FSI benchmark

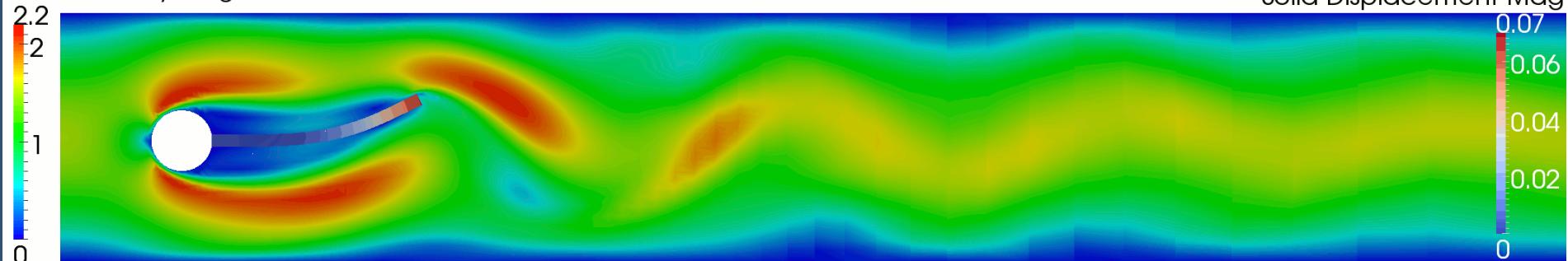


parameter	symbol	value [m]	property	value
Channel length	L	2.5	ρ_s [$\frac{kg}{m^3}$]	10000
Channel height	H	0.41	ν_s	0.4
Cylinder center	C	(0.2, 0.2)	E_s [E6 $\frac{kg}{ms^2}$]	5.6
Cylinder radius	r	0.05	ρ_f [$\frac{kg}{m^3}$]	1000
Flag length	l	0.35	μ_f [$\frac{kg}{ms}$]	1
Flag height	h	0.02	\bar{U} [$\frac{m}{s}$]	1
Reference point	A	(0.6, 0.2)	$ v_f _{in}$ [$\frac{m}{s}$]	$1.5 \bar{U} \frac{y(H-y)}{(H/2)^2}$
Reference point	B	(0.15, 0.2)		

Fluid Velocity Trace



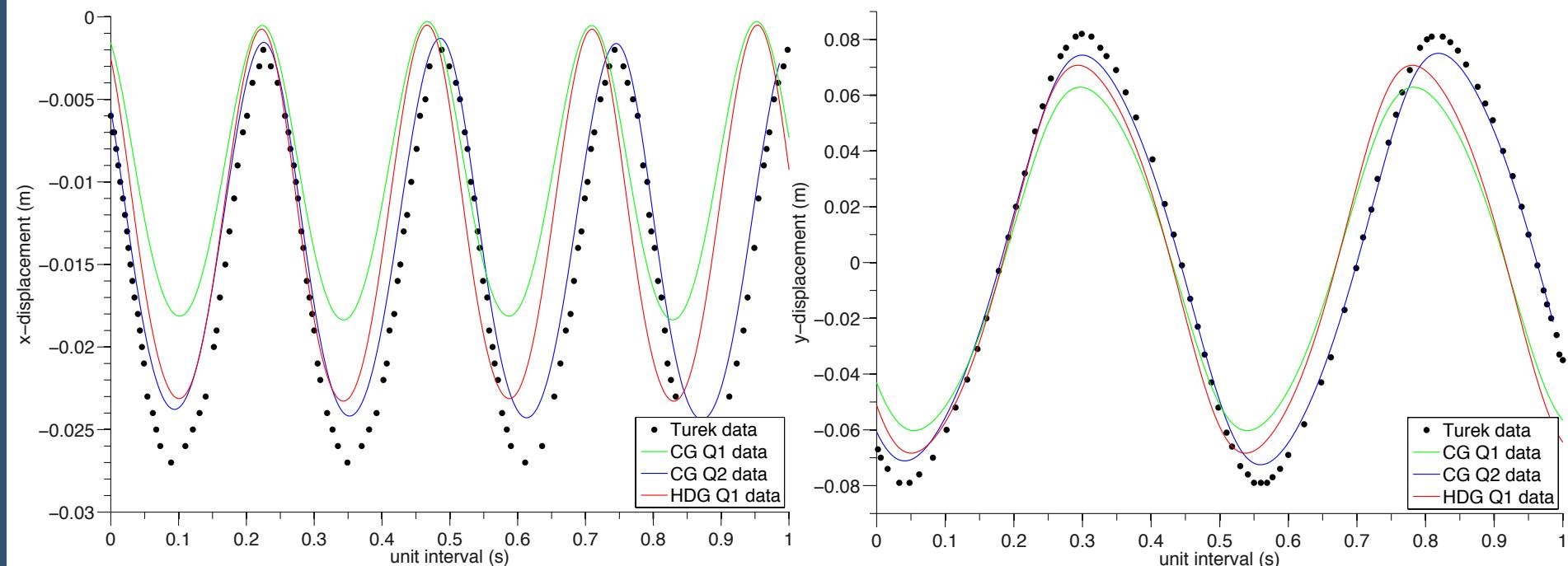
Fluid Velocity Mag



Tip displacement plots (at A)

Turek-Hron FSI benchmark tip displacement

Plotted against CG and HDG results, both using backward Euler time-stepping on same mesh



- Q1 HDG results match oscillation period for Q1 CG results
- Q1 HDG results are closer in amplitude to Q2 CG results than Q1

- **Goal:** Develop new computational tool, a HDG FSI model
 - HDG allows for arbitrarily high order polynomials and their inherently parallel nature leads to significant increase in computational efficiency
- **Progress:** Models implemented, tested, and coupled
 - Implemented and verified HDG elasticity and Navier-Stokes models
 - Considered preliminary test cases
 - Implemented HDG FSI formulation
- **HDG FSI:** Benchmarked against Turek and Hron (backward Euler in time)
 - Q1 HDG results match oscillation period for Q1 CG results
 - Q1 HDG results are closer in amplitude to Q2 CG results than Q1

Future research tasks / questions

- Implement higher order time-stepping, such as Diagonally implicit Runge-Kutta
- Perform verification with the method of manufactured solutions for the fully-coupled FSI problem.
- Implement superconvergent postprocess capabilities for HDG FSI as done for individual components.
- Are the various HDG formulations for the different physics models algebraically equivalent? Are there optimal formulations in terms of accuracy, computational efficiency, and/or stability?
- Can we quantify the effects on convergence and dissipation of varying the stability parameter S ?
- Plotting error vs. wall time, at what order element does using the HDG method for FSI become more computationally efficient than using other methods, such as our CG FSI model?

Thank you

Questions?