

# High-Order Semi-Implicit Time Integration Methods for Multiscale Advection Physics

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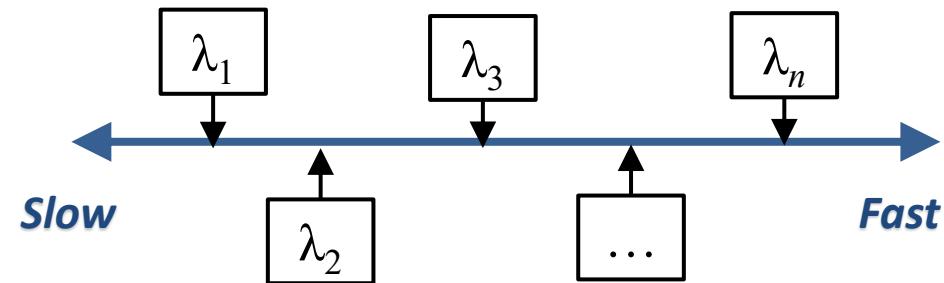
# Time Scales in Complex Physics Simulations

Model ODE  
in time

$$\frac{dy}{dt} = \lambda_1 y + \lambda_2 y + \cdots + \lambda_n y;$$

$$\begin{aligned}\lambda_i &\in \mathbb{Z} \\ \lambda_1 &< \lambda_2 < \cdots < \lambda_n\end{aligned}$$

Complex physics are characterized by a **large range of temporal scales**

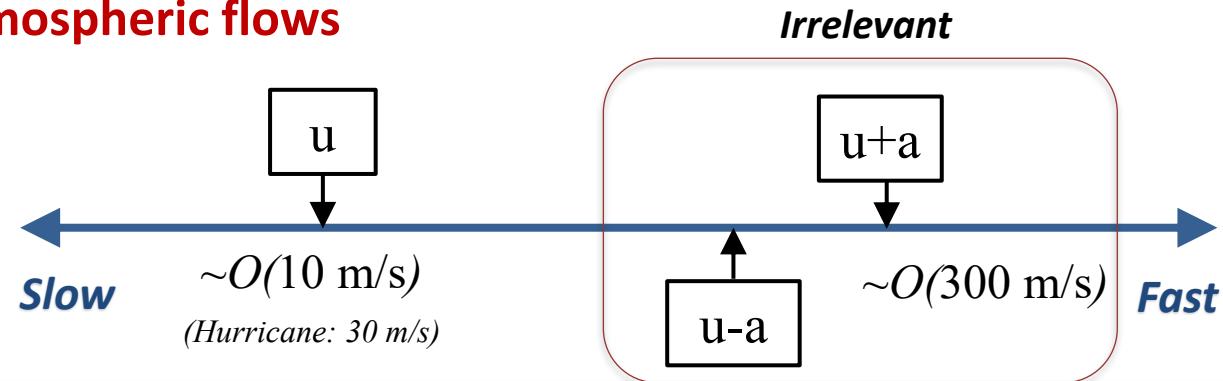


Which time scales do we want to resolve? (*Usually, some of them*)

In the context of atmospheric flows

$u$ : flow velocity

$a$ : speed of sound

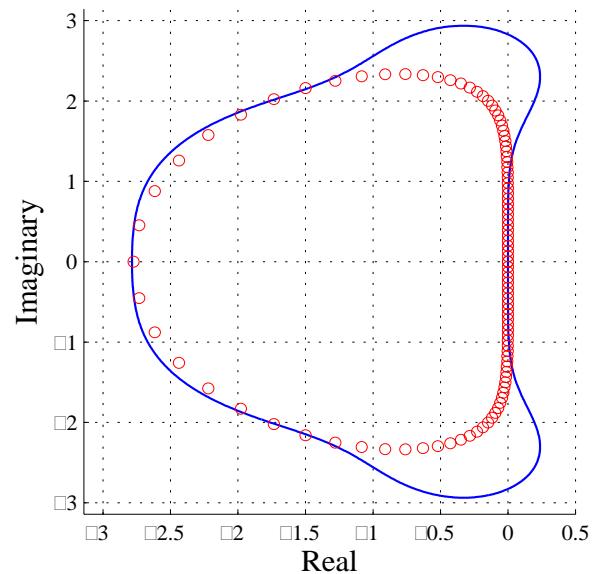


# Explicit vs. Implicit Time Integration

## Motivation for Implicit-Explicit (IMEX) Approach

**Explicit time-integration** constrained by *fastest time scale in the model*

- Simple to implement; very scalable
- Eigenvalues of RHS must lie within stability region of time integrator
- *Inefficient when resolving slow dynamics*



**Implicit time-integration** allows time steps determined by the physics

- *Unconditional stability*
- Requires solution to *nonlinear system of equations* (computational expense, scalability, preconditioning)
- *Why pay for inverting/solving the terms we want to resolve?*

**IMEX: Best of both worlds?**

# Implicit-Explicit (IMEX) Time Integration

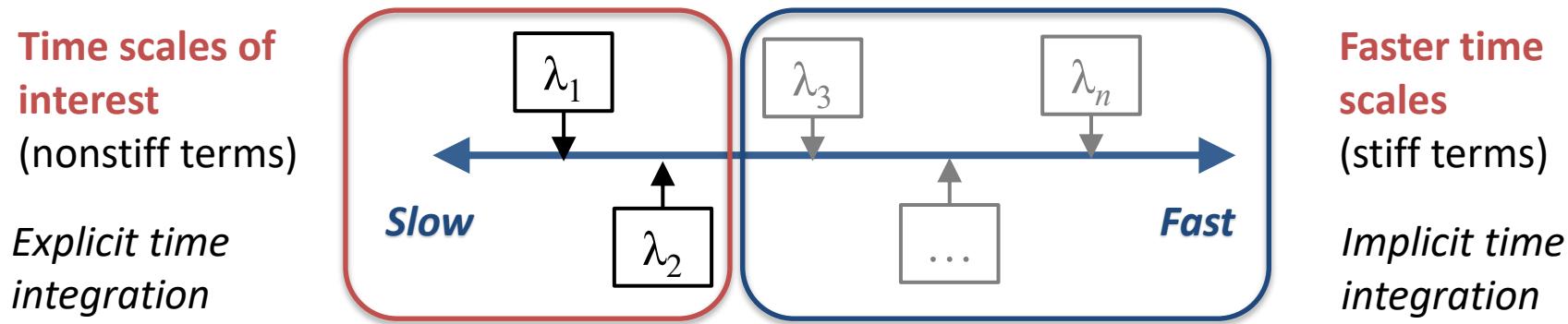
Resolve scales of interest; Treat implicitly faster scales

## Semi-discrete ODE in time

Resulting from spatial discretization of PDE

$$\frac{dy}{dt} = \mathcal{R}(y)$$

IMEX time integration: *partition RHS*  $\mathcal{R}(y) = \mathcal{R}_{\text{nonstiff}}(y) + \mathcal{R}_{\text{stiff}}(y)$



Linear stability constraint  
on time step  $\Delta t \left( \lambda \left[ \frac{d\mathcal{R}_{\text{nonstiff}}(y)}{dy} \right] \right) \in \{z : |R(z)| \leq 1\}$

Time step constrained by eigenvalues (time scales) of *nonstiff component of RHS*

# Additive Runge-Kutta (ARK) Time Integrators

Multistage, high-order, conservative IMEX methods

**Time step:** From  $t_n$  to  $t_{n+1} = t_n + \Delta t$

*Stage solutions*

$$\mathbf{y}^{(i)} = \mathbf{y}_n + \Delta t \sum_{j=1}^{i-1} a_{ij} \mathcal{R}_{\text{nonstiff}}(\mathbf{y}^{(j)}) + \Delta t \sum_{j=1}^i \tilde{a}_{ij} \mathcal{R}_{\text{stiff}}(\mathbf{y}^{(j)}), \quad i = 1, \dots, s$$

$$\mathbf{y}_{n+1} = \mathbf{y}_n + \Delta t \sum_{i=1}^s b_i \mathcal{R}(\mathbf{y}^{(i)}) \quad \textit{Step completion}$$

*Kennedy & Carpenter,  
J. Comput. Phys., 2003*

*Butcher tableaux representation*

0	0	Explicit RK		
$c_2$	$a_{21}$	0		
$\vdots$	$\vdots$	$\ddots$	0	
$c_s$	$a_{s1}$	$\cdots$	$a_{s,s-1}$	0
	$b_1$	$\cdots$	$\cdots$	$b_s$

+

0	0	Diagonally- Implicit RK (DIRK)		
$\tilde{c}_2$	$\tilde{a}_{21}$	$\gamma$		
$\vdots$	$\vdots$	$\ddots$	$\gamma$	
$\tilde{c}_s$	$\tilde{a}_{s1}$	$\cdots$	$\tilde{a}_{s,s-1}$	$\gamma$
	$b_1$	$\cdots$	$\cdots$	$b_s$

$s$  is the number  
of stages

**Note:** not any  
combination of an explicit  
RK and DIRK will work!

# Implicit Stage Solution

Requires solving nonlinear system of equations

Rearranging the stage solution expression:

$$\underbrace{\frac{1}{\Delta t \tilde{a}_{ii}} \mathbf{y}^{(i)} - \mathcal{R}_{\text{stiff}}(\mathbf{y}^{(i)}) - \left[ \mathbf{y}_n + \Delta t \sum_{j=1}^{i-1} \left\{ a_{ij} \mathcal{R}_{\text{nonstiff}}(\mathbf{y}^{(j)}) + \tilde{a}_{ij} \mathcal{R}_{\text{stiff}}(\mathbf{y}^{(j)}) \right\} \right]}_{\mathcal{F}(y) = 0} = 0$$

**Jacobian-free Newton-Krylov** method (*Knoll & Keyes, J. Comput. Phys., 2004*):

Initial guess:  $y_0 \equiv \mathbf{y}_0^{(i)} = \mathbf{y}^{(i-1)}$

Newton update:  $y_{k+1} = y_k - \mathcal{J}(y_k)^{-1} \mathcal{F}(y_k)$

Preconditioned GMRES

$$\mathcal{J}\mathcal{P}^{-1}\mathcal{P}\Delta y = \mathcal{F}(y_k)$$

Action of the Jacobian on a vector approximated by *directional derivative*

$$\mathcal{J}(y_k) x = \left. \frac{d\mathcal{F}(y)}{dy} \right|_{y_k} x \approx \frac{1}{\epsilon} [\mathcal{F}(y_k + \epsilon x) - \mathcal{F}(y_k)]$$

# Atmospheric Flows: Governing Equations

## Exner Pressure and Potential Temperature

- COAMP5 (US Navy), MM5 (NCAR/PSU), NMM (NCEP)
- Does not conserve mass/momentum/energy

## Mass, Momentum, and Potential Temperature

- WRF (NCAR), NUMA (NPS)
- Conserved mass and momentum, not energy
- Does not allow inclusion of true diffusion terms

## Mass, Momentum, and Energy

- Examples?
- Conserves mass, momentum, and energy
- Allows inclusion of viscosity and thermal conduction

Atmospheric flows: **small perturbations** around hydrostatic balance

Perturbation form of governing equations

**Balanced formulation with full quantities**

**Main Advantage?** Allows the application of the vast number of CFD codes with minimal modifications

# Fast Time Scales and Time Integration

**Limited-area** and **mesoscale** simulations require a **nonhydrostatic model**

Nonhydrostatic model introduces the **acoustic mode**

- Sound waves *much faster than flow velocities*
- **Insignificant effect** on atmospheric phenomena

Multiscale time integration

Explicit Time Integration

- Time step size restricted by acoustic waves and/or vertical grid spacing
- Acoustic waves do not significantly impact any atmospheric phenomenon
- **Split-explicit methods**

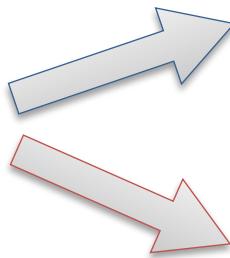
Implicit Time Integration

- Unconditionally stable
- Requires solutions to non-linear system or linearized approximation

# IMEX Time Integrators for Atmospheric Flows

## IMEX Time Integration

“Fast” waves implicitly  
“Slow” waves explicitly

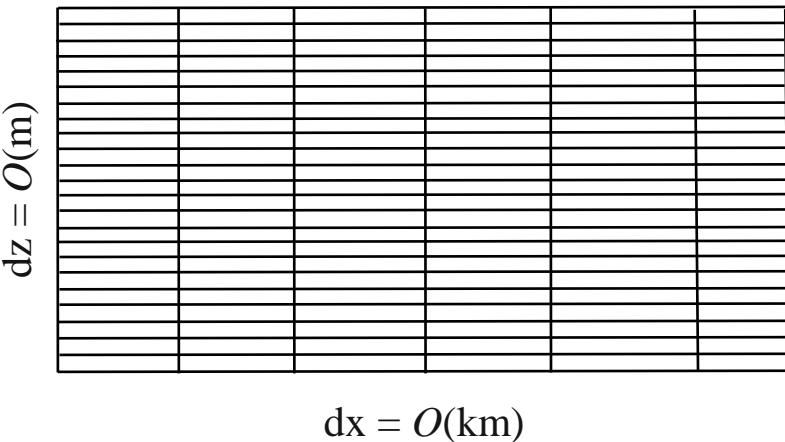


## Horizontal-Explicit, Vertical-Implicit (HEVI)

## Flux-Partitioned Methods

### Horizontal-Explicit, Vertical-Implicit Methods

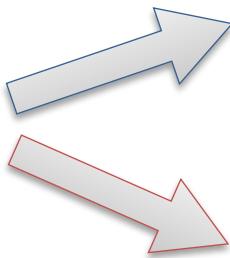
- Simulation domains are much larger horizontally than vertically
- Grids are typically *much finer* along the vertical ( $z$ ) axis
- Terms with  **$z$ -derivatives integrated implicitly**, remaining terms integrated explicitly



# IMEX Time Integrators for Atmospheric Flows

## IMEX Time Integration

“Fast” waves implicitly  
“Slow” waves explicitly



## Horizontal-Explicit, Vertical-Implicit (HEVI)

## Flux-Partitioned Methods

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{u}) = \mathbf{S}$$



$$\nabla \cdot \mathbf{F} = \nabla \cdot \mathbf{F}_{\text{slow}} + \nabla \cdot \mathbf{F}_{\text{fast}}$$

### Flux-Partitioned Methods

- Right-hand-side partitioned into linear stiff (fast) and nonlinear nonstiff (slow) components
- Formulation based on perturbations to the hydrostatic balance
- ***First-order perturbations treated implicitly;*** higher-order perturbations treated explicitly.

# Developing an Atmospheric Flow Code

Collaborator: Emil Constantinescu (ANL) (2013-2016)

Develop a conservative, high-order finite-difference based on the compressible Euler equations (*conservation of mass, momentum, energy*)

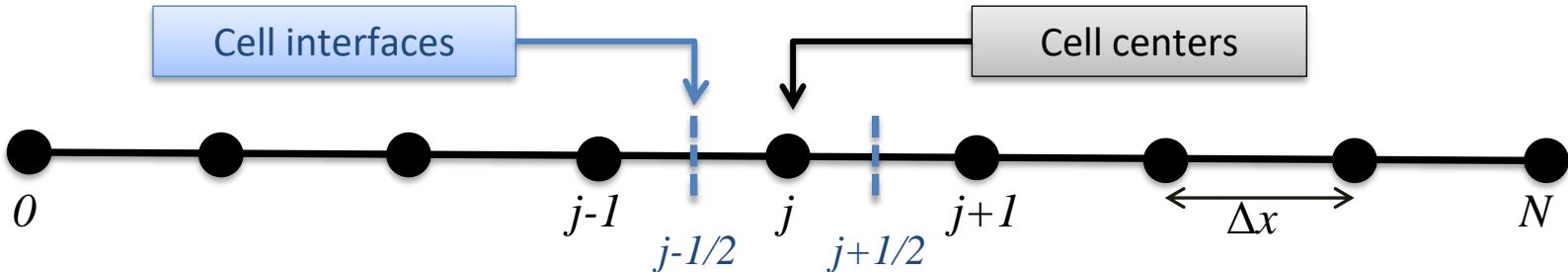
$$\frac{\partial}{\partial t} \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ e \end{bmatrix} + \frac{\partial}{\partial x} \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho u v \\ (e + p)u \end{bmatrix} + \frac{\partial}{\partial y} \begin{bmatrix} \rho v \\ \rho u v \\ \rho v^2 + p \\ (e + p)v \end{bmatrix} = \begin{bmatrix} 0 \\ \rho \mathbf{g} \cdot \hat{\mathbf{i}} \\ \rho \mathbf{g} \cdot \hat{\mathbf{j}} \\ \rho u \mathbf{g} \cdot \hat{\mathbf{i}} + \rho v \mathbf{g} \cdot \hat{\mathbf{j}} \end{bmatrix}$$

**Balanced formulation for full quantities:** Hydrostatic balance preserved to machine precision without writing equations in terms of perturbations

**Flux-partitioning for IMEX time-integration:** Isolate acoustic and gravity waves from convective mode

The work presented here is implemented in HyPar (<http://hypar.github.io/>) - C/C++ code for hyperbolic-parabolic PDEs.

# Conservative Finite-Difference Schemes



*Conservative finite-difference discretization of a 1D hyperbolic conservation law:*

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{u})}{\partial x} = 0 \quad \Rightarrow \quad \frac{\partial \mathbf{u}}{\partial t} + \frac{1}{\Delta x} \left( \mathbf{h}_{j+\frac{1}{2}} - \mathbf{h}_{j-\frac{1}{2}} \right) = 0 \quad \mathbf{f}(\mathbf{u}(x)) = \frac{1}{\Delta x} \int_{x-\frac{\Delta x}{2}}^{x+\frac{\Delta x}{2}} \mathbf{h}(\mathbf{u}(\xi)) d\xi$$

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{1}{\Delta x} \left( \hat{\mathbf{f}}_{j+\frac{1}{2}} - \hat{\mathbf{f}}_{j-\frac{1}{2}} \right) = 0$$

Spatially-discretized ODE in time

$$\hat{\mathbf{f}}_{j+\frac{1}{2}} = \mathbf{h} \left( \mathbf{u} \left( x_{j+\frac{1}{2}} \right) \right) + \mathcal{O}(\Delta x^p)$$

5<sup>th</sup> order WENO  
(Jiang & Shu, J. Comput. Phys., 1996)

5<sup>th</sup> order CRWENO  
(Ghosh & Baeder, SIAM J. Sci. Comput., 2012)

# Characteristic-based Flux Partitioning (1)

## 1D Euler equations

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{F}(\mathbf{u})}{\partial x} = 0$$

Spatial  
discretization  
→

## Semi-discrete ODE in time

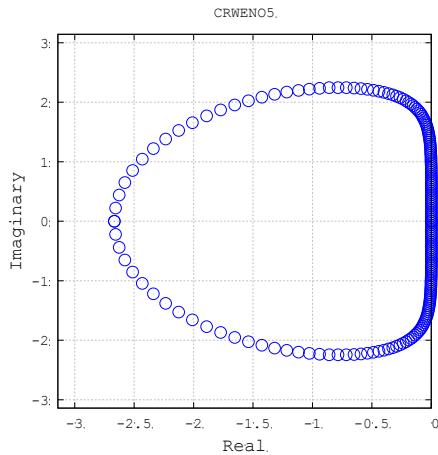
$$\frac{\partial \mathbf{u}}{\partial t} = \hat{\mathbf{F}}(\mathbf{u}) = [\mathcal{D} \otimes \mathcal{A}(u)] \mathbf{u}$$

Discretization operator  
(e.g.:WENO5, CRWENO5)

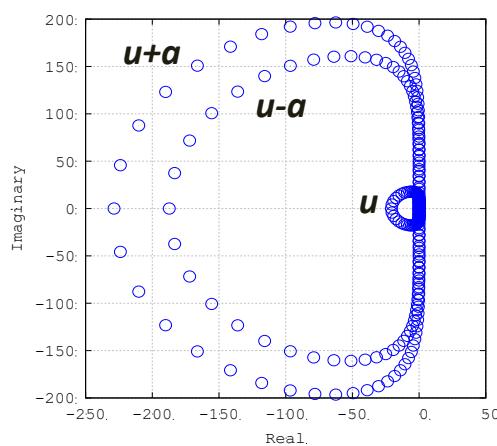
Flux Jacobian

$$\text{eig} \left[ \frac{\partial \hat{\mathbf{F}}}{\partial \mathbf{u}} \right] = \text{eig} [\mathcal{D}] \times \text{eig} [\mathcal{A}(u)]$$

Time step size limit for  
linear stability



Eigenvalues of the CRWENO5  
discretization



Eigenvalues of the right-  
hand-side operator  
(u=0.1, a=1.0, dx=0.0125)

Eigenvalues of the right-hand-side of  
the ODE are the eigenvalues of the  
discretization operator times the  
characteristic speeds of the physical  
system

# Characteristic-based Flux Partitioning (2)

Splitting of the **flux Jacobian** based on its eigenvalues

$$\begin{aligned}\frac{\partial \mathbf{u}}{\partial t} &= \hat{\mathbf{F}}(\mathbf{u}) = [\mathcal{D} \otimes \mathcal{A}(u)] \mathbf{u} \\ &= [\mathcal{D} \otimes \mathcal{A}_S(u) + \mathcal{D} \otimes \mathcal{A}_F(u)] \mathbf{u} \\ &= \hat{\mathbf{F}}_S(\mathbf{u}) + \hat{\mathbf{F}}_F(\mathbf{u})\end{aligned}$$

**“Slow” flux    “Fast” Flux**

$$\mathbf{f}_S(\mathbf{u}) = \begin{bmatrix} \left(\frac{\gamma-1}{\gamma}\right) \rho u \\ \left(\frac{\gamma-1}{\gamma}\right) \rho u^2 \\ \frac{1}{2} \left(\frac{\gamma-1}{\gamma}\right) \rho u^3 \end{bmatrix} \quad \text{Convective flux (slow)}$$

**Acoustic flux (fast)**

$$\mathbf{f}_F(\mathbf{u}) = \begin{bmatrix} \left(\frac{1}{\gamma}\right) \rho u \\ \left(\frac{1}{\gamma}\right) \rho u^2 + p \\ (e + p)u - \frac{1}{2} \left(\frac{\gamma-1}{\gamma}\right) \rho u^3 \end{bmatrix}$$

$$\begin{aligned}\mathcal{A}(\mathbf{u}) &= \mathcal{R} \Lambda \mathcal{L} \\ &= \mathcal{R} \Lambda_S \mathcal{L} + \mathcal{R} \Lambda_F \mathcal{L} \\ &= \mathcal{A}_S(\mathbf{u}) + \mathcal{A}_F(\mathbf{u})\end{aligned}$$

$$\Lambda_S = \begin{bmatrix} u & & \\ & 0 & \\ & & 0 \end{bmatrix}$$

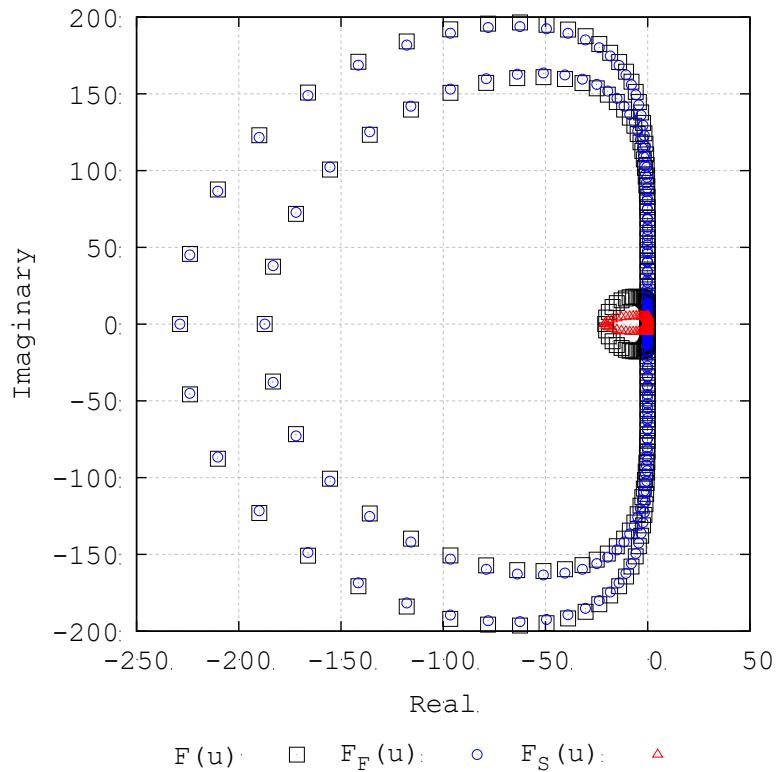
$$\Lambda_F = \begin{bmatrix} 0 & & \\ & u + a & \\ & & u - a \end{bmatrix}$$

# Characteristic-based Flux Partitioning (3)

**Example:** Periodic density sine wave on a unit domain discretized by  $N=80$  points (CRWENO5).

$$\frac{\partial \mathbf{F}_{S,F}(\mathbf{u})}{\partial \mathbf{u}} \neq [\mathcal{A}_{S,F}]$$

Small difference between the eigenvalues of the complete operator and the split operator.  
**(Not an error)**



$$\text{eig} \left[ \frac{\partial \hat{\mathbf{F}}_S}{\partial \mathbf{u}} \right] \approx u \times \text{eig} [\mathcal{D}] \quad \text{eig} \left[ \frac{\partial \hat{\mathbf{F}}_F}{\partial \mathbf{u}} \right] \approx \{u \pm a\} \times \text{eig} [\mathcal{D}]$$

# IMEX Time Integration with Characteristic-based Flux Partitioning (1)

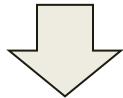
Apply **Additive Runge-Kutta (ARK)** time-integrators to the split form

**Stage values**  
( $s$  stages)

$$\mathbf{U}^{(i)} = \mathbf{u}_n + \Delta t \sum_{j=1}^{i-1} a_{ij} \hat{\mathbf{F}}_S (\mathbf{U}^{(j)}) + \Delta t \sum_{j=1}^i \tilde{a}_{ij} \hat{\mathbf{F}}_F (\mathbf{U}^{(j)})$$
$$i = 1, \dots, s$$

**Step completion**

$$\mathbf{u}_{n+1} = \mathbf{u}_n + \Delta t \sum_{i=1}^s b_i \hat{\mathbf{F}}_S (\mathbf{U}^{(i)}) + \Delta t \sum_{i=1}^s \tilde{b}_i \hat{\mathbf{F}}_F (\mathbf{U}^{(i)})$$



**Non-linear system of equations**

$$\hat{\mathbf{F}}_F (\mathbf{u}) = [\mathcal{D}(\omega) \otimes \mathcal{A}_F (\mathbf{u})] \mathbf{u}$$

**Solution-dependent** weights for  
the WENO5/CRWENO5 scheme

$$\omega = \omega [\mathbf{F} (\mathbf{u})]$$

**Nonlinear flux**

# Linearization of Flux Partitioning

**Redefine** the splitting as

$$\mathbf{F}_F(\mathbf{u}) = [\mathcal{A}_F(\mathbf{u}_n)] \mathbf{u}$$

$$\mathbf{F}_S(\mathbf{u}) = \mathbf{F}(\mathbf{u}) - \mathbf{F}_F(\mathbf{u})$$

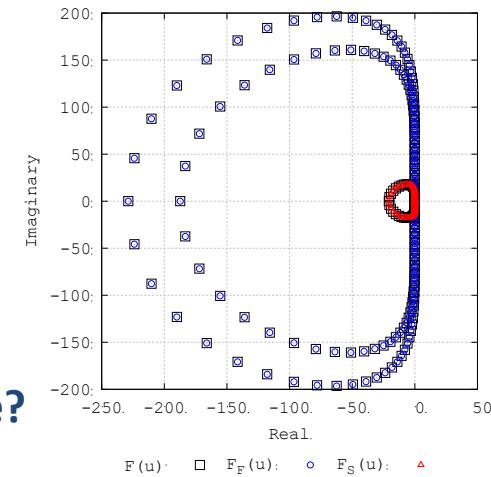
Note: Introduces **no error** in the governing equation.

Is  $\mathbf{F}_F$  a good approximation at each stage?

At the beginning of a time step:-

$$\text{eig} \left[ \frac{\partial \hat{\mathbf{F}}_S}{\partial \mathbf{u}} \right] = u \times \text{eig} [\mathcal{D}]$$

$$\text{eig} \left[ \frac{\partial \hat{\mathbf{F}}_F}{\partial \mathbf{u}} \right] = \{u \pm a\} \times \text{eig} [\mathcal{D}]$$



Linearization of the WENO/CRWENO discretization:

$$\begin{aligned} \omega [\mathbf{F}(\mathbf{u}_n)] &\leftarrow \dots \\ \omega [\mathbf{F}(\mathbf{U}^{(1)})] &\leftarrow \mathbf{U}^{(1)} = \mathbf{u}^n \\ \mathbf{U}^{(2)} &= \mathbf{u}^n + \Delta t \tilde{a}_{21} \hat{\mathbf{F}}_F(\mathbf{U}^{(1)}) + \Delta t \tilde{a}_{22} \hat{\mathbf{F}}_F(\mathbf{U}^{(2)}) \\ &\quad + \Delta t a_{21} \hat{\mathbf{F}}_S(\mathbf{U}^{(1)}) \\ \omega [\mathbf{F}(\mathbf{U}^{(2)})] &\leftarrow \dots \\ \mathbf{u}^{n+1} &= \mathbf{u}^n + \Delta t \tilde{b}_1 \hat{\mathbf{F}}_F(\mathbf{U}^{(1)}) + \Delta t \tilde{b}_2 \hat{\mathbf{F}}_F(\mathbf{U}^{(2)}) \\ &\quad + \Delta t b_1 \hat{\mathbf{F}}_S(\mathbf{U}^{(1)}) + \Delta t b_2 \hat{\mathbf{F}}_S(\mathbf{U}^{(2)}) \end{aligned}$$

Within a stage, the non-linear weights are kept fixed.

**Example:** 2-stage ARK method

# IMEX Time Integration with Characteristic-based Flux Partitioning (2)

Linear system of equations for implicit stages:

$$[\mathcal{I} - \Delta t \tilde{a}_{ii} \mathcal{D} \otimes \mathcal{A}_F(\mathbf{u}_n)] \mathbf{U}^{(i)} = \mathbf{u}_n + \Delta t \sum_{j=1}^{i-1} a_{ij} \hat{\mathbf{F}}_S(\mathbf{U}^{(j)}) + \Delta t [\mathcal{D} \otimes \mathcal{A}_F(\mathbf{u}_n)] \sum_{j=1}^{i-1} \tilde{a}_{ij} \mathbf{U}^{(j)},$$

$$i = 1, \dots, s$$

Preconditioning (Preliminary attempts)

$$\mathcal{P} = [\mathcal{I} - \Delta t \tilde{a}_{ii} \mathcal{D}^{(1)} \otimes \mathcal{A}_F(\mathbf{u}_n)] \approx [\mathcal{I} - \Delta t \tilde{a}_{ii} \mathcal{D} \otimes \mathcal{A}_F(\mathbf{u}_n)]$$



First order upwind discretization

Periodic boundaries ignored



Block n-diagonal matrices

- Block tri-diagonal (1D)
- Block penta-diagonal (2D)
- Block septa-diagonal (3D)

- **Jacobian-free approach:** Linear Jacobian defined as a function describing its action on a vector
- **Preconditioning matrix:** Stored as a sparse matrix

ARK Methods (PETSc)

ARKIMEX 2c

- 2<sup>nd</sup> order accurate
- 3 stage (1 explicit, 2 implicit)
- L-Stable implicit part
- Large real stability of explicit part

ARKIMEX 2e

- 2<sup>nd</sup> order accurate
- 3 stage (1 explicit, 2 implicit)
- L-Stable implicit part

ARKIMEX 3

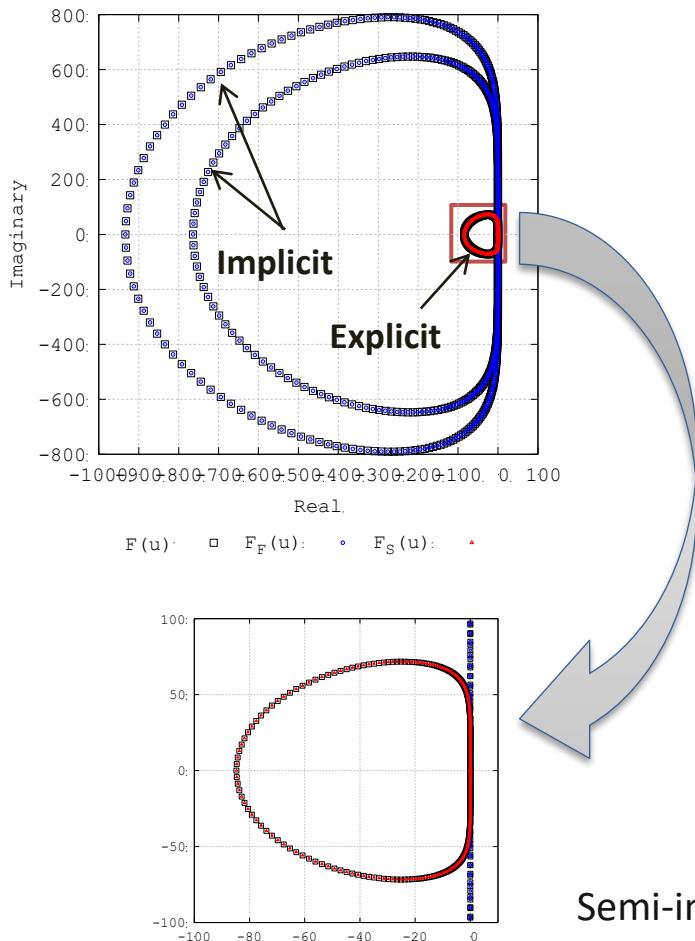
- 3<sup>rd</sup> order accurate
- 4 stage (1 explicit, 3 implicit)
- L-Stable implicit part

ARKIMEX 4

- 4<sup>th</sup> order accurate
- 5 stage (1 explicit, 4 implicit)
- L-Stable implicit part

# Example: 1D Density Wave Advection ( $M_\infty = 0.1$ )

## Eigenvalues



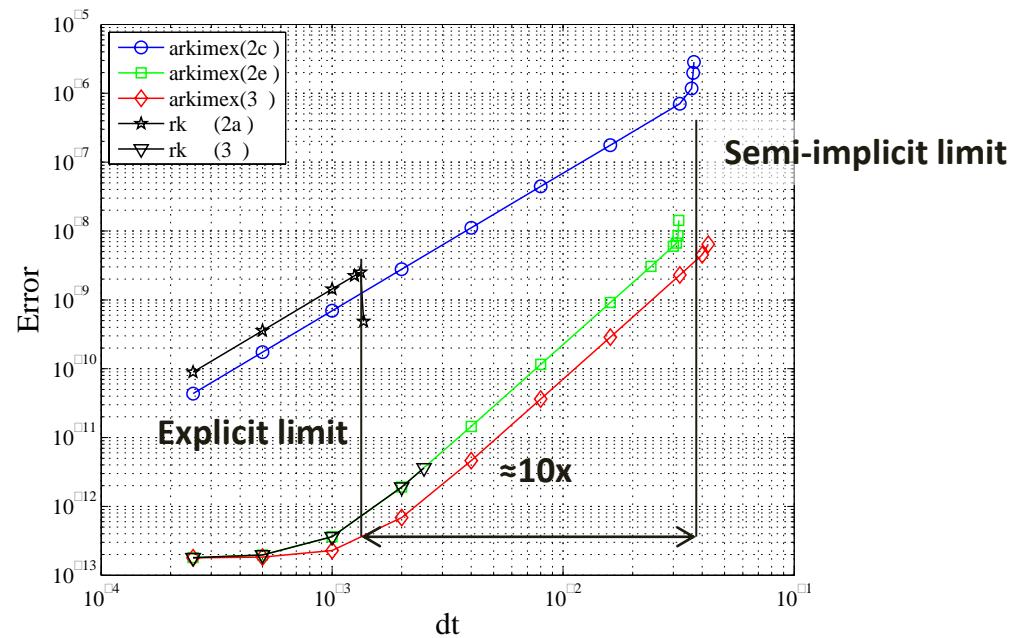
## Initial solution

$$0 \leq x \leq 1$$

$$\rho = \rho_\infty + \hat{\rho} \sin(2\pi x)$$

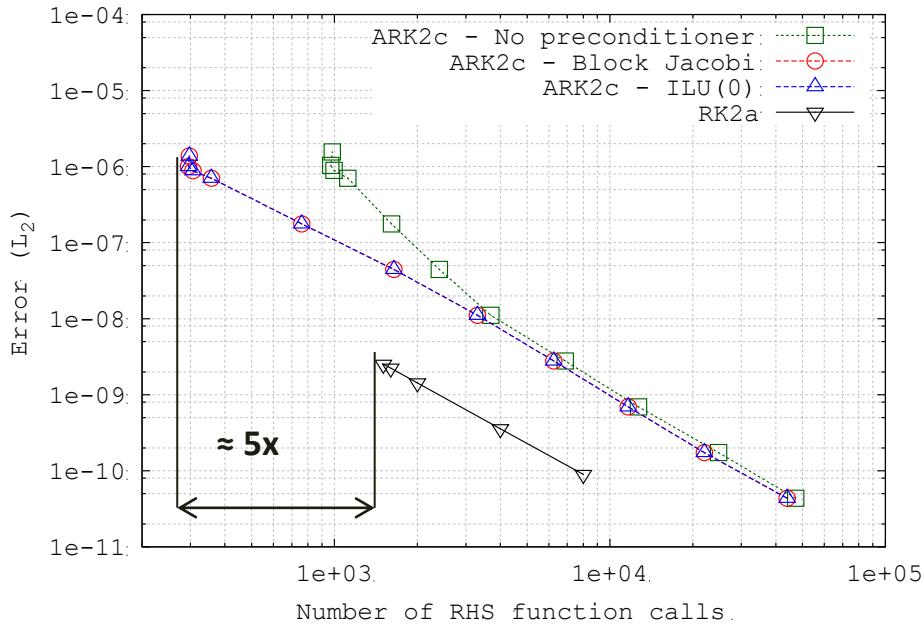
$$u = u_\infty, p = p_\infty$$

CRWENO5, 320 grid points

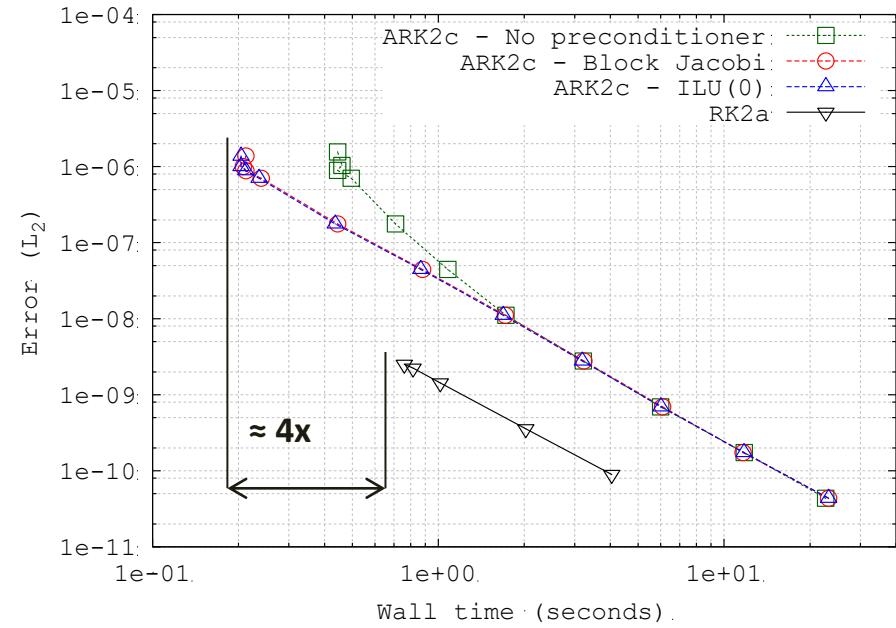


Semi-implicit time step size limit  $1/M_\infty$  than explicit time step size limit

# Example: 1D Density Wave Advection ( $M_\infty = 0.1$ ) Computational Cost



Number of function calls

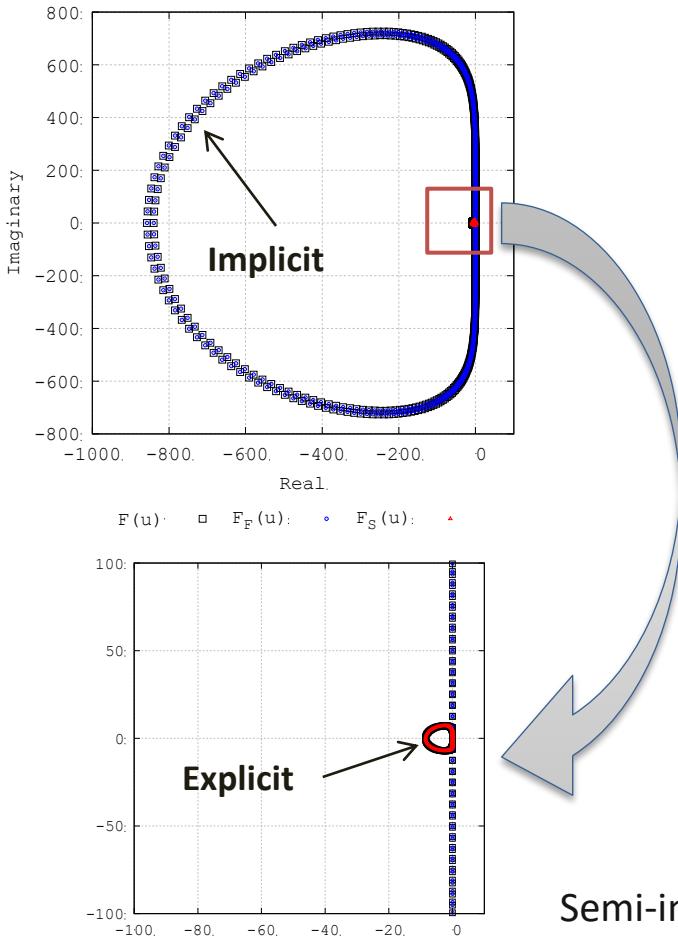


Wall time

**Number of function calls** = (Number of time steps  $\times$  number of stages) + Number of GMRES iterations  
(does not reflect cost of constructing preconditioning matrix and inverting it)

# Example: 1D Density Wave Advection ( $M_\infty = 0.01$ )

## Eigenvalues



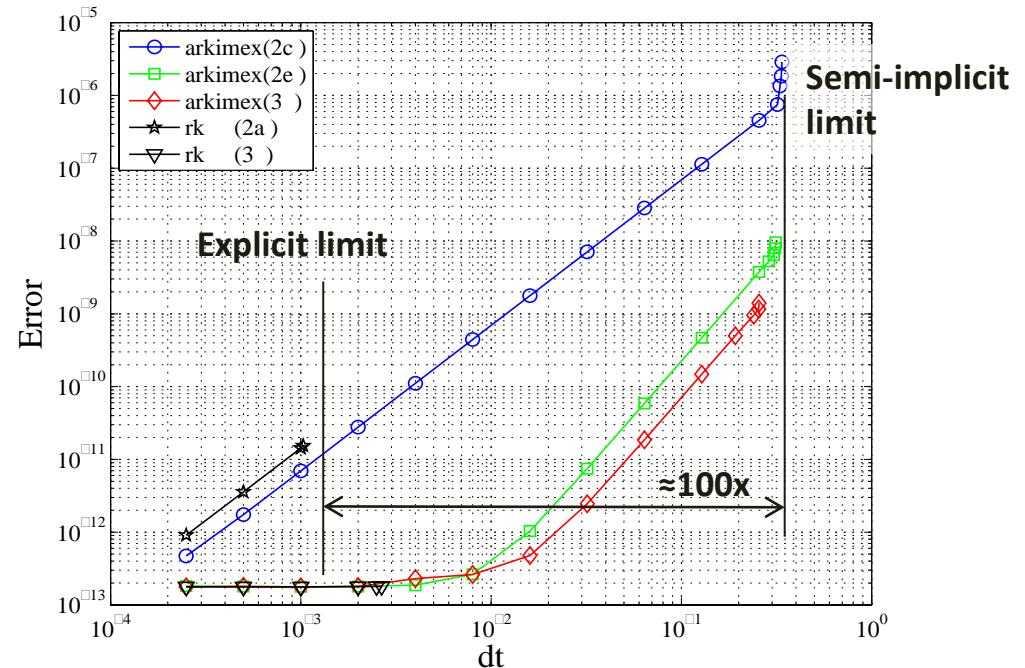
## Initial solution

$$0 \leq x \leq 1$$

$$\rho = \rho_\infty + \hat{\rho} \sin(2\pi x)$$

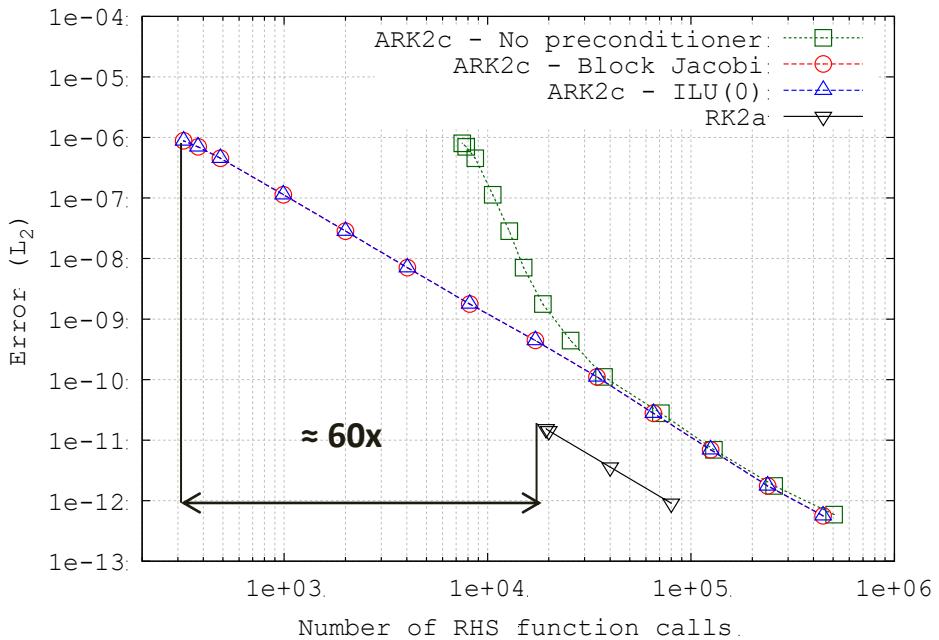
$$u = u_\infty, p = p_\infty$$

CRWENO5, 320 grid points

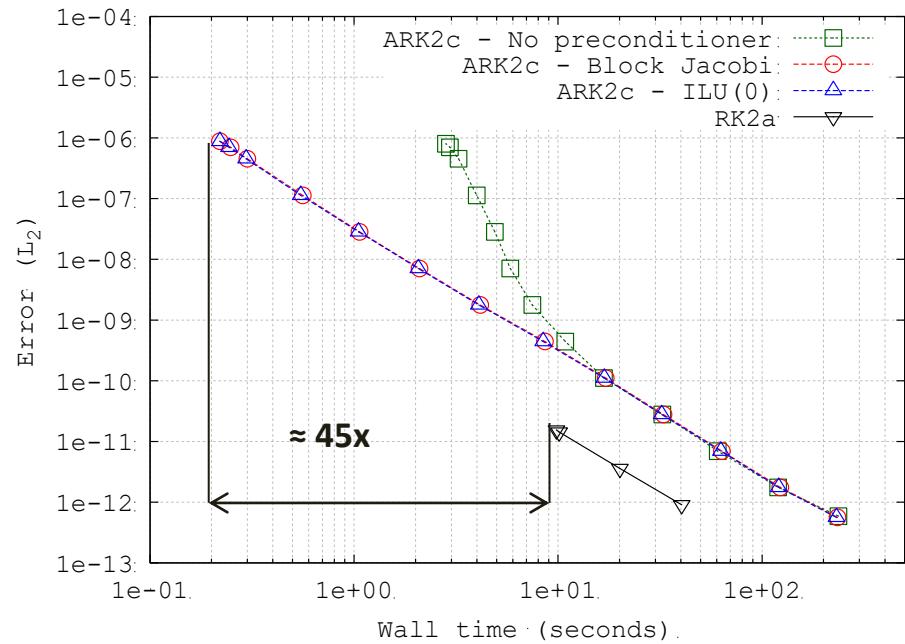


Semi-implicit time step size limit  $1/M_\infty$  than explicit time step size limit

# Example: 1D Density Wave Advection ( $M_\infty = 0.01$ ) Computational Cost



**Number of function calls**



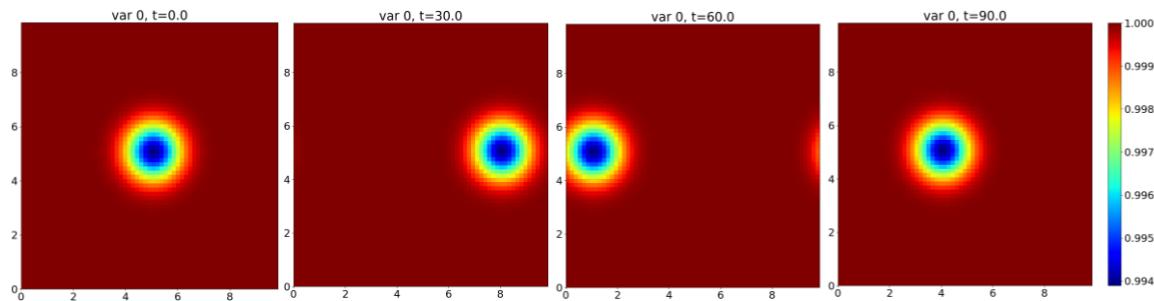
**Wall time**

**Number of function calls** = (Number of time steps  $\times$  number of stages) + Number of GMRES iterations  
(does not reflect cost of constructing preconditioning matrix and inverting it)

# Example: 2D Low Mach Isentropic Vortex Convection

**Freestream flow**

$$\left. \begin{array}{l} \rho_\infty = 1 \\ p_\infty = 1 \\ u_\infty = 0.1 \\ v_\infty = 0 \end{array} \right\} M_\infty \approx 0.08$$



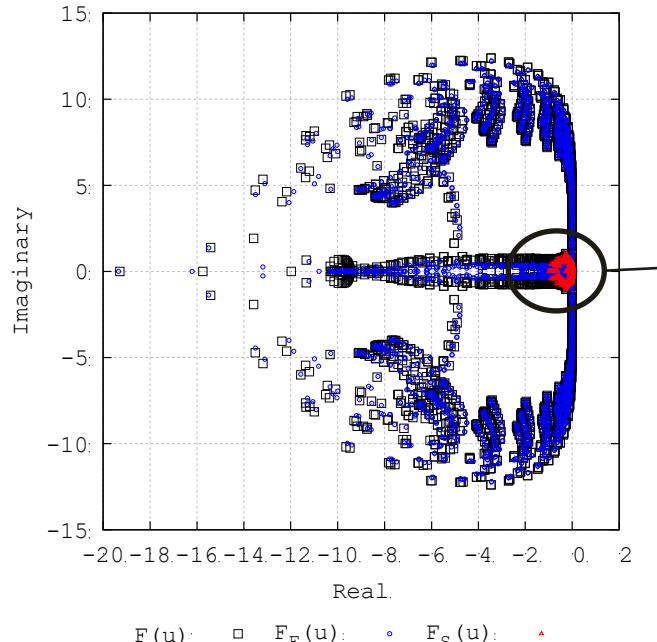
**Vortex (Strength  $b = 0.5$ )**

$$\rho = \left[ 1.0 - \frac{(\gamma - 1) b^2}{8\gamma\pi^2} \exp(1 - r^2) \right]^{\frac{1}{\gamma-1}}$$

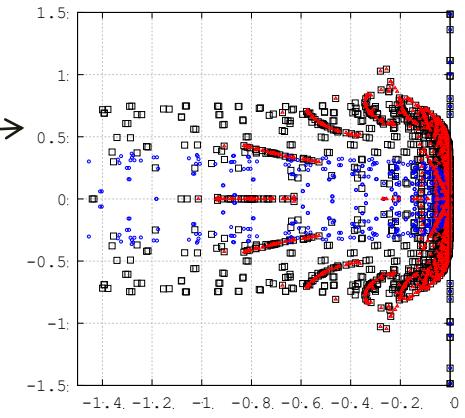
$$p = \left[ 1.0 - \frac{(\gamma - 1) b^2}{8\gamma\pi^2} \exp(1 - r^2) \right]^{\frac{\gamma}{\gamma-1}}$$

$$u = u_\infty - \frac{b}{2\pi} \exp\left(\frac{1 - r^2}{2}\right) (y - y_c)$$

$$v = v_\infty + \frac{b}{2\pi} \exp\left(\frac{1 - r^2}{2}\right) (x - x_c)$$

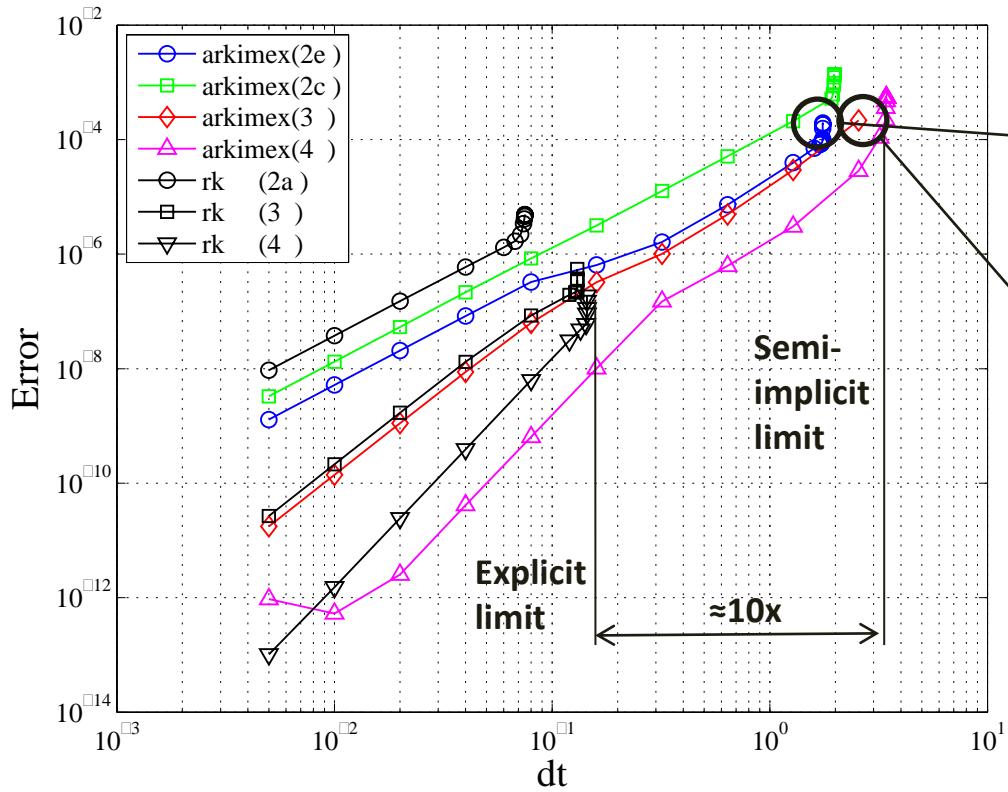


**Eigenvalues of the right-hand-side operators**

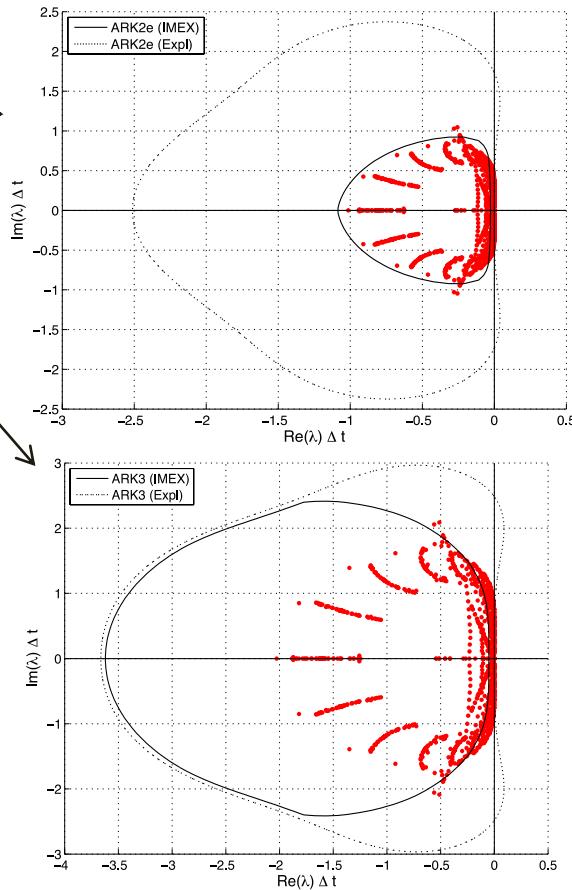


**Grid:  $32^2$  points,  
CRWENO5**

# Example: 2D Low Mach Isentropic Vortex Convection

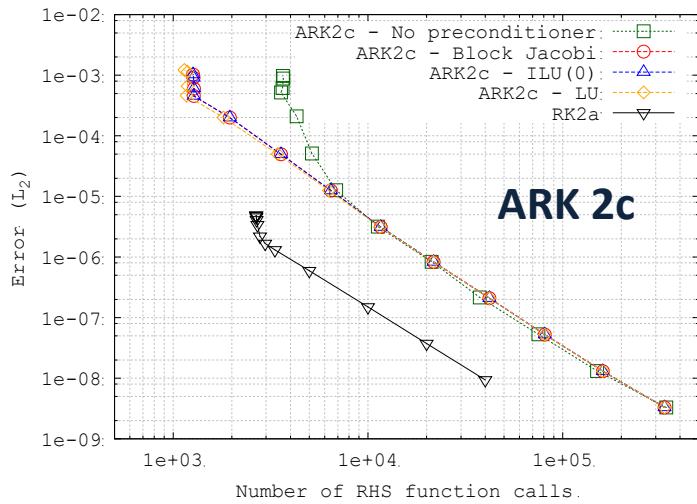


- Optimal orders of convergence observed for all methods
- Time step size limited by the “slow” eigenvalues.

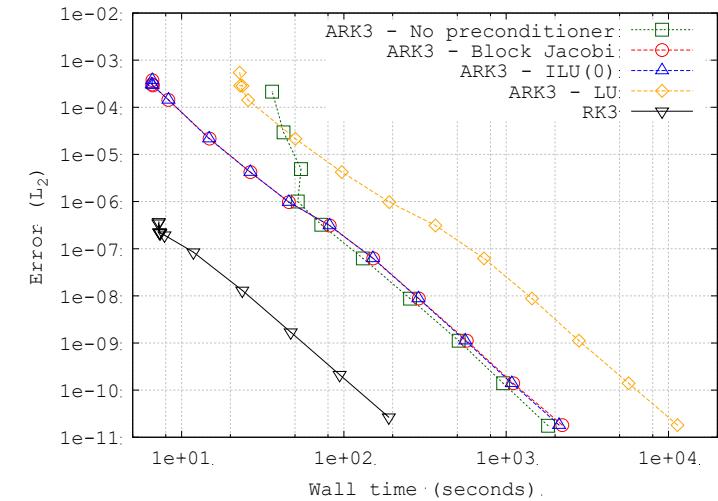
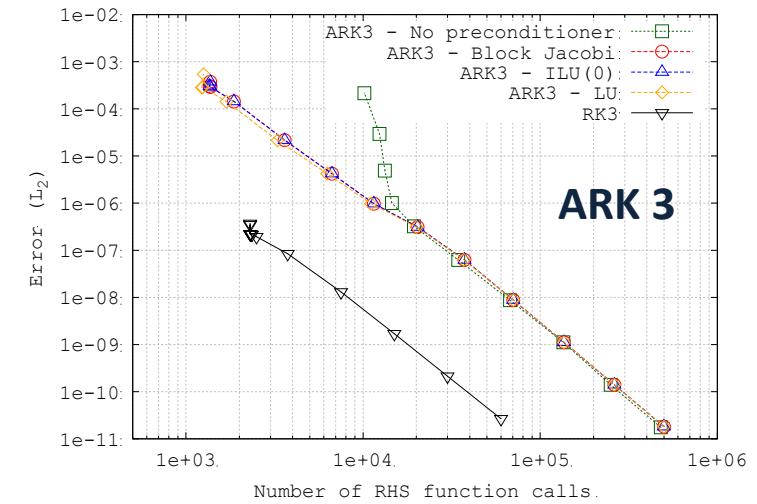
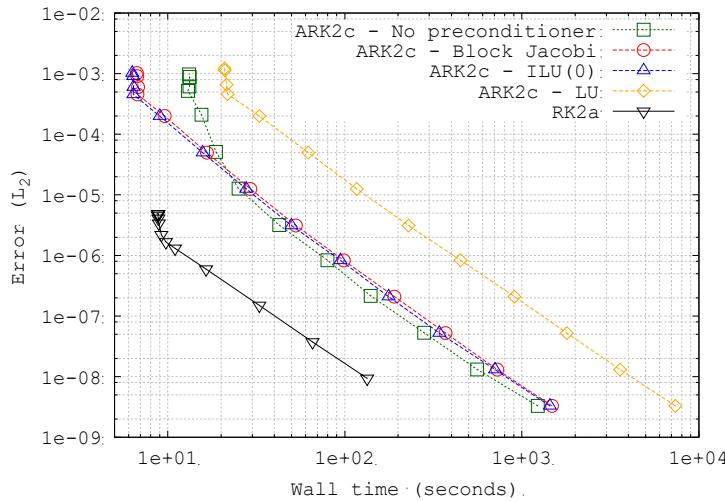


# Example: Vortex Convection (Computational Cost)

Number of function calls

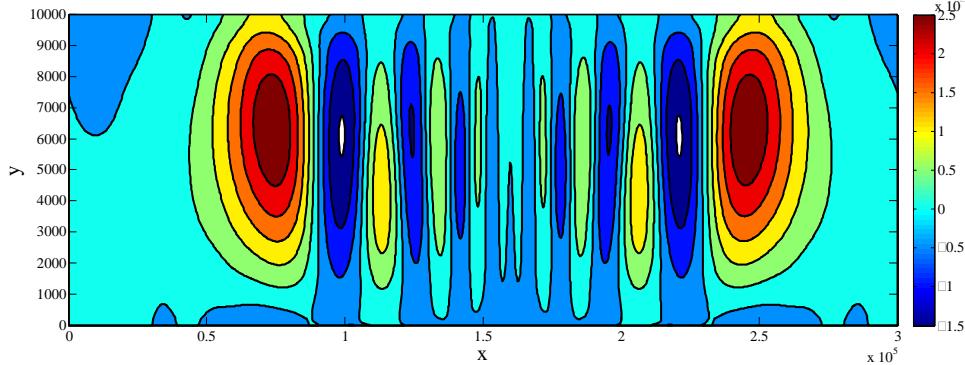


Wall time

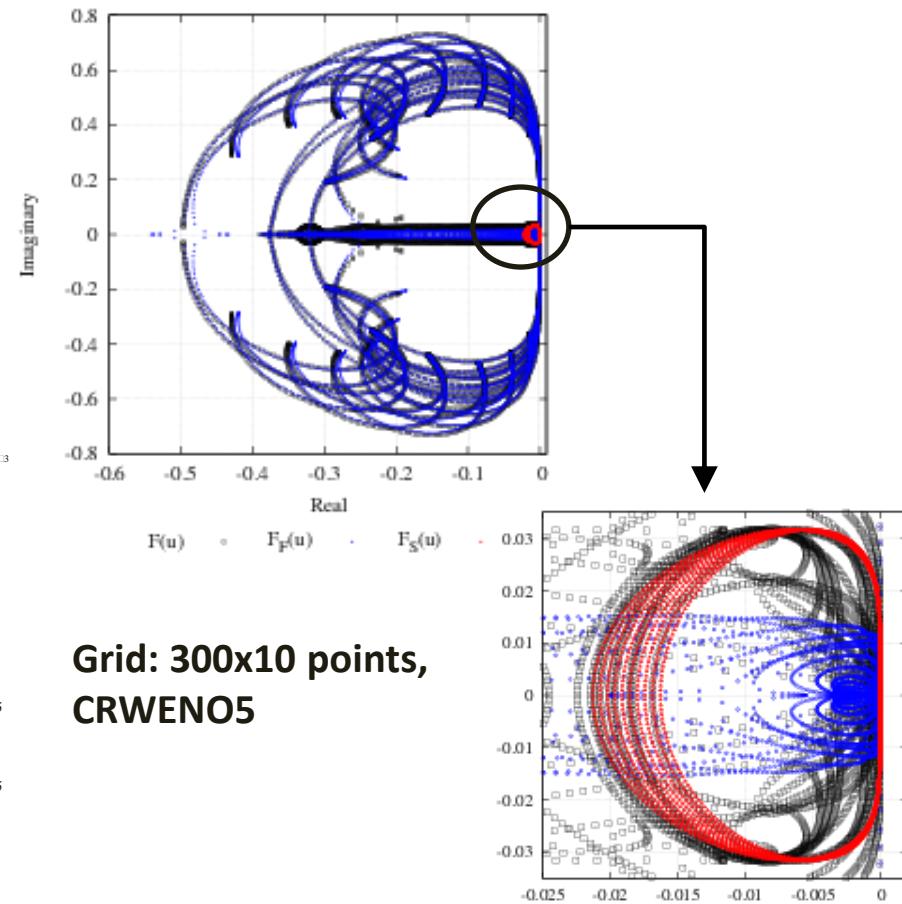


# Example: Inertia – Gravity Wave

- Periodic channel – 300 km x 10 km
- No-flux boundary conditions at top and bottom boundaries
- Mean horizontal velocity of 20 m/s in a uniformly stratified atmosphere ( $M_\infty \approx 0.06$ )
- Initial solution – Potential temperature perturbation

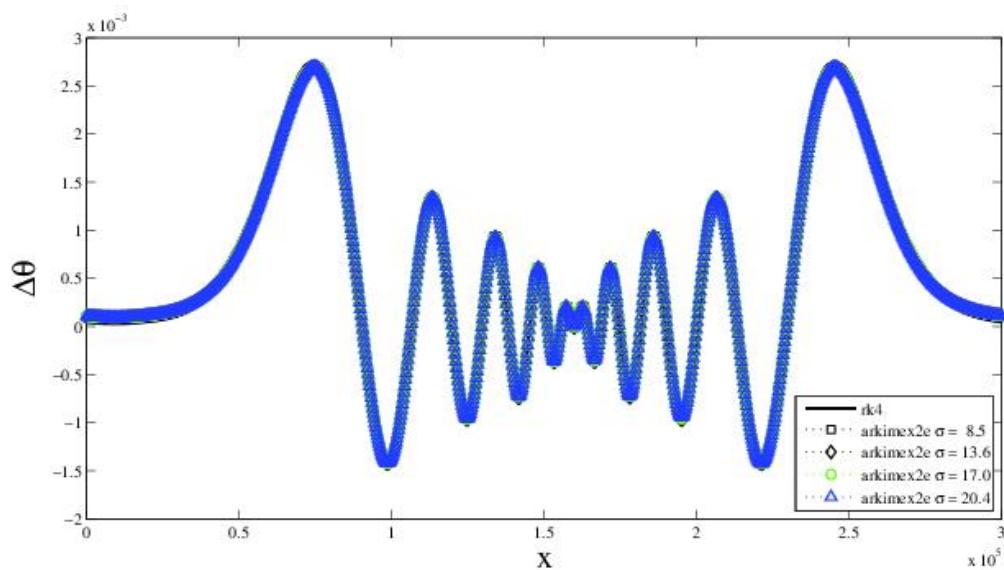


Eigenvalues of the right-hand-side operators



# Example: Inertia – Gravity Wave

CFL	Wall time		Function counts	
	Absolute (s)	Normalized (/RK4)	Absolute	Normalized (/RK4)
8.5	6,149	1.14	24,800	1.03
13.6	4,118	0.76	17,457	0.73
17.0	3,492	0.65	14,820	0.62
<b>20.4</b>	<b>2,934</b>	<b>0.54</b>	<b>12,895</b>	<b>0.54</b>



## Fastest RK4

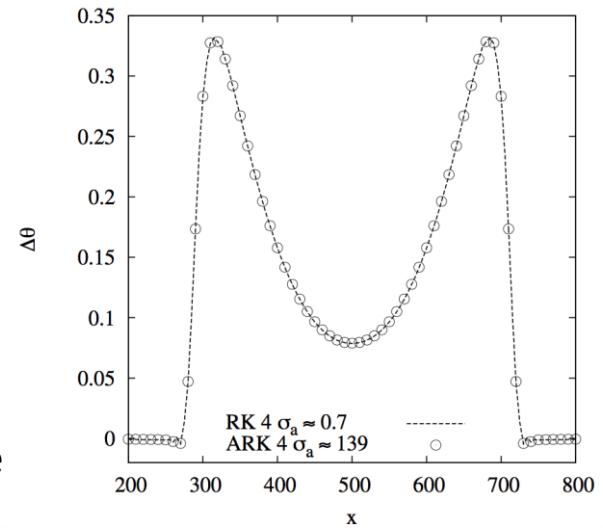
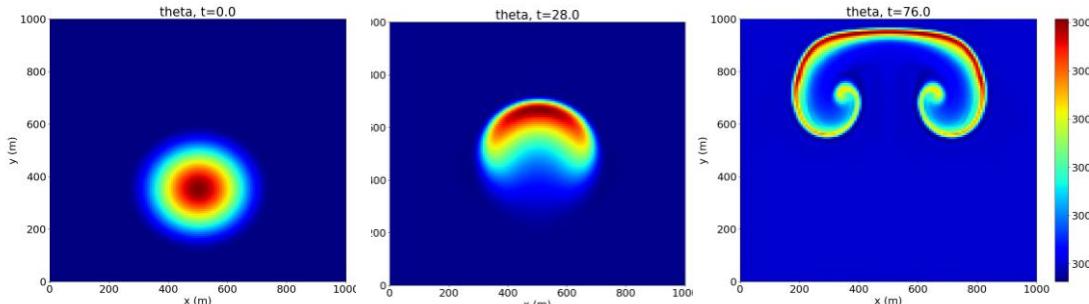
CFL ~ 1.0, Wall time: 5400 s  
# of function calls: 24000

Cross-sectional potential temperature perturbations at 3000 seconds ( $y = 5$  km) at CFL numbers **0.2 – 13.6**

# Example: Rising Thermal Bubble

CFL	Wall time		Function counts	
	Absolute (s)	Normalized (/RK4)	Absolute	Normalized (/RK4)
6.9	73,111	2.42	360,016	2.25
34.7	22,104	0.73	111,824	0.70
<b>138.9</b>	<b>8,569</b>	<b>0.28</b>	<b>45,969</b>	<b>0.29</b>

**Fastest RK4 CFL ~ 0.7, Wall time: 30,154 s, # of function calls: 160,000**



- Box – 1000 m<sup>2</sup>; **No-flux boundary conditions** on all boundaries
- **Warm bubble initially at rest** rises in a still ambient atmosphere

# Summary of Characteristic-Based Flux Partitioning for IMEX Methods

- Partitioning of flux **separates the acoustic and entropy modes**: Allows **larger time step sizes** (determined by flow velocity, not speed of sound).
- **Comparison** to alternatives
  - **Vs. explicit time integration:** Larger time steps → More efficient algorithm
  - **Vs. implicit time integration:** Semi-implicit solves a linear system without any approximations to the overall governing equations (as opposed to solving non-linear system of equations or linearize governing equations in a time step).
- **Disclaimer:** This work is quite old (~7 years); there has been more interesting work since then!

# Multirate Time Integration for Atmospheric Flows

## Background

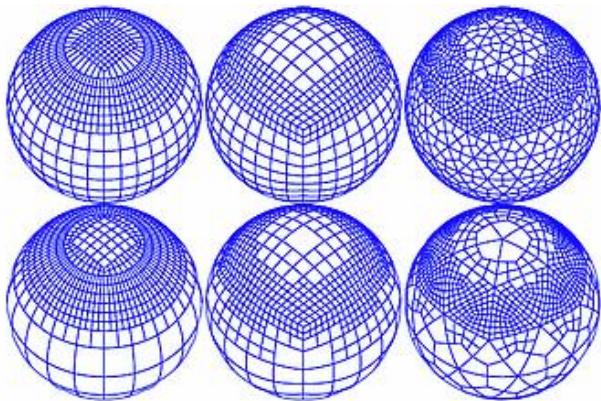
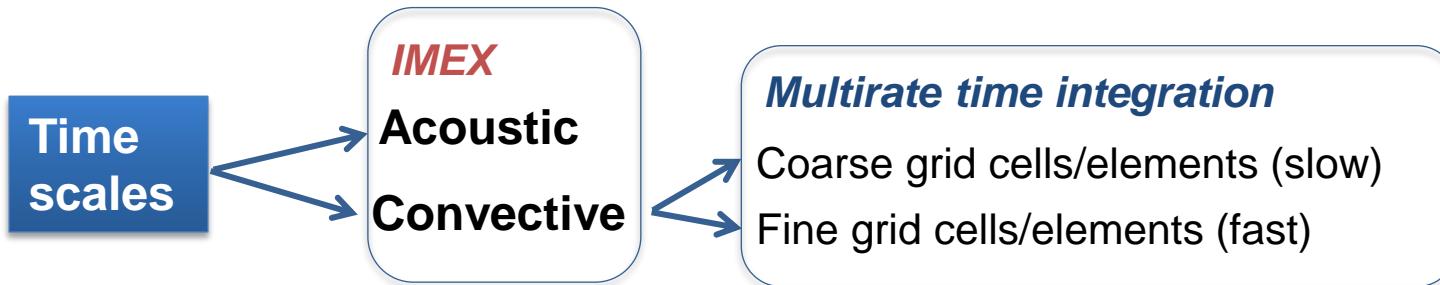


Image source:

<http://frankgiraldo.wixsite.com/mysite/numa>

### NUMA – Nonhydrostatic Unified Model of the Atmosphere

- A scalable *high-order spectral-element code* for solving the Navier-Stokes and shallow water equations on a cube or a sphere (*part of the U.S. Navy NEPTUNE project*)
- **AMR-capable** (p4est/p6est library - <http://p4est.github.io/>)
- **Collaborators:** *Emil Constantinescu (ANL)*, *Frank Giraldo (Naval Post. School)*, *Michal Kopera (UC Santa Cruz)*

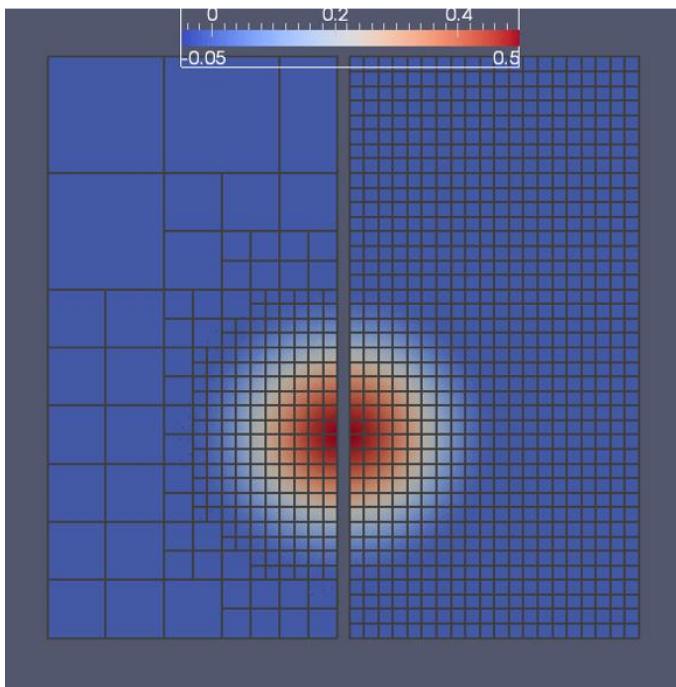


- **Implicit-Explicit (IMEX) Time Integration:** integrate acoustic terms implicitly, convective terms explicitly
- **Multirate Time Integration:** For AMR simulations, integrate refined elements with a “fast” method

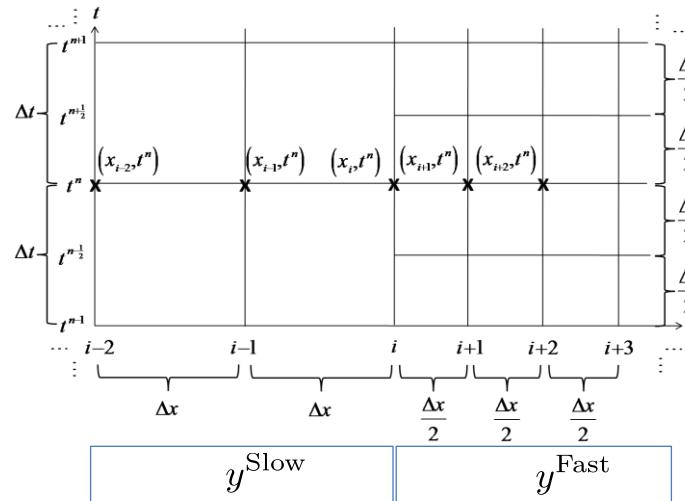
# Multirate Time Integration for Atmospheric Flows

## Adaptive Mesh Refinement (AMR):

Selective refining of the grid based on the solution



**Single-rate time-integrator:** Time step limited by refined elements

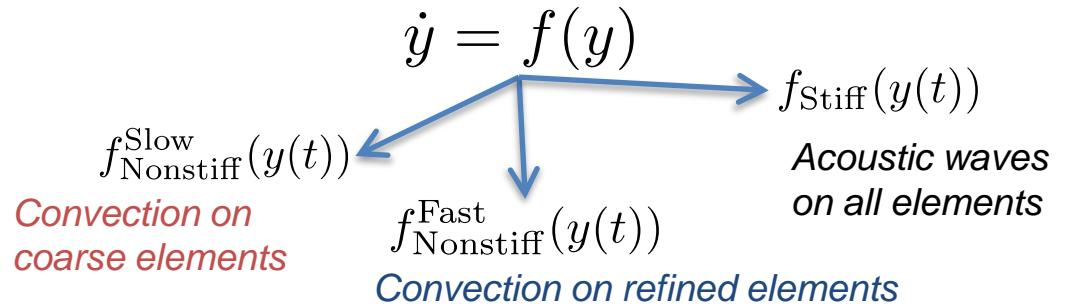


**Multirate** allows each cell to use the time-step suitable with local grid spacing

$$\begin{bmatrix} \dot{y}^{\text{Slow}} \\ \dot{y}^{\text{Fast}} \end{bmatrix} = \begin{bmatrix} f_1(y^{\text{Slow}}, y^{\text{Fast}}) \\ f_2(y^{\text{Slow}}, y^{\text{Fast}}) \end{bmatrix}$$

Illustration by: Emil Constantinescu (ANL)

**Partitioning** of the governing equation



# Extrapolated Methods Overview

Building high-order methods from low-order method

$\mathcal{I}_{\text{LO}}$

**Low-order**

(computationally cheap)  
time integrator,  
for example,  
**forward/backward Euler**

**Extrapolation**

**formula:** build higher  
order solutions

$$T_{j,k+1} = T_{j,k} + \frac{T_{j,k} - T_{j-1,k}}{j/(j-k) - 1}$$

$T_{11} \equiv y^{n+1} (\mathcal{I}_{\text{LO}} [\Delta t])$				
$T_{21} \equiv y^{n+1} \left( \mathcal{I}_{\text{LO}} \left[ \frac{\Delta t}{2} \right] \right)$	$T_{22}$			
$T_{31} \equiv y^{n+1} \left( \mathcal{I}_{\text{LO}} \left[ \frac{\Delta t}{3} \right] \right)$	$T_{32}$	$T_{33}$		
$T_{41} \equiv y^{n+1} \left( \mathcal{I}_{\text{LO}} \left[ \frac{\Delta t}{4} \right] \right)$	$T_{42}$	$T_{43}$	$T_{44}$	$\dots$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\dots$



**High-order solutions:** low  
order + (column index-1)

# Extrapolated Multirate IMEX Methods

## First-order IMEX Multirate Method

$$y_{n+1} = y_n + \int_{t_n}^{t_{n+1}} f_{\text{Nonstiff}}^{\text{Fast}}(y(s)) ds + \int_{t_n}^{t_{n+1}} f_{\text{Nonstiff}}^{\text{Slow}}(y(s)) ds + \int_{t_n}^{t_{n+1}} f_{\text{Stiff}}(y(s)) ds$$

$$\text{EX}_{\text{Nonstiff}}^{\text{Slow}} := \begin{pmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{pmatrix}$$

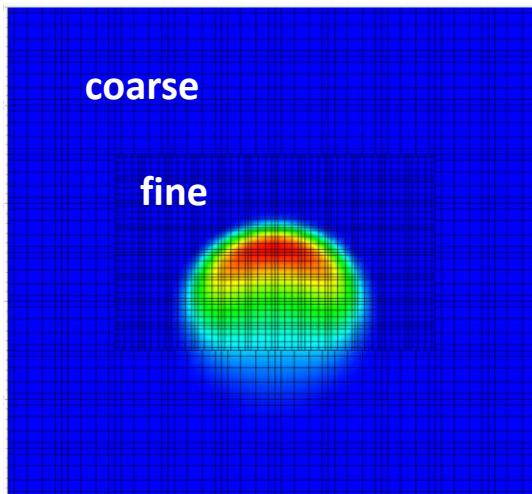
Forward Euler

$$\text{EX}_{\text{Nonstiff}}^{\text{Fast}} := \begin{pmatrix} 0 & 0 \\ \frac{1}{2} & \frac{1}{2} \\ 0 & 1 \end{pmatrix}$$

Two steps of forward Euler  
disguised as multistage RK

$$\text{IM}_{\text{Stiff}} := \begin{pmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{pmatrix}$$

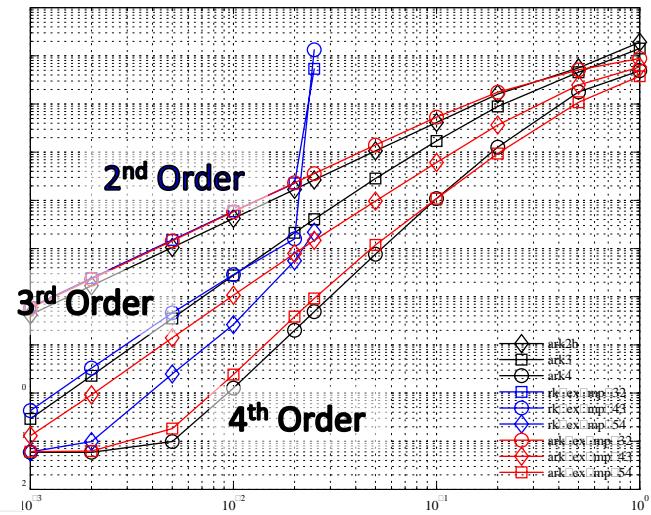
Backward Euler



Extended to higher-orders  
using **extrapolation**

Refinement  
levels: 0,1,2

Single-rate-IMEX  
Multirate explicit  
Multirate IMEX



**Thank you.  
Questions?**



# Balanced, Conservative Finite-Difference Formulation (1)

**Governing Equations** for 2D flows  
(gravity acting along  $-y$  axis)

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{F}(\mathbf{u})}{\partial x} + \frac{\partial \mathbf{G}(\mathbf{u})}{\partial y} = \mathbf{s}(\mathbf{u})$$

$$\mathbf{u} = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ e \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho u v \\ (e + p)u \end{bmatrix}, \quad \mathbf{G} = \begin{bmatrix} \rho v \\ \rho u v \\ \rho v^2 + p \\ (e + p)v \end{bmatrix}, \quad \mathbf{s} = \begin{bmatrix} 0 \\ 0 \\ -\rho g \\ -\rho v g \end{bmatrix}$$

**Hydrostatically balanced equilibrium**  
Pressure gradient balanced by gravitational source

$$u = \text{constant}, v = 0, \quad \rho = \rho_0 \varrho(y), \quad p = p_0 \varphi(y)$$

$$\frac{dp}{dy} = -\rho g$$

Flow variables at reference altitude

$$RT_0 [\varrho(y)]^{-1} \varphi'(y) = -g$$

# Balanced, Conservative Finite-Difference Formulation (2)

**Extension of Xing & Shu's method (*J. Sci. Comput.*, 2013)**

$$\varrho(y) = \exp\left(-\frac{gy}{RT}\right)$$
$$\varphi(y) = \exp\left(-\frac{gy}{RT}\right)$$

**Isothermal equilibrium**

$$\varrho(y) = \left[1 - \frac{(\gamma - 1)gy}{\gamma R\theta}\right]^{1/(\gamma-1)}$$
$$\varphi(y) = \left[1 - \frac{(\gamma - 1)gy}{\gamma R\theta}\right]^{\gamma/(\gamma-1)}$$

**Constant potential temperature**  
(Rising thermal bubble)

$$\varrho(y) = \exp\left(-\frac{\mathcal{N}^2}{g}y\right) \left[1 + \frac{(\gamma - 1)g^2}{\gamma RT_0\mathcal{N}^2} \left\{ \exp\left(-\frac{\mathcal{N}^2}{g}y\right) - 1 \right\}\right]^{1/(\gamma-1)}$$
$$\varphi(y) = \left[1 + \frac{(\gamma - 1)g^2}{\gamma RT_0\mathcal{N}^2} \left\{ \exp\left(-\frac{\mathcal{N}^2}{g}y\right) - 1 \right\}\right]^{\gamma/(\gamma-1)}$$

**Stratified atmosphere with a specified Brunt-Väisälä frequency**  
(Inertia-gravity wave)

# Balanced, Conservative Finite-Difference Formulation (3)

**Differential Form**

$$\frac{\partial \mathbf{G}(\mathbf{u})}{\partial y} = \mathbf{s}(\mathbf{u}) \quad \Rightarrow \quad$$

**Discretized Form**

$$\frac{1}{\Delta y} \mathcal{D} [\mathbf{G}(\mathbf{u})]_j = [\mathbf{s}(\mathbf{u})]_j$$

**Well-Balanced Formulation:**

Discretized equilibrium holds  
**not just for**  $\Delta y \rightarrow 0$   
 but for any grid resolution.

**Modified Governing Equations**

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{F}(\mathbf{u})}{\partial x} + \frac{\partial \mathbf{G}(\mathbf{u})}{\partial y} = \mathbf{s}^*(\mathbf{u}, y) \quad \mathbf{s}^* =$$

$$RT_0 [\varrho(y)]^{-1} \varphi'(y) = -g \Rightarrow \mathbf{s}^* \equiv \mathbf{s}$$

$$\begin{bmatrix} 0 \\ 0 \\ \rho RT_0 [\varrho(y)]^{-1} \varphi'(y) \\ \rho v RT_0 [\varrho(y)]^{-1} \varphi'(y) \end{bmatrix}$$

$$\Rightarrow \mathcal{D}_{\mathbf{G}} [p] = \rho RT_0 \{ \varrho(y) \}^{-1} \mathcal{D}_{\mathbf{s}^*} [\varphi(y)]$$

If flux and source discretized  
by **same operator**

$$\mathcal{D}_{\mathbf{G}} = \mathcal{D}_{\mathbf{s}^*} = \mathcal{D}$$

**Finite-Difference Discretization**

$$\left. \frac{\partial \phi}{\partial x} \right|_{x=x_j} \approx \mathcal{D}[\phi] \equiv \sum_{k=-m}^n \sigma_k^{\mathcal{D}} \phi_{j+k}$$

$$\Rightarrow \mathcal{D} \left[ p - \rho RT_0 \{ \varrho(y) \}^{-1} \varphi(y) \right] = \mathcal{D} \left[ p_0 \varphi(y) - \rho_0 \varrho(y) RT_0 \{ \varrho(y) \}^{-1} \varphi(y) \right] = 0$$

# Balanced, Conservative Finite-Difference Formulation (4)

	Flux	Source
<b>Interpolation</b>	$\hat{\mathbf{G}}_{j+1/2}^{L,R} = \mathcal{R}_{\mathbf{G}}^{L,R} [\mathbf{G}] \equiv \sum_{k=-m}^n \hat{\sigma}_k \mathbf{G}_{j+k}$	$\hat{\varphi}_{j+1/2}^{L,R} = \mathcal{R}_{\mathbf{G}}^{L,R} [\varphi] \equiv \sum_{k=-m}^n \hat{\sigma}_k \varphi_{j+k}$
<b>Upwinding (Rusanov)</b>	$\hat{\mathbf{G}}_{j+1/2} = \frac{1}{2} \left[ \hat{\mathbf{G}}_{j+1/2}^L + \hat{\mathbf{G}}_{j+1/2}^R \right] + \frac{1}{2} \max_{j,j+1} \nu_j \left( \hat{\mathbf{u}}_{j+1/2}^L - \hat{\mathbf{u}}_{j+1/2}^R \right)$	$\hat{\varphi}_{j+1/2} = \frac{1}{2} \left[ \hat{\varphi}_{j+1/2}^L + \hat{\varphi}_{j+1/2}^R \right]$
<b>Differencing</b>	$\frac{\partial \mathbf{G}}{\partial y} \Big _{y=y_j} \approx \frac{1}{\Delta y} \left[ \hat{\mathbf{G}}_{j+1/2} - \hat{\mathbf{G}}_{j-1/2} \right]$	$\frac{\partial \varphi}{\partial y} \Big _{y=y_j} \approx \frac{1}{\Delta y} \left[ \hat{\varphi}_{j+1/2} - \hat{\varphi}_{j-1/2} \right]$

$$\mathcal{R}_{\mathbf{G}}^{L,R} [\phi] \equiv \sum_{k=-m}^n \hat{\sigma}_k \phi_{j+k}$$

Represents the **WENO/CRWENO** finite-difference operator with the non-linear weights computed based on **G(u)**

**Diffusion term** in upwinding must vanish for equilibrium solution

$$\hat{\mathbf{G}}_{j+1/2} = \frac{1}{2} \left[ \hat{\mathbf{G}}_{j+1/2}^L + \hat{\mathbf{G}}_{j+1/2}^R \right] + \frac{1}{2} \max_{j,j+1} \nu_j \left( \hat{\mathbf{u}}_{j+1/2}^L - \hat{\mathbf{u}}_{j+1/2}^R \right)$$

$$\mathbf{u}^* = \begin{bmatrix} \rho \{ \varrho(y) \}^{-1} \\ \rho u \{ \varrho(y) \}^{-1} \\ \rho v \{ \varrho(y) \}^{-1} \\ \frac{p \{ \varphi(y) \}^{-1}}{\gamma-1} + \frac{1}{2} \rho \{ \varrho(y) \}^{-1} (u^2 + v^2) \end{bmatrix}$$

Constant at steady state

# Verification of Balanced Formulation

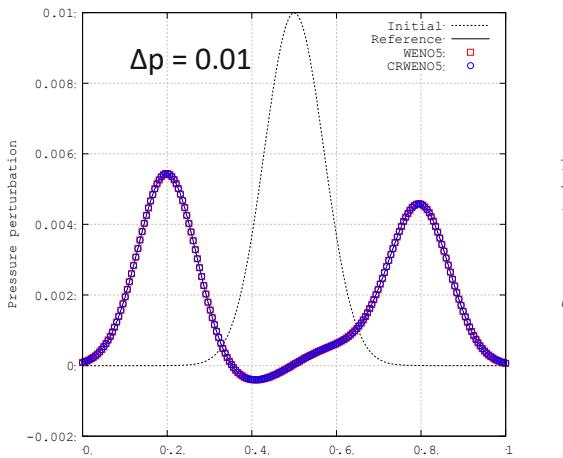
**Case 1:** Isothermal equilibrium

**Case 2:** Stratified atmosphere with constant potential temperature

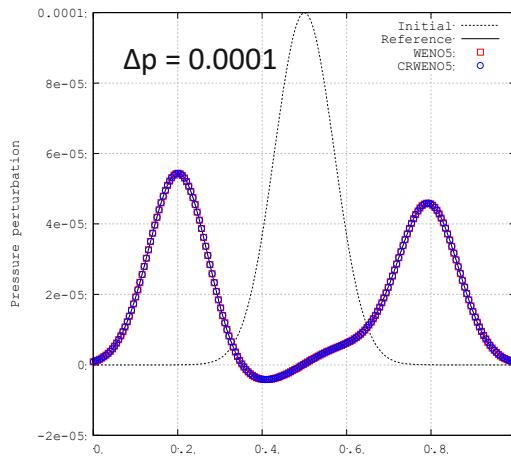
**Case 3:** Stratified atmosphere with specified Brunt-Väisälä frequency

**Difference of the final solution with the initial solution**  
(Verification that hydrostatic balance is preserved to machine precision)

Case	$L_1$	$L_2$	$L_\infty$	$L_1$	$L_2$	$L_\infty$
	WENO5			CRWENO5		
Case 1	2.46E-15	2.89E-15	3.91E-15	2.00E-14	1.71E-14	1.50E-14
Case 2	6.02E-15	7.11E-15	1.31E-14	1.50E-14	1.53E-14	2.09E-14
Case 3	3.63E-15	4.35E-15	8.15E-15	1.58E-14	1.83E-14	6.11E-14



Small perturbation to isothermal hydrostatic balance



- Algorithm is able to **preserve the hydrostatic balance** at any grid resolution and for any duration to machine precision.
- Small perturbations** to the hydrostatic balance are **accurately resolved**.