# Application of the entropy viscosity method to the 1-D grey Radiation-Hydrodynamic equations (RHD).

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Figure: Rhea

## Outline:

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- The theoretical approach.
  - A viscous regularization for the RHD
  - Definition of the viscosity coefficient.
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## Objective:

Apply the entropy viscosity method to the 1-D grey radiation-hydrodynamic equations  $\rightarrow$  multi-physic problem with source terms.

### Background:

- RHD are a wave-dominated problem with source terms.
- They are known to develop shocks due to the nature of Euler equations.
- Great amount of work available in the literature on how to solve RHD: approximate Riemann solver [13, 4], flux limiter [10], ...
- Have a common approach: focus on the hyperbolic part of the RHD.
- Attempts to derive a Riemann solver accounting for the source terms.
- Use of semi-implicit schemes because of the difference of characteristic time scale between the two physics  $\rightarrow$  implicit scheme has some advantage.

## The 1-D grey Radiation-Hydrodynamic equations (RHD):

## RHD system of equations:

$$\begin{split} &\partial_{t}\left(\rho\right)+\partial_{x}\left(\rho u\right)=0\\ &\partial_{t}\left(\rho u\right)+\partial_{x}\left(\rho u^{2}+P\right)=-\partial_{x}\left(\frac{\epsilon}{3}\right)\\ &\partial_{t}\left(\rho E\right)+\partial_{x}\left[u\left(\rho E+P\right)\right]=-\frac{u}{3}\partial_{x}\epsilon-\sigma_{a}c\left(aT^{4}-\epsilon\right)\\ &\partial_{t}\epsilon+\frac{4}{3}\partial_{x}\left(u\epsilon\right)=\frac{u}{3}\partial_{x}\epsilon+\partial_{x}\left(\frac{c}{3\sigma_{t}}\partial_{x}\epsilon\right)+\sigma_{a}c\left(aT^{4}-\epsilon\right) \end{split}$$

#### A few remarks:

- Relaxation term in the energy and radiation equations:  $\sigma_a c (aT^4 \epsilon)$ .
- Diffusion term:  $\partial_X \left( \frac{c}{3\sigma_t} \partial_X \epsilon \right)$ .
- The above system of equations is NOT hyperbolic ????

## The entropy viscosity method (EVM) [16]:

It is an artificial dissipation method with smart viscosity coefficient(s) capable of tracking the shock so that dissipation is only added into the shock region.

- The method requires a hyperbolic system of equations.
- Add artificial dissipative terms consistent with the entropy minimum principle.
- Define a local and smooth viscosity coefficient function of the grid size.
- The viscosity coefficient is defined proportional to the entropy production.
- The entropy production is locally computed by evaluating the entropy residual:

$$R_e = \partial_t s + \vec{u} \cdot \vec{\nabla} s \ge 0$$

## Our approach:

- Consider the hyperbolic part of the system of equations (no source terms).
- Keep in mind that the source terms may affect the entropy viscosity method and their effect will have to be studied later.

## Our hyperbolic system of equations:

$$\begin{cases} \partial_{t}(\rho) + \partial_{x}(\rho u) = 0 \\ \partial_{t}(\rho u) + \partial_{x}(\rho u^{2} + P + \frac{\epsilon}{3}) = 0 \\ \partial_{t}(\rho E) + \partial_{x}\left[u(\rho E + P)\right] = 0 \\ \partial_{t}\epsilon + \frac{4}{3}\partial_{x}(u\epsilon) - \frac{u}{3}\partial_{x}\epsilon = 0 \end{cases}$$

Eigenvalues:  $\lambda_1 = u - c$ ,  $\lambda_{2,3} = u$  and  $\lambda_4 = u + c$  where c is the speed of sound defined as:

$$c^{2} = \underbrace{P_{\rho} + \frac{P}{\rho^{2}} P_{e}}_{C_{\text{Euler}}^{2}} + \underbrace{\frac{4\epsilon}{9\rho}}_{C_{\text{ad}}^{2}}$$

## Viscous regularization and viscosity coefficient(s):

- Oerive the dissipative terms using the modified system of equations (no source term).
  - An entropy s function of the material density  $\rho$  and internal energy e, and the radiation density energy  $\epsilon$ .
- ② Define the viscosity coefficient(s).

#### Method of Manufactured Solutions and 1-D results:

- Study the effect of the source terms,  $\partial_x \left( \frac{c}{3\sigma_t} \partial_x \epsilon \right)$  and  $\sigma_a c \left( a T^4 \epsilon \right)$ , on the entropy viscosity method using the method of manufactured solutions, and show high-order convergence.
- Perform 1-D tests for different Mach numbers: Mach= 1.05, 1.2, 2, 5, and 50. Semi-analytical solutions are available.

## A viscous regularization for the RHD:

$$\begin{split} &\partial_{t}\left(\rho\right)+\partial_{x}\left(\rho u\right)=\partial_{x}\left(\kappa\partial_{x}\rho\right)\\ &\partial_{t}\left(\rho u\right)+\partial_{x}\left(\rho u^{2}+P+\frac{\epsilon}{3}\right)=\partial_{x}\left(\mu\partial_{x}u\right)+\partial_{x}\left(\kappa\partial_{x}\rho\right)\\ &\partial_{t}\left(\rho E\right)+\partial_{x}\left[u\left(\rho E+P\right)\right]=\partial_{x}\left(\kappa\partial_{x}\rho e\right)+0.5\partial_{x}\left(\kappa u^{2}\partial_{x}\rho\right)+\partial_{x}\left(\mu\rho u\partial_{x}u\right)\\ &\partial_{t}\epsilon+\frac{4}{3}\partial_{x}\left(u\epsilon\right)-\frac{u}{3}\partial_{x}\epsilon=\partial_{x}\left(\kappa\partial_{x}\epsilon\right) \end{split}$$

### The entropy inequality:

$$R_e = \partial_t s + u \partial_x s = \frac{s_e}{P_e} \underbrace{\left(\frac{DP}{Dt} - c_{Euler}^2 \frac{D\rho}{Dt}\right)}_{\tilde{R}_e} \ge 0$$

where  $s(\rho, e, \alpha) = s_{Euler}(\rho, e) + \frac{\rho_0}{\rho} \hat{s}(\alpha)$ ,  $s_{Euler}$  and  $\hat{s}$  being concave.

two viscosity coefficients:  $\kappa$  and  $\mu$ . In the rest of this presentation, we will assume that  $\kappa=\mu\to$  parabolic regularization.

## Definition of the viscosity coefficient $\kappa$ :

$$\begin{split} \mu(x,t) &= \min \left( \mu_{max}(x,t), \mu_{e}(x,t) \right) \\ \mu_{max}(x,t) &= 0.5 h \left( |u| + c \right) \\ \mu_{e}(x,t) &= h^2 \frac{\max \left( \tilde{R}_{e}(x,t), J \right)}{norm_{P}} \end{split}$$

#### Entropy residual:

$$\tilde{R}_e = \frac{DP}{Dt} - c_{Euler}^2 \frac{D\rho}{Dt}$$

### The jump J and the normalization parameter $norm_P$ :

$$J = \max \left( |u|[[\partial_x P]], |u|c_{Euler}^2[[\partial_x \rho]] \right)$$

$$norm_P = \rho c_{Euler}^2$$

## EVM and the diffusion term $\partial_x \left( \frac{c}{3\sigma_t} \partial_x \epsilon \right)$ :

In the radiation equation, there are two second-order terms: diffusion and dissipative terms.

$$\partial_{x}\left(\frac{c}{3\sigma_{t}}\partial_{x}\epsilon\right) + \partial_{x}\left(\kappa\partial_{x}\epsilon\right) \rightarrow \partial_{x}\left(\max\left(\frac{c}{3\sigma_{t}},\kappa\right)\partial_{x}\epsilon\right)$$

#### Relaxation term:

$$\begin{cases} \partial_t u + \partial_x v = 0 \\ \partial_t v + \partial_x p(u) = \frac{1}{\psi} (v - f(u)) \end{cases}$$

as  $\psi \to 0$ , it can be shown that:

$$\begin{cases} v \sim f(u) \\ \partial_t u + \partial_x f(u) = \partial_x (\beta \partial_x u) \end{cases}$$

where  $\beta$  is function of  $\psi$ , p(u) and f(u).

#### Problem:

⇒ the relaxation term behaves as a diffusion term in the asymptotic limit and thus, will compete with the dissipative term.

#### Solution:

MMS to investigate the behavior of the dissipative terms in the asymptotic limit.



### The code

- Idaho National Laboratory MOOSE framework.
- ullet Fully implicit o non-linear solver with a preconditioner.
- Continuous Galerkin Finite Element Method (CGFEM).
- Second-order in time (BDF2) and space (linear polynomials).
- Gauss quadrature rule.
- RHEA: Radiation-Hydrodynamic EquAtions (1-D code).

## MMS: the equilibrium diffusion limit

$$\rho = \sin(x - t) + 2$$

$$u = \cos(x - t) + 2$$

$$T = \frac{0.5\gamma(\cos(x - t) + 2)}{\sin(x - t) + 2}$$

$$\epsilon = aT^4$$

$$\sigma_{a} = \sigma_{t} = 1000 \text{ cm}^{-1}$$
.

Table:  $L_2$  norms of the error for for the equilibrium diffusion limit case using a manufactured solution.

# of cells	time step size (sh)	ρ	ratio	hoE	ratio
20	$10^{-1}$	0.590766	NA	1.333774	NA
40	$5 \ 10^{-1}$	0.290626	2.03	0.478819	2.79
80	$2.5 \ 10^{-2}$	0.0959801	3.021	0.154119	3.11
160	$1.25 \ 10^{-2}$	0.02593738	3.70	0.0405175	3.80
320	$6.25 \ 10^{-3}$	$6.471444 \ 10^{-3}$	4.00	$9.90446 \ 10^{-3}$	4.09
640	$3.125 \ 10^{-3}$	$1.584158 \ 10^{-3}$	4.01	$2.44727 \ 10^{-3}$	4.04
# of cells	time step size (sh)	$\epsilon$	ratio	hou	ratio
# of cells	$10^{-1}$	$\epsilon$ 0.00650085	ratio NA	ρ <b>u</b> 0.910998	ratio NA
	. , ,	_		'	
20	$10^{-1}$	0.00650085	NA	0.910998	NA
20	$   \begin{array}{r}     10^{-1} \\     5 10^{-1} \\     2.5 10^{-2} \\     1.25 10^{-2}   \end{array} $	0.00650085 0.00124983	NA 5.20	0.910998 0.4090946	NA 2.23
20 40 80	$   \begin{array}{r}     10^{-1} \\     5 \ 10^{-1} \\     2.5 \ 10^{-2}   \end{array} $	0.00650085 0.00124983 0.000262797	NA 5.20 4.76	0.910998 0.4090946 0.125943	NA 2.23 3.25

The second manufactured solution is used to test the method in the streaming limit: the radiation streaming dominates the absorption/re-emission term and evolves at a fast time scale.

## MMS: the streaming limit

$$\rho = \sin(x - t) + 2$$

$$u = (\sin(x - t) + 2)^{-1}$$

$$T = 0.5\gamma$$

$$\epsilon = \sin(x - 1000t) + 2$$

$$\sigma_a = \sigma_t = 1 \text{ cm}^{-1}$$
.

Table:  $L_2$  norms of the error for the streaming limit case using a manufactured solution.

# of cells	time step size (sh)	ρ	ratio	hoE	ratio
20	$10^{-1}$	$1.4373 \ 10^{-2}$	NA	$5.88521 \ 10^{-1}$	NA
40	5. 10 <sup>-2</sup>	$3.760208 \ 10^{-3}$	3.82	$1.4244 \ 10^{-1}$	4.13
80	$2.5 \ 10^{-2}$	$9.91724 \ 10^{-4}$	3.79	$3.2047 \ 10^{-2}$	4.44
160	$1.25 \ 10^{-2}$	$2.4455 \ 10^{-4}$	4.06	$7.4886 \ 10^{-3}$	4.28
320	$6.25 \ 10^{-3}$	$6.280715 \ 10^{-5}$	3.89	$1.82327 \ 10^{-3}$	4.11
640	$3.125 \ 10^{-3}$	$1.57920 \ 10^{-5}$	3.98	$4.50463 \ 10^{-4}$	4.05
1280	$1.5625 \ 10^{-4}$	$3.96096 \ 10^{-6}$	3.99	$1.12061 \ 10^{-4}$	4.02
# of cells	time step size (sh)	$\epsilon$	ratio	hou	ratio
# of cells	time step size $(sh)$ $10^{-1}$	$\epsilon$ 3.82001 $10^{-1}$	ratio NA	ho <b>u</b> 2.354671 10 <sup>-3</sup>	ratio NA
<u> </u>	. ,	-		,	
20	$10^{-1}$	$3.82001 \ 10^{-1}$	NA	$2.354671 \ 10^{-3}$	NA
20 40	10 <sup>-1</sup> 5. 10 <sup>-2</sup>	$3.82001 \ 10^{-1}$ $1.21500 \ 10^{-1}$ $3.27966 \ 10^{-2}$ $8.38153 \ 10^{-3}$	NA 3.14	$\begin{array}{c} 7 \\ 2.354671 \ 10^{-3} \\ 6.138814 \ 10^{-4} \end{array}$	NA 3.84
20 40 80	10 <sup>-1</sup> 5. 10 <sup>-2</sup> 2.5 10 <sup>-2</sup> 1.25 10 <sup>-2</sup> 6.25 10 <sup>-3</sup>	$3.82001 \ 10^{-1}$ $1.21500 \ 10^{-1}$ $3.27966 \ 10^{-2}$	NA 3.14 3.70	2.354671 10 <sup>-3</sup> 6.138814 10 <sup>-4</sup> 1.74974 10 <sup>-4</sup>	NA 3.84 3.51
20 40 80 160	10 <sup>-1</sup> 5. 10 <sup>-2</sup> 2.5 10 <sup>-2</sup> 1.25 10 <sup>-2</sup>	$3.82001 \ 10^{-1}$ $1.21500 \ 10^{-1}$ $3.27966 \ 10^{-2}$ $8.38153 \ 10^{-3}$	NA 3.14 3.70 3.91	2.354671 10 <sup>-3</sup> 6.138814 10 <sup>-4</sup> 1.74974 10 <sup>-4</sup> 3.61297 10 <sup>-5</sup>	NA 3.84 3.51 4.84

September 11, 2014

#### 1-D numerical results:

- Inlet Mach number: 1.05, 1.2, 2, 5 and 50.
- Step initial conditions.
- All tests reach a steady-state solution.
- BDF2 and linear polynomials.
- Uniform mesh.
- Semi-analytical solutions are plotted for comparison.

## Numerical results: Mach 1.05.

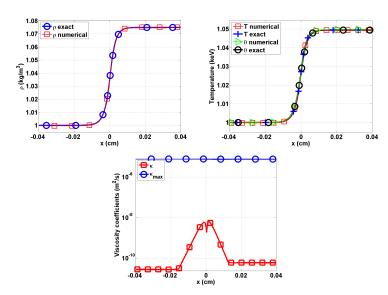


Figure: Steady-state numerical solution with 500 cells, linear polynomials and BDF2,

## Numerical results: Mach 1.2.

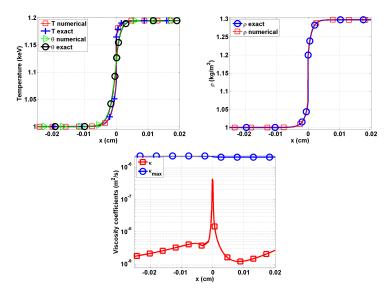


Figure: Steady-state numerical solution with 1000 cells, linear polynomials and BDF2.

## Numerical results: Mach 2.

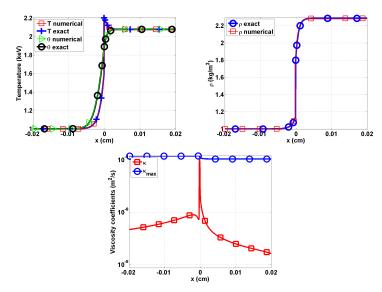


Figure: Steady-state numerical solution with 1000 cells, linear polynomials and BDF2.

### Numerical results: Mach 5.

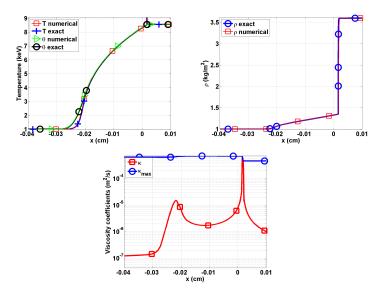
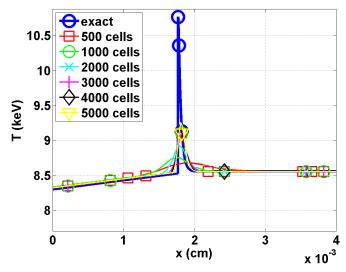


Figure: Steady-state numerical solution with 1000 cells, linear polynomials and BDF2.

## Numerical results: Mach 5, Zeldovich spike.



## Numerical results: Mach 50.

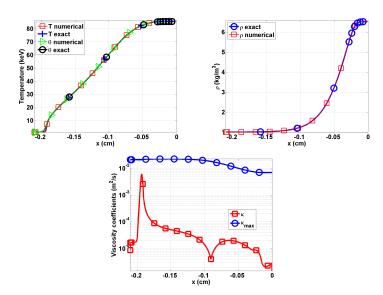


Figure: Steady-state numerical solution with 1000 cells, linear polynomials and BDF2,

#### Conclusions:

- The entropy viscosity method was successfully applied to the 1-D RHD.
- 1-D numerical results show good agreement with semi-analytical solutions.
- Demonstrated high-order accuracy and correct behavior in the equilibrium diffusion limit.
- The method can be applied with any equation of state with a convex entropy.
- The method is simple to implement and the viscosity coefficient is computed on the fly.

#### Future work:

- Extension to multi-D simulations: the theoretical approach holds.
- $S_n$  transport approximation (instead of the radiation-diffusion equation) coupled to Euler equations.

## **QUESTIONS/COMMENTS?**

## Entropy residual with dissipative terms:

$$\begin{split} \frac{\textit{Ds}}{\textit{Dt}} + \underbrace{\left(\textit{P}\partial_{e}\textit{s} + \rho^{2}\partial_{\rho}\textit{s} + \frac{4}{3}\rho\epsilon\partial_{\epsilon}\textit{s}\right)\partial_{x}\textit{u}}_{\text{(a)}} = \\ \partial_{x}\left(\rho\kappa\partial_{x}\textit{s}\right) + \kappa\partial_{e}\textit{s}\partial_{x}\textit{s} - \rho\kappa\underbrace{\textit{XAX}^{t}}_{\text{(b)}} + \underbrace{\textit{s}_{e}\rho\mu(\partial_{x}\textit{u})^{2}}_{\text{(c)}} \end{split}$$

where X is a row vector defined as  $X = (\rho, e, \epsilon)$  and A is the 3x3 symmetric matrix:

$$A = \left[ \begin{array}{ccc} \partial_{\rho} \left( \rho^{2} \partial_{\rho} s \right) & \partial_{\rho,e} s & \partial_{\rho} \left( \rho \partial_{\epsilon} s \right) \\ \partial_{\rho,e} s & \partial_{e,e} s & \partial_{e,\epsilon} s \\ \partial_{\rho} \left( \rho \partial_{\epsilon} s \right) & \partial_{e,\epsilon} s & \partial_{\epsilon,\epsilon} s \end{array} \right]$$



## Positivity of the matrix *A*:

With 
$$s(\rho, e, \epsilon) = \tilde{s}(\rho, e) + \frac{\rho_0}{\rho} \hat{s}(\epsilon)$$
:
$$A = \begin{bmatrix} \partial_{\rho} \left( \rho^2 \partial_{\rho} \tilde{s} \right) & \partial_{\rho, e} \tilde{s} & 0 \\ \partial_{\rho, e} \tilde{s} & \partial_{e, e} \tilde{s} & 0 \\ 0 & 0 & \rho^{-1} \partial_{\epsilon, \epsilon} \hat{s} \end{bmatrix}$$

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