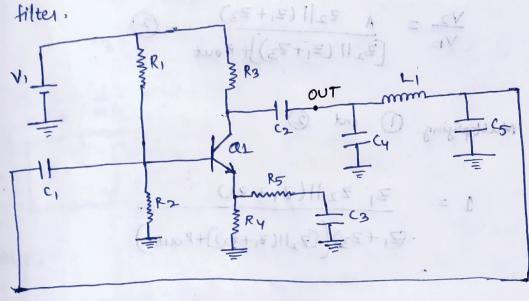
Colpitts Oscillatos

Frequency Calculation:

If we were to design an RC circuit as the tank circuit to achieve radio trequencies, we find out that the resistor and capacitor values have to be very small. Therefore we use inductor and capacitors in the feedback network for the



Colpitts Circuit

We can redraw the circuit in the following, way

here, A is the amplification factor

Since the ratio of voltages is equal to the ratio of the effective resistance the voltage supplies current to,

arty traff

we have

$$\frac{V_1}{V_2} = \frac{Z_1}{Z_1 + Z_3} - 0$$

$$\frac{V_2}{AV_1} = \frac{Z_2 ||(Z_1 + Z_3)|}{[Z_2||(Z_1 + Z_3)] + Rout}$$

$$\frac{V_2}{V_1} = \frac{A}{Z_2[1(Z_1+Z_3)]} - 2$$

$$1 = \frac{Z_1 \cdot Z_2 | 1(Z_1 + Z_2)}{(Z_1 + Z_2) \left((Z_2 | 1(Z_1 + Z_2)) + Pout \right)}$$

$$1 = \frac{2}{21 + 21 + 23} A$$

$$\frac{7}{21 + 21 + 23} \left(\frac{21(21 + 23)}{71 + 21 + 23} + Rout \right)$$

there a we be an echanton touter

$$\Delta = \int X_1 \int X_2 A$$

$$\int X_2 (\int X_1 + \int X_3) + (\int X_1 + \int X_2 + \int X_3) Rout$$

Since (JX1+JX2+JX3) Rout is the only imaginary part it must be o mangines and to sometimens

Here,
$$X_1 = -\frac{1}{wCy}$$
 $X_2 = -\frac{1}{wC_5}$
 $X_3 = wL_1$
 $X_4 = -\frac{1}{wC_5}$
 $X_5 = wL_1$
 $X_6 = wL_1$
 $X_$

(2nf) 2cycs

HMFF.001 = 14

= 17 6

486 3M

OC Slocking

13 3PM

Also,

$$A = \frac{22(2(+23))}{2(22)} = \frac{x_2(x_1 + x_3)}{x_1 x_2}$$

$$=) A = \frac{x_2(-x_2)}{x_1x_2}$$

$$= \frac{x_2(-x_2)}{x_1x_2}$$

$$A = -\left(\frac{1}{w_{1}}\right) = A = -\frac{C_{4}}{C_{5}}$$

DC current

The desired trequency is lookHz. We are not using capacitors with very low capacitance since the such or capacitance of pF order. Since the picofarads between rows and adjacent connections in the breadboard can interfere with the capacitance of the component making it capacitance of the component of nF range. ineffective. So we chose capacitors of nF range.

taking Cy = 47nF, $C_5 = 47nF$ Substituting these values along with trequency value in the tormula, $|C_4| = \frac{C_4 + C_5}{\omega^2 C_4 C_5}$

=)
$$L_1 = \frac{(4+15)^2}{(2\pi f)^2} = \frac{2(47\times 10^9)}{(2\times 3.14\times 10^5)^2\times 49\times 10^9}$$

22(31+33) =

CONT

We get = 1 = 100.794H

So we chose L1 = 100MH

DC Blocking

In order to make sure that the fransistor is in active mode [base-emitter in forward-bias and base-wheelor,] we need to make sure that DC wherent is not thowing into the base. So we werent is not thowing into the base. So we werent is not block DC current from feedback

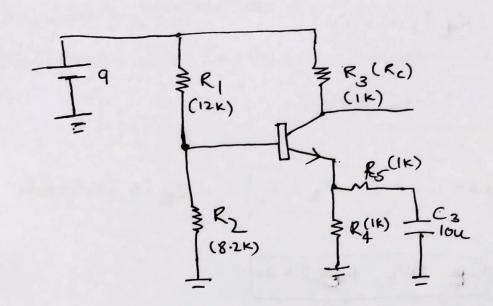
$$\frac{1}{wC_1} \leq R_1 + R_2$$

 $C_1 > \frac{1}{2\pi f(R_1 + R_2)}$

After biasing the BJT) $R_1 = 12 \text{KQ}$, $R_2 = 8.2 \text{KQ}$ $C_1 \ge \frac{1}{2 \times 3.14 \times 20.2 \times 10^3 \times 10^5}$

C1 3 0.08 nF

since we want to avoid values used to pf, we took (1 to be 100nf



- > BJT to Work as an Amplifier it must be in Active Region
- → (B-E) Junction => Forward Bais

(B 5) Junction ⇒ Reverse Bais

⇒ For Transtistor to be in Active Region, (VBE7,0.7.V)

So, let's fix R, = 12K, R2 = 8.2K and check that (B=7,0.7V) or Not

$$V_{88} = \frac{9 \times 8 \cdot 2}{12 + 8 \cdot 2} = \frac{9 \times 8 \cdot 2}{20 \cdot 2} = \frac{73 \cdot 8}{20 \cdot 2} = 3.65 > 0.7$$

So, we can fix R, and RZ.

→ For (B-F) Junction To Be in forward Bias,

⇒ For (B-c) Junction To Be in Reverse Bias, VB < Vc

$$2.95 = REIE \rightarrow 0$$

$$9 - REIE \rightarrow 3.65 \rightarrow 2$$

$$\Rightarrow I_{c} \approx I_{E}$$
 Because $I_{c} + I_{B} = I_{E}$

IB is Too Small.

$$\Rightarrow$$
 As Our Amplicification, $A = -\frac{Cz}{4} = -1$

So, Intially there will be a Amplification of a factor 2 and the Oscillations are Sustained through Amplification factor of