1D Compressible Gas Dynamics of a Perfect gas Analytical Calculations: Part I

Teaching Assistant: Chitradeep Saha

Let us list down the basic thermodynamic properties of a perfect gas,

(1) Equation of state:
$$p = \rho RT$$
 where, $R = \frac{k_B}{m}$
(2) Internal energy: $\epsilon = C_V T = \left(\frac{R}{\gamma - 1}\right) T$

(3) Entropy (per unit mass): $TdS = d\epsilon + p \ d\left(\frac{1}{\rho}\right)$

Using (2) in (3),

$$dS = \left(\frac{R}{\gamma - 1}\right) \frac{dT}{T} + \frac{p}{T} \left(-\frac{1}{\rho^2}\right) d\rho$$

$$= C_V \frac{dT}{T} - \frac{R}{\rho} d\rho$$

$$= C_V \left[\frac{dp}{p} - \frac{d\rho}{\rho}\right] - R \frac{d\rho}{\rho} \quad \text{(using (1))}$$

$$= C_V \frac{dp}{p} - \frac{d\rho}{\rho} \left(C_V + R\right)$$

$$= C_V \frac{dp}{p} - C_p \frac{d\rho}{\rho}$$

$$\therefore dS = C_v \left[\frac{dp}{p} - \gamma \frac{d\rho}{\rho}\right]$$

Integrating we can write,

$$\frac{S - S_0}{C_V} = \ln p - \gamma \ln \rho = \ln \left(\frac{p}{\rho^{\gamma}}\right)$$

$$\therefore S = C_V \ln \left(\frac{p}{\rho^{\gamma}}\right) + S_0 \tag{4}$$

For an adiabatic process,

$$\frac{dS}{dt} = 0$$

Using (4) we can write,

$$\frac{d}{dt}\left(\frac{p}{\rho^{\gamma}}\right) = 0\tag{5}$$

$$\therefore \frac{1}{\rho^{\gamma}} \frac{dp}{dt} = \frac{\gamma p}{\rho^{(\gamma+1)}} \frac{d\rho}{dt}$$
$$\therefore dp = \frac{\gamma p}{\rho} d\rho$$

$$\therefore$$
 by definition of sound speed, $c_s = \sqrt{\frac{dp}{d\rho}} = \sqrt{\frac{\gamma p}{\rho}}$

Here, c_s is the speed of sound propagation through this gas under adiabatic condition.

Defining the speed of sound in non-relativistic regime

Consider the sound wave propagating at speed v through a pipe aligned with the x axis and with a cross-sectional area of A. In time interval dt it moves length dx = vdt. In steady state, the mass flow rate $\dot{m} = \rho vA$ must be the same at the two ends of the tube, therefore the mass flux $\dot{j} = \rho v$ is constant and $vd\rho = -\rho dv$. As per Newton's second law, the pressure gradient force provides the acceleration:

$$\frac{dv}{dt} = -\frac{1}{\rho} \frac{dP}{dx}$$

$$\therefore dP = (-\rho dv) \frac{dx}{dt} = (vd\rho)v$$

$$\therefore v^2 \equiv c_s^2 = \frac{dP}{d\rho}$$

And therefore:

$$c_s = \sqrt{\left(\frac{\partial P}{\partial \rho}\right)}$$

Now, enthalpy (per unit mass),

$$W = \epsilon + \frac{p}{\rho} = \frac{R}{\gamma - 1}T + RT = \left(1 + \frac{1}{\gamma - 1}\right)RT$$

$$\therefore W = \frac{\gamma}{\gamma - 1}RT \tag{6}$$

Moreover,

$$dW = d\epsilon + p d\left(\frac{1}{\rho}\right) + \frac{1}{\rho}dp$$

$$\therefore dW = TdS + \frac{dp}{\rho} \quad \text{(using (3))}$$

Under adiabatic condition (i.e., dS = 0),

$$\int \frac{dp}{\rho} = W \tag{6a}$$

Hence, for a perfect gas under the adiabatic condition the Bernoulli's equation $\left[\frac{1}{2}v^2 + \int \frac{dp}{\rho} + \Phi = \text{constant}\right]$ reduces to,

$$\frac{1}{2}v^2 + \frac{\gamma}{\gamma - 1}RT + \Phi = \text{constant} \tag{7}$$

Small amplitude acoustic wave propagation in a homogeneous, perfect, compressible gas

Any process causing a pressure (or/and) density fluctuation (i.e. perturbation) in a gas (compressible medium) is expected to generate acoustic wave. Here, we consider homogeneous perfect gas of density ρ_0 and pressure p_0 in the absence of any external force. We show that linear perturbation in pressure $p_1(\vec{x},t)$ and density $\rho_1(\vec{x},t)$ will give rise to acoustic wave.

These perturbations will also give rise to an *additional* velocity field $\overrightarrow{v_1}(\vec{x},t)$ on top of **previously existing velocity field** $\overrightarrow{v_0}(\vec{x},t)$. Then the continuity equation in this case can be written as,

$$\frac{\partial \left(\rho_{0} + \rho_{1}\right)}{\partial t} + \vec{\nabla} \cdot \left[\left(\rho_{0} + \rho_{1}\right) \left(\vec{v}_{0} + \vec{v}_{1}\right)\right] = 0$$

$$\therefore \frac{\partial \rho_{0}}{\partial t} + \vec{\nabla} \cdot \left(\rho_{0} \vec{v}_{0}\right) + \frac{\partial \rho_{1}}{\partial t} + \vec{\nabla} \cdot \left(\rho_{0} \vec{v}_{1}\right) + \vec{\nabla} \cdot \left(\rho_{1} \vec{v}_{0}\right) + \underbrace{\vec{\nabla} \cdot \left(\rho_{1} \vec{v}_{1}\right)^{0}}_{\text{linearization}} = 0$$

$$\therefore \frac{\partial \rho_{1}}{\partial t} + \underbrace{\vec{v}_{1} \cdot \vec{\nabla} \rho_{0}}_{\text{cont. eqn.}} + \vec{v}_{0} \cdot \vec{\nabla} \rho_{1} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) + \rho_{1} \left(\vec{\nabla} \cdot \vec{v}_{0}\right) = 0$$

$$\therefore \frac{\partial}{\partial t} \left(\rho_{0} \xi\right) + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) + \left(\rho_{0} \xi\right) \vec{\nabla} \cdot \vec{v}_{0} = 0 \quad [\text{ putting } \xi = \frac{\rho_{1}}{\rho_{0}}]$$

$$\therefore \rho_{0} \frac{\partial \xi}{\partial t} + \xi \frac{\partial \rho_{0}}{\partial t} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) + \xi \left(\rho_{0} \vec{\nabla} \cdot \vec{v}_{0}\right) = 0$$

$$\therefore \xi \left[\frac{\partial \rho_{0}}{\partial t} + \rho_{0} \vec{\nabla} \cdot \vec{v}_{0}\right] + \rho_{0} \frac{\partial \xi}{\partial t} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) = 0$$

$$\therefore \frac{\partial \xi}{\partial t} + \left(\vec{\nabla} \cdot \vec{v}_{1}\right) = 0$$

$$\therefore \frac{\partial \rho_{1}}{\partial \rho_{0}} - \frac{\rho_{1}}{\rho_{0}^{2}} \frac{\partial \rho_{0}}{\partial t} + \left(\vec{\nabla} \cdot \vec{v}_{1}\right) = 0$$

$$\therefore \frac{\partial \rho_{1}}{\partial \rho_{0}} - \frac{\rho_{1}}{\rho_{0}} \frac{\partial \rho_{0}}{\partial t} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) = 0$$

$$\therefore \frac{\partial \rho_{1}}{\partial \rho_{1}} - \frac{\rho_{1}}{\rho_{0}} \frac{\partial \rho_{0}}{\partial t} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) = 0$$

$$\therefore \frac{\partial \rho_{1}}{\partial \rho_{1}} + \rho_{0} \left(\vec{\nabla} \cdot \vec{v}_{1}\right) + \left(\vec{\nabla} \cdot \vec{v}_{0}\right) \rho_{1} = 0$$

In the last step, we use the continuity equation for corresponding unperturbed flow. It is worth noting that the compression term associated with the non-zero fluid velocity acts as an additional source of mass flux in the continuity equation.

The Euler equation, under the same linear perturbation reduces to,

$$(\rho_{0} + \rho_{1}) \left[\frac{\partial \vec{v}_{1}}{\partial t} + \underbrace{\left(\vec{v}_{1} \cdot \vec{\nabla}\right) \vec{v}_{1}}^{0} + \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \cdot \vec{v}_{0} + \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \vec{v}_{1} + \left(\vec{v}_{1} \cdot \vec{\nabla}\right) \vec{v}_{0} \right] = -\nabla p_{1} = -\nabla \left(c_{s}^{2} \rho_{1}\right)$$

$$\therefore \rho_{0} \frac{\partial \vec{v}_{1}}{\partial t} + \rho_{1} \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \vec{v}_{0} + \rho_{0} \left(\vec{v}_{1} \cdot \vec{\nabla}\right) \vec{v}_{0} + \rho_{0} \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \vec{v}_{0} + \rho_{0} \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \vec{v}_{0} + \rho_{0} \left(\vec{v}_{0} \cdot \vec{\nabla}\right) \vec{v}_{1} = -c_{s}^{2} \nabla \rho_{1}$$

Applying gradient operator on both sides,

$$\vec{\nabla} \cdot \left[\rho_0 \frac{\partial \vec{v}_1}{\partial t} + \rho_1 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{V}_1 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_1 \right] = -c_s^2 \nabla^2 \rho_1$$

$$\therefore \frac{\partial}{\partial t} \left[\rho_0 \left(\vec{\nabla} \cdot \vec{v}_1 \right) \right] + \vec{\nabla} \cdot \left[\rho_1 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{V}_1 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_0 + \rho_0 \left(\vec{v}_0 \cdot \vec{\nabla} \right) \vec{v}_1 \right] = -c_s^2 \nabla^2 \rho_1$$

$$\therefore -\frac{\partial^2 \rho_1}{\partial t^2} - \frac{\partial}{\partial t} \left(\vec{\nabla} \cdot \vec{v}_0 \right) \rho_1 + \vec{\nabla} \cdot \left[\text{terms containing } v_0 \right] = -c_s^2 \nabla^2 \rho_1$$

$$\therefore \left(\frac{\partial^2}{\partial t^2} - c_s^2 \nabla^2 \right) \rho_1 = \vec{\nabla} \cdot \left[\text{terms containing } v_0 \right] - \frac{\partial}{\partial t} \left(\vec{\nabla} \cdot \vec{v}_0 \right) \rho_1$$

$$\therefore \Box^2 \rho_1 = \vec{\nabla} \cdot \left[\text{terms containing } v_0 \right] - \frac{\partial}{\partial t} \left(\vec{\nabla} \cdot \vec{v}_0 \right) \rho_1$$

For $v_0 = 0$, above equation reduces to density perturbation wave equation,

$$\Box^2 \rho_1 = 0$$

Concept: For a truly incompressible fluid, a very large excess pressure dP would produce a negligible change in density $d\rho$, thus, $c_s^2 = \sqrt{\frac{dp}{d\rho}} \to \infty$, hence the sound speed in such a medium is infinite.

Concept: In an incompressible fluid system, any instability is wiped out instantaneously.