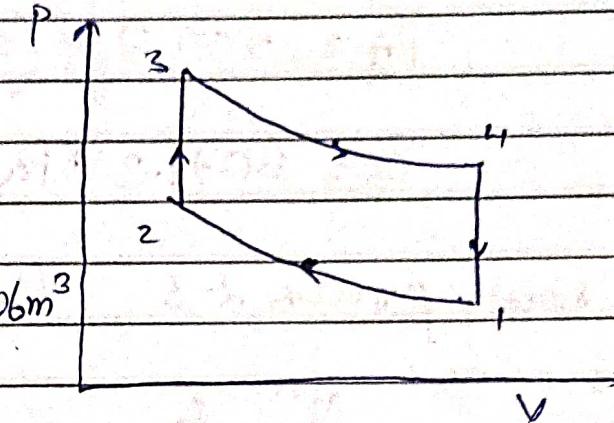


TUTORIAL - 7

Otto cycle

$$r_{eR} = 9.5 = \frac{V_1}{V_2}$$



@ State 1: $P_1 = 100 \text{ kPa}$

$$T_1 = 35^\circ \text{C}$$

$$V_1 = 600 \text{ cm}^3 = 0.0006 \text{ m}^3$$

$$V_2 = \frac{V_1}{9.5}$$

$$T_4 = 800 \text{ K}$$

$$V_2 = 0.63 \times 10^{-4} \text{ m}^3$$

$$m = \frac{P_1 V_1}{RT_1} = \frac{100 \times 6 \times 10^{-4}}{0.287 \times 308}$$

$$V_4 = V_1 \quad V_2 = V_3$$

$$m = 0.678 \times 10^{-3} \text{ kg}$$

The highest temp & Pressure after heat addition i.e. at state 3.

Process 3-4 isentropic

$$TV^{\gamma-1} = K$$

$$\frac{T_3 V_3^{\gamma-1}}{T_3} = \frac{T_4 V_4^{\gamma-1}}{T_4}$$

$$\frac{1}{T_3} = \frac{1}{T_4} (\frac{V_4}{V_3})^{\gamma-1}$$

$$T_3 = \frac{1}{1968.61} = 1968.61 \text{ K} \\ \approx 1969 \text{ K}$$

~~$$T_2 = 100 \text{ K}$$~~

Process 4-1 isochoric

$$\frac{P_1}{T_1} = \frac{P_4}{T_4}$$

$$P_4 = \frac{100}{308} \times 800$$

$$= 259.7 \text{ kPa}$$

$$P_3 V_3^r = P_4 V_4^r$$

$$P_3 = 259.7 \times (9.5)^{7/5}$$

$$P_3 = 6071.3 \text{ kPa}$$

Now process 2-3 isochoric $w=0$

$$\Delta U = \dot{Q}_{in}$$

$$cmC_v(\Delta T) = \dot{Q}_{in}$$

$$0.678 \times 10^{-3} (0.718)(T_3 - T_2) = \dot{Q}_{in}$$

Now process 1-2 isentropic

$$T_1 V_1^{r-1} = T_2 V_2^{r-1}$$

$$T_2 = 308 \times (9.5)^{2/5}$$

$$T_2 = 758 \text{ K}$$

$$\dot{Q}_{in} = 0.678 \times 10^{-3} (0.718) (1969 - 758)$$

$$\dot{Q}_{in} = 0.589 \text{ kJ}$$

$$\eta_{thermal} = 1 - \frac{\dot{Q}_{out}}{\dot{Q}_{in}}$$

$$\dot{Q}_{out} = m_C(T_1 - T_4)$$

$$= 0.678 \times 10^{-3} \times 0.718 \times (308 - 800)$$

$$\dot{Q}_{out} = -0.239 \text{ kJ}$$

$$\eta_{thermal} = 1 - \frac{0.239}{0.589} = 0.589$$

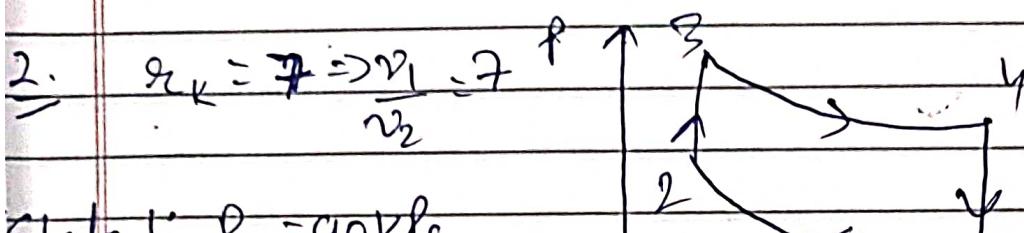
$$= 0.594 \approx 59.4\%$$

Mean effective pressure = $\frac{W_{net}}{V_1 - V_2}$

$$= \frac{|Q_{in}| - |Q_{out}|}{V_1 - V_2}$$

$$= \frac{0.589 - 0.239}{0.0006 - 0.000063} = \frac{0.35 \times 10^4}{5.37}$$

$$= 651.7 \text{ kPa}$$



Otto
cycle

State 1: $P_1 = 90 \text{ kPa}$

$$T_1 = 27^\circ\text{C} = 300 \text{ K}$$

$$V_1 = 0.004 \text{ m}^3$$

$$T_3 = 1127^\circ\text{C} = 1400 \text{ K}$$

$$m = \frac{P_1 V_1}{R T_1} = \frac{90 \text{ kPa} \times 0.004 \text{ m}^3}{0.287 \text{ kJ/kg} \times 300 \text{ K}}$$

$$= 4.18 \times 10^{-3} \text{ kg}$$

Now - Process $V_2 = \frac{V_1}{7} = \frac{0.004}{7}$
 $= 0.00057 \text{ m}^3$

$$V_2 = V_3 \quad V_1 = V_4 \quad \Rightarrow \frac{V_1}{V_2} = \frac{V_4}{V_3} = 7$$

Process 1-2 isentropic

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$

$$\therefore T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$$

$$T_2 = 300 (7)^{\frac{1}{\gamma-1}}$$

$$T_2 = 653.3 \text{ K}$$

$$P_2 = 90 \times \left(\frac{7}{8}\right)^{1.4}$$

$$P_2 = 196 \text{ kPa} \quad 1372.08 \text{ kPa}$$

Process 2-3 isochoric

$$P_2 = P_3$$

$$T_2 = T_3$$

$$\Phi P_3 = \frac{1400}{653.3} \times 1372$$

$$= 420 \text{ kPa} \quad 2940.1 \text{ kPa}$$

Process 3-4 isentropic

$$T_3 V_3^{r-1} = T_4 V_4^{r-1}$$

$$T_4 = 1400 \left(\frac{1}{\gamma}\right)^{0.4}$$

$$T_4 = 1400 \left(\frac{1}{7}\right)^{0.4}$$

$$T_4 = 642.8 \text{ K}$$

Process Apply first law in process 2-3

\dot{Q}_{in}

$$\Delta U = \dot{Q}_{in} - W \rightarrow 0 \quad \text{isochoric process}$$

$$m C_v (\Delta T) = \dot{Q}_{in}$$

$$\dot{Q}_{in} = 4.18 \times 10^{-3} (0.718) (1400 - 653.3)$$

$$\dot{Q}_{in} = 2.24 \text{ kJ}$$

Φ First law in process ~~2-3~~ 4-5

$$\dot{Q}_{out} = m C_v (\Delta T) \quad \text{isochoric} \Rightarrow W = 0$$

$$\dot{Q}_{out} = 4.18 \times 10^{-3} (0.718) (300 - 642.8)$$

$$= -1.028 \text{ kJ} \Rightarrow \text{Heat rejected in process}$$

$$W_{net} = |Q_{in}| - |P_{out}| \\ = 2.24 - 1.028$$

$$W_{net} = 1.211 \text{ kJ}$$

$$\eta_{Thermal} = 1 - \frac{P_{out}}{Q_{in}}$$

$$= 1 - \frac{1.028}{2.24}$$

$$= 0.541 \approx 54.1\%$$

$$\text{Mean effective pressure} = \frac{W_{net}}{V_1 - V_2}$$

$$= \frac{1.211}{0.004} = 302.75$$

$$= \frac{1.211}{0.004 - 0.00057} = 343$$

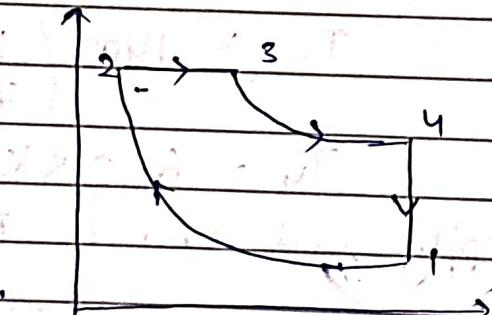
$$= 353$$

$$\Rightarrow \gamma R = 20$$

$$\Rightarrow \frac{V_1}{V_2} = 20$$

$$@ \text{State 1: } P_1 = 95 \text{ kPa}$$

$$T_1 = 20^\circ\text{C} = 293 \text{ K}$$



$$T_3 = 2200 \text{ K}$$

~~$$T_2 = T_1 = 293 \text{ K}$$~~

$$v_4 = v_1 = 20 v_2$$

Process 1-2

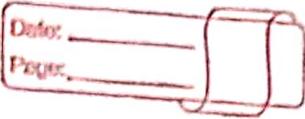
$$\bar{T}_1 V_1^{r-1} = \bar{T}_2 V_2^{r-1}$$

$$\bar{T}_2 = 293 \left(\frac{20}{20} \right) = 293 \text{ K}$$

$$T_2 = 971.1 \text{ K}$$

Process 2-3

$$\frac{V_2}{T_2} = \frac{V_3}{T_3} \quad V_3 = \frac{2200}{971.1} V_2 \Rightarrow$$



$$v_3 = 2.26 v_2$$

Process 3-4: isentropic

$$\bar{T}_3 v_3^{\gamma-1} = \bar{T}_4 v_4^{\gamma-1}$$

$$\bar{T}_4 = \bar{T}_3 \cdot (2.26)^{2/5} \cdot \left(\frac{1}{20}\right)^{2/5}$$

$$T_4 = 919.7 \text{ K}$$

Now first law in process 4-1

$$C_v(\Delta T) = q_{\text{out}}$$

$$0.718 (293 - 919.7) = q_{\text{out}}$$

$$q_{\text{out}} = -480 \text{ kJ/kg}$$

In process 2-3

In open

$$C_p(\Delta T) = q_{\text{in}}$$

$$q_{\text{in}} = 1.005 (2200 - 971.1)$$

$$q_{\text{in}} = 1235 \text{ kJ/kg}$$

$$\eta_{\text{Thermal}} = 1 - \frac{q_{\text{out}}}{q_{\text{in}}}$$

$$= 1 - \frac{480}{1235} = 0.635 = 63.5\%$$

Mean effective pressure

$$v_1 = \frac{RT_1}{P_1} = \frac{0.287 \times 293}{95 \text{ kPa}} = 0.885 \text{ m}^3/\text{kg}$$

$$v_2 = \frac{v_1}{20} \rightarrow v_2 = 0.04425 \text{ m}^3/\text{kg}$$

$$\text{Mean effective pressure} = \frac{\text{Heat input}}{V_1 - V_2}$$

$$= \frac{q_{in} - q_{out}}{V_1 - V_2}$$

$$= 1235 - 450$$

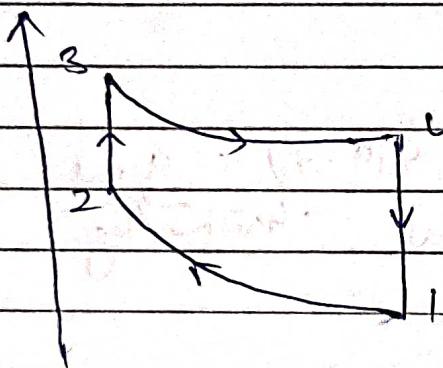
$$0.885 - 0.04425$$

$$: 785 - \frac{933.6 \text{ kPa}}{0.84025}$$

Q. i) Otto cycle

Given $T_3 = 1400 \text{ K}$.

$T_4 = 700 \text{ K}$



State 1: $P_1 = 0.1 \text{ MPa}$

$= 100 \text{ kPa}$

$T_1 = 300 \text{ K}$

Process 1-2 : isentropic $V_3 = V_2$

$V_4 = V_1$

~~$PV^\gamma = K$~~

~~$P_1^{\gamma-1} T_1^\gamma = P_2^{\gamma-1} T_2^\gamma$~~

$$\gamma_K = \frac{V_1}{V_2} = \text{Compress. ratio}$$

Process 3-4 : Isentropic

~~$T_3 V_3^{\gamma-1} = T_4 V_4^{\gamma-1}$~~

$$\frac{T_3}{T_4} = \left(\frac{V_4}{V_3} \right)^{\gamma-1}$$

$$T_3 = \left(\gamma_K \right)^{1/\gamma}$$

T_4

$$(2)^{1/2} \times \gamma_K \Rightarrow \gamma_K = 5.65$$

Maximum pressure @ state 3.

$$\frac{V_1}{V_2} = 5.65$$

Process 1-2 : Isentropic

$$\begin{aligned} P_1 V_1^r &= P_2 V_2^r \\ P_2 &= P_1 (\gamma_k)^{\frac{r}{r-1}} \\ &= 100 (5.65)^{\frac{7}{15}} \\ P_2 &= 1129.45 \text{ kPa} \end{aligned} \quad \begin{aligned} T_1 V_1^{\gamma-1} &= T_2 V_2^{\gamma-1} \\ T_2 &= 300 (\gamma_k)^{\frac{2}{r-1}} \\ &= 300 (5.65)^{\frac{2}{15}} \\ T_2 &= 599.7 \text{ K} \end{aligned}$$

Process 2-3 : Isochoric

$$\frac{P_2}{T_2} = \frac{P_3}{T_3}$$

$$P_3 = \frac{T_3}{T_2} P_2$$

$$= \frac{1400}{599.7} \times 1129.45$$

$$P_3 = 2636.7 \text{ kPa} = 2.63 \text{ MPa}$$

First law in 2-3:

$$C_v (T_3 - T_2) = q_{in}$$

$$0.718 (1400 - 599.7) = q_{in}$$

$$q_{in} = 574.6 \text{ kJ/kg}$$

First law in 4-1:

$$C_v (T_{10} - T_4) = q_{out}$$

$$0.718 (300 - 700) = q_{out}$$

$$q_{out} = -287.2 \text{ kJ/kg}$$

$$\begin{aligned}\eta_{\text{Thermal}} &= \frac{q_{\text{out}}}{q_{\text{in}}} \\ &= 1 - \frac{287.8}{574.6} \\ &= 0.499 \approx 49.9\% \approx 50\%\end{aligned}$$

$$W_{\text{net}} = q_{\text{in}} - q_{\text{out}}$$

$$w_{\text{net}} = 574.6 - 287.8 \text{ KJ/Kg}$$

$$w_{\text{net}} = 287.1 \text{ KJ/Kg}$$

$$\dot{W}_{\text{net}} = \dot{m} w_{\text{net}}$$

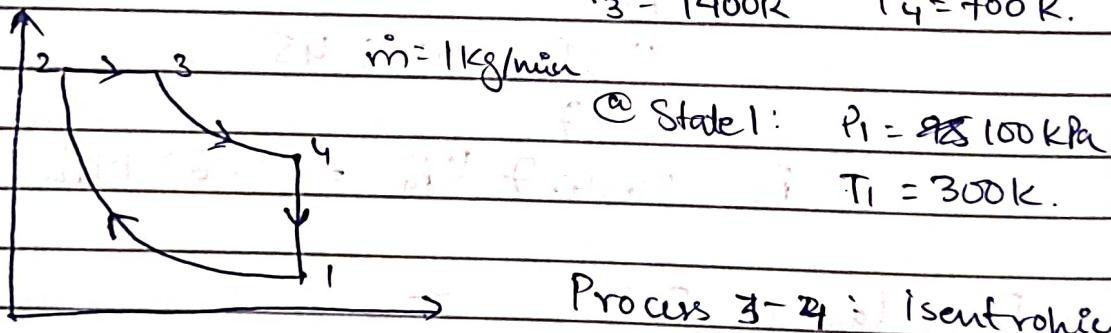
$$= 1 \times 287.1$$

$$\approx 287.1 \text{ KJ}$$

min

ii) Diesel Cycle

$$T_3 = 1400\text{K} \quad T_4 = 700\text{K}$$



Process 2-3: isobaric

$$\frac{V_2}{T_2} = \frac{V_3}{T_3} \quad 2 = \left(\frac{V_4}{V_3}\right)^{2/5}$$

$$V_3 = \frac{T_3}{T_2} V_2$$

$$\frac{T_3 V_3}{T_2} = \frac{T_4 V_4}{V_3}$$

$$5.65 = \frac{V_4}{V_3}$$

$$5.65 = \frac{V_1}{V_3}$$

$$\Rightarrow \frac{V_1 T_2}{T_3 V_2} = 5.65$$

Process

~~Process 1-2: $T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$~~

~~$T_2 = 300 \left(\frac{V_1}{V_2} \right)^{2/5}$~~

$\therefore V_3 = \frac{1400}{300} \left(\frac{V_2}{V_1} \right)^{2/5}, V_2 = 4.67 \frac{V_2}{V_1^{2/5}}$

And $V_1 = 5.65$

~~$\frac{V_1 \cdot V_1^{2/5}}{4.67 V_2^{2/5}} = 5.65$~~

$\left(\frac{V_1}{V_2} \right)^{7/5} = 5.65 \times 4.67$

Process 1-2: isentropic

$T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$

$T_2 = T_1 \left(\frac{V_1}{V_2} \right)^{\gamma-1}$

$$\Rightarrow \frac{V_1}{T_3 V_2} \cdot T_1 \left(\frac{V_1}{V_2} \right)^{\gamma-1} = 5.65$$

$$\frac{300}{1400} \left(\frac{V_1}{V_2} \right)^{7/5} = 5.65$$

$$\therefore r_k = 10.35$$

$$\therefore T_2 = 300 (r_k)^{2/5}$$

$$T_2 = 300 (10.35)^{2/5}$$

$$T_2 = 764 \text{ K}$$

$$\text{Process 1-2: } P_1 T_1 = P_2^{1-\gamma} T_2^\gamma$$

$$\Rightarrow \left(\frac{P_2}{P_1}\right)^{1-\gamma} = \left(\frac{T_1}{T_2}\right)^\gamma$$

$$\left(\frac{P_2}{P_1}\right)^{-2/5} = \left(\frac{300}{764}\right)^{2/5}$$

$$\frac{P_2}{100} \approx \left(\frac{300}{764}\right)^{-2/5}$$

$$P_2 = 100 \times 26.357$$

$$P_2 = 2635.7 \text{ kPa} \rightarrow$$

Highest pressure

$$\text{First law 2-3: } q_{in} = C_p(T_3 - T_2)$$

$$q_{in} = 1.005 (1400 - 764)$$

$$q_{in} = 639.18 \text{ kJ/kg}$$

$$\text{First law 4-1: } q_{out} = C_v(T_1 - T_4)$$

$$q_{out} = 0.718(300 - 764)$$

$$q_{out} = -287.2 \text{ kJ/kg}$$

$$\eta_{\text{Thermal}} = 1 - \frac{q_{out}}{q_{in}}$$

$$= 1 - 0.449 = 0.8509 \approx 55.09\%$$

$$w_{net} = |q_{in}| - |q_{out}| = 639.18 - 287.2 = 351.98$$

$$\dot{W} = \dot{m} w_{net}$$

$$= 1 \times 351.98 \text{ kJ/min}$$

$$= 351.98 \text{ kJ/min}$$

5. Diesel cycle $r_{ek} = 16 \Rightarrow \frac{v_1}{v_2} = 16$

~~in beginning of
isentropic compression~~

State 2

Given

① State 2: $T_2 = 15^\circ\text{C} = 288\text{K}$

$$P_2 = 100 \text{ kPa}$$

② State 3: $T_3 = 1480^\circ\text{C} = 1753\text{K}$

Process 2-3: isobaric

$$\frac{P_2}{T_2} = \frac{P_3}{T_3}$$

$$\frac{T_3}{T_2} = \frac{P_3}{P_2}$$

$$\frac{T_3}{T_2} = \frac{P_3}{P_2} \Rightarrow r_e = \frac{1753}{288}$$

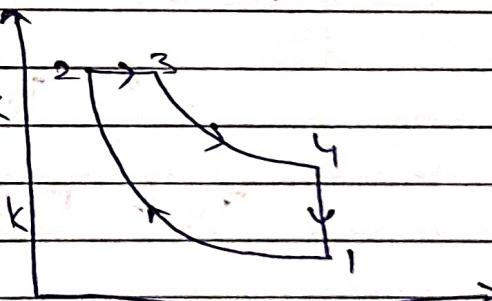
$$r_e = 6.086$$

5. diesel engine: $r_{ek} = 16 \Rightarrow \frac{v_1}{v_2} = 16$

Given ① State 1: $P_1 = 100 \text{ kPa}$

$$T_1 = 15^\circ\text{C} = 288\text{K}$$

② State 3: $T_3 = 1480^\circ\text{C} = 1753\text{K}$



Process 1-2: Isentropic

$$T_1 v_1^{Y-1} = T_2 v_2^{Y-1}$$

$$T_2 = 288 \cdot (16)^{\frac{2}{15}}$$

$$T_2 = 873\text{K}$$

Process 2-3: Isobaric

$$\begin{aligned} \frac{V_B}{V_2} &= \frac{T_3}{T_2} \\ \frac{V_3}{V_2} &= \frac{1753}{873} \approx 2.01 \\ V_3 &= 2.01 V_2 \end{aligned}$$

$$n_c = 2.01$$

Heat is supplied in process 2-3: q_{in} kJ/kg

$$\begin{aligned} q_{in} &= c_p(T_3 - T_2) \\ &= 1.005(1753 - 873) \\ &\approx 884.8 \text{ kJ/kg} \end{aligned}$$

Process 3-4: Isentropic

$$\theta T_3 V_3^{\gamma-1} = T_4 V_4^{\gamma-1}$$

$$T_4 = T_3 \left(\frac{V_3}{V_4} \right)^{\gamma-1}$$

$$T_3 \left(\frac{V_3}{16V_2} \right)^{\gamma-1}$$

$$T_4 = 1753 \left(\frac{2.01}{16} \right)^{2/5}$$

$$T_4 = 264.5 \text{ K}$$

Now heat rejected in process 4-1 :

$$q_{out} = c_v(T_1 - T_4)$$

$$q_{out} = 0.718(288 - 264.5)$$

$$q_{out} = -342.12 \text{ kJ/kg}$$

$$\eta_{\text{Thermal}} = 1 - \frac{q_{\text{out}}}{q_{\text{in}}}$$

$$= 1 - \frac{342.12}{884.8}$$

$$= 0.613$$

$$\eta_{\text{Thermal}} = 61.3\%$$

Q6 Process 1-2: isentropic

$$P_1^{1-r} T_1^r = P_2^{1-r} T_2^r$$

$$\left(\frac{P_1}{P_2}\right)^{\frac{1}{r}} = \left(\frac{873}{288}\right)^{\frac{1}{r}}$$

$$\frac{P_1}{P_2} = 0.0206$$

$$w_{\text{net}} = q_{\text{in}} - q_{\text{out}}$$

$$= 884.8 - 342.12$$

$$= 542.68 \text{ kJ/kg}$$

$$P_2 = \frac{100}{0.0206}$$

$$P_2 = 4854.3 \text{ kPa}$$

$$v_1 = \frac{RT_1}{P_1}$$

$$= \frac{0.287 \times 288}{100}$$

$$= 0.826 \text{ m}^3$$

$$v_2 = R T_2$$

$$P_2$$

$$= 0.287 \times 873$$

$$4854.3$$

$$= 0.05 \text{ m}^3$$

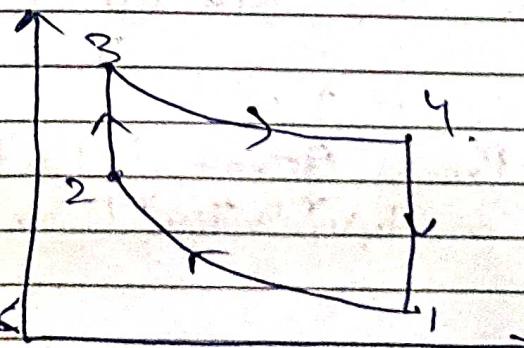
Mean effective pressure = $\frac{w_{\text{net}}}{v_1 - v_2}$

$$= \frac{542.68 \text{ kJ/kg}}{0.826 - 0.05}$$

$$= 699.3 \text{ kPa}$$

Q7 Let's calculate for 1 cylinder first

otto cycle



@ State 1: $P_1 = 96.5 \text{ kPa}$

$T_1 = 41^\circ\text{C} = 314 \text{ K}$

$T_3 = 1315^\circ\text{C} = 1588 \text{ K}$

@ State 3: $T_3 = 1315^\circ\text{C} = 1588 \text{ K}$

Given ~~$V_2 = 9.8\% \text{ of } V_1$~~ $V_2 = 9.8\% \text{ of } V_1$

$$\Rightarrow V_2 = 0.098 V_1$$

$$\frac{V_1}{V_2} = \frac{1000}{98}$$

$$V_1 = 10.2 V_2$$

$$V_2 = 10.2 V_1$$

Also $V_1 - V_2 = \text{stroke} \times \text{Area of cylinder}$

$$= L \times \pi D^2 \quad D \rightarrow \text{bore}$$

Given stroke = 9.91 cm

bore = 8.89 cm

$$V_1 - V_2 = 9.91 \times 3.14 \times 8.89 \times 8.89$$

$$V_1 - V_2 = 607.9 \text{ cm}^3$$

$$10.2 V_2 - V_2 = 607.9 \text{ cm}^3$$

$$9.2 V_2 = 607.9 \text{ cm}^3$$

$$V_2 = 66.07 \text{ cm}^3$$

$$V_1 = 10.2 V_2$$

$$V_1 = 673.9 \text{ cm}^3$$

Process 1-2 : Isentropic

$$T_1 V_1^{Y-1} = T_2 V_2^{Y-1}$$

$$314 \left(10.2\right)^{2/5} = T_2$$

$$T_2 = 795 \text{ K}$$

3-4

Process ~~3-4~~ : Isentropic

$$T_4 V_4^{Y-1} = T_3 V_3^{Y-1} \Rightarrow T_4 = 1588 \times \left(\frac{1}{10.2}\right)^{2/5}$$

$$T_4 = 627.2 \text{ K}$$

$$m = \frac{P_1 V_1}{RT_1} = \frac{96.5 \times 0.673 \times 10^3}{0.287 \times 314}$$

$$m = 0.72 \times 10^3 \text{ kg}$$

Now $\dot{Q}_{in} = m c_v (T_3 - T_2)$ first law in 2-3
 $\dot{Q}_{in} = 0.72 \times 10^3 \times 0.718 (1588 - 395)$
 $\dot{Q}_{in} = 409.9 \text{ J}$

$$\begin{aligned} \dot{Q}_{out} &= m c_v (T_1 - T_4) \quad \text{first law in 4-1} \\ &= 0.72 \times 10^3 \times 0.718 (314 - 627.2) \\ &= -161.9 \text{ J} \end{aligned}$$

$$\begin{aligned} W_{net} &= \dot{Q}_{in} - |\dot{Q}_{out}| \\ &= 409.9 - 161.9 \end{aligned}$$

$W_{net} = 248 \text{ J} \rightarrow$ Work produced by one device

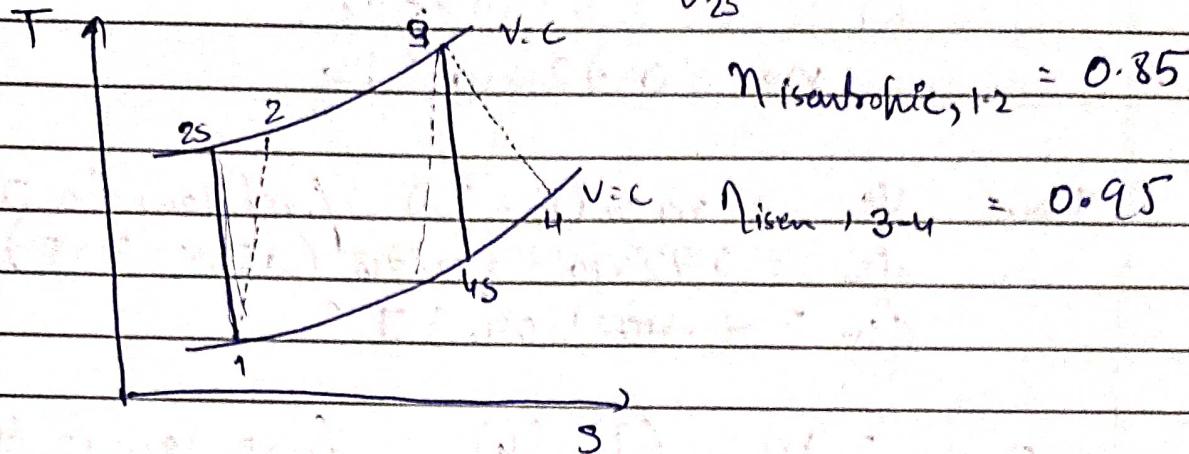
$$\begin{aligned} W_{total} - 6 \times W_{net} &= 1488 \text{ J} \\ &\approx 1.48 \text{ KJ/cycle} \end{aligned}$$

$$\begin{aligned} \text{Given } 2800 \text{ rev} &\\ \text{min} & \frac{2500 \text{ rev}}{60 \text{ s.}} \\ & \cdot 41.67 \text{ rev} \\ & \quad \quad \quad \text{s} \end{aligned}$$

$$\begin{aligned} \text{In a four stroke engine } 2 \text{ rev} &= 1 \text{ cycle} \\ &= \frac{41.67}{2} \text{ cycles} \\ & \quad \quad \quad \text{s} \\ & \approx 20.835 \text{ cycles} \end{aligned}$$

$$\begin{aligned} \text{Power produced} &= W_{total} \times \text{speed} \\ &= \frac{1.48 \text{ KJ}}{\text{cycle}} \times \frac{20.835 \text{ cycle}}{\text{s}} \\ &= 30.83 \text{ kW} \end{aligned}$$

Q. Otto cycle $r_{ik} = 8 \Rightarrow v_1 = v_{25}$



Now processes 1-2 & 3-4 are reversible giving reversible processes 1-2 & 3-4 are actual processes give actual

$$-W_{1-2s} = \cancel{\text{DU}} \quad \varphi = 0 \quad (\text{Adiabatic})$$

$$W_{1-2s} = cv(T_1 - T_{2s})$$

Similarly

$$W_{3-4s} = cv(T_3 - T_{4s}) \quad W_{12} = cv(T_1 - T_2)$$

$$W_{34} = cv(T_3 - T_4)$$

Compression

$$\eta_{1-2s, 1-2} = \frac{W_{12}}{W_{1-2s}} = \frac{cv(T_1 - T_{2s})}{cv(T_1 - T_2)}$$

$$0.85 = \frac{T_1 - T_{2s}}{T_1 - T_2} \rightarrow (1)$$

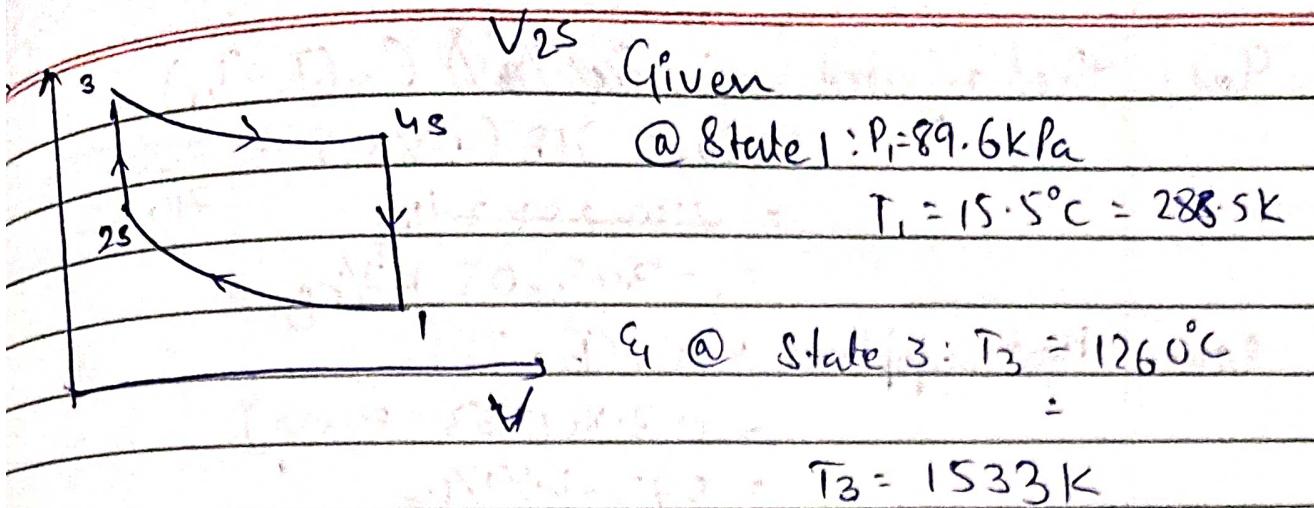
expansion

Similarly

$$\eta_{3-4s, 3-4} = \frac{W_{34}}{W_{3-4s}} \Rightarrow 0.95 = \frac{T_3 - T_{4s}}{T_3 - T_4} \rightarrow (2)$$

Let us assume an ideal Otto cycle to find T_{2s} & T_{4s}

$$w \cdot k \cdot t \quad \frac{V_1}{V_{2s}} = 8$$



Process 1-2s : Isentropic.

$$\bar{T}_1 V_1^{r-1} = \bar{T}_{2s} V_{2s}^{r-1} \quad 2/5$$

$$\bar{T}_{2s} = 288.5 \times 8$$

$$\bar{T}_{2s} = 662.8 \text{ K}$$

Process 3-4s : Isentropic

$$\bar{T}_3 V_3^{r-1} = \bar{T}_{4s} V_{4s}^{r-1}$$

$$V_1 = V_{4s}$$

$$V_3 = V_{2s}$$

$$\bar{T}_{4s} = 1533 \left(\frac{1}{8}\right)^{2/5}$$

$$\bar{T}_{4s} = 667.3 \text{ K}$$

Now Eqn (1)

$$0.85 = \bar{T}_1 - \bar{T}_{2s}$$

$$\bar{T}_1 - \bar{T}_2$$

$$0.85(288.5 - \bar{T}_2) = 288.5 - 662.8 \quad | 0.95(1533 - \bar{T}_4) = (1533 - 667.3)$$

$$\bar{T}_2 = 728.8 \text{ K}$$

$$0.95: \bar{T}_3 - \bar{T}_4$$

$$\bar{T}_3 - \bar{T}_{4s} = 0.95$$

$$\bar{T}_4 = 1533 - 822.2$$

$$\Rightarrow 621.93 \text{ K}$$

$$\bar{T}_4 = 710.585 \text{ K}$$

~~Heat supplied per unit mass = $C_v (T_2 - T_1)$~~

~~$$0.718(728.8 - 288.5)$$~~

~~$$= 316.1 \text{ KJ}$$~~

$$q_{out} = \text{Heat rejected} = \cancel{C_v(T_1 - T_2)} \quad C_v(T_1 - T_4)$$

$$= 0.718(288.5 - 621.23)$$

$$= \frac{239.25 \text{ kJ/kg}}{710.58}$$

$$= -303.05 \text{ kJ/kg}$$

$$q_{in} = \text{Heat supplied} = C_v(T_3 - T_2)$$

$$= 0.718(1533 - 928.8)$$

$$= 577.41 \text{ kJ/kg}$$

$$\eta_{Thom} = 1 - \frac{q_{out}}{q_{in}}$$

$$= 1 - \frac{239.25}{577.41} 303.05$$

$$= \cancel{0.585} \approx 58.5\%$$

$$= 0.475 \approx 47.5\%$$

$$\text{Now } v_1 = \frac{RT_1}{P_1} = \frac{0.287 \times 288.5}{89.6}$$

$$v_1 = 0.924 \cancel{\text{m}^3/\text{kg}}$$

$$v_2 = v_{2s} = \frac{v_1}{8} = 0.115 \text{ m}^3/\text{kg}$$

$$\text{Mean effective pressure} = \frac{|q_{in} - q_{out}|}{v_1 - v_2}$$

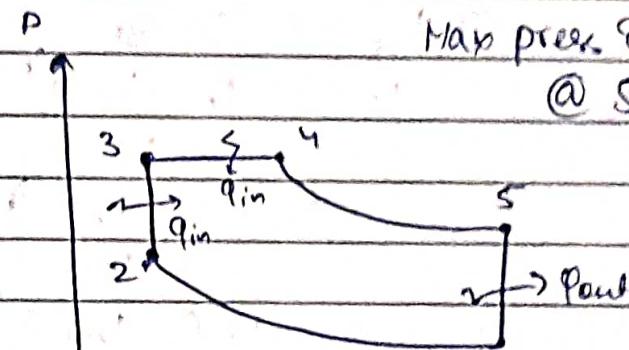
$$= \frac{577.41 - 303.05}{0.924 - 0.115}$$

$$= \frac{274.36}{0.809} = 339.1 \text{ kPa}$$

Dual cycle. $r_K = 14$, $\sigma_{rc} = 1.2$

$$r_p = 1.5$$

$$\begin{aligned} v_1 &= 14 & v_4 &= 1.2 \\ v_2 & & v_2 & \\ p_3 &= 1.5 & p_2 & \end{aligned}$$



Given @ State 1: $P_1 = 80 \text{ kPa}$

$$T_1 = 20^\circ\text{C} = 293 \text{ K}$$

Process 1-2 : isentropic

$$T_2 V_2^{\gamma-1} = T_1 V_1^{\gamma-1} \quad 2/5$$

$$T_2 = 293 (14)$$

$$T_2 = 842.01 \text{ K}$$

Process 2-3: isochoric.

$$T_3 = P_3$$

$$T_2 = P_2$$

$$T_3 = 1.5 \times 842.01$$

$$T_3 = 1263.01 \text{ K}$$

Process 3-4: isobaric

$$\frac{T_4}{T_3} = \frac{P_4}{P_3} \frac{V_4}{V_3}$$

$$T_4 = 1263.01 \times 1.2$$

$$T_4 = 1515.6 \text{ K.} \rightarrow \text{Maximum temp}$$

Process



Process 5-4 : Isentropic

$$T_5 V_5^{r-1} = T_4 V_4^{r-1}$$

$$T_5 = T_4 \left(\frac{V_4}{V_5} \right)^{r-1}$$

$$= T_4 \left(\frac{V_4}{V_1} \cdot \frac{V_1}{V_3} \right)^{r-1}$$

$$\approx T_4 \left(\frac{V_4}{14 V_3} \right)^{r-1}$$

$$T_5 = 1515.6 \left(\frac{1.2}{14} \right)^{7/15}$$

$$T_5 = 567.3 \text{ K}$$

New q_{in} Process 1-2:

$$P_1 V_1^r = P_2 V_2^r$$

$$P_2 = 80 (14)^{7/15}$$

$$P_2 = 3218.6 \text{ kPa}$$

~~Process 2-3: w.k. P₃ 1.5~~

$$1.5 P_2$$

$$P_3 = 1.5 P_2$$

$$P_3 = 4827.9 \text{ kPa}$$

$$P_1 : P_3 = 4827.9 \text{ kPa} \rightarrow \text{Maximum pressure}$$

By first

$$q_{in, total} = q_{in, isochoric} + q_{in, isobaric}$$

$$= C_v (T_3 - T_2) + C_p (T_4 - T_3)$$

$$q_{in, total} = 0.718 (1263.01 - 842.01) + 1.005 (1515.6 - 1263.01)$$

$$= 302.3 + 253.8$$

$$q_{in, total} = 556.15 \text{ kJ/kg}$$

First Law in 5-1

$$q_{out} = Cv(T_1 - T_5)$$

$$q_{out} = 0.718 (293 - 567.3)$$

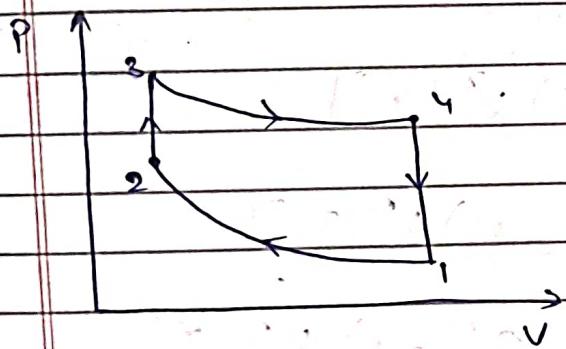
$$q_{out} = -196.9 \text{ kJ/kg}$$

$$\eta_{\text{Therm}} = \frac{1 - q_{out}}{q_{in}}$$

$$= 1 - \frac{196.9}{556.15}$$

$$= 0.645 \approx 64.6\% \text{ efficiency.}$$

- Q. Given: i) Otto cycle
 ii) q_{in} remains same
 iii) State 1 remains same
- Let $\left(\frac{v_1}{v_2}\right)_i = k$



The compression ratio is doubled

$$\Rightarrow \left(\frac{v_1}{v_2}\right)_f = 2k.$$

Process 1-2: Initially

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$

$$P_2 i = P_1 (K)^{\gamma}$$

$$\text{finally } P_{2f} = 2^\gamma P_1 (K)^\gamma \Rightarrow P_{2f} = 2^\gamma P_2 i$$

Initially $\gamma = 1$

$$\text{Now } T_1 V_1 = T_{2i} V_{2i}$$

~~$$T_{2i} = T_1 (K)^{\gamma-1}$$~~

$$\text{finally } T_{2f} = 2^{\gamma-1} T_1 (K)^{\gamma-1}$$

$$T_{2f} = 2^{\gamma-1} T_{2i}$$

Heat addition remain same.

$$\Rightarrow \rho u (T_{3f} - T_{2i}) = \rho u (T_{3i} - T_{2f})$$

$$T_{3i} - T_{2i} = T_{3f} - T_{2f}$$

$$T_{3i} + (2^{r-1} + 1)T_{2i} = T_{3f}$$

Maximum temperature $T_{3f} = T_{3i} + (2^{r-1} + 1) k^{r-1} \cdot T_i$ ✓
 finally. \hookrightarrow Max temperature initially.

Process 2-3: isochoric

$$\frac{P_3}{P_2} = \frac{T_3}{T_2}$$

$$P_3 = P_2 \frac{T_3}{T_2}$$

Final state: T_3 Initial state: T_2

$$P_{3f} = P_{2f} \frac{T_{3f}}{T_{2f}}$$

$$P_{3i} = P_{2i} \frac{T_{3i}}{T_{2i}}$$

$$= 2^r P_2 i \frac{[T_{3i} + (2^{r-1} + 1) k^{r-1} \cdot T_i]}{T_{2i}}$$

$$P_{3f} = 2 P_2 i \frac{[T_{3i} + (2^{r-1} + 1) k^{r-1} \cdot T_i]}{T_{2i}}$$

$$= 2 P_2 i \frac{T_{3i}}{T_{2i}} + 2 P_2 i (2^{r-1} + 1) k^{r-1} T_i$$

$$P_{3f} = 2 P_2 i + 2 P_2 i k^r (2^{r-1} + 1)$$

$$P_{3f} = 2 [P_{2i} + P_2 i k^r (2^{r-1} + 1)]$$

Maximum pressure
@ finally

Maximum temp.
@ first initially