# Entropy-based artificial viscosity stabilization for non-equilibrium Grey Radiation-Hydrodynamics

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09/09/2015

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#### Outline

- Background and Motivation
  - Grey Radiation-Hydrodynamics
  - A Brief Review of the Entropy Viscosity Method for Conservation Laws
- Development of entropy-based artificial viscosity for the GRHD
  - Questions to answer
  - Previous results (JCP 2015)
  - New developments
- Numerical results
  - Constant opacities
  - Temperature-dependent opacities
- Conclusions

# Grey Radiation-Hydrodynamics (GRHD)

#### GRHD system of equations

$$\begin{split} \partial_t \left( \rho \right) + \partial_x \left( \rho u \right) &= 0 \\ \partial_t \left( \rho u \right) + \partial_x \left( \rho u^2 + P \right) &= -\partial_x \left( \frac{\epsilon}{3} \right) \\ \partial_t \left( \rho E \right) + \partial_x \left[ u \left( \rho E + P \right) \right] &= -\frac{u}{3} \partial_x \epsilon - \sigma_a c \left( a T^4 - \epsilon \right) \\ \partial_t \epsilon + \frac{4}{3} \partial_x \left( u \epsilon \right) &= \frac{u}{3} \partial_x \epsilon + \partial_x \left( \frac{c}{3 \sigma} \partial_x \epsilon \right) + \sigma_a c \left( a T^4 - \epsilon \right) \end{split}$$

- ullet  $\rho$  material density
- u material velocity
- E material specific total energy
- ullet  $\epsilon$  radiation energy density
- P material pressure

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T material temperature

#### A few remarks:

- Relaxation term in the energy and radiation equations:  $\sigma_{ac}(aT^4 \epsilon)$ .
- Diffusion term:  $\partial_X \left( \frac{c}{3\sigma_t} \partial_X \epsilon \right)$ .
- The above system of equations is NOT hyperbolic.

#### Proposed goal

To stabilize the above system with a high-order artificial viscosity method based on the local entropy production

### Quick overview of the entropy-based artificial viscosity formalism

General scalar conservation law:  $\partial_t u + \vec{\nabla} \cdot \vec{f}(u) = 0$ .

- **Q** Let the amount of artificial viscosity  $\mu$  be  $\underline{\propto}$  the local entropy production
  - Determine an entropy pair  $(s(u), \vec{\Psi}(u))$  for the PDE under consideration
  - Compute the entropy residual  $R_e := \partial_t s(u_h) + \vec{\nabla} \cdot \Psi(u_h)$ , in each cell K, at each quadrature point  $x_a$
  - Compute the speed and kinematic entropy viscosity associated with this residual

$$v_e^K(x_q) := h_K \frac{|R_e(x_q)|_K}{|s - \overline{s}|_{\infty}} \quad \text{and} \quad \mu_e^K(x_q) := h_K v_e^K(x_q) \tag{1}$$

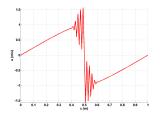
 $\bullet$  Limit the viscosity: upper bound = <u>Local Lax-Friedrichs</u> (LLF) viscosity

$$\mu^{K}(x_q) := \min\left(\frac{h_K}{2} \max_{x \in K} |\vec{f}'(u(x))|, \, \mu_e^{K}(x_q)\right) \tag{2}$$

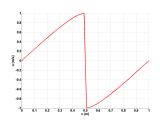
Plug in the standard Galerkin weak form as a viscous regularization

$$\int_{V} (\partial_{t} u_{h} + \vec{\nabla} \cdot \vec{f}(u_{h})) b \, dx + \sum_{K} \int_{K} \mu^{K} \vec{\nabla} u_{h} \cdot \vec{\nabla} b \, dx = 0 \quad \forall b$$
 (3)

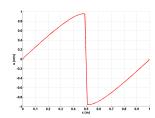
# Example: Burgers equation $\partial_t u + \frac{1}{2} \partial_x u^2 = 0$



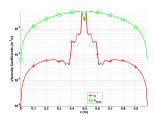




(c) With entropy viscosity

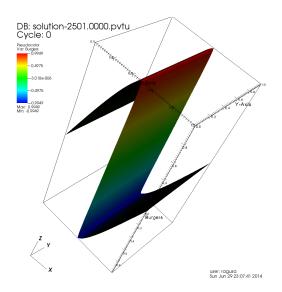


(b) With first-order viscosity



(d) Viscosity coefficient profiles





### Viscous regularization of Euler equations

#### Regularized Euler equations

$$\begin{split} \partial_t \rho + \vec{\nabla} \cdot (\rho \vec{u}) &= \vec{\nabla} \cdot \vec{f} \\ \partial_t (\rho \vec{u}) + \vec{\nabla} \cdot (\rho \vec{u} \otimes \vec{u} + P \mathbb{I}) &= \vec{\nabla} \cdot \mathbf{g} \\ \partial_t (\rho E) + \vec{\nabla} \cdot [\vec{u} (\rho E + P)] &= \vec{\nabla} \cdot \vec{h} \end{split}$$

How to select the artificial viscous fluxes?

By proving that the regularized equations satisfy a minimum principle on the specific entropy,  $s(\rho, e)$  [Guermond/Popov/Pasquetti (JCP 2011)]

#### Minimum entropy principle

$$\inf_{x \in \mathbb{R}^d} s(x, t) \ge \inf_{x \in \mathbb{R}^d} s_0(x) \qquad \forall t \ge 0$$
 (5)

### General idea of the derivation

### Goal: To obtain an entropy relationship: $\rho(\partial_t s + \vec{u} \cdot \vec{\nabla} s) = \ldots \geq 0$

Entropy is a function of density  $\rho$  and internal energy e. Using chain rule, we have

$$\partial_{\alpha} s = s_{\rho} \frac{\partial_{\alpha} \rho}{\partial \alpha} + s_{e} \frac{\partial_{\alpha} e}{\partial \alpha}$$
 with  $\alpha = t, x$ 

Now, re-write Euler equations in non-conservative form as a function of  $\rho$ , u, and e.

#### Entropy equation

The following choice of viscous fluxes,  $\vec{f} = \kappa \vec{\nabla} \rho$ ,  $g = \mu \rho \vec{\nabla}^s \vec{u} + \vec{u} \otimes \vec{f}$ , and  $\vec{h} = \kappa \vec{\nabla} (\rho e) - \frac{1}{2} u^2 \vec{f} + g \cdot \vec{u}$ , yields:

$$\rho \left( \partial_t \mathbf{s} + \vec{u} \cdot \vec{\nabla} \mathbf{s} \right) = \vec{\nabla} \cdot \left( \rho \kappa \vec{\nabla} \mathbf{s} \right) - \kappa \rho \mathbf{Q} + \mathbf{s}_e \mu \vec{\nabla}^s \vec{u} : \vec{\nabla} \vec{u}$$

#### Quadratic form

$$\mathbf{Q} = X^t \Sigma X \quad \text{ with } X = \begin{bmatrix} \vec{\nabla} \rho \\ \vec{\nabla} e \end{bmatrix} \text{ and } \Sigma = \begin{bmatrix} \partial_\rho (\rho^2 \partial_\rho \mathbf{s}) & \partial_{\rho, \mathbf{e}} \mathbf{s} \\ \partial_{\rho, \mathbf{e}} \mathbf{s} & \partial_{e, \mathbf{e}} \mathbf{s} \end{bmatrix}$$

The form  ${\bf Q}$  is negative definite if and only if -s is convex with respect to e and  $\rho^{-1}$ .

QED (recall:  $s_e = 1/T > 0$ )

### Euler equations with viscous regularization (final form)

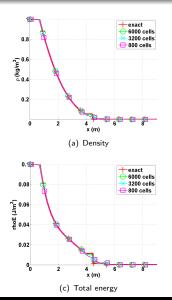
$$\begin{split} \partial_t \rho + \vec{\nabla} \cdot (\rho \vec{u}) &= \vec{\nabla} \cdot \left( \kappa \vec{\nabla} \rho \right) \\ \partial_t \left( \rho \vec{u} \right) + \vec{\nabla} \cdot \left( \rho \vec{u} \otimes \vec{u} + P \mathbb{I} \right) &= \vec{\nabla} \cdot \left( \mu \rho \vec{\nabla}^s \vec{u} + \kappa \vec{u} \otimes \vec{\nabla} \rho \right) \\ \partial_t \left( \rho E \right) + \vec{\nabla} \cdot \left[ \vec{u} \left( \rho E + P \right) \right] &= \vec{\nabla} \cdot \left( \kappa \vec{\nabla} \left( \rho e \right) + \frac{1}{2} ||\vec{u}||^2 \kappa \vec{\nabla} \rho + \rho \mu \vec{u} \vec{\nabla} \vec{u} \right) \end{split}$$

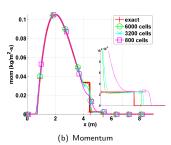
where  $\kappa$  and  $\mu$  are positive viscosity coefficients.

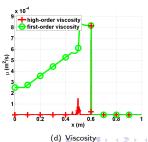
#### Definition of the viscosity coefficients

- As before,  $\mu = \min(\mu^{LLF}, \mu^{entr})$  and  $\kappa = \min(\kappa^{LLF}, \kappa^{entr})$
- All-speed (from low-Mach to supersonic) extension by Delchini/Ragusa/Berry in Computers & Fluids, 2015

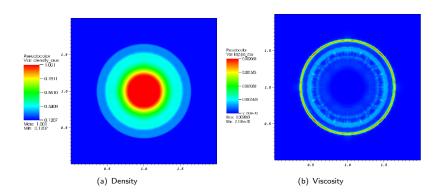
### Leblanc shock tube







### 2-D explosion test



### Entropy-based artificial viscosity technique for the GRHD

#### Questions to answer:

- The GRHD equations are not hyperbolic. Can we apply the entropy viscosity method (EVM)?
  - Our initial attempt: apply the EVM to the hyperbolic part of the GRHD [an idea similar to Balsara JQSRT 1999, Lowrie&Morel JQSRT 2001]
- ② What is an appropriate functional form for the entropy of the GRHD,  $s(\rho, e, \epsilon) = ...???$
- What is an appropriate expression for the viscous fluxes so that the regularized GRHD eqs satisfy the minimum entropy principle?
- Is the viscous regularization well-behaved in the equilibrium-diffusion limit?

### Hyperbolic part of the GRHD

$$\partial_t \left( \rho \right) + \partial_x \left( \rho u \right) = 0 \tag{7a}$$

$$\partial_t (\rho u) + \partial_x \left( \rho u^2 + P + \frac{\epsilon}{3} \right) = 0$$
 (7b)

$$\partial_{t}\left(\rho E\right)+\partial_{x}\left[u\left(\rho E+P\right)\right]+\frac{u}{3}\partial_{x}\epsilon=0$$
 (7c)

$$\partial_t \epsilon + \frac{4}{3} \partial_x (u\epsilon) - \frac{u}{3} \partial_x \epsilon = 0$$
 (7d)

#### Eigenvalues

$$\lambda_{1,4} = u \pm c_m$$

$$\lambda_{2,3} = u$$

with

$$c_m^2 = \underbrace{P_\rho + \frac{P}{\rho^2} P_e}_{c_{\text{cuter}}^2} + \underbrace{\frac{4\epsilon}{9\rho}}_{c_{\text{cuter}}^2}$$

### Entropy-based artificial viscosity for the GRHD: derivation

#### Study of the hyperbolic parts of the GRHD: process

Add viscous regularization (fluxes) to the equations

$$\partial_t \left( \rho \right) + \partial_x \left( \rho \mathbf{u} \right) = \frac{\partial_x \mathbf{f}}{\partial_x \mathbf{f}} \tag{8a}$$

$$\partial_t (\rho u) + \partial_x \left( \rho u^2 + P + \frac{\epsilon}{3} \right) = \partial_x \mathbf{g}$$
 (8b)

$$\partial_t (\rho E) + \partial_x [u(\rho E + P)] + \frac{u}{3} \partial_x \epsilon = \frac{\partial_x h}{\partial_x \epsilon}$$
 (8c)

$$\partial_t \epsilon + \frac{4}{3} \partial_x (u\epsilon) - \frac{u}{3} \partial_x \epsilon = \frac{\partial_x \ell}{2}$$
 (8d)

**4** With  $s(\rho, e, \epsilon)$ , use chain rule to obtain the entropy relationship

$$\partial_{\alpha} \mathbf{s} = \partial_{\rho} \mathbf{s} \partial_{\alpha} \rho + \partial_{e} \mathbf{s} \partial_{\alpha} \mathbf{e} + \partial_{\epsilon} \mathbf{s} \partial_{\alpha} \epsilon \tag{9}$$

**②** An observation: we can greatly simplify the expression by assuming  $s(\rho, e, \epsilon) = s_{Euler}(\rho, e) + s_{rad}(\rho, \epsilon)$ 



#### Study of the hyperbolic parts of the GRHD: results

•

$$s(\rho, e, \epsilon) = s_{Euler}(\rho, e) + \frac{4a^{1/4}}{3\rho} \epsilon^{\frac{3}{4}}$$
 (10)

 Using the Eulerian viscous fluxes, supplemented by an radiation energy viscous flux

$$\begin{cases}
f = \kappa \partial_{x} \rho \\
g = \rho \mu \partial_{x} u + uf \\
h = \kappa \partial_{x} (\rho e) - \frac{1}{2} u^{2} f + gu \\
\ell = \kappa \partial_{x} \epsilon
\end{cases} (11)$$

we get the following result:

Entropy conservation statement:

$$\left| \rho \frac{Ds}{Dt} = \partial_x \left( \rho \kappa \partial_x s \right) + (\kappa \partial_x \rho) (\partial_x s) - \rho \kappa X^T A X + s_e \rho \mu (\partial_x u)^2 \ge 0 \right|$$

$$X = \begin{bmatrix} \partial_x \rho \\ \partial_x e \\ \partial_x \epsilon \end{bmatrix} \text{ and } A = \begin{bmatrix} \partial_\rho \left( \rho^2 \partial_\rho s_{Euler} \right) & \partial_{\rho,e} s_{Euler} & 0 \\ \partial_{\rho,e} s_{Euler} & \partial_{e,e} s_{Euler} & 0 \\ 0 & 0 & -\frac{a^{1/4}}{4\rho} \epsilon^{-5/4} \end{bmatrix}$$

The form  $X^TAX$  is negative -definite (Delchini/Ragusa/Morel, JCP 2015)



### New developments

#### Entropy conservation statement for the full GRHD equations

Recently, we have been able to show:

$$\rho \frac{Ds}{Dt} = \partial_{x} \left( \rho \kappa \partial_{x} s \right) + (\kappa \partial_{x} \rho) (\partial_{x} s) - \rho \kappa X^{T} A X + s_{e} \rho \mu (\partial_{x} u)^{2} \\
+ \left( \rho s_{\epsilon} - s_{e} \right) \sigma_{\theta} c \left( a T^{4} - \epsilon \right) + \rho s_{\epsilon} \partial_{x} \left( \frac{c}{3\sigma_{t}} \partial_{x} \epsilon \right) \geq 0 \quad (12)$$

where the terms in red are unconditionally entropy-producing (unpublished, in preparation)

### Finally, the Regularized full GRHD equations are: (shown with $\kappa=\mu$ )

$$\partial_{t}\left(\rho\right) + \partial_{x}\left(\rho u\right) = \frac{\partial_{x}\left(\kappa \partial_{x} \rho\right)}{\left(\kappa \partial_{x} \rho\right)} \tag{13a}$$

$$\partial_t (\rho u) + \partial_x \left( \rho u^2 + P + \frac{\epsilon}{3} \right) = \frac{\partial_x (\kappa \partial_x (\rho u))}{(13b)}$$

$$\partial_{t} (\rho E) + \partial_{x} \left[ u \left( \rho E + P \right) \right] = -\frac{u}{3} \partial_{x} \epsilon - \sigma_{a} c \left( a T^{4} - \epsilon \right) + \frac{\partial_{x} \left( \kappa \partial_{x} (\rho E) \right)}{\partial_{x} \left( \rho E \right)}$$
(13c)

$$\partial_{t}\epsilon + \frac{4}{3}\partial_{x}\left(u\epsilon\right) = \frac{u}{3}\partial_{x}\epsilon + \partial_{x}\left(\frac{c}{3\sigma_{+}}\partial_{x}\epsilon\right) + \sigma_{a}c\left(aT^{4} - \epsilon\right) + \frac{\partial_{x}\left(\kappa\partial_{x}\epsilon\right)}{\partial_{x}\left(\kappa\partial_{x}\epsilon\right)}$$
(13d)

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### Equilibrium Diffusion Limit

#### non-dimensionalization:

$$\partial_{t'}(\rho') + \partial_{x'}(\rho'u') = \mathbb{V}_{\infty}\partial_{x}\left(\kappa'\partial_{x'}\rho'\right) \tag{14a}$$

$$\partial_{t'} \left( \rho' u' \right) + \partial_{x'} \left( \rho u^{2'} + P' + \mathbb{P}_{\infty} \frac{\epsilon'}{3} \right) = \mathbb{V}_{\infty} \partial_{x'} \left( \kappa' \partial_{x'} (\rho' u') \right) \tag{14b}$$

$$\partial_{t'} \left( \rho' E' \right) + \partial_{x'} \left[ u' \left( \rho' E' + P' \right) \right] = -\mathbb{P}_{\infty} \frac{u'}{3} \partial_{x'} \epsilon'$$

$$- \mathbb{P}_{\infty} \mathbb{C}_{\infty}^{-1} \mathbb{L}_{\infty} \left( \sigma'_{t} - \mathbb{L}_{s,\infty} \sigma'_{s} \right) \left( T'^{,4} - \epsilon' \right) + \mathbb{V}_{\infty} \partial_{x'} \left( \kappa' \partial_{x'} (\rho' E') \right)$$
 (14c)

$$\partial_{t'}\epsilon' + \frac{4}{3}\partial_{x'}\left(u'\epsilon'\right) = \frac{u'}{3}\partial_{x'}\epsilon' + \mathbb{L}_{\infty}^{-1}\mathbb{C}_{\infty}^{-1}\partial_{x'}\left(\frac{1}{3\sigma'_{t}}\partial_{x'}\epsilon'\right) + \mathbb{C}_{\infty}^{-1}\mathbb{L}_{\infty}\left(\sigma'_{t} - \mathbb{L}_{s,\infty}\sigma'_{s}\right)\left(T'^{,4} - \epsilon'\right) + \mathbb{V}_{\infty}\partial_{x'}\left(\kappa'\partial_{x'}\epsilon'\right)$$
(14d)

#### non-dimensional parameters

$$\begin{split} \mathbb{L}_{\infty} &= L_{\infty} \sigma_{t,\infty} = \mathcal{O}(\varepsilon^{-1}), \ \mathbb{L}_{s,\infty} = \frac{\sigma_{s,\infty}}{\sigma_{t,\infty}} = \mathcal{O}(\varepsilon), \ \mathbb{C}_{\infty} = \frac{c_{m,\infty}}{c} = \mathcal{O}(\varepsilon) \\ \mathbb{P}_{\infty} &= \frac{a T_{\infty}^4}{\rho_{\infty} c_{m,\infty}^2} = \mathcal{O}(1), \ \mathbb{V}_{\infty} = \frac{\kappa_{\infty}}{c_{m,\infty} L_{\infty}} = \mathcal{O}(1) \end{split}$$

The variables are expanded in a power series in arepsilon

#### Equilibrium Diffusion Limit results:

$$\partial_t \rho_0 + \partial_x \left(\rho u\right)_0 = \frac{\partial_x \left(\kappa \partial_x \rho\right)_0}{\left(\kappa \partial_x \rho\right)_0} \tag{15a}$$

$$\partial_{t} (\rho u)_{0} + \partial_{x} (\rho u^{2} + P^{*})_{0} = \frac{\partial_{x} (\kappa \partial_{x} (\rho u))_{0}}{(15b)}$$

$$\partial_{x} (\rho E^{*})_{0} + \partial_{x} \left[ u \left( \rho E^{*} + P^{*} \right) \right]_{0} = \partial_{x} \left( \frac{1}{3\sigma_{t}} \partial_{x} T^{4} \right)_{0} + \frac{\partial_{x} \left( \kappa \partial_{x} \rho E^{*} \right)_{0}}{(15c)}$$

$$P^* = P + \mathbb{P}_{\infty} \frac{T^4}{3}$$
 and  $E^* = E + \mathbb{P}_{\infty} \frac{T^4}{\rho}$ 

#### Leading order of entropy

$$s_0(\rho, e) = s_{Euler,0}(\rho, e) + \frac{4}{3} \frac{T_0^3}{\rho_0}$$
 (16)

We recover the EDL results (Lowrie/Morel, JQSRT, 2001).

Viscous regularization scales adequately with  $V_{\infty} = \mathcal{O}(1)$ .

#### Numerical solution

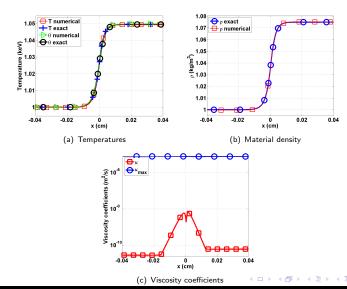
- spatial discretization: CFEM
- temporal discretization: fully implicit (BDF2)
- solution technique: JFNK with finite-difference approximation of the Jacobian as preconditioner
- semi-analytical solutions provided by Jim Ferguson (LANL)
- Two sets of results presented today:
  - with constant opacities (Mach 1.05, 2, 5, 50)
  - 2 with temperature-dependent opacities (Mach 3)

#### Additional results in the back-up slides

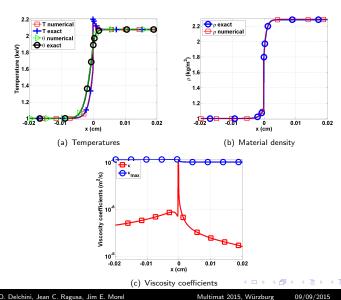
Second-order convergence for manufactured solutions in

- streaming limit
- diffusion limit

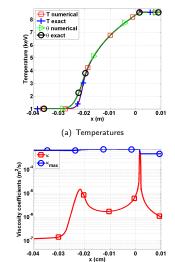
# Steady-state solution for Mach 1.05



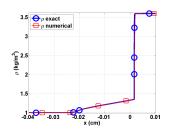
# Steady-state solution for Mach 2

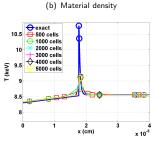


# Steady-state solution for Mach 5

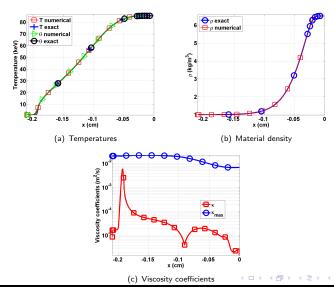


(c) Viscosity coefficients



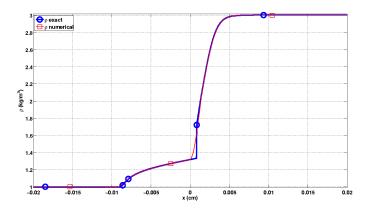


# Steady-state solution for Mach 50

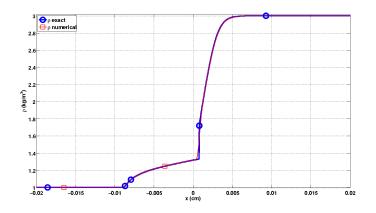


# Steady-state solution for Mach 3: density, 500 cells

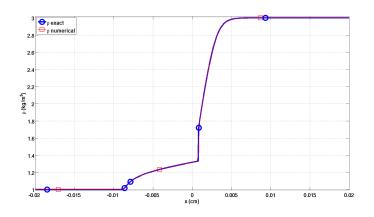
Now, results with temperature-dependent opacities:



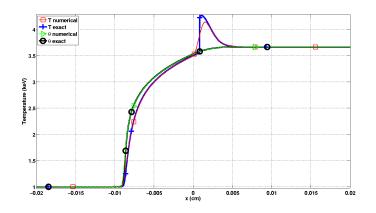
### Steady-state solution for Mach 3: density, 1000 cells



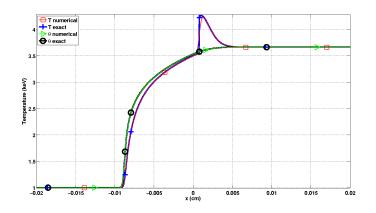
### Steady-state solution for Mach 3: density, 2000 cells



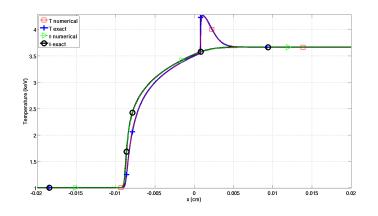
# Steady-state solution for Mach 3: temperature, 500 cells



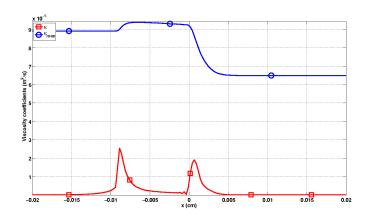
# Steady-state solution for Mach 3: temperature, 1000 cells



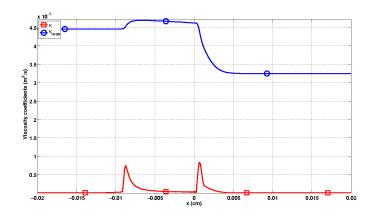
# Steady-state solution for Mach 3: temperature, 2000 cells



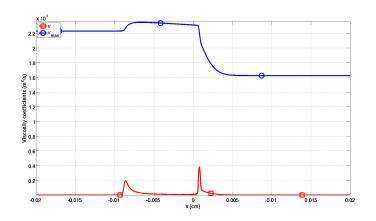
### Steady-state solution for Mach 3: viscosity, 500 cells



### Steady-state solution for Mach 3: viscosity, 1000 cells



### Steady-state solution for Mach 3: viscosity, 2000 cells



#### Conclusions

- Extended the entropy-viscosity method to the <u>full</u> Grey Radiation-Hydrodynamic equations.
- Verified the entropy minimum principle for the regularized equations GRHD.
- Viscous regularization scales appropriately in the equilibrium-diffusion limit.
- Numerical results are in excellent agreement with semi-analytical solutions.

#### Outlook

- Multi-D.
- Replace radiation diffusion with  $S_n$  radiation transport.
- Switch solution technique to IMEX (implicit for radiation, explicit for hydro).
- Other spatial discretization (DGFEM).
- FCT
  - → poster tomorrow on FCT for radiation transport

### Seven-equation two-phase flow model

#### with viscous regularization

$$\frac{\partial \alpha_k A}{\partial t} + A \vec{u}_{int} \cdot \vec{\nabla} \alpha_k - A \mu_P (P_k - P_j) = \vec{\nabla} \cdot \vec{l}_k$$
 (17a)

$$\frac{\partial \left(\alpha \rho\right)_{k} A}{\partial t} + \vec{\nabla} \cdot \left[ (\alpha \rho \vec{u})_{k} A \right] = \vec{\nabla} \cdot \vec{f}_{k}$$
(17b)

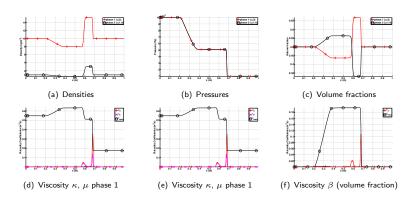
$$\frac{\partial (\alpha \rho \vec{u})_k A}{\partial t} + \vec{\nabla} \cdot \left[ \alpha_k A (\rho \vec{u} \otimes \vec{u} + P \mathbb{I})_k \right] - P_{int} A \vec{\nabla} \alpha_k + P_k \alpha_k \vec{\nabla} A \\
- A \lambda_u (\vec{u}_j - \vec{u}_k) = \vec{\nabla} \cdot g_k \quad (17c)$$

$$\frac{\partial (\alpha \rho E)_k A}{\partial t} + \vec{\nabla} \cdot \left[ \alpha_k \vec{u}_k A (\rho E + P)_k \right] - P_{int} A \vec{u}_{int} \cdot \vec{\nabla} \alpha_k + \bar{P}_{int} A \mu_P (P_k - P_j) \\
- A \lambda_u \vec{u}_{int} \cdot (\vec{u}_j - \vec{u}_k) = \vec{\nabla} \cdot \left( \vec{h}_k + \vec{u}_k \cdot g_k \right) \tag{17d}$$

#### Viscous fluxes:

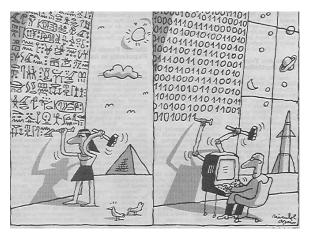
$$\begin{split} \vec{l}_k &= \beta_k A \vec{\nabla} \alpha_k \,, \quad \vec{f}_k = \alpha_k A \kappa_k \vec{\nabla} \rho_k + \rho_k \vec{l}_k \\ \mathbb{g}_k &= \alpha_k A \mu_k \rho_k \vec{\nabla}^s \vec{u}_k + \vec{f}_k \otimes \vec{u}_k \,, \quad \vec{h}_k = \alpha_k A \kappa_k \vec{\nabla} \left( \rho \mathbf{e} \right)_k - \frac{\|\vec{u}_k\|^2}{2} \vec{f}_k + (\rho \mathbf{e})_k \vec{l}_k \end{split}$$

### 7-equation two-phase flow: shock tube with large relaxation



### Thank you

Thanks to Jim Ferguson (LANL) for the semi-analytical solutions. Thanks to Jean-Luc Guermond and Bojan Popov (Texas A&M) for fruitful discussions.



# Why an upper bound for viscosity?

Large entropy residual in shocks  $\longrightarrow$  large entropy viscosity  $\mu_{\mathrm{e}}$ 

There is such a thing as too much of a good thing ... Il ne faut point être plus royaliste que le Roy

#### Upper bound for $\mu$

First-order upwind scheme is monotone but over dissipative. We should not exceed the amount of stabilization that such a scheme provides.

upwinding = centered approximation (Galerkin) - numerical diffusion Example: linear advection  $\partial_t u + \beta \partial_x u = 0$ 

$$\beta \frac{u_{i} - u_{i-1}}{h} = \beta \frac{u_{i+1} - u_{i-1}}{2h} - \frac{\beta h}{2} \frac{u_{i+1} - 2u_{i} + u_{i-1}}{h^{2}}$$
(18)

So, the dissipative term is  $\frac{\beta h}{2}\partial_{\rm xx} u$  and the first-order viscosity is  $\frac{\beta h}{2}$ 

#### First-order viscosity

- scalar conservation law:  $\frac{h}{2}|f'(u)|$
- system:  $\frac{h}{2}$  max (eig( $\partial_u f$ ))

### Manufactured solution: equilibrium-diffusion limit

Table:  $L_2$  norms of the error for the equilibrium diffusion limit case using a manufactured solution.

# of cells	time step size (sh)	ρ	ratio	hoE	ratio
20	$10^{-1}$	0.590766	NA	1.333774	NA
40	5 10 <sup>-2</sup>	0.290626	2.03	0.478819	2.79
80	$2.5 \ 10^{-2}$	0.0959801	3.021	0.154119	3.11
160	$1.25 \ 10^{-2}$	0.02593738	3.70	0.0405175	3.80
320	$6.25 \ 10^{-3}$	$6.471444 \ 10^{-3}$	4.00	$9.90446 \ 10^{-3}$	4.09
640	$3.125 \ 10^{-3}$	$1.584158 \ 10^{-3}$	4.01	$2.44727 \ 10^{-3}$	4.04
# of cells	time step size (sh)	$\epsilon$	ratio	hou	ratio
20	$10^{-1}$	0.00650085	NA	0.910998	NA
40	$5 \ 10^{-2}$	0.00124983	5.20	0.4090946	2.23
80	$2.5 \ 10^{-2}$	0.000262797	4.76	0.125943	3.25
160	$1.25 \ 10^{-2}$	$6.17726 \ 10^{-5}$	4.25	$3.381042 \ 10^{-3}$	3.72
320	$6.25 \ 10^{-3}$	$1.509184 \ 10^{-5}$	4.09	$8.373657 \ 10^{-3}$	4.04
640	$3.125 \ 10^{-3}$	$3.72548 \ 10^{-6}$	4.05	$2.070538 \ 10^{-3}$	4.04

### Manufactured solution: streaming limit

Table:  $L_2$  norms of the error for the streaming limit case using a manufactured solution.

# of cells	time step size (sh)	ρ	ratio	hoE	ratio
20	$10^{-1}$	$1.4373 \ 10^{-2}$	NA	$5.88521 \ 10^{-1}$	NA
40	5. 10 <sup>-2</sup>	$3.760208 \ 10^{-3}$	3.82	$1.4244 \ 10^{-1}$	4.13
80	$2.5 \ 10^{-2}$	$9.91724 \ 10^{-4}$	3.79	$3.2047 \ 10^{-2}$	4.44
160	$1.25 \ 10^{-2}$	$2.4455 \ 10^{-4}$	4.06	$7.4886 \ 10^{-3}$	4.28
320	$6.25 \ 10^{-3}$	$6.280715 \ 10^{-5}$	3.89	$1.82327 \ 10^{-3}$	4.11
640	$3.125 \ 10^{-3}$	$1.57920 \ 10^{-5}$	3.98	$4.50463 \ 10^{-4}$	4.05
1280	$1.5625 \ 10^{-4}$	$3.96096 \ 10^{-6}$	3.99	$1.12061 \ 10^{-4}$	4.02
# of cells	time step size (sh)	$\epsilon$	ratio	hou	ratio
20	$10^{-1}$	$3.82001 \ 10^{-1}$	NA	$2.354671 \ 10^{-3}$	NA
40	5. 10 <sup>-2</sup>	$1.21500 \ 10^{-1}$	3.14	$6.138814 \ 10^{-4}$	3.84
80	$2.5 \ 10^{-2}$	$3.27966 \ 10^{-2}$	3.70	$1.74974 \ 10^{-4}$	3.51
160	$1.25 \ 10^{-2}$	$8.38153 \ 10^{-3}$	3.91	$3.61297 \ 10^{-5}$	4.84
320	$6.25 \ 10^{-3}$	$2.10925 \ 10^{-3}$	3.97	$9.03866 \ 10^{-6}$	3.99
640	$3.125 \ 10^{-3}$	$5.28472 \ 10^{-4}$	3.99	$2.25649 \ 10^{-6}$	4.01
1280	$1.5625 \ 10^{-4}$	$1.322268 \ 10^{-4}$	3.99	$5.69984 \ 10^{-7}$	3.95