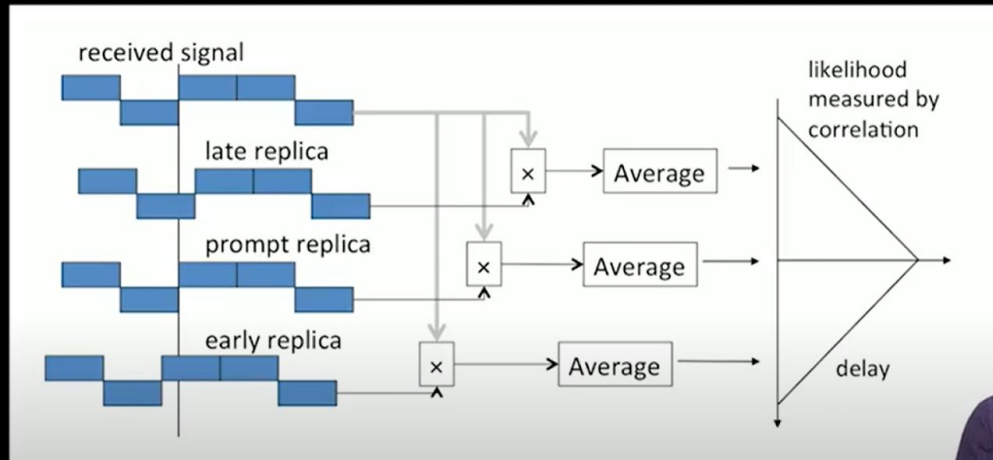


1.9 - Pseudo ranging

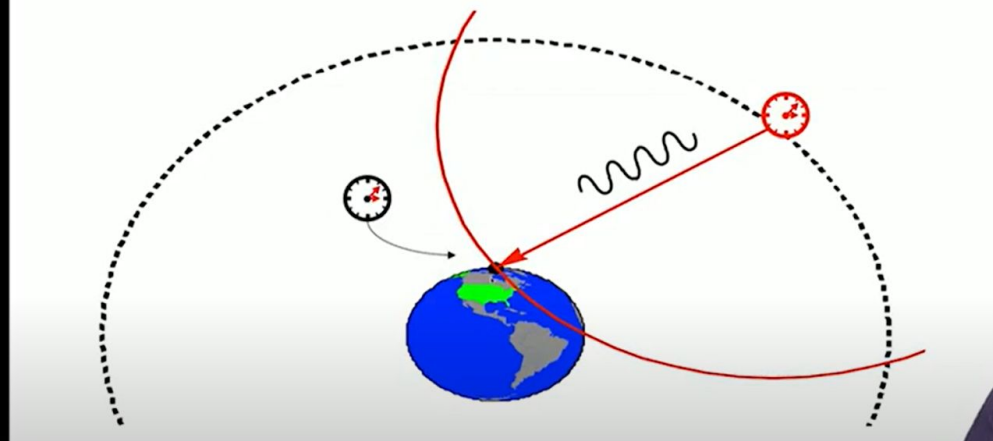
GPS Receivers: Time of Arrival Measurements



0:39 / 19:33

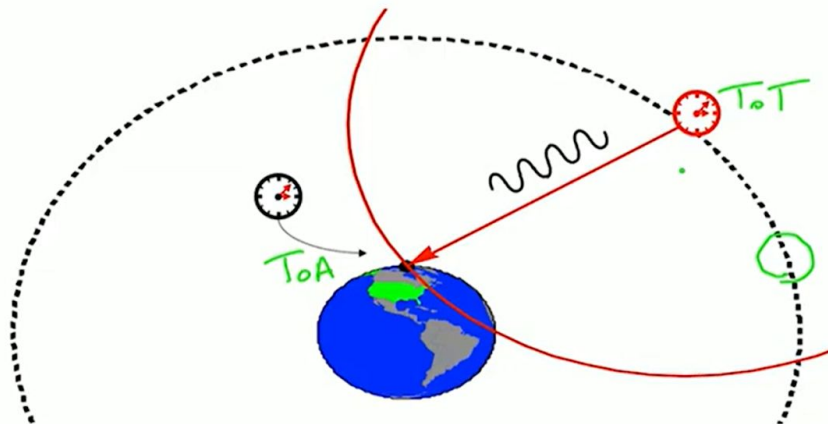
1.9 - Pseudo ranging

Each Satellite Stamps the **Transmission Time**.
GPS Receiver Measures the **Arrival Time**.



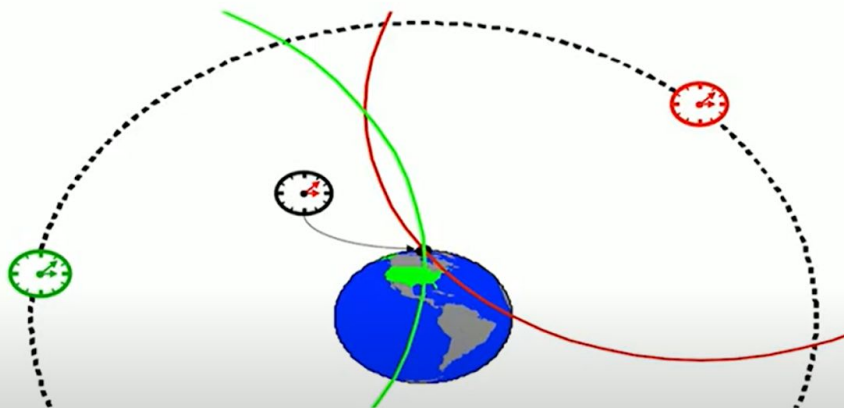
4:04 / 19:33

Each Satellite Stamps the **Transmission Time**.
GPS Receiver Measures the **Arrival Time**.

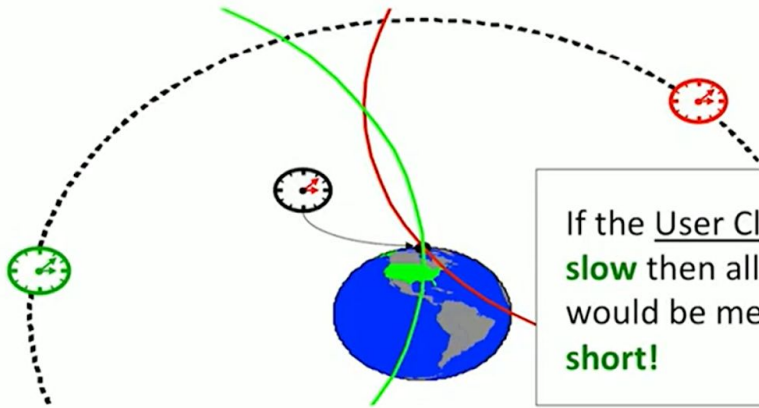


1.9 - Pseudo ranging

If the User Clock is **fast** then all ranges would be measured **long!**

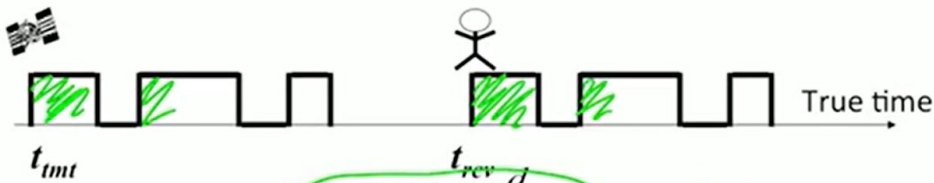


If the User Clock is **fast** then all ranges would be measured **long!**



If the User Clock is **slow** then all ranges would be measured **short!**

Measured Arrival Time—Including Clock Bias



$$t_{rcv} - t_{tmt} = \frac{d}{c}$$

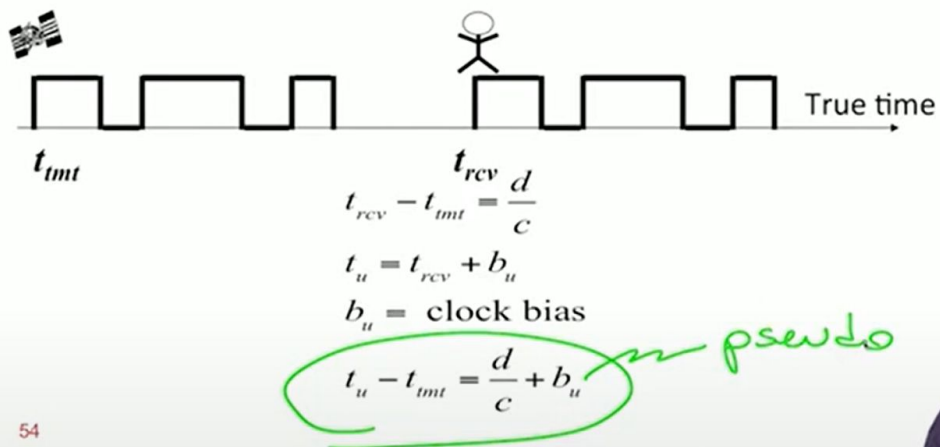
$$t_u = t_{rcv} + b_u$$

$$b_u = \text{clock bias}$$

$$t_u - t_{tmt} = \frac{d}{c} + b_u$$

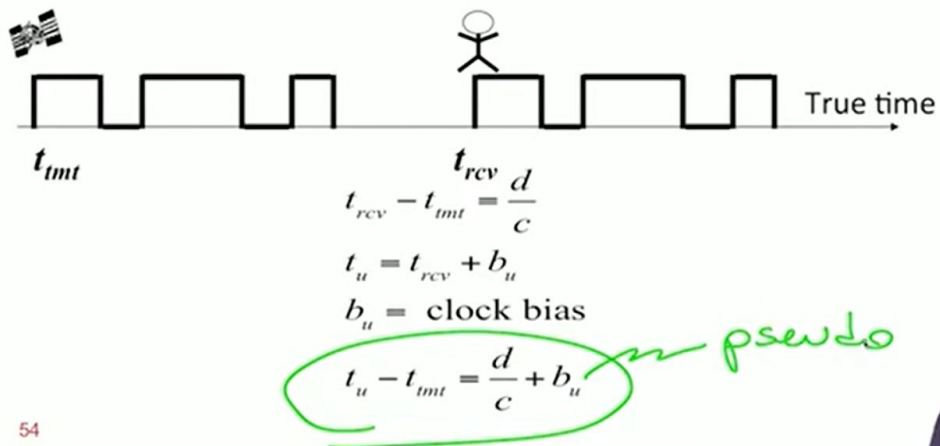
state augmentation
 $\{x, y, z\}$ 3D
 $\{x, y, z, b_u\}$

Measured Arrival Time—Including Clock Bias

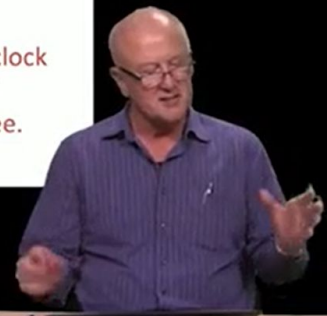
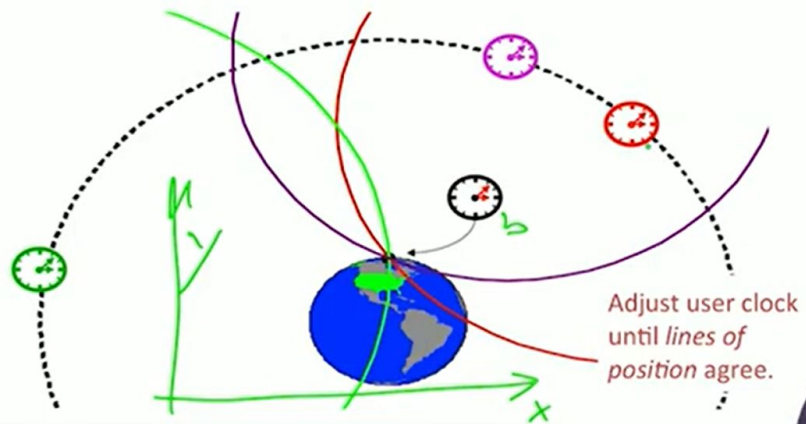


13:08 / 19:33

Measured Arrival Time—Including Clock Bias

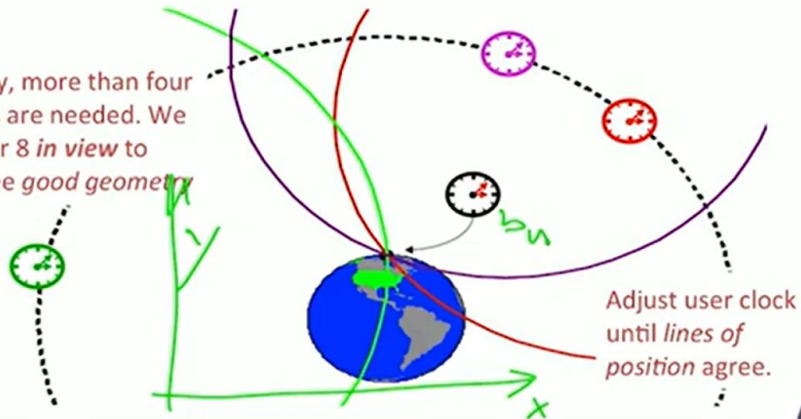


Every aircraft must be able to view
at least(!) 4 GPS satellites

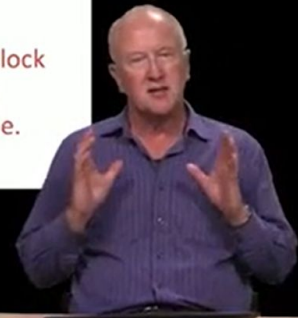


Every aircraft must be able to view
at least(!) 4 GPS satellites

Generally, more than four
satellites are needed. We
favor 7 or 8 *in view* to
guarantee *good geometry*

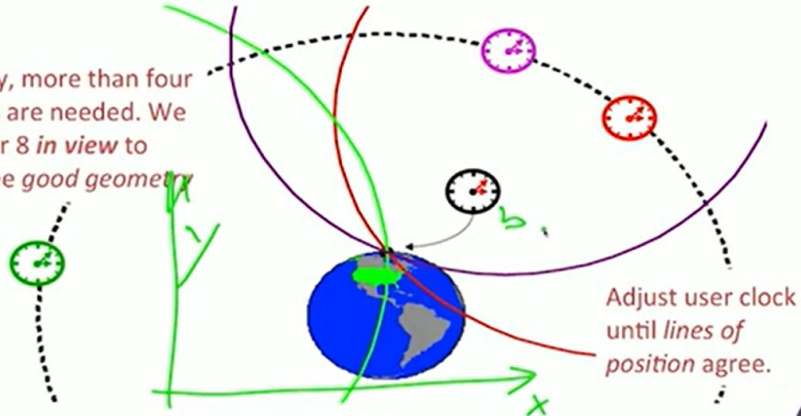


Adjust user clock
until *lines of*
position agree.



Every aircraft must be able to view
at least(!) 4 GPS satellites

Generally, more than four
satellites are needed. We
favor 7 or 8 *in view* to
guarantee *good geometry*



Adjust user clock
until *lines of*
position agree.



Navigation Equations: Solve for four unknowns

$$\begin{aligned}\tau^{(1)} &= \sqrt{(x_u - x^{(1)})^2 + (y_u - y^{(1)})^2 + (z_u - z^{(1)})^2} + b_u - B^{(1)} + \varepsilon_u^{(1)} \\ \tau^{(2)} &= \sqrt{(x_u - x^{(2)})^2 + (y_u - y^{(2)})^2 + (z_u - z^{(2)})^2} + b_u - B^{(2)} + \varepsilon_u^{(2)} \\ \tau^{(3)} &= \sqrt{(x_u - x^{(3)})^2 + (y_u - y^{(3)})^2 + (z_u - z^{(3)})^2} + b_u - B^{(3)} + \varepsilon_u^{(3)} \\ \tau^{(4)} &= \sqrt{(x_u - x^{(4)})^2 + (y_u - y^{(4)})^2 + (z_u - z^{(4)})^2} + b_u - B^{(4)} + \varepsilon_u^{(4)}\end{aligned}$$



Navigation Equations: Solve for four unknowns

$$\begin{aligned}\tau^{(1)} &= \sqrt{(x_u - x^{(1)})^2 + (y_u - y^{(1)})^2 + (z_u - z^{(1)})^2} + b_u - B^{(1)} + \varepsilon_u^{(1)} \\ \tau^{(2)} &= \sqrt{(x_u - x^{(2)})^2 + (y_u - y^{(2)})^2 + (z_u - z^{(2)})^2} + b_u - B^{(2)} + \varepsilon_u^{(2)} \\ \tau^{(3)} &= \sqrt{(x_u - x^{(3)})^2 + (y_u - y^{(3)})^2 + (z_u - z^{(3)})^2} + b_u - B^{(3)} + \varepsilon_u^{(3)} \\ \tau^{(4)} &= \sqrt{(x_u - x^{(4)})^2 + (y_u - y^{(4)})^2 + (z_u - z^{(4)})^2} + b_u - B^{(4)} + \varepsilon_u^{(4)}\end{aligned}$$



Navigation Equations: Solve for four unknowns

$$\begin{aligned}\tau^{(1)} &= \sqrt{(x_u - x^{(1)})^2 + (y_u - y^{(1)})^2 + (z_u - z^{(1)})^2} + b_u - B^{(1)} + \varepsilon_u^{(1)} < 1\text{m} \\ \tau^{(2)} &= \sqrt{(x_u - x^{(2)})^2 + (y_u - y^{(2)})^2 + (z_u - z^{(2)})^2} + b_u - B^{(2)} + \varepsilon_u^{(2)} \\ \tau^{(3)} &= \sqrt{(x_u - x^{(3)})^2 + (y_u - y^{(3)})^2 + (z_u - z^{(3)})^2} + b_u - B^{(3)} + \varepsilon_u^{(3)} \\ \tau^{(4)} &= \sqrt{(x_u - x^{(4)})^2 + (y_u - y^{(4)})^2 + (z_u - z^{(4)})^2} + b_u - B^{(4)} + \varepsilon_u^{(4)}\end{aligned}$$

this to be less than one meter in terms
of measurement errors and then having



Navigation Equations: Solve for four unknowns

$$\begin{aligned}\tau^{(1)} &= \sqrt{(x_u - x^{(1)})^2 + (y_u - y^{(1)})^2 + (z_u - z^{(1)})^2} + b_u - B^{(1)} + \varepsilon_u^{(1)} < 1\text{m} \\ \tau^{(2)} &= \sqrt{(x_u - x^{(2)})^2 + (y_u - y^{(2)})^2 + (z_u - z^{(2)})^2} + b_u - B^{(2)} + \varepsilon_u^{(2)} \\ \tau^{(3)} &= \sqrt{(x_u - x^{(3)})^2 + (y_u - y^{(3)})^2 + (z_u - z^{(3)})^2} + b_u - B^{(3)} + \varepsilon_u^{(3)} \\ \tau^{(4)} &= \sqrt{(x_u - x^{(4)})^2 + (y_u - y^{(4)})^2 + (z_u - z^{(4)})^2} + b_u - B^{(4)} + \varepsilon_u^{(4)}\end{aligned}$$

this to be less than one meter in terms
of measurement errors and then having

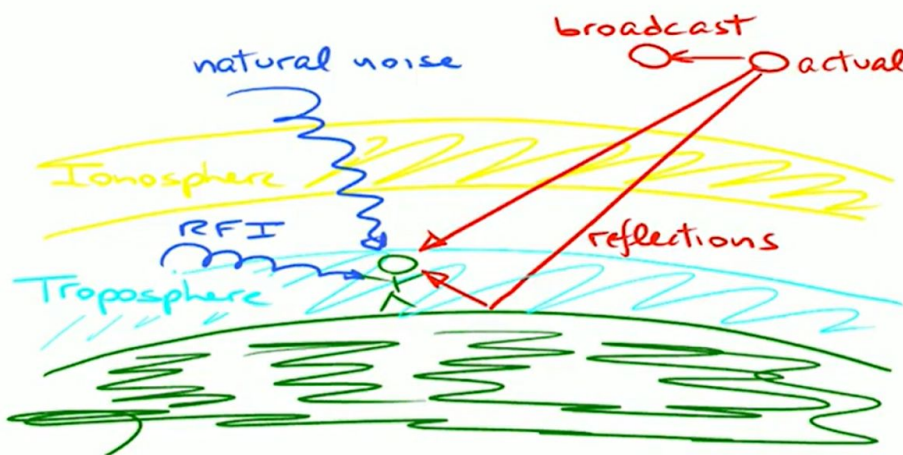


Module 2: GPS Performance & Analysis

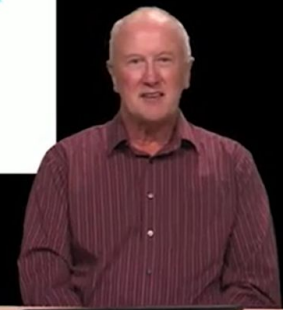
- 2.1 Pseudoranges including errors
- 2.2 Linearization
- 2.3 Solving the linearized navigation equations
- 2.4 Dilution of precision
- 2.5 GPS error budgets



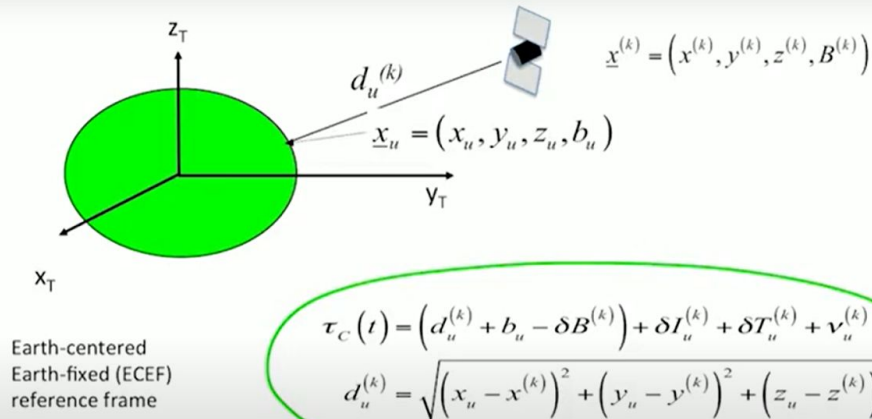
Error Sources



green stick figures standing on the surface of the earth and depicted



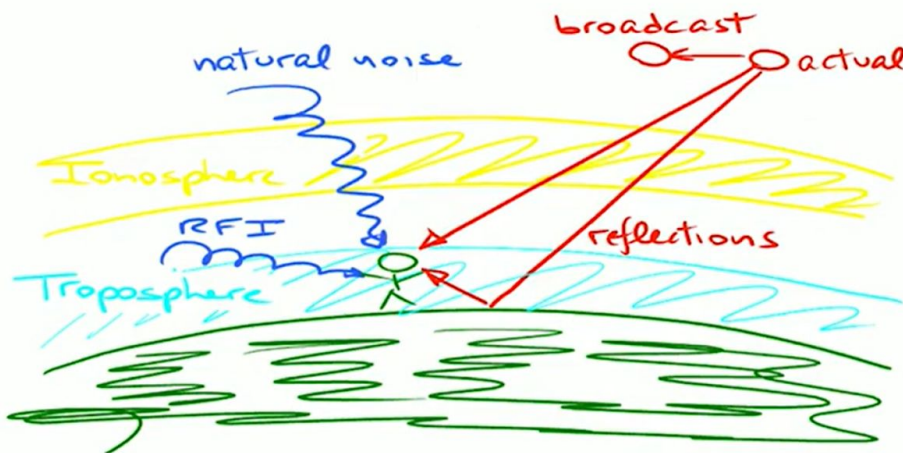
Pseudorange



equation for the pseudo range so it puts those things together be

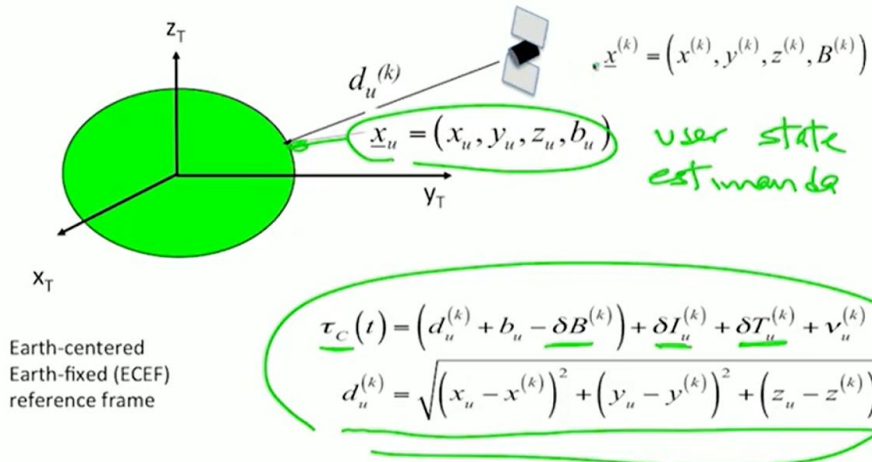
10:10 / 12:41

Error Sources



troposphere it also causes the wave to slow now

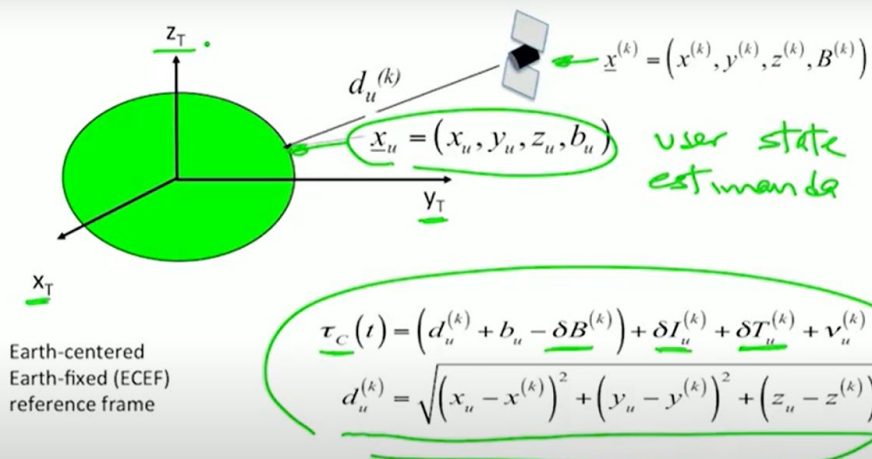
Pseudorange



appears there pictorially and down here mathematically up here we've shown the

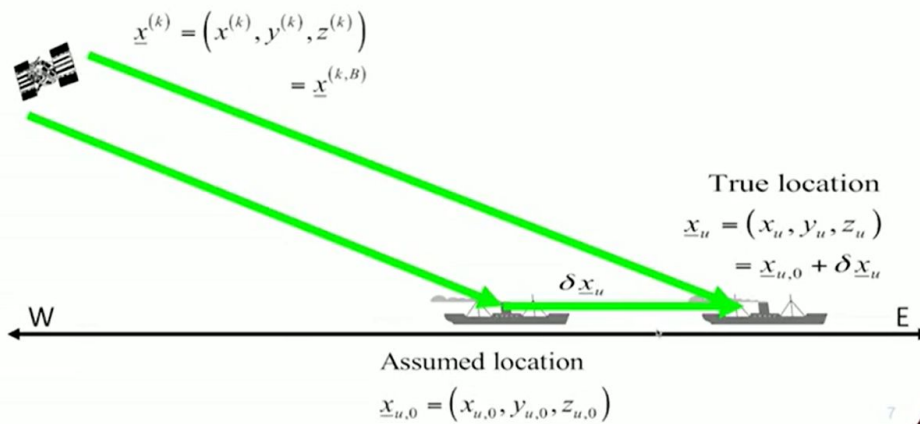
2.1 - Pseudoranges, including errors

Pseudorange



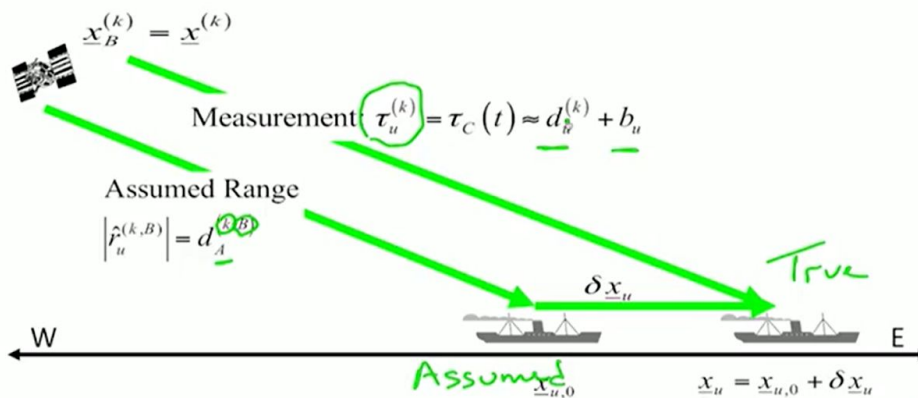
terms of the notation in this course so I hope this has

Navigation Solution: Assumed Position



7

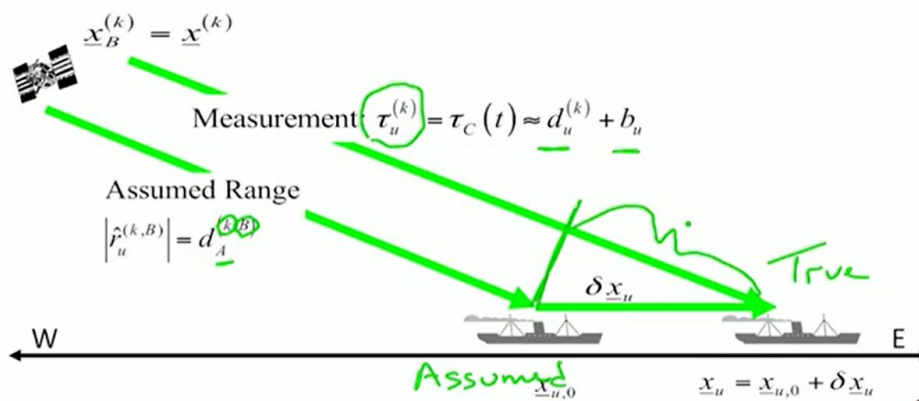
Navigation Solution: Pseudo-range & Theo-range



8

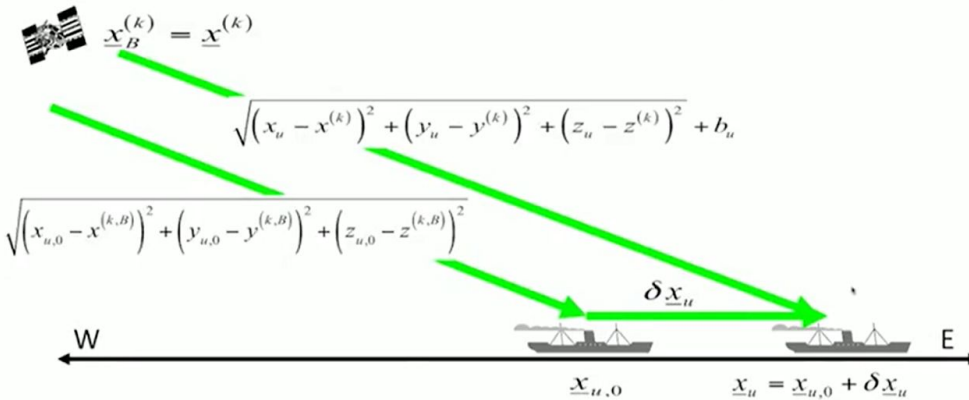
Super K is the true distance and da
Super

Navigation Solution: Pseudo-range & Theo-range



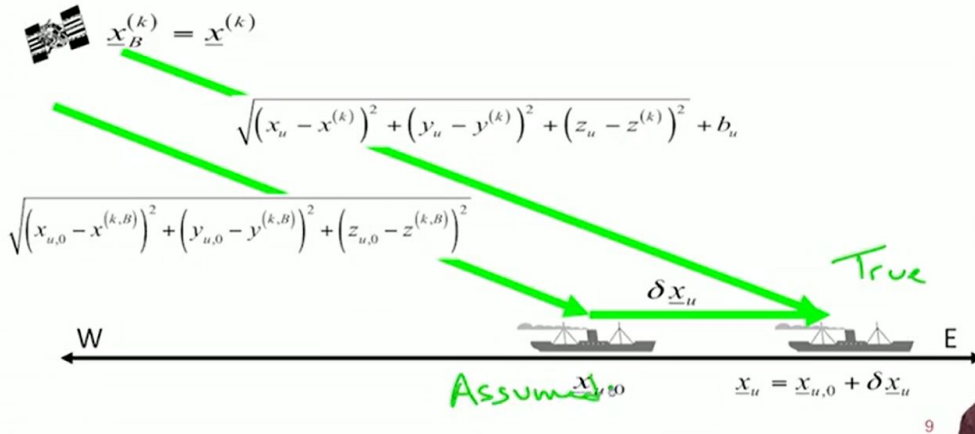
say well that difference can be solved
for if we know

Navigation Solution Pseudo-range & Theo-range



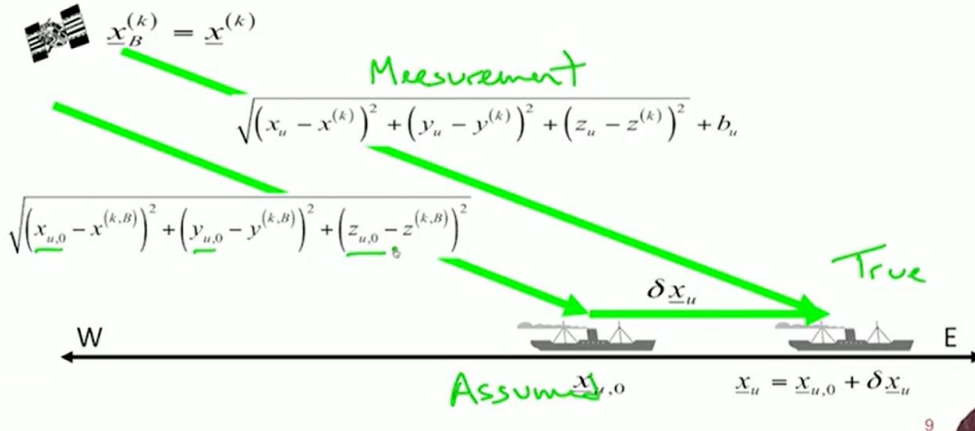
little bit more detail
same situation true

Navigation Solution Pseudo-range & Theo-range



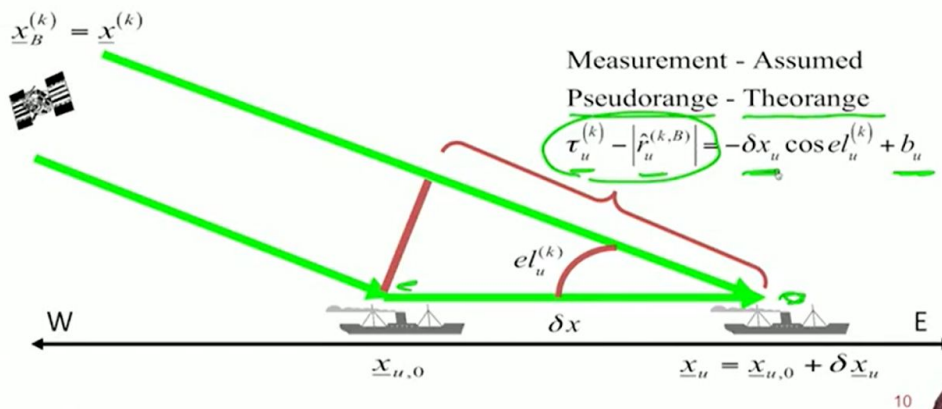
same situation true location over here
assumed over here now we've provided

Navigation Solution Pseudo-range & Theo-range



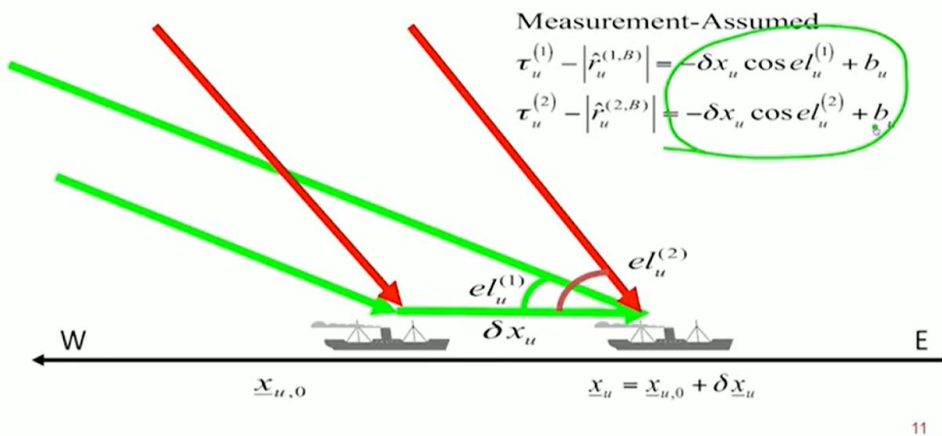
distance measurement in the case of the
true measurement and

One Dimensional Navigation Solution



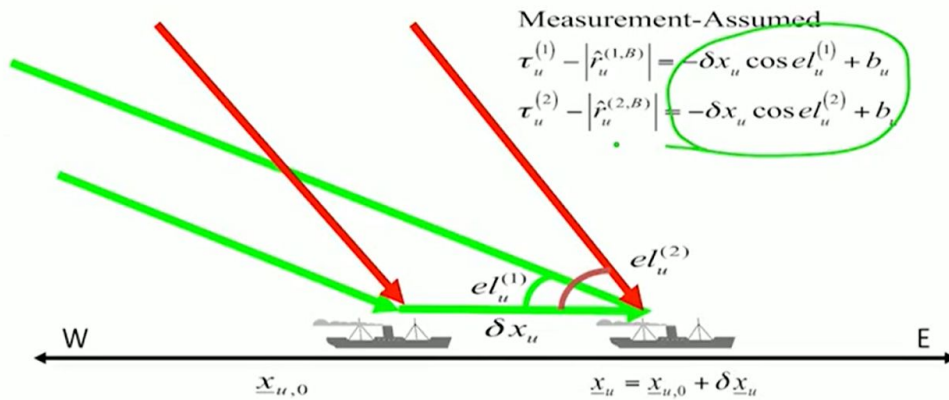
contained or somehow obliterated the
esta manda we

1 D Navigation Solution Two satellites to Solve for x_u and b_u



angles to be a little bit different at
least a little bit different

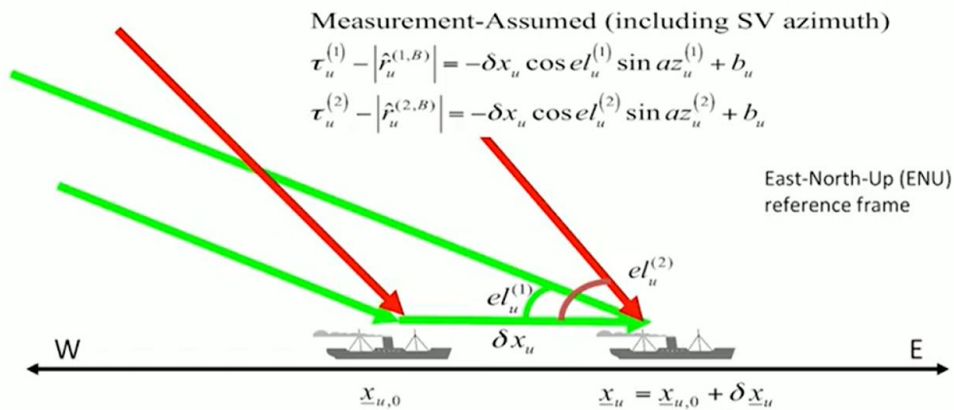
1 D Navigation Solution Two satellites to Solve for x_u and b_u



11

number is in the case of satellite one
similarly we have a number

1 D Navigation Solution Two satellites to Solve for x_u and b_u



12

the horizon azimuth is the angle made by
that line of sight relative

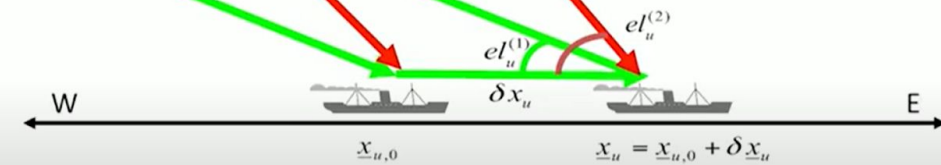
1 D Navigation Solution

Two satellites to Solve for x_u and b_u

Measurement-Assumed (including SV azimuth)

$$\tau_u^{(1)} - \left| \hat{r}_u^{(1,B)} \right| = -\delta x_u \cos el_u^{(1)} \sin az_u^{(1)} + b_u$$

$$\tau_u^{(2)} - \left| \hat{r}_u^{(2,B)} \right| = -\delta x_u \cos el_u^{(2)} \sin az_u^{(2)} + b_u$$

East-North-Up (ENU)
reference frame

12

equations has not disappeared by the way
when we talk about navigation

17:47 / 23:17

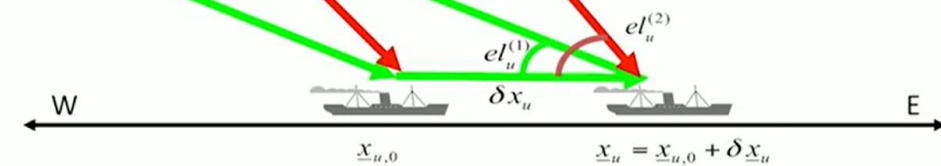
1 D Navigation Solution

Two satellites to Solve for x_u and b_u

Measurement-Assumed (including SV azimuth)

$$\tau_u^{(1)} - \left| \hat{r}_u^{(1,B)} \right| = -\delta x_u \cos el_u^{(1)} \sin az_u^{(1)} + b_u$$

$$\tau_u^{(2)} - \left| \hat{r}_u^{(2,B)} \right| = -\delta x_u \cos el_u^{(2)} \sin az_u^{(2)} + b_u$$

East-North-Up (ENU)
reference frame

12

reference frame called
east north up

Linearized Navigation Equations

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\cos e l_u^{(1)} \sin az_u^{(1)} & -\cos e l_u^{(1)} \cos az_u^{(1)} & -\sin e l_u^{(1)} & 1 \\ -\cos e l_u^{(2)} \sin az_u^{(2)} & -\cos e l_u^{(2)} \cos az_u^{(2)} & -\sin e l_u^{(2)} & 1 \\ \vdots & \vdots & \vdots & \vdots \\ -\cos e l_u^{(K)} \sin az_u^{(K)} & -\cos e l_u^{(K)} \cos az_u^{(K)} & -\sin e l_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} \tilde{G}^{(1)} \\ \tilde{G}^{(2)} \\ \vdots \\ \tilde{G}^{(K)} \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\delta\tau^{(k)} - \tilde{G}^{(k)} \begin{bmatrix} \delta E_u & \delta N_u & \delta U_u & \delta b_u \end{bmatrix}^T$$

East-North-Up (ENU)
reference frame

here's the next

Linearized Navigation Equations

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\cos e l_u^{(1)} \sin az_u^{(1)} & -\cos e l_u^{(1)} \cos az_u^{(1)} & -\sin e l_u^{(1)} & 1 \\ -\cos e l_u^{(2)} \sin az_u^{(2)} & -\cos e l_u^{(2)} \cos az_u^{(2)} & -\sin e l_u^{(2)} & 1 \\ \vdots & \vdots & \vdots & \vdots \\ -\cos e l_u^{(K)} \sin az_u^{(K)} & -\cos e l_u^{(K)} \cos az_u^{(K)} & -\sin e l_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} \tilde{G}^{(1)} \\ \tilde{G}^{(2)} \\ \vdots \\ \tilde{G}^{(K)} \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\delta\tau^{(k)} - \tilde{G}^{(k)} \begin{bmatrix} \delta E_u & \delta N_u & \delta U_u & \delta b_u \end{bmatrix}^T$$

East-North-Up (ENU)
reference frame

discover that the multiplying terms on a
satellite by satellite basis are

Linearized Navigation Equations

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\cos e_l^{(1)} \sin az_u^{(1)} & -\cos e_l^{(1)} \cos az_u^{(1)} & -\sin e_l^{(1)} & 1 \\ -\cos e_l^{(2)} \sin az_u^{(2)} & -\cos e_l^{(2)} \cos az_u^{(2)} & -\sin e_l^{(2)} & 1 \\ \vdots & \vdots & \vdots & \vdots \\ -\cos e_l^{(K)} \sin az_u^{(K)} & -\cos e_l^{(K)} \cos az_u^{(K)} & -\sin e_l^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} \tilde{G}^{(1)} \\ \tilde{G}^{(2)} \\ \vdots \\ \tilde{G}^{(K)} \end{bmatrix} \begin{bmatrix} \delta E_u \\ \delta N_u \\ \delta U_u \\ \delta b_u \end{bmatrix}$$

$$\delta\tau^{(k)} - \tilde{G}^{(k)} \begin{bmatrix} \delta E_u & \delta N_u & \delta U_u & \delta b_u \end{bmatrix}^T$$

East-North-Up (ENU)
reference frame

K might be the ten or nine that we have
in view this matrix is so

20:34 / 23:17

Linearized Navigation Equations

$$\tau_u^{(k)} = \left| \underline{x}^{(k)} - \underline{x}_u \right| + b_u + v_u^{(k)} \quad \text{pseudorange}$$

$$\tau_{u,0}^{(k)} = \left| \underline{x}_B^{(k)} - \hat{\underline{x}}_{u,0} \right| + \hat{b}_{u,0} \quad \text{Xorange}$$

$$\delta\tau^{(k)} = -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta\underline{x}^{(k)} \cdot \underline{1}_u^{(k)} + \delta I + \delta T + \delta b_u - \delta B^{(k)} + v_u^{(k)}$$

$$\delta\tau^{(k)} = -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta b_u + \tilde{v}_u^{(k)}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\underline{1}_u^{(1)} & 1 \\ -\underline{1}_u^{(2)} & 1 \\ \vdots & \vdots \\ -\underline{1}_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta x_u \\ \delta y_u \\ \delta z_u \\ \delta b_u \end{bmatrix} + \begin{bmatrix} \tilde{v}_u^{(1)} \\ \tilde{v}_u^{(2)} \\ \vdots \\ \tilde{v}_u^{(K)} \end{bmatrix}$$

$$\delta\tau = G\delta\underline{x}_u + \tilde{\underline{v}}_u$$

Earth-centered
Earth-fixed (ECEF)
reference frame

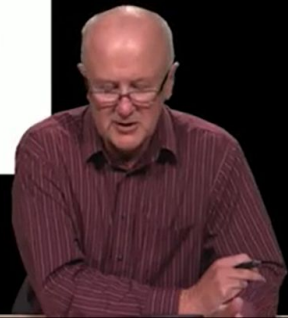
Linearized Navigation Equations

$$\begin{aligned}
 \tau_u^{(k)} &= \left| \underline{x}^{(k)} - \underline{x}_u \right| + b_u + v_u^{(k)} && \text{pseudorange} \\
 \tau_{u,0}^{(k)} &= \left| \underline{x}_B^{(k)} - \hat{\underline{x}}_{u,0} \right| + \hat{b}_{u,0} && \text{Xorange} \\
 \delta \tau^{(k)} &= -\delta \underline{x}_u \cdot \underline{1}_u^{(k)} + \delta \underline{x}^{(k)} \cdot \underline{1}_u^{(k)} + \delta I + \delta T + \delta b_u - \delta B^{(k)} + v_u^{(k)} \\
 \delta \tau^{(k)} &= -\delta \underline{x}_u \cdot \underline{1}_u^{(k)} + \delta b_u + \tilde{v}_u^{(k)}
 \end{aligned}$$

$$\begin{bmatrix} \delta \tau^{(1)} \\ \delta \tau^{(2)} \\ \vdots \\ \delta \tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\underline{1}_u^{(1)} & 1 \\ -\underline{1}_u^{(2)} & 1 \\ \vdots & \vdots \\ -\underline{1}_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta x_u \\ \delta y_u \\ \delta z_u \\ \delta b_u \end{bmatrix} + \begin{bmatrix} \tilde{v}_u^{(1)} \\ \tilde{v}_u^{(2)} \\ \vdots \\ \tilde{v}_u^{(K)} \end{bmatrix}$$

$$\delta \underline{\tau} = G \delta \underline{x}_u + \tilde{\underline{v}}_u$$

Earth-centered
Earth-fixed (ECEF)
reference frame



Linearized Navigation Equations

$$\begin{aligned}
 \tau_u^{(k)} &= \left| \underline{x}^{(k)} - \underline{x}_u \right| + b_u + v_u^{(k)} && \text{pseudorange} \\
 \tau_{u,0}^{(k)} &= \left| \underline{x}_B^{(k)} - \hat{\underline{x}}_{u,0} \right| + \hat{b}_{u,0} && \text{Xorange} \\
 \delta \tau^{(k)} &= -\delta \underline{x}_u \cdot \underline{1}_u^{(k)} + \delta \underline{x}^{(k)} \cdot \underline{1}_u^{(k)} + \delta I + \delta T + \delta b_u - \delta B^{(k)} + v_u^{(k)} \\
 \delta \tau^{(k)} &= -\delta \underline{x}_u \cdot \underline{1}_u^{(k)} + \delta b_u + \tilde{v}_u^{(k)}
 \end{aligned}$$

$$\begin{bmatrix} \delta \tau^{(1)} \\ \delta \tau^{(2)} \\ \vdots \\ \delta \tau^{(K)} \end{bmatrix} = \begin{bmatrix} -\underline{1}_u^{(1)} & 1 \\ -\underline{1}_u^{(2)} & 1 \\ \vdots & \vdots \\ -\underline{1}_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta x_u \\ \delta y_u \\ \delta z_u \\ \delta b_u \end{bmatrix} + \begin{bmatrix} \tilde{v}_u^{(1)} \\ \tilde{v}_u^{(2)} \\ \vdots \\ \tilde{v}_u^{(K)} \end{bmatrix}$$

$$\delta \underline{\tau} = G \delta \underline{x}_u + \tilde{\underline{v}}_u$$

Earth-centered
Earth-fixed (ECEF)
reference frame



there we have just smushed them all in
there so our belief and in

Linearized Navigation Equations

$$\begin{aligned}\tau_u^{(k)} &= \left| \underline{x}^{(k)} - \underline{x}_u \right| + b_u + v_u^{(k)} && \text{pseudorange} \\ \tau_{u,0}^{(k)} &= \left| \underline{x}_B^{(k)} - \hat{\underline{x}}_{u,0} \right| + \hat{b}_{u,0} && \text{X-range} \\ \delta\tau^{(k)} &= -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta\underline{x}^{(k)} \cdot \underline{1}_u^{(k)} + \delta I + \delta T + \delta b_u - \delta B^{(k)} + v_u^{(k)} \\ \delta\tau^{(k)} &= -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta b_u + \tilde{v}_u^{(k)}\end{aligned}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -1_u^{(1)} & 1 \\ -1_u^{(2)} & 1 \\ \vdots & \vdots \\ -1_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta x_u \\ \delta y_u \\ \delta z_u \\ \delta b_u \end{bmatrix} + \begin{bmatrix} \tilde{v}_u^{(1)} \\ \tilde{v}_u^{(2)} \\ \vdots \\ \tilde{v}_u^{(K)} \end{bmatrix}$$

measurements $\delta\tau = G\delta\underline{x}_u + \tilde{\underline{v}}_u$ state noise

Earth-centered Earth-fixed (ECEF) reference frame

we'll just write Delta Tau is equal to G Delta X plus noise

Linearized Navigation Equations

$$\begin{aligned}\tau_u^{(k)} &= \left| \underline{x}^{(k)} - \underline{x}_u \right| + b_u + v_u^{(k)} \\ \tau_{u,0}^{(k)} &= \left| \underline{x}_B^{(k)} - \hat{\underline{x}}_{u,0} \right| + \hat{b}_{u,0} \\ \delta\tau^{(k)} &= -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta\underline{x}^{(k)} \cdot \underline{1}_u^{(k)} + \delta I + \delta T + \delta b_u - \delta B^{(k)} + v_u^{(k)} \\ \delta\tau^{(k)} &= -\delta\underline{x}_u \cdot \underline{1}_u^{(k)} + \delta b_u + \tilde{v}_u^{(k)}\end{aligned}$$

$$\begin{bmatrix} \delta\tau^{(1)} \\ \delta\tau^{(2)} \\ \vdots \\ \delta\tau^{(K)} \end{bmatrix} = \begin{bmatrix} -1_u^{(1)} & 1 \\ -1_u^{(2)} & 1 \\ \vdots & \vdots \\ -1_u^{(K)} & 1 \end{bmatrix} \begin{bmatrix} \delta x_u \\ \delta y_u \\ \delta z_u \\ \delta b_u \end{bmatrix} + \begin{bmatrix} \tilde{v}_u^{(1)} \\ \tilde{v}_u^{(2)} \\ \vdots \\ \tilde{v}_u^{(K)} \end{bmatrix}$$

$$\delta\tau = G\delta\underline{x}_u + \tilde{\underline{v}}_u$$

Earth-centered Earth-fixed (ECEF) reference frame

that idea is repeated on the next view graph let's have

Solving the Linearized Equations

$$\delta \underline{\tau} = G \delta \underline{x}_u + \underline{\tilde{v}}_u$$

$$K = 4$$

$$\begin{aligned}\delta \hat{\underline{x}}_u &= G^{-1} (\delta \underline{\tau} - \underline{\tilde{v}}_u) \\ &= G^{-1} \delta \underline{\tau} - G^{-1} \underline{\tilde{v}}_u\end{aligned}$$

$$\delta \hat{\underline{x}}_u - G^{-1} \delta \underline{\tau} = -G^{-1} \underline{\tilde{v}}_u$$

$$K > 4$$

$$\delta \hat{\underline{x}}_u = (G^T G)^{-1} G (\delta \underline{\tau} - \underline{\tilde{v}}_u)$$

$$\min S = \sum_k (\tau^{(k)} - G^{(k)} \underline{x})^2$$

graph let's have a look here it is broken



Navigation Solution

- Correlation (provides sub-chip and whole chip resolution)
- Arrival and transmission time (includes whole codes and navigation bits)
- Pseudorange
 - measurement
 - includes a user clock bias
- Theorange
 - constructed from assumed location
 - navigation message
- Difference of pseudorange and theorange is a linear function of unknowns
- Solve system of linear equations for four unknowns

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all told the navigation solution



Solving the Linearized Equations

$$\delta \underline{\tau} = G \delta \underline{x}_u + \tilde{\underline{v}}_u$$

$$K = 4$$

$$\delta \hat{\underline{x}}_u = G^{-1} (\delta \underline{\tau} - \tilde{\underline{v}}_u)$$

$$= G^{-1} \delta \underline{\tau} - G^{-1} \tilde{\underline{v}}_u$$

$$\delta \hat{\underline{x}}_u - G^{-1} \delta \underline{\tau} = -G^{-1} \tilde{\underline{v}}_u$$

exactly specified

$$K > 4$$

$$\delta \hat{\underline{x}}_u = (G^T G)^{-1} G^T (\delta \underline{\tau} - \tilde{\underline{v}}_u)$$

$$\min S = \sum_k (\tau^{(k)} - G^{(k)} \underline{x})^2$$

credit of two different satellites
they've collapsed

